

PRELIMINARY DRAINAGE REPORT
MONUMENT CLUB CONDOMINIUMS AT TROON NORTH

For

Monument Club Condominiums, Troon North LCC

A Portion of the

SE 1/4, SEC. 29, T5N, R5E
Of the Gila & Salt River Base and Meridian,
City of Scottsdale
Maricopa County, Arizona

Assessor's Parcel Number 216-72-585 B

Graham Engineering & Surveying Job Number 07-169

Prepared for:

RD Architecture
7440 E Karen Drive
Scottsdale, AZ 85260
Contact
Rick Daugherty
(480) 607-3337

Prepared by:

GRAHAM ENGINEERING & SURVEYING, INC.
Post Office Box 1243
Carefree, Arizona 85377
Office (480) 488-4393
Facsimile (480) 488-2488

September 28, 2007



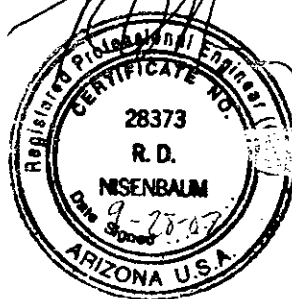
7/28

CASE DRAINAGE

4719-07

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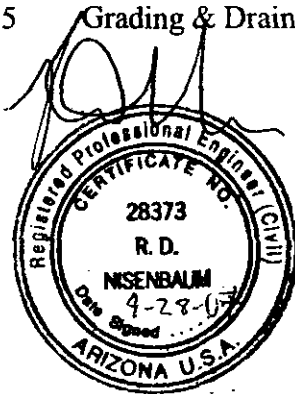
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1.0 Introduction

1.1 SCOPE

Provided herein are offsite and onsite hydrologic, hydraulic and detention analyses/designs. No off-site improvements are included in the design and specific surface drainage analyses but rather the pre-developed off-site, Scottsdale 2-foot interval topographic information is the basis for the HEC-1 offsite hydrology that is used for channel water surface profile elevation estimates.

This preliminary report does not include ground water hydrology or hydrogeology. Any issues that arise must be addressed by an engineering firm or an engineer whose specialty covers ground water issues. Graham Engineering & Surveying, Inc. will be held harmless for any damages as a result of ground water issues.

1.2 SITE DESCRIPTION

Monument Club Condominiums at Troon North is located to the northwest of 103rd St. and Dynamite Boulevard. The cadastral description is "That Portion of the Southeast one-quarter of Section 29, Township 5 North, Range 5 East of the Gila & Salt River Base and Meridian, City of Scottsdale, Maricopa County, Arizona. For the full legal description that is a meets and bounds description see the plate labeled figure The Assessor's Parcel Number is 216-72-585 B. The Graham Engineering & Surveying, Inc.TM Job Number is 07-169. This project gross area is 2.5574 acres.

Access to the site is provided to this lot off White Feather Lane being a paved local street with an asphalt surface and 4-inch concrete rolled curbs on either edge.

The site geography is typical of upper Sonoran Desert alluvial fan terrain. The slope is about 1.5% to the south and southwest with decomposed granite with various outcroppings of granite boulders and some granite latholith intrusion caps.

The predominant surface soil 'Gran', 'Wickenburg' and 'Rock Outcrop' and classified as hydrologic soil group 'D' according to the Aguila-Carefree Soil Study (United States Department of Agriculture, Soil Conservation Service, current publication).

2.0 Existing Conditions

2.1 OFF-SITE

This project is located adjacent to the Monument Golf Course at Troon which was not a mass graded development. The surface is covered with small braided washes that traverse down-slope to the south and southwest. A large wash runs along the northwest portion of this site. The tributary area is 330 acres of sparsely developed up slope residential homes.

2.2 ON-SITE

The proposed development consists of undeveloped sonoran desert. One poorly defined wash exists on the east half of the property and drains from the northeast to the southwest. Another poorly defined wash exists in the southwest section of the property and generally drains to the west into a large defined wash. The large off-site wash runs along the northwest portion of this site, between the roadway and the undeveloped desert area.

3.0 Hydrology

2.1 OFF-SITE

The off-site hydrology was estimated using HEC-1 for the entire off-site watershed. Individual basins were not delineated for this preliminary drainage report (see Appendix A). The 100-year, 24-hour S rainfall graph, (Phoenix Mountain, foothills area runoff basin) is used to model the off-site watershed. The results of which is a peak flow of 779 cfs.

2.2 ON-SITE

The off-site hydrology that affects the retention was estimated using HEC-1 for the entire off-site watershed for the water surface profile in HEC-RAS. Individual basins were not delineated for this preliminary drainage report (see Appendix A). The 100-year, 2-hour MCFCD rainfall graph (Phoenix Mountain, foothills area runoff basin) is used to model the off-site watershed. The results of which is a peak flow of 486 cfs.

An on-site hydrology estimate for the minor flow on this site is the area to the east of the property designated as wash W2 (See Figure 7) is estimated using the City of Scottsdale Rational Method with an added frequency factor. The City of Scottsdale Rational Method Form 2.2-18 is found in Appendix A. The resultant flow quantity estimated using the rational worksheet for the 100-year storm event is 34 cfs.

Pre and post on-site runoff was estimated to determine the size of the detention system and discharge rate. Flow-rates were estimated using the City of Scottsdale Rational Method Form 2.2-18. Two drainage basins, DA-1 and DA-2, were delineated for the pre-development surface runoff (see Figure 7). Both basins are comprised of nearly impervious soils (see Figure 4 and above description). A Runoff Coefficient of 0.78 was used for this soil. DA-1 pre-development condition (pre) has an area

of 1.2 acres and the resultant flow quantity estimated using the COS rational worksheet for the 100-year storm event is 11 cfs. This flow is discharged to the south to White Feather Ln. at concentration point CP1 (see Figure 7). DA-2 pre has an area of 0.45 acres and the resultant flow quantity estimated using the COS rational worksheet for the 100-year storm event is 4 cfs. This flow is discharged to west into a large wash at concentration point CP2 (see Figure 7).

Two drainage basins, DA-1 and DA-2 post development condition (post), were delineated (see Figure 8). A Runoff Coefficient of 0.95 is used for these basins for the moderately high content of impervious surfaces. DA-1 post has a total area of 0.68 acres and the resultant flow quantity estimated using the COS rational worksheet for the 100-year storm event is 7 cfs (see Figure 8). This flow consists entirely of roof runoff. Roof runoff will be conveyed from roof downspouts directly to an underground detention system. The reduction of flow from this area due to detention is 1 cfs from the peak flow. The peak flow occurs at a different time than the off-site peak and hence the metering will not increase the peak flow of the main channel that flows through the site on the northwest portion of this project.

DA-2 post has a total area of 0.94 acres and the resultant flow quantity estimated using the COS rational worksheet for the 100-year storm event is 10 cfs (see Figure 8). This flow consists of general ground runoff. Roof runoff will be conveyed from roof downspouts directly to an underground detention system. The reduction of flow from this area due to detention is 1 cfs from the peak flow. The peak flow occurs at a different time than the off-site peak and hence the metering will not increase the peak flow of the main channel that flows through the site on the northwest portion of this project.

4.0 Hydraulics

Hydraulic analysis supports the grading plan of which the intention is to direct storm water runoff around or away from all proposed building structures. Storm water runoff across the property is graded to maintain historic drainage patterns entering and exiting the site in a similar manner to the pre-improvement drainage patterns. Field investigations verified storm water runoff patterns and topographic mapping accuracy.

The water surface profile analysis using HEC-RAS version 3.1.1 uses mapping from two sources:

1. "Wash W-1" City of Scottsdale 2-foot contour interval
2. Local topographic information collected by Graham Engineering and Surveying, Inc, survey crews.

The vertical datum for source 1 and source 2 is based on the NAVD 88.

5.0 Erosion Set-Back

A level one procedure for estimation of channel degradation depth was used. This level of analysis provides an initial estimate of the potential scour depth to consider for design structures to be placed near the banks of a channel. Level I analysis requires the peak discharge associated with the 100-

year flood. The total scour depth is the combination of general degradation and long term degradation. Level I erosion set back $\text{SQRT}(779) = 28$ feet.

5.0 Flood Zone Information

See FIRM map (Figure 2) for flood zone information. The finish floor elevation is set one foot above the HEC-RAS water surface elevation being 2548.25.

FIGURES

SOILS SURVEY OF AGUILA-CAREFREE AREA

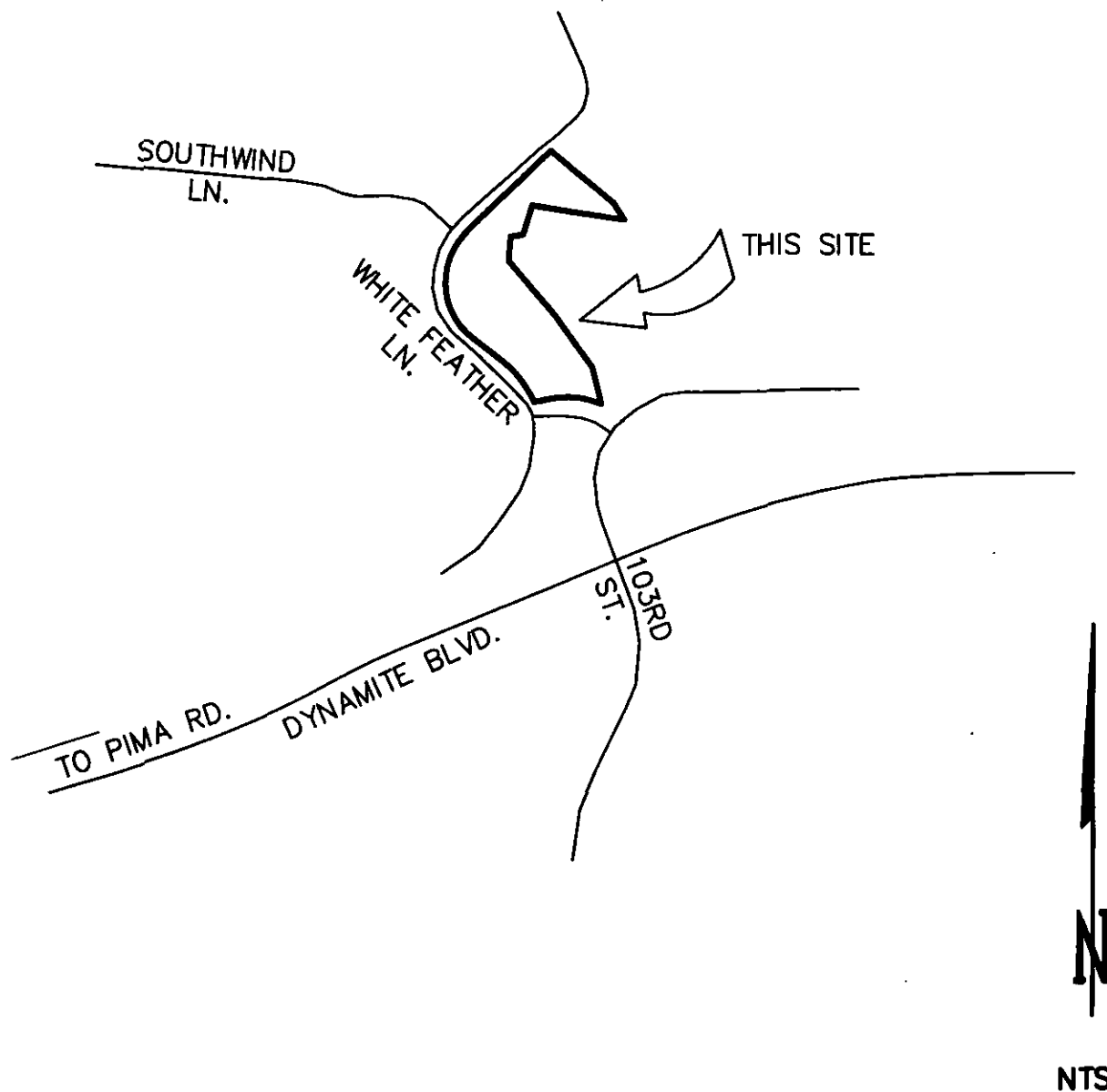
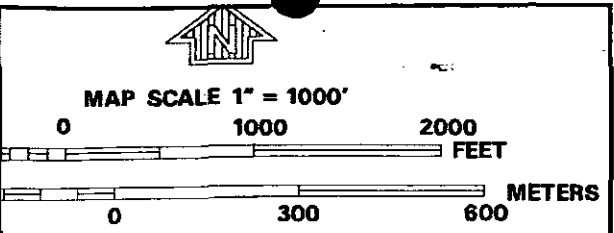


FIGURE 1

GRAHAM ENGINEERING & SURVEYING INC.
Civil Engineers & Land Surveyors
P.O. BOX 1243, Carefree, Arizona 85377
(480) 488-4393
DATE: 09/27/07
JOB # 07-169



NFIP

PANEL 1255G


FIRM
FLOOD INSURANCE RATE MAP
MARICOPA COUNTY,
ARIZONA
AND INCORPORATED AREAS

PANEL 1255 OF 4350
(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

CONTAINS

COMMUNITY	NUMBER	PANEL	SUFFIX
SCOTTSDALE, CITY OF	049072	1255	5

Notice to User: The map shown below should be used when placing new orders; the Community Map shown above should be used on insurance applications for the subject community.

 **MAP NUMBER**
04013C1255G
MAP REVISED
SEPTEMBER 30, 2005
Federal Emergency Management Agency

This is an official copy of a portion of the above referenced flood map. It was extracted using F-MIT On-Line. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For the latest product information about National Flood Insurance Program flood maps check the FEMA Flood Map Store at www.msc.fema.gov

FIGURE 2

SOILS SURVEY OF AGUILA-CAREFREE AREA



GRAHAM ENGINEERING & SURVEYING INC.
Civil Engineers & Land Surveyors
P.O. BOX 1243, Carefree, Arizona 85377
(480) 488-4393
DATE: 09/27/07
JOB # 07-169

PRE-DEVELOPMENT RUNOFF

A PORTION OF THE SE 1/4, SEC. 29, T5N, R5E
OF THE GILA & SALT RIVER BASE & MERIDIAN,
CITY OF SCOTTSDALE,
MARICOPA COUNTY, ARIZONA.

LEGEND:

- DA1 DRAINAGE AREA
- ← FLOW ARROW
- CP2 CONCENTRATION POINT
- DRAINAGE AREA BOUNDARY

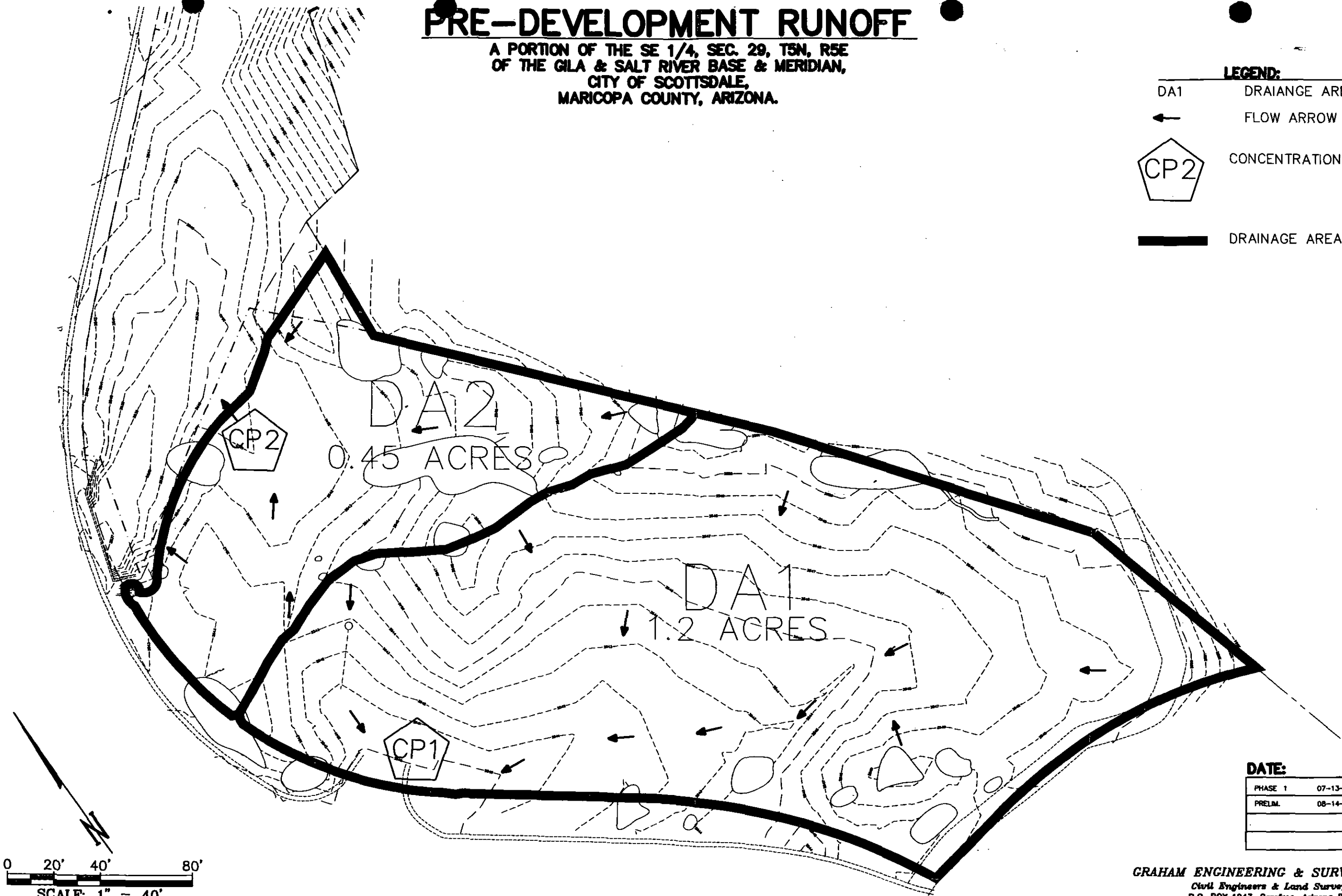


FIGURE 7

DATE:

PHASE 1	07-13-07	CAM
PRELIM.	08-14-07	PS

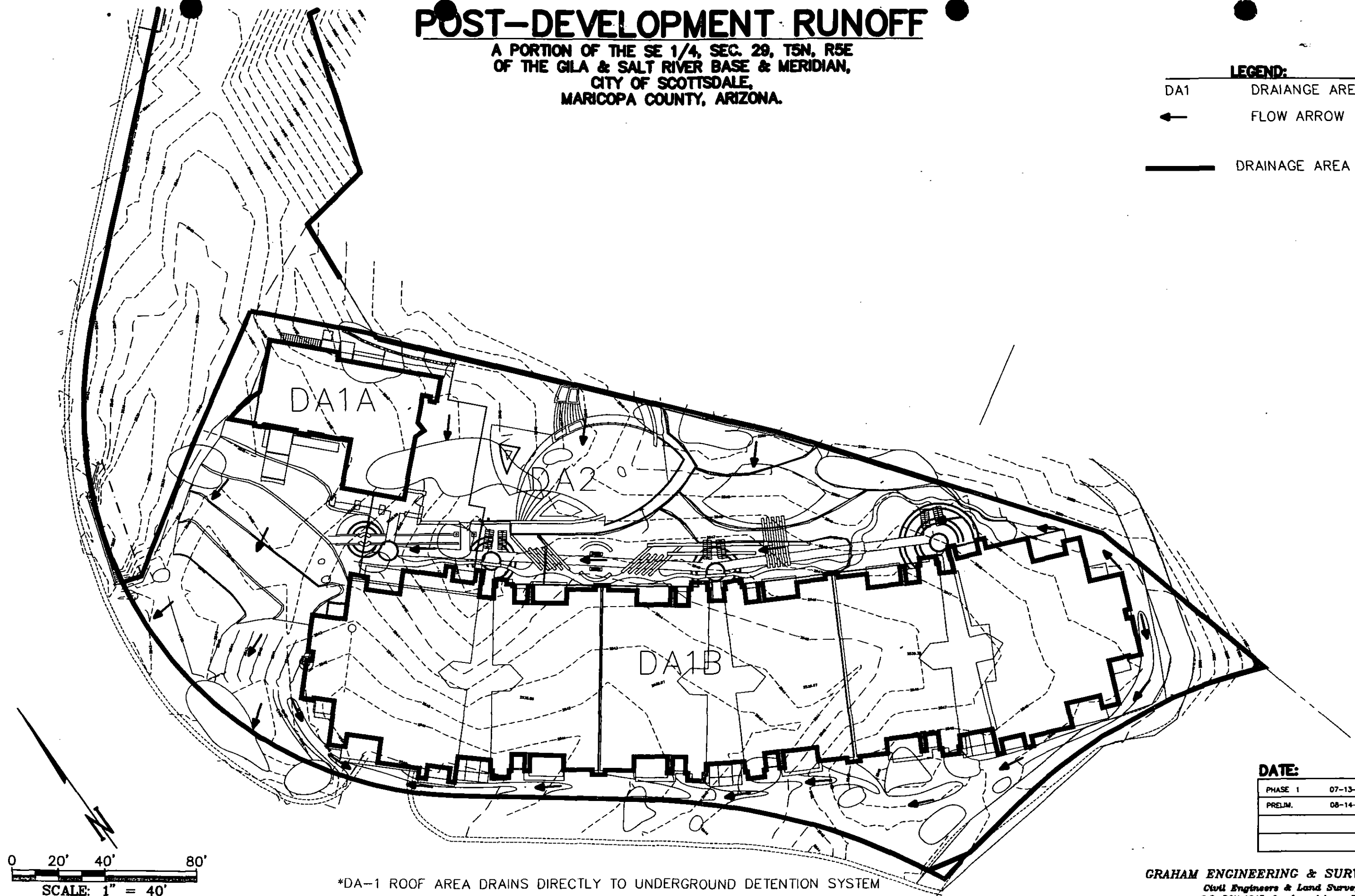
GRAHAM ENGINEERING & SURVEYING INC.
Civil Engineers & Land Surveyors
P.O. BOX 1243, Carefree, Arizona 85377
(480) 488-4393

POST-DEVELOPMENT RUNOFF

A PORTION OF THE SE 1/4, SEC. 29, T5N, R5E
OF THE GILA & SALT RIVER BASE & MERIDIAN,
CITY OF SCOTTSDALE,
MARICOPA COUNTY, ARIZONA.

LEGEND:

- DA1 DRAINAGE AREA
← FLOW ARROW
— DRAINAGE AREA BOUNDARY



DATE:

PHASE 1	07-13-07	CAM
PRELIM.	08-14-07	PS

*DA-1 ROOF AREA DRAINS DIRECTLY TO UNDERGROUND DETENTION SYSTEM

GRAHAM ENGINEERING & SURVEYING INC.

Civil Engineers & Land Surveyors
P.O. BOX 1243, Carefree, Arizona 85377
(480) 488-4393

PART OF THE SE 1/4, SEC. 29, T5N, R5E, SHT. 1 OF 1, JOB #07-169

FIGURE 8

Appendix A
Hydrology Backup

CITY OF SCOTTSDALE
HYDROLOGIC DESIGN DATA RECORD
RATIONAL METHOD

LOCATION DATA

EXHIBIT B 1

PROJECT: GRADING/DRAINAGE CONCENTRATION POINT: EXIT FLOW
LOCATION: 10200 E. Dynamite Blvd.
PROJECT NO.: 07-169 STATION: _____
NAME OF STREAM/WATERSHED: Pre-Development Onsite Flows

DESIGN DATA

DESIGN FREQUENCY:

2	5	10	25	50	100
---	---	----	----	----	-----

 YEARS
DRAINAGE AREA: DA1 1.20 ACRES
DA2 0.45
TOTAL (A) Individual areas considered separately
DRAINAGE LENGTH: 199 FEET
ELEVATION: _____
TOP OF DRAINAGE AREA: 2554 FEET
AT STRUCTURE 2540 FEET
DRAINAGE AREA SLOPE: 7.0 PERCENT
HYDROLOGIC SOIL GROUP: D Gran
Wickenburg

DESIGN COMPUTATIONS

FREQUENCY FACTOR (F):

1.00	1.00	1.00	1.10	1.20	1.25
------	------	------	------	------	------

TIME OF CONCENTRATION: T_c 5 MINUTES
RAINFALL INTENSITY (I):

					9.25
--	--	--	--	--	------

 INCHES/HOUR
(Figure 2.2-13)
RUNOFF COEFFICIENT [C]: 0.78
WEIGHTED RUNOFF COEFFICIENT (C_w): C_w Individual areas considered separately
PEAK DISCHARGE $Q_p = C_w I A (F)$: CP1 (EXIT FLOW)

					11
--	--	--	--	--	----

 cfs
CP2 (EXIT FLOW)

					4
--	--	--	--	--	---

 cfs

COMPUTED BY: NATHAN WYLLIE, EIT DATE: 9/25/2007
CHECKED BY: RALPH NISENBAUM, P.E. DATE: 9/26/2007

FIGURE 2.2-18
Hydrologic Design Data Record

CITY OF SCOTTSDALE
HYDROLOGIC DESIGN DATA RECORD
RATIONAL METHOD

LOCATION DATA

EXHIBIT B 2

PROJECT: GRADING/DRAINAGE CONCENTRATION POINT: EXIT FLOW
LOCATION: 10200 E. Dynamite Blvd.
PROJECT NO.: 07-169 STATION: _____
NAME OF STREAM/WATERSHED: Post-Development Onsite Flows

DESIGN DATA

DESIGN FREQUENCY:

2	5	10	25	50	100
---	---	----	----	----	-----

 YEARS

DRAINAGE AREA: DA1 0.68 ACRES
DA2 0.94 ACRES

TOTAL (A) Individual areas considered separately

DRAINAGE LENGTH: 199 FEET
ELEVATION: _____
TOP OF DRAINAGE AREA: 2554 FEET
AT STRUCTURE 2540 FEET
DRAINAGE AREA SLOPE: 7.0 PERCENT
HYDROLOGIC SOIL GROUP: D Gran
Wickenburg

DESIGN COMPUTATIONS

FREQUENCY FACTOR (F):

1.00	1.00	1.00	1.10	1.20	1.25
------	------	------	------	------	------

TIME OF CONCENTRATION: T_c 5 MINUTES

					9.25
--	--	--	--	--	------

 INCHES/HOUR
(Figure 2.2-13)

RAINFALL INTENSITY (I): _____

RUNOFF COEFFICIENT [C]: Roof and Asphalt 0.95

WEIGHTED RUNOFF COEFFICIENT (C_w): Individual areas considered separately

PEAK DISCHARGE $Q_p = C_w I A(F)$: DA1 (EXIT FLOW)

					7
--	--	--	--	--	---

 cfs
DA2 (EXIT FLOW)

					10
--	--	--	--	--	----

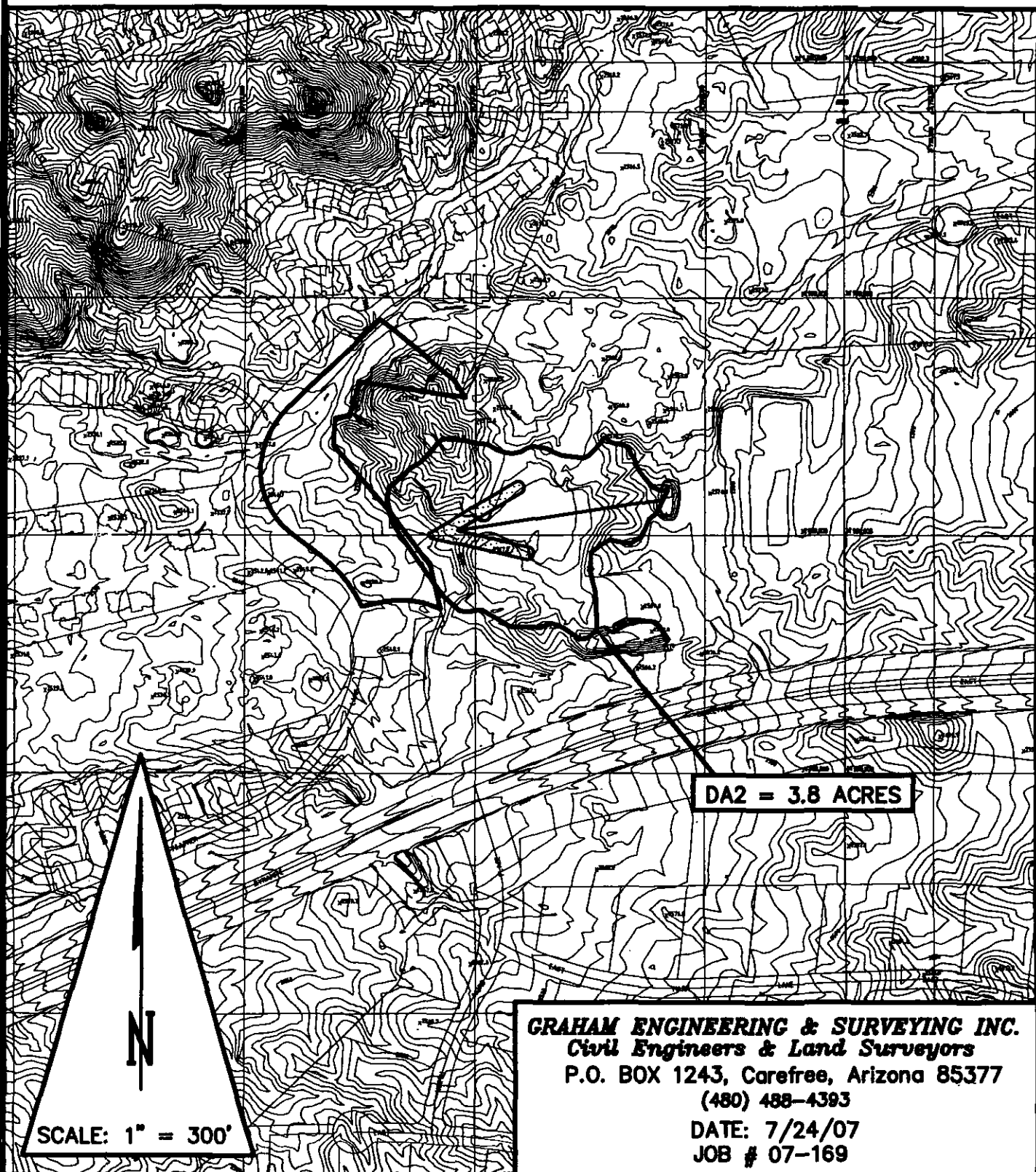
 cfs

COMPUTED BY: NATHAN WYLLIE, EIT DATE: 9/25/2007
CHECKED BY: RALPH NISENBAUM, P.E. DATE: 9/26/2007

FIGURE 2.2-18

Hydrologic Design Data Record

EXHIBIT "A"
DRAINAGE AREA DELINEATION
MONUMENT CLUB



CITY OF SCOTTSDALE
HYDROLOGIC DESIGN DATA RECORD
RATIONAL METHOD

LOCATION DATA

EXHIBIT B2

PROJECT: GRADING/DRAINAGE CONCENTRATION POINT: EXIT FLOW
LOCATION: _____
PROJECT NO.: 07-169 STATION: _____
NAME OF STREAM/WATERSHED: DA-2 IN GRADING/DRAINAGE PLAN

DESIGN DATA

DESIGN FREQUENCY:

2	5	10	25	50	100
---	---	----	----	----	-----

 YEARS
DRAINAGE AREA: DA2

3.8

 ACRES

TOTAL (A) Individual areas considered separately
DRAINAGE LENGTH: 553 FEET
ELEVATION: _____
TOP OF DRAINAGE AREA: 2588 FEET
AT STRUCTURE 2554 FEET
DRAINAGE AREA SLOPE: 6.1 PERCENT
HYDROLOGIC SOIL GROUP: D Gran
Wickenburg

DESIGN COMPUTATIONS

FREQUENCY FACTOR (F):

1.00	1.00	1.00	1.10	1.20	1.25
------	------	------	------	------	------

TIME OF CONCENTRATION: T_c 5 MINUTES
RAINFALL INTENSITY (I):

					9.25
--	--	--	--	--	------

 INCHES/HOUR
(Figure 2.2-13)
RUNOFF COEFFICIENT (C): 0.78
(FOR R4-R)
SEE NEXT PAGE

WEIGHTED RUNOFF COEFFICIENT (C_w): C_w Individual areas considered separately
PEAK DISCHARGE Q_p = C_wIA(F): DA2

					34

 cfs

COMPUTED BY: Nathan Wyllie, EIT DATE: 9/25/2007
CHECKED BY: Ralph Nissembaum, P.E. DATE: 9/26/2007

FIGURE 2.2-18

Hydrologic Design Data Record

Runoff Coefficients

Land Use	"C" Value Hydrologic Soil Group		
	B	C	D
Composite Area-wide Values			
Commercial and industrial areas:	0.9		
Residential areas-single family (average lot size):			
R1-1-190:	0.33	0.50	0.58
R1-130:	0.35	0.51	0.59
R1-70:	0.37	0.52	0.60
R1-43:	0.38	0.55	0.61
R1-35 (35,000 sq. ft./lot):	0.40	0.56	0.62
R1-18 (18,000 sq. ft./lot):	0.43	0.58	0.64
R1-10 (10,000 sq. ft./lot):	0.47	0.62	0.67
R1-7 (7,000 sq. ft./lot):	0.51	0.64	0.70
Townhouses (R-2, R-4):	0.63	0.74	0.78
Apartments and condominiums (R-3, R-5):	0.76	0.83	0.87
Specific Surface Type Values			
Paved streets or parking lot (concrete or asphalt), roofs, driveways, etc.	0.95		
Lawns, golf courses, and parks (grassed areas):	0.33	0.56	0.66
Undisturbed natural desert or desert landscaping (no impervious weed barrier):	0.31	0.48	0.56
Desert landscaping (with impervious weed barrier)	0.83	0.83	0.83
Mountain terrain - slopes greater than 10%:	0.70	0.70	0.70
Agricultural areas (Flood Irrigated Fields):	0.20	0.20	0.20

FIGURE 2.2-17

Runoff Coefficients "C" for use with the Rational Formula

Graham Engineering & Surveying, Inc.
POB 1243
7406 E. Nonchalant, Carefree, AZ 85377
Job Number: 07-169

28-Sep-07
Ralph Nisenbaum, PE
HEC-1 Input Parameters

INPUT PARAMETERS FOR BOTH S GRAPH AND MCFCD DISTRIBUTION

INPUT PARAMETER	VALUE & UNITS
AREA	0.517 SQ-MI
EVENT	100-YEAR, 24-HR
STORM SIZE	0.517 SQ-MI
STREAM LENGTH	2.029 MILES
LENGTH TO CA	0.918 MILES
SLOPE	152 FT./MI.
K _n ROUGHNESS	0.033
IA	0.25
DTHETA	0.1
PSIF	10
XKSAT	0.02
RTIMP	25
100 Yr. Precipitations	
	24-Hr. = 4.60
	2-Hr. = 2.75

S DISTRIBUTION LAG TIME USED IS 28 MINUTES

MCFCD DISTRIBUTION LAG TIME USED IS 23.17 MINUTES

Note: see the HEC-1 output files for more detailed information.

 *
 *
 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * U.S. ARMY CORPS OF ENGINEERS *
 * JUN 1998 *
 * HYDROLOGIC ENGINEERING CENTER *
 * VERSION 4.1 *
 * 609 SECOND STREET *
 *
 * DAVIS, CALIFORNIA 95616 *
 * RUN DATE 27SEP07 TIME 19:55:06 *
 * (916) 756-1104 *
 *


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X      X  XXXXXXXX  XXXXX      X
X      X  X        X      X      XX
X      X  X        X        X      X
XXXXXXX XXXX      X        XXXXX  X
X      X  X        X        X      X
X      X  X        X      X      X
X      X  XXXXXXXX  XXXXX      XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1 PAGE 1 HEC-1 INPUT

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

1 ID FULL WATERSHED, RALPH NISENBAUM, 27SEP07

2 ID

	3	IT	15	300					
	4	IO	3						
	5	KK							
	6	KM	BASIN MONUMENT						
	7	KM	THE FOLLOWING PARAMETERS WERE PROVIDED FOR THIS BASIN						
	8	KM	L=	2.0	Lca=	.9	S=	152.0	Kn= .033 LAG= 28.0
	9	KM	PHOENIX MOUNTAIN S-GRAPH WAS USED FOR THIS BASIN						
	10	BA	.52						
	11	IN	15						
RECORD	12	KM	RAINFALL DEPTH OF 4.60 WAS SPACIALLY REDUCED AS SHOWN BY THE PB						
	13	KM	AN AREAL REDUCTION COEFFICIENT OF 1.000 WAS USED						
	14	PB	4.600						
	15	KM	THE FOLLOWING PC RECORD USED A 24-HOUR SCS TYPE II RAINFALL						
.023	.026	16	PC	.000	.002	.005	.008	.011	.014 .017 .020
.056	.060	17	PC	.029	.032	.035	.038	.041	.044 .048 .052
.100	.105	18	PC	.064	.068	.072	.076	.080	.085 .090 .095
.166	.175	19	PC	.110	.115	.120	.126	.135	.142 .150 .158
.678	.716	20	PC	.184	.195	.208	.224	.243	.266 .318 .479
.844	.851	21	PC	.743	.764	.781	.795	.808	.818 .828 .837
.905	.910	22	PC	.858	.865	.871	.877	.883	.889 .895 .900
.947	.951	23	PC	.915	.919	.923	.927	.931	.935 .939 .943
.978	.981	24	PC	.954	.957	.960	.963	.966	.969 .972 .975
		25	PC	.984	.987	.990	.993	.996	.999 1.000
		26	LG	.25	.10	10.00	.02	20.00	
0.	0.	27	UI	188.	533.	300.	157.	78.	39. 19. 12.
0.	0.	28	UI	0.	0.	0.	0.	0.	0. 0. 0.
		29	ZZ						

1*****

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* FLOOD HYDROGRAPH PACKAGE (HEC-1)
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* JUN 1998
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* DAVIS, CALIFORNIA 95616
* RUN DATE 27SEP07 TIME 19:55:06
* (916) 756-1104
*
*****
*****

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FULL WATERSHED, RALPH NISENBAUM, 27SEP07

```

4 IO      OUTPUT CONTROL VARIABLES
          IPRNT      3  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0.  HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      15  MINUTES IN COMPUTATION INTERVAL
          IDATE      1  0  STARTING DATE
          ITIME      0000 STARTING TIME
          NQ         300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE     4  0  ENDING DATE
          NDTIME     0245 ENDING TIME
          ICENT      19  CENTURY MARK

          COMPUTATION INTERVAL .25 HOURS
          TOTAL TIME BASE     74.75 HOURS

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

```

*** **
*** **

```

5 KK

*
*
*
*

BASIN MONUMENT

THE FOLLOWING PARAMETERS WERE PROVIDED FOR THIS BASIN

L= 2.0 Lca= .9 S= 152.0 Kn= .033 LAG= 28.0

PHOENIX MOUNTAIN S-GRAPH WAS USED FOR THIS BASIN

RECORD

RAINFALL DEPTH OF 4.60 WAS SPACIALLY REDUCED AS SHOWN BY THE PB

AN AREAL REDUCTION COEFFICIENT OF 1.000 WAS USED

THE FOLLOWING PC RECORD USED A 24-HOUR SCS TYPE II RAINFALL

11 IN

TIME DATA FOR INPUT TIME SERIES

JXMIN 15 TIME INTERVAL IN MINUTES
JXDATE 1 0 STARTING DATE
JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

10 BA

SUBBASIN CHARACTERISTICS

TAREA .52 SUBBASIN AREA

PRECIPITATION DATA

15 PB

STORM 4.60 BASIN TOTAL PRECIPITATION

15 PI

INCREMENTAL PRECIPITATION PATTERN

		.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.01	.00	.01	.00	.00	.00	.01	.01	.00
.01	.01	.01	.01	.00	.01	.01	.01	.01
.01	.01	.01	.01	.01	.02	.02	.02	.05
.20	.04	.03	.02	.02	.01	.01	.01	.01
.01	.01	.01	.01	.01	.01	.01	.01	.01
.00	.01	.00	.01	.01	.01	.01	.01	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
		.00	.00	.00	.00	.00	.00	

26 LG

GREEN AND AMPT LOSS RATE

STRTL	.25	STARTING LOSS
DTH	.10	MOISTURE DEFICIT
PSIF	10.00	WETTING FRONT SUCTION
XKSAT	.02	HYDRAULIC CONDUCTIVITY
RTIMP	20.00	PERCENT IMPERVIOUS AREA

26 UI

INPUT UNITGRAPH, 8 ORDINATES, VOLUME = .99
 188.0 533.0 300.0 157.0 78.0 39.0 19.0

12.0

HYDROGRAPH AT STATION

TOTAL RAINFALL = 4.60, TOTAL LOSS = 1.08, TOTAL EXCESS = 3.52

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW 24-HR	72-HR	74.75-HR
+	(CFS)	(HR)	(CFS)			
+	779.	12.25	165.	49.	16.	16.
			(INCHES)	3.478	3.481	3.481
			(AC-FT)	96.	97.	97.

CUMULATIVE AREA = .52 SQ MI

1

RUNOFF SUMMARY
 FLOW IN CUBIC FEET PER SECOND
 TIME IN HOURS, AREA IN SQUARE MILES

BASIN	MAXIMUM OPERATION STAGE	TIME OF STATION MAX STAGE	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD		
AREA					6-HOUR	24-HOUR	72-HOUR
+							
	HYDROGRAPH AT						
+			779.	12.25	165.	49.	16.
.52							

*** NORMAL END OF HEC-1 ***

2 HR

```

*****
*****
*
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
* U.S. ARMY CORPS OF ENGINEERS
* JUN 1998
* HYDROLOGIC ENGINEERING CENTER
* VERSION 4.1
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
* RUN DATE 28SEP07 TIME 09:00:04
* (916) 756-1104
*
*****
*****

```

```

X      X  XXXXXXXX  XXXXX      X
X      X  X        X      X    XX
X      X  X        X        X    X
XXXXXXX XXXX      X      XXXXX  X
X      X  X        X        X    X
X      X  X        X      X    X
X      X  XXXXXXXX  XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.

THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION

NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,

DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION

KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE
ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          ID  MONUMENT5MINOUTFALL,RDN
2          ID

```

	3	IT	5	300							
	4	IO	3								
	5	KK									
	6	KM	BASIN M5								
	7	KM	THE FOLLOWING PARAMETERS WERE PROVIDED FOR THIS BASIN								
	8	KM	L= 2.0 Lca= .9 S= 152.0 Kn= .033 LAG= 28.0								
	9	KM	PHOENIX MOUNTAIN S-GRAPH WAS USED FOR THIS BASIN								
	10	BA	.52								
	11	IN	15								
RECORD	12	KM	RAINFALL DEPTH OF 4.60 WAS SPACIALLY REDUCED AS SHOWN BY THE PB								
	13	KM	AN AREAL REDUCTION COEFFICIENT OF 1.000 WAS USED								
	14	PB	2.750								
	15	KM	THE FOLLOWING PC RECORD USED A 24-HOUR SCS TYPE II RAINFALL								
.023	.026	16	PC	.000	.002	.005	.008	.011	.014	.017	.020
.056	.060	17	PC	.029	.032	.035	.038	.041	.044	.048	.052
.100	.105	18	PC	.064	.068	.072	.076	.080	.085	.090	.095
.166	.175	19	PC	.110	.115	.120	.126	.135	.142	.150	.158
.678	.716	20	PC	.184	.195	.208	.224	.243	.266	.318	.479
.844	.851	21	PC	.743	.764	.781	.795	.808	.818	.828	.837
.905	.910	22	PC	.858	.865	.871	.877	.883	.889	.895	.900
.947	.951	23	PC	.915	.919	.923	.927	.931	.935	.939	.943
.978	.981	24	PC	.954	.957	.960	.963	.966	.969	.972	.975
		25	PC	.984	.987	.990	.993	.996	.999	1.000	
		26	LG	.25	.10	10.00	.02	25.00			
246.	189.	27	UI	62.	161.	341.	466.	669.	466.	355.	299.
30.	15.	28	UI	151.	130.	94.	76.	65.	48.	39.	30.
0.	0.	29	UI	12.	12.	12.	12.	12.	0.	0.	0.
		30	UI	0.	0.	0.	0.	0.	0.	0.	0.

```

1*****
*****
*
*
*   FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   U.S. ARMY CORPS OF ENGINEERS
*       JUN 1998
*   HYDROLOGIC ENGINEERING CENTER
*       VERSION 4.1
*       609 SECOND STREET
*
*   DAVIS, CALIFORNIA 95616
*   RUN DATE 28SEP07 TIME 09:00:04
*       (916) 756-1104
*
*
*****
*****

```

MONUMENT5MINOUTFALL,RDN

```

4 IO      OUTPUT CONTROL VARIABLES
          IPRNT      3  PRINT CONTROL
          IPLOT      0  PLOT CONTROL
          QSCAL      0. HYDROGRAPH PLOT SCALE

IT        HYDROGRAPH TIME DATA
          NMIN      5  MINUTES IN COMPUTATION INTERVAL
          IDATE      1  0  STARTING DATE
          ITIME      0000 STARTING TIME
          NQ         300 NUMBER OF HYDROGRAPH ORDINATES
          NDDATE      2  0  ENDING DATE
          NDTIME      0055 ENDING TIME
          ICENT       19  CENTURY MARK

          COMPUTATION INTERVAL .08 HOURS
          TOTAL TIME BASE     24.92 HOURS

ENGLISH UNITS
DRAINAGE AREA      SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION  FEET
FLOW               CUBIC FEET PER SECOND
STORAGE VOLUME     ACRE-FEET
SURFACE AREA       ACRES
TEMPERATURE        DEGREES FAHRENHEIT

```

*** ** MONU 2.0 ***
 *** **

5 KK

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 *

BASIN M5

THE FOLLOWING PARAMETERS WERE PROVIDED FOR THIS BASIN

L= 2.0 Lca= .9 S= 152.0 Kn= .033 LAG= 28.0

PHOENIX MOUNTAIN S-GRAPH WAS USED FOR THIS BASIN

RECORD

RAINFALL DEPTH OF 4.60 WAS SPACIALLY REDUCED AS SHOWN BY THE PB

AN AREAL REDUCTION COEFFICIENT OF 1.000 WAS USED

THE FOLLOWING PC RECORD USED A 24-HOUR SCS TYPE II RAINFALL

11 IN

TIME DATA FOR INPUT TIME SERIES

JXMIN 15 TIME INTERVAL IN MINUTES
 JXDATE 1 0 STARTING DATE
 JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

10 BA

SUBBASIN CHARACTERISTICS

TAREA .52 SUBBASIN AREA

PRECIPITATION DATA

15 PB

STORM 2.75 BASIN TOTAL PRECIPITATION

15 PI

INCREMENTAL PRECIPITATION PATTERN

		.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00
.00	.00	.00	.00	.00	.00	.00	.00	.00

HYDROGRAPH AT STATION

TOTAL RAINFALL = 2.75, TOTAL LOSS = .90, TOTAL EXCESS = 1.85

PEAK FLOW (CFS)	TIME (HR)	(CFS)	6-HR 1.613 (INCHES) (AC-FT)	MAXIMUM AVERAGE FLOW 24-HR 26. 1.829 51.	72-HR 25. 1.830 51.	24.92-HR 25. 1.830 51.
463.	12.17	90.	45.			
CUMULATIVE AREA =			.52 SQ MI			

1

RUNOFF SUMMARY
FLOW IN CUBIC FEET PER SECOND
TIME IN HOURS, AREA IN SQUARE MILES

BASIN AREA +	MAXIMUM OPERATION STAGE	TIME OF STATION MAX STAGE	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD		
					6-HOUR	24-HOUR	72-HOUR
+	HYDROGRAPH AT		463.	12.17	90.	26.	25.
.52							

*** NORMAL END OF HEC-1 ***

Appendix B
Hydrologic Backup

24 Hr

HEC-RAS Version 3.1.3 May 2005
 U.S. Army Corp of Engineers
 Hydrologic Engineering Center
 609 Second Street
 Davis, California

```

X      X  XXXXXX      XXXX      XXXX      XX      XXXX
X      X  X          X  X      X  X      X  X      X
X      X  X          X          X  X      X  X      X
XXXXXXXX XXXX      X          XXX XXXX      XXXXXX      XXXX
X      X  X          X          X  X      X  X      X
X      X  X          X          X  X      X  X      X
X      X  XXXXXX      XXXX      X  X      X  X      XXXXX

```

PROJECT DATA

Project Title: Wash W-1

Project File : 07169100YR24HRprj.prj

Run Date and Time: 9/28/2007 9:53:50 AM

Project in English units

Project Description:

FLOW = 790 CFS 100-YR 24-HOUR STORM

PLAN DATA

Plan Title: Plan 02

Plan File : z:\Projects\2007\07-169\HEC-RAS\07169100YR24HRprj.p02

Geometry Title: Geom 01

Geometry File : z:\Projects\2007\07-169\HEC-RAS\07169100YR24HRprj.g01

Flow Title : Flow 06

Flow File : z:\Projects\2007\07-169\HEC-RAS\07169100YR24HRprj.f06

Plan Summary Information:

Number of: Cross Sections	= 11	Multiple Openings	= 0
Culverts	= 1	Inline Structures	= 0
Bridges	= 0	Lateral Structures	= 0

Computational Information

Water surface calculation tolerance	= 0.01
Critical depth calculation tolerance	= 0.01
Maximum number of iterations	= 20
Maximum difference tolerance	= 0.3
Flow tolerance factor	= 0.001

Computation options

Critical depth computed only where necessary	
Conveyance Calculation Method:	At breaks in n values only
Friction Slope Method:	Average Conveyance
Computational Flow Regime:	Subcritical Flow

FLOW DATA

Flow Title: Flow 06

Flow File : z:\Projects\2007\07-169\HEC-RAS\07169100YR24HRprj.f06

Flow Data (cfs)

River
W-1Reach
Wash W-1RS
11PF 1
779

Boundary Conditions

River
Downstream

Reach

Profile

Upstream

W-1 Wash W-1 PF 1 Normal S = 0.0267 Normal S =
0.0305

GEOMETRY DATA

Geometry Title: Geom 01

Geometry File : z:\Projects\2007\07-169\HEC-RAS\07169100YR24HRprj.g01

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 11

INPUT

Description:

Station Elevation Data				num=				
Sta	Elev	Sta	Elev		Sta	Elev	Sta	Elev
0	2549	3.47	2548	9	15.15	2547	39.22	2546
57.94	2546	61.3	2547		70.51	2548	78.78	2548.91

Manning's n Values

Sta	n Val	Sta	n Val	num=	Sta	n Val
0	.04	39.22	.03	3	57.94	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	39.22	57.94		58.47 49.8	50.03	.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 10

INPUT

Description:

Station Elevation Data				num=				
Sta	Elev	Sta	Elev		Sta	Elev	Sta	Elev
0	2548	3.99	2547	13	7.76	2546	11.53	2545
20.81	2543.8	26.64	2544		30.64	2545	34.74	2546
51.21	2548	52.21	2548.1		53.02	2548		

Manning's n Values

Sta	n Val	Sta	n Val	num=	Sta	n Val
0	.04	15.26	.03	3	26.64	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff Contr.	Expan.
	15.26	26.64		50.17 50.85	50.51	.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 9

INPUT

Description:

Station Elevation Data			num=	11						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2547	2.64	2546	5.28	2545	7.93	2544	23.95	2543	
32.08	2542.91	34.76	2543	38.35	2544	42.34	2545	46.42	2546	
59.66	2546.58									

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	23.95	.03	34.76	.04

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
	23.95	34.76		50.02	50.51	50.29		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 8

INPUT

Description:

Station Elevation Data			num=	9						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2545	5.8	2544	11.27	2543	19.76	2542	24.44	2541.81	
28.57	2542	42.09	2543	55.93	2544	64.39	2544.86			

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	19.76	.03	28.57	.04

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
	19.76	28.57		56.96	50.5	50.31		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 7

INPUT

Description:

Station Elevation Data			num=	11						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2544	15.95	2543	21.54	2542	28.75	2541	54.08	2540	
58.55	2539.83	61.64	2540	67.62	2541	73.91	2542	85.61	2543	
96.93	2543.67									

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	54.08	.03	61.64	.04

Bank Sta:	Left	Right	Lengths:	Left	Channel	Right	Coeff	Contr.	Expan.
	54.08	61.64		52.54	49.75	49.99		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 6

INPUT

Description:

Station Elevation Data			num=	11						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2549.25	0	2541.51	3.62	2541	21	2540	31.85	2539	
38.94	2538.45	46.25	2539	59.59	2540	67.12	2541	75.03	2542	
84.66	2543									

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val

0 .04 31.85 .03 46.25 .04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	31.85	46.25		45.76 42.18	40.42		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 5

INPUT

Description:

Station Elevation Data			num=	13					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2549	0	2541.2	6.77	2541	10.64	2540	14.13	2539
24.62	2538	29.6	2537.69	34.83	2538	40.12	2539	43.61	2540
45.88	2541	55.05	2542	61.44	2542.75				

Manning's n Values

num=

3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	24.62	.03	34.83	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	24.62	34.83		30.54 20.58	21.29		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 4

INPUT

Description:

Station Elevation Data			num=	12					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2546.5	0	2540.14	.91	2540	7.42	2539	13.94	2538
23.27	2537.68	30.68	2538	32.53	2539	34.38	2540	36.25	2541
36.94	2541.3	36.94	2542						

Manning's n Values

num=

3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	13.94	.03	30.68	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	13.94	30.68		42.2 23.89	9.92		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 3

INPUT

Description:

Station Elevation Data			num=	17					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2544	0	2543.2	.34	2543	1.28	2542	2.23	2541
3.21	2540	4.19	2539	5.28	2538	17.26	2537	25.38	2536.9
25.92	2537	35.52	2538	37.24	2539	40.06	2540	42.5	2541
44.17	2542	45	2542.2						

Manning's n Values

num=

3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	5.28	.03	35.52	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	5.28	35.52		108.63 71.04	74.11		.1	.3

Ineffective Flow

num=

2

Sta L	Sta R	Elev	Permanent
0	5.2	2543	F

39.7 45 2543

CULVERT

IVER: W-1

EACH: Wash W-1

RS: 2.0902

INPUT

Description:

Distance from Upstream XS = 10.2

Deck/Roadway Width = 24

Weir Coefficient = 2.6

Upstream Deck/Roadway Coordinates

num= 2

Sta	Hi Cord	Lo Cord	Sta	Hi Cord	Lo Cord
0	2543.95	2536	53	2543.95	2536

Upstream Bridge Cross Section Data

Station Elevation Data num= 17

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2544	0	2543.2	.34	2543	1.28	2542	2.23	2541
3.21	2540	4.19	2539	5.28	2538	17.26	2537	25.38	2536.9
25.92	2537	35.52	2538	37.24	2539	40.06	2540	42.5	2541
44.17	2542	45	2542.2						

Manning's n Values

num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	5.28	.03	35.52	.04

Bank Sta:	Left	Right	Coeff Contr.	Expan.
	5.28	35.52	.1	.3

Ineffective Flow

num= 2

Sta L	Sta R	Elev	Permanent
0	5.2	2543	F
39.7	45	2543	F

Downstream Deck/Roadway Coordinates

num= 2

Sta	Hi Cord	Lo Cord	Sta	Hi Cord	Lo Cord
0	2543.95	2535	121	2543.95	2535

Downstream Bridge Cross Section Data

Station Elevation Data num= 6

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2540	65.92	2538	87.93	2536	91.28	2536	107.72	2538
121.36	2540								

Manning's n Values

num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	87.93	.03	91.28	.04

Bank Sta:	Left	Right	Coeff Contr.	Expan.
	87.93	91.28	.1	.3

Upstream Embankment side slope

= 2 horiz. to 1.0 vertical

Downstream Embankment side slope

= 2 horiz. to 1.0 vertical

Maximum allowable submergence for weir flow

= .95

Elevation at which weir flow begins

=

Energy head used in spillway design

=

Spillway height used in design

=

Weir crest shape

= Broad Crested

Number of Culverts = 1

Culvert Name Shape Rise Span

Culvert #1 Ellipse 4.5 6

FHWA Chart # 29- Horizontal Ellipse; Concrete

FHWA Scale # 1 - Square edge with headwall

Solution Criteria = Highest U.S. EG

Culvert Upstrm Dist Length Top n Bottom n Depth Blocked Entrance Loss Coef Exit Loss

Coef 5.32 58.96 24 .024 0 .5 1

Number of Barrels = 4

Upstream Elevation = 2536.95

Centerline Stations

Sta.	Sta.	Sta.	Sta.
8.86	16.77	27.88	35.98

Downstream Elevation = 2535.8

Centerline Stations

Sta.	Sta.	Sta.	Sta.
85.17	93.08	104.19	112.29

CROSS SECTION

RIVER: W-1

REACH: Wash W-1 RS: 2

INPUT

Description:

Station Elevation Data num= 6

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2540	65.92	2538	87.93	2536	91.28	2536	107.72	2538
121.36	2540								

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	87.93	.03	91.28	.04

Bank Sta: Left Right Lengths: Left Channel Right Coeff Contr. Expan.

87.93	91.28	107.85	101.61	93.35	.1	.3
-------	-------	--------	--------	-------	----	----

CROSS SECTION

RIVER: W-1

REACH: Wash W-1 RS: 1

INPUT

Description:

Station Elevation Data num= 7

Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2538	60.32	2536	63.52	2534	69.48	2533.56	75.95	2534
87.33	2536	114.67	2538						

Manning's n Values num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	63.52	.03	75.95	.04

Bank Sta: Left Right Coeff Contr. Expan.

63.52	75.95	.1	.3
-------	-------	----	----

SUMMARY OF MANNING'S N VALUES

River:W-1

Reach	River Sta.	n1	n2	n3
Wash W-1	11	.04	.03	.04
Wash W-1	10	.04	.03	.04
Wash W-1	9	.04	.03	.04
Wash W-1	8	.04	.03	.04
Wash W-1	7	.04	.03	.04
Wash W-1	6	.04	.03	.04
Wash W-1	5	.04	.03	.04
Wash W-1	4	.04	.03	.04
Wash W-1	3	.04	.03	.04
Wash W-1	2.0902	Culvert		
Wash W-1	2	.04	.03	.04

Wash W-1

1

.04

.03

.04

SUMMARY OF REACH LENGTHS

River: W-1

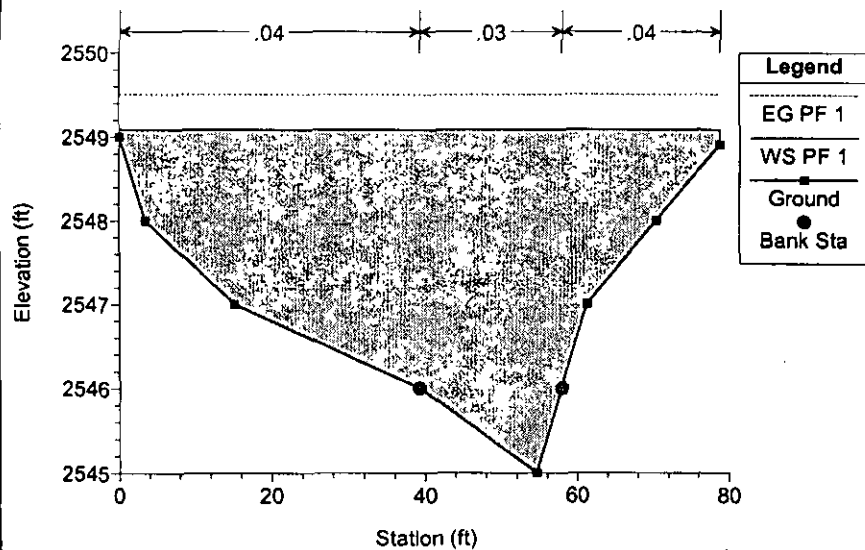
Reach	River Sta.	Left	Channel	Right
Wash W-1	11	58.47	49.8	50.03
Wash W-1	10	50.17	50.85	50.51
Wash W-1	9	50.02	50.51	50.29
Wash W-1	8	56.96	50.5	50.31
Wash W-1	7	52.54	49.75	49.99
Wash W-1	6	45.76	42.18	40.42
Wash W-1	5	30.54	20.58	21.29
Wash W-1	4	42.2	23.89	9.92
Wash W-1	3	108.63	71.04	74.11
Wash W-1	2.0902	Culvert		
Wash W-1	2	107.85	101.61	93.35
Wash W-1	1			

SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

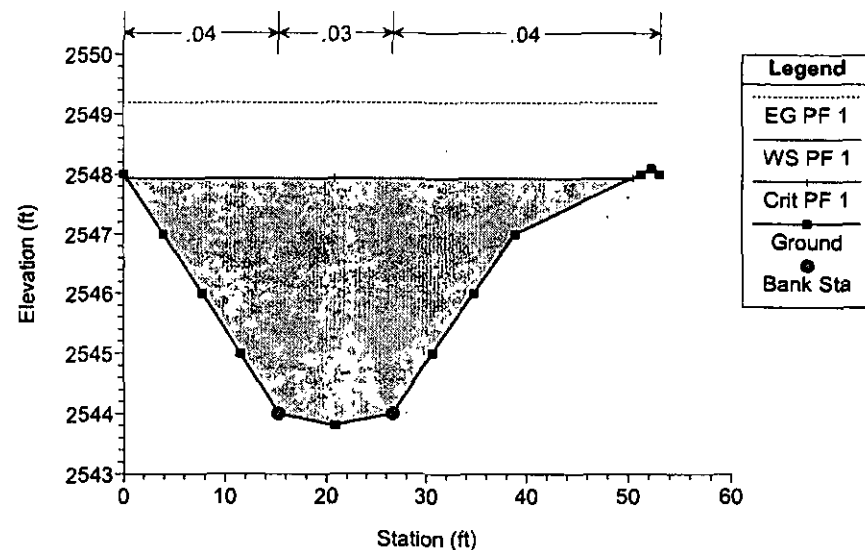
River: W-1

Reach	River Sta.	Contr.	Expan.
Wash W-1	11	.1	.3
Wash W-1	10	.1	.3
Wash W-1	9	.1	.3
Wash W-1	8	.1	.3
Wash W-1	7	.1	.3
Wash W-1	6	.1	.3
Wash W-1	5	.1	.3
Wash W-1	4	.1	.3
Wash W-1	3	.1	.3
Wash W-1	2.0902	Culvert	
Wash W-1	2	.1	.3
Wash W-1	1	.1	.3

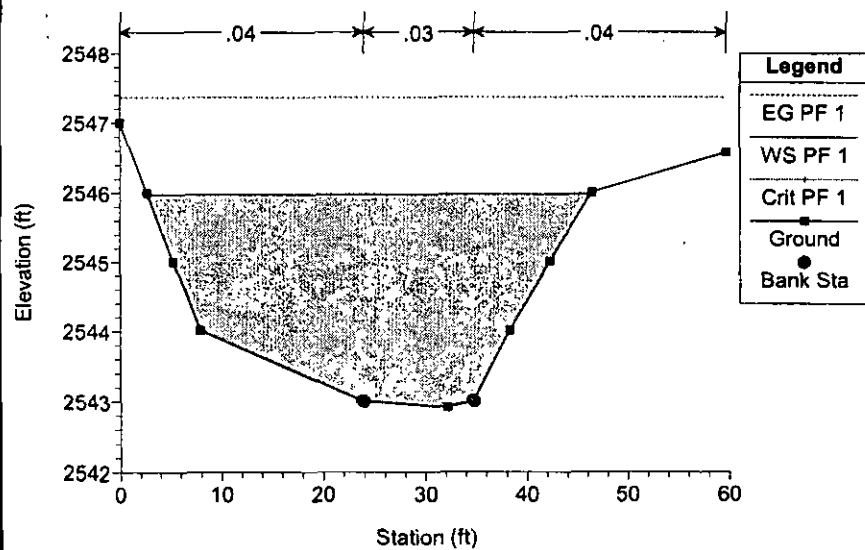
Wash W-1 Plan: Plan 02 9/28/2007



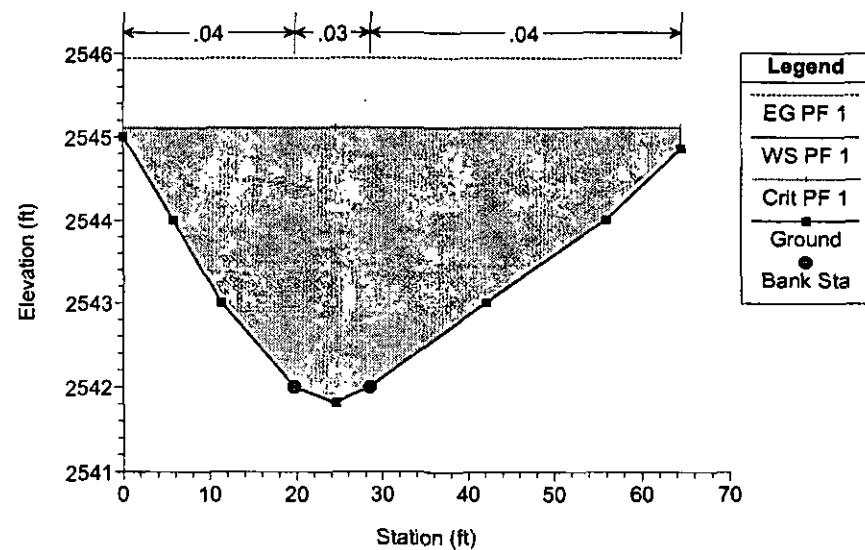
Wash W-1 Plan: Plan 02 9/28/2007

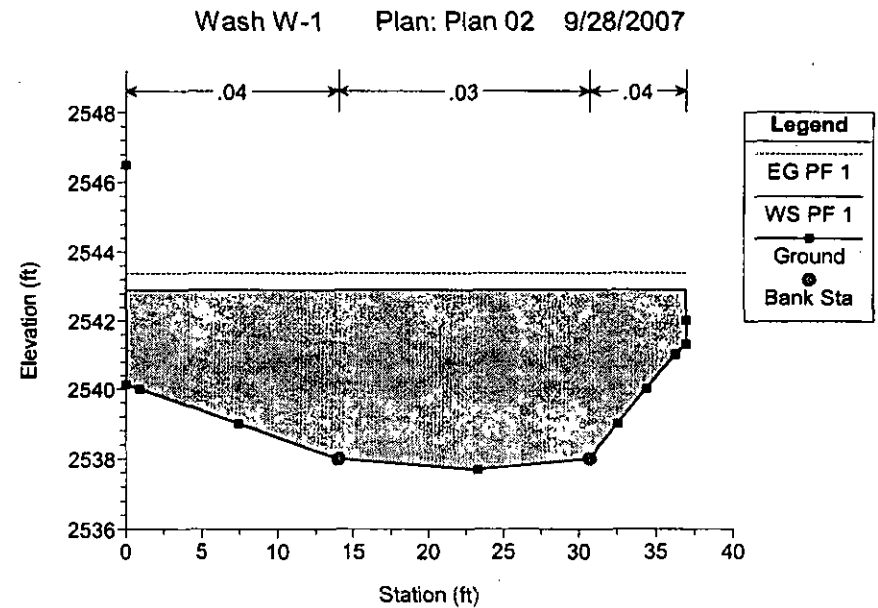
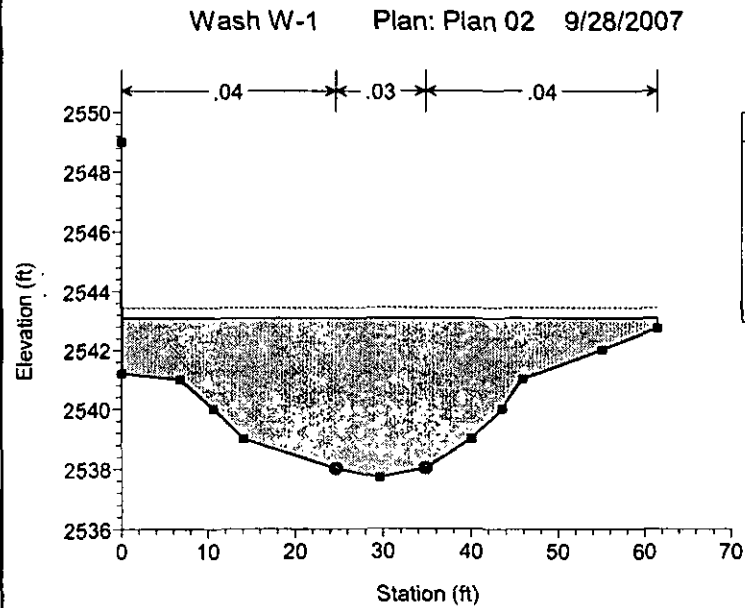
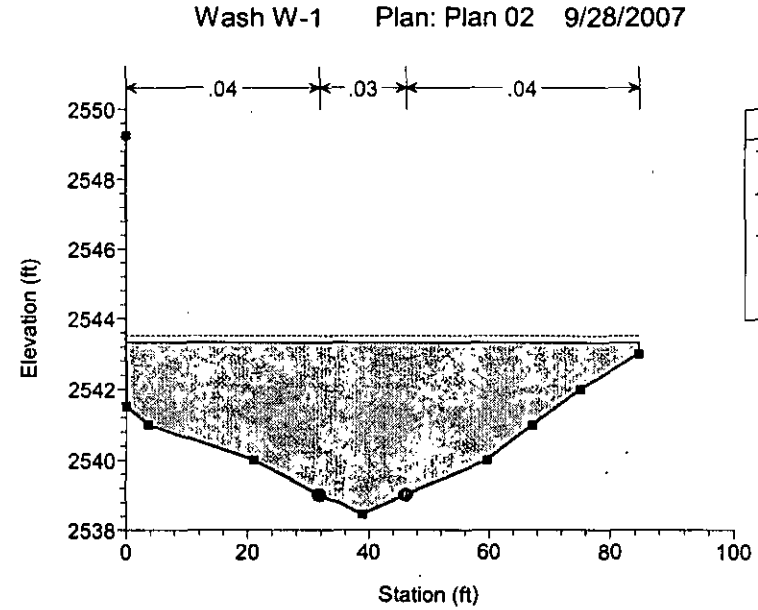
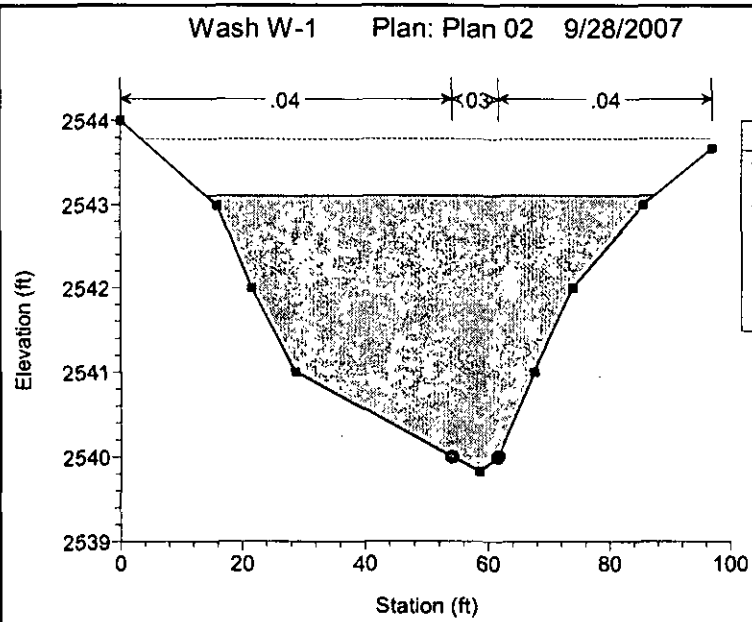


Wash W-1 Plan: Plan 02 9/28/2007

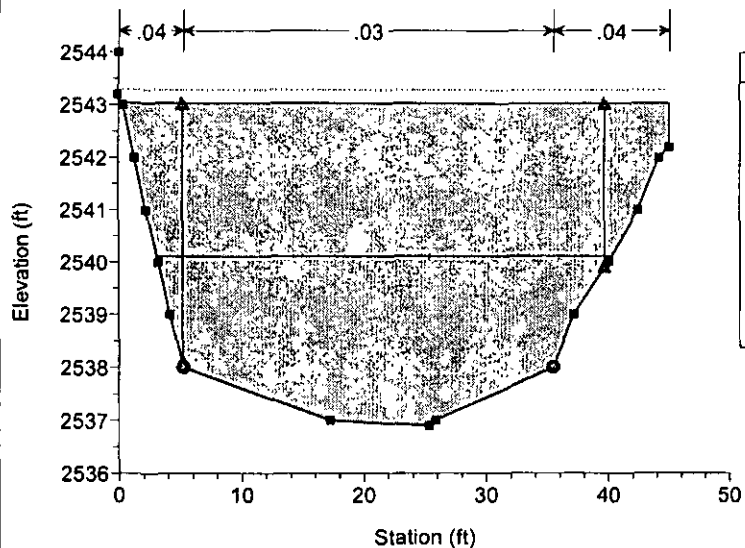


Wash W-1 Plan: Plan 02 9/28/2007

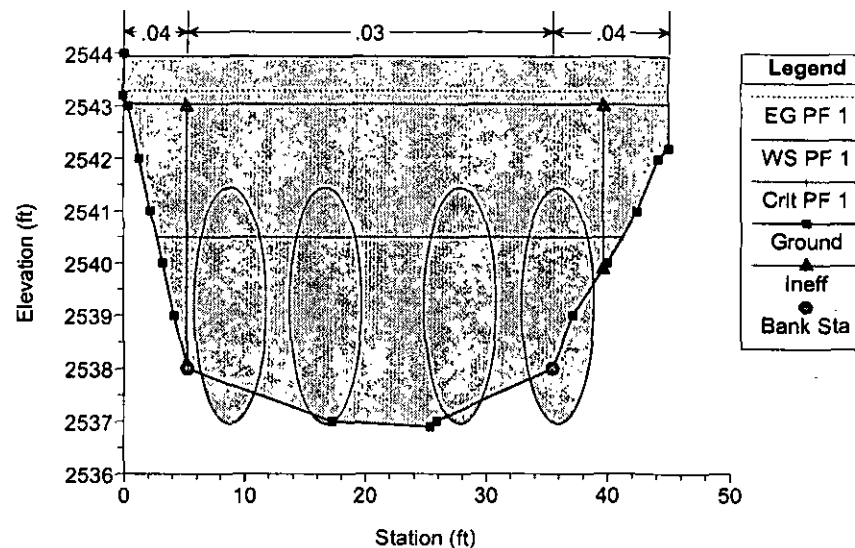




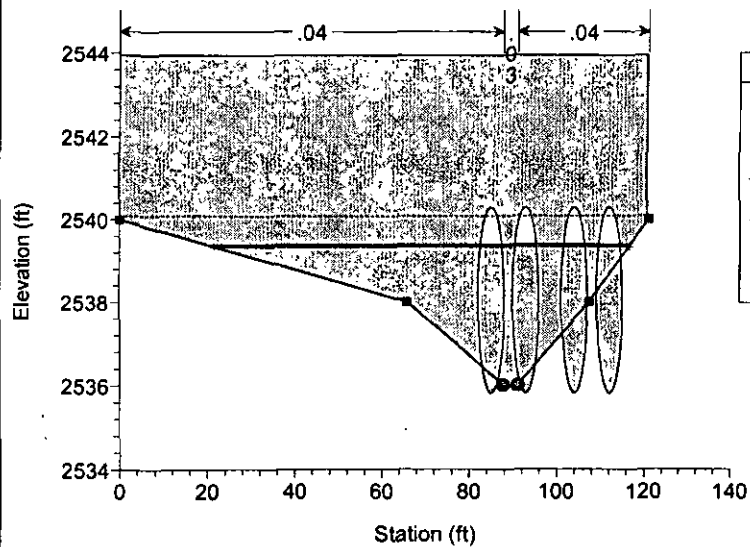
Wash W-1 Plan: Plan 02 9/28/2007



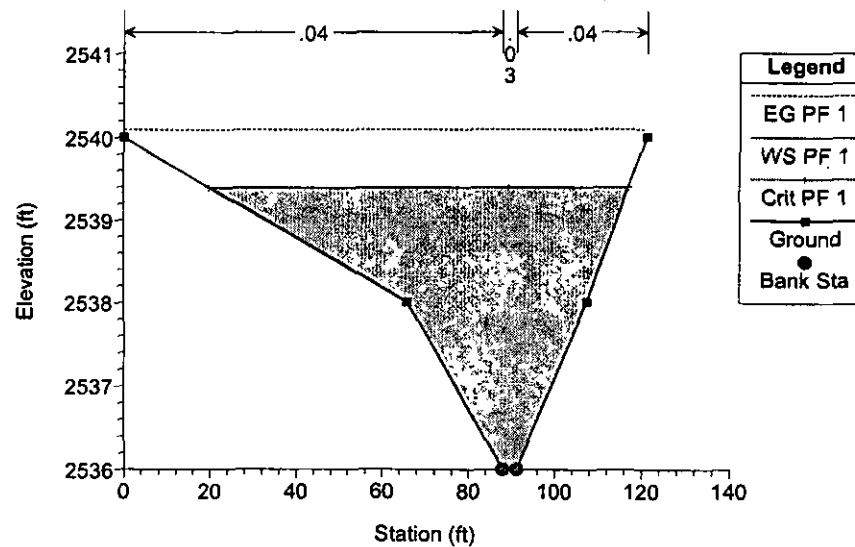
Wash W-1 Plan: Plan 02 9/28/2007



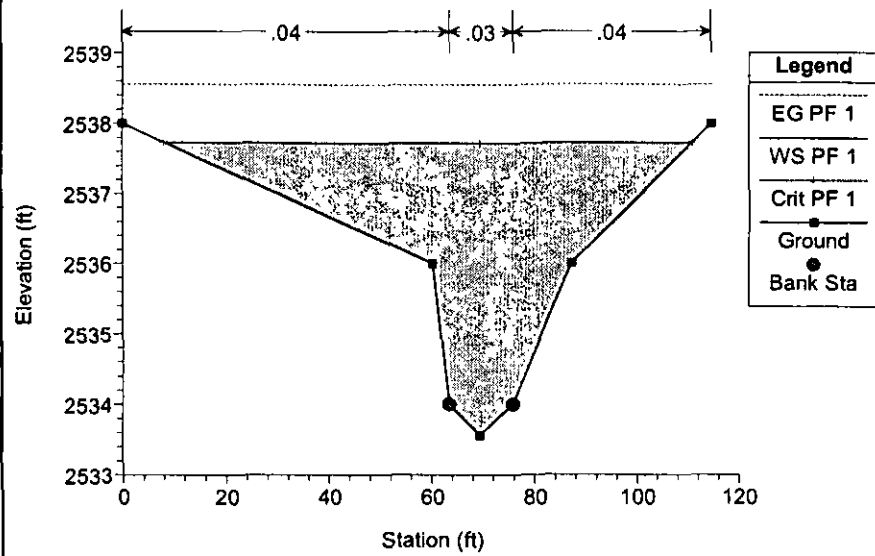
Wash W-1 Plan: Plan 02 9/28/2007



Wash W-1 Plan: Plan 02 9/28/2007



Wash W-1 Plan: Plan 02 9/28/2007



2 HR

HEC-RAS Version 3.1.3 May 2005
 U.S. Army Corp of Engineers
 Hydrologic Engineering Center
 609 Second Street
 Davis, California

```

X      X  XXXXXX  XXXX      XXXX      XX      XXXX
X      X  X      X      X      X      X      X
X      X  X      X      X      X      X      X
XXXXXXXX XXXX      X      XXX XXXX      XXXXXX      XXXX
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X      X  XXXXXX  XXXX      X      X      X      X      XXXXX

```

PROJECT DATA

Project Title: wash w-1
 Project File : 07169.prj
 Run Date and Time: 9/28/2007 9:13:13 AM

Project in English units

Project Description:

FLOW = 496 CFS 100-YR 2-HOUR STORM

PLAN DATA

Plan Title: Plan 02
 Plan File : z:\Projects\2007\07-169\HEC-RAS\07169.p02

Geometry Title: Geom 01
 Geometry File : z:\Projects\2007\07-169\HEC-RAS\07169.g01

Flow Title : Flow 06
 Flow File : z:\Projects\2007\07-169\HEC-RAS\07169.f06

Plan Summary Information:

Number of:	Cross Sections =	11	Multiple Openings =	0
	Culverts =	1	Inline Structures =	0
	Bridges =	0	Lateral Structures =	0

Computational Information

Water surface calculation tolerance =	0.01
Critical depth calculation tolerance =	0.01
Maximum number of iterations =	20
Maximum difference tolerance =	0.3
Flow tolerance factor =	0.001

Computation Options

Critical depth computed only where necessary
 Conveyance calculation Method: At breaks in n values only
 Friction Slope Method: Average Conveyance
 Computational Flow Regime: Subcritical Flow

FLOW DATA

Flow Title: Flow 06
 Flow File : z:\Projects\2007\07-169\HEC-RAS\07169.f06

Flow Data (cfs)

0 .04 31.85 .03 46.25 .04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	31.85	46.25		45.76 42.18	40.42		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1 RS: 5

INPUT

Description:

Station	Elevation	Data	num=	13					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2549	0	2541.2	6.77	2541	10.64	2540	14.13	2539
24.62	2538	29.6	2537.69	34.83	2538	40.12	2539	43.61	2540
45.88	2541	55.05	2542	61.44	2542.75				

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	24.62	.03	34.83	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	24.62	34.83		30.54 20.58	21.29		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1 RS: 4

INPUT

Description:

Station	Elevation	Data	num=	12					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2546.5	0	2540.14	.91	2540	7.42	2539	13.94	2538
23.27	2537.68	30.68	2538	32.53	2539	34.38	2540	36.25	2541
36.94	2541.3	36.94	2542						

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	13.94	.03	30.68	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	13.94	30.68		42.2 23.89	9.92		.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1 RS: 3

INPUT

Description:

Station	Elevation	Data	num=	17					
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2544	0	2543.2	.34	2543	1.28	2542	2.23	2541
3.21	2540	4.19	2539	5.28	2538	17.26	2537	25.38	2536.9
25.92	2537	35.52	2538	37.24	2539	40.06	2540	42.5	2541
44.17	2542	45	2542.2						

Manning's n Values

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	5.28	.03	35.52	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	5.28	35.52		108.63 71.04	74.11		.1	.3

Ineffective Flow

Sta L	Sta R	Elev	Permanent
0	5.2	2543	F

39.7 45 2543

F

CULVERT

RIVER: W-1

REACH: Wash W-1

RS: 2.0902

INPUT

Description:

Distance from Upstream XS = 10.2

Deck/Roadway Width = 24

Weir Coefficient = 2.6

Upstream Deck/Roadway Coordinates

num= 2

Sta	Hi Cord	Lo Cord	Sta	Hi Cord	Lo Cord
0	2543.95	2536	53	2543.95	2536

Upstream Bridge Cross Section Data

Station Elevation Data		num=								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2544	0	2543.2	.34	2543	1.28	2542	2.23	2541	
3.21	2540	4.19	2539	5.28	2538	17.26	2537	25.38	2536.9	
25.92	2537	35.52	2538	37.24	2539	40.06	2540	42.5	2541	
44.17	2542	45	2542.2							

Manning's n Values

num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	5.28	.03	35.52	.04

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	5.28	35.52	.1		.3

Ineffective Flow num= 2

Sta L	Sta R	Elev	Permanent
0	5.2	2543	F
39.7	45	2543	F

Downstream Deck/Roadway Coordinates

num= 2

Sta	Hi Cord	Lo Cord	Sta	Hi Cord	Lo Cord
0	2543.95	2535	121	2543.95	2535

Downstream Bridge Cross Section Data

Station Elevation Data		num=								
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	
0	2540	65.92	2538	87.93	2536	91.28	2536	107.72	2538	
121.36	2540									

Manning's n Values

num= 3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	87.93	.03	91.28	.04

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	87.93	91.28	.1		.3

Upstream Embankment side slope = 2 horiz. to 1.0 vertical

Downstream Embankment side slope = 2 horiz. to 1.0 vertical

Maximum allowable submergence for weir flow = .95

Elevation at which weir flow begins =

Energy head used in spillway design =

Spillway height used in design =

Weir crest shape = Broad Crested

Number of Culverts = 1

Culvert Name	Shape	Rise	Span
Culvert #1	Ellipse	4.5	6

FHWA Chart # 29- Horizontal Ellipse; Concrete
FHWA Scale # 1 - Square edge with headwall

Solution Criteria = Highest U.S. EG

Culvert Upstrm Dist Length Top n Bottom n Depth Blocked Entrance Loss Coef Exit Loss

Coef

5.32 58.96 24 .024 0 .5

1

Number of Barrels = 4

Upstream Elevation = 2536.95

Centerline Stations

Sta. Sta. Sta. Sta.
8.86 16.77 27.88 35.98

Downstream Elevation = 2535.8

Centerline Stations

Sta. Sta. Sta. Sta.
85.17 93.08 104.19 112.29

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 2

INPUT

Description:

Station Elevation Data		num=	6						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2540	65.92	2538	87.93	2536	91.28	2536	107.72	2538
121.36	2540								

Manning's n Values

num=

3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	87.93	.03	91.28	.04

Bank Sta:	Left	Right	Lengths:	Left Channel	Right	Coeff	Contr.	Expan.
	87.93	91.28		107.85	101.61	93.35	.1	.3

CROSS SECTION

RIVER: W-1

REACH: Wash W-1

RS: 1

INPUT

Description:

Station Elevation Data		num=	7						
Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev	Sta	Elev
0	2538	60.32	2536	63.52	2534	69.48	2533.56	75.95	2534
87.33	2536	114.67	2538						

Manning's n Values

num=

3

Sta	n Val	Sta	n Val	Sta	n Val
0	.04	63.52	.03	75.95	.04

Bank Sta:	Left	Right	Coeff	Contr.	Expan.
	63.52	75.95		.1	.3

SUMMARY OF MANNING'S N VALUES

River: W-1

Reach	River Sta.	n1	n2	n3
Wash W-1	11	.04	.03	.04
Wash W-1	10	.04	.03	.04
Wash W-1	9	.04	.03	.04
Wash W-1	8	.04	.03	.04
Wash W-1	7	.04	.03	.04
Wash W-1	6	.04	.03	.04
Wash W-1	5	.04	.03	.04
Wash W-1	4	.04	.03	.04
Wash W-1	3	.04	.03	.04
Wash W-1	2.0902	culvert		
Wash W-1	2	.04	.03	.04

SUMMARY OF REACH LENGTHS

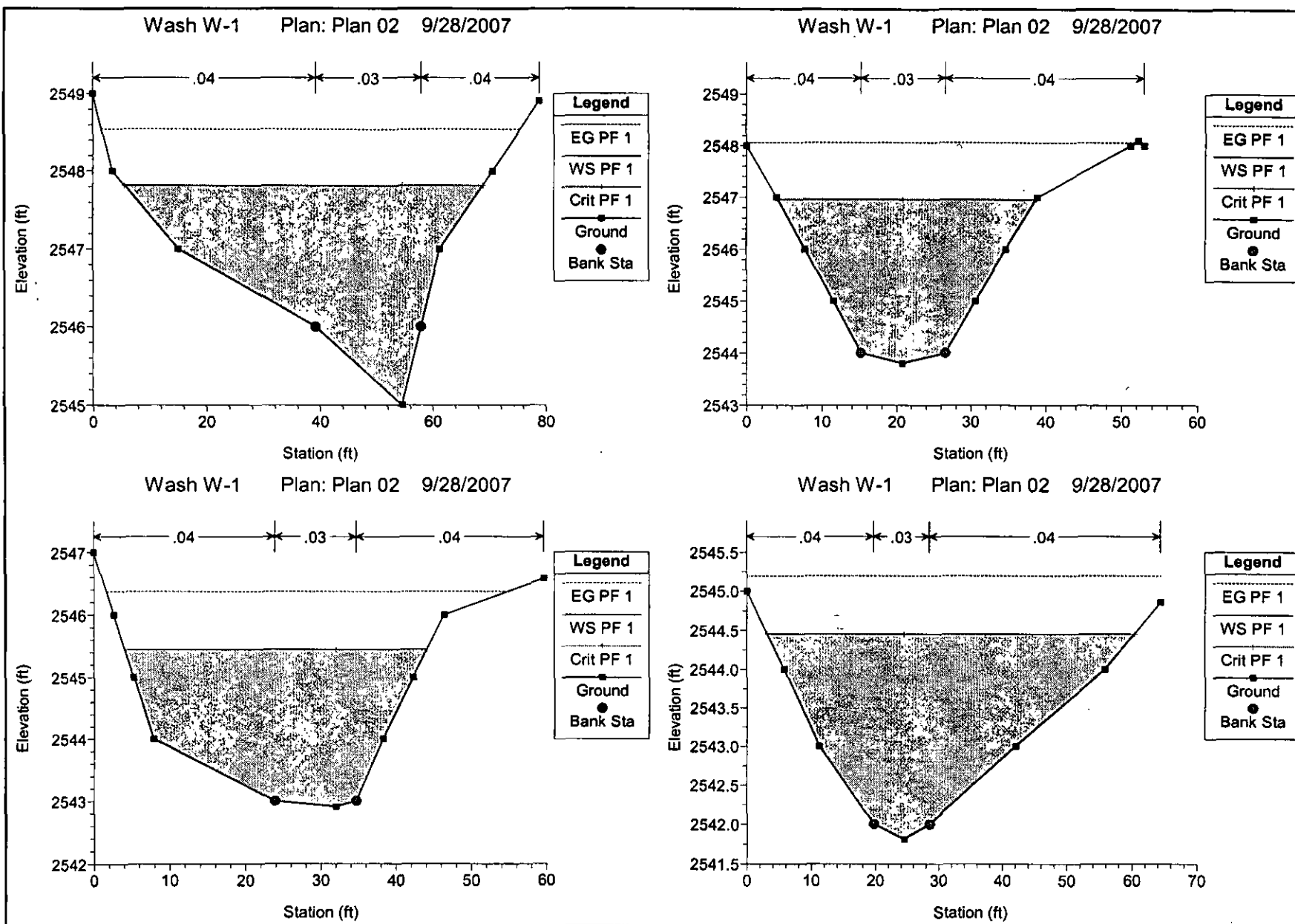
River: W-1

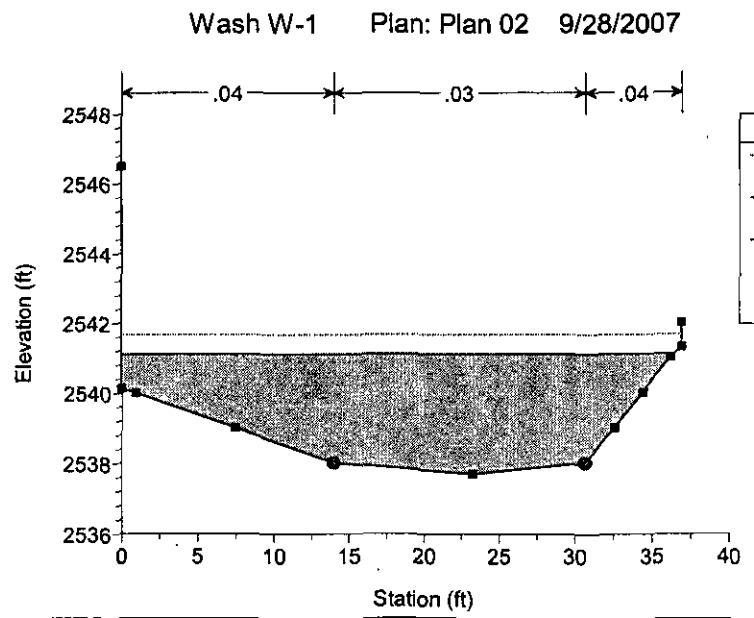
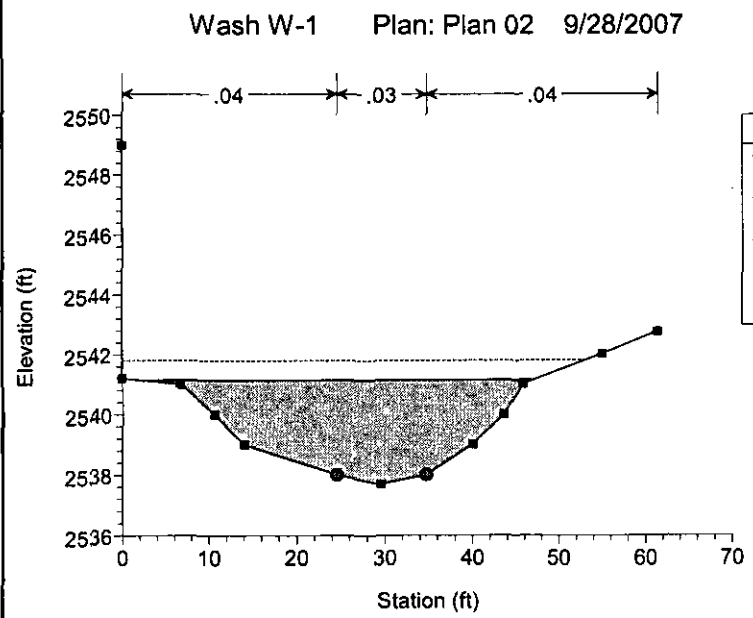
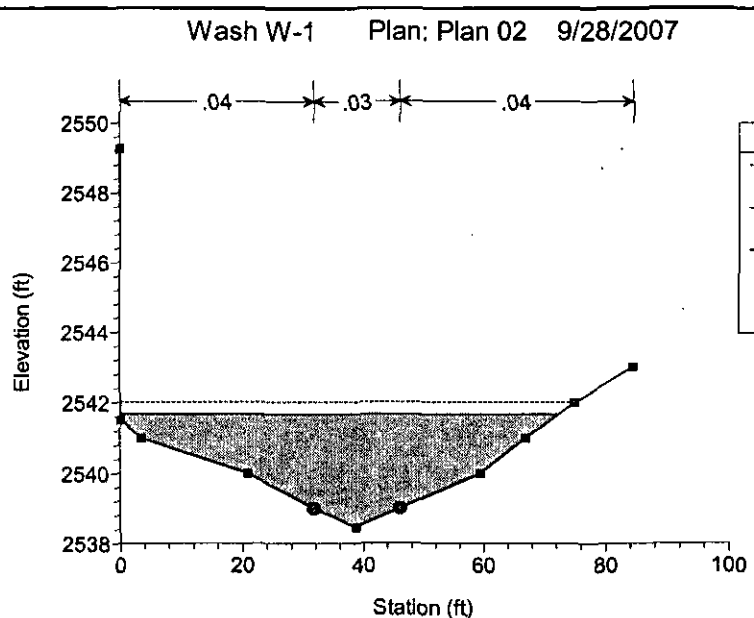
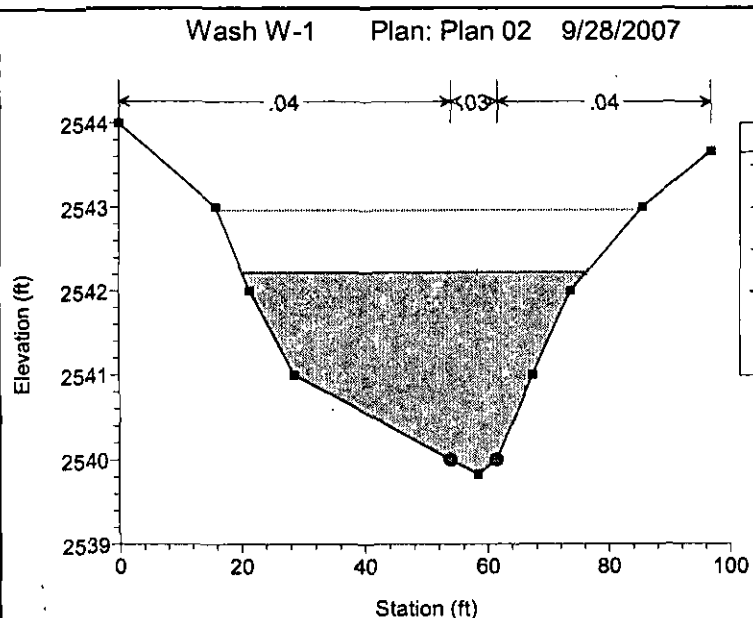
Reach	River Sta.	Left	Channel	Right
Wash W-1	11	58.47	49.8	50.03
Wash W-1	10	50.17	50.85	50.51
Wash W-1	9	50.02	50.51	50.29
Wash W-1	8	56.96	50.5	50.31
Wash W-1	7	52.54	49.75	49.99
Wash W-1	6	45.76	42.18	40.42
Wash W-1	5	30.54	20.58	21.29
Wash W-1	4	42.2	23.89	9.92
Wash W-1	3	108.63	71.04	74.11
Wash W-1	2.0902	culvert		
Wash W-1	2	107.85	101.61	93.35
Wash W-1	1			

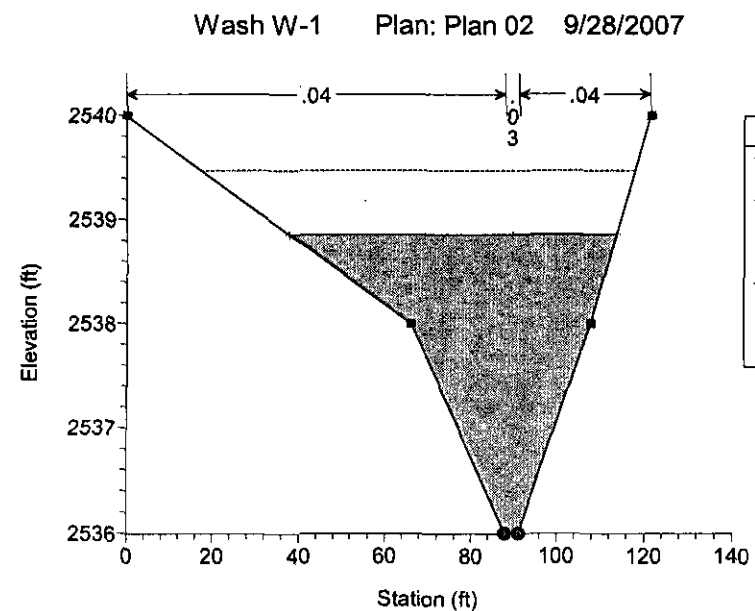
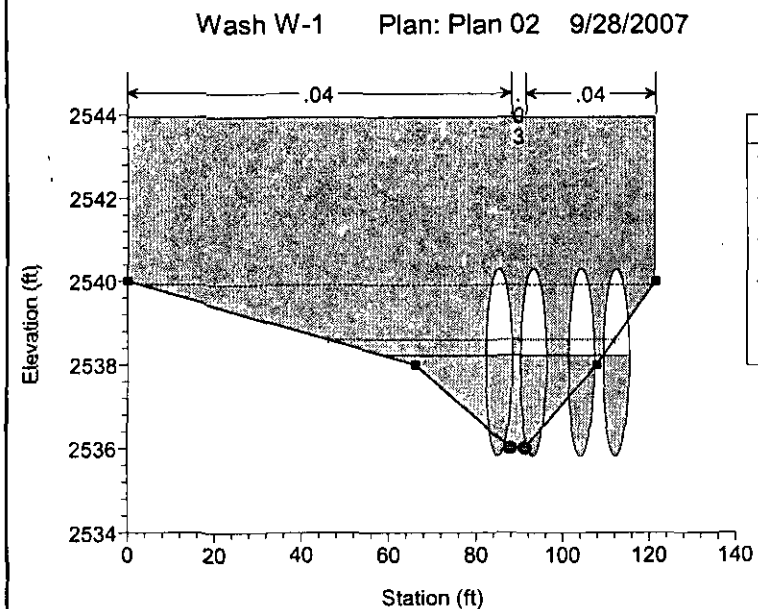
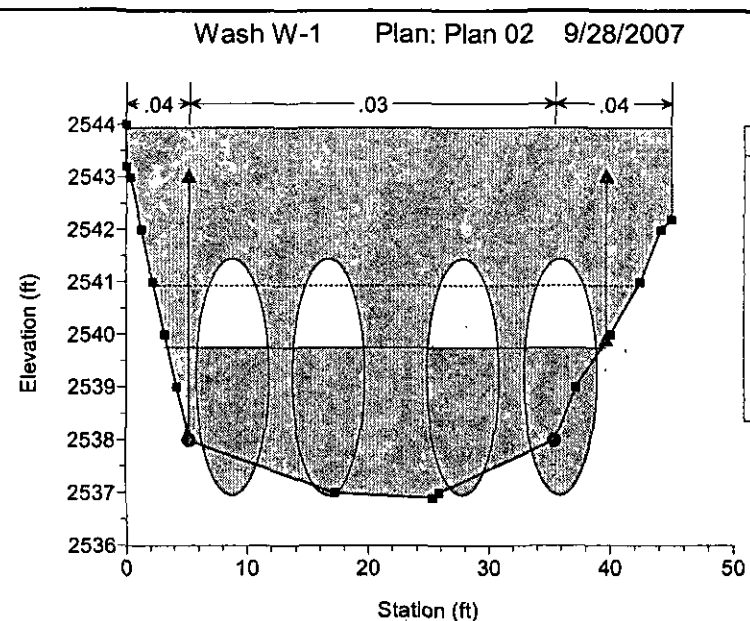
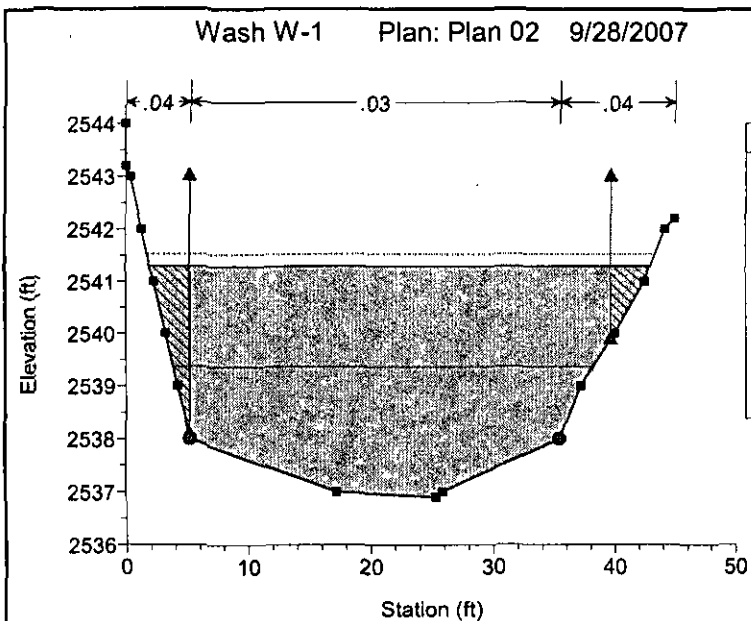
SUMMARY OF CONTRACTION AND EXPANSION COEFFICIENTS

River: W-1

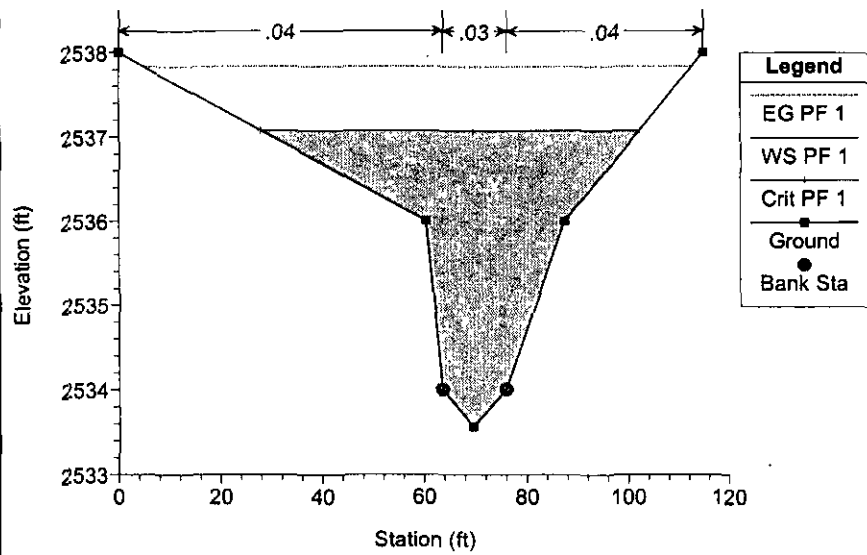
Reach	River Sta.	Contr.	Expan.
Wash W-1	11	.1	.3
Wash W-1	10	.1	.3
Wash W-1	9	.1	.3
Wash W-1	8	.1	.3
Wash W-1	7	.1	.3
Wash W-1	6	.1	.3
Wash W-1	5	.1	.3
Wash W-1	4	.1	.3
Wash W-1	3	.1	.3
Wash W-1	2.0902	culvert	
Wash W-1	2	.1	.3
Wash W-1	1	.1	.3







Wash W-1 Plan: Plan 02 9/28/2007



07-169~1

Type II 24-hr 2.00 hrs Rainfall=2.80"

Prepared by {enter your company name here}

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Pond 2P: DETENTION STORAGE

Inflow = 7.16 cfs @ 1.05 hrs, Volume= 0.092 af
 Outflow = 2.97 cfs @ 1.12 hrs, Volume= 0.089 af, Atten= 59%, Lag= 4.0 min
 Primary = 2.97 cfs @ 1.12 hrs, Volume= 0.089 af

Routing by Sim-Route method, Time Span= 0.00-2.00 hrs, dt= 0.01 hrs

Peak Elev= 2,544.72' Storage= 1,381 cf

Flood Elev= 2,544.77' Storage= 1,400 cf

Plug-Flow detention time= 6.4 min calculated for 0.089 af (97% of inflow)

Elevation (feet)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
2,541.27	0	0
2,541.77	200	200
2,542.77	400	600
2,543.77	400	1,000
2,544.77	400	1,400

Primary OutFlow (Dynamic Tailwater)

↑1=Culvert

#	Routing	Invert	Outlet Devices
1	Primary	2,541.27'	8.0" x 15.0' long Culvert CMP, square edge headwall, Ke= 0.500 Outlet Invert= 2,540.50' S= 0.0513 ' n= 0.015 Cc= 0.900

07-169~1

Type II 24-hr 2.00 hrs Rainfall=2.80"

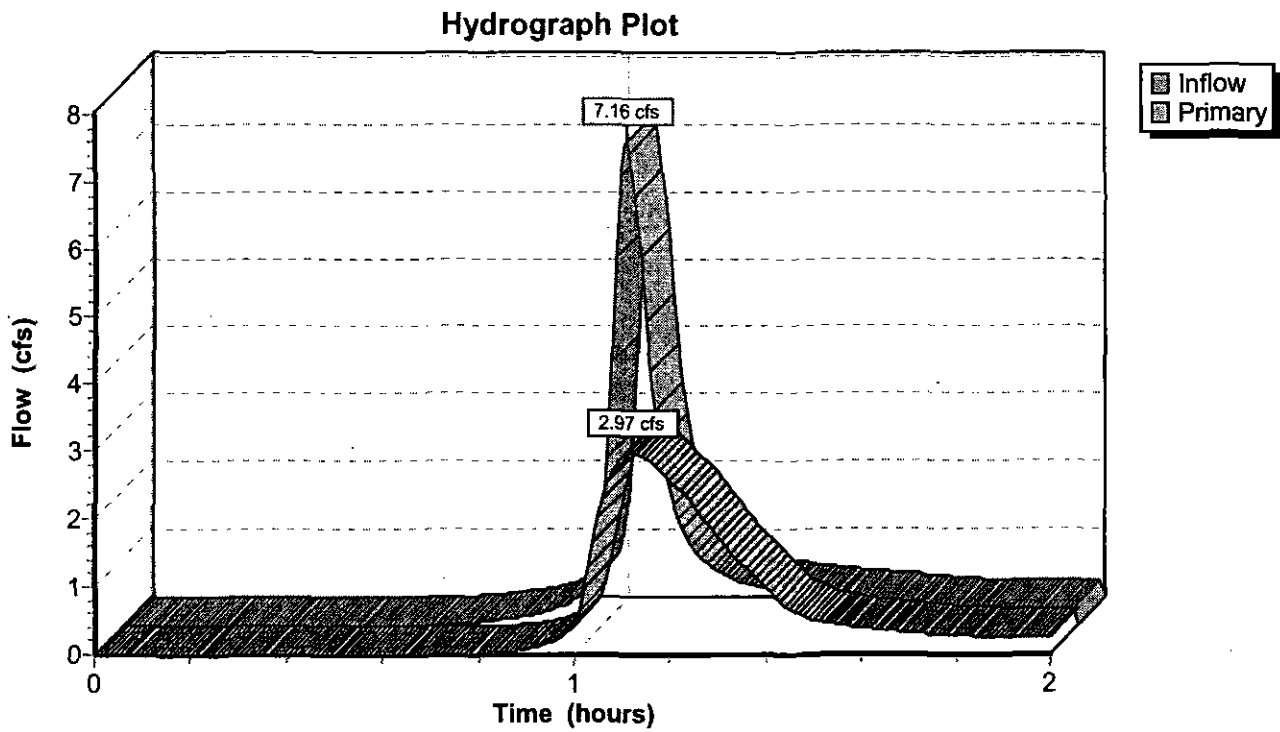
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Pond 2P: DETENTION STORAGE



07-169~1

Type II 24-hr 2.00 hrs Rainfall=2.80"

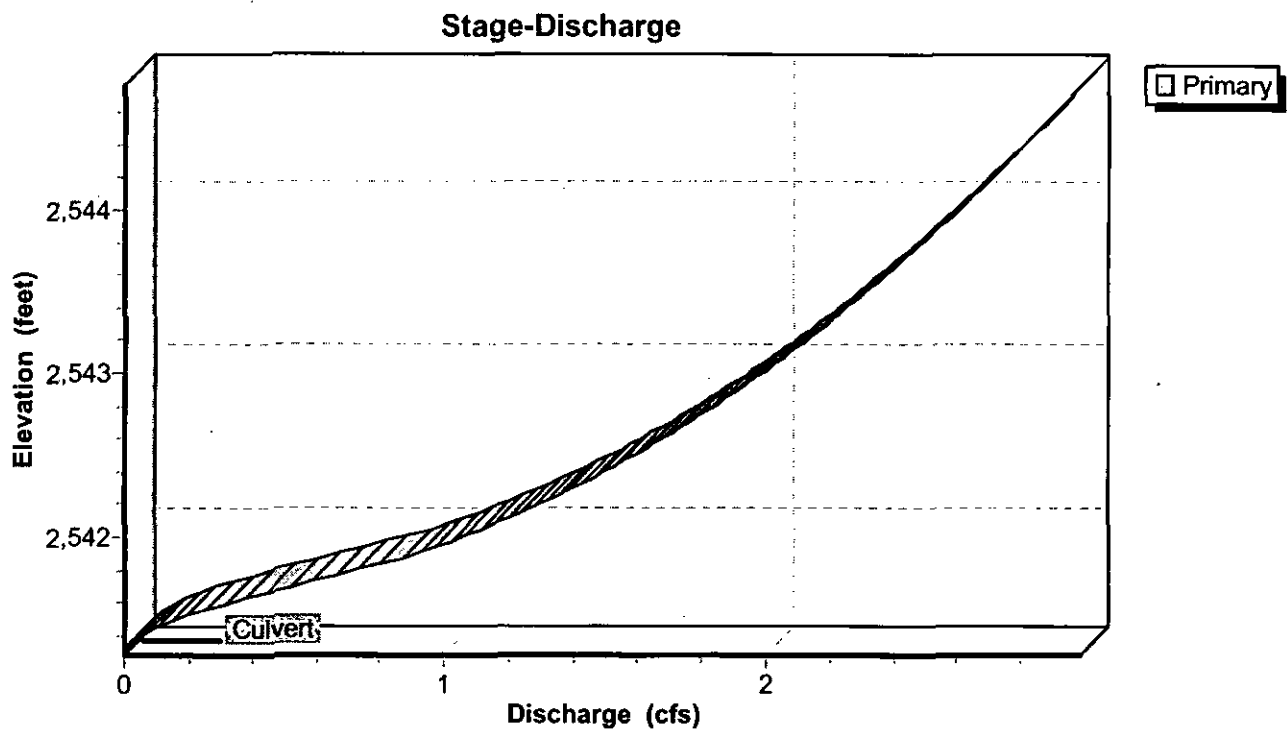
Prepared by {enter your company name here}

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Pond 2P: DETENTION STORAGE



07-169~1

Type II 24-hr 2.00 hrs Rainfall=2.80"

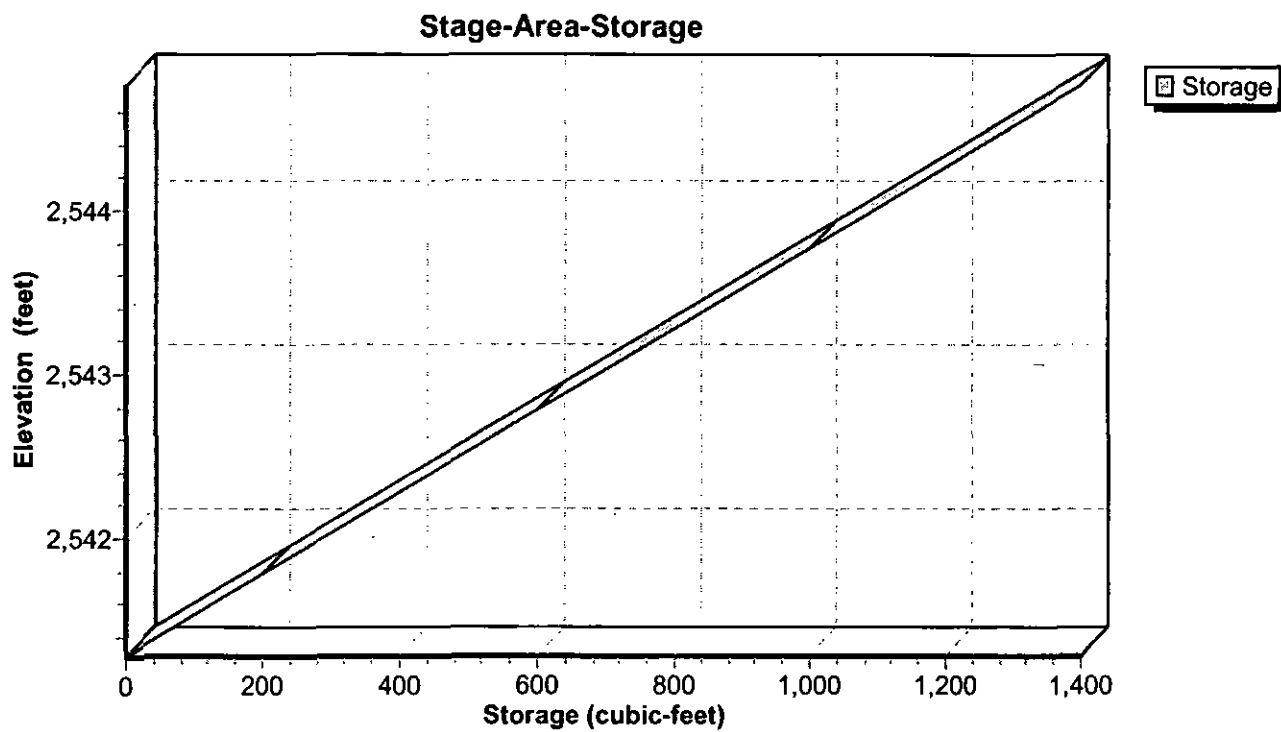
Prepared by {enter your company name here}

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Pond 2P: DETENTION STORAGE



07-169~1

Type II 24-hr 2.00 hrs Rainfall=2.80"

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Pond 2P: DETENTION STORAGE

