# DRAINAGE REPORTS

## ABBREVEATED WATER & SEWER NEED REPORTS

WATER STUDY

**WASTEWATER STUDY** 

STORMWATER WAIVER APPLICATION

### **ABBREVIATED WATER & SEWER NEED REPORT**

Non-Residential Water & Wastewater Development Fees

When applying for a Development Review Board Hearing, the Developer submits one report for each Non-Residential Development to the assigned City Project Coordinator. Project Coordinator submits this report to Water Resources.

| Project Name:   | Date:   |  |   |                           |                                      |  |  |
|---|---|--|---|---------------------------|--------------------------------------|--|--|
| Blue Sky Scottsdale   | Kara Land   |  |   | November 21               |                                      |  |  |
| Project Address:  |   |  |   | City Pre-Applica          |                                      |  |  |
| NE Corner of Scottsdale Road & C  |   |  |   | 396 - PA                  | A - 2010                             |  |  |
| Target Date to Submit Final Plans (Cons   | struction Documer   | nts):  | GPD/SF Bldg:                                | Building Size:            |                                      |  |  |
| June 2012 Type of Project:  |   |  | Varies/Use                                  | 976,169<br>Landscape Plan | Square Feet                          |  |  |
| Mixed Use Development; Residen  | tial and Cooling  | Towers   |   | 33,170                    | Square Feet                          |  |  |
| Number & Sizes of Domestic Water Met  |   | No. & Sizes Lan  | ndscape Meters:                             | Landscape Tur             |                                      |  |  |
| 3-4" Meters & 2-2" Meters   |   |  | Meter                                       | 1,435                     | Square Feet                          |  |  |
| NON-RESIDENTIAL DEVELOPMI   | ENT FEES:   |  |   |                           |                                      |  |  |
| Effective January 5, 2009   |   | WATER<br>Dev. Fee  | RESOURCE<br>Dev. Fee                        | WASTEWATER<br>Dev. Fee    | TOTAL<br>Dev. Fees                   |  |  |
| COST PER GALLON   |   | \$9.36   | \$2.41                                      | \$18.26                   | \$30.03                              |  |  |
| . FEE CALCULATION TABLE: (Mu  | Itiply Cost per G   | allon above x G  | allons per Day b                            | pelow)                    |                                      |  |  |
| TYPE OF WATER DEMAND  | Gallons/Day<br>(GPY / 365)  | WATER<br>Dev. Fee  | RESOURCE<br>Dev. Fee                        | WASTEWATER<br>Dev. Fee    | TOTAL<br>Dev. Fees                   |  |  |
| Domestic - TO SEWER   | 150,162   | \$1,405,516.32   | \$361,890.42                                | \$2,741,958.12            | \$4,509,364.86                       |  |  |
| Domestic - NOT to Sewer   | 31,320  | \$293,155.20   | \$75,481.20                                 | - None -                  | \$368,636.40                         |  |  |
| Landscape - PLANTS & TREES  | 1,990   | \$18,626.40  | \$4,795.90                                  | - None -                  | \$23,422.30                          |  |  |
| Landscape - TURF  | 144   | \$1,347.84   | \$347.04                                    | - None -                  | \$1,694.88                           |  |  |
| Credit for pre-existing water meter   |   |  |   |                           |                                      |  |  |
| SUB-TOTALS  | 183,616   | \$1,718,645.76   | \$442,514.56                                | \$2,741,958.12            | \$4,903,118.44                       |  |  |
| ADMINISTRATION FEE  | 2.04%   | \$35,060.37  | \$9,027.30                                  | \$55,935.95               | \$100,023.62                         |  |  |
| TOTAL DEVELOPMENT FEES  | y 24 2 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1                            | \$1,753,706.13   | \$451,541.86                                | \$2,797,894.07            | \$5,003,142.06                       |  |  |
| WATER METER FEE (5/8"=\$70, 3/4   | "=\$95, 1"=\$140  | , 1.5"=\$270, 2"=\$  | 350, 3"=\$1,905,                            | 4"= \$3,135)              | \$10,455.00                          |  |  |
| TOTAL FEES  |   |  |   |                           | \$5,013,597.06                       |  |  |
| . CONTACT INFORMATION & CITY  | APPROVAL:   |  |   |                           |                                      |  |  |
| Printed Name of Owner:  | E-mail Addres   | s:   |   | Phone #:                  | Cell Phone #:                        |  |  |
| Brian Kearney   | bkearney@gr   | rayus.com  |   | (602) 954-0109            | ,                                    |  |  |
| Printed Name of Preparer:   | E-mail Addres   |  |   | Phone #:                  | Cell Phone #:                        |  |  |
| Brian Kearney   | bkearney@gr   |  |   | (602) 954-0109            | (602) 370-325                        |  |  |
| Signature of Owner.*  | Date:   | CITY USE ONL   | Y: Water Resource                           | ces Approval:             | Date:                                |  |  |
| By signing above, I acknowledge that I am aw ust be submitted upon the first submittal of Co 04% administration fee must be paid prior to cars if the average annual water and/or wasteness not attest to or validate the accuracy of the | instruction Documen<br>obtaining a Building F<br>water demand excee | ts for Building Plan Re<br>Permit. I am aware of<br>ds the estimated dem | eview & Permits. I a<br>the fees and penalt | am aware that develo      | pment fees and a ced after three (3) |  |  |
| Water & Sewer Use Limit - Gallons   | per Month:  | 5,584,987  | Gallo                                       | ns per Year:              | 67,019,840                           |  |  |
| gpd/sf - Domestic 0.186   | gpd/sf Plants   | 0.060  |   | gpd/sf Turf               | 0.100                                |  |  |

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City of Scottsdale Water Resources

Effective January 5, 2009

### **CALCULATION TABLES**

Non-Residential Water and Wastewater Development Fees

|  |         | GALLONS F | ER DAY | MEASURABLE       | (B) ENTER                                   | (A x B) =  |
|--|---------|-----------|--------|------------------|---|--|
| TYPE OF USE                            | MINIMUM |           | HIGH   | UNIT             | # of UNITS                                  | GAL./DAY   |
| Air Services - Jet Hangars             | 0.05    | 0.07      | 0.08   | Sq. Ft. of Bldg. |   |  |
| Auto Dealer (no service)               | 1,120   | 1,400     | 1,680  | Metered Account  |   |  |
| Auto Dealer (with service)             | 2,530   | 3,165     | 3,800  | Metered Account  | 17.0  |  |
| Auto Service Station                   | 900     | 1,000     | 1,100  | First Bay        |   |  |
| Auto Service Station                   | 450     | 500       | 550    | Additional Bay   |   |  |
| Bank                                   | 0.03    | 0.05      | 0.06   | Sq. Ft. of Bldg. |   |  |
| Barber Shop                            | 44      | 55        | 66     | Seat             |   |  |
| Beauty Salon                           | 216     | 270       | 324    | Station          |   |  |
| Bowling Alley                          | 70      | 75        | 80     | Lane             |   |  |
| Car Wash (coin-op)                     | 374     | 384       | 394    | Bay              | 2,000                                       | BEN SIN  |
| Car Wash (full service)                | 10,000  | 14,600    | 19,200 | Metered Account  |   |  |
| Child Care / Day Care Facility         | 0.15    | 0.17      | 0.19   | Sq. Ft. of Bldg. |   | F 842 12 12  |
| Church                                 | 4       | 5         | 6      | Seat             |   |  |
| Church (with kitchen)                  | 6       | 7         | 8      | Seat             |   |  |
| Dental Office                          | 0.07    | 0.09      | 0.10   | Sq. Ft. of Bldg. | MED CEL                                     |  |
| Department Store                       | 0.20    | 0.30      | 0.40   | Sq. Ft. of Bldg. | - W. C. |  |
| Department Store                       | 320     | 400       | 480    | Toilet Room      | St. Medical                                 |  |
| Drug Store                             | 0.12    | 0.14      | 0.16   | Sq. Ft. of Bldg. | 1.20  | De la companya della companya della companya de la companya della  |
| Dry Cleaner                            | 0.36    | 0.45      | 0.54   | Sq. Ft. of Bldg. |   |  |
| Grocery Store                          | 0.16    | 0.18      | 0.19   | Sq. Ft. of Bldg. | 15 DEC 28                                   |  |
| Hospital                               | 200     | 250       | 300    | Bed              |   |  |
| Hotel and Resort                       | 96      | 120       | 144    | Unit             | THE STATE OF                                |  |
| Industrial / Manufacturing             | 20      | 25        | 30     | Employee         |   |  |
| Industrial / Mfg. (with cafeteria)     | 25      | 30        | 35     | Employee         |   | Size of the  |
| Industrial / Mfg. (cafeteria & showers | 35      | 40        | 45     | Employee         | 17.7  |  |
| Laundry (coin-op)                      | 147     | 184       | 221    | Machine          | 4000  |  |
| Laundry (commercial)                   | 201     | 251       | 301    | Machine          |   |  |
| Medical Lab                            | 2,320   | 2,905     | 3,490  | Metered Account  |   | DE LIPERIO   |
| Medical Office                         | 0.07    | 0.09      | 0.10   | Sq. Ft. of Bldg. |   |  |
| Motel                                  | 80      | 100       | 120    | Unit             |   | 14.6   |
| Motel (with kitchen)                   | 90      | 110       | 130    | Unit             |   |  |
| Movie Theater                          | 3       | 4         | 5      | Seat             | 2, 1 17 17                                  |  |
| Nursery                                | 2,950   | 3,690     | 4,430  | Metered Account  |   |  |
| Office Building                        | 0.07    | 0.09      | 0.10   | Sq. Ft. of Bldg. | Control of the last                         |  |
| Real Estate Office                     | 0.03    | 0.05      | 0.06   | Sq. Ft. of Bldg. |   | The state of the s |
| Restaurant (with auto. dishwasher)     | 0.60    | 0.80      | 1.00   | Sq. Ft. of Bldg. |   |  |
| Restaurant (w/o auto. dishwasher)      | 0.20    | 0.25      | 0.30   | Sq. Ft. of Bldg. |   | -W-3 - N - 11  |
| Retail Shop                            | 0.03    | 0.05      | 0.06   | Sq. Ft. of Bldg. |   | BATTA LA   |
| School                                 | 0.03    | 0.05      | 0.06   | Sq. Ft. of Bldg. |   | 1 3 V 2 2  |
| Senior Care Facility                   | 90      | 100       | 110    | Bed Bed          |   |  |
| Shell Building (retail & restaurant)   | 0.16    | 0.18      | 0.19   | Sq. Ft. of Bldg. |   |  |
| Shopping Center                        | 0.16    | 0.18      | 0.19   | Sq. Ft. of Bldg. |   | Control of   |

The City provides water demand data to assist developers with demand estimates. Regional and local studies provide minimum acceptable standards for demand estimates and development fees. Demand estimates will be approved by Water Resources staff if they meet or exceed the minimum standards provided above. Demand estimates may also be determined by metered water billing statements for similar projects. These tables serve only as informational guides. The Developer is responsible for the accuracy of the water and wastewater demand estimates.

#### **CALCULATION TABLES**

Non-Residential Water and Wastewater Development Fees

| TABLE #2: DOMESTIC WAT |                 |                    | tive in the state of    |                       |  |
|------------------------|-----------------|--------------------|-------------------------|-----------------------|--|
| TYPE OF USE            | (A)<br>STANDARD | MEASURABLE<br>UNIT | (B) ENTER<br># of UNITS | (A x B) =<br>GAL,/DAY |  |
| Car Washes             | 15%             | Water Demand       |                         |                       |  |
| Pools & Fountains      | 0.144           | Sq. Ft. of Pool    |                         |                       |  |
| Cooling Towers         | 0.006           | Cu. Ft. of Area    |                         |                       |  |
| Cooling Towers         | 21.60           | Ton of Cooler      |                         |                       |  |
| Evaporative Coolers    | 0.003           | Cu. Ft. of Area    |                         |                       |  |
| Misting Systems        | 0.003           | Cu. Ft. of Area    |                         |                       |  |
| Wash Down Areas        | 15%             | Water Demand       |                         | ,                     |  |

#### TABLE #3: LANDSCAPE WATER USE -- NOT to SEWER

| TYPE OF USE  | (A)<br>Standard | MEASURABLE UNIT   | (B) ENTER<br># of UNITS | (A x B) =<br>GAL./DAY |
|--|-----------------|-------------------|-------------------------|-----------------------|
| Plants & Trees                                     | 0.06            | Sq. Ft. of Plants |                         |                       |
| Temporary Re-Vegetation -<br>Native Plants & Trees | 0.01            | Sq. Ft. of Plants |                         |                       |
| Turf Landscaping                                   | 0.10            | Sq. Ft. of Turf   |                         |                       |

#### TABLE #4: DOMESTIC WATER USE -- BASED ON SIZE OF WATER METER

| SIZE OF WATER METER | Meter<br>Fees | Average Gallons per YEAR | Average Gallons per MONTH | Average Gallons<br>per DAY |
|---------------------|---------------|--------------------------|---------------------------|----------------------------|
| 5/8"                | \$<br>70      | 114,610                  | 9,551                     | . 314                      |
| 3/4"                | \$<br>95      | 107,675                  | 8,973                     | 295                        |
| 1"                  | \$<br>140     | 266,450                  | 22,204                    | 730                        |
| 1.5"                | \$<br>270     | 566,115                  | 47,176                    | 1,551                      |
| 2"                  | \$<br>350     | 1,243,920                | 103,660                   | 3,408                      |
| 3"                  | \$<br>1,905   | 2,872,915                | 239,410                   | 7,871                      |
| 4"                  | \$<br>3,135   | 8,544,650                | 712,054                   | 23,410                     |
| 6"                  | \$<br>5,510   | 12,689,225               | 1,057,435                 | 34,765                     |

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# WATER BASIS OF DESIGN REPORT FOR BLUE SKY SCOTTSDALE

#### PREPARED FOR

# GRAY DEVELOPMENT, LLC 4040 E CAMELBACK ROAD, SUITE 275 PHOENIX, AZ 85018

(602) 508-7141 Contact: Brian Kearney

#### PREPARED BY

ZACKARY POPE, P.E. DAVID EVANS & ASSOCIATES, INC. 4600 E WASHINGTON STREET, SUITE 430 PHOENIX, AZ 85034 (602) 678-5151

> 1<sup>ST</sup> SUBMITTAL OCTOBER 2011

DEA PROJECT NO. GRYD0000-0001



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#### **EXHIBITS**

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#### **APPENDICES**

ABCD

E



#### TITLE

Vicinity Map
Water Distribution System Improvements
Existing Utilities and Surface Improvements

#### TITLE

City of Scottsdale Water Quarter Section Map Fire Hydrant Flow Test Results Fire Flow Calculation Table Water Demand Table Water Modeling Output

#### A. INTRODUCTION

This basis of design report was completed under a contract with the Gray Development, LLC. The proposed Blue Sky Scottsdale project consists of three buildings containing retail, residential, office, restaurant, hotel, and grocery components. An underground parking structure will also be provided. The buildings will be constructed in two phases. The parking structure, the North Building, and the Main Building will be constructed as part of Phase 1. The East Building will be constructed as part of Phase 2. However, all of the water improvements will be constructed during Phase 1.

#### 1. Project Location

The proposed Blue Sky Scottsdale project is located near the northeast corner of the intersection of Scottsdale Road & Camelback Road within the city of Scottsdale, Arizona. The site is located within the northwest quarter of Section 23 of Township 2 North, Range 4 East of the Gila and Salt River Base and Meridian. The site is approximately 4.28 acres and irregularly shaped. It is generally bound by Scottsdale Road to the west, the Fashion Square road entrance alignment to the south, 72<sup>nd</sup> Way to the east, and Coolidge Street to the north. The area's street system in relationship to the location of the site is illustrated in Exhibit 1, the project's vicinity map.

#### 2. Site Zoning

The zoning of the Blue Sky Scottsdale site is discussed in Section C.1 of this report.

#### 3. General Plan

The Blue Sky project will provide strong support for the goals and policies of the City's General Plan. It will be consistent with the Downtown Plan and reflect its vision, goals, and policies. It will support the City's efforts to "boldly look to its metropolitan future" through the development of an urban oasis that brings to life the City's vision for:

- Mixed-use urban neighborhoods
- World class planning, architecture, and design
- Sustainability
- Connectivity and walkability
- Economic vitality, and
- Worldwide recognition as the premier destination in the United States

#### **B. DESIGN DOCUMENTATION**

#### 1. Design Procedures

The analysis of the proposed water system was done in compliance with the City of Scottsdale Design Standards & Policies Manual.

The proposed water distribution system will serve the project in accordance with City of Scottsdale design standards and the ADEQ Engineering Bulletin 10.

The estimated Average Day Demand of the Blue Sky Scottsdale project was determined based on the following Average Day Demand values. All of the values below include both inside use and outside use demands.

- Residential Units = 185.3 gallons per person per day
- Hotel = 446.3 gallons per person per day per room
- Retail = 0.8 gallons per square foot per day
- Restaurant = 1.3 gallons per square foot per day
- Offices = 0.6 gallons per square foot per day
- Grocery = 0.7 gallons per square foot per day

Note that the Grocery Land Use is not specifically listed in Figure 6.1-2 of the Design Standards and Policy Manual. However, the demand of 0.7 gallons per square foot per day was utilized for the design of the Scottsdale Quarter project located near the intersection of Scottsdale Road & Greenway Hayden Loop.

The Maximum Day Demand was calculated using a factor of 2.0 times the Average Day Demand. The Peak Hour Demand was determined by multiplying the Average Day Demand by 3.5.

#### 2. Software

Water demands were determined using a Microsoft Excel spreadsheet. DEA created a WaterCAD™ model of the proposed water system. WaterCAD is a water distribution system modeling software created by Haestad Methods. To run WaterCAD, a user inputs the water system map, waterline sizes, and demand locations. WaterCAD connects these elements as a system and uses mathematical equations to determine flow directions, flow magnitudes and pressures for the water system modeled.

#### C. EXISTING CONDITIONS

#### 1. Zoning and Land Use

The site falls under the Downtown Regional Multiple Use Type 2 Land Use designation. The site is currently zoned Downtown Regional Commercial Office, Type 2, Planned Block Development Downtown Overlay (D/RCO-2 PBD DO) with amended development standards.

#### 2. Existing Topography, Vegetation, and Landform Features

Generally, the existing topography slopes in a southeasterly direction at approximately 0.40%, with approximately 3 feet of fall across the property. The site in its existing condition is generally an unimproved dirt lot. An entrance road bisects the site that provides access to the existing Safari Drive condominiums located to the east of the site. The entrance road also provides access to a commercial development located to the south of the site.

#### 3. Existing Utilities

There is existing water infrastructure located within the adjacent streets as illustrated on the City of Scottsdale Quarter Section map provided in Appendix A. This infrastructure includes an existing 6-inch ACP and an existing 16-inch DIP waterline within Scottsdale Road. There is also an existing 8-inch DIP waterline within Coolidge Street. An 8-inch waterline is located within the northern portion of 72<sup>nd</sup> Way and connects to the waterline in Coolidge Street. A portion of this line in 72<sup>nd</sup> Way will be removed in order to construct the underground parking structure. The fire hydrant at the end of this line will be relocated to the intersection of Coolidge Street and 72<sup>nd</sup> Way.

#### 4. Existing Master Plans or Design Reports

A Water Basis of Design Report for Safari Drive was prepared by DEA in 2006 for the Safari Drive condominiums. Phase 1 of Safari Drive has been constructed.

#### 5. Certified Flow Testing

A fire flow test was performed for this project on fire hydrants adjacent to the project site. The results and location of the test are provided in Appendix B.

#### D. PROPOSED CONDITIONS

#### 1. Site Plan

Exhibit 2 illustrates the proposed site improvements.

#### 2. Proposed Connections

Exhibit 2 illustrates the proposed connections to the existing system. Along Scottsdale Road, two 2-inch service lines, one 4-inch service line, and one 6-inch fire hydrant line will connect to the existing 16-inch waterline within Scottsdale Road. Additionally, two 4-inch service lines, one 8-inch fire line, and one 6-inch fire hydrant line will connect to the existing 8-inch line within Coolidge Street. The service and fire line sizes are based on the requirements of the project's Mechanical Engineer and have been modeled in this report to assess their performance.

A portion of the existing public waterline within 72<sup>nd</sup> Way will be removed in order to construct the underground parking garage. A public abandonment will be required in order to remove a portion of this line.

Private water service lines will be installed under landscaping when necessary. Backflow prevention assemblies will be installed on private waterlines.

A new private fire hydrant will be installed within the development south of the Main Building. The addition of the new fire hydrant allows Fire Department access within 600' as measured along the accessible fire routes to the east side of the East Blue Sky Building and it can also serve Safari Phase II. The existing public fire hydrant in 72<sup>nd</sup> Way will be relocated to near the intersection of Coolidge Street & 72<sup>nd</sup> Way. The relocation of the fire hydrant within 72<sup>nd</sup> Way will also provide added protection to both Blue Sky and Safari Phase II.

#### 3. Water Zone, Fire Flow, and System Pressures

The Blue Sky development lies within the City of Scottsdale Water Zone 1-A per the 2008 Integrated Water Master Plan prepared by Carollo. This zone serves areas with ground elevations from 1250 feet to 1330 feet. The finished floor (FF) elevation of the first levels of the North and East buildings is 1280.8'. The FF elevation of the first level of the Main building is 1280.5'.

The static pressure within the 16-inch waterline in Scottsdale Road is approximately 96 psi based on the flow test performed by EJ Flow Test. The buildings will incorporate private booster pumps to supply water to the upper floors and will be designed to maintain a minimum residual pressure of 50 psi at the highest finished floor level under normal operating conditions. The building system will maintain a minimum pressure of 20 psi under fire flow conditions.

All buildings on site will be fully sprinkled and will be of construction Type IA based on the *International Building Code*. The garage will be fully sprinkled and will be of Type IB construction.

The Design Standards and Policies Manual dictates that the minimum fire flow for high rise structures is 2,500 gpm. Per the 2006 International Fire Code, the fire flow calculation area of buildings constructed of Type IA or IB construction shall be the greater of the area of the three largest successive floors of the building or the largest floor area of the garage. Additionally, up to a 75% reduction may be taken when the building is supplied with an approved automatic sprinkler system. Based on this information and the table provided in Appendix C, the fire flow for the Blue Sky development will be 2,500 gpm with a residual pressure of 30 psi.

#### E. COMPUTATIONS

#### 1. Computer Calculations

A hard copy of the demand calculations and the WaterCAD output for this report has been provided in Appendices D and E. The modeling in this Blue Sky basis of design report accounts for the future Safari Phase II development. As a factor of safety, a 20% increase in dwelling units for Phase 2 of the Safari Drive project.

#### 2. Demand Summary

Table E.2.1 summarizes the water demands for the Blue Sky project. A detailed demand table that breaks down the values listed below is provided in Appendix D.

TABLE E.2.1 – WATER DEMAND SUMMARY

| Phase                      | Average Day<br>(gpm) | Max Day<br>(gpm) | Peak Hour<br>(gpm) |
|----------------------------|----------------------|------------------|--------------------|
| 1                          | 97                   | 193              | 339                |
| 1 & 2 + Safari<br>Phase II | 223                  | 447              | 782                |

#### 3. Water Modeling Results

Average Day, Max Day, Max Day + FF, and Peak Hour demand scenarios were analyzed for Phase 1 and Phase 1 + Phase 2 + Safari Phase II. The water demand for the Safari Phase II development was modeled at the same location (J-9) that it was originally modeled in the Water Basis of Design Report for Safari Drive. This location conforms to the location of the single water service that was proposed for the Safari Phase II project.

The WaterCAD output for the most conservative scenarios (Max Day + FF and Peak Hour) for the proposed water system modeled can be found in Appendix E. This output includes system pressures, pipe velocities, demands, and headloss information for each of the two phases modeled.

All pressures in the model are at street level. The lowest pressure available in the system during the Peak Hour Scenario is 58 psi. Based on the City's criteria requiring 50 psi at the buildings' highest levels, any building requiring water above two stories will require a private booster pump system.

The available fire flow for each model was calculated at the street within the distribution lines. The models do not account for sprinkler demands within each building. Each building's individual sprinkler demands and the services that feed them must be assessed by the building's sprinkler system designer.

All backflow prevention assemblies were modeled by adding a WaterCAD General Purpose Valve and its corresponding headloss curve.

The following table summarizes the expected pressures during the Phase 1 scenario. The pressures range from 63 psi to 72 psi for all scenarios.

TABLE E.3.1 - PHASE 1 PRESSURE SUMMARY

| Model S     | Model Scenario |                  | Max                     | Ave |
|-------------|----------------|------------------|-------------------------|-----|
|             | Pressure (psi) | 63               | 72                      | 70  |
| Average Day | Node           | J-12, J-16, J-22 | Multiple, See<br>Output | •   |
| ,           | Pressure (psi) | 62               | 72                      | 70  |
| Max Day     | Node           | J-12, J-16, J-22 | Multiple, See Output    | •   |
|             | Pressure (psi) | 59               | 72                      | 70  |
| Peak Hour   | Node           | J-12, J-16, J-22 | Multiple, See<br>Output | -   |

All nodes pass the Max Day + Fire Flow scenario with all pressures greater than or equal to 30 psi.

The following table summarizes the expected pressures during the Phase 1 & 2 + Safari Phase II scenario. The pressures range from 58 psi to 72 psi for all scenarios.

TABLE E.3.2 - PHASE 1 & 2 + SAFARI PHASE II PRESSURE SUMMARY

| Model S     | Model Scenario |                  | Max                     | Ave |
|-------------|----------------|------------------|-------------------------|-----|
| _           | Pressure (psi) | 62               | 72                      | 70  |
| Average Day | Node           | J-12, J-16, J-22 | Multiple, See<br>Output | -   |
|             | Pressure (psi) | 58               | 72                      | 69  |
| Max Day     | Node           | J-12, J-16, J-22 | Multiple, See<br>Output | -   |
| De de III   | Pressure (psi) | 59               | 72                      | 69  |
| Peak Hour   | Node           | J-12, J-16, J-22 | J-27                    | -   |

All nodes pass the Max Day + Fire Flow scenario with all pressures greater than or equal to 30 psi.

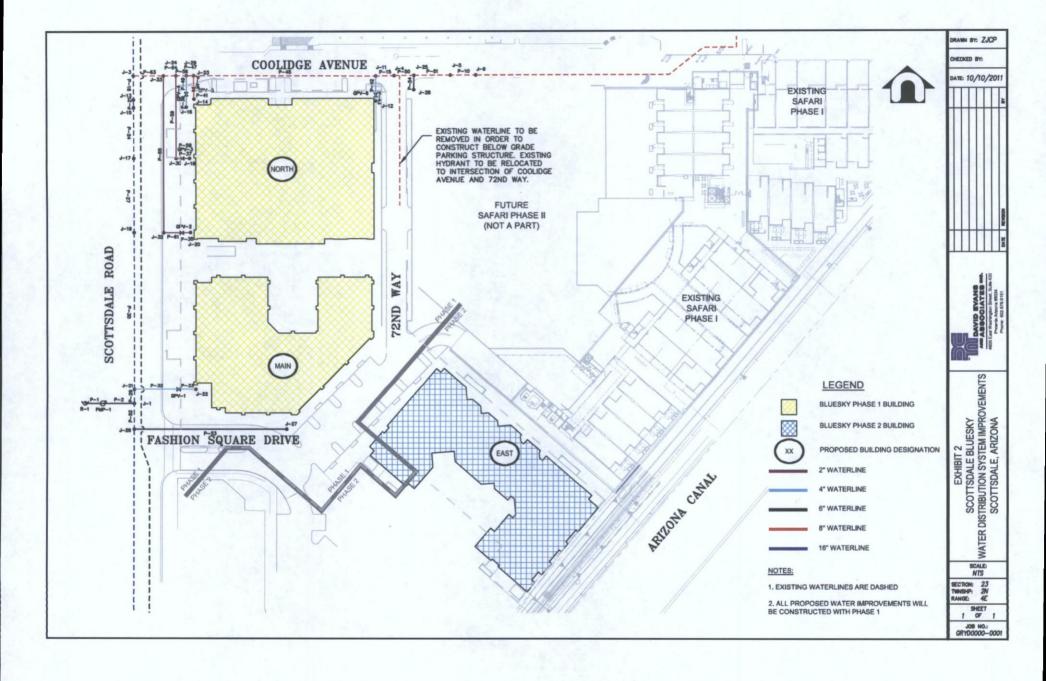
All non-fire flow headlosses are less than 10 ft/1000ft. Detailed modeling output has been provided in Appendix E. Based on the modeling results, the existing infrastructure and proposed water line improvements can support the project.

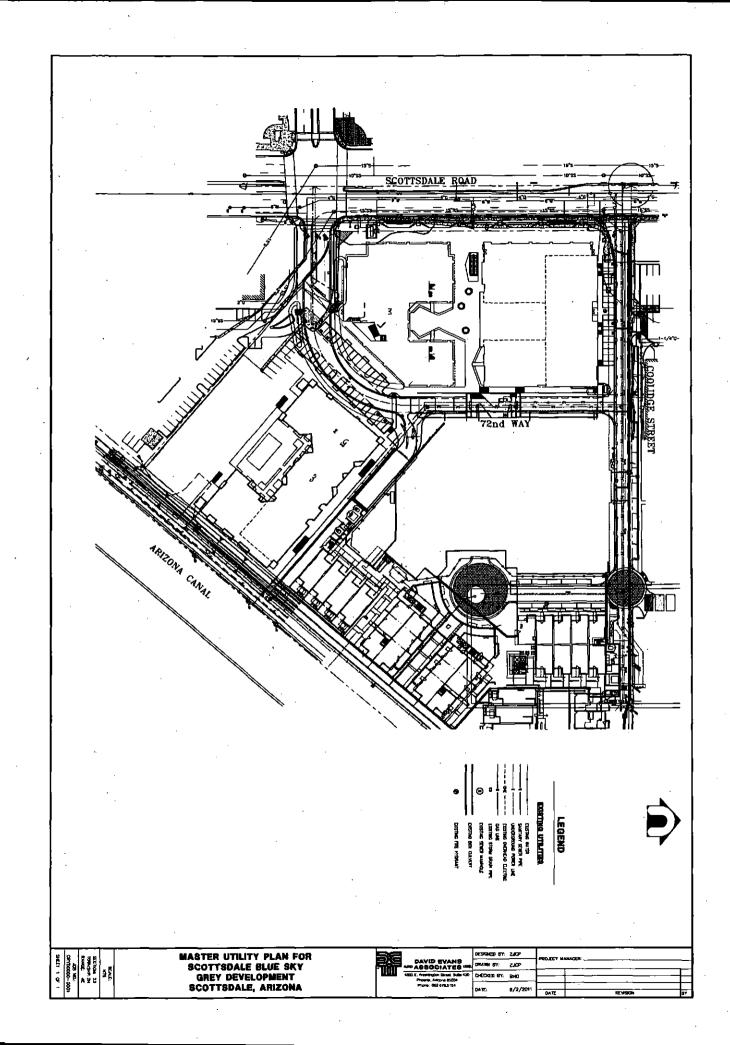
#### F. SUMMARY

The proposed Blue Sky water distribution system is illustrated on Exhibit 2. New water services, a new fire line, and a new hydrant will be installed as part of this project. An existing fire hydrant will be relocated, as well.

The proposed water improvements meet all City of Scottsdale pressure, velocity, and headloss requirements. It is recommended that the Blue Sky water distribution system improvements be designed as dictated in this report.

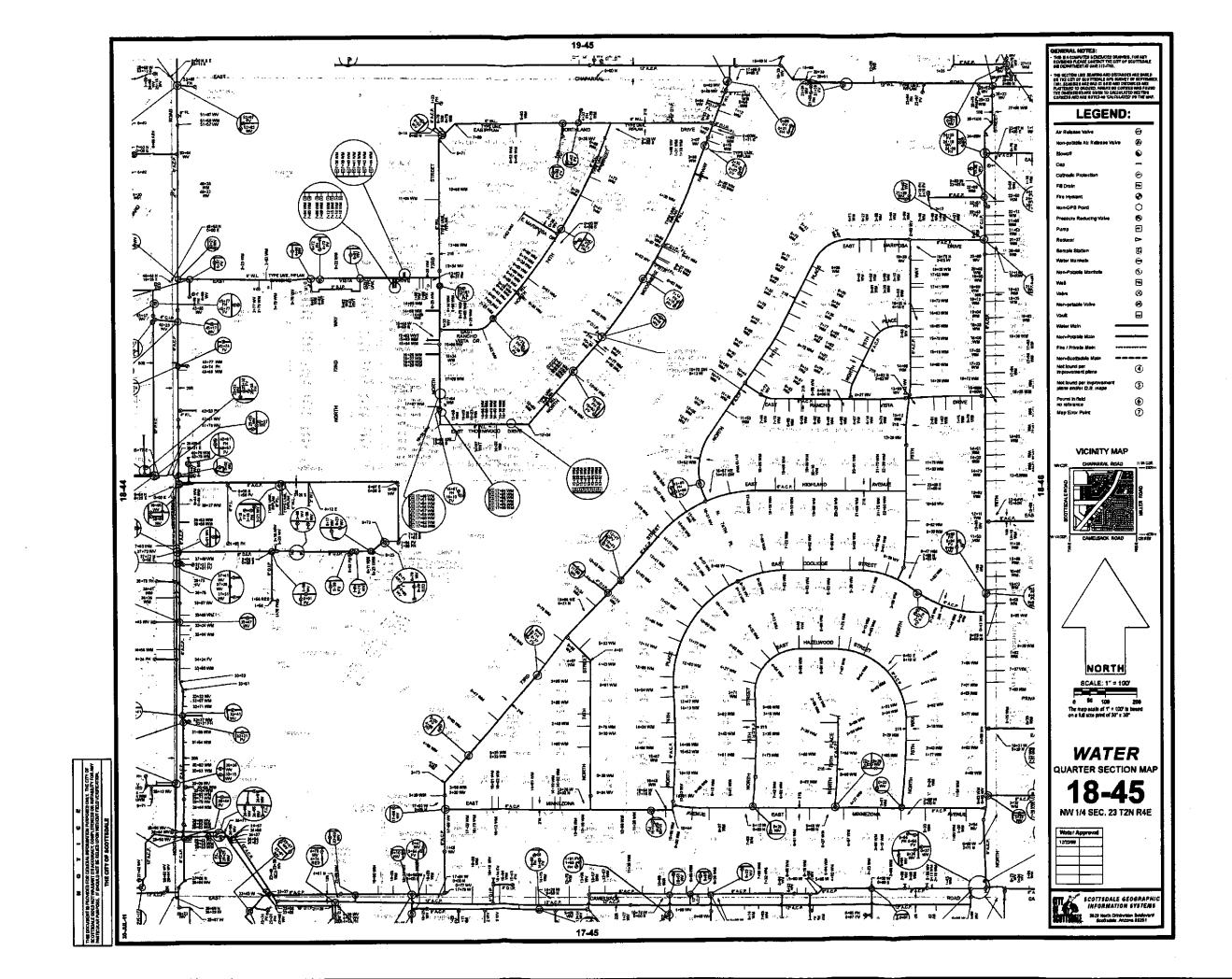
Although exact dates of construction are unknown at this time, it is currently anticipated that Phase 1 will begin construction in June 2012. Phase 1 is expected to be complete in April 2014. Phase 2 is anticipated to begin construction in January 2015. Phase 2 is expected to be complete in April 2016. This schedule is subject to change.





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APPENDIX A
CITY OF SCOTTSDALE WATER QUARTER SECTION MAP



# APPENDIX B FIRE HYDRANT FLOW TEST RESULTS



FLOW TESTING SERVICES

### FLOW TEST SUMMARY

EJ Flow Tests Project Name:

Scottsdale Blue Sky

EJ Flow Tests Project No.:

Project Address:

Camelback Road and Scottsdale Road (northeast corner), Scottsdale, Arizona

#### **Raw Test Data:**

Date of Flow Test: August 15, 2011 Time of Flow Test: 7:30 AM

Data is current and reliable until: February 15, 2012

Static Pressure:

96 psi

(measured in pounds per square inch)

Residual Pressure:

85 psi

(measured in pounds per square inch)

Pitot Pressure:

24 psi (4-1/2 inch)

25 psi (2-1/2 inch)

(measured in pounds per square inch)

Fire Hydrant Orifice Diameter: One (4-1/2 inch)

(measured in inches)

One (2-1/2 inch)

Coefficient of Discharge: .90 = smooth outlet each

Flowing GPM: 3,050

2,211 gpm + 839 gpm = 3,050 gpm(measured in gallons per minute)

(.83 coefficient applied for pumper outlet per NFPA 291)

GPM @ 20 PSI: 8,661

Data with 24 PSI Safety Factor (minimum):

Static Pressure:

72.0 psi

(measured in pounds per square inch)

Scottsdale requires a maximum Static Pressure of 72 psi for safety factor data

Residual Pressure:

61.0 psi

(measured in pounds per square inch)

Distance between hydrants: Approx. 275-ft

Main size: 16-inch main-per Phil Cipolla

Flowing GPM:

3,050

GPM @ 20 PSI: 7,055

Conducted by/Witnessed by/City Forces Contacted:

Conducted by: Jaron Fletcher and Floyd Vaughan – EJ Flow Tests (602.999.7637)

Witnessed by: Phil Cipolla - City of Scottsdale Inspector (602.828.0847)

#### Flow Test Vicinity Map (no scale)





Coco's Restaurant

**Existing Flow** Fire Hydrant

Existing Static/Residual Fire Hydrant



Arizona Canal

North Scottsdale Road

East Camelback Road

E J Flow Test, LLC

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### APPENDIX C FIRE FLOW CALCULATION TABLE

#### SCOTTSDALE BLUESKY FIRE FLOW REQUIREMENTS

|        | D. II. | No.  |         |         |         |         |        |        |        | Area<br>(sf) |        |        |        |        |        |   |                       | Fire                            | Flow                            |                                |
|--------|--------|--|---------|---------|---------|---------|--------|--------|--------|--------------|--------|--------|--------|--------|--------|---|-----------------------|---------------------------------|---------------------------------|--------------------------------|
|        | Build  | aing                                       |         |         |         |         | •      |        | Level  |              |        |        |        | -      |        | Three Largest<br>Consecutive<br>Floors or |                       | FF w/ 50%                       | FF w/ 75%                       |                                |
| ID     | Туре   | Land Uses                                  | 1       | 2       | 3       | 4       | 5      | 6      | 7.     | 8.           | 9      | 10     | 11     | 12     | 13     | Largest<br>Garage Floor                   | Per 2006 IFC<br>(gpm) | Sprinkler<br>Reduction<br>(gpm) | Sprinkler<br>Reduction<br>(gpm) | Required <sup>1</sup><br>(gpm) |
| North  | IA     | Residential, Grocery                       | 34,013  | 0       | 34,013  | 28,757  | 28,757 | 27,610 | 27,610 | 13,844       | 13,844 | 13,844 | 13,844 | 13,844 | 13,488 | 91,527                                    | 3,250                 | 1,625                           | 813                             | 2,500                          |
| Main   | IA     | Residential, Retail,<br>Office, Restaurant | 25,373  | 10,585  | 24,343  | 24,343  | 22,916 | 22,916 | 22,916 | 21,696       | 21,696 | 21,696 | 21,696 | 20,124 | 14,224 | 71,602                                    | 3,000                 | 1,500                           | 750                             | 2,500                          |
| East   | IÁ     | Residential, Hotel                         | 25,388  | 23,785  | 25,576  | 25,576  | 25,576 | 25,576 | 25,576 | 20,390       | 20,390 | 20,390 | 20,390 | 20,390 | 19,259 | 76,728                                    | 3,000                 | 1,500                           | 750                             | 2,500                          |
| Garage | IB     | Garage (Below Ground)                      | 137,166 | 136,166 | 137,080 | 136,770 | •      | ٠.     | -      | •            |        | -      | 1      | •      | ٠      | 137,166                                   | 4,000                 | 2,000                           | 1,000                           | 2,500                          |

Notes

Notes

Per Section 6-1.501 of the City of Scottsdale Design Standards & Policy Manual (January 2010)

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## APPENDIX D WATER DEMAND TABLE

GRYD0000-0001

## SCOTTSDALE BLUESKY WATER DEMANDS

October 10, 2011

| Node | Building        | Phase | Land Use and Description | Area<br>Sq. Ft. | Dwellings<br>Served | Average<br>Daily Demand<br>Per Unit<br>(gpd) | Average<br>Daily<br>Demand<br>(gpm) | Max. Day<br>Factor | Maximum<br>Daily<br>Demand<br>(gpm) | Peak Hour<br>Factor | Peak<br>Hour<br>Demand<br>(gpm) |
|------|-----------------|-------|--------------------------|-----------------|---------------------|--|-------------------------------------|--------------------|-------------------------------------|---------------------|---------------------------------|
| J-9  | Safari Phase II | -     | Residential              |                 | 130                 | 446.3  | 40.2                                | 2.0                | 80.3                                | 3,5                 | 140.6                           |
| J-12 | East            | 2     | 1/3 Hotel                | 59,018          | 76                  | 446.3  | 23.7                                | 2.0                | 47.3                                | 3.5                 | 82.6                            |
| J-12 | East            | 2     | 1/3 Residential          | 40,403          | 40                  | 185.3  | 5.1                                 | 2.0                | 10.3                                | 3.5                 | 18.0                            |
| J-12 | North           | 1     | 1/3 Residential          | 80,489          | 76                  | 185.3  | 9,8                                 | 2.0                | 19,6                                | 3.5                 | 34,2                            |
| J-12 | Main            | 1     | 1/3 Retail               | 8,458           |                     | 0.8  | 4.7                                 | 2.0                | 9.4                                 | 3.5                 | 16.4                            |
| J-12 | Main            | 1     | 1/3 Office               | 3,156           |                     | 0,6  | 1.3                                 | 2.0                | 2.6                                 | . 3.5               | 4.6                             |
| J-12 | Main            | 1     | 1/3 Residential          | 76,370          | 72                  | 185.3  | 9.3                                 | 2.0                | 18.6                                | 3.5                 | 32.6                            |
| J-16 | East            | 2     | 1/3 Hotel                | 59,018          | 76                  | 446.3  | 23.7                                | 2.0                | 47.3                                | 3.5                 | 82.8                            |
|      | East            | 2     | 1/3 Residential          | 40,403          | 40                  | 185.3  | 5.1                                 | 2.0                | 10.3                                | 3.5                 | 18.0                            |
|      | North           | 1 1   | 1/3 Residential          | 80,489          | 76                  | 185.3  | 9,8                                 | 2.0                | 19.6                                | 3.5                 | 34.2                            |
| J-16 | Main            | 1     | 1/3 Retail               | 8,458           |                     | 8.0  | 4.7                                 | 2.0                | 9.4                                 | 3.5                 | 16.4                            |
| J-16 | Main            | 1     | 1/3 Office               | 3,156           |                     | 0,6  | 1.3                                 | 2.0                | 2.6                                 | 3.5                 | 4.6                             |
| J-16 | Main            | 1     | 1/3 Residential          | 76,370          | 72                  | 185.3  | 9.3                                 | 2.0                | 18.6                                | 3.5                 | 32.6                            |
| J-18 | North           | 1     | Grocery                  | 32,000          |                     | 0.7  | 15.6                                | 2.0                | 31.1                                | 3.5                 | 54.4                            |
| J-20 | Main            | 1     | Restaurant               | 10,574          |                     | 0.8  | 5.9                                 | 2.0                | 11.7                                | 3.5                 | 20.6                            |
| J-22 | East            | 2     | 1/3 Hotel                | 59,018          | 76                  | 446.3  | 23.7                                | 2.0                | 47.3                                | 3.5                 | 82.8                            |
| J-22 | East            | 2     | 1/3 Residential          | 40,403          | 40                  | 185.3  | 5.1                                 | 2.0                | 10.3                                | 3,5                 | 18.0                            |
| J-22 | North           | 1     | 1/3 Residential          | 80,489          | 76                  | 185.3  | 9.8                                 | 2.0                | 19.6                                | 3.5                 | 34.2                            |
| J-22 | Main            | 1 1   | 1/3 Retail               | 8,458           |                     | 0.8  | 4.7                                 | 2.0                | 9.4                                 | 3.5                 | 16.4                            |
| J-22 | Main            | 11    | 1/3 Office               | 3,156           |                     | 0.6  | 1.3                                 | 2.0                | 2.6                                 | 3.5                 | 4.6                             |
| J-22 | Main            | 1 1   | 1/3 Residential          | 76,370          | 72                  | 185.3  | 9.3                                 | 2.0                | 18.6                                | 3.5                 | 32.6                            |

| PHASE 1 TOTALS   |   | 97  | 193 | 339 |
|--|---|-----|-----|-----|
| ULTIMATE BUILDOUT (PHASE 1 & PHASE 2 + SAFARI PHASE II) TOTALS | - | 223 | 447 | 782 |

Note: The original Residential dwelling unit (DU) count for the Safari Phase II project was 108 DUs per the Safari Drive Water Design Report prepared by DEA in May of 2006. An additional 22 DUs were added to this count as a factor of safety (a 20% increase) since the exact unit count for this development is currently unknown.

Printed: 9/28/2011

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# APPENDIX E WATER MODELING OUTPUT

PHASE 1

GRYD0000-0001

Water Basis of Design Report Scottsdale BlueSky

# SCOTTSDALE BLUESKY PHASE 1 PEAK HOUR JUNCTION REPORT

October 10, 2011

|       | Hydraulic |            |       |              |  |  |  |
|-------|-----------|------------|-------|--------------|--|--|--|
|       | Elevation | Demand     | Grade | Pressure     |  |  |  |
| Label | (ft)      | (gpm)      | (ft)  | (psi)        |  |  |  |
| J-1   | 1,280     | 0          | 1,446 | 71.8         |  |  |  |
| J-3   | 1,280     | . 0        | 1,446 | 71.8         |  |  |  |
| J-4   | 1,279     | 0          | 1,446 | 72.1         |  |  |  |
| J-5   | 1,279     | 0          | 1,446 | 72.1         |  |  |  |
| J-9   | 1,279     | 0          | 1,446 | 72.1         |  |  |  |
| J-11  | 1,279     | 0          | 1,446 | 72.1         |  |  |  |
| J-12  | 1,281     | 88         | 1,418 | 59. <b>4</b> |  |  |  |
| J-13  | 1,280     | 0          | 1,446 | 71.8         |  |  |  |
| J-14  | 1,281     | 0          | 1,446 | 71.3         |  |  |  |
| J-15  | 1,280     | . 0        | 1,446 | 71.8         |  |  |  |
| J-16  | 1,281     | 88         | 1,418 | 59.4         |  |  |  |
| J-17  | 1,280     | 0          | 1,446 | 71.8         |  |  |  |
| J-18  | 1,281     | · 54       | 1,424 | 62.0         |  |  |  |
| J-19  | 1,280     | 0          | 1,446 | 71.8         |  |  |  |
| J-20  | 1,281     | 21         | 1,431 | 64.9         |  |  |  |
| J-21  | 1,280     | 0          | 1,446 | 71.8         |  |  |  |
| J-22  | 1,281     | 88         | 1,418 | 59.4         |  |  |  |
| J-23  | 1,281     | 0          | 1,446 | 71.3         |  |  |  |
| J-24  | 1,281     | 0          | 1,446 | 71.3         |  |  |  |
| J-25  | 1,279     | 0          | 1,446 | 72.1         |  |  |  |
| J-26  | 1,280     | 0          | 1,446 | 71.8         |  |  |  |
| J-27  | 1,279     | 0          | 1,446 | <b>72</b> .2 |  |  |  |
| J-28  | 1,279     | 0          | 1,446 | 72.1         |  |  |  |
| J-29  | 1,281     | ´ 0        | 1,446 | 71.3         |  |  |  |
| J-30  | 1,280     | 0          | 1,439 | 68.8         |  |  |  |
| J-32  | 1,281     | · <b>0</b> | 1,444 | 70.4         |  |  |  |
| J-33  | 1,280     | 0          | 1,446 | 71.7         |  |  |  |

Printed: 10/5/2011

# PHASE 1 PEAK HOUR PIPE REPORT

Printed: 10/5/2011

| Label             | Length<br>(ft) | Start<br>Node  | Stop<br>Node | Diameter<br>(in) | Hazen-<br>Williams C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------------------|----------------|----------------|--------------|------------------|----------------------|---------------|--------------------|---------------------------------|
| P-1               | 1              | R-1            | PMP-1        | 54               | 130                  | 339           | 0.1                | 0.000                           |
| P-2               | 1              | PMP-1          | <b>J</b> -1  | 54               | 130                  | 339           | 0.1                | 0.000                           |
| P-10              | 29             | J-5            | J-9          | . 8              | 130                  | 0             | 0.0                | 0.000                           |
| P-15              | 22             | J-11           | J-4          | 8                | 130                  | 0             | 0.0                | 0.000                           |
| P-18              | 28             | J-13           | J-3          | 16               | 130                  | 251           | 0.4                | 0.000                           |
| P-21              | 9              | J-15           | J-13         | 16               | 130                  | 251           | 0.4                | 0.000                           |
| P-24              | 59             | J-17           | J-15         | 16               | 130                  | 251           | 0.4                | 0.000                           |
| P-27              | 85             | J-19           | J-17         | ·16              | 130                  | 251           | 0.4                | 0.000                           |
| P-29              | 17             | J-1            | J-21         | 16               | 130                  | 339           | 0.5                | 0.000                           |
| P-30              | . 180          | J-21           | J-19         | 16               | 130                  | 251           | 0.4                | 0.000                           |
| P-32              | 51             | J-21           | GPV-1        | 4 .              | 130                  | - 88          | 2.2                | 0.006                           |
| P-33              | 20             | GPV-1          | J-22         | 4                | 130                  | 88            | 2.2                | 0.006                           |
| P-35              | 10             | GPV-2          | J-20         | 2                | 130                  | 21            | 2.1                | 0.012                           |
| P-37              | 9              | GPV-3          | J-18         | 2                | 130                  | 54            | 5.6                | 0.071                           |
| P-39              | 15             | GPV-4          | J-16         | 4                | 130                  | · 88          | 2.2                | 0.006                           |
| P-41              | . 11           | GPV-5          | J-14         | 8                | 130                  | 0             | 0.0                | 0.000                           |
| P-42              | 22             | J-1.1          | GPV-6        | 4                | 130                  | 88            | 2.2                | 0.006                           |
| P-43              | 7              | GPV-6          | J-12         | 4                | 130                  | 88            | 2.2                | 0.006                           |
| P <del>-4</del> 5 | 213            | J-23           | J-11         | 8                | 130                  | 88            | 0.6                | 0.000                           |
| P-47              | 8              | J-24           | J-23         | . 8              | 130                  | 88            | 0.6                | 0.000                           |
| P-48              | 16             | GPV-5          | J-23         | 8                | 130                  | 0             | 0.0                | 0.000                           |
| P-49              | 21             | GPV-4          | J-24         | 4                | 130                  | -88           | 2.2                | 0.006                           |
| P-50              | 23             | J-4            | J-25         | . 8              | 130                  | 0 .           | 0.0                | 0.000                           |
| P-51              | 42             | J-25           | J-5          | 8                | 130                  | 0             | 0.0                | 0.000                           |
| P-52              | 30             | J-1            | J-26         | 16               | 130                  | 0             | 0.0                | 0.000                           |
| P-53              | 178            | . J- <b>26</b> | J-27         | 6                | 130                  | 0             | 0.0                | 0.000                           |
| P-54              | 17             | J-25           | J-28         | 6                | 130                  | 0             | 0.0                | 0.000                           |
| P-56              | . 1 <b>2</b>   | J-29           | J-24         | 8.               | 130                  | 176           | 1.1                | 0.001                           |
| P-58              | 7              | J-30           | GPV-3        | .2               | 130                  | 54            | 5.6                | 0.071                           |
| P-59              | 95             | J-29           | J-30         | <b>^2</b>        | 130                  | 54            | 5.6                | 0.071                           |
| P-61.             | 21             | J-32           | GPV-2        | . 2              | 130                  | 21            | 2.1                | 0.012                           |
| P-63              | 35             | J-3            | J-33         | 8                | 130                  | 251           | 1.6                | 0.001                           |
| P-64              | 15             | J-33           | J-29         | 8                | 130                  | 230           | 1.5                | 0.001                           |
| P-65              | 181            | J-32           | J-33         | 2                | 130                  | -21           | 2.1                | 0.012                           |

GRYD0000-0001

# SCOTTSDALE BLUESKY PHASE 1 PEAK HOUR PUMP REPORT

Printed: 10/5/2011

| Label | Elevation<br>(ft) | Pump<br>Definition | Status<br>(Initial) | Hydraulic<br>Grade<br>(Suction)<br>(ft) | Hydraulic<br>Grade<br>(Discharge)<br>(ft) | Pump<br>Head<br>(ft) | Flow<br>(Total)<br>(gpm) |
|-------|-------------------|--------------------|---------------------|---|---|----------------------|--------------------------|
| PMP-1 | 1280.0            | 8/15/2011          | On                  | 1 280 0                                 | 1 445 9                                   | 165.9                | 339                      |

GRYD0000-0001

# SCOTTSDALE BLUESKY PHASE 1 PEAK HOUR RESERVOIR REPORT

Printed: 10/5/2011

|       |           | Hydraulic | Flow      |  |
|-------|-----------|-----------|-----------|--|
|       | Elevation | Grade     | (Out net) |  |
| Label | (ft)      | (ft)      | (gpm)     |  |
| R-1   | 1280.0    | 1 280 0   | 339       |  |

# SCOTTSDALE BLUESKY PHASE 1 PEAK HOUR VALVE REPORT

Printed: 10/5/2011

| Label | Elevation (ft) | Diameter<br>(in) | General<br>Purpose<br>Valve<br>Headloss<br>Curve | Flow<br>(gpm) | Hydraulic<br>Grade<br>(From)<br>(ft) | Hydraulic<br>Grade<br>(To)<br>(ft) | Headloss<br>(ft) |
|-------|----------------|------------------|--|---------------|--------------------------------------|------------------------------------|------------------|
| GPV-1 | 1,281          | 4                | 4" - Febco 880V                                  | 88            | 1445.6                               | 1418.4                             | 27.2             |
| GPV-2 | 1,281          | 2                | 2" - Febco 850U                                  | 21            | 1443.4                               | 1431.1                             | 12.3             |
| GPV-3 | 1,281          | 2                | 2" - Febco 850U                                  | 54            | 1438.5                               | . 1424.9                           | 13.6             |
| GPV-4 | 1,281          | 4                | 4" - Febco 880V                                  | 88            | 1445.7                               | 1418.5                             | 27.2             |
| GPV-5 | 1,281          | 8                | 8" - Febco 880V                                  | 0             | 1445.8                               | 1445.8                             | 0.0              |
| GPV-6 | 1,281          | 4                | 4" - Febco 880V                                  | 88            | 1445.6                               | 1418.4                             | 27.2             |

#### SCOTTSDALE BLUESKY PHASE 1 MAX DAY + FF FIRE FLOW REPORT

October 10, 2011

|                  | Satisfies<br>Fire<br>Flow | Fire Flow<br>(Needed) | Fire Flow<br>(Available) | Flow<br>(Total Needed) | Flow<br>(Total Available) | Pressure<br>. (Residual Lower ,<br>Limit) | Pressure (Calculated<br>Residual) | Pressure<br>(System Lower<br>Limit) | Pressure (Calculated<br>System Lower Limit) | Junction w/<br>Minimum<br>• Pressure |
|------------------|---------------------------|-----------------------|--------------------------|------------------------|---------------------------|---|-----------------------------------|-------------------------------------|---|--------------------------------------|
| Label            | Constraints?              | (gpm)                 | (gpm)                    | (gpm)                  | (gpm)                     | (psi)                                     | (psi)                             | (psi)                               | (psl)                                       | (System)                             |
| J-1              | TRUE                      | 2,500                 | 5,000                    | 2,500                  | 5,000                     | 30.0                                      | 42.5                              | 30.0                                | 32.3  | J-22                                 |
| j-3              | TRUE                      | 2,500                 | 5,000                    | 2,500                  | 5,000                     | 30.0                                      | 40.4                              | 30.0                                | 30.2  | J-12                                 |
| J-4              | TRUE                      | 2,500                 | 3,063                    | 2,500                  | 3,063                     | 30.0                                      | 39.2                              | 30.0                                | 30.0  | J-12                                 |
| J-5              | TRUE                      | 2,500                 | 3,063                    | 2,500                  | 3,063                     | 30.0                                      | 35.1                              | 30.0                                | 30.0  | J-12                                 |
| J-9 ·            | TRUE                      | 2,500                 | 3,063                    | 2,500                  | 3,063                     | 30.0                                      | 33.3                              | 30.0                                | 30.0  | J-12                                 |
| J-11             | TRUE                      | 2,500                 | 3,063                    | 2,500                  | 3,063                     | 30.0                                      | 40.6                              | 30.0                                | 30.0  | J-12                                 |
| J-12             | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                      | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                              |
| J-13             | TRUE                      | 2,500                 | 5,000                    | 2,500                  | 5,000                     | 30.0                                      | 40.5                              | 30.0                                | 30.4  | J-12                                 |
| J-14             | TRUE                      | 2,500                 | 3,569                    | 2,500                  | 3,569                     | 30.0                                      | 30.0                              | 30.0                                | 38.2  | J-12                                 |
| J-15             | TRUE                      | 2,500                 | 5,000                    | 2.500                  | 5,000                     | 30.0                                      | 40.6                              | 30.0                                | 30.4  | J-12                                 |
| J-16             | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30,0                                      | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                              |
| J-17             | TRUE                      | 2,500                 | 5,000                    | 2,500                  | 5,000                     | 30.0                                      | 40.9                              | 30.0                                | 30.7  | J-12                                 |
| J-18             | (N/A)                     | 2,500                 | . (N/A)                  | (N/A)                  | (N/A)                     | 30.0                                      | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                              |
| J-19             | TRUE                      | 2,500                 | 5,000                    | 2,500                  | 5,000                     | 30.0                                      | 41.4                              | 30.0                                | 31,2  | J-12                                 |
| J-20             | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | . (N/A)                   | 30.0                                      | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                              |
| J-21             | TRUE                      | 2,500                 | 5,000                    | 2,500                  | 5,000                     | 30.0                                      | 42.4                              | 30.0                                | 32.2  | J-22                                 |
| J-22             | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                      | (N/A)                             | 30.0                                | (N/A)*                                      | ((N/A))                              |
| J-23             | TRUE                      | 2,500                 | 4,223                    | 2,500                  | 4,223                     | 30.0                                      | 39.7                              | 30.0                                | 30.0  | `J-12                                |
| J-24             | TRUE                      | 2,500                 | 4,297                    | 2,500                  | 4,297                     | 30.0                                      | 39.7                              | 30.0                                | 30,0  | J-12                                 |
| J-25             | TRUE                      | 2,500                 | 3,063                    | 2,500                  | 3,063                     | 30.0                                      | 37.8                              | 30.0                                | 30,0  | J-12                                 |
| J-26             | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                      | (N/A) ·                           | 30.0                                | · (N/A)                                     | ((N/A))                              |
| J-27             | TRUE                      | 2,500                 | 2,585                    | 2,500                  | 2,585                     | 30.0                                      | 30.0                              | 30,0                                | 52,5  | J-22                                 |
| J-28             | TRUE                      | 2,500                 | 3,063                    | 2,500                  | 3,063                     | 30.0                                      | 33.5                              | 30.0                                | 30.0  | J-12                                 |
| J-2 <del>9</del> | TRUE                      | 2,500                 | 4,416                    | 2,500                  | 4,416                     | 30.0                                      | 39.7                              | 30.0                                | 30.0  | J-12                                 |
| J-30             | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30,0                                      | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                              |
| J-32             | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                      | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                              |
| J-33             | TRUE                      | 2,500                 | 4,571                    | 2,500                  | 4,571                     | 30.0                                      | 40.2                              | 30.0                                | 30.0  | J-12                                 |

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| UL | TIMATE BU | ILDOUT (PHASE 1 & | : PHASE 2 + S | AFARI PHAS | E II) |    |
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# SCOTTSDALE BLUESKY ULTIMATE BUILDOUT (PHASES 1 AND 2 + SAFARI PHASE II) PEAK HOUR JUNCTION REPORT

October 10, 2011

|       |           |              | Hydraulic      |          |
|-------|-----------|--------------|----------------|----------|
|       | Elevation | Demand       | Grade          | Pressure |
| Label | (ft)      | (gpm)        | (ft)           | (psi)    |
| J-1   | 1,280     | 0            | 1,444          | 71.1     |
| J-3   | 1,280     | 0            | 1,444          | 71.0     |
| J-4   | 1,279     | 0            | 1,443          | 71.1     |
| J-5   | 1,279     | 0            | 1,443          | 71.1     |
| J-9   | 1,279     | 141          | 1,443          | 71.0     |
| J-11  | 1,279     | 0            | 1,443          | 71.1     |
| J-12  | 1,281     | 189          | 1,417          | 58.7     |
| J-13  | 1,280     | 0            | 1,444          | 71.0     |
| J-14  | 1,281     | 0            | 1,444          | 70.4     |
| J-15  | 1,280     | 0            | 1,444          | 71.0     |
| J-16  | 1,281     | 189          | 1,417          | 58.8     |
| J-17  | 1,280     | 0            | 1,444          | 71.0     |
| J-18  | 1,281     | 54           | 1,422          | 61.1     |
| J-19  | 1,280     | 0            | 1,444          | 71.1     |
| J-20  | 1,281     | 21           | 1,429          | 64.1     |
| J-21  | 1,280     | 0            | 1,444          | 71.1     |
| J-22  | 1,281     | 189          | 1,417          | 58.6     |
| J-23  | 1,281     | 0            | 1,444          | 70.4     |
| J-24  | 1,281     | 0 .          | 1,444          | 70.4     |
| J-25  | 1,279     | 0            | 1,443          | 71.1     |
| J-26  | 1,280     | 0            | 1, <b>44</b> 4 | 71.1     |
| J-27  | 1,279     | 0 .          | 1,444          | 71.5     |
| J-28  | 1,279     | <b>o</b> '   | 1,443          | 71.1     |
| J-29  | 1,281     | 0            | 1,444          | 70.5     |
| J-30  | 1,280·    | 0            | 1,437          | 67.9     |
| J-32  | 1,281     | 0            | 1,442          | 69.6     |
| J-33  | 1,280     | , <b>0</b> - | 1,444          | 70.9     |

Printed: 10/5/2011

# SCOTTSDALE BLUESKY ULTIMATE BUILDOUT (PHASES 1 AND 2 + SAFARI PHASE II) PEAK HOUR PIPE REPORT

October 10, 2011

|   | Label  | Length<br>(ft) | Start<br>Node | Stop<br>Node | Diameter<br>(in) | Hazen-<br>Williams C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|---|--------|----------------|---------------|--------------|------------------|----------------------|---------------|--------------------|---------------------------------|
| _ | P-1    | <u> </u>       | R-1           | PMP-1        | 54               | 130                  | 782           | 0.1                | 0.000                           |
|   | P-2    | 1              | PMP-1         | J-1          | 54               | 130                  | 782           | 0.1                | 0.000                           |
|   | P-10   | 29             | J-5           | J-9          | 8                | 130                  | 141           | 0.9                | 0.000                           |
|   | P-15   | 22             | J-11          | J-4          | . 8              | 130                  | 141           | 0.9                | 0.000                           |
|   | P-18   | 28             | J-13          | J-3          | .16              | 130                  | 593           | 1.0                | 0.000                           |
|   | P-21   | 9              | . J-15        | J-13         | 16               | 130                  | 593           | 1.0                | 0.000                           |
|   | P-24   | 59             | J-17          | J-15         | 16               | 130                  | 593           | 1.0                | 0.000                           |
|   | P-27   | 85             | J-19          | J-17         | 16               | 130                  | 593           | 1.0                | 0.000                           |
|   | P-29   | 17             | J-1           | J-21         | 16               | 130                  | 782           | 1.3                | 0.000                           |
|   | P-30   | 180            | J-21          | J-19         | · 16             | 130                  | 593           | 1.0                | 0.000                           |
|   | P-32   | 51             | J-21          | GPV-1        | 4                | 130                  | 189           | 4.8                | 0.024                           |
|   | P-33   | 20             | GPV-1         | J-22         | 4                | 130                  | 189           | 4.8                | 0.024                           |
|   | P-35   | 10             | GPV-2         | J-20         | 2                | 130                  | 21            | 2.1                | 0.012                           |
|   | P-37   | ` 9            | GPV-3         | J-18         | 2                | 130                  | 54            | 5.6                | 0.071                           |
| • | P-39   | 15             | GPV-4         | J-16         | 4                | 130                  | 189           | 4.8                | 0.024                           |
|   | P-41   | 11             | GPV-5         | J-14         | 8                | 130                  | 0             | 0.0                | 0.000                           |
|   | P-42   | 22             | J-11          | GPV-6        | 4                | 130                  | 189           | 4.8                | 0.024                           |
|   | P-43   | 7              | GPV-6         | J-12         | 4                | 130                  | 189           | 4.8                | 0.024                           |
|   | P-45   | 213            | J-23          | J-11         | 8                | 130                  | 329           | 2.1                | 0.002                           |
|   | P-47   | 8              | J-24          | J-23         | 8                | 130                  | 329           | 2.1                | 0.002                           |
|   | P-48   | 16             | GPV-5         | J-23         | 8                | 130                  | 0             | 0.0                | 0 000                           |
|   | P-49   | 21             | GPV-4         | J-24         | 4                | 130                  | -189          | 4.8                | 0.024                           |
|   | P-50   | 23             | J-4           | J-25         | 8                | 130                  | 141           | 0.9                | 0.000                           |
|   | P-51   | 42             | J-25          | J-5          | 8                | 130                  | 141           | 0.9                | 0.000                           |
|   | P-52   | 30             | J-1           | J-26         | 16               | 130                  | 0             | 0.0                | 0.000                           |
|   | P-53   | 178            | · J-26        | J-27         | 6                | 130                  | 0             | 0.0                | 0.000                           |
|   | P-54   | 17             | J-25          | J-28         | 6                | 130                  | 0             | 0.0                | 0.000                           |
|   | P-56   | 12             | J-29          | J-24         | 8                | 130                  | 518           | 3.3                | 0.005                           |
|   | P-58   | 7 .            | J-30          | GPV-3        | 2                | 130                  | 54            | 5.6                | 0.071                           |
|   | . P-59 | 95             | J-29          | J-30         | 2                | 130                  | 54            | 5.6                | 0.071                           |
|   | P-61   | <b>2</b> 1     | J-32          | GPV-2        | 2                | 130                  | 21            | 2.1                | 0.012                           |
|   | P-63   | 35             | J-3           | J-33         | 8                | 130                  | 593           | 3.8                | 0.007                           |
|   | P-64   | 15             | J-33          | J-29         | . 8              | 130                  | 572           | 3.7                | 0.007                           |
|   | P-65   | 181            | J-32          | J-33         | . 2              | 130                  | -21           | 2.1                | 0.012                           |

Printed: 10/5/2011

GRYD0000-0001

## SCOTTSDALE BLUESKY ULTIMATE BUILDOUT (PHASES 1 AND 2 + SAFARI PHASE II) PEAK HOUR PUMP REPORT

Printed: 10/5/2011

|       |           |            |           | Hydraulic<br>Grade | Hydraulic<br>Grade | Pump  | Flow    |
|-------|-----------|------------|-----------|--------------------|--------------------|-------|---------|
|       | Elevation | Pump       | Status    | (Suction)          | (Discharge)        | Head  | (Total) |
| Label | (ft)      | Definition | (Initial) | (ft)               | (ft)               | (ft)  | (gpm)   |
| PMP-1 | 1280.0    | 8/15/2011  | On        | 1.280.0            | 1.444.3            | 164.3 | 782     |

GRYD0000-0001

## SCOTTSDALE BLUESKY ULTIMATE BUILDOUT (PHASES 1 AND 2 + SAFARI PHASE II) PEAK HOUR RESERVOIR REPORT

Printed: 10/5/2011

|   |       | Elevation | Hydraulic<br>Grade | Flow<br>(Out net) |
|---|-------|-----------|--------------------|-------------------|
|   | Label | (ft)      | (ft)               | (gpm)             |
| _ | R-1   | 1280 D    | 1280.0             | 782               |

GRYD0000-0001

#### SCOTTSDALE BLUESKY **ULTIMATE BUILDOUT (PHASES 1 AND 2 + SAFARI PHASE II) PEAK HOUR VALVE REPORT**

Printed: 10/5/2011

| Label | Elevation<br>(ft) | Diameter | General<br>Purpose<br>Valve<br>Headloss<br>Curve | Flow<br>(gpm) | Hydraulic<br>Grade<br>(From)<br>(ft) | Hydraulic<br>Grade<br>(To)<br>(ft) | Headloss<br>(ft) |
|-------|-------------------|----------|--|---------------|--------------------------------------|------------------------------------|------------------|
| GPV-1 | 1,281             | 4        | 4" - Febco 880V                                  | 189           | 1443.0                               | 1417.0                             | 26.0             |
| GPV-2 | 1,281             | · 2      | 2" - Febco 850U                                  | 21            | 1441.6                               | 1429.3                             | 12.3             |
| GPV-3 | 1,281             | 2        | 2" - Febco 850U                                  | 54            | 1436.5                               | 1422.9                             | 13.6             |
| GPV-4 | 1,281             | 4        | 4" - Febco 880V                                  | 189           | 1443.3                               | 1417.3                             | 26.0             |
| GPV-5 | 1,281             | 8        | 8" - Febco 880V                                  | 0             | 1443.8                               | 1443.7                             | 0.0              |
| GPV-6 | 1.281             | 4        | 4" - Febco 880V                                  | 189           | 1442.7                               | 1416.7                             | 26.0             |

### SCOTTSDALE BLUESKY ULTIMATE BUILDOUT (PHASES 1 AND 2 + SAFARI PHASE II) MAX DAY + FF FIRE FLOW REPORT

|       | Satisfies<br>Fire<br>Flow | Fire Flow<br>(Needed) | Fire Flow<br>(Available) | Flow<br>(Total Needed) | Flow<br>(Totał Avallable) | Pressure<br>(Residual Lower<br>Limit) | Pressure (Calculated<br>Residual) | Pressure<br>(System Lower<br>Limit) | Pressure (Calculated<br>System Lower Limit) | Junction w/<br>Minimum<br>Pressure |
|-------|---------------------------|-----------------------|--------------------------|------------------------|---------------------------|---------------------------------------|-----------------------------------|-------------------------------------|---|------------------------------------|
| Label | Constraints?              | (gpm)                 | (gpm)                    | (gpm)                  | (gpm)                     | (psi)                                 | (psi)                             | (psi)                               | (psi)                                       | (System)                           |
| J-1   | TRUE                      | 2,500                 | 4,643                    | 2,500                  | 4,643                     | 30.0                                  | 43.6                              | 30.0                                | 30,0  | J-22                               |
| J-3   | TRUE                      | 2,500                 | 4,462                    | 2,500                  | 4,462                     | 30.0                                  | 43.6                              | 30.0                                | 30.0  | J-12                               |
| J-4   | TRUE                      | 2,500                 | 2,692                    | 2,500                  | 2,692                     | 30.0                                  | 42.7                              | 30.0                                | 30.0  | J-12                               |
| J-5 、 | TRUE                      | 2,500                 | 2,692                    | 2,500                  | 2,692                     | 30.0                                  | 39.3                              | 30.0                                | 30.0  | J-12                               |
| J-9   | TRUE `                    | 2,500                 | 2,692                    | 2,580                  | 2,772                     | 30.0                                  | 37.8                              | 30.0                                | 30.0  | J-12                               |
| J-11  | TRUE                      | 2,500                 | 2,692                    | 2,500                  | 2,692                     | 30.0                                  | 43.B                              | 30.0                                | 30.0  | J-12                               |
| J-12  | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.D                                  | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                            |
| J-13  | TRUE                      | 2,500                 | 4,474                    | 2,500                  | 4,474                     | 30.0                                  | 43.6                              | 30.0                                | 30.0  | J-12                               |
| J-14  | TRUE                      | 2;500                 | 3,396                    | 2,500                  | 3,396                     | 30,0                                  | 30.0                              | 30.0                                | 34.2  | J-12                               |
| J-15  | TRUE                      | 2,500                 | 4,479                    | 2,500                  | 4,479                     | 30.0                                  | 43.6                              | 30.0                                | 30.0  | J-12                               |
| J-16  | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                  | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                            |
| J-17  | TRUE                      | 2,500                 | 4,506                    | 2,500                  | 4,506                     | 30.0                                  | 43.6                              | 30.0                                | 30.0  | J-12                               |
| J-18  | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                  | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                            |
| J-19  | ŤRUĖ                      | 2,500                 | 4,546                    | 2,500                  | 4,546                     | 30.0                                  | 43.6                              | 30,0                                | 30.0  | J-12                               |
| J-20  | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                  | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                            |
| J-21  | TRUE                      | 2,500                 | 4,635                    | 2,500                  | 4,635                     | 30.0                                  | 43.6                              | 30.0                                | 30.0  | J-22                               |
| J-22  | (N/A) ·                   | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                  | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                            |
| J-23  | TRUE                      | 2,500                 | 3,736                    | 2,500                  | 3,736                     | 30.0                                  | 43.1                              | 30.0                                | 30.0  | J-12                               |
| J-24  | TRUE                      | 2,500                 | 3,802                    | 2,500                  | 3,802                     | 30.0                                  | 43.1                              | 30.0                                | 30.0  | J-12                               |
| J-25  | TRUE                      | 2,500                 | 2,692                    | 2,500                  | 2.692                     | 30.0                                  | 41.5                              | 30.0                                | 30.0  | J-12                               |
| J-26  | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                  | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                            |
| J-27  | TRUE                      | 2,500                 | 2,532                    | 2,500                  | 2,532                     | 30.0                                  | 30.0                              | 30.0                                | 47.9  | J-22                               |
| J-26  | TRUE                      | 2,500                 | 2,692                    | 2,500                  | 2,692                     | 30.0                                  | 38.2                              | 30.0                                | 30.0  | J-12                               |
| J-29  | TRUE                      | 2,500                 | 3,911                    | 2,500                  | 3,911                     | 30.0                                  | 43.1                              | 30.0                                | 30.0  | J-12                               |
| J-30  | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                  | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                            |
| J-32  | (N/A)                     | 2,500                 | (N/A)                    | (N/A)                  | (N/A)                     | 30.0                                  | (N/A)                             | 30.0                                | (N/A)                                       | ((N/A))                            |
| J-33  | TRUE                      | 2,500                 | 4,053                    | 2,500                  | 4,053                     | 30.0                                  | 43.5                              | 30.0                                | 30.0  | J-12                               |

# WASTEWATER BASIS OF DESIGN REPORT FOR BLUE SKY SCOTTSDALE

#### PREPARED FOR

### GRAY DEVELOPMENT, LLC 4040 E CAMELBACK ROAD, SUITE 275 PHOENIX, AZ 85018

(602) 508-7141 CONTACT: BRIAN KEARNEY

#### PREPARED BY

ZACKARY POPE, P.E. DAVID EVANS & ASSOCIATES, INC. 4600 E WASHINGTON STREET, SUITE 430 PHOENIX, AZ 85034 (602) 678-5151

> 1<sup>ST</sup> SUBMITTAL OCTOBER 2011

DEA PROJECT NO. GRYD0000-0001



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**Wastewater Collection** 

**Existing Utilities and Surface Improvements** 

#### **APPENDICES**

В

С

<u>TITLE</u> City of Scottsdale Wastewater Quarter **Section Map** 

**Wastewater Generation Calculations** FlowMaster Modeling Calculations



#### A. INTRODUCTION

This basis of design report was completed under a contract with the Gray Development, LLC. The proposed Blue Sky Scottsdale project consists of three buildings containing retail, residential, office, restaurant, hotel, and grocery components. An underground parking structure will also be provided. The buildings will be constructed in two phases. The parking structure, the North Building, and the Main Building will be constructed as part of Phase 1. The East Building will be constructed as part of Phase 2. However, all of the wastewater improvements will be constructed during Phase 1.

#### 1. Project Location

The proposed Blue Sky Scottsdale project is located near the northeast corner of the intersection of Scottsdale Road & Camelback Road within the city of Scottsdale, Arizona. The site is located within the northwest quarter of Section 23 of Township 2 North, Range 4 East of the Gila and Salt River Base and Meridian. The site is approximately 4.28 acres and irregularly shaped. It is generally bound by Scottsdale Road to the west, the Fashion Square road entrance alignment to the south, 72<sup>nd</sup> Way to the east, and Coolidge Street to the north. The area's street system in relationship to the location of the site is illustrated in Exhibit 1, the project's vicinity map.

#### 2. Site Zoning

The zoning of the Blue Sky Scottsdale site is discussed in Section C.1 of this report.

#### 3. General Plan

The Blue Sky project will provide strong support for the goals and policies of the City's General Plan. It will be consistent with the Downtown Plan and reflect its vision, goals, and policies. It will support the City's efforts to "boldly look to its metropolitan future" through the development of an urban oasis that brings to life the City's vision for:

- Mixed-use urban neighborhoods
- World class planning, architecture, and design
- Sustainability
- · Connectivity and walkability
- Economic vitality, and
- Worldwide recognition as the premier destination in the United States

#### **B. DESIGN DOCUMENTATION**

#### 1. Design Procedures

The analysis of the proposed wastewater collection system was done in compliance with the City of Scottsdale Design Standards & Policies Manual. The proposed wastewater collection system will serve the project in accordance with City of Scottsdale design standards and the ADEQ Engineering Bulletin 10.

The estimated Average Day Sewer Design Flows of the Blue Sky Scottsdale project were determined based on the following values.

- Residential Units = 140 gallons per DU per day (PF = 4.5)
- Hotel = 380 gallons per room per day (PF = 4.5)
- Retail = 0.5 gallons per square foot per day (PF = 3)
- Restaurant = 1.2 gallons per square foot per day (PF = 6)
- Offices = 0.3 gallons per square foot per day (PF = 3)
- Grocery = 0.19 gallons per square foot per day (PF = 4)

Note that the Grocery Land Use is not specifically listed in Figure 7.1-2 of the Design Standards and Policy Manual. However, the estimated wastewater generation of 0.19 gallons per square foot per day was utilized for the design of the Scottsdale Quarter project located near the intersection of Scottsdale Road & Greenway Hayden Loop. A peaking factor of 4.0 is utilized as a conservative measure.

#### 2. Software

Wastewater generation was determined using a Microsoft Excel spreadsheet. DEA prepared FlowMaster<sup>TM</sup> calculations for the proposed wastewater collection system. FlowMaster is a pipe modeling software created by Bentley and Haestad Methods.

#### C. EXISTING CONDITIONS

#### 1. Zoning and Land Use

The site falls under the Downtown Regional Multiple Use Type 2 Land Use designation. The site is currently zoned Downtown Regional Commercial Office, Type 2, Planned Block Development Downtown Overlay (D/RCO-2 PBD DO) with amended development standards.

#### 2. Existing Topography, Vegetation, and Landform Features

Generally, the existing topography slopes in a southeasterly direction at approximately 0.40%, with approximately 3 feet of fall across the property. The site in its existing condition is generally an unimproved dirt lot. An entrance road bisects the site that provides access to the existing

Safari Drive condominiums located to the east of the site. The entrance road also provides access to a commercial development located to the south of the site.

#### 3. Existing Utilities

There is existing wastewater infrastructure located within the adjacent streets as illustrated on the City of Scottsdale Quarter Section map provided in Appendix A. This infrastructure includes an existing 8-inch line within Coolidge Street, an existing 15-inch line and an existing 10-inch line in Scottsdale Road, an existing 15-inch line that runs to the southeast from Scottsdale Road to just south of the project, and an existing private line within 72<sup>nd</sup> Way and bordering the southeast portion of the site.

The existing public line within 72<sup>nd</sup> Way currently conveys flow from Safari Phase I to the existing line in Coolidge Street.

Based on correspondence with the City of Scottsdale, there is adequate capacity offsite to convey the wastewater generated by the proposed improvements.

#### 4. Existing Master Plans or Design Reports

A Wastewater Basis of Design Report for Safari Drive was prepared by DEA in 2006 for the Safari Drive condominiums. Phase 1 of Safari Drive has been constructed.

#### D. PROPOSED CONDITIONS

#### 1. Site Plan

Exhibit 2 illustrates the proposed site improvements.

#### 2. Proposed Connections

All of the proposed sewer lines will be private. Exhibit 2 illustrates the proposed connections to the existing system. The North and Main buildings will be served by a single line that conveys their flow to the existing 15-inch line in Scottsdale Road.

A portion of the existing public line in 72<sup>nd</sup> Way will be removed in order to construct the underground parking structure. A public abandonment will be required in order to remove this sewer. The flow from the existing 26 DUs in Safari Phase I that currently utilize this sewer will be rerouted to the south through the Blue Sky parking garage where it will ultimately tie into the existing manhole along the southern border of the Blue Sky property. A common property owner's association will be created in order to maintain the private sewer.

The East building will be served by the line that is to be re-routed through the garage.

#### 3. Maintenance Responsibilities

The maintenance responsibilities of the Blue Sky Scottsdale development are that of any typical commercial development in the area. No onsite wastewater pumping stations are required for the project. A common property owner's association will be created in order to maintain the private sewer that runs through the Blue Sky parking garage.

#### E. COMPUTATIONS

#### 1. Computer Calculations

The Blue Sky development's proposed wastewater collection system was analyzed for the Phase 1 and Ultimate Buildout scenarios. Phase 1 includes the rerouting of the sewer of the existing Safari Phase 1 development. Exhibit 2 illustrates the onsite wastewater collection system improvements required to serve the development. Note that all of the wastewater improvements will be constructed during Phase 1.

Table E.1.1 summarizes the wastewater flows for Blue Sky. It also summarizes the existing flow from Safari Phase 1 (26 DUs) that will be rerouted through the Blue Sky development. Detailed sanitary sewer calculations that break down the values listed below and the FlowMaster output for this report are provided in Appendices B and C, respectively. The peak flows are based on peaking factors as set forth in the City of Scottsdale Design Standards & Policies Manual.

TABLE E.1.1 – WASTEWATER GENERATION SUMMARY

| 171000 0.1.1                       | JIE WILL GEIVE | ICTION SOMMINE  |
|------------------------------------|----------------|-----------------|
| Phase                              | ADWF<br>(gpd)  | Peak Flow (gpd) |
| Portion of Existing Safari Phase I | 3,640          | 16,380          |
| Blue Sky Phase 1                   | 96,596         | 427,328         |
| Blue Sky Ultimate Buildout         | 200,416        | 894,574         |

Appendix C contains the FlowMaster output for both Phase 1 and Ultimate Buildout.

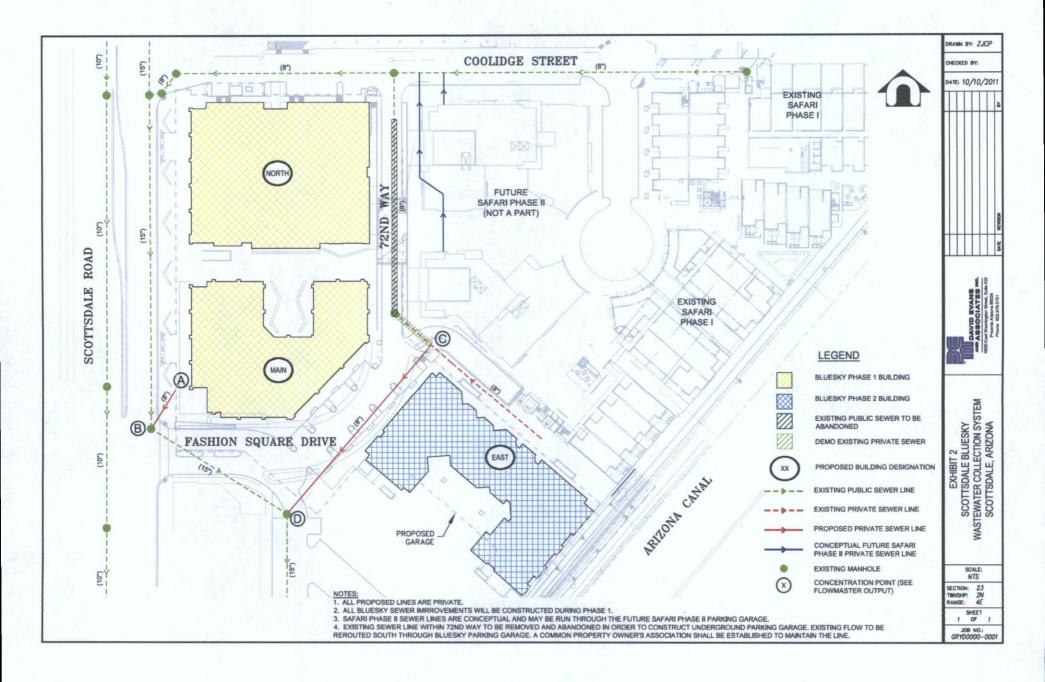
The downstream impacts to the existing wastewater system due to the proposed improvements were not analyzed.

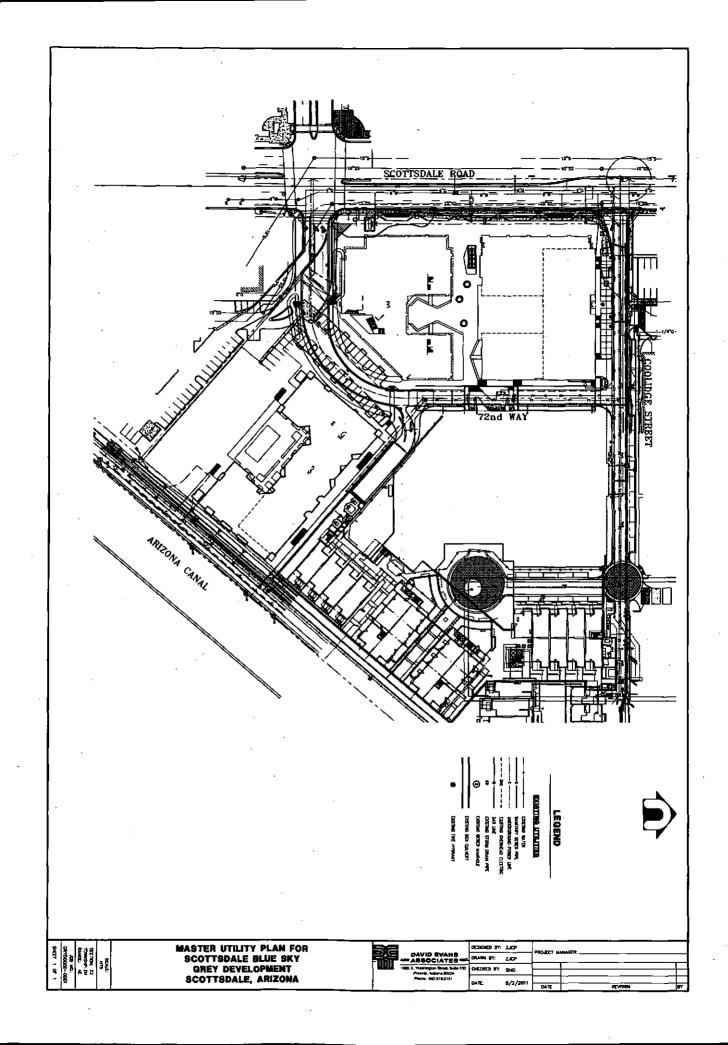
#### F. SUMMARY

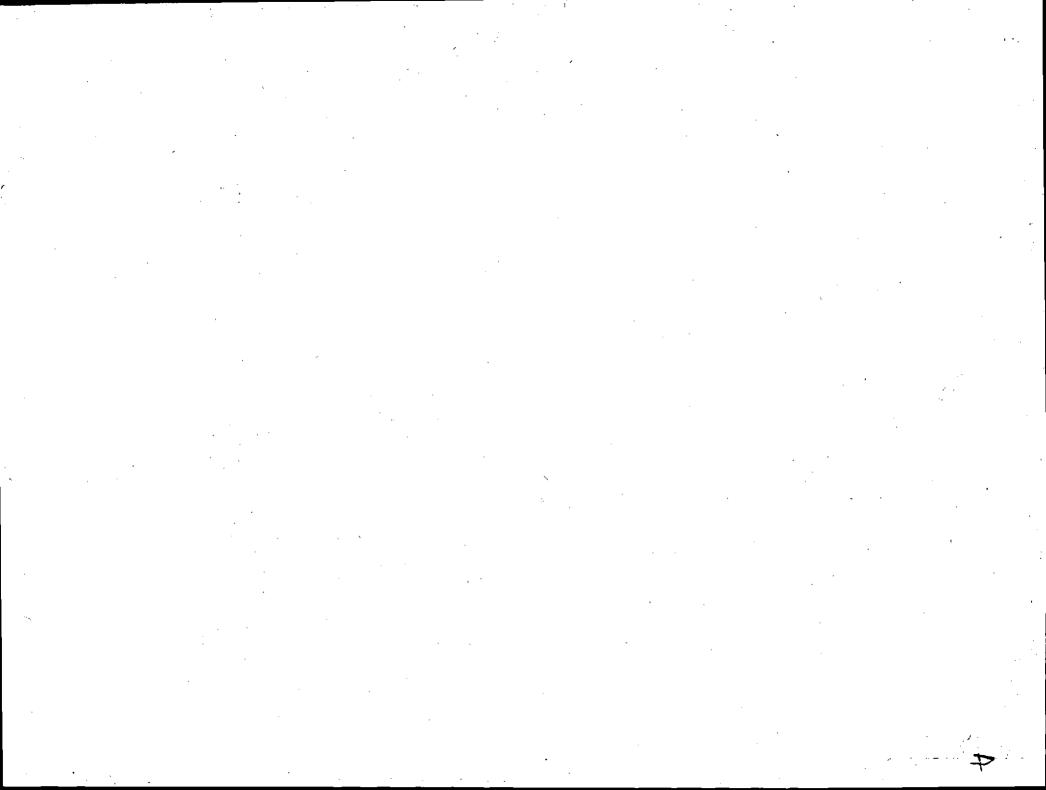
The construction of Blue Sky Scottsdale will require minor improvements to the City's existing sewer infrastructure as indicated in this report. This project will require the abandonment of

existing onsite sewer and the construction of new onsite sewer lines. The proposed wastewater collection system detailed in this report has been designed in accordance with all City of Scottsdale design standards and policies.

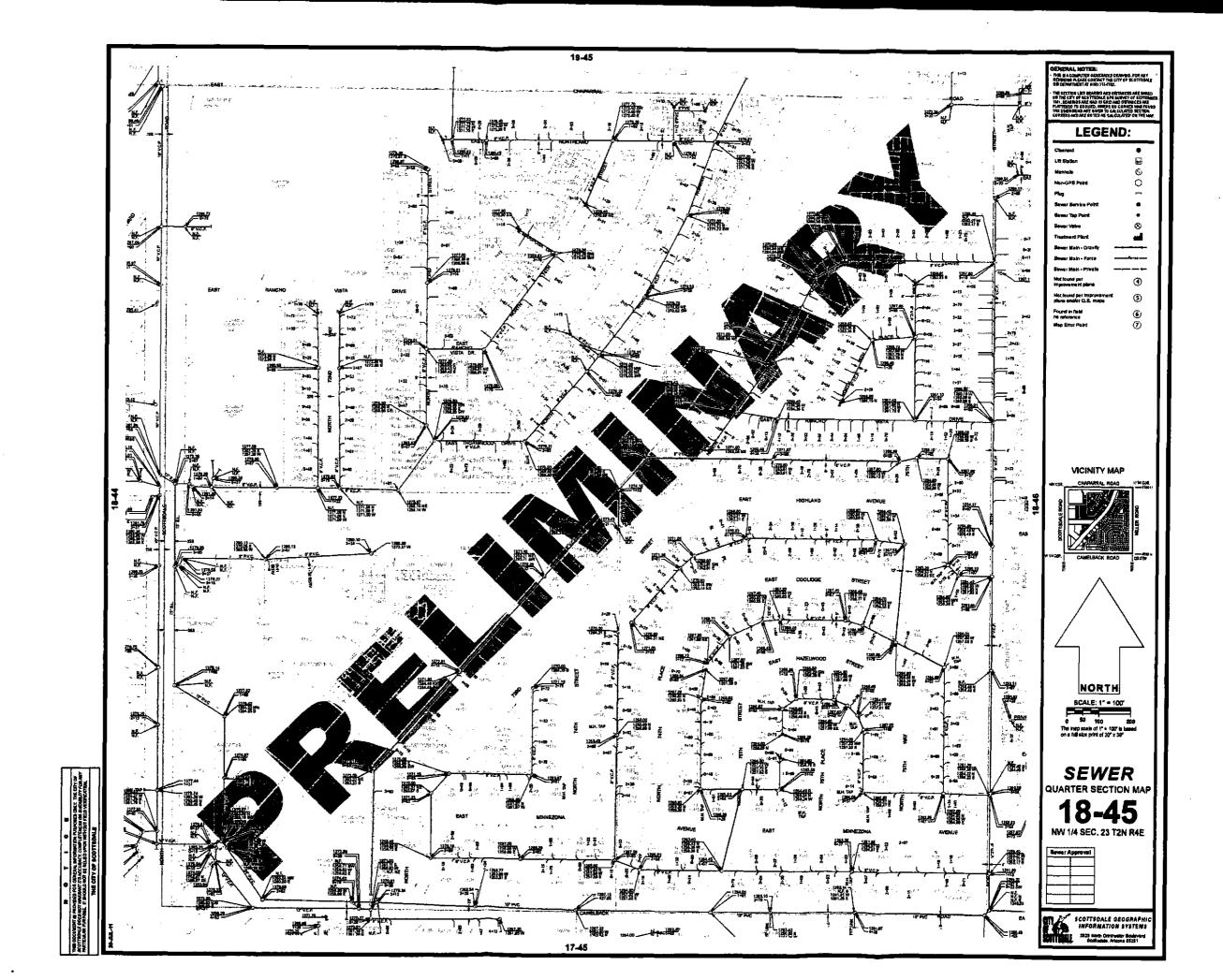
Although exact dates of construction are unknown at this time, it is currently anticipated that Phase 1 will begin construction in June 2012. Phase 1 is expected to be complete in April 2014. Phase 2 is anticipated to begin construction in January 2015. Phase 2 is expected to be complete in April 2016. This schedule is subject to change.







APPENDIX A CITY OF SCOTTSDALE WASTEWATER QUARTER SECTION MAP



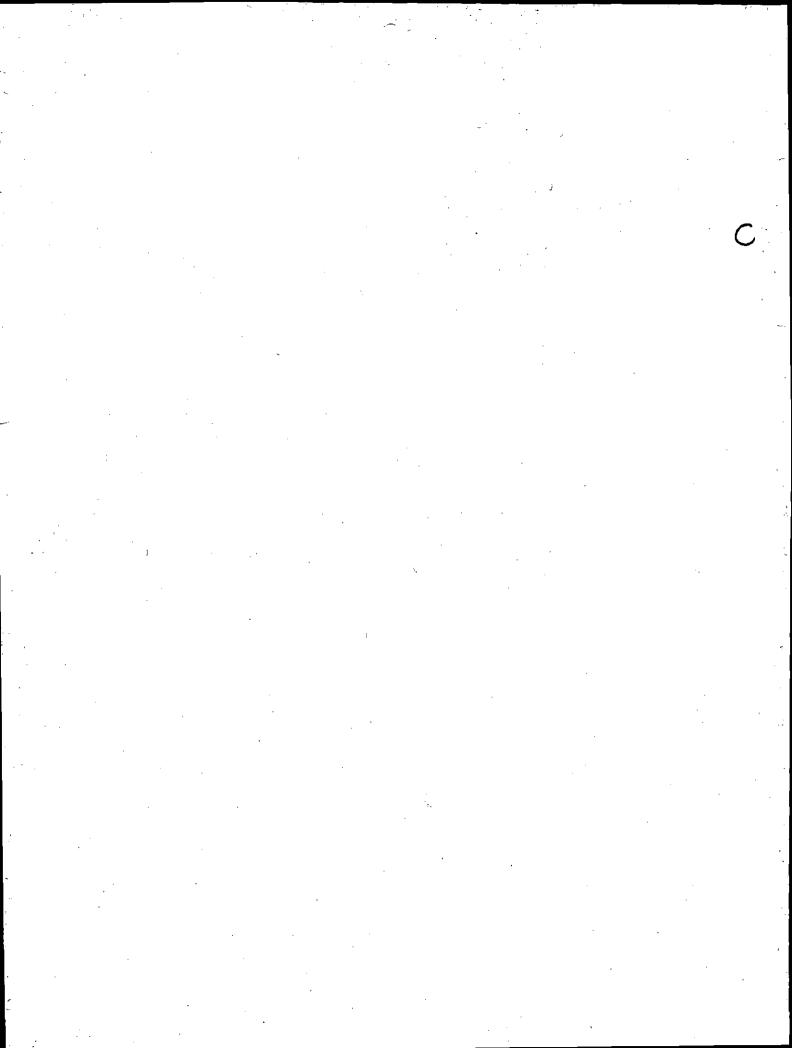
### APPENDIX B WASTEWATER GENERATION CALCULATIONS

### SCOTTSDALE BLUESKY WASTEWATER GENERATION SUMMARY

Printed: 10/11/2011

| Building ID               | Phase | Line<br>Contribution | Land Use               | Area<br>(ft²) | Seats       | Dwelling<br>Units<br>(DU) | Persons /      | Population /<br>Equivalent<br>Population | Unit<br>Wastewater<br>Flow<br>(GPD) | Average<br>Daily Flow<br>(GPD) | Peak<br>Factor | Peak Flow<br>(GPD) | Cumulative<br>Building Peal<br>Flow<br>(GPD) |
|---------------------------|-------|----------------------|------------------------|---------------|-------------|---------------------------|----------------|--|-------------------------------------|--------------------------------|----------------|--------------------|--|
| Portion of Sarari Phase I |       | C-D                  | Residential            |               |             | 26                        | 2.5            | 65                                       | 140                                 | 3,640                          | 4.5            | 16,380             | 16,380                                       |
| North                     | 1     | A-B                  | Grocery                | 32,000        |             |                           | <del> </del>   | 61                                       | 0.19                                | 6,080                          | 4.0            | 24,320             | <del></del> -                                |
| North                     | 1     | A-B                  | Residential            | 241,468       |             | 228                       | 2.5            | 570                                      | 140                                 | 31,920                         | 4.5            | 143,640            | 167,960                                      |
| Main                      | 1     | A-B                  | Retail                 | 25,373        | <del></del> | <del>'</del>              | <del>  -</del> | 127                                      | 0.50                                | 12,687                         | 3.0            | 38,060             | +  |
| Main .                    | 1     | A-B                  | Office                 | 9,468         | -           | -                         | -              | 28                                       | 0.30                                | 2,840                          | 3.0            | 8,521              |  |
| Main                      | 1     | A-B                  | Restaurant             | 10,574        | -           |                           | -              | 127-                                     | 1.2                                 | 12,689                         | 6.0            | 76,133             | <del></del>                                  |
| Main                      | 1     | A-B                  | Residential            | 229,109       |             | 217                       | 2.5            | 543                                      | 140                                 | 30,380                         | 4.5            | 136,710            | 259,424                                      |
| East                      | 2     | C-D                  | Hotel                  | 177,053       |             | 229                       |                | 870                                      | 380                                 | 87,020                         | 4.5            | 391,590            | <del> </del>                                 |
| East                      | 2     | C-D                  | Residential            | 121,209       | _ :         | 120                       | 2,5            | 300                                      | 140                                 | 16,800                         | 4.5            | 75,600             | 467,190                                      |
|                           |       | <u> </u>             | ASE 1 TOTAL (BLUESKY C | INI VS        | <u> </u>    | <u></u>                   | <del> </del>   | <u> </u>                                 |                                     | 96.596                         |                | 427.384            | 427.384                                      |

| PHASE 1 TOTAL (BLUESKY ONLY) | 96,596  | 427,384 | 427,384 |
|------------------------------|---------|---------|---------|
| TOTAL (BLUESKY ONLY)         | 200,416 | 894,574 | 894,574 |
|                              |         | •       |         |
| LINE A-B                     | 96,596  | 427,384 | 427,384 |
| LINE C-D (PHASE 1)           | 3,640   | 16,380  | 16,380  |
| LINE C-D (PHASE 1 + PHASE 2) | 107,460 | 483,570 | 483,570 |



### APPENDIX C FLOWMASTER MODELING CALCULATIONS

#### Worksheet for Line A-B (Phase 1)

|                             | worksneet for   | Line A-B   | <u>(Pnase</u> | <u> </u> |
|-----------------------------|-----------------|------------|---------------|----------|
| Project Description         |                 |            |               |          |
| Friction Method             | Manning Formula |            |               |          |
| Solve For                   | Normal Depth    |            |               |          |
| liput Data                  |                 |            |               |          |
| Roughness Coefficient       |                 | 0.013      |               |          |
| Channel Slope               |                 | 0.1110     | ft/ft         |          |
| Diameter                    | •               | 8          | in            |          |
| Discharge                   |                 | 427384     | gal/day       |          |
| Results                     |                 |            |               |          |
| Normal Depth                |                 | 0.18       | ft            | ,        |
| Flow Area ·                 |                 | 0.08       | ft²           |          |
| Wetted Perimeter            |                 | 0.74       | ft            |          |
| Hydraulic Radius            |                 | 0.11       | ft            | •        |
| Top Width                   | •               | 0.59       | ft            |          |
| Critical Depth              |                 | 0.38       | ft            |          |
| Percent Full                | ÷               | 27.4       | %             |          |
| Critical Slope              |                 | 0.00757    | ft/ft         |          |
| Velocity                    |                 | 8.50       | ft/s          |          |
| Velocity Head               | ,               | 1.12       | ft            |          |
| Specific Energy             |                 | 1.31       | ft            |          |
| Froude Number               |                 | 4.15       |               |          |
| Maximum Discharge           | ÷*              | 2798930.84 | gal/day       |          |
| Discharge Full              |                 | 2601948.10 | gal/day       |          |
| Slope Full                  |                 | 0.00299    | ft/ft         | •        |
| Flow Type                   | SuperCritical   |            |               | •        |
| EVF input Data              | · <u>.</u>      |            |               |          |
| Downstream Depth            |                 | 0.00       | ft            |          |
| Length                      |                 | 0.00       | ft .          |          |
| Number Of Steps             |                 | 0          | •             |          |
| CVF Output Data             |                 |            |               |          |
| Upstream Depth              | ·               | 0.00       | ft            |          |
| Profile Description         | •               |            |               |          |
| Profile Headloss            | •               | 0.00       | ft            | •        |
| Average End Depth Over Rise |                 | 0.00       | %             |          |
| Normal Depth Over Rise      |                 | 27.44      | %             |          |
|                             |                 |            |               |          |

Infinity ft/s

Downstream Velocity

#### Worksheet for Line A-B (Phase 1)

#### CVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.18
 ft

 Critical Depth
 0.38
 ft

 Channel Slope
 0.1110
 ft/ft

 Critical Slope
 0.00757
 ft/ft

#### Worksheet for Line C-D - Outside of Garage (Phase 1)

| Friction Method Solve For Normal Depth    Imput   | Project Description         |                 |           |         |                  |   |   |
|---|-----------------------------|-----------------|-----------|---------|------------------|---|---|
| Solve For         Normal Depth           Input Deta         0.013         Channel Slope         0.0052         ft/ft           Discharge         0.0052         ft/ft           Discharge         16380         gal/day           Results           Normal Depth         0.9         ft²           Normal Depth         0.02         ft²           Wetted Perimeter         0.47         ft           Hydraulic Radius         0.5         in           Vetted Perimeter         0.47         ft           Hydraulic Radius         0.5         in           Perimeter         0.47         ft           Vetter Depth         0.007         ft           Velocity         1.11         ft/fs           Velocity         1.11         ft/fs           Velocity         1.00         ft/fs           Velocity         1.0   | Friction Method             | Manning Formula |           |         |                  |   |   |
| Roughmess Coefficient   | Solve For                   | Normal Depth    |           |         |                  |   | • |
| Channel Slope         0.0052         t/th           Discharge         16380         gal/day           Results         Normal Depth         0.9 in           Flow Area         0.02 ft²           Wetted Perimeter         0.47 ft           Hydraulic Radius         0.6 in           Top Width         0.43 ft           Critical Depth         0.07 ft           Percent Full         11.7 %           Critical Slope         0.00745 ft/ft           Velocity         1.11 ft/s           Velocity Head         0.02 ft           Specific Energy         0.10 ft           Froude Number         0.84           Maximum Discharge         605804.30 gal/day           Discharge Full         563169.99 gal/day           Slope Full         0.00000 ft/ft           Flow Type         SubCritical           SubCritical           SWF Input Data           Downstream Depth         0.0           Number Of Steps         0           GWF Output Data           Upstream Depth         0.0           Froile Description         0           Froile Description         0           Froile Description | else lucid                  |                 |           |         | •                |   |   |
| Channel Slope         0.0052         ft/ft           Diameter         8         in           Discharge         16380         gal/day           Results           Normal Depth         0.9         in           Flow Area         0.02         ft²           Wetted Perimeter         0.47         ft           Hydraulic Radius         0.6         in           Top Width         0.43         ft           Critical Depth         0.07         ft           Percent Full         11.7         %           Critical Slope         0.0076 ft         ft           Velocity         1.11         ft/s           Velocity Head         0.02         ft           Specific Energy         0.10         ft           Froude Number         0.84         gal/day           Maximum Discharge         605504.30         gal/day           Discharge Full         563169.99         gal/day           Slope Full         0.00000         ft/ft           Flow Type         SubCritical         SubCritical           SubCritical           SubCritical         Tritical           SubCr                          | Roughness Coefficient       |                 | 0.013     |         | · <del>- ·</del> |   |   |
| Discharge   16380   gal/day   |                             |                 | 0.0052    | ft/ft   |                  |   |   |
| Normal Depth   0.9 in   | Diameter                    |                 | . 8       | in      |                  |   |   |
| Normal Depth Flow Area  0.02 ft² Wetted Perimeter 0.47 ft Hydraulic Radius 0.6 in Top Width 0.43 ft Critical Depth 0.07 ft Percent Full 11.7 % Critical Slope 0.00746 ft/ft Velocity 1.11 ft/s Velocity 1.11 ft/s Velocity 1.11 ft/s Velocity 1.11 ft/s Velocity 0.000 ft Naximum Discharge 605804.30 gal/day Discharge Full 583169.09 gal/day Slope Full 0.00000 ft/ft Flow Type SubCritical  SWF Input Deta Downstream Depth 0.0 in Length 0.00 ft Number Of Steps 0 in Frofile Description Profile Description Profile Description Profile Description Profile Description Profile Description Profile Description 50.00 ft Average End Depth Over Rise 0.00 % Normal Depth Over Rise 0.00 %   | Discharge                   |                 | 16380     | gal/day |                  | - |   |
| Flow Area   | Results                     |                 |           |         |                  |   |   |
| Wetted Perimeter       0.47       ft         Hydraulic Radius       0.6       in         Top Width       0.43       ft         Critical Depth       0.07       ft         Percent Full       11.7       %         Critical Slope       0.00745       ft/ft         Velocity       1.11       ft/s         Velocity Head       0.02       ft         Specific Energy       0.10       ft         Froude Number       0.84       Maximum Discharge         Maximum Discharge       605804.30       gal/day         Discharge Full       563169.09       gal/day         Stope Full       0.00000       ft/ft         Flow Type       SubCritical       SubCritical         SWF Input Data         Downstream Depth       0.0       in         Length       0.00       ft         Number Of Steps       0       In         SWF Output Data         Upstream Depth       0.0       in         Profile Description       In       In         Profile Description       In       In         Profile Description       In       In         Profile Description   | Normal Depth                | •               | 0.9       | in      |                  |   |   |
| Hydraulic Radius   0.6 in   1   1   1   1   1   1   1   1   1   | Flow Area                   |                 | 0.02      | ft²     |                  |   |   |
| Top Width 0.43 ft Critical Depth 0.007 ft Percent Full 11.7 % Critical Slope 0.00745 ft/ft Velocity 11.11 ft/s Velocity 11.11 ft/s Velocity Head 0.02 ft Specific Energy 0.10 ft Froude Number 0.84 Maximum Discharge 605804.30 gal/day Discharge Full 563159.09 gal/day Slope Full 0.00000 ft/ft Flow Type SubCritical  SVF Input Data  Downstream Depth 0.0 in Number Of Steps 0 in Profile Description Profile Description Profile Headloss 0.00 ft Average End Depth Over Rise 0.00 % Normal Depth Over Rise 11.72 %  | Wetted Perimeter            |                 | 0.47      | ft ,    |                  |   |   |
| Critical Depth       0.07       ft         Percent Full       11.7       %         Critical Slope       0.00745       ft/ft         Velocity       1.11       ft/s         Velocity Head       0.02       ft         Specific Energy       0.10       ft         Froude Number       0.84       Waximum Discharge         Maximum Discharge       605804.30       gal/day         Discharge Full       563169.09       gal/day         Slope Full       0.00000       ft/ft         Flow Type       SubCritical       SubCritical         SWF Input Data         Downstream Depth       0.0       ft         Number Of Steps       0       ft         SWF Output Data         Upstream Depth       0.0       in         Profile Description       0.0       ft         Profile Headloss       0.00       ft         Average End Depth Over Rise       0.00       %         Normal Depth Over Rise       11.72       %   | Hydraulic Radius            |                 | 0.6       | în      |                  |   |   |
| Percent Full         11.7         %           Critical Slope         0.00745         ft/ft           Velocity         1.11         ft/s           Velocity Head         0.02         ft           Specific Energy         0.10         ft           Froude Number         0.84  | Top Width                   | ,               | 0.43      | ft      |                  |   |   |
| Critical Slope         0.00746         ft/ft           Velocity         1.11         ft/s           Velocity Head         0.02         ft           Specific Energy         0.10         ft           Froude Number         0.84  | Critical Depth              |                 | 0.07      | ft      |                  |   |   |
| Critical Slope         0.00746         ft/ft           Velocity         1.11         ft/s           Velocity Head         0.02         ft           Specific Energy         0.10         ft           Froude Number         0.84  | Percent Full                |                 | 11.7      | %       |                  |   | • |
| Velocity Head         0.02         ft           Specific Energy         0.10         ft           Froude Number         0.84         Naximum Discharge           Maximum Discharge         605804.30         gal/day           Discharge Full         563169.09         gal/day           Slope Full         0.00000         ft/ft           Flow Type         SubCritical           SVF Input Data         0.0         in           Length         0.00         ft           Number Of Steps         0         in           SVF Output Data         0.00         in           Profile Description         0.00         ft           Profile Headloss         0.00         ft           Average End Depth Over Rise         0.00         %           Normal Depth Over Rise         11.72         %   | Critical Slope              | •               |           |         |                  |   | , |
| Specific Energy   | Velocity                    | •               | 1.11      | ft/s    |                  |   |   |
| Froude Number         0.84           Maximum Discharge         605804.30         gal/day           Discharge Full         563169.09         gal/day           Slope Full         0.00000         ft/ft           Flow Type         SubCritical           GVF Input Data           Downstream Depth         0.0         in           Length         0.00         ft           Number Of Steps         0         in           GVF Output Data           Upstream Depth         0.0         in           Profile Description         0.00         ft           Average End Depth Over Rise         0.00         %           Normal Depth Over Rise         11.72         %   | Velocity Head               |                 | 0.02      | ft      |                  |   |   |
| Maximum Discharge         605804.30         gal/day           Discharge Full         563169.09         gal/day           Slope Full         0.00000         ft/ft           Flow Type         SubCritical           GVF Input Data           Downstream Depth         0.0         in           Length         0.00         ft           Number Of Steps         0         in           GVF Output Data         0.0         in           Profile Description         0.00         ft           Average End Depth Over Rise         0.00         %           Normal Depth Over Rise         11.72         %   | Specific Energy             |                 | 0.10      | ft      |                  |   |   |
| Discharge Full   563169.09   gal/day  | Froude Number ,             |                 | 0.84      |         |                  |   |   |
| Slope Full   0.00000 ft/ft  | Maximum Discharge           |                 | 605804.30 | gal/day | •                |   |   |
| Slope Full   0.00000   ft/ft  | Discharge Full              |                 | 563169.09 | gal/day |                  |   |   |
| CVF Input Data  Downstream Depth 0.0 in  Length 0.00 ft  Number Of Steps 0  CVF Output Data  Upstream Depth 0.0 in  Profile Description  Profile Headloss 0.00 ft  Average End Depth Over Rise 0.00 %  Normal Depth Over Rise 11.72 %   | Stope Full                  |                 | 0.00000   |         |                  |   |   |
| Downstream Depth  | Flow Type                   | SubCritical     | •         |         |                  | • |   |
| Length         0.00 ft           Number Of Steps         0           GVF Output Data           Upstream Depth         0.0 in           Profile Description           Profile Headloss         0.00 ft           Average End Depth Over Rise         0.00 %           Normal Depth Over Rise         11.72 %   | GVF liput Data              |                 |           |         |                  |   |   |
| Length         0.00 ft           Number Of Steps         0           GVF Output Data           Upstream Depth         0.0 in           Profile Description           Profile Headloss         0.00 ft           Average End Depth Over Rise         0.00 %           Normal Depth Over Rise         11.72 %   | Downstream Depth            |                 | 0.0       | in      |                  |   |   |
| Number Of Steps         0           GVF Output Data         0.0           Upstream Depth         0.0         in           Profile Description         0.00         ft           Profile Headloss         0.00         %           Average End Depth Over Rise         0.00         %           Normal Depth Over Rise         11.72         %   | Length                      |                 | 0.00      | ft      |                  |   |   |
| Upstream Depth 0.0 in  Profile Description  Profile Headloss 0.00 ft  Average End Depth Over Rise 0.00 %  Normal Depth Over Rise 11.72 %  |                             |                 | 0         |         |                  |   |   |
| Profile Description Profile Headloss 0.00 ft Average End Depth Over Rise 0.00 % Normal Depth Over Rise 11.72 %  | GAL ONIONI DETE             |                 |           |         | _                |   |   |
| Profile Description Profile Headloss 0.00 ft Average End Depth Over Rise 0.00 % Normal Depth Over Rise 11.72 %  | Upstream Depth              |                 | 0.0       | in      |                  |   |   |
| Average End Depth Over Rise 0.00 %  Normal Depth Over Rise 11.72 %  | •                           |                 |           |         |                  |   |   |
| Normal Depth Over Rise 11.72 %  | Profile Headloss            |                 | 0.00      | ft      |                  |   |   |
| Normal Depth Over Rise 11.72 %  | Average End Depth Over Rise |                 | 0.00      | %       |                  |   |   |
|   |                             |                 | 11.72     | %       |                  |   |   |
|   | Downstream Velocity         |                 | Infinity  | ft/s    |                  |   |   |

### Worksheet for Line C-D - Outside of Garage (Phase 1)

#### CVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.9
 in

 Critical Depth
 0.07
 ft

 Channel Slope
 0.0052
 ft/ft

 Critical Slope
 0.00746
 ft/ft

#### Worksheet for Line C-D - Through Garage (Phase 1)

|                       | eet for Fille C-D | - I mrougi | ii Garagi | e (Phase I |   |
|-----------------------|-------------------|------------|-----------|------------|---|
| Project Description   |                   |            |           |            |   |
| Friction Method       | Manning Formula   |            |           |            | 4 |
| Solve For             | Normal Depth      |            | -         |            |   |
| Input Data            |                   |            |           |            |   |
| Raughness Coefficient |                   | 0.013      |           |            |   |
| Channel Slope         |                   | 0.0046     | ft/ft     |            |   |
| Diameter              |                   | 8          | in        |            |   |
| Discharge             | •                 | 16380      | gal/day   |            | • |
| Results               |                   |            |           | · _        |   |
| Normal Depth          |                   | 1.0        | in        |            |   |
| Flow Area             |                   | 0.02       | ft²       |            |   |
| Wetted Perimeter      |                   | 0.47       | · ft      |            | • |
| Hydraulic Radius      |                   | 0.6        | in        |            |   |
| Top Width             | •                 | 0.43       | ft        |            |   |
| Critical Depth        |                   | . 0.07     | ft        |            |   |
| Percent Full          |                   | 12.0       | % .       | ·          |   |
| Critical Slope        |                   | 0.00746    | ft/ft     |            | • |
| Velocity              |                   | 1.06       | ft/s      | • •        |   |
| Velocity Head         |                   | 0.02       | ft        |            |   |
| Specific Energy       |                   | 0.10       | ft        |            |   |
| Froude Number         |                   | 0.80       |           |            |   |
| Maximum Discharge     |                   | 569783.14  | gal/day   |            |   |
| Discharge Full        |                   | 529683.03  | gal/day   |            |   |
| Slope Full            | •                 | 0.00000    | ft/ft     |            | - |
| Flow Type             | SubCritical       |            |           |            | , |
| CVF Input Data        |                   |            |           |            |   |
| Downstream Depth      |                   | 0.0        | in        |            |   |
| Length                | •                 | 0.00       | ft,       | •          |   |
| Number Of Steps       |                   | 0          |           |            |   |
| GAL Ontony Deta       |                   |            |           |            |   |

| Upstream Depth              | 0.0      | in   |
|-----------------------------|----------|------|
| Profile Description         |          |      |
| Profile Headloss            | 0.00     | ft   |
| Average End Depth Over Rise | 0.00     | %    |
| Normal Depth Over Rise      | 12.04    | %    |
| Downstream Velocity         | Infinity | ft/s |
|                             |          |      |

#### Worksheet for Line C-D - Through Garage (Phase 1)

#### CALL CALLANT DELE

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 1.0 in
 in

 Critical Depth
 0.07 ft
 th/ft

 Channel Slope
 0.0046 ft/ft
 th/ft

 Critical Slope
 0.00746 ft/ft
 th/ft

|                                       | Worksheet for Line A-B (I             | Jitir      | nate Bu       | ildlout) | _        |   |
|---------------------------------------|---------------------------------------|------------|---------------|----------|----------|---|
| Project Description                   |                                       |            |               |          |          |   |
| Friction Method                       | Manning Formula                       |            |               |          |          | , |
| Solve For                             | Normal Depth                          |            |               |          |          |   |
| hpul Dala                             |                                       |            |               |          |          |   |
| · · · · · · · · · · · · · · · · · · · | · · · · · · · · · · · · · · · · · · · |            |               |          | <u>-</u> |   |
| Roughness Coefficient                 |                                       | 0.013      | G.10          |          |          |   |
| Channel Slope<br>Diameter             |                                       | . 1110     | ft/ft<br>i    |          |          |   |
| Discharge                             | <b>A</b> 5                            | 0<br>27384 | in<br>gal/day |          |          |   |
| ·                                     |                                       | .730+      | gailuay       | ·        |          |   |
| Results                               |                                       |            |               |          |          |   |
| Normal Depth                          | •                                     | 2.2        | in '          |          |          |   |
| Flow Area                             |                                       | 80.0       | ft²           |          |          |   |
| Wetted Perimeter                      |                                       | 0.74       | ft            |          |          |   |
| Hydraulic Radius                      |                                       | 1.3        | in            |          |          |   |
| Top Width                             |                                       | 0.59       | ft            |          |          |   |
| Critical Depth                        |                                       | 0.38       | ft            |          |          |   |
| Percent Full                          |                                       | 27.4       | %             |          |          |   |
| Critical Slope                        | 0.0                                   | 0757       | ft/ft         |          |          |   |
| Velocity                              |                                       | 8.50       | ft/s          |          |          |   |
| Velocity Head                         |                                       | 1,12       | ft            |          |          |   |
| Specific Energy                       |                                       | 1.31       | ft            |          |          |   |
| Froude Number                         |                                       | 4.15       |               |          |          |   |
| Maximum Discharge                     | 27989                                 | 30.84      | gal/day       |          |          |   |
| Discharge Full                        | 26019                                 | 48.10      | gal/day       |          |          |   |
| Slope Full                            | · · · · · · · · · · · · · · · · · · · | 0299       | ft/ft         | ě.       |          |   |
| Flow Type                             | SuperCritical                         |            |               |          |          |   |
| <b>GVF Input Data</b>                 |                                       |            |               |          |          |   |
| Downstream Depth                      |                                       | 0.0        | in            | •        |          |   |
| Length                                | •                                     | 0.00       | ft ·          |          |          |   |
| Number Of Steps                       |                                       | . 0        |               |          | •        |   |
| CVF Output Data                       |                                       |            |               |          |          |   |

| GAL CALLARIDEE              |          |      |  |
|-----------------------------|----------|------|--|
| Upstream Depth              | 0.0      | in   |  |
| Profile Description         |          |      |  |
| Profile Headloss            | 0.00     | ft   |  |
| Average End Depth Over Rise | 0.00     | %    |  |
| Normal Depth Over Rise      | 27.44    | %    |  |
| Downstream Velocity         | Infinity | ft/s |  |
|                             |          |      |  |

#### **Worksheet for Line A-B (Ultimate Buildlout)**

#### GVF Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 2.2
 in

 Critical Depth
 0.38
 ft

 Channel Slope
 0.1110
 ft/ft

 Critical Slope
 0.00757
 ft/ft

#### Worksheet for Line C-D - Outside of Garage (Ultimate Buildlout)

|                             |                 | <u> </u>  | rage (Ortimate Danialout) |  |
|-----------------------------|-----------------|-----------|---------------------------|--|
| Project Description         |                 |           |                           |  |
| Friction Method             | Manning Formula |           |                           |  |
| Solve For                   | Normal Depth    |           |                           |  |
| hpul Dafa                   |                 |           |                           |  |
| Roughness Coefficient       |                 | 0.013     |                           |  |
| Channel Slope               |                 | 0.0052    | ft/ft                     |  |
| Diameter                    | ·               | 8         | in                        |  |
| Discharge                   |                 | 483870    | gal/day                   |  |
| Resulis                     |                 |           |                           |  |
| Normal Depth                |                 | 5.7       | in                        |  |
| Flow Area                   |                 | 0.27      | ft²                       |  |
| Wetted Perimeter            | 7               | 1.34      | ft                        |  |
| Hydraulic Radius            |                 | 2.4       | in ,                      |  |
| Top Width                   |                 | 0.60      | ft                        |  |
| Critical Depth              | •               | 0.41      | ft                        |  |
| Percent Full                |                 | 71.4      | %                         |  |
| Critical Slope              |                 | 0.00795   | ft/ft                     |  |
| Velocity                    |                 | 2.81      | ft/s                      |  |
| Velocity Head               |                 | 0.12      | ft .                      |  |
| Specific Energy             |                 | 0.60      | ft                        |  |
| Froude Number               |                 | 0.74      |                           |  |
| Maximum Discharge           |                 | 605804.30 | gal/day                   |  |
| Discharge Full              |                 | 563169.09 | gal/day                   |  |
| Slope Full                  | •               | 0.00384   | ft/ft                     |  |
| Flow Type                   | SubCritical     |           |                           |  |
| GVF Input Data              |                 |           |                           |  |
| Downstream Depth            |                 | 0.0       | in .                      |  |
| Length                      |                 | 0.00      | ft                        |  |
| Number Of Steps             |                 | 0         |                           |  |
| GAL Ordent Data             |                 |           |                           |  |
| Upstream Depth              |                 | 0.0       | in                        |  |
| Profile Description         | •               |           | :                         |  |
| Profile Headloss            |                 | 0.00      | ft .                      |  |
| Average End Depth Over Rise |                 | 0.00      | %                         |  |
| Normal Depth Over Rise      |                 | 71.38     | %                         |  |
|                             |                 |           |                           |  |

Infinity ft/s

Downstream Velocity

## Worksheet for Line C-D - Outside of Garage (Ultimate Buildlout)

#### GVF Output Data

| Upstream Velocity |   |   | Infinity | ft/s  |
|-------------------|---|---|----------|-------|
| Normal Depth      |   |   | 5.7      | in    |
| Critical Depth    | , |   | 0.41     | ft    |
| Channel Slope     |   |   | 0.0052   | ft/ft |
| Critical Slope    |   | C | .00795   | ft/ft |

#### Worksheet for Line C-D - Through Garage (Ultimate Buildlout)

| Worksheet for                    |                 |                                       | - 3 - (·         |    |   |   |   |
|----------------------------------|-----------------|---------------------------------------|------------------|----|---|---|---|
| Project Description              | <del></del>     | · · · · · · · · · · · · · · · · · · · |                  |    |   |   |   |
| Friction Method                  | Manning Formula |                                       |                  |    |   |   |   |
| Solve For                        | Normal Depth    |                                       | •                |    |   |   |   |
| Input Data                       |                 |                                       |                  |    | , |   |   |
| Roughness Coefficient            |                 | 0.013                                 |                  |    |   |   |   |
| Channel Slope                    |                 | 0.0046                                | ft/ft            |    |   |   |   |
| Diameter                         |                 | 8                                     | in               |    |   |   |   |
| Discharge                        |                 | 483870                                | gal/day          |    |   |   |   |
| Results                          | '               | ę.                                    |                  | ι. |   |   |   |
| Normal Depth                     |                 | 6.0                                   | ·_               |    |   |   |   |
| Normai Depth<br>Flow Area        | •               | 6.0                                   | in<br>A2         |    |   |   |   |
| Netted Perimeter                 |                 | 0.28                                  | ft²              |    |   | 4 |   |
|                                  |                 | 1.40                                  | ft.              |    |   |   |   |
| Hydraulic Radius                 |                 | 2.4                                   | in               |    |   |   |   |
| Fop Width<br>Critical Depth      |                 | 0.58                                  | ft<br>4          |    |   |   |   |
| Percent Full                     |                 | 0.41                                  | ft<br>%          |    |   |   |   |
| •                                |                 | 75.1                                  | %<br>ft∕ft       |    |   |   |   |
| Critical Slope                   |                 | 0.00795<br>2.66                       |                  |    |   |   |   |
| /elocity                         |                 | 2.00<br>0.11                          | ft√s             |    |   |   |   |
| /elocity Head<br>Specific Energy | •               | 0.11                                  | ft.<br>ft        |    |   |   |   |
| Froude Number                    |                 | 0.61<br>0.67                          | Ц                |    |   |   |   |
| Maximum Discharge                |                 | 569783.14                             | noliday          |    |   |   |   |
| Discharge Full                   |                 | 529683.03                             | gal/day          |    |   |   |   |
| Slope Full                       |                 | 0.00384                               | gal/day<br>ft/ft |    |   |   |   |
| Flow Type                        | SubCritical     | 0.00364                               | וטונ             |    |   |   |   |
| ·                                |                 |                                       |                  |    |   |   |   |
| SVF Input Data                   |                 |                                       |                  |    |   |   |   |
| Downstream Depth                 | . •             | 0.0                                   | in               | •  |   |   |   |
| _ength                           |                 | 0.00                                  | ft               |    |   |   |   |
| Number Of Steps                  | •               | 0                                     |                  | •  |   |   |   |
| GVF Output Data                  |                 |                                       |                  |    |   | • | • |
| Jpstream Depth                   |                 | . 0.0                                 | in               |    |   |   | - |
| Profile Description              | •               |                                       |                  |    | • |   |   |
| Profile Headloss                 |                 | 0.00                                  | ft               |    |   |   |   |
| Average End Depth Over Rise      |                 | 0.00                                  | %.               |    |   |   |   |
| TOTAL CITA COPUL OFFI 1406       | •               | 0.00                                  | 7 <b>0</b> .     |    |   |   |   |

75.12 %

Infinity ft/s

Normal Depth Over Rise Downstream Velocity

#### Worksheet for Line C-D - Through Garage (Ultimate Buildlout)

#### **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 6.0
 in

 Critical Depth
 0.41
 ft

 Channel Slope
 0.0046
 ft/ft

 Critical Slope
 0.00795
 ft/ft



#### **Downtown Scottsdale Checklist**

#### **Urban Design & Architectural Guidelines**

| Review Date(s) | Project Name | Case # |
|----------------|--------------|--------|
|                |              |        |

This checklist summarizes the primary components found in the General section of the Downtown Urban and Architectural Design Guidelines – online at <a href="https://www.scottsdaleaz.gov/projects/downtown">www.scottsdaleaz.gov/projects/downtown</a>. The checklist is divided into two parts, - the first, applied at the pre-Application stage, is used to establish each component of the Guidelines as they may apply to a specific project. The second, to be applied during the review of submittals, is intended to help assess a project's response to specific design considerations and community design objectives. This checklist may not represent every potential design related concern or issue related to a project as other considerations from the neighborhood, staff or the Development Review Board may arise. This checklist is not a regulatory device, a replacement of the provisions in the actual Guidelines, nor is it a substitute for a thorough due diligence.

| SEC                      | SECTION A: SITE DEVELOPMENT |        | Design Response   |            |         |              |  |
|--------------------------|-----------------------------|--------|---|------------|---------|--------------|--|
| A1.                      | Relatio                     | nshi   | p to Adjoining Development  | Responsive | Partial | Unresponsive |  |
| ance                     | ☐ High                      | a.     | Builds upon existing predominant development character              |            |         |              |  |
| Importance<br>/ Emphasis | □ Mod.                      | b.     | Coordination with adjacent site plans                               |            | V       |              |  |
| A2.                      | Activat                     | ting t | he Street   | Responsive | Partial | Unresponsive |  |
| Importance<br>/ Emphasis | □ High                      | a.     | Buildings and landscaping define street frontage                    |            |         |              |  |
| Impor<br>/ Emp           | □ Mod.                      | b.     | Front entrance provided   | /          |         |              |  |
| A3.                      | Pedest                      | rian   | Courtyards and Passages   | Responsive | Partial | Unresponsive |  |
| tance                    | ☐ High                      | a.     | Incorporate exterior pedestrian spaces                              |            |         |              |  |
| Importance<br>/ Emphasis | □ Mod.                      | b.     | Building street entrance connects with parking                      |            |         |              |  |
| A4.                      | Parking                     | g Fac  | cilities  | Responsive | Partial | Unresponsive |  |
| ance                     | □ High                      | a.     | Minimize parking frontage   | V          | 2       |              |  |
| Importance<br>/ Emphasis | ☐ Mod.                      | b.     | Interior of blocks utilized for parking                             | V          |         |              |  |
|                          |                             | C.     | Parking and street frontage connected                               | 19/        | 1       |              |  |
|                          |                             | d.     | Buffer sidewalks from parking                                       | -/         | V       |              |  |
|                          |                             | e.     | 15%+ parking lot landscaping (ordinance)                            | V          | 1       | 11           |  |
|                          |                             | f.     | Provide 3 ft. tall parking screening (ordinance)                    |            | MA      | 1            |  |
|                          | 3                           | g.     | Building and parking areas separated with landscape (base planting) |            | 0 1/1   | • /          |  |

Planning & Development Services Department

7447 E Indian School Road, Suite 100, Scottsdale, AZ 85251 • Phone: 480-312-2500 • Fax: 480-312-7088



## **Downtown Scottsdale Checklist**

### **Urban Design & Architectural Guidelines**

| SEC                      | CTION         | B: BUILDING FORM  | Des        | sign Res <sub>l</sub> | ponse        |
|--------------------------|---------------|---|------------|-----------------------|--------------|
| B1.                      | Reduct        | ion of Apparent Size and Bulk   | Responsive | Partial               | Unresponsive |
| 1                        |               | a. Building mass divided into smaller scale components  |            | //                    |              |
| Importance /<br>Emphasis | ☐ High        | b. Horizontal and vertical changes in wall plane  |            |                       |              |
| 1                        |               | c. Building divided horizontally into base, middle and top (or other method)                                    |            |                       |              |
| B2.                      | Covere        | d Walkways  | Responsive | Partial               | Unresponsive |
| o o                      |               | a. Covered walkways provided on pedestrian frontages  |            |                       |              |
| Importance Emphasis      | ☐ High ☐ Mod. | b. Walkway design integral to building  |            |                       |              |
| ğы ш моа.                |               | c. Preferred configuration – 1 story, 16 ft. high, vertical supports  | /          |                       |              |
|                          |               | d. See specific Guidelines for specialty districts  | 7          |                       | 100000       |
|                          | Swi .         | e. Covered walkways may encroach into r.o.w. or setback area  | MA         |                       |              |
| SEC                      | TION          | C: ARCHITECTURAL CHARACTER  | Des        | ign Resp              | oonse        |
| C1.                      | Propor        | tion, Scale and Composition   | Responsive | Partial               | Unresponsive |
|                          |               | a. Composition emphasizes horizontal proportions  |            | 1                     |              |
| Importance /<br>Emphasis | ☐ High ☐ Mod. | <ul> <li>Composition of elevations organized according to defined hierarchy<br/>and rhythmic pattern</li> </ul> |            | 1                     |              |
|                          |               | c. Avoids rigid monotonous patterning   |            | 100                   |              |
|                          |               | d. More wall than window  |            |                       | _            |
|                          |               | e. Wall thickness and mass exaggerated  |            |                       |              |
|                          |               | a. Ground level exhibits human scale  |            |                       |              |
| C2.                      | Buildin       | g Materials   | Responsive | Partial               | Unresponsive |
|                          |               | a. Simple and rich material palette   |            |                       |              |
| Importance /<br>Emphasis | ☐ High ☐ Mod. | b. Material appears honest in its use, placement and in its relationship to other materials                     | ,          | /                     |              |
| _                        |               | c. Material palette incorporates materials in predominant use   |            |                       |              |
|                          | 1977          | d. Glazing is transparent and non-reflective, dull or matte finished  |            | /                     |              |
|                          |               | Avoids repetitive horizontal banding, floor to ceiling window walls and volumes rendered primarily in glass     |            | 1                     |              |

Planning & Development Services Department

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## **Improvement Plan Application Review**

## **Resubmittal Checklist**

| -  | This for  | m plus redlines from the separated by discipline.   | e prev<br>Incon                   | ious su<br>nplete a                    | bmittal(s<br>pplicatio                       | ) must ac<br>n resubr                      | ccompan<br>nittals w                      | y all res<br>ill not be                   | submittals<br>e accepted                                  |
|--|---|---|-----------------------------------|--|--|--|---|---|---|
| Date: <u>1/1</u>   | 18/2012   |   |                                   | Re                                     | view No.:                                    | ☐ 1 <sup>st</sup>                          | 2 <sup>nd</sup>                           | 3 <sup>rd</sup>                           | ☐ 4 <sup>th</sup> or greater                              |
| Plan Che<br>No.: 5016  | eck/Project<br>6-11-1                                   | Case No.:369-PA-2010  |                                   |  | Project L                                    | ocation: <u>4</u>                          | 605 N SC                                  | OTTSDALI                                  | E RD  |
| Civil Plar<br>Reviewe  |   |   |                                   | Em                                     | ıail:  |  |   |   |   |
| Planning<br>Reviewe  |   |   |                                   | Em                                     | ıail:  |  |   |   |   |
| Fire Plan Reviewer:  |   | Email:  |                                   |  |  |  |   |   |   |
| Stormwa<br>Plan Rev  |   | Rumann  |                                   | Em                                     | nail:  | jrumann                                    | @scotts                                   | daleaz.go                                 | <u>ov</u>   |
| EACH R<br>PLANS.<br>REVIEW<br>IMPROV                                   | EVIEWER<br>EACH IMP<br>ER. EASE<br>EMENT PL<br>TALS THA | ATED SHALL BE INCLU (CIVIL, PLANNING, AND ROVEMENT PLAN PACK MENTS AND REPORTS S AN PACKET. PACKETS T HAVE SEPARATE PAC | FIRE) F<br>ET SH<br>SHALL<br>THAT | REQUIR<br>ALL INC<br>ONLY E<br>ARE INC | ES SEPAI<br>CLUDE AL<br>BE INCLUI<br>COMPLET | RATE CO<br>L REQUI<br>DED WIT<br>'E WILL I | MPLETE<br>RED PLA<br>H THE RE<br>NOT BE A | SET OF<br>INS INDIC<br>EQUESTE<br>ACCEPTE | IMPROVEMENT<br>CATED BY EACH<br>ED REVIEWERS<br>ED. (e.g. |
|  |   | lmį   | orove                             | ement                                  | Plan M                                       | lylars                                     |   |   | ·   |
| Sub  | omit Civil, L   | andscape, etc. mylars   |                                   |  | Civil, etc. n                                |  |   |   |   |
|  |   | Mylars ma   | y only                            | be sub                                 | mitted wh                                    | en reque                                   | sted                                      |   | _   |
| Planning Civil and Planning Landscape Review Resubmittal Requirements: |   |   |                                   |  |  |  |   |   |   |
|  | _   | v is complete; see other nents and requirements.  |                                   |  | ırance pol<br>nd industr                     | -  |   | 0 days (C                                 | commercial, multi-  |
| Cor  | mplete set o  | f revised Improvement anning, Fire requirements)  |                                   | Original                               |  | graphic d                                  | escription                                | and ded                                   | ication for Natural                                       |
| □ be i   | included in   | d Irrigation Plans (Shall<br>all Improvement plan<br>nning, and Fire))  |                                   | M.O.D.                                 | Plan (for re                                 | eference o                                 | nly)                                      |   | S dedication<br>reference only)                           |
| ☐ 3 co   | opies of the  | revised N.A.O.S. Exhibit  | (N.A.O.                           | .S. lot int                            | ormation s                                   | shall be pa                                | rovide on                                 | the plan i                                | if applicable).   |
|  | tive plant pl<br>or to the (                            | an (This is separate submi<br>) submittal of the Impro  |                                   | •                                      |  |  | ive Plant                                 | Applicatio                                | on shall be submitted                                     |



## **Improvement Plan Application Review**

#### **Resubmittal Checklist**

| 00 | 791 19bran  |      |       |                     |   |  |  |
|----|---|------|-------|---------------------|---|--|--|
|    | ONLY THE LAST REVIEWER TO COMPL   | ETE  | HIS   | S/HEF               | CKLIST IS TO BE COMPLETED BY ALL REVIEWERS.  R REVIEW IS TO PRINT OUT THE RESUBMITTAL  RERWISE DO NOT PRINT IT OUT. DELETE THIS |  |  |
|    | Fire Civil and Fire Lands   | sca  | pe    | Re                  | view Resubmittal Requirements:  |  |  |
|    | Fire Review is complete; see other  |      | Fin   | al Pla              | at Plan or Condominium Plat Plan (for reference only)   |  |  |
|    | reviewer's comments and requirements.                                     |      | Alta  | a Sur               | vey Plan (no older than one year - for reference only)  |  |  |
|    | Complete set of revised Improvement                                       |      | M.    | D.D.                | Plan (for reference only)   |  |  |
|    | Plans. (Civil, Planning, Fire requirements)                               |      | Fire  | е Нус               | Irant Flow Report (test results)  |  |  |
|    | Other Required Information: THE RESUBN                                    | MITT | AL (  | CHEC                | CKLIST IS TO BE COMPLETED BY ALL REVIEWERS.   |  |  |
|    | ONLY THE LAST REVIEWER TO COMPL   | ETE  | HIS   | S/HEF               | R REVIEW IS TO PRINT OUT THE RESUBMITTAL  |  |  |
|    | CHECKLIST AND RETURN IT WITH THE  | PLA  | NS.   | OTH                 | IERWISE DO NOT PRINT IT OUT. DELETE THIS  |  |  |
| 1  | COMMENT BEFORE PRINTING   |      |       |                     |   |  |  |
|    |   | 900  |       |                     |   |  |  |
|    |   |      |       |                     |   |  |  |
|    | Civil Plan and Civil Landso   | ap   | e P   | lan                 | Review Resubmittal Requirements   |  |  |
|    | Civil Review is complete; see other reviewer's comments and requirements. |      |       |                     | Insurance policy -dated within 30 days (Commercial, multily, and industrial only).  |  |  |
|    | Complete set of revised Improvement Plans.                                |      |       | Orig                | inal Lien holder consent form for each separate dedication  |  |  |
|    | (Civil, Planning, Fire plan requirements)                                 |      |       | Orig                | inal Legal and graphic description and dedication for:  |  |  |
|    | ☐ Grading and Drainage plan(s)  |      |       |                     | Right-of-way  |  |  |
|    | ☐ Paving Plan(s)  |      |       | ☐ Drainage Easement |   |  |  |
|    | ☐ Water Plan(s)   |      |       | ☐ Water Easement    |   |  |  |
|    | Sewer Plan(s)   |      |       |                     | Sewer Easement  |  |  |
|    | Structural Plan(s)  |      | 56    |                     | Multi-use Public Trail Easement   |  |  |
|    | ☐ Horizontal Control Plan   |      |       |                     | Multi-use Public Path Easement  |  |  |
|    | ☐ Traffic Plan  |      |       |                     | Multi-use Public Path and Trail Easement  |  |  |
|    | ☐ Structural / Wall Plans and Calculation                                 | ns   |       |                     | Sight Distance Easement   |  |  |
|    | Revised Drainage Report & redline copy                                    |      | A. C. |                     | Public Access Easement  |  |  |
|    | Soils and Pavement Design Report  |      |       |                     | Emergency and Service Vehicle Access Easement   |  |  |
|    | Water Basis of Design Report  |      |       | M.O                 | .D. Plan (for reference only)   |  |  |
|    | Sewer Basis of Design Report  |      |       | Fina                | l Plat Plan or Condominium Plat Plan (for reference only)   |  |  |
|    | Flow test results   |      |       | Alta                | Survey Plan (no older than one year for reference only)   |  |  |
|    | Water and / or Sewer Service Agreement                                    |      |       | NOI                 | form/permit   |  |  |
|    | County Health Approval  |      |       | 401                 | permit Certificate of Approval  |  |  |
|    | 404 permit Certificate of Approval  |      |       | 404                 | C.O.S. Certification Form   |  |  |



## **Improvement Plan Application Review**

#### Resubmittal Checklist

Other Required Information: The attached drainage review comments need to be addThe following comments are based upon a second review of a preliminary drainage report by David Evan & Associates submitted to the City of Scottsdale (City) on 1/6/2012. This report is intended to explain the phased development of the site as opposed to defining improvements associated with obtaining a CLOMA (Plan Check number 4994-11). This review is also associated with case number 62-DR-2011:

X

- 1. As part of the offsite drainage the report needs to indicate what the depth and finished floor elevations are using COS datum.
- 2. The drainage watershed map needs to be provided on Exhibit A.
- 3. A reference for the regression equation used to calculate peak discharge is needed.
- 4. A reference needs to be corrected.
- 5. The storm drain hydraulic analysis needs to demonstrate that the system does not surcharge or explain the circumstances surrounding the condition.
- 6. Please address all red line comments provided in the preliminary report.
- 7. Provide documentation that other involve agencies have accepted the plan (e.g. FCDMC) ressed.

#### Planning, Neighborhood and Transportation

7447 E Indian School Road, Suite 125, Scottsdale, AZ 85251 • Phone: 480-312-7080 • Fax: 480-312-7781

#### Case Drainage Review - Blue Sky

PROJECT NAME:

BLUE SKY

LOCATION:

4605 N. SCOTTSDALE RD.

PLAN NO:

5016-11

DATE:

12-7-2011

The following comments are based upon a second review of a preliminary drainage report by David Evan & Associates submitted to the City of Scottsdale (City) on 1/6/2012. This report is intended to explain the phased development of the site as opposed to defining improvements associated with obtaining a CLOMA (Plan Check number 4994-11). This review is also associated with case number 62-DR-2011:

- 1. As part of the offsite drainage the report needs to indicate what the depth and finished floor elevations are using COS datum.
- 2. The drainage watershed map needs to be provided on Exhibit A.
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- 4. A reference needs to be corrected.
- 5. The storm drain hydraulic analysis needs to demonstrate that the system does not surcharge or explain the circumstances surrounding the condition.
- Please address all red line comments provided in the preliminary report.
- 7. Provide documentation that other involve agencies have accepted the plan (e.g. FCDMC)

J.M. Rumann, P.E., CFM
Senior Stormwater Engineer
Stormwater Management Division
City of Scottsdale
Phone: 480-312-7072
jrumann@scottsdaleaz.gov

1/2/12

# FINAL DRAINAGE REPORT BLUE SKY SCOTTSDALE FILL PLAN

| Plan #               |
|----------------------|
| Accepted Corrections |
| Reviewed By Date     |

January 2012 DEA PROJECT NO. GRYD00001

4994-1

## FINAL DRAINAGE REPORT **FOR BLUE SKY SCOTTSDALE** FILL PLAN

#### PREPARED FOR

## **GRAY DEVELOPMENT** 1400 E. CAMELBACK ROAD, SUITE 275 PHOENIX, AZ 85018

PREPARED BY

PAUL PAL, P.E. RAMZI GEORGES, PE, CFM DAVID EVANS AND ASSOCIATES, INC. 4600 E WASHINGTON STREET, SUITE 430 PHOENIX, AZ 85034 (602) 678-5151



January 2012 DEA PROJECT NO. GRYD00001

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| 2.0 EXISTI              | NG DRAINAGE CONDITIONS                               | 1               |
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| $\mathbf{F}$            | Reports by Others                                    | 1 1 Saconard    |
| G                       | CLOMR-F/Community Acknowledgement Letter             | Oned.           |
| H                       | Warning and Disclaimer Liability form                | ARIZONA, U.S.K  |
| I                       | 404 Certification                                    | Constant public |
| <u>-</u>                |  | Exp: 3-21-2014  |

#### 1.0 INTRODUCTION

This drainage report has been prepared under a contract with Gray Development, LLC, owner and developer of the Blue Sky Scottsdale project in Scottsdale. The purpose of this report is to provide hydraulic analysis, required by the City of Scottsdale, to support the Blue Sky Scottsdale Stockpile Plans. The plans are to raise the site above the base flood elevation. Preparation of this report has been done in accordance with the procedures detailed in the City of Scottsdale Design Standards and Policies Manual (Reference 1) along with the City of Scottsdale Supplement to MAG Uniform Standard Specifications For Public Works Construction (Reference 2) and Drainage Design Manuals for Maricopa County, Arizona, Volumes I & II (References 3 and 4).

The proposed Blue Sky Scottsdale project is located northeast of the intersection of Scottsdale Road and Camelback Road, within the City of Scottsdale, Maricopa County, Arizona. The site is located within Section 23, Township 2 North, Range 4 East of the Gila and Salt River Base and Meridian.

The site is bound by Coolidge Street to the North, Safari Drive condominium to the northeast, Arizona Canal to the east, Renaissance Center (commercial development) to the south and Scottsdale Road to the West. See Figure 1 Vicinity Map, in Appendix A. Access to the site will be provided from two entrances from Scottsdale Road along 72nd Place and Coolidge Street. The project is located within what is considered the Downtown Core Area of the City of Scottsdale General Plan (see waiver section in Appendix E).

The proposed Blue Sky Scottsdale project is approximately 3± acres. The portion of the site that is under the flood plain will be raised above the determined 100-year base flood elevation.

#### 2.0 EXISTING DRAINAGE CONDITIONS

The initial offsite drainage conditions were analyzed in the previous phase of the project (Safari Drive) and have been referenced and updated based on the latest topographic information and available documents. The updated drainage information is used as the base of the design of the current phase (Blue Sky Scottsdale).

According to the topography in the area, the general lay of the land is in a southeasterly direction, towards the Arizona Canal. The runoff ponds against the canal before it is conveyed through an 8x6 box culvert or weirs over the Arizona Canal. There are three locations that offsite runoff can impact the site. The first location is along the west side of the Arizona Canal. The second location is along Scottsdale Road. The last location is from water backing up from the intersection of Scottsdale and Camelback Roads.

Offsite runoff that reaches the northeastern portion of the site is conveyed along the western boundary of the Arizona Canal in a southwesterly direction through an existing underground box

culvert that was constructed as part of the initial phase known as Safari Drive project. The Arizona Canal is supposed to be drained during major storm events, in addition to a 4-foot of freeboard that would allow the canal to accept additional storm runoff into its system.

The site is located in an area that drains into what is known as Reach 4 of the Flood Control District's side channel drainage system. There is a series of grated inlet structures that capture runoff along the western side of the canal and convey runoff into the underground box culvert mentioned above which outfalls into the storm drain system in Camelback Road. Some of the grate inlet structures are several feet in size and can capture large amount of the runoff that reaches the area.

Scottsdale Road is an improved street with curb and gutter and drains in a southerly direction, adjacent to the site, towards Camelback Road. The majority of the runoff along Scottsdale Road is conveyed within the street section of the road and a smaller portion is conveyed into the existing storm drain system along Scottsdale Road, that outfall into the main storm drain system in Camelback Road.

It is estimated that there is approximately 3,638 cfs that would reach the intersection of Camelback and Scottsdale Roads based on the Safari Drive Final Drainage Report (Reference 8). The majority of the runoff (3,563 cfs) will weir over the Arizona Canal bank into the canal itself, which is supposed to convey the runoff. Approximately 75 cfs of the runoff will spill over Camelback Road in a southerly direction.

The current published FEMA Flood Insurance Rate Map (FIRM) for this area is map number 04013C1695H (Effective date is September 30, 2005). Portions of the site are located within Zones A and X. Zone A is defined as the flood insurance rate zone that corresponds to the 100-year floodplains that are determined in the Flood Insurance Study by approximate methods. Because detailed hydraulic analyses are not performed for such areas, no Base Flood Elevations or depths are shown within this zone. Zone X is defined as "areas of 500-year flood; areas of 100-year flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from the 100-year flood." A copy of the FIRM panel is provided in Appendix B.

#### 3.0 PROPOSED DRAINAGE CONCEPT

The proposed drainage concept is presented in three parts: onsite drainage, off-site drainage, and storage requirements. The hydrologic analysis is in section 4.0 and the hydraulic analysis is summarized in section 5.0. See Exhibit A, located in Appendix A, for an illustration of the proposed drainage concept.

#### 3.1 On-site Drainage Conveyance

The northern portion of the site, will sheet flow into a several feet deep basin as shown on the grading plans in Exhibit A, in Appendix A. The basin will be excavated to provide dirt to raise the eastern portion of the site. The runoff generated in the northern portion of the site will dissipate into the ground. The ponding depth in this basin will be 0.35 feet. Refer to Exhibit F in Appendix A and retention calculations in Appendix D.

The runoff generated along the southern portion of the site will sheet flow southeast into a small ditch on the west side of Canal. The runoff from this ditch will be captured by grated inlet structures west of canal. Refer to grading plans in Appendix A for a graphical illustration of the proposed onsite drainage.

#### 3.2 Off-site Drainage Conveyance

The hydrology for this report is based on the approved final drainage report completed by CVL in 1999. Since then there has been development that took place to the north and west of project site, which restricted the offsite flow from reaching the Arizona Canal. Offsite drainage conditions were studied in the initial phase of the project (Safari Drive) and they are modified during the design of the current phase (Blue Sky Scottsdale) based on the latest available drainage information. Although the original model is used, it is important to mention that Goldwater Boulevard acts as a buffer from offsite flow since it is a raised road in the north east directions and has a major depression that does not flood in the north south directions. As mentioned earlier, there are only three ways the site can be impacted by offsite runoff. The first area that runoff can impact the site is along the northeastern portion of the site, where runoff is being conveyed in a southwesterly direction along the west bank of the Arizona Canal. The second area offsite runoff that could potentially impact the site is from runoff flowing south along Scottsdale Road. The last potential impact to the site is from runoff reaching the intersection of Camelback Road and Scottsdale Road that weir over the Arizona Canal and backs up towards the site.

The first area of investigation was to quantify the offsite runoff along the northeastern portion of the site. Runoff that may impact the site is generated north of Chapparal Road. During field visits it was observed that an 8'x4' concrete box culvert underneath Chapparal Road, west of the Arizona Canal. Few feet upstream of the culvert, is a 20.5'x13' grate inlet structure. Runoff from the north captured by the grate inlet is conveyed in an easterly direction through an approximately what seemed to be a 96" pipe underneath the Arizona Canal. Any runoff that bypasses the grate inlet structure (which is not likely) will flow through the 8'x4' culvert, underneath Chaparral Road, in a southerly direction.

Based on the maximum capacity of 8'x4' box culvert, 277 cfs will flow in southerly direction, of which 200 cfs will spill into the Arizona Canal and the remaining 77 cfs will

continue in the southerly towards the Blue Sky Scottsdale project. This quantification was part of the approved Safari drive final drainage report. However these hydraulic calculations are not included in this report because runoff that reaches the site from the northeast is restricted by existing development to the north or captured by the 8'x6' box culvert inlet (north of Safari Drive). Additional runoff will spill over the Arizona Canal before reaching the BlueSky Scottsdale project. Picture 1 in Appendix A illustrates how the area north of the site, along the Arizona Canal, does not have hydraulic capacity to convey offsite flow.

The second area of investigation was runoff along Scottsdale Road. The final drainage report for Safari Drive (Reference 10) quantified 378 cfs in the vicinity of Scottsdale Road and Coolidge Road. Exhibit H, in Appendix A reflects the existing drainage conditions prior to the Safari Drive development. Scottsdale Road has a half street capacity, adjacent to the site, of approximately 160 cfs. The remainder of the 189 cfs (half the 378 cfs mentioned previously) used to weir into the Safari Drive site through Coolidge Street. To compensate for not allowing the 29 cfs from entering the site, two catch basins were installed along Coolidge Road as part of Safari Drive development that capture approximately 70 cfs from the street flow in Scottsdale Road. Refer to the StormCAD output in Appendix D that shows that the existing catch basins will capture approximately 70 cfs.

Exhibit E in Appendix A reflects the grading information at the intersection of Scottsdale Road and Coolidge Road after the development of the Safari Drive project. The grading allows for runoff to enter the catch basins along Coolidge Road, especially when it exceeds two inches of depth at the gutter. This matched and exceeded the existing grading conditions prior to development of the Safari Drive project.

The ponding depth of 1.2' along the gutter elevation was calculated in the Final drainage report of Safari Drive (Reference 10). Hence the finish floors of the proposed buildings within the Blue Sky Project adjacent to Scottsdale Road are kept 1.2' above the gutter elevation in the street.

Under existing conditions, a flow of 119 cfs resulting from half street runoff of 189cfs along Scottsdale Road with 70 cfs diversion into Coolidge Street mentioned above will reach the intersection of Scottsdale Road and Fashion Square Drive. At that intersection, 80 cfs will continue south along Scottsdale Road and 39 cfs will divert east into Fashion Square Drive. Since Fashion Square Drive (east of Scottsdale Road) will be raised as part of the Blue Sky Scottsdale project development, this will not allow the 39 cfs to continue towards the canal along its historic path. However, since Coolidge storm system captured 70 cfs, which is 41 cfs in additional flow that can compensate for raising Fashion Square Drive. This means that the development will not adversely impact the development to the south. It is important to mention that the area south of the site is already in the floodplain and below the calculated high water elevation for the canal.

The third area of investigation and the last area that could impact the site is the intersection of Scottsdale road and Camelback road. CVL's drainage report (Reference 8 with pertinent excerpts in Appendix F) has quantified approximately 3,638 cfs will reach the intersection of Scottsdale Road and Camelback Road. This runoff will weir into canal with 75 cfs of the runoff will spill over Camelback Road. Refer to Appendix C for summary of the estimated peak Flows. During the initial phase of Safari Drive project, this flow is used to calculate the high water adjacent to the Arizona Canal. The modeling did not take into account the 8'x6' box culvert and no hydraulic calculations for the Camelback Road between Goldwater Boulevard and Scottsdale Road was included.

Based on the same drainage report prepared by CVL (Reference 10), the box culvert will carry approximately 1,000 cfs. The capacity of the culvert has been verified with StormCAD software and the data information is included in Appendix D.

There is approximately 823 cfs that spills into Camelback Road, west of Goldwater Boulevard, refer to exhibit C in Appendix A. FlowMaster computer program (Reference 7) has been used to analyze the split flow at this intersection. The split flow analysis explanation is included in section 5.0 of this report. 184 cfs will flow north along Goldwater Boulevard, 245 cfs will flow south along Goldwater Boulevard and the remainder 393 cfs will continue east along Camelback Road. At the intersection of Marshall Way and Camelback Road; 125 cfs will flow south along Marshall Way and remainder 268 cfs will continue east along Camelback Road. There are three catch basins along the south side of Camelback Road that will capture the remainder of the flow of 268 cfs. These catch basins can capture 288 cfs. Hence, 823 cfs will be subtracted from the total flow that weirs over the canal. Refer to Appendix D for FlowMaster data sheets in Appendix D.

The drainage report prepared by Rick Engineering (Reference 11) dated 2007 for Scottsdale Fashion Square Phase 10 (pertinent excerpts are included in Appendix F), explains that no onsite or offsite flow will spill into the Scottsdale Road through the Fashion Square Mall. In addition, the grading of the area south of the mall drains to the south towards Camelback Road. Hence, the 543 cfs originally estimated by the final drainage report for Safari Drive that would spill into Scottsdale Road will be subtracted from the total flow that weirs over the canal.

Based on the above explanations, the 3,638 cfs runoff originally estimated is reduced by 2,436 cfs. The reduction is based on removing 70 cfs from Coolidge Street diversion, 823 cfs from Camelback Road diversions, 543 cfs from Fashion Square development and 1,000 cfs from the culvert system capacity diversion along the canal. The new flow used in the weir calculation is 1,202 cfs based on straight reduction for all the diversions which is a conservative approach and since a HEC-1 model has not been part of the scope of this study. Based on this reduced flow, the high-water along the Arizona Canal was calculated to be 1279.50. Refer to CulvertMaster (Reference 9) inputs/outputs in Appendix D. The canal overbank has been surveyed in order to model the weir for this report.

In addition as another check of the offsite runoff, the estimated contributing watershed is included in Exhibit J located in Appendix A. The total estimated area is 870 acres or 1.36 square miles. Based on this area and using regression equation  $y=707.21 \ln (x) +1,216$ , where y is the peak flow in cfs and x is the area in square miles, the peak flow is estimated at 1,433 cfs, which is close to 1,202 cfs that we have estimated.

The existing finish floors of the buildings in the Renaissance Center development, south of Blue Sky Scottsdale, vary from 1278.20 to 1278.60, which is approximately 1-foot lower than the existing elevations along the adjacent Arizona Canal. This property may probably flood before runoff weirs over the Arizona Canal. Refer to Exhibit D for a section of the proposed and existing finished grade elevations.

The portion of the Blue Sky Scottsdale project that is under the floodplain will be raised above the 100-year base flood elevation (1279.50) as depicted on the fill plans located in Appendix A. Based on the existing FEMA floodplain, a small portion of the flood plain is being replaced by the fill, approximately 5,690 CY. A portion of this volume will be compensated for in the existing box culvert that has excess storage volume of 670 CY.

The City of Scottsdale vertical datum elevation is 1277.619' based on the NAVD elevation. The proposed finish floor elevations and the future grade breaks at the garage entrances are set minimum 1 foot higher than the high water elevation which is 1279.50'. The fill elevation is 1280.00, which is 0.5 feet higher than the weir elevation. It is important to mention that raising the site above the floodplain was very challenging due to a steep transition from Scottsdale Road of almost 10 percent in one location.

Raising the site above the weir elevation should not impact the base flood elevation. The weir elevations along the canal are not altered. In addition two additional grate inlets structure 4'x4' will be added to increase the capacity of the grated inlets along the Canal. This will compensate for volume loss and accounts for the abandonment of an existing inlet structure along the east portion of the site. Refer to Exhibit C in Appendix A for illustration of the proposed structures and to Appendix D for hydraulic data sheets. The addition of the inlet structures will allow for less ponding behind the canal during smaller storm events that do not weir over the canal. There will additional inlet capacity of 203 cfs that will allow the area to drain faster in the storm drain system.

A CLOMR-F will be filed for this project with FEMA. A copy of the Conditional Letter of Map Revision (CLOMR-F) has been included in Appendix G. A community support letter is included in the same Appendix. The CLOMR-F is based on raising the site higher than base flood elevation. The future proposed structures and finish floors will be free from inundation during a 100-year design storm event.

#### Interim Conditions

In the interim, after the fill plan construction and prior to the project development, the big basin along the north side of the project will pond 0.35 feet. If the water does not percolate in 36 hours, dissipation measures will need to be addressed.

There is an existing berm along Scottsdale Road that will prevent the street runoff from spilling into the Blue Sky Project. The drainage conditions along Coolidge Road will not differ between existing and developed conditions. Fashion Square Entrance will be raised during the fill plan and runoff will not be allowed to spill to the east.

As mentioned earlier, there will be one grate inlet structure abandoned during the fill plan improvements along the Arizona Canal. Refer to the fill plans for details. The structure will be replaced and another grate inlet structure will be added to compensate for filling in the floodplain. Easements for these structures will be coordinated with the reviewer during final design of the project.

#### Grading Along the Canal Grate Inlet Structures

Based on the current grading that is shown along the Arizona Canal bank, no retaining walls are needed at the existing and proposed grate inlet structures since the existing canal bank is away from the drainage structures. The cross section of the canal embankment is shown on the attached Fill Plan in Appendix A.

#### 3.3 Storage Requirements

The proposed Blue Sky Scottsdale project has retention waiver that has been approved by the City of Scottsdale. A copy of the waiver is included in Appendix E. Although the project has retention waiver, this project still provide some storage volume in the existing box culvert (18,000 cubic feet).

#### 4.0 HYDROLOGIC ANALYSIS

No hydrologic analysis has been completed as a part of this drainage report. Offsite flow was based on prior approved Drainage report prepared by CVL (reference 8). One Rational calculation was completed to determine the peak flow for the curb opening along Fashion square. Refer to Exhibit F in Appendix A.

#### 5.0 HYDRAULIC ANALYSIS

The hydraulic analyses of the proposed storm water management facilities is based on the City of Scottsdale's Supplement to MAG Uniform Standard Specifications for Public Works Construction and the Drainage Design Manuals for Maricopa County, Arizona, Volume II Hydraulics.

FlowMaster (Reference 7), a Bentley computer program, has been utilized to analyze the hydraulic capacity for the adjacent street sections to determine the 100-year high water surface elevations based on known offsite runoff along Scottsdale Road. The Flow Master cross sections were cut along Scottsdale Road just south of every intersection with Coolidge Street and Fashion Square Road (Scottsdale slopes in a southerly direction). The cross section south of every intersection was used for split flow analysis (equating the water surface elevation in both directions) because there is momentum with runoff along Scottsdale Road in a southerly direction. In addition, weir to the east will occur after the after runoff reaches the intersection itself and this would another reason for the south location of the cross sections used in the split flow analysis. If the sections were cut to the north of the intersection, it would not represent the field conditions. However the cross sections are include Appendix D but are not used in the analysis.

Camelback Road split flow analysis was based on the top of curb road capacity as shown in Exhibit C. FlowMaster analysis is based on Manning's equation. Refer to Appendix D for detailed input and output data sheets.

DEA modeled the weir along the Arizona Canal based on 1,202 cfs mentioned in section 3.2 using StormCAD software (Reference 9). The high water elevation along the Arizona Canal bank canal was determined to be 1279.50. Survey points were used in modeling the weir over the canal. A separate model was prepared to determine the flow along Scottsdale Road, south of Camelback Road which was determined to be 75 cfs.

StormCAD software (Reference 6) was used in determining the capacity of the culverts installed during the Safari Drive development along Coolidge Street and along the canal. Refer to Appendix D for detailed hydraulic input/output data sheets. The 100-year Hydraulic Grade Line (HGL) was kept below the 100 year weir elevation along the canal and below the 100 year ponding depth along Coolidge Street.

#### 6.0 CONCLUSIONS

Based on the results of this study, it can be concluded that:

- The site will be filled according to the City of Scottsdale Design Standards and Policies Manual.
- The site has a retention waiver and it will directly discharge into the existing box culvert along the western side of the Arizona Canal.
- Coordination with the Flood Control District has been initiated.
- The ultimate outfall (Elevation 1279.20) is located at the southeast corner of the project site maintaining the historic outfall condition.
- Raising a portion of the site above the floodplain elevation will not adversely impact adjacent properties south of the site.
- Properties in the floodplain north of the site are at higher elevations then the project and are not impacted by the proposed development
- Refer to Appendix H for the Warning and Disclaimer Liability form.
- Refer to Appendix I for the Section 404 Certification form.

#### 7.0 REFERENCES

- 1. City of Scottsdale Design Standards and Policies Manual, January 2010
- 2. City of Scottsdale Supplement to MAG Uniform Standard Specifications for Public Works Construction, June 2010.
- 3. Drainage Design Manuals for Maricopa County, Arizona, Volume I, Hydrology, February 2011.
- 4. Drainage Design Manuals for Maricopa County, Arizona, Volume II, Hydraulics, January 28, 1996.
- 5. City of Scottsdale Stormwater Master Plan and Management Program, KVL, 1994.
- 6. Bentley StormCAD V8i, Haestad Methods, Inc.
- 7. Bentley FlowMaster V8i, Haestad Methods, Inc.
- 8. Drainage Report Scottsdale Riverwalk Center Hotel prepared by CVL dated April 9, 1999. Revised March 28, 2001.
- 9. Bentley Culvert Master program V3.3, dated 2009.
- 10. Final Drainage Report for Safari Drive, prepared by David Evans and Associates, Oct 2006.
- 11. Preliminary Grading and Drainage Report by Rick Engineering Company dated 8-6-2012 for Scottsdale and Fashion Square.

## APPENDIX A FIGURES AND EXHIBITS

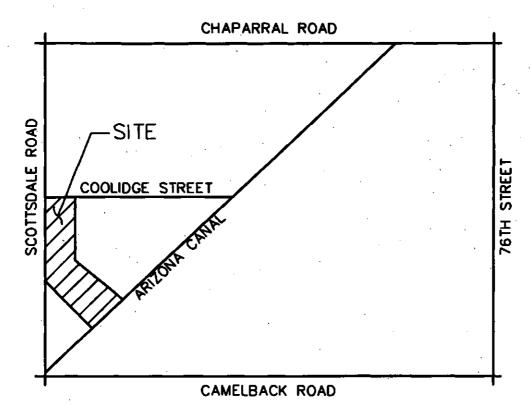


FIGURE 1 - VICINITY MAP

NTS

#### **GENERAL NOTES FOR CONSTRUCTION**

- 1. ALL CONSTRUCTION IN PUBLIC RIGHTS-OF-WAY OR IN EASEMENTS GRANTED FOR PUBLIC USE MUST CONFORM TO LATEST MARICOPA ASSOCIATION OF GOVERNMENTS (MAC) UNIFORM STANDARD SPECIFICATIONS AND UNIFORM STANDARD DETAILS FOR PUBLIC WORKS CONSTRUCTION AS AMENDED BY THE LATEST VERSION OF THE CITY OF SCOTTSDALE (COS) SUPPLEMENTAL STANDARD SPECIFICATIONS AND SUPPLEMENTAL STANDARD DETAILS. IF THERE IS A CONFLICT, LATTER
- 2 THE ENGINEERING DESIGNS ON THESE PLANS ARE ONLY APPROVED BY THE CITY IN SCOPE AND NOT IN DETAIL. IF CONSTRUCTION QUANTITIES ARE SHOWN ON THESE PLANS, THEY ARE NOT VERIFIED BY THE CITY.
- 3. APPROVAL OF PLANS IS VALID FOR SIX (6) MONTHS, IN AN ENCROACHMENT PERMIT FOR THE CONSTRUCTION HAS NOT BEEN ISSUED WITHIN SIX MONTHS, THE PLANS SHALL BE RESUBNITED TO THE CITY FOR RE-APPROVAL.
- 4. A PUBLIC WORKS INSPECTOR WILL INSPECT ALL WORKS WITHIN THE CITY OF SCOTTSOALE RIGHTS-OF-WAY AND IN EASEMENTS. NOTIFY INSPECTION SERVICES 24 HOURS PRIOR TO STARTING CONSTRUCTION (TELEPHONE 480-312-5750).
- 5. WHENEVER EXCAVATION IS TO BE DONE, CALL "BLUE STAKE CENTER," 602-263-1100, TWO WORKING DAYS BEFORE EXCAVATION IS TO BEGIN. THE CENTER WILL SEE THAT THE LOCATION OF THE UNDERGROUND UTILITY LINES IS IDENTIFIED FOR THE PROJECT. CALL "COLLECT" IF NECESSARY.
- 6. ENCROACHMENT PERMITS ARE REQUIRED FOR ALL WORK IN PUBLIC RIGHTS-OF-WAY AND EASEMENTS GRANTED FOR PUBLIC PURPOSES. AN ENCROACHMENT PERMIT WILL BE ISSUED BY THE CITY UPON RECEIPT OF PAYMENT OF A BASE FEE PLUS A FEE FOR INSPECTION SERVICES TO BE PROVIDED BY THE CITY. COPIES OF ALL PERMITS SHALL BE RETAINED ON-SITE AND SHALL BE AVAILABLE FOR INSPECTION AT ALL HEMS. FAILURE TO PRODUCE THE REQUIRED PERMITS WILL RESULT IN IMMEDIATE WORK STOPPAGE UNTIL THE PROPER PERMIT DOCUMENTATION IS OBTAINED.
- 7. ALL EXCAVATION AND GRADING WHICH IS NOT IN PUBLIC RIGHT-OF-WAY OR NOT IN EASEMENTS GRANTED FOR PUBLIC USE MUST CONFORM TO CHAPTER 70, EXCAVATION AND GRADING, OF THE LATEST EDITION OF THE UNIFORM BUILDING CODE PREPARED BY THE INTERNATIONAL CONFERENCE OF BUILDING OFFICIALS. A PERMIT OF THIS GRADING MUST BE SECURED FROM THE CITY FOR A FEE ESTABLISHED BY THE UNIFORM BUILDING CODE.
- 8. ALL CONFINED SPACES ARE SUBJECT TO OSHA STANDARDS.

#### GRADING AND DRAINAGE NOTES

- I. AN ON-SITE GRADING PERMIT IS REQUIRED.
- 2. A SEPARATE PERMIT IS NECESSARY FOR ANY OFF-SITE CONSTRUCTION.
- 3. THE CITY SHALL BE NOTIFIED 24 HOURS BEFORE ANY ON-SITE CONSTRUCTION BEGINS.
- 4. YOU ARE HEREBY ADMSED THAT NO PERSON SHALL USE ANY MECHANICAL EQUIPMENT FOR LAND LEVELING OR CLEARING, ROAD CONSTRUCTION, TRENCHING, EXCAVATING, DEMOLITION OR ENGAGED IN ANY EARTH MOVING ACTIVITY MITHOUT FIRST OBTAINING A PERMIT FROM AIR POLLUTION CONTROL, MARICOPA COUNTY DEPARTMENT OF HEALTH SERVICE'S 1001 N. CENTRAL AVE. SUITE 150 PHOENIX, AZ 85003. PHONE: (802) 508-6666 (THIS NOTICE IS ISSUED PURSUANT TO A.R.S. 36-779.07, NOTICE OF BUILDING AGENCIES.)
- 5. STAKING PAD AND/OR FINISHED FLOOR ELEVATIONS ARE THE RESPONSIBILITY OF THE DEVELOPER OR HIS ENGINEER. IN NON-CRITICAL AREAS, THE DEVELOPER'S ENGINEER SHALL SUBMIT CERTIFICATIONS OF CONSTRUCTED BUILDING PAD ELEVATIONS PRIOR TO THE CITY'S ACCEPTANCE OF PROJECT.
- 6. GRADING CONTRACTOR SHALL DESIGNATE THE LOCATION FOR WASTING SPOIL MATERIALS AND A LETTER FROM THE OWNER GIVING PERMISSION FOR SAID DISPOSAL PRIOR TO STARTING ON-SITE CONSTRUCTION.
- 7. GRADING AND DRAINAGE PLAN APPROVAL INCLUDES: CONSTRUCTION OF DRAINAGE PLAN INCLUDING, BUT NOT LIMITED TO, RETENTION AREAS AND/OR OTHER DRAINAGE FACILITIES, SURFACE GRADING, WALLS, CURBS, ASPHALT PAVEMENT, AND BUILDING FLOOR ELEVATIONS.
- 8. CONTRACTOR IS RESPONSIBLE FOR LOCATING AND CONFIRMING DEPTHS OF ALL THE EXISTING UTILITY LINES WITHIN PROPOSED RETENTION BASIN AREAS. IF THE BASIN CANNOT BE CONSTRUCTED PER PLAN BECAUSE OF CONFLICTS, THE CONTRACTOR SHOULD DISCUSS MODIFICATION OF BASIN CONFIGURATION WITH THE CITY INSPECTOR TO DETERMINE IF A PLAN REVISION OR A FIELD CHANGE IS REQUIRED.
- 9. AN APPROVED GRADING AND DRAINAGE PLAN SHALL BE ON THE JOB SITE AT ALL TIMES. DEVIATIONS FROM THE PLAN MUST BE PRECEDED BY AN APPROVED PLAN REMSION.
- 10. COMPACTION SHALL COMPLY WITH M.A.G. SECTION 601 (95% COMPACTION FOR CMP BACKFILL).
- 11. ALL RAMPS MUST MEET ADA ACCESSIBILITY GUIDELINES (ADAAG) STANDARDS; 2% MAX CROSS SLOPES AND 12:1 MAX LONGTUDINAL SLOPES.
- 12. SIGNS REQUIRE SEPARATE PERMIT AND APPROVAL

#### FEMA TECHNICAL BULLETIN 10-01 - DESIGN REQUIREMENTS

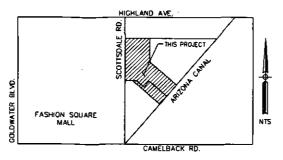
- 1. THE CROWND SURFACE AROUND THE BUILDING AND WITHIN A DEFINED SETBACK DISTANCE FORM THE SPECIAL FLOOD HAZARD AREAS (SFHA) MUST BE AT OR ABOVE THE BASE FLOOD ELEVATION (BFE).
- 2. THE SETBACK IS THE DISTANCE FROM THE EDGE OF THE SFHA TO THE NEAREST WALL OF THE BASEMENT. THE MINIMUM ALLOWABLE SETBACK DISTANCE IS 20 FEET.
- 3. THE GROUND AROUND THE BUILDING MUST BE COMPACTED FILL: THE FILL MATERIAL, OR SOIL OF CLASSIFICATION AND DEGREE OF PERMEABILITY MUST EXTEND TO AT LEAST 5 FEET BELOW THE BOTTOM OF THE BASEMENT FLOOR SLAB.
- 4. THE FILL MATERIAL MUST BE COMPACTED TO AT LEAST 95 PERCENT OF STANDARD LABORATORY MAXIMUM DRY DENSITY (STANDARD PROCTOR). ACCORDING TO ASTM STANDARD D-698. FILLS SOILS MUST BE FINE-CRAINED SOILS OF LOW PERMEABILITY, SUCH AS THOSE CLASSIFIED AS CH. CL. SC OR ML ACCORDING TO ASTM 0-2487. CLASSIFICATIONS OF SOILS FOR ENGINEERING PURPOSES. SEE TABLE 1804.2 IN THE 2000 INTERNATIONAL BUILDING CODE (IBC) FOR DESCRIPTIONS OF THESE SOILS TYPES.
- 5. THE FILL MATERIAL MUST BE HOMOGENEOUS AND ISOTROPIC: THAT IS THE SOIL MUST BE ALL OF ONE MATERIAL, AND THE ENCINEERING PROPERTIES MUST BE THE SAME IN ALL DIRECTIONS.
- 6. THE ELEVATION OF THE BASEMENT FLOOR SHOULD BE NO MORE THAN 5 FEET BELOW THE BFE.
- 7. THERE MUST BE GRANULAR DRAINAGE LATER BENEATH THE FLOOR SLAB AND A \$\frac{1}{2}\$ HORSEPOWER SUMP PUMP WITH BACKUP POWER SUPPLY MUST BE PROVIDED TO REMOVE SEEPAGE FLOW. THE PUMP MUST BE RATED AT FOUR TIMES THE ESTIMATED SEEPAGE RATE AND MUST DISCHARGE ABOVE THE BFE AND AWAY FROM THE BUILDING. THIS ARRANGEMENT IS ESSENTAL TO PREVENT FLOODING OF THE BASEMENT OR UPLIFT OF THE FLOOR UNDER THE EFFECT OF THE SEEPAGE PRESSURE.
- 8. THE CRAINAGE SYSTEM MUST BE EQUIPPED WITH A POSITIVE MEANS OF PREVENTING BACKFLOW.
- 9. NODEL BUILDING CODES ALSO ADDRESS FOUNDATION DRAINAGE (IRC SECTION R-405) AND FOUNDATION WALLS (IRC 9. MODEL BULLING CODES ALD MODIFIES POUNDATION DIVINITIES (THE SECTION R-404) MODEL BUILDING CODES CEREFALLY ALLOW FOUNDATION DRAINS TO DISCHARGE THROUGH ÉITHER MECHANICAL MEANS OR GRAVITY DRAINS. IN ADDITION THERE IS OFTEN AN EXCEPTION TO THE REQUIREMENT FOR DRAINAGE SYSTEM IN WELL-DRAINED SOILS. HOWEVER, IN OR NEAR FLOODPLAINS. WELL-DRAINED SOILS CAN, IN FACT, HELP CONVEY GROUNDWATER TOWARDS THE BUILDING FOUNDATION. THEREFORE, THIS EXCEPTION SHOULD NOT APPLY IN OR NEAR FLOODPLAINS.
- 10. IN SOME CASES IN OR NEAR FLOODPLAINS, EVEN WITH STANDARD DRAINAGE SYSTEMS, HYDROSTATIC PRESSURES FROM GROUNDWATER AGAINST THE BASEMENT CAN RESULT. WHEN A STANDARD DRAINAGE SYSTEM IS UNABLE TO ELIMINATE HYDROSTATIC PRESSURE ON THE FOUNDATION, MODEL BUILDING CODES, INCLUDING THE 2000 INTERNATIONAL RESIDENTIAL CODE (INC SECTION R-404.1.3) REQUIRE THAT THE FOUNDATION BE DESIGNED IN ACCORDANCE WITH ACCEPTED ENGINEERING PRACTICES.

#### **NATIVE PLANT PERMIT:**

NO NATIVE PLANT WILL BE DISTURBED DURING THE CONSTRUCTION OF THIS PROJECT, THIS SITE IS IN A NON-ESL AND NON-NAOS AREA.

## FILL IMPROVEMENT PLANS **FOR** BLUE SKY SCOTTSDALE

A PORTION OF TRACK 'A' OF PARADISE TRIANGLE AS RECORDED IN BOOK 46, PAGE 26, RECORDS OF MARICOPA COUNTY ARIZONA BEING A PORTION OF SECTION 23, TOWNSHIP 2 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER MERIDIAN, MARICOPA COUNTY, ARIZONA



#### VICINITY MAP

#### SHEET INDEX

CIVIL COVER SHEET FILL IMPROVEMENT PLAN

#### **EARTHWORK QUANTITIES FOR ZONE 'A' AREA**

OPTION NO. 1

RAW NUMBERS CUT: 0 CY FILL: 7,353 CY NET: 7.353 CY

RAW NUMBERS CUT: D CY FILL: 6,385 CY NET: 6,385 CY

ADJUSTED REQUIRED FILL: 8.824 CY\* WITH 20% COMPACTION FACTOR

ADJUSTED REQUIRED FILL: 7 662 CY \*WITH 20% COMPACTION FACTOR

#### **EARTHWORK QUANTITIES**

BORROW AREA
CUT: 9,2:1 CY
FILL: D CY
NET: 9,2:1 CY
\*THE GUANTITIES SHOWN HEREON ARE AN ESTIMATE ONLY.
CONTRACTOR SHALL BE RESPONSIBLE FOR VERIFYING ALL
QUANTITIES BEFORE BIDDING.

#### **CITY APPROVALS**

| PANNG                 | TRAFFIC  |
|-----------------------|----------|
| GRADING &<br>DRAINAGE | PLANNING |
| WATER<br>& SEWER      | FIRE     |
| RET.                  |          |

#### **ENGINEER'S FEMA CERTIFICATION**

THE LOWEST FLOOR ELEVATION(S) AND/OR FLOODPROOFING ELEVATION(S) ON THIS PLANS COMPLY WITH THE CLOME FOR THIS PROJECT.

| COMMUNITY | PANEL #<br>PANEL DATE | SUFFIX | DATE OF FIRM<br>(INDEX DATE) | FIRM ZONE | BASE FLOOD ELEY.<br>(IN AO ZONE, USE<br>DEPTH) |
|-----------|-----------------------|--------|------------------------------|-----------|--|
| 045012    | 1695                  | н      | 09-30-2005                   | ZONE "A"  | 1278.5   |
| 5.5012    | 1033                  |        | 09-30-2003                   | ZONE "X"  | N/A  |

#### NO CONFLICT SIGNATURE BLOCK

| UTILITY     | UTILITY COMPANY | NAME OF COMPANY<br>REPRESENTATIVE | TELEPHONE<br>NUMBER | DATE          |
|-------------|-----------------|-----------------------------------|---------------------|---------------|
| ELECTRIC    | APS             | <del>-</del>                      | 502-493-4433        | T-            |
| TELEPHONE   | OWEST           | -                                 | 602-630-0496        | 1-            |
| NATURAL GAS | SOUTH WEST GAS  | -                                 | 602-484-5344        | 1-            |
| CABLE TV    | COX CABLE       | -                                 | 623-328-3506        | 1-            |
| IRRIGATION  | SRP WATER       | -                                 | 602-236-2962        | -             |
| OTHER       |                 |                                   |                     | $\overline{}$ |

#### ENGINEER'S CERTIFICATION

SPACE EASEMENTS.

THE ENGINEER OF RECORD ON THESE PLANS HAS RECEIVED A COPY OF THE APPROVED STIPULATIONS FOR THIS PROJECT AND HAS DESIGNED THESE PLANS IN CONFORMANCE WITH THE APPROVED STIPULATIONS.

#### GEOTECHNICAL NOTE:

A GEOTECHINCAL REPORT HAS BEEN PREPARED FOR THIS A GEOTECHINCAL REPORT HAS BEEN PREPARED FOT HIS 2011; PROJECT 819 FORCE & VANN, INC., DATED AUGUST 911, 2011; PROJECT 21088. CONTRACTOR SHALL REFERENCE 1HIS REPORT AND COMPLY WITH ALL RECOMMEDATIONS CONTAINED THEREIN AS PART OF THIS EARTHWORK MOVING AND COMPACTION EFFORT. MIN COMPACTION FOR FLOODPLAIN RELIEF IS 95%. CONTRACTOR SHALL PROVIDE TESTING DURING COMPACTION EFFORTS AS REQUIRED TO MEET FEMA REQUIREMENTS.

#### SITE DATA

GROSS AREA = 186,526 SQ. FT., 4.282 ± ACRES

#### ENGINEER

DAVID EVANS & ASSOCIATES, INC. 4600 EAST WASHINGTON STREET STE 430 PHDENIX, ARIZONA 85034 PHONE: (602) 678-5151 CONTACT: RAMZI GEORGES, P.E.

#### DEVELOPER/OWNER

GREY DEVELOPMENT LLC 4040 EAST CAMELBACK ROAD, SUITE 275 PHONE: (602) 954-0109

#### **BENCHMARK**

MARICOPA COUNTY ENGINEERING DEPARTMENT BRASS CAP IN A HANDHOLE FOUND AT THE INTERSECTION OF CAMELBACK ROAD AND SCOTTSOALE ROAD, OTY OF SCOTTSOALE GPS POINT 4223. NAVD 88 ELEVATION = 1277.519 (CITY OF SCOTTSDALE VERTICAL DATUM)

#### **BASIS OF BEARING**

BEARINGS SHOWN HEREON ARE BETWEEN A MARICOPA COUNTY ENGINEERING DEPARTMENT BRASS CAP IN A HAND HOLE FOUND AT THE WEST CLUARTER CORNER OF SECTION 23, TOWNSHIP 2 NORTH, RANGE 4 EAST, ALSO BEING THE INTERSECTION OF SCOTTSOALE ROAD AND CAMELBACK ROAD AND A MARICOPA COUNTY ENGINEERING DEPARTMENT BRASS CAP IN A HAND HOLE FOUND AT THE NORTHWEST CORNER OF SECTION 23, TOWNSHIP 2 NORTH, RANGE 4 EAST, ALSO BEING THE INTERSECTION OF SCOTTSDALE ROAD AND CHAPARRAL ROAD, BEARING NOOTOGOE, AS REFERENCED ON THE SAFARI DRIVE I PLAT OF CONDOMINIUM. BOOK 850, PAGE 14, RECORDS OF MARICOPA COUNTY, ARIZONA.

#### STANDARD ABBREVIATIONS

CONCRETE
CATCH BASIN
PAVEMENT
EXISTING
FIRE HYDRANT
FINISHED FLOOR
FLOWLINE
CUTTER ELEVATION GRADE BREAK(CHANGE OF SLOPE)
CITY OF SCOTTSDALE
NATURAL GROUND NG NATURAL GROUM
S SEWER
SD STORM DRAIN
RW RIGHT OF WAY
TC TOP OF CURB
WL WATER LINE
VG VALLEY GUTTER
470.00 (ADD 1400")
0.70.00 EX EX GRADE

#### LEGEND

NOTE: SYMBOLS SHOWN ON THIS MAP IDENTIFYING TOPOGRAPHIC FEATURES MAY NOT BE TO ACTUAL SCALE. SYMBOLS MAY BE ENLARGED FOR VISUAL PURPOSES.

| <del></del> 1 <del></del> | EXIST. TELEPHONE      |
|---------------------------|-----------------------|
| — Е —                     | EXIST. ELECTRICAL     |
| _ <del></del> c           | EXIST. GAS            |
|                           | RIGHT OF WAY          |
|                           | CENTERLINE            |
|                           | BOUNDARY/PROPERTY UNE |
|                           | EASEMENT DESIGNATION  |
| -**                       | CHAIN LINK FENCE      |
| c.:                       | PROPOSED SEWER        |
|                           | PROPOSED WATER        |
| :B1 57                    | PROPOSED STORM ORAIN  |
| s · -                     | EXISTING SEWER        |
| -· · «                    | EXISTING WATER        |
| 52                        | EXISTING STORM DRAIN  |
| 32- 4-                    | EXISTING CONTOURS     |
| 1328                      | PROPOSED CONTOURS     |

#### PROFESSIONAL CERTIFICATION

FEMA FLOCOPLAIN LINE

LICENSE EXPIRATION DATE

SCOTTSDALE BLUESKY, NORTHEAST CORNER OF SCOTTSDALE ROAD AND CAMELBACK ROAD, SCOTTSDALE ARIZONA PROJECT NAME AND ADDRESS

CERTIFY THAT THE DESIGN FOR THE AFOREMENTIONED DEVELOPMENT IS REASONABLY SAFE FROM FLODDING IN ACCORDANCE WITH THE CUIDANCE PROVIDED WITHIN FEMA'S TECHNICAL BULLETIN 10-01 RELATED TO ENSURING THAT STRUCTURES ARE REASONABLY SAFE FROM FLODDING AND IN ACCORDANCE WITH ACCEPTED PROFESSIONAL PRACTICES.

| SIGNATURE      | DATE           |
|----------------|----------------|
| TLE            |                |
| YPE OF LICENSE | LICENCE NUMBER |

EXHIBIT A

DESIGNED DRAWN BY CHECKED E DAVID EVANS
ASSOCIATES II

E. Washington Street, Suite 4
Phoens, Adams 6004
Phone: 602.678.5151

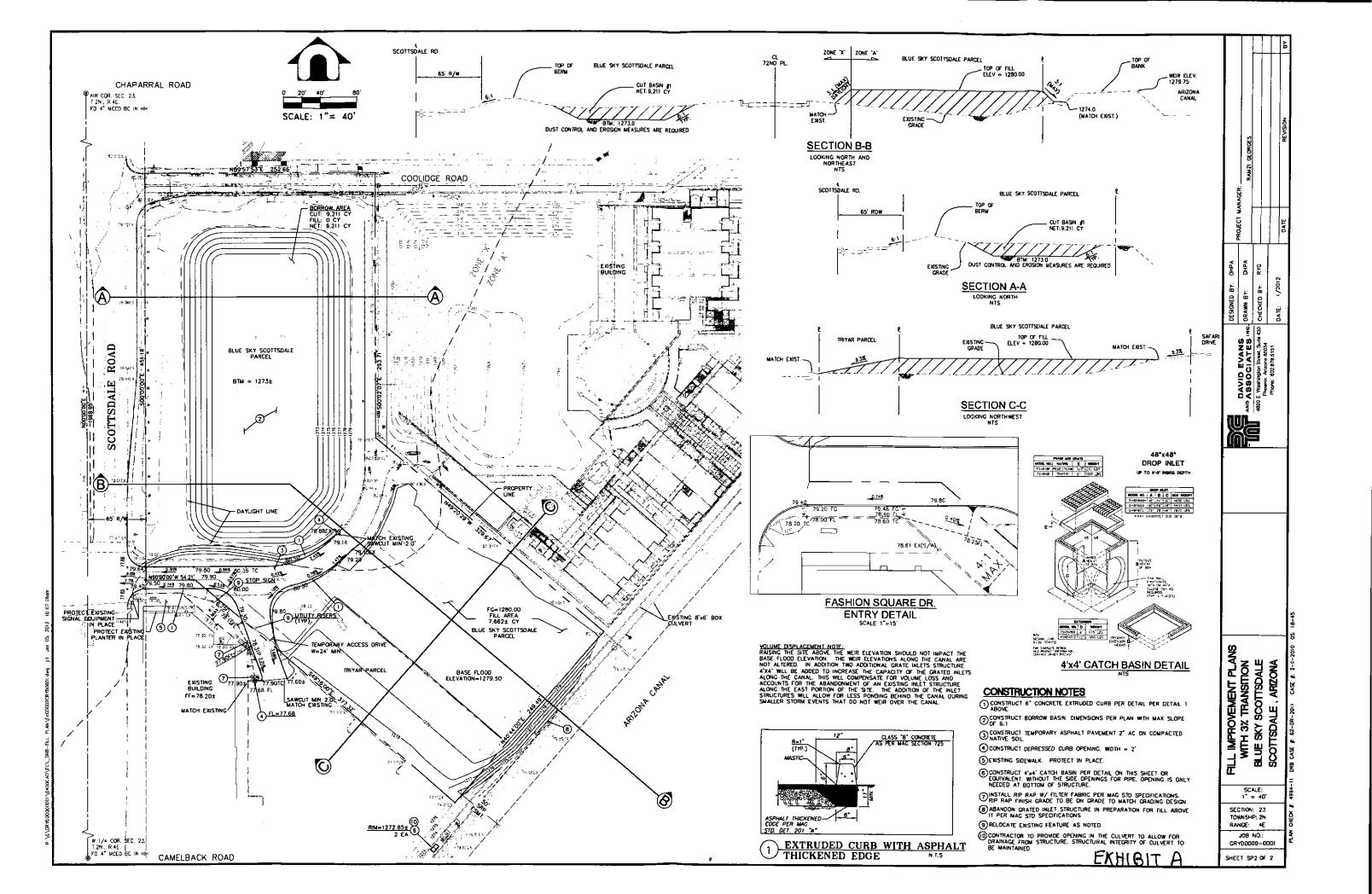
**PLANS** 

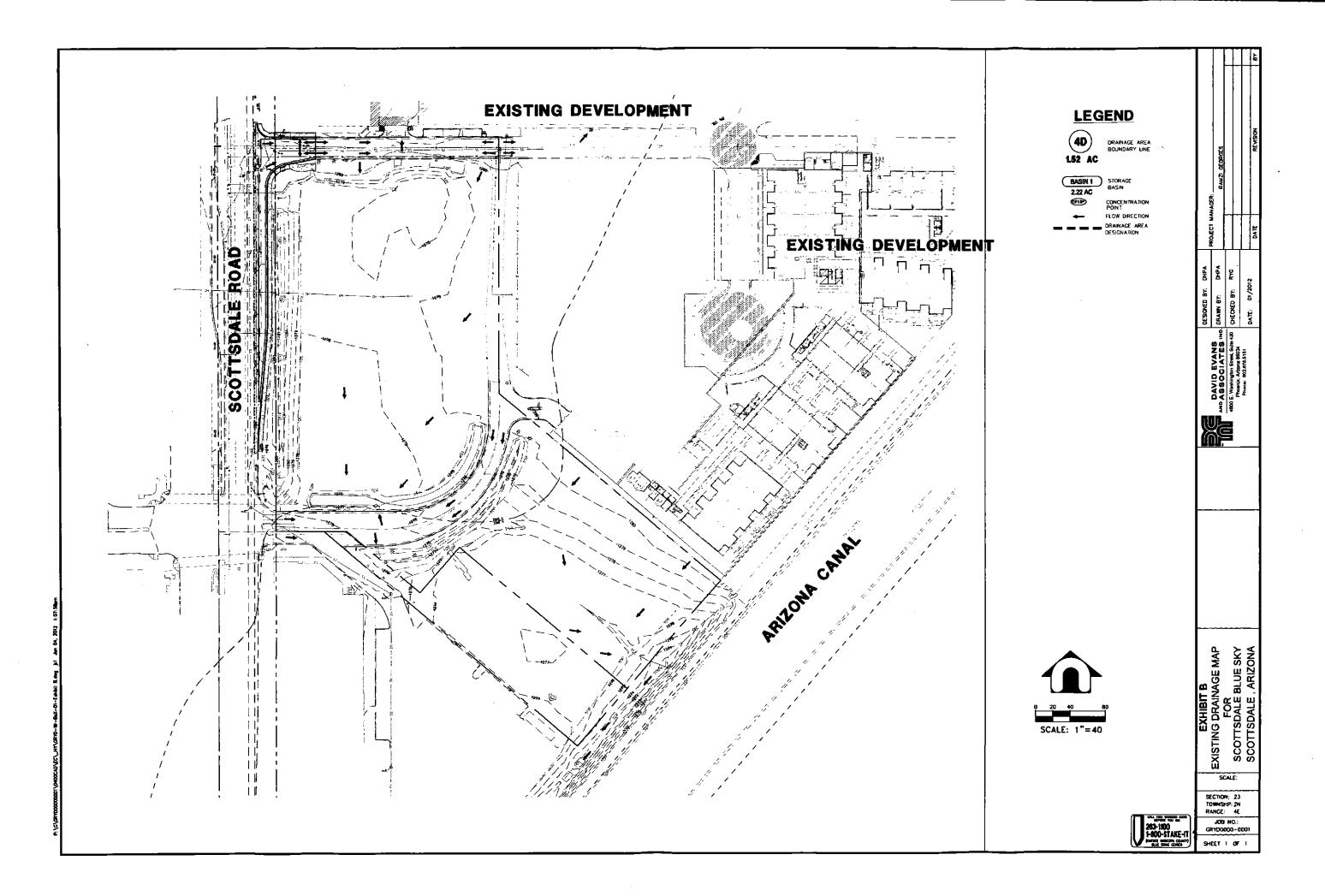
FILL IMPROVEMENT PLAN FOR BLUE SKY SCOTTSDALE SCOTTSDALE, ARIZONA 핕

SCALE: SECTION: 23

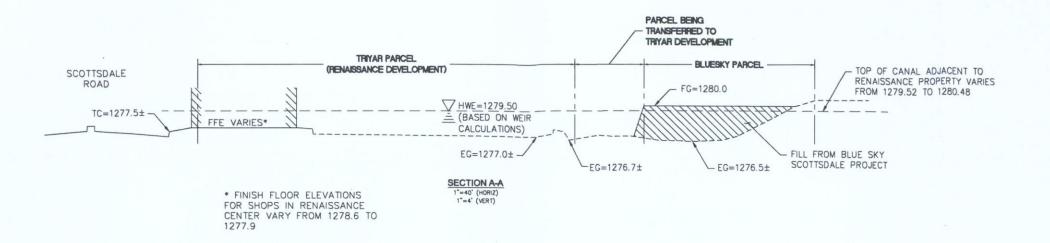
RANGE: 4E JOB NO.:

GRYD0000-0001 SHEET SPLOF 2











DAVID EVANS
AND ASSOCIATES IN
400 E. Warkington Sine, Sub 43
Phone, Afron 6004
Phone, 602,578,5151

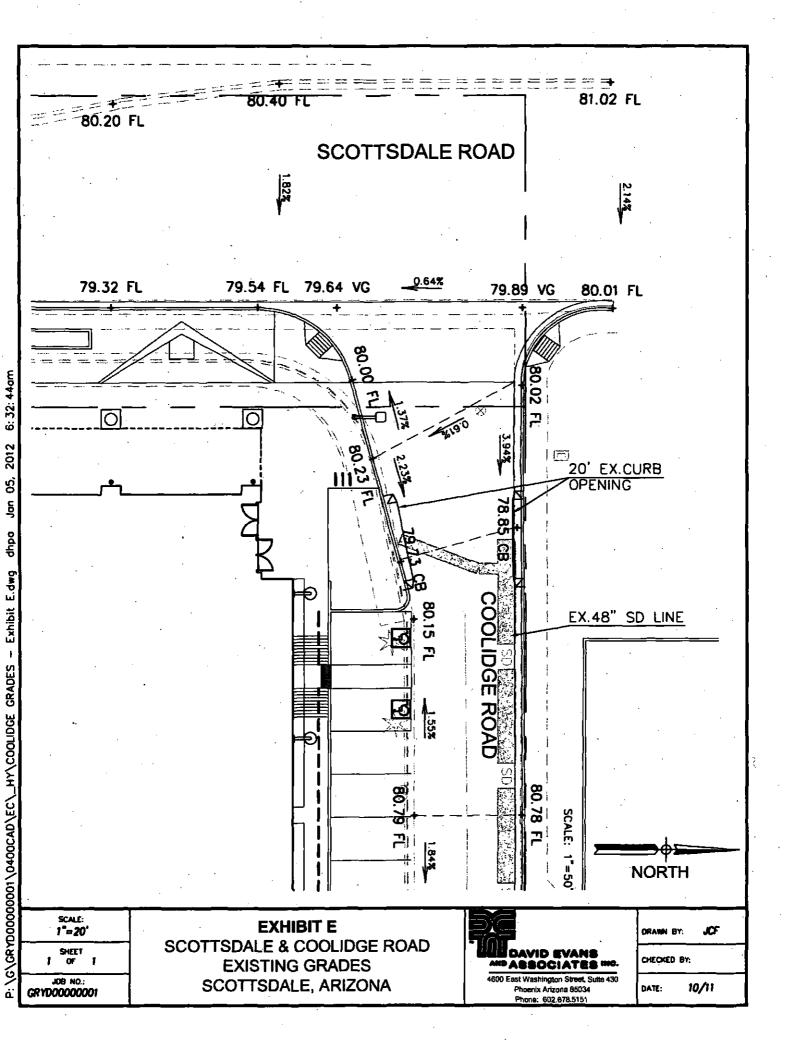
EXHIBIT D
FLOODPLAIN CROSS
SECTION FOR
SCOTTSDALE BLUE SKY
SCOTTSDALE, ARIZONA

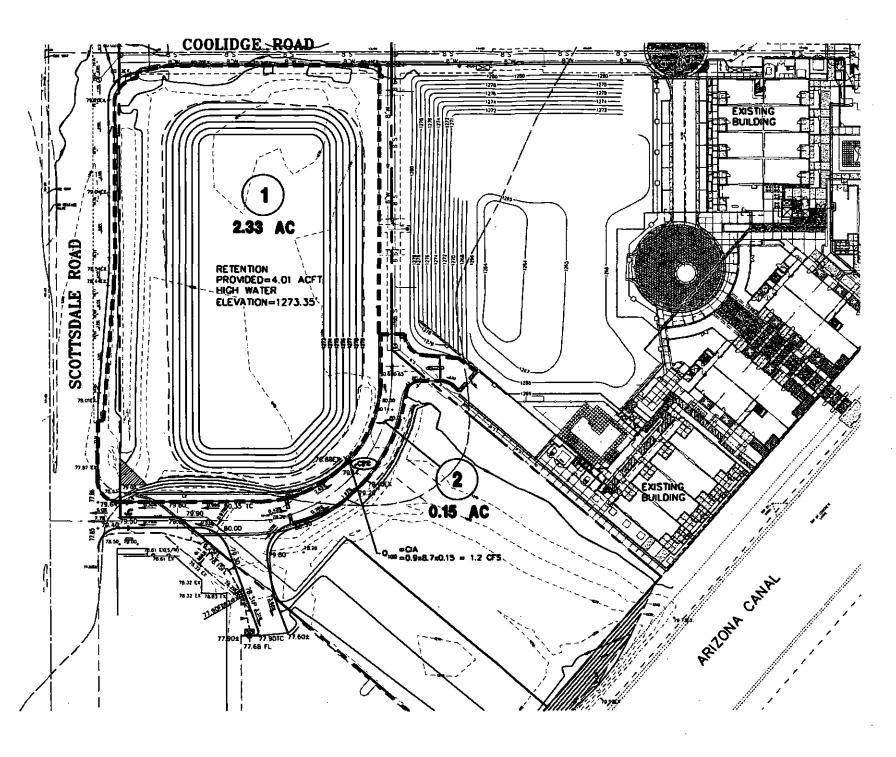
SCALE:

SECTION: 23 TOWNSHP: 2N RANGE: 4E JOB NO.:

JOB NO.: GRYD0000-0001 SHEET 1 OF 1

CALL THIS WORKING DAYS
BETTINE YOU DIG
263-1100
1-800-STAKE-IT
(OUTSEE MARGORA COLARTY)
RUE STAKE CHIER









## **LEGEND**

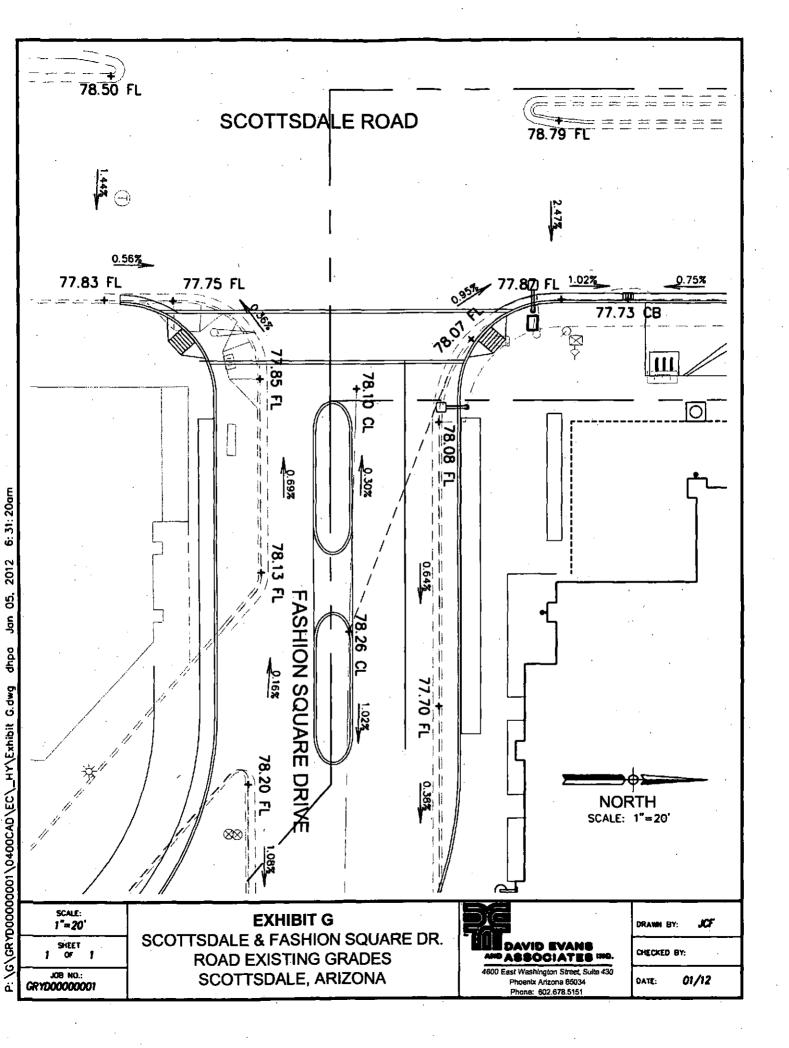
1 1.52 AC

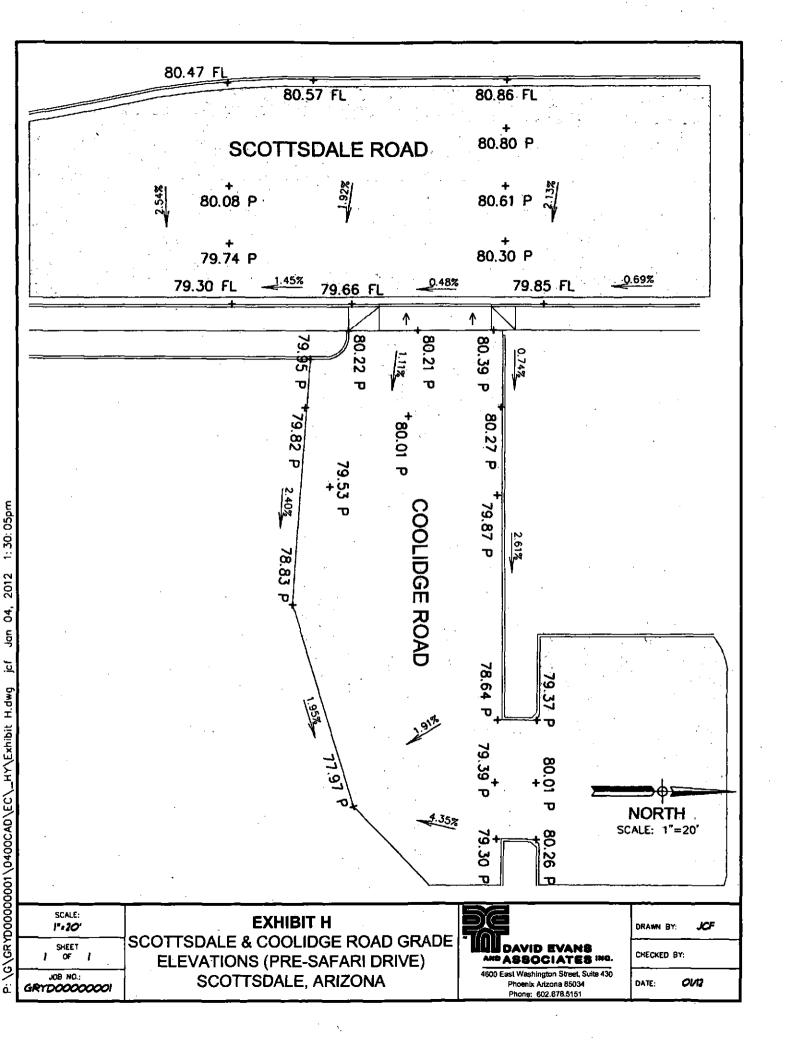
DRAINAGE AREA BOUNDARY LINE

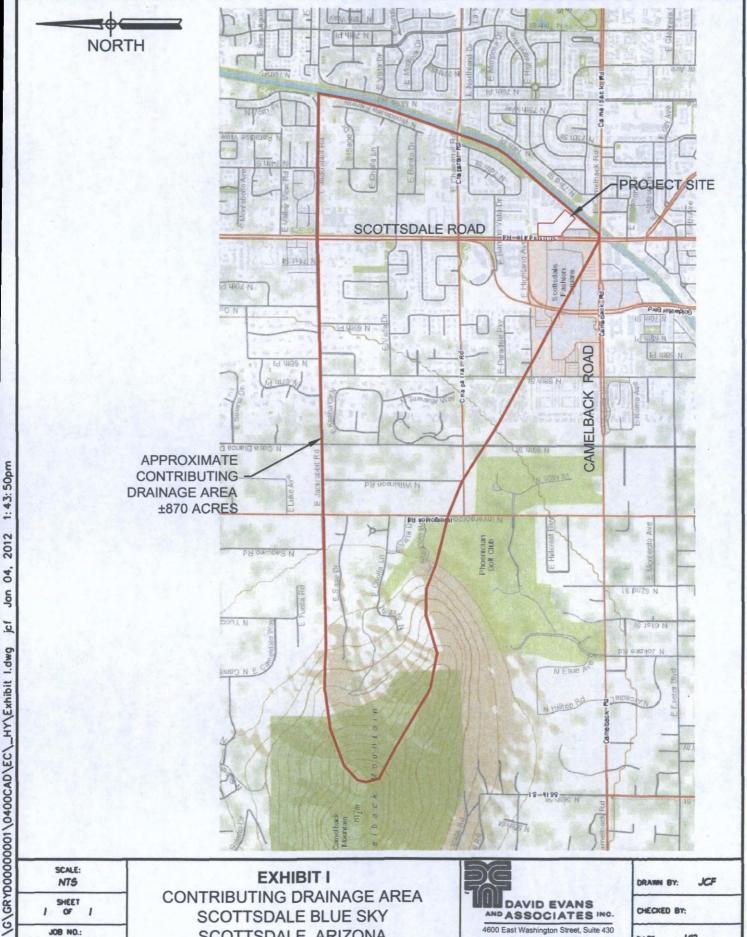
DRAINAGE AREA DESIGNATION CONCENTRATION POINT DAVID EVANS
OF WAShington Street, Suite ASS
AND E. Weshington Street, Suite ASS
Prome, Auton 6004
Prome, Auton 6004
Prome And 8718 6161

EXHIBIT F
RETENTION BASIN EXHIBIT
FOR
BLUE SKY SCOTTSDALE
SCOTTSDALE, ARIZONA

SCALE: 1"=40" SECTION: 23 TOWNSIP: 2N RANGE: 4E JOB NO.: GRYDDOOD-0001 SHEET 1 OF 1







SCOTTSDALE, ARIZONA

Phoenix Arizona 85034 Phone: 602.678.5151

DATE:

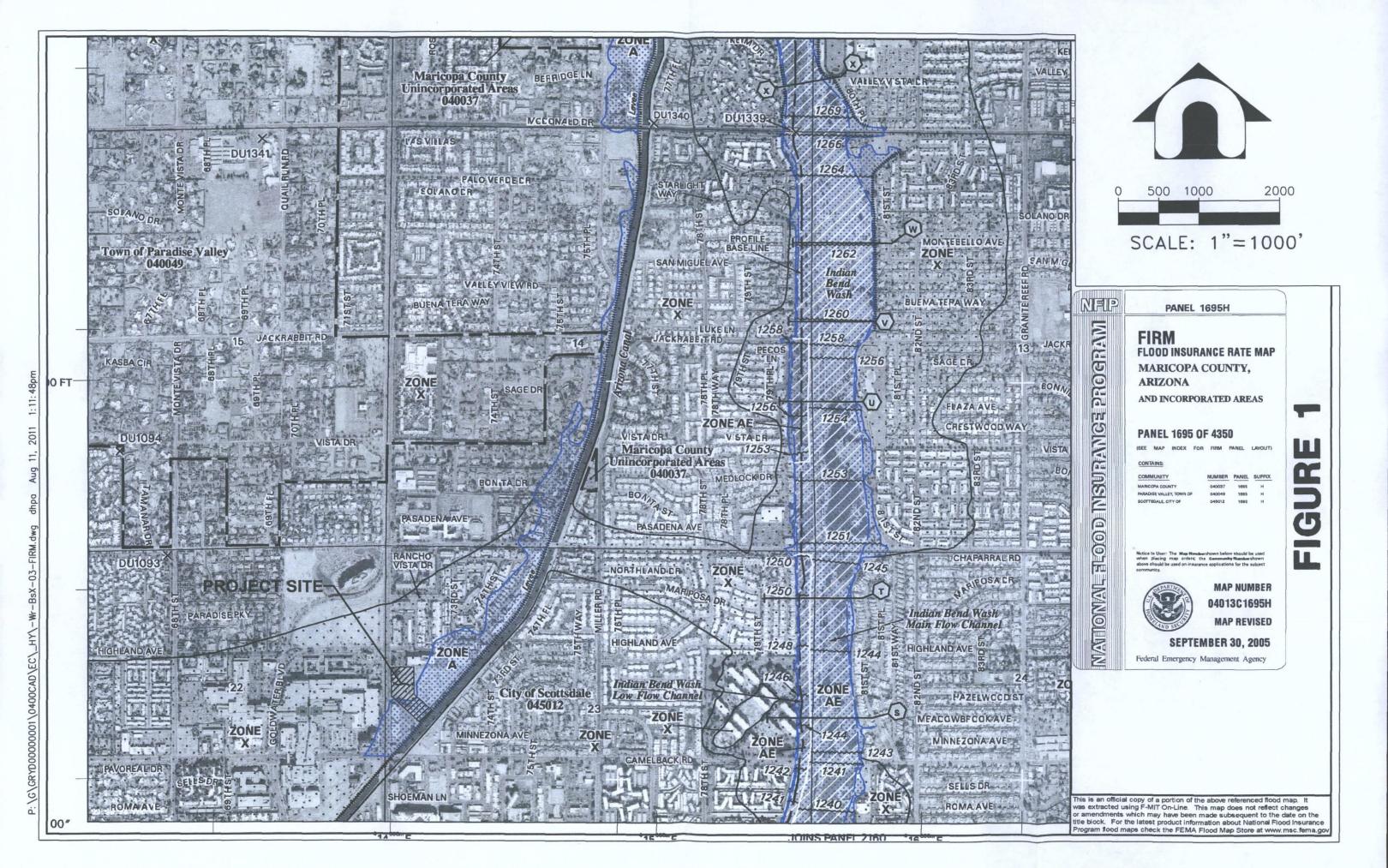
1/12

Jan jo P: \G\GRYD00000001\0400CAD\EC\\_HY\Exhibit 1.dwg

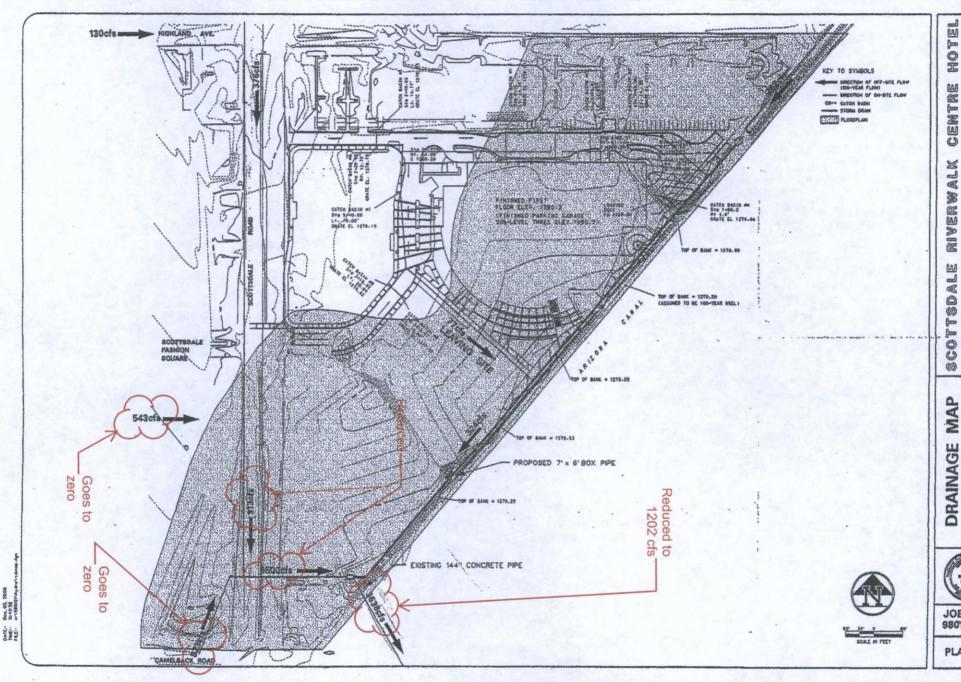
GRYD00000001



# APPENDIX B FLOOD INSURANCE RATE MAP



APPENDIX C RUNOFF EXHIBIT BASED ON SAFARI DRIVE APPROVED DRAINAGE REPORT



1550 NORTH 12TH STREET PHOENIX, ARIZONA 85014



980121-03

PLATE 1

# APPENDIX D HYDRAULIC CALCULATIONS AND DATA SHEETS

Street Section Calculations

## Worksheet for Goldwater Blvd South of Camelback Road - Section 1

| Results             |  |       |   |  |
|---------------------|--|-------|---|--|
|                     |  |       | • |  |
| Top Width           | 40.10  | ft    |   |  |
| Normal Depth        | 0.51   | ft    |   |  |
| Critical Depth      | 0.49   | ft    |   |  |
| Critical Slope      | 0.00640  | ft/ft |   |  |
| Velocity            | 2.34   | ft/s  |   |  |
| Velocity Head       | 0.08   | ft    |   |  |
| Specific Energy     | 0.60   | ft    |   |  |
| Froude Number       | 0.89   |       |   |  |
| Flow Type           | Subcritical  |       |   |  |
| GVF Input Data      | en de la companya de<br>La companya de la co |       |   |  |
| Downstream Depth    | d  | ft    |   |  |
| Length              | 0.00   | ft    |   |  |
| Number Of Steps     | o  |       |   |  |
| GVF Output Data     |  |       |   |  |
| Upstream Depth      | . 0  | ft    | - |  |
| Profile Description |  |       |   |  |
| Profile Headloss    | 0.00   | ft    |   |  |
| Downstream Velocity | Infinity   |       |   |  |
| Upstream Velocity   | Infinity   |       |   |  |
| Normal Depth        | 0.51   | ft    |   |  |
| Critical Depth      | 0.49   |       |   |  |
| Channel Slope       | 0.00500  |       |   |  |
| Critical Slope      | 0.00640  |       |   |  |
| Ontioal Glope       | 0.000-10   | IDIL  |   |  |

| Worksheet for Go  | oldwater Blvd Sou | th of C                 | amelba    | k Road   | - Section 1   |
|---|-------------------|-------------------------|-----------|----------|---------------|
| Project Description   |                   |                         |           |          |               |
| Friction Method   | Manning Formula   |                         |           |          |               |
| Solve For   | Normal Depth      |                         |           |          |               |
| Input Data  |                   | المحادث المحادث المحادث |           |          |               |
| Channel Slope   |                   | 0.00500                 | ft/ft     |          |               |
| Discharge   |                   | 20.00                   | ft³/s     |          |               |
| Section Definitions   |                   |                         |           |          | -             |
| Station (ft)  | Eleyati           | òn (ft)                 |           |          |               |
|   | 0+00              |                         | 0.50      |          |               |
|   | 0+01              |                         | 0.00      |          | •             |
|   | 0+55              |                         | 1.09      |          |               |
|   | 0+56              |                         | 1.59      |          |               |
|   | 0+62              |                         | 1.59      |          |               |
|   | 0+63              |                         | 1.09      |          |               |
|   | 1+06              |                         | 0.25      |          |               |
|   | 1+07              |                         | 0.75      |          |               |
| Roughness Segment Definitions   | 12                | <del></del>             |           |          |               |
| Start Station   | Ending            | Station                 |           | Roughnes | s Coefficient |
| . (0-   | +00, 0.50)        | (1+                     | 07, 0.75) |          | 0.016         |
| Options   | .,                |                         |           |          |               |
| Current Roughness vveignted Method Open Channel Weighting Method Closed Channel Weighting Metho |                   |                         |           |          |               |
| Results   |                   |                         |           |          |               |
| Normal Depth  |                   | 0.51                    | ft        |          |               |
| Elevation Range   | 0.00 to 1.59 ft   |                         |           | 1        |               |
| Flow Area   |                   | 8.56                    | ft²       |          |               |
| Wetted Perimeter  |                   | 40.43                   | ft        |          |               |
|   | •                 |                         |           |          |               |

# Cross Section for Goldwater Blvd South of Camelback Road - Section 1

#### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

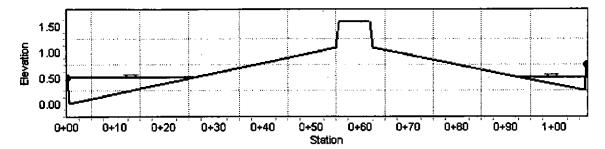
0.00500 ft/ft

Normal Depth

0.51 ft

Discharge

20.00 ft<sup>3</sup>/s



## Worksheet for Camelback Road east of Goldwater Blvd - Section 2

| Project Description          |                               |  |
|------------------------------|-------------------------------|--|
| Friction Method<br>Solve For | Manning Formula  Normal Depth |  |
| Input Data                   |                               |  |
| Channel Slope                | 0.00500 ft/ft                 |  |

32.00 ft<sup>3</sup>/s

Section Definitions

Discharge

| Station (ft) | Elevation (ft) |  |
|--------------|----------------|--|
| 0+00         | 0.50           |  |
| 0+01         | 0.00           |  |
| . 0+47       | 0.85           |  |
| 0+48         | 1.35           |  |
| 0+55         | 1.35           |  |
| 0+56         | 0.85           |  |
| 0+92         | 0.00           |  |
| 0+93         | 0.50           |  |

#### Roughness Segment Definitions

| Start Station  | Ending Station                                    | 3          | Roi | ughness Coefficier | ıt    |
|--|---|------------|-----|--------------------|-------|
| (0+00,   | 0.50)   | (0+93, 0.  | 50) | •                  | 0.016 |
| Options  |   | 3          |     |                    |       |
| Current Rougnness vveignted<br>Method<br>Open Channel Weighting Method | Improved Lotter's Method Improved Lotter's Method |            |     |                    |       |
| Closed Channel Weighting Method  | Horton's Method                                   |            |     |                    |       |
| Results  |   |            |     |                    |       |
| Normal Depth   |   | 0.5 ft     |     |                    |       |
| Elevation Range  | 0.00 to 1.35 ft                                   |            |     |                    |       |
| Flow Area  | 12  | 2.38 . ft² |     |                    |       |
| Wetted Perimeter   | 50  | ).10 ft    |     |                    |       |
| Hydraulic Radius   | (   | ).25 ft    |     |                    |       |

## Worksheet for Camelback Road east of Goldwater Blvd - Section 2

| Results             |             |       | , |
|---------------------|-------------|-------|---|
| Top Width           | 49.68       | ft    |   |
| Normal Depth        | 0.5         | ft    |   |
| Critical Depth      | 0.48        | ft    |   |
| Critical Slope      | 0.00607     | ft/ft | • |
| Velocity            | 2.58        | ft/s  |   |
| Velocity Head       | 0.10        | ft    |   |
| Specific Energy     | 0.60        | ft    |   |
| Froude Number       | 0.91        |       |   |
| Flow Type           | Subcritical |       |   |
| GVF Input Data      |             | -     |   |
| Downstream Depth    | 0           | ft    |   |
| Length              | 0.00        | ft    |   |
| Number Of Steps     | 0           |       |   |
| GVF Output Data     |             |       |   |
| Upstream Depth      | 0           | ft    |   |
| Profile Description |             |       |   |
| Profile Headloss    | 0.00        | ft    |   |
| Downstream Velocity | Infinity    | ft/s  |   |
| Upstream Velocity   | Infinity    | ft/s  |   |
| Normal Depth        | 0.5         | ft    |   |
| Critical Depth      | 0.48        | ft    |   |
| Channel Slope       | 0.00500     | ft/ft |   |
| Critical Slope      | 0.00607     | ft/ft |   |
| •                   |             |       |   |

## Cross Section for Camelback Road east of Goldwater Blvd - Section 2

#### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

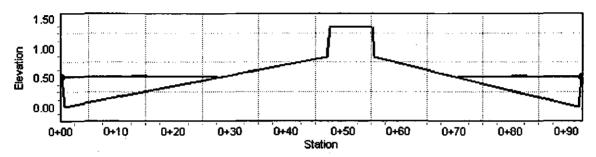
0.00500 ft/ft

**Normal Depth** 

0.5

32.00 ft³/s

Discharge



## Worksheet for Goldwater Blvd North of Camelback Road-Section 3

## Project Description

Friction Method Manning Formula
Solve For Normal Depth

7,76 t 01

# Input Data

 Channel Slope
 0.00500
 ft/ft

 Discharge
 15.00
 ft³/s

**Section Definitions** 

| Station (ft) | Elevation (ft) |
|--------------|----------------|
| 0+00         | 0.50           |
| 0+01         | 0.00           |
| 0+65         | 1.27           |
| 0+66         | 1.77           |
| 0+73         | 1.77           |
| 0+73         | 1.27           |
| 0+96         | 0.83           |
| 0+97         | 1.33           |

#### Roughness Segment Definitions

| Start Station | <u> </u> | Ending | Station | Roughness Coeffi | cient . |
|---------------|----------|--------|---------|------------------|---------|

(0+00, 0.50)

(0+97, 1.33)

0.016

#### **Options**

Current Roughness vveignted

Method

Open Channel Weighting Method

Improved Lotter's Method

Improved Lotter's Method

Closed Channel Weighting Method Horton's Method

## Results

 Normal Depth
 0.48 ft

 Elevation Range
 0.00 to 1.77 ft

 Flow Area
 5.95 ft²

 Wetted Perimeter
 25.03 ft²

0.24

Hydraulic Radius

#### Worksheet for Goldwater Blvd North of Camelback Road-Section 3 Results Top Width 24.83 ft Normal Depth 0.48 Critical Depth 0.46 Critical Slope 0.00615 Velocity 2.52 ft/s Velocity Head 0.10 Specific Energy 0.58 Froude Number 0.91 Flow Type Subcritical **GVF Input Data Downstream Depth**

0.00 ft

| Number Of Steps     | 0        |       |
|---------------------|----------|-------|
| GVF Output Data     | -        |       |
| Upstream Depth      | 0        | ft    |
| Profile Description |          |       |
| Profile Headloss    | 0.00     | ft    |
| Downstream Velocity | Infinity | ft/s  |
| Upstream Velocity   | Infinity | ft/s  |
| Normal Depth        | 0.48     | ft    |
| Critical Depth      | 0.46     | ft    |
| Channel Slope 0.    | 00500    | ft/ft |
| Critical Slope 0.   | 00615    | ft/ft |

Length

# Cross Section for Goldwater Blvd North of Camelback Road-Section 3

#### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

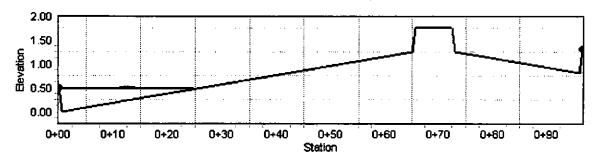
0.00500 ft/ft

**Normal Depth** 

0.48 ft

Discharge

15.00 ft³/s



## Worksheet for Marshall Way South of Camelback Road - Section 4

## Project Description

**Friction Method** 

Manning Formula

Solve For

**Normal Depth** 

## Input Data

Channel Slope

0.00300 ft/ft

Discharge

28.00 ft³/s

**Section Definitions** 

| Station (fi) |      | Elevation (11) |       |
|--------------|------|----------------|-------|
|              | 0+00 |                | 80.00 |
|              | 0+01 |                | 79.58 |
|              | 0+22 |                | 79.74 |
|              | 0+43 |                | 79.43 |
|              | 0+44 |                | 79.93 |

**Roughness Segment Definitions** 

| Stern Sterion | Anding Station | Roughness Coefficient |
|---------------|----------------|-----------------------|

(0+00, 80.00)

(0+44, 79.93)

0.016

#### Options

Current Roughness vveignted

Method

Improved Lotter's Method

**Open Channel Weighting Method** 

Improved Lotter's Method

Closed Channel Mainting Mathod

Horton's Method

| Closed Channel Weighting Method | Horton's Method   |       |     |      |   |
|---------------------------------|-------------------|-------|-----|------|---|
| Resuls                          |                   | ,     |     |      |   |
| Normal Depth                    | •                 | 0.49  | ft  |      |   |
| Elevation Range                 | 79.43 to 80.00 ft |       |     |      |   |
| Flow Area                       |                   | 12.61 | ft² |      |   |
| Wetted Perimeter                |                   | 43.71 | ft  |      |   |
| Hydraulic Radius                |                   | 0.29  | ft  |      |   |
| Top Width                       |                   | 43.38 | ft  |      |   |
| Normal Depth                    |                   | 0.49  | ft  |      | ÷ |
| Critical Depth                  |                   | 0.43  | ft  |      |   |
|                                 |                   |       |     | <br> |   |

# Worksheet for Marshall Way South of Camelback Road - Section 4

| Results             | ·                                   |          |       |   |
|---------------------|-------------------------------------|----------|-------|---|
| Critical Slope      |                                     | 0.00610  | ft/ft |   |
| Velocity            |                                     | 2.22     | ft/s  |   |
| Velocity Head       |                                     | 0.08     | ft    |   |
| Specific Energy     |                                     | 0.56     | ft    |   |
| Froude Number       |                                     | 0.73     |       |   |
| Flow Type           | Subcritical                         |          |       |   |
| GVF Input Data      | - · · · · · · · · · · · · · · · · · |          |       | 1 |
| Downstream Depth    |                                     | 0        | ft    |   |
| Length              |                                     | 0.00     | ft    | • |
| Number Of Steps     |                                     | 0        |       |   |
| GVF Output Data     |                                     |          |       |   |
| Upstream Depth      |                                     | 0        | ft    |   |
| Profile Description |                                     |          |       |   |
| Profile Headloss    |                                     | 0.00     | ft    |   |
| Downstream Velocity |                                     | Infinity | ft/s  |   |
| Upstream Velocity   |                                     | Infinity | ft/s  |   |
| Normal Depth        |                                     | 0.49     | ft    |   |
| Critical Depth      |                                     | 0.43     | ft    |   |
| Channel Slope       |                                     | 0.00300  | ft/ft |   |
| Critical Slope      |                                     | 0.00610  | ft/ft |   |
|                     |                                     |          |       |   |

# Cross Section for Marshall Way South of Camelback Road - Section 4

#### **Project Description**

**Friction Method** 

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

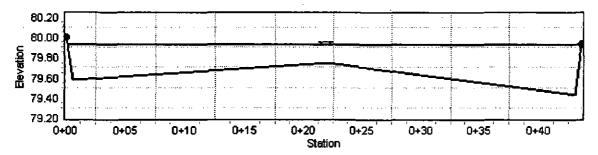
0.00300 ft/ft

**Normal Depth** 

0.49

Discharge

28.00 ft³/s



## Worksheet for Camelback Road east of Marshall Way - Section 5

## Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

#### Input Data

Channel Slope

0.00500 ft/ft

Discharge

60.00 ft<sup>3</sup>/s

Section Definitions

| Station (ff) Elevation (ff). |      |      |  |  |  |
|------------------------------|------|------|--|--|--|
|                              | 0+00 | 0.50 |  |  |  |
|                              | 0+01 | 0.00 |  |  |  |
|                              | 0+52 | 0.54 |  |  |  |
|                              | 0+53 | 1.04 |  |  |  |
|                              | 0+59 | 1.04 |  |  |  |
|                              | 0+60 | 0.54 |  |  |  |
|                              | 0+96 | 0.00 |  |  |  |
|                              | 0+97 | 0.50 |  |  |  |

#### Roughness Segment Definitions

| Start Station   | Ending Station Roughness Coefficient   |
|---|--|
| Marie Control | The state of the s |

(0+00, 0.50)

(0+97, 0.50)

0.016

## Options

Current Roughness vveignted Method

Improved Lotter's Method

**Open Channel Weighting Method** 

Improved Lotter's Method

Closed Channel Weighting Method

Horton's Method

## Results

Normal Depth

0.52 ft

Elevation Range

0.00 to 1.04 ft

Flow Area

22.47 ft<sup>2</sup>

Wetted Perimeter

86.52 ft

Hydraulic Radius

0.26 ft

# Worksheet for Camelback Road east of Marshall Way - Section 5

| Results             |             |       |
|---------------------|-------------|-------|
| Top Width           | 86.06       | ft    |
| Normal Depth        | 0.52        | ft    |
| Critical Depth      | 0.51        | ft    |
| Critical Slope      | 0.00594     | ft/ft |
| Velocity .          | 2.67        | ft/s  |
| Velocity Head       | 0.11        | π     |
| Specific Energy     | 0.63        | ft    |
| Froude Number       | 0.92        |       |
| Flow Type           | Subcritical |       |
| GVF Input Data      |             |       |
| Downstream Depth    | 0           | ft    |
| Length              | 0.00        | ft    |
| Number Of Steps     | 0           |       |
| GVF Output Data     |             |       |
| Upstream Depth      | . 0         | ft    |
| Profile Description |             |       |
| Profile Headloss    | 0.00        | ft    |
| Downstream Velocity | Infinity    | ft/s  |
| Upstream Velocity   | Infinity    | ft/s  |
| Normal Depth        | 0.52        | ft    |
| Critical Depth      | 0.51        | ft .  |
| Channel Slope       | 0.00500     | ft/ft |
| Critical Slope      | 0.00594     | ft/ft |

# Cross Section for Camelback Road east of Marshall Way - Section 5

#### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

0.00500 ft/ft

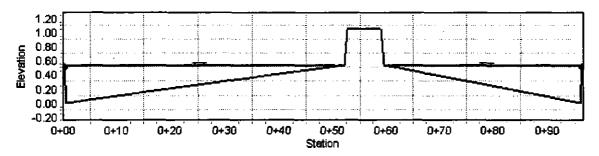
Normal Depth

0.52

ft

Discharge

60.00 ft³/s



| Сара                              | acity of Half-Scottsd       | lale R       | oad - SECTION 7 |            |
|-----------------------------------|-----------------------------|--------------|-----------------|------------|
| Project Description               |                             | A TOP OF THE |                 |            |
| Friction Method                   | Manning Formula             |              |                 | •          |
| Solve For                         | Normal Depth                |              | •               |            |
| Input Data                        |                             |              |                 |            |
| Channel Slope                     | ÷                           | 0.00750      | ft/ft           |            |
| Discharge                         |                             | 160.00       | ft³/s           |            |
| Section Definitions               |                             |              |                 |            |
| Station (ft)                      | Elevation                   | n (ft)       |                 |            |
|                                   | 0+00                        |              | 79.34           |            |
| ,                                 | 0+01                        | ,            | 78.84           |            |
|                                   | 0+02                        |              | 78.79           | •          |
|                                   | 0+24                        |              | 78.34           |            |
|                                   | 0+36                        |              | 77.92           |            |
| •                                 | 0+38                        |              | 77.85           |            |
|                                   | 0+38                        |              | 78.38           |            |
|                                   | 0+43                        |              | 78.47           |            |
|                                   | 0+55                        |              | 79.03           |            |
| Roughness Segment Definitions     | s                           |              |                 | ÷          |
| Start Station                     | Ending St                   | tation       | Roughness C     | cefficient |
| (0                                | 0+00, 79.34)                | (0+5         | 5, 79.03)       | 0.016      |
| Options                           |                             |              |                 |            |
| Current Roughness Weighted Method | Improved Lotter's Method    |              |                 |            |
| Open Channel Weighting Metho      | od Improved Lotter's Method |              | •               | ٠          |
| Closed Channel Weighting Met      | hod Horton's Method         |              |                 |            |
| Results                           |                             |              |                 |            |
| Normal Depth                      |                             | 1.18         | ft ,            |            |
| Elevation Range                   | 77.85 to 79.34 ft           |              |                 |            |
|                                   |                             |              |                 |            |
| Flow Area                         |                             | 29.81        | ft²             |            |

| Capacity                     | of Half-Scottsdale Ro | oad - SECTION 7 |
|------------------------------|-----------------------|-----------------|
| Results                      |                       |                 |
| Hydraulic Radius             | 0.55                  | ft ·            |
| Top Width                    | 54.34                 | ft              |
| Normal Depth                 | 1.18                  | ft              |
| Critical Depth               | 1.28                  | π               |
| Critical Slope               | 0.00437               | ft/ft           |
| Velocity                     | 5.37                  | fl/s            |
| Velocity Head                | 0.45                  | ft              |
| Specific Energy              | 1.63                  | ft ·            |
| Froude Number                | 1.28                  |                 |
| Flow Type S                  | upercritical          | •               |
| GVF Input Data               |                       |                 |
| Downstream Depth             | 0.00                  | ft              |
| Length                       | . 0.00                | ft              |
| Number Of Steps              | 0                     |                 |
| GVF Output Data              |                       |                 |
| Upstream Depth               | 0.00                  | <b>ft</b>       |
| Profile Description          |                       |                 |
| Profile Headloss             | 0.00                  | ft ·            |
| Downstream Velocity          | Infinity              | ft/s            |
| Upstream Velocity            | Infinity              | ft/s            |
| Normal Depth                 | 1.18                  | ft              |
|                              |                       |                 |
| Critical Depth               | 1.28                  | ft              |
| Critical Depth Channel Slope | 1.28<br>0.00750       | ft<br>ft/ft     |

# Capacity of Half-Scottsdale Road - SECTION 7

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

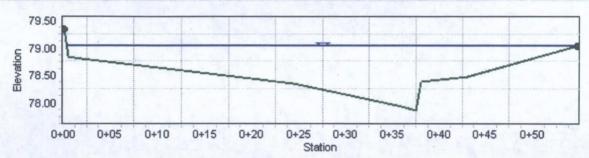
#### Input Data

 Channel Slope
 0.00750 ft/ft

 Normal Depth
 1.18 ft

 Discharge
 160.00 ft³/s

#### **Cross Section Image**



Scottsdale Road Capacity=160 cfs

70 cfs spills into Coolidge Street and captured by 2-20' curb inlets installed as a part of Safari Drive project.

## Half St. Scottsdale Rd South of Fashion Sq Dr-Section 8

## Profest Description

Friction Method

Manning Formula

Solve For

Normal Depth

#### Input Data

Channel Slope

0.00800 ft/ft

Discharge

80.00 ft³/s

**Section Definitions** 

|          |    | . / |       |       |       |
|----------|----|-----|-------|-------|-------|
| Selo (i) |    |     | Eleva | im(i) |       |
|          | 0+ | -00 |       |       | 78.65 |
|          | 0+ | -18 |       |       | 78.35 |
|          | 0+ | -19 |       |       | 77.72 |
|          | 0+ | -64 |       |       | 78.40 |
|          | 0+ | -65 |       |       | 78.90 |

#### **Roughness Segment Definitions**

| SiniSi | වේගා | Ending Station | Roughness@ceiitden? |
|--------|------|----------------|---------------------|

(0+00, 78.65)

(0+65, 78.90)

0.016

#### emiliqo e

Current Rougnness vveignted

Method

Improved Lotter's Method

Open Channel Weighting Method

Improved Lotter's Method

**Closed Channel Weighting Method** 

Horton's Method

|  | Ш |  |
|--|---|--|
|  |   |  |

| Normal Depth     | 0.7               | 5 ft            |
|------------------|-------------------|-----------------|
| Elevation Range  | 77.72 to 78.90 ft |                 |
| Flow Area        | 19.1              | O ft²           |
| Wetted Perimeter | 53.3              | 7 ft            |
| Hydraulic Radius | 0.3               | 6 <del>ft</del> |
| Top Width        | 53.0              | 4 ft            |
| Normal Depth     | 0.7               | 5 ft            |
| Critical Depth   | 0.8               | 1 ft            |
|                  |                   |                 |

# Half St. Scottsdale Rd South of Fashion Sq Dr-Section 8

| Results             | And the second s |        |          |
|---------------------|--|--------|----------|
| Critical Slope      | 0.0  | 0513   | ft/ft    |
| Velocity            |  | 4.19   | ft/s     |
| Velocity Head       |  | 0.27   | ft       |
| Specific Energy     | •  | 1.02   | ft       |
| Froude Number       |  | 1.23   |          |
| Flow Type           | Supercritical  |        |          |
| GVF Input Data      | •  |        |          |
| Daymatanam Danth    |  | 0.00   | ft       |
| Downstream Depth    | ·  | 0.00   | rt<br>ft |
| Length              |  |        | π        |
| Number Of Steps     |  | 0      |          |
| GVF Output Data     | · · · · · · · · · · · · · · · · · · ·  | -      |          |
| Upstream Depth      |  | 0.00   | ft .     |
| Profile Description | ·  |        |          |
| Profile Headloss    |  | 0.00   | ft       |
| Downstream Velocity | In   | finity | ft/s     |
| Upstream Velocity   | In   | finity | ft/s     |
| Normal Depth        |  | 0.75   | ft       |
| Critical Depth      |  | 0.81   | ft       |
| Channel Slope       | 0.0  | 0080   | ft/ft    |
| Critical Slope      | 0.0  | 0513   | ft/ft    |

# Half St. Scottsdale Rd South of Fashion Sq Dr-Section 8

#### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

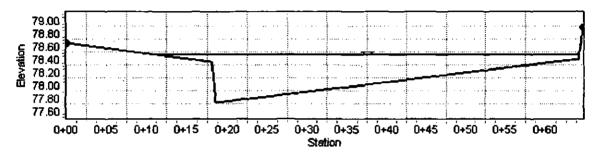
0.00800 ft/ft

Normal Depth

0.75 ft

Discharge

80.00 ft<sup>3</sup>/s



## **Worksheet for Fashion Square Drive - Section 9**

## Project Description

**Friction Method** 

Manning Formula

Solve For

Normal Depth

#### input Data

Channel Slope

0.00350 ft/ft

Discharge

39.00 ft³/s

**Section Definitions** 

|              | ,            |                |       |
|--------------|--------------|----------------|-------|
| Stellen (ii) |              | Elevation (ii) | ·     |
|              | 0 <b>+00</b> |                | 78.50 |
|              | 0+02         | -              | 78.08 |
|              | 0+02         |                | 78.11 |
|              | 0+19         |                | 78.15 |
| •            | 0+23         |                | 78.15 |
|              | 0+39         |                | 77.89 |
|              | 0+40         |                | 78.39 |
|              | 0+54         |                | 78.65 |

#### **Roughness Segment Definitions**

|   | Start Station | India Station | Roughness Coefficient |       |
|---|---------------|---------------|-----------------------|-------|
| • | (0+00, 78.50) | (0+54, 78.65) | -<br>-                | 0.016 |

#### Options

Current Roughness vveignted Method

Improved Lotter's Method

**Open Channel Weighting Method** 

Improved Lotter's Method

**Closed Channel Weighting Method** 

Horton's Method

#### allyee#

| Normal Depth     |                   | 0.57  | ft  |
|------------------|-------------------|-------|-----|
| Elevation Range  | 77.89 to 78.65 ft |       |     |
| Flow Area        |                   | 14.67 | ft² |
| Wetted Perimeter |                   | 43.58 | ft  |
| Hydraulic Radius |                   | 0.34  | ft  |

## **Worksheet for Fashion Square Drive - Section 9**

|                     | <del></del> | <u>oqua.o</u>     | , =111, 0 , 0001-01-1 |
|---------------------|-------------|-------------------|-----------------------|
| Results             |             |                   |                       |
| Top Width           |             | 43.34             | <b>4</b> π            |
| Normal Depth        |             | 0.57              | 7 ft                  |
| Critical Depth      |             | 0.52              | ? ft                  |
| Critical Slope      |             | 0.00556           | 6 ft/ft               |
| Velocity            |             | 2. <del>6</del> 6 | ∄ ft/s                |
| Velocity Head       |             | 0.11              | l ft                  |
| Specific Energy     | ·           | 0.68              | 3 ft                  |
| Froude Number       |             | 0.81              | l                     |
| Flow Type           | Subcritical |                   |                       |
| GVF Input Data      |             | -                 |                       |
| Downstream Depth    |             | 0.00              | ) ft                  |
| Length              |             | 0.00              | ) ft                  |
| Number Of Steps     |             | 0                 | )                     |
| GVF Output Data     |             |                   |                       |
| Upstream Depth      |             | 0.00              | ) ft                  |
| Profile Description |             |                   |                       |
| Profile Headloss    |             | 0.00              | ) ft                  |
| Downstream Velocity |             | Infinity          | / ft/s                |
| Upstream Velocity   |             | Infinity          | / ft/s                |
| Normal Depth        |             | 0.57              | 'ft                   |
| Critical Depth      |             | 0.52              | <sup>2</sup> ft       |
| Channel Slope       |             | 0.00350           | ) ft/ft               |
| Critical Slope      |             | 0.00556           | 5 ft/ft               |

# **Cross Section for Fashion Square Drive - Section 9**

## **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

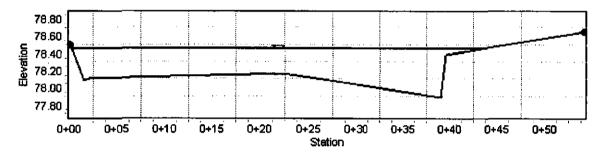
0.00350 ft/ft

Normal Depth

0.57 ft

Discharge

39.00 ft³/s



| Worksheet for Sco  | iccount Road Sc  | Julii or Cooling                   | <del>5 .10 4 5 5 5 5 1 5 1 5 1 5 1 5 1 5 1 5 1 5 1</del>   |
|--|--|------------------------------------|--|
| Project Description  |  |                                    |  |
| Friction Method  | Manning Formula  |                                    |  |
| Solve For  | Normal Depth   |                                    |  |
| Input Data   |  |                                    | The second secon |
| Channel Slope  |  | 0.00900 ft/ft                      | The second of th |
| Discharge  | •  | 119.00 ft³/s                       |  |
| Section Definitions  |  |                                    |  |
|  |  |                                    |  |
| •  |  | •                                  |  |
| Station (ft)   | Elevation  | on (ft)                            |  |
|  | 0+00   | 80.48                              |  |
| •  | 0+06   | 80.22                              |  |
|  | 0+06   | 79.61                              |  |
|  | 0+47   | 80.59                              |  |
|  |  |                                    |  |
| ,  | 0+48   | 81.09                              |  |
| Roughness Segment Definitions  | <b>0+48</b>  | 81.09                              | - · · · · · · · · · · · · · · · · · · ·  |
| Roughness Segment Definitions  Start Station   | 0+48 Ending 9  |                                    | Roughness Coefficient  |
|  | Ending \$  |                                    | Roughness Coefficient<br>0.016   |
| Start Station (0+00,   | Ending \$  | Station                            |  |
| Start Station (0+00,   | Ending \$  | Station                            |  |
| Start Station (0+00, 4) Options Current Roughness everginged Method  | Ending (<br>80.48)<br>Improved Lotter's Method                                     | Station                            |  |
| Start Station  (0+00, 6)  Options  Current Roughness evelgated Method Open Channel Weighting Method  | Ending (<br>80.48)<br>Improved Lotter's Method<br>Improved Lotter's Method         | Station                            |  |
| Options  Current Rougnness evergnted Method Open Channel Weighting Method Closed Channel Weighting Method  | Ending (<br>80.48)<br>Improved Lotter's Method                                     | Station                            |  |
| Start Station  (0+00, 6)  Options  Current Rougnness everginged Method Open Channel Weighting Method Closed Channel Weighting Method   | Ending (<br>80.48)<br>Improved Lotter's Method<br>Improved Lotter's Method         | Station<br>(0+48, 81.09)           |  |
| Options  Current Rougnness evergnted Method Open Channel Weighting Method Closed Channel Weighting Method  | Ending (<br>80.48)<br>Improved Lotter's Method<br>Improved Lotter's Method         | Station<br>(0+48, 81.09)           |  |
| Start Station  (0+00, 6)  Options  Current Rougnness everynted Method Open Channel Weighting Method Closed Channel Weighting Method Results  | Ending (<br>80.48)<br>Improved Lotter's Method<br>Improved Lotter's Method         | Station (0+48, 81.09)              |  |
| Start Station  (0+00, 4)  Options  Current Rougnness vveignted Method Open Channel Weighting Method Closed Channel Weighting Method Results  Normal Depth  | Ending 8 80.48)  Improved Lotter's Method Improved Lotter's Method Horton's Method | Station (0+48, 81.09)              |  |
| Start Station  (0+00, 4)  Options  Current Rougnness everginged Method Open Channel Weighting Method Closed Channel Weighting Method Results  Normal Depth Elevation Range   | Ending 8 80.48)  Improved Lotter's Method Improved Lotter's Method Horton's Method | O.99 ft                            |  |
| Start Station  (0+00, 6)  Options  Current Rougnness everynted Method Open Channel Weighting Method Closed Channel Weighting Method Results  Normal Depth Elevation Range Flow Area                                    | Ending 8 80.48)  Improved Lotter's Method Improved Lotter's Method Horton's Method | 0.99 ft                            |  |
| Start Station  (0+00, 4)  Options  Current Rougnness vveignted Method Open Channel Weighting Method Closed Channel Weighting Method Results  Normal Depth Elevation Range Flow Area Wetted Perimeter                   | Ending 8 80.48)  Improved Lotter's Method Improved Lotter's Method Horton's Method | 0.99 ft 22.32 ft² 47.45 ft         |  |
| Start Station  (0+00, 6)  Options  Current Rougnness everginted Method Open Channel Weighting Method Closed Channel Weighting Method Results  Normal Depth Elevation Range Flow Area Wetted Perimeter Hydraulic Radius | Ending 8 80.48)  Improved Lotter's Method Improved Lotter's Method Horton's Method | 0.99 ft 22.32 ft² 47.45 ft 0.47 ft |  |

# Worksheet for Scottsdale Road South of Coolidge Road-Section 10

| Results             |                                       |       |   |
|---------------------|---------------------------------------|-------|---|
| Critical Slope      | 0.00454                               | ft/ft |   |
| Velocity            | 5.33                                  | ft/s  |   |
| Velocity Head       | 0.44                                  | ft    |   |
| Specific Energy     | 1.43                                  | ft    |   |
| Froude Number       | 1.36                                  |       | • |
| Flow Type           | Supercritical                         |       |   |
| GVF Input Data      |                                       |       |   |
| Downstream Depth    | 0.00                                  | ft    | _ |
| Length              | 0.00                                  | ft    |   |
| Number Of Steps     | 0.00                                  | rt.   | • |
| Number Of Steps     | · · · · · · · · · · · · · · · · · · · |       |   |
| GVF Output Data     |                                       | -     |   |
| Upstream Depth      | 0.00                                  | ft    |   |
| Profile Description |                                       |       | • |
| Profile Headloss    | 0.00                                  | ft    |   |
| Downstream Velocity | Infinity                              | ft/s  |   |
| Upstream Velocity   | Infinity                              | ft/s  |   |
| Normal Depth        | 0.99                                  | ft    |   |
| Critical Depth      | 1.10                                  | ft    |   |
| Channel Slope       | 0.00900                               | ft/ft |   |
| Critical Slope      | 0.00454                               | ft/ft |   |
|                     | •                                     |       |   |

# Cross Section for Scottsdale Road South of Coolidge Road-Section 10

#### **Project Description**

Friction Method

Manning Formula

Solve For

**Normal Depth** 

Input Data

Channel Slope

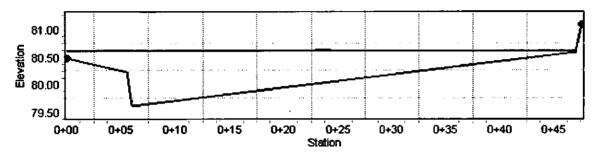
0.00900 ft/ft

Normal Depth

0.99 ft

Discharge

119.00 ft<sup>3</sup>/s



# Coolidge St. before Safari Dr. Development-Section 11

## Project Description

Friction Method

Manning Formula

Solve For

Normal Depth

#### මාමේ මෙන්

Channel Slope

0.00600 ft/ft

Discharge

29.00 ft<sup>3</sup>/s

Section Definitions

| g ar         |                |
|--------------|----------------|
| Stillon (fi) | Elevation (ii) |
| 0+00         | 80.76          |
| 0+11         | 80.39          |
| 0+27         | 80.21          |
| 0+41         | 80.22          |
| 0+42         | 80.48          |

#### Roughness Segment Definitions

| Sen Selion | (Bidling Steller) | Raginess Coeffeeni |
|------------|-------------------|--------------------|

(0+00, 80.76)

(0+42, 80.48)

0.016

#### Options

Current Rougnness vveignted Method

Improved Lotter's Method

Open Channel Weighting Method

Improved Lotter's Method

Closed Channel Weighting Method

Horton's Method

#### Rædle

| Normal Depth     | 0.35              | ft  |
|------------------|-------------------|-----|
| Elevation Range  | 80.21 to 80.76 ft |     |
| Flow Area        | 9.66              | ft² |
| Wetted Perimeter | 35.82             | ft  |
| Hydraulic Radius | 0.27              | ft  |
| Top Width        | 35.67             | ft  |
| Normal Depth     | 0.35              | ft  |
| Critical Depth   | 0.36              | ft  |

#### Coolidge St. before Safari Dr. Development-Section 11 Results 0.00578 Critical Slope 3.00 ft/s Velocity **Velocity Head** 0.14 Specific Energy 0.49 1.02 Froude Number Flow Type Supercritical **GVF Input Data Downstream Depth** 0.00 0.00 Length **Number Of Steps** 0 **GVF Output Data** Upstream Depth 0.00 **Profile Description Profile Headloss** 0.00 **Downstream Velocity** Infinity Infinity **Upstream Velocity** ft/s **Normal Depth** 0.35 0.36 Critical Depth Channel Slope 0.00600

0.00578

ft/ft

Critical Slope

# Coolidge St. before Safari Dr. Development-Section 11

## **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

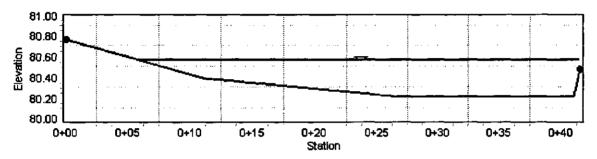
0.00600

**Normal Depth** 

0.35 ft

Discharge

29.00 ft³/s



## Scottsdale Rd North of Coolidge Rd-Section 13

| Scottsd                              | ale Rd North of                         | Coolidge F            | Rection 13  | <del></del>   |
|--------------------------------------|---|-----------------------|-------------|---|
| Project Description                  |   |                       |             |   |
| Friction Method                      | Manning Formula                         |                       |             |   |
| Solve For                            | Normal Depth                            |                       |             |   |
| Input Data                           |   |                       | ·           |   |
| Channel Slope                        |   | 0.00900 ft/ft         |             | INCLUDEDBUT   |
| Discharge                            |   | 70.00 ft³/s           |             | NOT USED  |
| Section Definitions                  |   |                       |             | NOT USED AS PART OF THE ANALYSIB DUE TO EXPLANATION IN THE RERORT |
| Station (ft)                         | Elevati                                 | ion (ft)              |             | M (the webel)   |
|                                      | 0+00                                    | 81                    | .51         | •   |
|                                      | 0+01                                    | . 81                  | .00         |   |
|                                      | 0+47                                    | 80                    | 0.00        |   |
|                                      | 0+48                                    | 80                    | 0.52        |   |
|                                      | 0+53                                    | 80                    | ).64        |   |
| Roughness Segment Definitions        |   |                       |             |   |
| Start Station                        | Ending                                  | Station               | Roughness 6 | Coefficient   |
| (0+00,                               | 81.51)                                  | (0+53, 80.            | .64)        | 0.016   |
| Options                              |   |                       |             |   |
| Current Rougnness vveignted          | Improved Lotter's Method                |                       |             |   |
| Method Open Channel Weighting Method | Improved Lotter's Method                |                       |             |   |
| Closed Channel Weighting Method      | Horton's Method                         |                       |             |   |
| Results                              |   |                       |             |   |
| Normal Depth                         |   | 0.78 ft               |             |   |
| Elevation Range                      | 80.00 to 81.51 ft                       | 5.75 <u>1,</u>        |             |   |
| Flow Area                            | *************************************** | 15.57 <del>ft</del> ² |             |   |
| Wetted Perimeter                     |   | 42.71 ft              |             |   |
| Hydraulic Radius                     |   | 0.36 ft               |             |   |
|                                      |   |                       |             |   |

42.34 ft

0.78 ft

0.86 ft

Top Width

Normal Depth

**Critical Depth** 

# Scottsdale Rd North of Coolidge Rd-Section 13

| Results             |   |   |
|---------------------|---|---|
| Critical Slope      | 0.0050                                  | 07 ft/ft                                |
| Velocity            | 4.5                                     | 50 ft/s                                 |
| Velocity Head       | 0.3                                     | 31 ft                                   |
| Specific Energy     | 1.1                                     | 10 ft                                   |
| Froude Number       | 1.3                                     | 31                                      |
| Flow Type           | Supercritical                           |   |
| GVF Input Data      |   |   |
| Downstream Depth    | 0.0                                     | 00 ft                                   |
| Length              | 0.0                                     | ••                                      |
| Number Of Steps     |   | 0                                       |
| GVF Output Data     |   | · · · · · · · · · · · · · · · · · · ·   |
| OAL Onthat pare     | - · · · · · · · · · · · · · · · · · · · | - · · · · · · · · · · · · · · · · · · · |
| Upstream Depth      | 0.0                                     | 00 ft                                   |
| Profile Description |   | •                                       |
| Profile Headloss    | 0.0                                     | 00 ft                                   |
| Downstream Velocity | Infini                                  | ity ft/s                                |
| Upstream Velocity   | Infini                                  | ity ft/s                                |
| Normal Depth        | 0.7                                     | 78 ft                                   |
| Critical Depth      | . O.8                                   | 86 ft                                   |
| Channel Slope       | 0.0090                                  | 00 ft/ft                                |
| Critical Slope      | 0.0050                                  | 07 ft/ft                                |

#### Scottsdale Rd North of Coolidge Rd-Section 13

#### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

**Channel Slope** 

0.00900 ft/ft

Normal Depth

0.78 ft

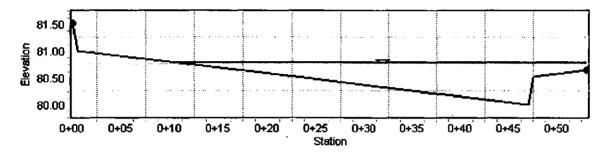
**D**:---

0.70 10

Discharge

70.00 ft³/s

#### **Cross Section Image**



#### Half St. Scottsdale Rd North of Fashion Sq Dr-Section 14

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

Discharge

0.00800 52.00

ft³/s

Section Definitions

NOT USED AS PART

OF THE ANALYSIS

DUE TO EXPLANATION IN THE REPORT

Station (ft)

Elevation (ft)

| 0+00 | 79.22 |
|------|-------|
| 0+01 | 78.79 |
| 0+38 | 77.87 |
| 0+39 | 78.28 |
| 0+44 | 78.48 |

**Roughness Segment Definitions** 

Start Station

**Ending Station** 

Roughness Coefficient

(0+00, 79.22)

(0+44, 78.48)

0.016

**Options** 

Current Rougnness vveignted

Method

Improved Lotter's Method
Improved Lotter's Method

Open Channel Weighting Method
Closed Channel Weighting Method

Horton's Method

Results

| Normal Depth     |                   | 0.74  | ft  |
|------------------|-------------------|-------|-----|
| Elevation Range  | 77.87 to 79.22 ft |       |     |
| Flow Area        |                   | 12.66 | ft² |
| Wetted Perimeter |                   | 36.42 | ft  |
| Hydraulic Radius |                   | 0.35  | ft  |
| Top Width        |                   | 36.13 | ft  |
| Normal Depth     |                   | 0.74  | ft  |
| Critical Depth   |                   | 0.80  | ft  |

#### Half St. Scottsdale Rd North of Fashion Sq Dr-Section 14

| Results             |                                       |        | :     |  |
|---------------------|---------------------------------------|--------|-------|--|
| Critical Slope      | 0.00                                  | 519    | ft/ft |  |
| Velocity            | 4                                     | .11    | ft/s  |  |
| Velocity Head       | C                                     | .26    | ft    | •  |
| Specific Energy     | 1                                     | .00    | ft    | •  |
| Froude Number       | 1                                     | .22    |       |  |
| Flow Type           | Supercritical                         |        |       | ·  |
| GVF Input Data      |                                       |        |       | and the second of the second o |
| OTT Input Data      | · · · · · · · · · · · · · · · · · · · |        | -     |  |
| Downstream Depth    | C                                     | .00    | ft    |  |
| Length              | C                                     | .00    | ft    |  |
| Number Of Steps     |                                       | 0      |       |  |
| GVF Output Data     |                                       |        | _     |  |
| Upstream Depth      | C                                     | .00    | ft    |  |
| Profile Description |                                       |        |       |  |
| Profile Headloss    | C                                     | .00 (  | ft    |  |
| Downstream Velocity | Inf                                   | nity 1 | ft/s  |  |
| Upstream Velocity   | Infi                                  | nity ( | ft/s  |  |
| Normal Depth        | C                                     | .74 1  | ft    |  |
| Critical Depth      | c                                     | .80 1  | ft    |  |
| Channel Slope       | 0.00                                  | 300 1  | ft/ft | •  |
| Critical Slope      | 0.00                                  | 519 1  | ft/ft |  |

#### Half St. Scottsdale Rd North of Fashion Sq Dr-Section 14

#### **Project Description**

Friction Method

Manning Formula

Solve For

Normal Depth

Input Data

Channel Slope

0.00800 ft/ft

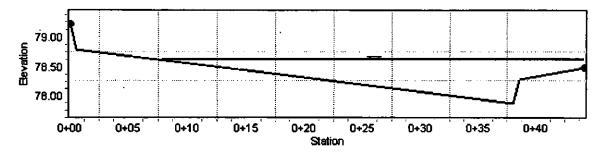
Normal Depth

0.74 ft

Discharge

52.00 ft³/s

#### **Cross Section Image**



#### AZ Canal Weir Analysis, Refer to Exhibit C located under Appendix A

#### Component:Weir

| Hydraulic Component(s): Roadwa | у            |                         |          |
|--------------------------------|--------------|-------------------------|----------|
| Discharge                      | 1,202.00 cfs | Allowable HW Elevation  | 79.50 ft |
| Roadway Width                  | 12.00 ft     | Overtopping Coefficient | 2.99 US  |
| Low Point                      | 77.52 ft     | Headwater Elevation     | 79.50 ft |
| Discharge Coefficient (Cr)     | 2.99         | Submergence Factor (Kt) | 1.00     |
| Tailwater Elevation            | 0.00 ft      |                         |          |

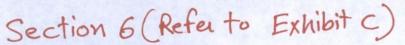
| SECTION STATES |            |
|----------------|------------|
| Sta (ft)       | Elev. (ft) |
| -200.00        | 79.00      |
| 0.00           | 79.56      |
| 30.00          | 79.59      |
| 56.00          | 79.38      |
| 109.00         | 79.64      |
| 190.00         | 79.68      |
| 245.00         | 79.72      |
| 303.00         | 79.74      |
| 386.00         | 79.95      |
| 517.00         | 79.58      |
| 661.00         | 79.47      |
| 693.00         | 79.45      |
| 735.00         | 79.69      |
| 802.00         | 79.46      |
| 831.00         | 79.43      |
| 856.00         | 79.39      |
| 955.00         | 79.21      |
| 1,030.00       | 79.34      |
| 1,097.00       | 79.42      |
| 1,146.00       | 79.29      |
| 1,196.00       | 79.25      |
| 1,304.00       | 79.69      |
| 1,330.00       | 80.36      |
| 1,364.00       | 79.69      |
| 1,388.00       | 78.56      |
| 1,467.00       | 79.08      |
| 1,494.00       | 78.53      |
| 1,532.00       | 79.17      |
| 1,532.50       | 79.59      |
| 1,536.00       | 79.66      |
| 1,536.50       | 79.22      |
| 1,561.00       | 79.03      |
| 1,561.50       | 79.53      |
| 1,615.50       | 78.95      |
| 1,616.00       | 78.43      |
| 1,658.00       | 78.32      |
| 1,710.00       | 77.52      |
| 1,710.50       | 77.96      |
| 1,735.00       | 77.72      |
| 1,751.00       | 77.61      |
| 1,752.00       | 80.18      |
| 1,752.50       | 79.67      |
| 1,773.50       | 79.74      |
| 1,794.50       | 79.58      |

The Weir elevations are based on the survey points taken in the field

80.00

1,795.00

| Sta (ft) | Elev. (ft) |
|----------|------------|
| 1,862.50 | 79.46      |



| Analysis Compone                             | ent                               |               |     |                 |          |           |
|--|-----------------------------------|---------------|-----|-----------------|----------|-----------|
| Storm Event                                  |                                   | Design        |     | Discharge       |          | 75.00 cfs |
| Peak Discharge M                             | ethod: User-Specified             |               |     |                 |          |           |
| Design Discharge                             |                                   | 75.00         | cfs | Check Discharge |          | 75.00 cfs |
| Tailwater propertie                          | es: Irregular Channel             | V ON A        |     |                 |          |           |
|  |                                   |               |     |                 |          |           |
| Tailwater condition                          | ns for Design Storm.              |               |     |                 |          |           |
| Tailwater condition<br>Discharge<br>Velocity | ns for Design Storm.              | 75.00<br>0.00 |     | Actual Depth    |          | 0.00 ft   |
| Discharge                                    | ns for Design Storm.  Description |               |     |                 | Velocity | 0.00 ft   |

| Analysis Compon       | ent                    |               |           |                 |          |           |
|-----------------------|------------------------|---------------|-----------|-----------------|----------|-----------|
| Storm Event           |                        | Design        |           | Discharge       |          | 75.00 cfs |
| Peak Discharge I      | Method: User-Specified | :             |           |                 |          | ,         |
| Design Discharg       | 8                      | 75.00         | cfs       | Check Discharge |          | 75.00 cfs |
| Tailwater propert     | es: Irregular Channel  |               | _         |                 |          |           |
| Tailwater condition   | ns for Design Storm.   |               |           |                 |          |           |
| Discharge<br>Velocity |                        | 75.00<br>0.00 |           | Actual Depth    |          | 0.00 ft   |
| Name                  | Description            |               | Discharge | e HW Elev.      | Velocity |           |
| Weir                  | Roadway                | _             | 75.00     | cfs 78.50 ft    | N/A      | -         |

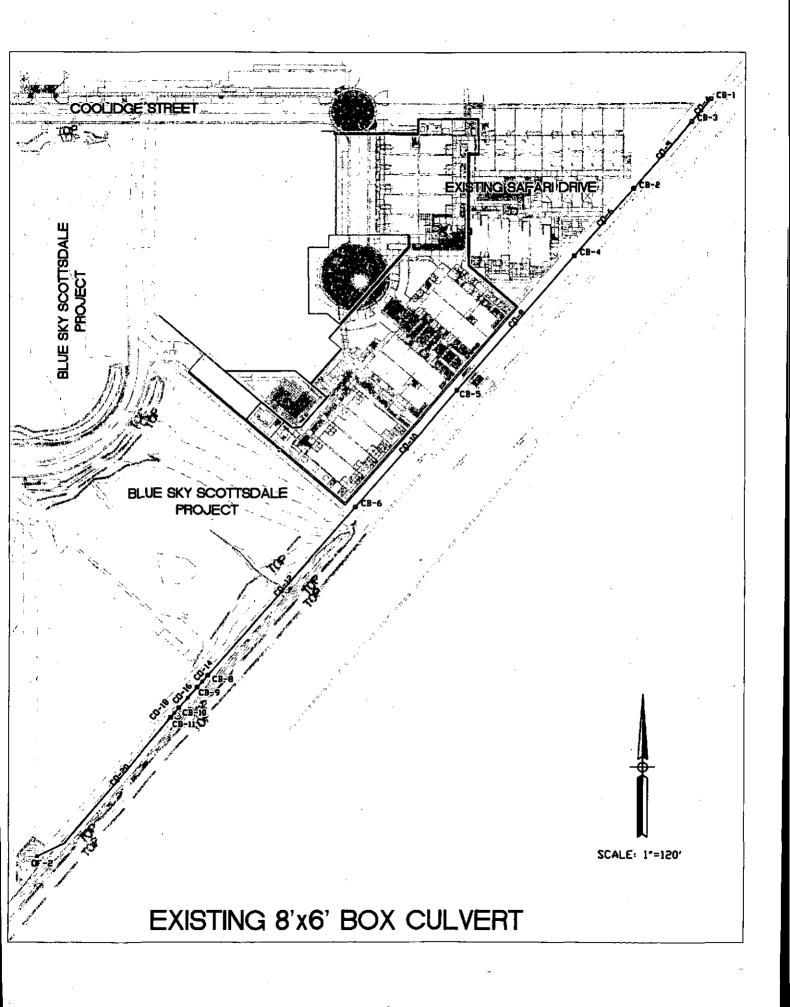
#### Component:Weir

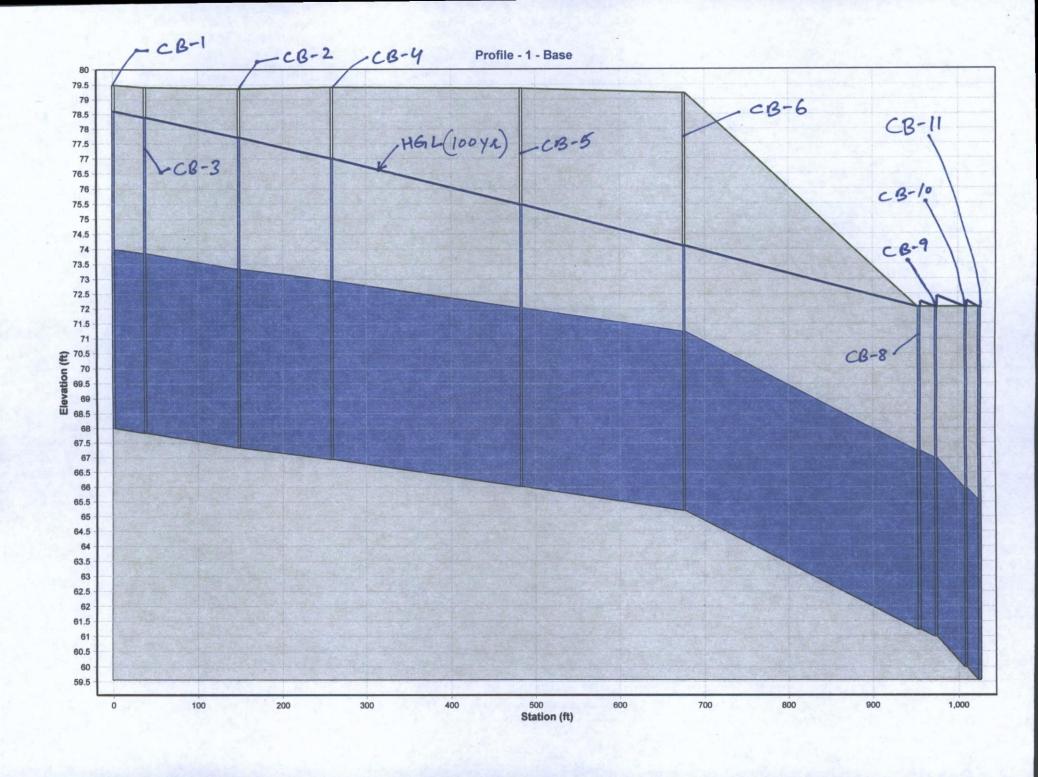
| Hydraulic Component(s): Roadway |           |                         |          |
|---------------------------------|-----------|-------------------------|----------|
| Discharge                       | 75.00 cfs | Allowable HW Elevation  | 78.50 ft |
| Roadway Width                   | 12.00 ft  | Overtopping Coefficient | 2.99 US  |
| Low Point                       | 77.52 ft  | Headwater Elevation     | 78.50 ft |
| Discharge Coefficient (Cr)      | 2.99      | Submergence Factor (Kt) | 1.00     |
| Tailwater Elevation             | 0.00 ft   | - • •                   | *        |

| Sta (ft) | Elev. (ft) |
|----------|------------|
| 1,615.50 | 1,278.95   |
| 1,616.00 | 78.43      |
| 1,658.00 | 78.32      |
| 1,710.00 | 77.52      |
| 1,710.50 | 77.96      |

Retention Volume Calculations for Excavated Basin Existing 8'x6' Box Culvert Capacity StormCAD Model Existing Strom Drain system on Coolidge StormCAD Model (Refer to Exhibit F for Drainage Area)

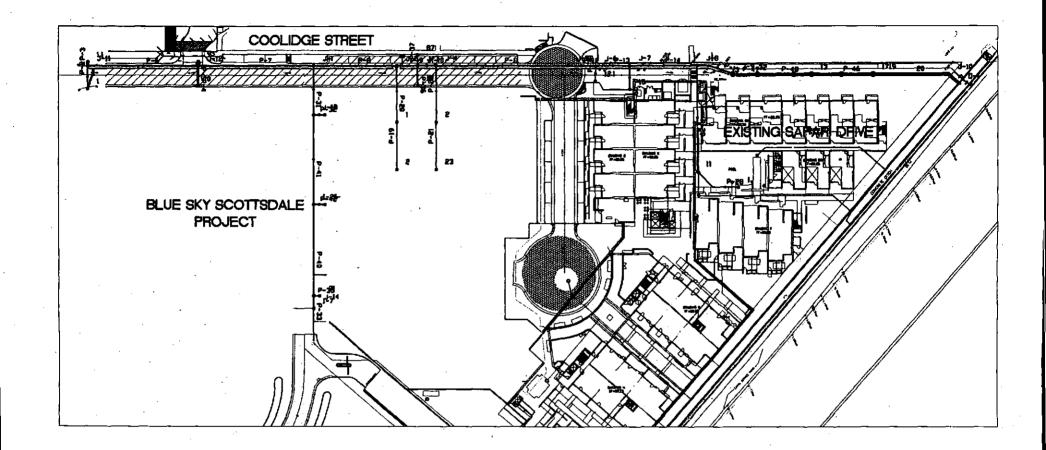
|  |  | •   |                 |  |  |   |  |
|--|--|---|-----------------|--|--|---|--|
| Contributing Drainage Areas<br>Retention Basin(s): | s: 1                                     |   |                 | -                                      | -  |   |  |
| OLUME REQUIRED CALCU                               | ILATIONS                                 |   |                 |  |  |   |  |
|  | Area                                     |   | 'C' Coefficient | Precipitation                          | Reten  | tion Re                                 | quired   |
| Туре   | (ft)                                     | (Ac)  | С               | (Inches)                               | (ft³)  |   | (Ac-ft   |
| Landscaped   | 108,246                                  | 2.48  | 0.50            | 2.20                                   | 9,923  |   | 0.2  |
| Total  | 108,246                                  | 2.48  |                 | •                                      | 9,923  | •                                       | 0.2  |
|  |  |   |                 |  |  |   |  |
| PETENTION BASIN CALCUI                             | ATIONS                                   |   | •               |  |  |   |  |
| RETENTION BASIN CALCUL                             |  | urface Area                                   | ·<br>a          | Vol                                    | lume Pro   | vided                                   |  |
| <del>-</del>                                       | Delta Depth                              | urface Area                                   | a               | Vol                                    | lume Pro<br>Σ (ft³)  |   | Σ (Ac-fi   |
| ·  |  |   | a               |  |  | (Ac-ft)                                 |  |
| Elevation  | Delta Depth<br>(ft)                      | (ft²)   | a               | (ft³)                                  | $\Sigma$ (ft <sup>3</sup> )                                  | (Ac-ft)<br>1.18                         | 4.0  |
| Elevation<br>1277.0                                | Delta Depth<br>(ft)                      | (ft²)<br>54,300                               | a               | (ft <sup>3</sup> )<br>51,528           | Σ (ft <sup>3</sup> )<br>174,608                              | (Ac-ft)<br>1.18                         | 4.0<br>2.8   |
| Elevation<br>1277.0<br>1276.0                      | Delta Depth<br>(ft)<br>1.0<br>1.0        | (ft²)<br>54,300<br>48,805<br>43,511           | a               | (ft <sup>3</sup> )<br>51,528<br>46,133 | Σ (ft <sup>3</sup> )<br>174,608<br>123,080                   | (Ac-ft)<br>1.18<br>1.06<br>0.94         | 4.0<br>2.8<br>1.7  |
| Elevation<br>1277.0<br>1276.0<br>1275.0            | Delta Depth<br>(ft)<br>1.0<br>1.0<br>1.0 | (ft²)<br>54,300<br>48,805<br>43,511           | a               | (ft³)<br>51,528<br>46,133<br>40,951    | Σ (ft³)<br>174,608<br>123,080<br>76,947                      | (Ac-ft)<br>1.18<br>1.06<br>0.94<br>0.83 | 4.0<br>2.8<br>1.7<br>0.8   |
| 1277.0<br>1276.0<br>1275.0<br>1274.0               | Delta Depth<br>(ft)<br>1.0<br>1.0<br>1.0 | (ft²)<br>54,300<br>48,805<br>43,511<br>38,444 | Provided        | (ft³)<br>51,528<br>46,133<br>40,951    | Σ (ft³)<br>174,608<br>123,080<br>76,947<br>35,996            | (Ac-ft)<br>1.18<br>1.06<br>0.94<br>0.83 | 4.0<br>2.8<br>1.7<br>0.8<br>4.0                                  |
| 1277.0<br>1276.0<br>1275.0<br>1274.0               | Delta Depth<br>(ft)<br>1.0<br>1.0<br>1.0 | (ft²)<br>54,300<br>48,805<br>43,511<br>38,444 |                 | (ft³)<br>51,528<br>46,133<br>40,951    | Σ (ft³)<br>174,608<br>123,080<br>76,947<br>35,996<br>174,608 | (Ac-ft)<br>1.18<br>1.06<br>0.94<br>0.83 | 4.0<br>2.8<br>1.7<br>0.8<br>4.0                                  |
| 1277.0<br>1276.0<br>1275.0<br>1274.0               | Delta Depth<br>(ft)<br>1.0<br>1.0<br>1.0 | (ft²)<br>54,300<br>48,805<br>43,511<br>38,444 | Provided        | (ft³)<br>51,528<br>46,133<br>40,951    | Σ (ft³)<br>174,608<br>123,080<br>76,947<br>35,996<br>174,608 | (Ac-ft)<br>1.18<br>1.06<br>0.94<br>0.83 | Σ (Ac-fi<br>4.0<br>2.8<br>1.7<br>0.8<br>4.0<br>4.0<br>0.2<br>3.7 |

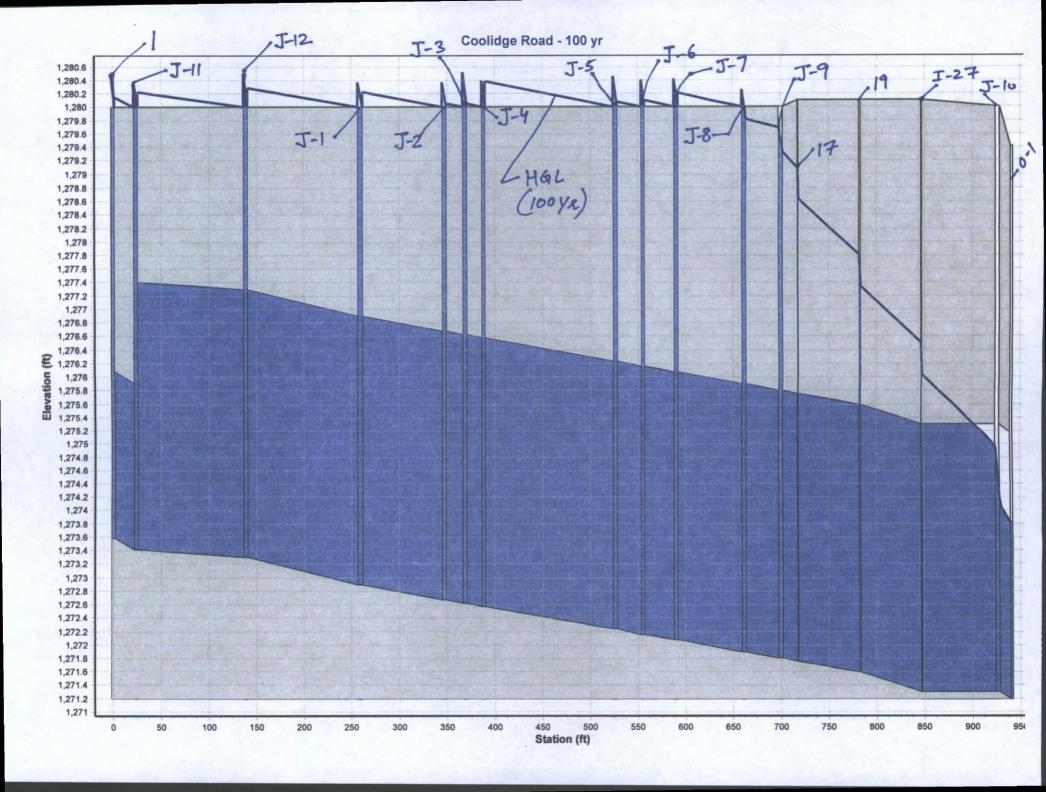




### FlexTable: Conduit Table (8'x6' Box Culvert.stc)

| Label | Start Node | Invert<br>(Upstream)<br>(ft) | Stop Node | Invert<br>(Downstream)<br>(ft) | Manning's n | Flow<br>(ft³/s) | Length<br>(Unified)<br>(ft) | Slope<br>(Calculated)<br>(ft/ft) | Elevation<br>Ground<br>(Start)<br>(ft) | Elevation<br>Ground<br>(Stop)<br>(ft) | Hydraulic Grade<br>Line (In)<br>(ft) | Hydraulic Grade<br>Line (Out)<br>(ft) | Velocity<br>(Average)<br>(ft/s) | System Fixed<br>Flow<br>(ft³/s) |
|-------|------------|------------------------------|-----------|--------------------------------|-------------|-----------------|-----------------------------|----------------------------------|--|---------------------------------------|--------------------------------------|---------------------------------------|---------------------------------|---------------------------------|
| CO-4  | CB-1       | 68.00                        | CB-3      | 67.85                          | 0.013       | 600.00          | 37.0                        | 0.004                            | 79.50                                  | 79.40                                 | 78.59                                | 78.37                                 | 12.50                           | 600.00                          |
| CO-5  | CB-3       | 67.85                        | CB-2      | 67.35                          | 0.013       | 615.00          | 111.0                       | 0.005                            | 79.40                                  | 79.35                                 | 78.37                                | 77.69                                 | 12.81                           | 615.00                          |
| CO-6  | CB-2       | 67.35                        | CB-4      | 66.94                          | 0.013       | 630.00          | 111.0                       | 0.004                            | 79.35                                  | 79.40                                 | 77.69                                | 76.98                                 | 13.13                           | 630.00                          |
| CO-8  | CB-4       | 66.94                        | CB-5      | 66.02                          | 0.013       | 645.00          | 224.0                       | 0.004                            | 79.40                                  | <i>7</i> 9.35                         | 76.98                                | 75.47                                 | 13.44                           | 645.00                          |
| CO-10 | CB-5       | 66.02                        | CB-6      | 65.23                          | 0.013       | 660.00          | 193.0                       | 0.004                            | 79.35                                  | 79.20                                 | 75.47                                | 74.11                                 | 13.75                           | 660.00                          |
| CO-12 | CB-6       | 65.23                        | CB-8      | 61.24                          | 0.013       | 675.00          | 278.0                       | 0.014                            | 79.20                                  | 72.06                                 | 74.11                                | 72.06                                 | 14.06                           | 675.00                          |
| CO-14 | CB-8       | 61.24                        | CB-9      | 61.00                          | 0.013       | 733.00          | 20.0                        | 0.012                            | 72.06                                  | 72.06                                 | 72.23                                | 72.06                                 | 15.27                           | 733.00                          |
| CO-16 | CB-9       | 61.00                        | CB-10     | 59.99                          | 0.013       | 792.00          | 35.0                        | 0.029                            | 72.06                                  | 72.05                                 | 72.41                                | 72.05                                 | 16.50                           | 792.00                          |
| CO-18 | CB-10      | 59.9 <del>9</del>            | CB-11     | 59.58                          | 0.013       | 896.00          | 16.0                        | 0.026                            | 72.05                                  | 72.05                                 | 72.25                                | 72.05                                 | 18.67                           | 896.00                          |
| CO-20 | CB-11      | <u>59.58</u>                 | OF-2      | 53.00                          | 0.013       | 1,000.00        | 242.0                       | 0.027                            | 72.05                                  | 72.50                                 | 78.92                                | 75.00                                 | 20.83                           | 1,000.00                        |





#### Title: FlexTable: Conduit Table (Coolidge Storm Drain.stc)

| Label | Start Node | Invert<br>(Upstream)<br>(ft) | Stop Node       | Invert<br>(Downstream)<br>(ft) | Manning's n | Diameter<br>(in) | Flow<br>(ft³/s)    | Length<br>(Unified)<br>(ft) | Slope<br>(Calculated)<br>(ft/ft) | Elevation<br>Ground<br>(Start)<br>(ft) | Elevation<br>Ground<br>(Stop)<br>(ft) | Hydraulic Grade<br>Line (In)<br>(ft) | Hydraulic Grade<br>Line (Out)<br>(ft) | Velocity<br>(Average)<br>(ft/s) | System Fixed<br>Flow<br>(ft³/s) |
|-------|------------|------------------------------|-----------------|--------------------------------|-------------|------------------|--------------------|-----------------------------|----------------------------------|--|---------------------------------------|--------------------------------------|---------------------------------------|---------------------------------|---------------------------------|
| P-17  | J-10       | •                            | 0-1             | 1,271.19                       | 0.012       | 48.0             | 89.00              | 15.0                        | 0.008                            | 1,280.00                               | 1,279.41                              | 1,274.17                             | 1,273.82                              | 11.75                           | 89.00                           |
| 20    | 1-27       | 1,271.31                     |                 | 1,271.31                       | 0.024       | 48.0             | 89.00              | 79.0                        | 0.000                            | 1,280.10                               | 1,280.00                              | 1,276.04                             | 1,274.97                              | 7.08                            | 89.00                           |
| P-46  | 19         | 1,271.60                     |                 | 1,271.31                       | 0.024       | 48.0             | 8 <del>9</del> .00 | 64.0                        | 0.005                            | 1,280.10                               | 1,280.10                              | 1,277.34                             | 1,276.50                              | 7.08                            | 89.00                           |
| P-4   | 3          | 1,273.65                     |                 | 1,273.30                       | 0.012       | 18.0             | 5.00               | 21.0                        | 0.017                            | 1,280.06                               | 1,280.00                              | 1,280.04                             | 1,280.00                              | 2.83                            | 5.00                            |
| P-5   | 2          | 1,273.23                     |                 | 1,273.30                       | 0.012       | 18.0             | 1,00               | 3.0                         | -0.023                           | 1,279.99                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.57                            | 1.00                            |
| P-7   | J-12       | 1,273.30                     | J-1             | 1,272.90                       | 0.012       | 48.0             | 76.00              | 121.0                       | 0.003                            | 1,280.00                               | 1,280.00                              | 1,280.29                             | 1,280.00                              | 6.05                            | 76.00                           |
| P-8   | J-1        | 1,272.90                     |                 | 1,272.68                       | 0.012       | 48.0             | 80.00              | 88.0                        | 0.003                            | 1,280.00                               | 1,280.00                              | 1,280.23                             | 1,280.00                              | 6.37                            | 80.00                           |
| P-9   | J-2        | 1,272.68                     |                 | 1,272.63                       | 0.012       | 48.0             | 80.00              | 22.0                        | 0.002                            | 1,280.00                               | 1,280.00                              | 1,280.06                             | 1,280.00                              | 6.37                            | 80.00                           |
| P-10  | J-3        | 1,272.63                     |                 | 1,272.58                       | 0.012       | 48.0             | 82.00              | 19.0                        | 0.003                            | 1,280.00                               | 1,280.00                              | 1,280.05                             | 1,280.00                              | 6.53                            | 82.00                           |
| P-11  | J-4        | 1,272.58                     | J-5             | 1,272.24                       | 0.012       | 48.0             | 82.00              | 138.0                       | 0.002                            | 1,280.00                               | 1,280.00                              | 1,280.38                             | 1,280.00                              | 6.53                            | 82.00                           |
| P-12  | J-5        | 1,272.24                     |                 | 1,272.16                       | 0.012       | 48.0             | 82.00              | 29.0                        | 0.003                            | 1,280.00                               | 1,280.00                              | 1,280.08                             | 1,280.00                              | 6.53                            | 82.00                           |
| P-13  | J-6        | 1,272.16                     |                 | 1,272.08                       | 0.012       | 48.0             | 83.00              | 35.0                        | 0.002                            | 1,280.00                               | 1,280.00                              | 1,280.10                             | 1,280.00                              | 6.60                            | 83.00                           |
| P-14  | 3-7        | 1,272.08                     |                 | 1,271.90                       | 0.012       | 48.0             | 85.00              | 71.0                        | 0.003                            | 1,280.00                               | 1,280.00                              | 1,280.21                             | 1,280.00                              | 6.76                            | 85.00                           |
| P-15  | J-8        | 1,271.90                     | J-9             | 1,271.81                       | 0.012       | 48.0             | 87.00              | 39.0                        | 0.002                            | 1,280.00                               | 1,280.00                              | 1,279.82                             | 1,279.70                              | 6.92                            | 87.00                           |
| P-19  | 8          | 1,273.20                     | 7               | 1,272.96                       | 0.012       | 18.0             | 0.00               | 49.0                        | 0.005                            | 1,280.55                               | 1,280.55                              | 1,280.00                             | 1,280.00                              | 0.00                            | 0.00                            |
| P-20  | ] 7        | 1,272.96                     |                 | 1,272.68                       | 0.012       | 18.0             | 0.00               | 58.0                        | 0.005                            | 1,280.55                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.00                            | 0.00                            |
| P-21  | 10         | 1,273.82                     |                 | 1,273.58                       | 0.012       | 18.0             | 0.00               | 49.0                        | 0.005                            | 1,280.55                               | 1,280.55                              | 1,280.00                             | 1,280.00                              | 0.00                            | 0.00                            |
| P-22  | 9          | 1,273.58                     | J <del>-4</del> | 1,272.58                       | 0.012       | 18.0             | 0.00               | 59.0                        | 0.017                            | 1,280.55                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.00                            | 0.00                            |
| P-28  | 23         | 1,273. <del>94</del>         | 22              | 1,273.69                       | 0.012       | 18.0             | 1.00               | 50.0                        | 0.005                            | 1,280.45                               | 1,280.45                              | 1,280.06                             | 1,280.06                              | 0.57                            | 1.00                            |
| P-29  | 22         | 1,273. <del>6</del> 9        |                 | 1,273.15                       | 0.012       | 18.0             | 2.00               | 109.0                       | 0.005                            | 1,280.45                               | 1,280.00                              | 1,280.03                             | 1,280.00                              | 1.13                            | 2.00                            |
| P-2   | 1          | 1,273.59                     | J-11            | 1,273.41                       | 0.012       | 30.0             | 35.00              | 24.0                        | 0.007                            | 1,280.00                               | 1,280.00                              | 1,280.15                             | 1,280.00                              | 7.13                            | 35.00                           |
| P-3   | 1.1        | 1,273.53                     | J-11            | 1,273.41                       | 0.012       | 30.0             | 35.00              | 3.0                         | 0.040                            | 1,280.00                               | 1,280.00                              | 1,280.02                             | 1,280.00                              | 7.13                            | 35.00                           |
| P-6   | J-11       | 1,273.41                     |                 | 1,273.30                       | 0.012       | 48.0             | 70.00              | 114.0                       | 0.001                            | 1,280.00                               | 1,280.00                              | 1,280.23                             | 1,280.00                              | 5.57                            | 70.00                           |
| P-31  | J-13       | 1,273.24                     | J-1             | 1,272.90                       | 0.012       | 18.0             | 4.00               | 51.0                        | 0.007                            | 1,280.00                               | 1,280.00                              | 1,280.06                             | 1,280.00                              | 2.26                            | 4.00                            |
| P-32  | 6          | 1,273.30                     | J-13            | 1,273.24                       | 0.012       | 18.0             | 3.00               | 12.0                        | 0.005                            | 1,280.00                               | 1,280.00                              | 1,280.01                             | 1,280.00                              | 1.70                            | 3.00                            |
| P-36  | 12         | 1,273.27                     |                 | 1,273.17                       | 0.012       | 18.0             | 1.00               | 21.0                        | 0.005                            | 1,279.41                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.57                            | 1.00                            |
| P-37  | 13         | 1,273.22                     | J-3             | 1,273.17                       | 0.012       | 18.0             | 1.00               | 11.0                        | 0.005                            | 1,279.70                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.57                            | 1.00                            |
| P-38  | 12.1       | 1,274.36                     | J-6             | 1,274.27                       | 0.012       | 18.0             | 1.00               | 16.0                        | 0.006                            | 1,279.78                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.57                            | 1.00                            |
| P-39  | 15         | 1,274.57                     | J-7             | 1,274.45                       | 0.012       | 18.0             | 2.00               | 25.0                        | 0.005                            | 1,280.13                               | 1,280.00                              | 1,280.01                             | 1,280.00                              | 1.13                            | 2.00                            |
| P-33  | I-7        | 1,274.20                     | J-14            | 1,274.18                       | 0.012       | 18.0             | 0.00               | 13.0                        | 0.002                            | 1,279.01                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.00                            | 0.00                            |
| P-35  | 31         | 1,274.27                     | J-14            | 1,274.18                       | 0.012       | 18.0             | 0.00               | 6.0                         | 0.015                            | 1,279.80                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.00                            | 0.00                            |
| P-40  | J-14       | 1,274.18                     | I-26            | 1,273.70                       | 0.012       | 18.0             | 0.00               | 94.0                        | 0.005                            | 1,280.00                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.00                            | 0.00                            |
| P-41  | I-26       | 1,273.70                     | J-13            | 1,273.24                       | 0.012       | 18.0             | 1.00               | 92.0                        | 0.005                            | 1,280.00                               | 1,280.00                              | 1,280.01                             | 1,280.00                              | 0.57                            | 1.00                            |
| P-42  | 11         | 1,273.76                     | I-26            | 1,273.70                       | 0.012       | 18.0             | 1.00               | 12.0                        | 0.005                            | 1,280.25                               | 1,280.00                              | 1,280.00                             | 1,280.00                              | 0.57                            | 1.00                            |
| P-47  | J-9        | 1,271.81                     | 17              | 1,271.76                       | 0.024       | 48.0             | 87.00              | 18.0                        | 0.003                            | 1,280.00                               | 1,280.10                              | 1,279.32                             | 1,279.10                              | 6.92                            | 87.00                           |
| P-48  | 17         | 1,271.76                     | 19              | 1,271.60                       | 0.024       | 48.0             | 88.00              | 65.0                        | 0.002                            | 1,280.10                               | 1,280.10                              | 1,278.64                             | 1,277.81                              | 7.00                            | 88.00                           |

**Grated Inlet Structures Hydraulic Capacity Calculations** 

# Capacity of a catch basin in a Sag operating as an Orifice $Q = C A (2gd)^0.50$

C = 0.67 Orifice Coefficient, g=32.2 ft/s<sup>2</sup>

Capacity of Existing Catch basin along the Canal that will beremoved and replaced with 2-4'x4' catch basins

| 1st New Catch Basin along Canal |
|---------------------------------|
| 79.5                            |
| 73                              |
| 6.5                             |
| 3                               |
| of the inlet 1.5 sq. ft.        |
| on the inlet 6.5 ft.            |
| of the inlet = 21 cfs           |
|                                 |

Refer to Exhibit A, Fill Plans for the Location of this Catch Basin

# Capacity of a catch basin in a Sag operating as an Orifice $Q = C A (2gd)^0.50$

C = 0.67 Orifice Coefficient, g=32.2 ft/s<sup>2</sup>

Capacity of New 2-4'x4' Catch basins that will be added to along the Canal to to replace existing catch basin and to compensate for filling in the flood plain.

Based on HWE of 79.50'

| Concentration Point    | 1st New Catch Basin along Canal to replace existing catch basin |
|------------------------|---|
| High Water at Weir=    | 79.5  |
| Rim of Catch Basin=    | 72.85   |
| Head on Rim=           | 6.65  |
| Total Area of Grate=   | 16  |
| 50% of Open area       | of the inlet 8 sq. ft.  |
| Depth of water ponding | on the inlet 6.65 ft.   |
| Capacity of            | of the inlet = 111 cfs  |

| Concentration Point    | 2nd New Catch Basin along Canal to compensate |
|------------------------|---|
|                        | for filling in the flood plain                |
| High Water at Weir=    | 79.5  |
| Rim of Catch Basin=    | 72.57   |
| Head on Rim=           | 6.93  |
| Total Area of Grate=   | 16  |
| 50% of Open area       | of the inlet 8 sq. ft.                        |
| Depth of water ponding | on the inlet 6.93 ft.                         |
| Capacity of            | of the inlet = 113 cfs                        |

Refer to Exhibit A, Fill Plans for the Location of these Catch Basins

# Capacity of a catch basin in a Sag operating as an Orifice $Q = C A (2gd)^0.50$

C = 0.67 Orifice Coefficient, g=32.2 ft/s<sup>2</sup>

#### Refer to Exhibit C for the location of below Catch Basins along Camelback Road

Based on HWE of 79.50'

| Concentration Point                        | <b>East Catch Basin</b> |                         |
|--|-------------------------|-------------------------|
| High Water at Weir=                        | 79.5                    |                         |
| Rim of Catch Basin=                        | 76.6                    |                         |
| Head on Rim=                               | 2.9                     |                         |
| Total Area of Grate=                       | 19.68                   |                         |
| 50% of Open area<br>Depth of water ponding |                         | 9.84 sq. ft.<br>2.9 ft. |
| Capacity of                                | of the inlet =          | 90 cfs                  |

| Concentration Point                        | Middle Catch Basin    |
|--|-----------------------|
| High Water at Weir=                        | 79.5                  |
| Rim of Catch Basin=                        | 76.73                 |
| Head on Rim=                               | 2.77                  |
| Total Area of Grate=                       | 19.68                 |
| 50% of Open area<br>Depth of water ponding |                       |
| Capacity of                                | of the inlet = 88 cfs |

| Concentration Point    | West Catch Basin          |
|------------------------|---------------------------|
| High Water at Weir=    | 79.5                      |
| Rim of Catch Basin=    | 75.15                     |
| Head on Rim=           | 4.35                      |
| Total Area of Grate=   | 19.68                     |
| 50% of Open area       | of the inlet 9.84 sq. ft. |
| Depth of water ponding | on the inlet 4.35 ft.     |
|                        |                           |
| Capacity or            | f the inlet = 110 cfs     |
|                        |                           |

# APPENDIX E CORRESPONDENCE, WAIVERS AND SUPPORTING DOCUMENTS



| PA  | ZN   | City of Scottsdal   | e Case Numbers:<br>45 - DR - <u>2005</u>   | PP   | PC# 2013-0   |
|---|--|---|--|--|--|
| The applicant/devel submitting improved Review Board.   | oper must complete a<br>ement plans. Denial  | nd submit this form to the of the waiver may require Kelated  | e city for processing and obta   | in approval of waivevised site plan to t   | er request <b>before</b><br>he Development<br>(Safari - Ph             |
| Applicant Contact<br>Phone 602-474-92   | 601 N SCOTTSDALE RD<br>Ramzi Georges   | SCOTTSDALE, AZ 85251 Fax 602-678-5155 AZ Suite #430   |  | ns and Associates, in  | С.   |
| stormwater stora<br>demonstrate th<br>applicable box a<br>project meets the<br>If the runoff for the<br>demonstrate that  | neet at least one of f<br>age. However, regal<br>at the effect of a wand provide a signed<br>a criteria and that the<br>the project has been<br>t the stormwater sto | rdiess of the criteria,<br>alver will not increase<br>engineering report and<br>effect of a waiver will<br>included in a storage f<br>rage facility was specif    | o for the city to consider we a waiver will only be grade the potential for flooding supporting engineering at not increase the potential acility at another location, fically designed to accomment through an adequately designed to accommendately desi | Inted If the appliing on any prope analysis that demail for flooding on a the applicant munodate runoff from | cant can inty. Check the constrate the iny property. st in the subject |
| and con  2. The de  3. Stormy Ordina Pro Pro def  | restructed to handle to velopment is on a payater storage required nee (ESLO). A confluperty located in the aperty where more the ined in the city Zonia             | he additional runoff.  arcel less than one-hal- ments conflict with rec- ct with ESLO is limited hillside landform as de- an thirty-five (35) pero- ng Ordinance. | quirements of the Environr   | nentally Sensitive<br>rdinance.<br>I natural area ope  | e Lands  |
| By signing below attached documents by signing below attached documents by the significant control of |  | ated project meets the  | walver criteria selected al  | sove as demonstrated $8/3/$  | rated by the   |

Planning, Neighborhood & Transportation Division
7447 E Indian School Road, Suite 105, Scottsdale, AZ 85251 • Phone: 480-312-7000 • Fax: 480-312-7088



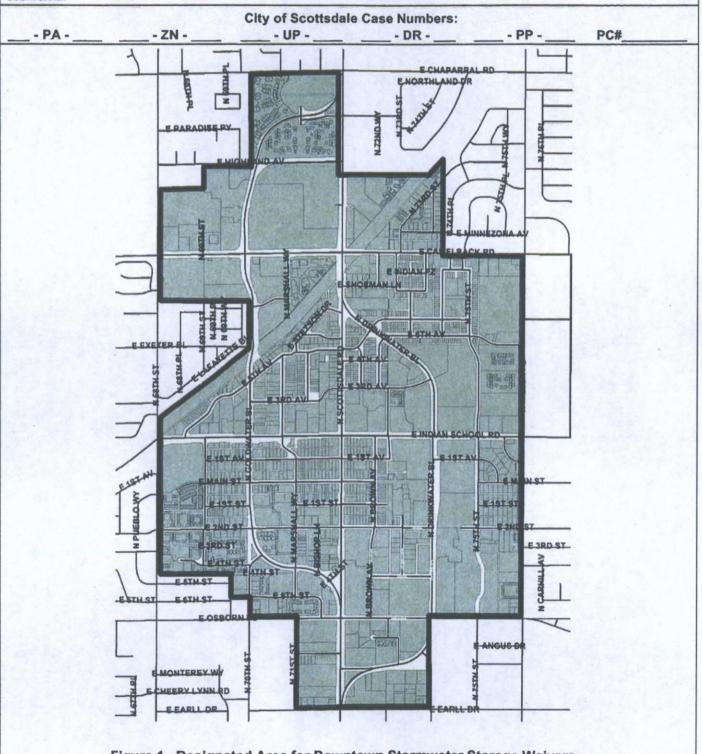


Figure 1. Designated Area for Downtown Stormwater Storage Waivers

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| ÇŢY     | À |        |
|---------|---|--------|
| OF SECT |   | M<br>M |

| P/      | City of Scottsdale Case<br>A ZN UP <u>45</u>  | e Numbers:<br>- DR - <u>200</u> 5 | PP | PC# 2013-18                           |
|---------|---|-----------------------------------|----|---------------------------------------|
|         | CITY STAFF TO COMPLET   |                                   |    |                                       |
| Project | Name Scottsoala Bluesky   |                                   |    | <i>1</i>                              |
|         | `   |                                   |    |                                       |
| Check   | Appropriate Boxes:  |                                   |    |                                       |
|         | Meets waiver criteria (specify): □1 □2 □3   | <b>127</b> 4                      |    |                                       |
| V       | Recommend approve waiver.   |                                   |    |                                       |
|         | Recommend <u>denv</u> waiver:  None of waiver criteria met.   | ·                                 | 1  |                                       |
|         | ☐ Downstream conditions prohibit waiver of any store  | age.                              |    | ÷                                     |
|         | Other: Explain:   |                                   |    | · · · · · · · · · · · · · · · · · · · |
|         | Return waiver request:  Insufficient data provided.  Other:  Explain:   |                                   | •  |                                       |
|         | ommended Conditions of Waiver: All storage requirements waived. Pre development conditions must be maintained. Other: |                                   |    |                                       |
| ·       |   |                                   |    |                                       |
|         | Waiver approved per above conditions.   |                                   |    |                                       |
|         | C. Ashay Couch  | 8/16/11                           |    |                                       |
| . 1     | Floodplain Administrator or Designee  | Date                              |    |                                       |
|         | Planning, Neighborhood &  |                                   |    | 1                                     |



|  |   | •  | le Case Numbers:  |                                   |                                  |
|--|---|--|---|-----------------------------------|----------------------------------|
| <u>- PA</u>  | ZN  | UP   | 45-DR-2005_   | PP                                | PC#_2015-09                      |
|  | , Ir  | n-Lieu Fee and In-K  | ind Contributions   |                                   |                                  |
| it would cost the construction, land the fee for this  | ne city to provide the<br>andscaping, design,<br>s cost is \$3.22 per o | e waived storage vol<br>, construction manag               | calculate and contributions, including costs spement, and maintenater storage waived. The cost at any time. | such as land ac<br>nce over a 75- | equisition,<br>year design life. |
| contribution ca<br>stormwater rel  | an serve as part of o   | or instead of the calc                                     | utions on a case-by-ca<br>ulated in-lieu fee. In-k<br>it. In-lieu fees and in-k<br>se.                      | ind contribution                  | ns must be                       |
| Project Name   | Scottsdate BlueSky  |  |   | <del></del>                       | •                                |
| The waived st  | ormwater storage v  | olume is calculated  | as follows:   | ٠.                                |                                  |
| C =weighted a<br>R =100-year/2   | r storage volume re<br>average runoff coeff                             |  |   | ge 11), and                       |                                  |
| Furthermore,   |   |  |   |                                   |                                  |
| $V_w = V - V_p$ ; w<br>$V_w \approx \text{volume w}$<br>V = volume re<br>$V_p = \text{volume p}$ | vaived,<br>quired, and  | C = 0.86<br>A = 163<br>V = 25.6<br>$V_p = 0$<br>$V_w = 25$ | 000 SF<br>53  |                                   |                                  |
|  |   | sed on the following<br>3.22 per cubic foot =              | calculations and supp   | orting docume                     | ntation:                         |
| 🛛 An in-kind   | contribution will be  | made, as follows:  | ,   |                                   |                                  |
| As previously  | approved for the overall proje  | ct, an 8' x 6' box cuivert was in                          | stalled along the SRP canal (See  | attached plans) in lieu           | of an in-kind fee.               |
| Approved by  | C. Ashley   | r Couch  |   | 8/16/11                           |                                  |
| Floodplain Admir   | nistrator or Designee V   |  |   | Date                              |                                  |
|  | <del></del>   |  | <u> </u>  | <del></del>                       |                                  |

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# GENERAL NOTES FOR CONSTRUCTION

- ALL CONSTRUCTION DE REGIOT BORNS-OF-DAY OR IL LOCADATS COLUMNO FOR PROJECT USE BLOS CORPORA TO LARST MARCOPA ASSOCIATION OF CONSTRUCTION DAYS UND STANDARD SCOPICATIONS, AND UNFORM STRUCTION OF CRITICAL FOR PUBLIC WINNES CONSTRUCTION AN ARCHIOLO BY THE LIVENT PERSON OF THE CITY OF SCOTISSIALE (CASS) SUPPLICIENTAL STANDARD SPECIFICIDATES AND SUPPLINGUIAL STANDARD DEVALS OF THERE IS A CONSTRUCT, LATTER SHALL CONSTRU
- the exchement designs on these plants and only approxim by the city in scope and hat at detail if constitutions Guartines and shown on these plants, they are not nother by the city.
- APPROVAL OF PLANS IS VALID FOR SIX (8) MORCHS OF AN EMISCALCHARDT PERMIT FOR THE CONSTRUCTION HAS NOT REDMISSION IS ALSO FOR SIX (8) MORCHS OF APPROVAL.
- A PUBLIC WHATS INSPECTION WILL INSPECT ALL WICHES WICHIN THE CITY OF SCOTTSTALE RICHTS-CY-WAY AND IN CASSIDENTS, MOTEY INSPECTION (SERVICES 34 HOLDES POORT TO STANDING CONSTRUCTION (CELEPHOLE 400-112-5750).
- ANDERED EXCESSES. THAT THE COCKNOW OF THE CHOESCHOOLD FIRST LIKES IS CONTRESD FOR THE PROJECT CALT SETS OF COURTS BY SEE THAT THE COCKNOWN IS TO SEED AND THE PROJECT CALT. THE STATE COURTS COURTS INC. THE PROJECT CALT.
- Annachadh Franch air Reimheid fàr all woll in Paill Eights-Of-Bay and Leichen's Gainte de Right Treis, an Dhoidheadh Frant Bl. (6 1921) by 116 cht leo George of Rhoheid of Annach 117 cht. Litzus Synces to 66 fronced of the Chin. Chies of All Francis Shall be arthaed of-Ste and Shall by Louis for Annach at all the Louis faller to Produce de Requires Points wal Result was inaughait work Stoppage L die Rhoheid Formet Cocamathadan is Gethard.
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STANDARD. ABBREVIATIONS

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DATA MILITA

# SCOTTSDALE, ARIZONA IMPROVEMENT PLANS

# GENERAL WATER NOTES 1. DEVLOPE IS RESPONSEE FOR WORK PROPE APPLATION AND PATRIC THE PREVIOUS PETS FROM TO CONSTRUCTION OF ALL SERVICES. DETAINS ON HOM 21 STATE AS CONTROL AND SEATOR METATO DO DE VLENERO DE SE CON VOI SELO DE DE CONTROL D THE VALUES SHALL BE FLANCE BY MECHANICAL JURIS TO ALLIES SHALL BE FLANCE BY MECHANICAL JURIS SHALL BE MADE MADE AND THE CITY PROPERTIES FOR THE SHALL BE MADE WHITE SHALL BE MADE WHITE SHALL BE AND THE CITY PROPERTIES FOR T CAMBLEACK ROAD

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# MICHITY MAP (N)

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A38OCIATES INC.
21:11 East Highland Ave.
Suite 200

Pipenix Arizona 85016

Phone: 602.678.5151

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PHASE 1 & 2

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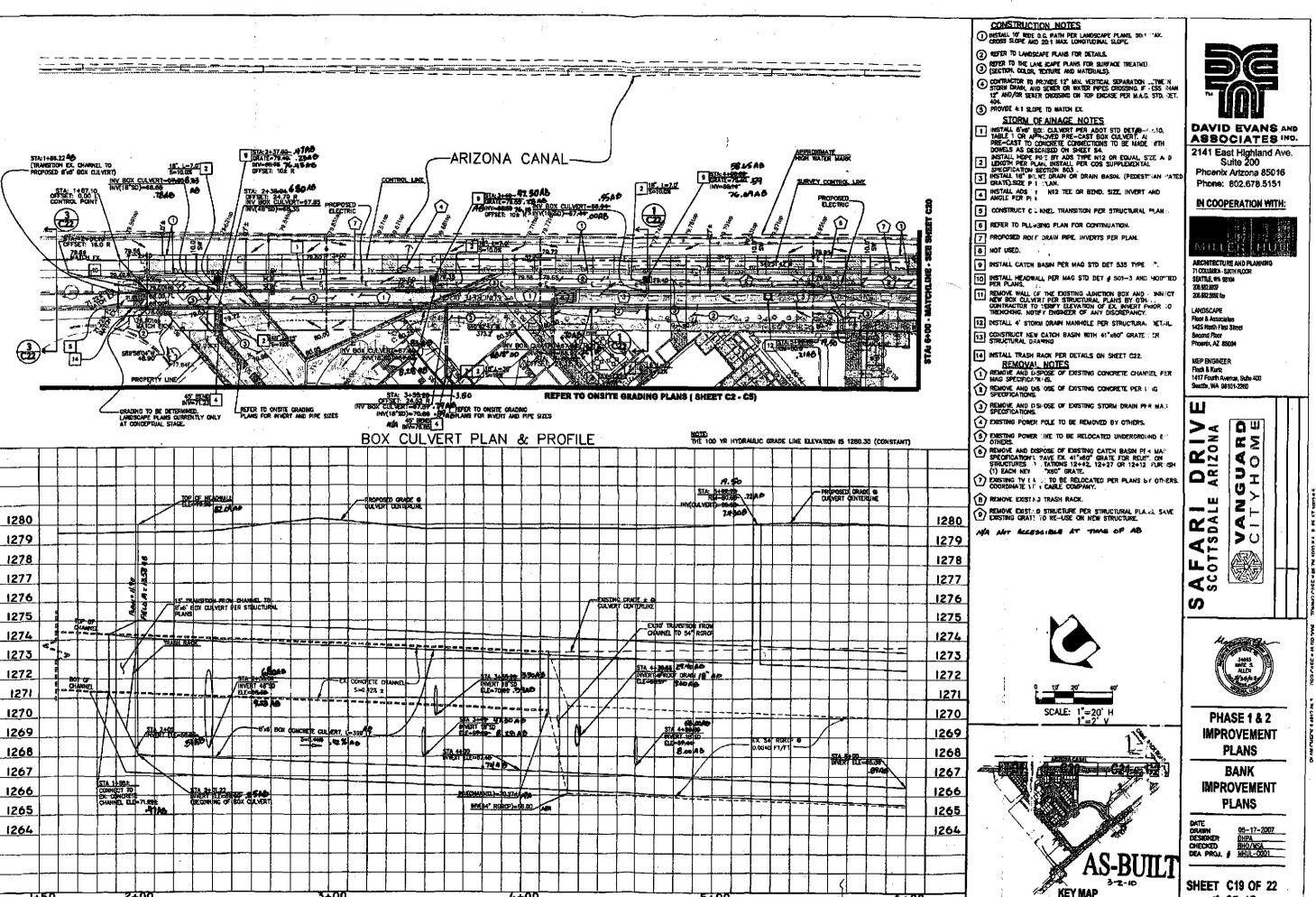
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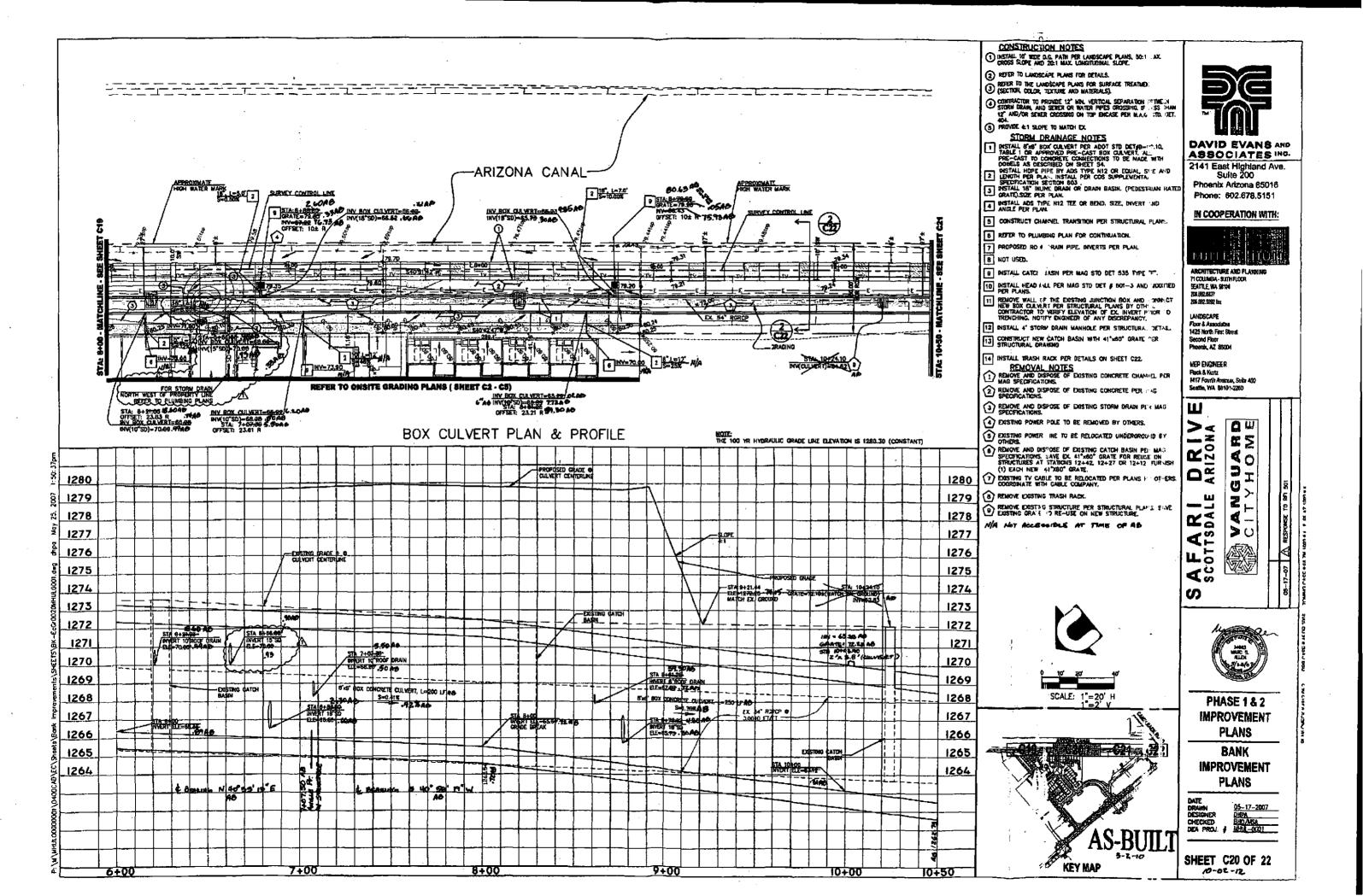
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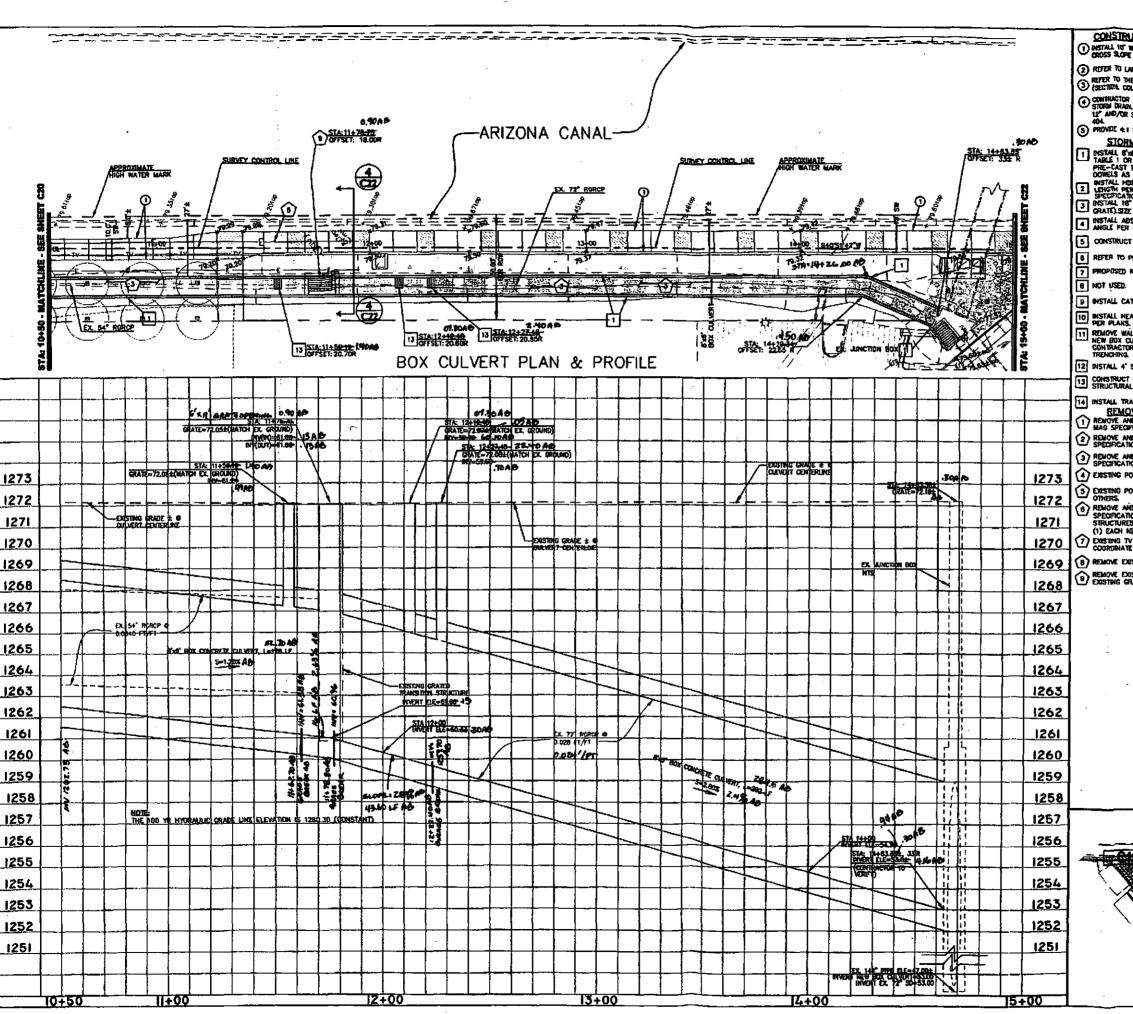
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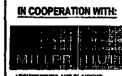
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- 5 CONSTRUCT CHANNEL TRANSITION PER STRUCTURAL : LANS
- B REFER TO PLUMBING PLAN FOR CONTINUATION.
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- 12 INSTALL 4" STORM BRADI MANHOLE PER STRUCTURAL DETAIL
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- 14 INSTALL TRASH RACK PER DETAILS ON SHEET CZZ.
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- (B) REMOVE EXISTING TRASH RACK.
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DAVID EVANS AND

ASSOCIATES INC.

2141 East Highland Ave. Suite 200 Phoenix Arizona 85016 Phone: 602.676.5151

ARCHITECTURE AND PLANNING 71 COLUMBIA - SOTH FLOOR SENTELS WAS SLOW 216 602 5002 to

LANDSCAPE Floor & Associates 1425 North First Street Second Floor Phoenix, AZ 85004

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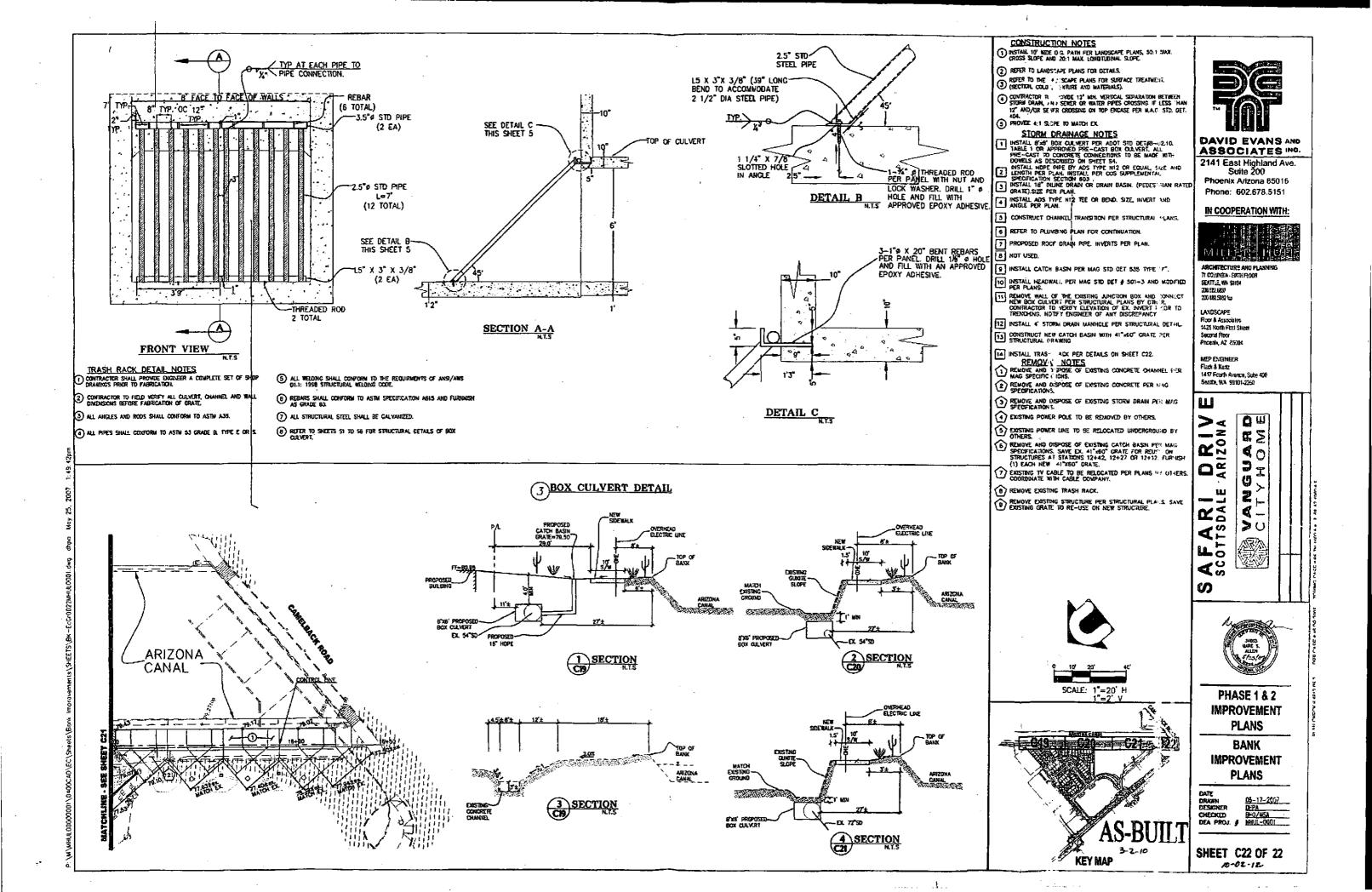


**PHASE 1 & 2 IMPROVEMENT PLANS** 

BANK **IMPROVEMENT** PLANS

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|                          |  | City of Scottadi                   | 3502-45<br>ale Cese Numbers  |
|--------------------------|--|------------------------------------|------------------------------|
|                          |  |                                    | 45 00 100                    |
| 4                        | 300  |                                    |                              |
|                          | Before the submittal of improvement plans the developer must obtain approval of this waiver request may require a revised site plan be submitted to the DR Bo  |                                    | PP                           |
|                          | REQUEST FOR STORMWATER STORAGE WAIVER F (To be completed by the applicant and submitted to the city for process  | ORM (Page 1                        | of 3)                        |
| wa<br>f th<br>nus<br>nai | ver Criteria alver is an intentional relinquishment of a claim or right. Before the claim or right. Before the claim required stormwater storage at least one of the following city ordinates to the criteria below that applies to this project and processes that demonstrate that the effect of this walver will not increase the property. | ance criteria (î<br>vide the engin | n bold)<br>eering            |
| ]                        | 1. The runoff has been included in a storage facility at another developer must demonstrate that runoff from this site will be safely location through an adequately designed conveyance facility.   |                                    |                              |
|                          | 2. Application is for a building permit to construct a single-fam structure.   | ily residential                    |                              |
| Ø                        | 3. Development is adjacent to a watercourse or channel that he constructed to handle the additional runoff flow without increasional damage to any other downstream property. The develope the watercourse has the extra capacity needed to convey the additional runoff.  | aing the pote<br>or must demon     | ntial for                    |
|                          | 4. The development is for a parcel under one-half acre in an ardemonstrated by engineering analysis that no significant increficed damage will be created by the development.  |                                    |                              |
|                          | 5. There is a possible conflict with the requirements of the city<br>Sensitive Lands Ordinance (city staff must make the final determinance)   |                                    |                              |
| · <b>=</b>               | Taro Shape Taye 5/3/65 cer   | lify that:                         |                              |
| Γhe                      | Riverwalk Square meets one of the criteria   | checked above                      | 9.                           |
|                          | ject Location North of the north east comer of Sca<br>Discant Phone (480) 346-3200   | tsdal + & C                        | amelback 2d.                 |
|                          | Sicent Mailing Address 7272 E. Indian School Rd. Surta 470 Scotts-dale A2 85251  |                                    |                              |
| ۰                        |  |                                    | is correct and ces not) meet |

# REQUEST FOR STORMWATER STORAGE WAIVER FORM (PAGE 3 of 3) (This page to be completed by city staff) (4/7/00)

| Project Name   |                      |
|--|----------------------|
| CHECK APPROPRIATE BOXES                                  |                      |
| Warver criteria met (specify) 🔲 1 🔲 2 💢 3 🔲              | 4 🔲 5                |
| Wajver approval recommended                              | ,                    |
| Waryer recommended for denial                            |                      |
| None of the waiver criteria met                          |                      |
| Downstream conditions prohibit the waiver of any storage | 1                    |
| Other  | _                    |
| Waiver request returned .                                |                      |
| insufficient data provided                               |                      |
| Other  |                      |
| Explain  |                      |
| Recommended Conditions of Warver                         |                      |
| All storage requirements warved                          |                      |
| Pre development conditions must be maintained            |                      |
| Other See in Kind contabution                            | <u> </u>             |
| Explain  |                      |
|  |                      |
| Above Recommended by DRAINAGE PLANNER                    | DATE                 |
| WAIVER APPROVED, ORDENIED, _                             | per above conditions |
| By Help  | 7/1/05               |
| FLOODPLAIN ADMINISTRATOR                                 | DATE 7/1/0S          |
| By CON DOMESTIC CHIPLIANCE DIRECTOR                      | DATE DE              |



Job No 5140.0001 Project Riverwalk Square

Subject Storm Drain Retautor 100 YV-Zhr

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#### RIVERWALK SQUARE STORAGE WEER EXHIBIT

By I David Lopez Ivich, P.E.

Tri-core Engineering, 7272 E. Indian School Rd Suite 420

Scottsdale, AZ Tel 480-346-3200

| Table 1 Cost Estimate of Improvements                                |          |      |  |              |  |  |
|--|----------|------|--|--------------|--|--|
| DESCRIPTION  | QUANTITY | UNIT | COST   | TOTAL        |  |  |
| New 84" HDPE   | 976      | LF   | \$120 00                                     | \$117,120 00 |  |  |
| Extantion of exesting 64 pipe  | 220      | LF   | \$120 00                                     | \$27,480 00  |  |  |
| Downstream Junton Box (connects 2-54 pipes to 72" pipe)              | 1        | EA   | \$3,500 00                                   | \$3,500 00   |  |  |
| Upstream Junton Box and Trush Rack (connects 2-64° pipes to Channel) | 1        | EA   | \$5,000 00                                   | \$5,000 0    |  |  |
| Storm water poliulant remover  | 4        | EA   | \$700 00                                     | \$2 800 00   |  |  |
| Removal of existing catch basin grates                               | 2        | EA   | \$500 00                                     | \$1,000 00   |  |  |
| Removal of existing junction box and trash rack                      | 1        | EA   | \$1 500 00                                   | \$1,500 00   |  |  |
|  |          |      | <u>                                     </u> |              |  |  |
|  |          |      | Total  | \$158,400 0  |  |  |

| Table 2 Cost Estimate of Retention                              |          |      |        |               |  |  |
|---|----------|------|--------|---------------|--|--|
| DESCRIPTION   | QUANTITY | UNIT | COST   | TOTAL<br>COST |  |  |
| Refention Required 1 acrest (Using storm drain chambers system) | 43 282   | CF   | \$3 80 | \$151,487 00  |  |  |
|   | _ · ]    |      |        |               |  |  |
|   |          |      | Total  | \$151,500 00  |  |  |



#### DAVID EVANS AND ASSOCIATES INC.

August 4, 2011

Joe Rumann 7447 E. Indian School Road, Suite 125 6263 Scottsdale Road, Suite 330 Scottsdale, AZ 85251

SUBJECT: Retention Waiver Application Cover Letter for DR Submittal #2013-08 (Safari - Ph 3)

Dear Mr. Rumann:

This letter is in support of the retention waiver application for the development of the Scottsdale BlueSky project. The site is located within the City of Scottsdale core downtown area near the northeast corner of the intersection of Scottsdale Road and Camelback Road. There will be no adverse impacts on adjacent properties due to the development of the Scottsdale BlueSky project site. The site is located in two flood zones. The southern portion of the site is located in flood Zone A and the northern portion of the site is located in flood Zone X.

The project is comprised of approximately three acres within Section 23, Township 2 North, Range 4 East of the Gila and Salt River Base and Meridian. The Scottsdale BlueSky project will be a mixed use development consists of multi-family residential apartments, grocery store, Restaurant, Retail, Club/fitness house, and office. There will be 4-levels of below grade parking that will provide approximately 1,511 parking spaces.

Site grading and drainage is designed to elevate finish floor elevations above the base flood elevation, maintaining at least minimum required freeboard during the design 100-year storm event.

Offsite runoff that reaches the northeastern portion of the site is conveyed along western boundary of the Arizona Canal in a southwesterly direction through an existing underground box culvert that was constructed as part of the initial phase of the project.

Scottsdale Road is an improved street with curb and gutter that drains in a southerly direction adjacent to the site. The majority of the runoff along Scottsdale Road is conveyed within the street section of the road and a smaller portion is conveyed into the existing storm drain system along Scottsdale Road that outfalls into the main storm drain in Camelback Road. There is also a small amount of runoff diverted from Scottsdale Road into Coolidge Street and is then conveyed in an easterly direction into the culvert mentioned above.

The existing runoff conditions were carefully studied in the initial phase of the project (Safari Drive) and they will be maintained during the design of the current phase (Blue Sky). The existing drainage conditions will be used as guidelines in the development and design of the Blue Sky project.



In addition, the box culvert installed during the initial/previous phase of the project has been constructed in-lieu of onsite retention. Based on the above information and the attached retention waiver application, we respectfully request that you consider the previously approved culvert, built as part of the initial phase of the project, to be utilized in-lieu of onsite retention for the project.

Should you have any questions, please contact me at (602) 474-9223.

Sincerely,

DAVID EVANS AND ASSOCIATES, INC.

Ramzi Georges, P.E., CFM Senior Project Manager

## APPENDIX F REPORTS BY OTHERS

# FINAL DRAINAGE REPORT SAFARI DRIVE

OCTOBER 2006 DEA PROJECT NO. MHUL0000-0001

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#### 1.0 INTRODUCTION

This final drainage report has been prepared under a contract from Riverwalk Square, LLC for the Safari Drive project in Scottsdale. The purpose of this report is to provide hydrologic and hydraulic analyses, required by the City of Scottsdale, to support the Safari Drive improvement plans. Preparation of this report has been done in accordance with the procedures detailed in the City of Scottsdale Design Standards and Policies Manual (Reference #1) along with the City of Scottsdale Supplement to MAG Uniform Standard Specifications For Public Works Construction (Reference #2) and Drainage Design Manuals for Maricopa County, Arizona, Volumes I & II (References #3 and #4).

The proposed Safari Drive project is located northeast of the intersection of Scottsdale Road and Camelback Road, within the City of Scottsdale, Maricopa County, Arizona. The site is located within Section 23, Township 2 North, Range 4 East of the Gila and Salt River Base and Meridian.

The project site is bound by a commercial development to the north (Highland Park), undeveloped parcel to the west (east of Scottsdale Road), a commercial development to the south and the Arizona Canal to the east. Access to the site will be provided via two entrances from Scottsdale Road along 72<sup>nd</sup> Place and Coolidge Street. The project is located within what is considered the Downtown Area of the City's General Plan.

The proposed Safari Drive project site is approximately 5 acres (for Phase 1 and 2). The project is going to be developed in phases. Onsite improvements include the demolition of existing structures, site grading, and construction of the new Safari Drive buildings with associated hardscape and landscaped areas. Offsite improvements include asphalt pavement for portions of the adjacent street sections and a proposed turning lane along Scottsdale Road.

#### 2.0 EXISTING DRAINAGE CONDITIONS

As mentioned in the section above, the site is located east of Scottsdale Road, west of the Arizona Canal and south of Coolidge Street. Through researching several drainage reports, aerial photos and as built information, it was determined that the site was occupied with a resort known as the Safari Hotel and Resort, See Appendix F. The resort site was demolished in 1998 and it was regarded. Aerial photos and field visits show that there are no washes impacting the site.

Offsite runoff that may impact the site is conveyed along western boundary of the Arizona Canal in a southwesterly direction. According to the topography in the area, the general lay of

the land is in a southeasterly direction, towards to the Arizona Canal, where runoff ponds against the canal before it is conveyed through storm drain systems or weirs over the canal. The Arizona Canal is supposed to be drained during major storm events, in addition to a 4-foot of freeboard that would allow the canal to accept additional storm runoff into its system.

The site is located in an area that drains into what is known as Reach 4 of the Flood Control District's side channel drainage system. This storm drain system runs along Camelback Road and outfalls into the Indian Bend Wash and it was installed in the 1980's through coordination with the City of Scottsdale, Flood Control District and the US Army Corps of Engineers. The system was designed to convey the 25 year storm event. There is a series of grated inlet structures (equivalent to two MAG 535 structures) that capture runoff along the western side of the canal and convey runoff into an underground 54 inch storm drain pipe that changes into a 72 inch pipe which outfalls into the storm drain system in Camelback Road. These area drains and the underground storm drain system traverse the eastern boundary of the Safari Drive site. There is also a large grate inlet structure, northeast of Camelback Road and Scottsdale Road intersection, along the western side of the Canal between the two commercial developments south of the safari site that captures runoff that ponds west of the Arizona Canal.

Scottsdale Road is an improved street with curb and gutter that drains in a southerly direction, adjacent to the site, towards Camelback Road. The majority of the runoff along Scottsdale Road is conveyed within the street section of the road and a smaller portion is conveyed into the existing storm drain system, along Scottsdale Road, that outfalls into the main storm drain in Camelback Road.

It is estimated that there is approximately 3,638 cfs that would reach the intersection of Camelback and Scottsdale Road (based on CVL report, Reference 8). The majority of the runoff will weir over the Arizona Canal bank into the canal itself, which is supposed to convey the runoff. Some of the runoff may spill over Camelback Road in a southerly direction as well.

The current published FEMA Flood Insurance Rate Map (FIRM) for this area is map number 04013C1695H (Effective date is September 30, 2005). Portions of the site were located within zones A and X. Zone A is defined as the flood insurance rate zone that corresponds to the 100-year floodplains that are determined in the Flood Insurance Study by approximate methods. Because detailed hydraulic analyses are not performed for such areas, no Base Flood Elevations or depths are shown within this zone. Zone X is defined as "areas of 500-year flood; areas of 100-year flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from the 100-year flood." A copy of the FIRM panel is provided in Appendix B.

A CLOMR has been filed for Safari Drive project by different firm than DEA, before DEA was contracted to finish the design improvement documents for the project. A copy of the Conditional Letter of Map Revision (CLOMR) Response from FEMA is included in Appendix E of this drainage report. The CLOMR was based on fill and that the proposed finish floor elevations are higher than Arizona Canal bank. The proposed structures should be free from inundation during a 100-yeat storm event. A Letter of Map Revision (LOMR) will be submitted after the project is build and all the design documents have been approved.

#### 3.0 PROPOSED DRAINAGE CONCEPT

The proposed drainage concept is presented in three parts: onsite drainage, off-site drainage, and storage requirements. The hydrologic analysis is summarized in section 4.0 and the hydraulic analysis is summarized in section 5.0. See Exhibit A, located in the back pocket, for an illustration of the proposed drainage concept.

#### 3.1 On-site Drainage Conveyance

The Safari Drive site runoff is mostly generated on the roof, the hardscape and landscape areas surrounding the buildings and the courtyard areas. The runoff generated on the roof is conveyed into roof drains that direct the runoff onsite storm drain system or directly into the 54 inch pipe west of the Arizona Canal. Refer to Exhibit A for a graphical illustration of the proposed onsite drainage.

#### 3.2 Off-site Drainage Conveyance

DEA designers have conducted field visits, reviewed aerial maps and available topography to determine the hydraulic/hydrological conditions of the contributing watershed north of the Safari Drive project site. Runoff that may impact the site could enter the site from the northeastern portion of the site, with runoff being conveyed in a southwesterly direction along the west bank of the Arizona Canal. The second area of offsite runoff that could potentially impact the site is runoff flowing south along Scottsdale Road. In addition to that, runoff concentrating at the intersection of Camelback Road and Scottsdale Road weirs over the Arizona Canal could back into the site if the weir high water elevation over the canal bank is higher than the proposed finished grade elevations onsite.

The first area of investigation was to quantify the offsite runoff along the northeastern portion of the site. Runoff that may impact the site is generated north of Chapparal Road. During field visits it was observed that an 8'x4' concrete box culvert exists underneath Chapparal Road, west of the Arizona Canal. Few feet upstream of the culvert, is a 20.5'x13' grate inlet structure. Runoff from the north captured by the grate inlet is conveyed in an easterly direction through an

approximately what seemed to be a 96" pipe underneath the Arizona Canal. Any runoff that by pass the grate inlet structure (which is not likely) will flow through the 8'x4' culvert, underneath Chaparral Road, in a southerly direction. However, field observations have shown that there are sidewalks extending from hotel buildings, west of the Arizona Canal and south of Chapparal Road, to the Arizona Canal bank. These sidewalks create berms/dam situation along the west side of the canal with 2 -18 inch bleed off pipes underneath these sidewalks. This occurs in 3 different locations upstream of the site.

Each of the 18 inch pipes is estimated to convey a flow amount that is less than what the full 8'x4' concrete box culvert can convey. The runoff that ponds upstream of the sidewalks in excess of the 18 inch pipe conveyance capacity would weir into the Arizona Canal (to the west) and over the sidewalk in a southerly direction. The sidewalks and the canal banks seemed to have the same elevations and it is assumed that 50 percent split will occur at each of the sidewalk locations.

Hydraulic analysis has been conducted for the 8'x4' culvert at Chaparral Road in order to determine the maximum capacity of the culvert and it was found to be 277 cfs. The 277 cfs representing the maximum capacity of the culvert is used at the downstream three sidewalk locations to determine the split flows in each direction. The result was that 200 cfs will spill into the Arizona Canal and the remaining 77 cfs will continue in the southerly towards the Safari Drive project. Refer to Appendix D for detailed split flow analysis data sheets.

In addition to the flow calculated above, the existing 54-inch/72 inch storm drain system east of the site will receive runoff from the development north of site. The majority of the runoff generated in the subdivision and the commercial development upstream of the site is bounded by Chapparal Road to the north, Scottsdale Road to the west, the Arizona Canal to the east and the Safari Drive project northern boundary to the south. The runoff outfalls to the channel northeast of the corner of the Safari project site. The Rational method was used to determine the flow and 140 cfs was estimated to be the peak flow that combines with the 77 cfs mentioned above. Thus, the total flow that enters at the northeastern portion of the site is 217 cfs (within the concrete channel, west of the Arizona Canal).

A FlowMaster (Reference 7) was used to determine the high water elevation, using the 217 cfs. An earthen channel, west of the canal and above the 54 inch pipe, was modeled to check the high water elevation in the channel using the 217 cfs. The modeling did not take into account the 54 inch pipe and the high water elevation at the upstream portion of the site was found to be 77.2 which is 3.7 feet lower than the proposed finish floor elevations onsite.

Several drainage reports have quantified the runoff flowing south along Scottsdale Road. Based on the Final Drainage Report prepared by CVL (Reference #8), the flow along

Scottsdale Road is in the vicinity of the project 378 cfs. This flow is approximately consistent with flow quantified DMJM (Reference 9). FlowMaster program was used to determine if the street flow depth can be contained in the street without spilling into the Safari Drive project. The calculations have shown that ponding above the gutter elevation of 1.2 feet. Hence, the entrances and future frontage along Scottsdale Road are and will be elevated to 1.2 feet from the gutter elevation, thus creating a berm minimizing the possibility of the street runoff from entering the site.

The contributing drainage areas to Scottsdale Road extend all the way to the mountains west of Invergordon Road. The majority of the runoff from the mountains will flow in a southeasterly direction towards Scottsdale Road and Camelback Road. Gold Water Boulevard acts as a ridge line because of its elevated topography in some locations, deep dip locations in others and the existing development as well. Any runoff from the mountains that reaches Camelback Road from the north will flow in an easterly direction along Camelback Road, while breaching south into the north-south streets such as 66th Street, 68th Street, Goldwater Boulevard and Scottsdale Road. The CVL report, mentioned earlier, has quantified that approximately 3,638 cfs will reach Scottsdale Road and Camelback Road intersection, where it will then spill into Arizona Canal. From several conversations with different agencies, it is believed that the Arizona Canal is maintained in such a way that it is capable of conveying the additional 3,638 cfs without breaching in a southeasterly direction. Although, the 3,638 cfs seems overly conservative and is questionable because of the hydraulic conditions of Camelback Road (mentioned above), DEA modeled the weir along the Arizona Canal based on that flow. The high water ponding elevation along the Arizona Canal bank canal was determined to be 1280.30, which is 0.65 feet below the lowest proposed finish floor elevation of 1280.95. This indicates that the proposed buildings will not be flooded during the 100-year design storm event.

As mentioned earlier, the Arizona Canal causes ponding along the west side of its bank. An older drainage report that was produced by the Corps of engineers has accounted for inlets west of the canal to reduce or bleedoff the amount ponding that was occurring west of the Arizona Canal. Hence, the Safari project provided a passage for the runoff from Scottsdale Road (approximately 70 cfs) into the inlets along the west side of the canal or the existing 54 inch, west of the canal. This is partially accomplished by adding two 20 foot catch basins on both side of Coolidge Street, east of Scottsdale Road. The two catch basins convey captured runoff into a 48 inch diameter pipe flowing in the easterly direction towards the Arizona Canal that connects into the 54 inch storm drain pipe. The remainder of the flow along Scottsdale Road will continue along its historic path towards Camelback Road and ponds along the west side of the Arizona Canal and enters the inlets that were designed by the Army Corps of engineers or the revised inlets with equal or greater capacity.

#### 3.3 Storage Requirements

Historically, the proposed Safari site used to be a commercial resort with many buildings and associated parking, landscape and hardscape areas. The resort was known as the Safari Hotel and Resort and it did not seem to have onsite retention.

The proposed Safari project has retention waiver that is included in Appendix E. Portions of the site drain through roof drains directly into the existing 54 inch west of the Arizona Canal (which will be replaced with a proposed 8x6 concrete culvert). Also, portions of the site that are surrounding the onsite buildings, along the eastern portion of the site, sheet flow into the landscape area, west of the Arizona Canal. Portions of the site that drain into catch basins onsite will be retained in underground conveyance pipes located at the northeastern portion of the site and along Coolidge Street.

City of Scottsdale requires that runoff generated during a 100-year, 2-hour storm event within the project site to be stored onsite. The required storage volume for the project site is estimated as follows:

$$V_R = C_{wt} * (P / 12) * A$$

Where:  $V_R = Calculated volume in acre-ft or ft<sup>3</sup>$ 

Cwt = Weighted Runoff coefficient

P = Rainfall depth in inches (2.82 inches)

A = Drainage area in acres

The proposed site plan allocates some open space for storage. Basins have maximum 4 to 1 side slopes. The volume required is calculated based on a weighted "C" coefficient and 2.82 inches of rainfall. See Exhibit A in back pocket of this report for proposed storage layout.

## Summary of Storage Requirements Table 3.2

| Basin Label  | Estimated Volume Required ft <sup>3</sup> | Estimated Volume Provided ft <sup>3</sup> | Excess/Shortage<br>ft <sup>3</sup> |
|--------------|---|---|------------------------------------|
| Basin 1      | 1,533                                     | 802                                       | -731, overflow to Storage Pipe     |
| Basin 2      | 456                                       | 554                                       | 98,                                |
| Pipe Storage | 32,190                                    | 32,229                                    | 39                                 |

The underground CMP storage pipes will bleedoff in 36 hrs through conveyance pipes into the drainage system west of the Arizona Canal.

Refer to Appendix D that shows detailed volume calculations for the site fill placement. Based on these calculations, the proposed improvements for the site (including the offsite box culvert) have excess capacity of approximately 18 thousand cubic feet. Hence, the site development has provided more than the compensatory volume for the fill that has been placed onsite to keep the finish floors from flooding during a 100-year storm event.

#### 4.0 HYDROLOGIC ANALYSIS

The hydrologic analysis for this report has been prepared using City of Scottsdale's Supplement to MAG Uniform Standard Specifications for Public Works Construction and the Drainage Design Manuals for Maricopa County, Arizona, Volume I Hydrology. Peak flows were computed using the Rational Method. The project site was divided into several drainage areas, to determine peak flows at catch basins and inlet structures. These drainage areas are illustrated in Exhibit A, along with the location of their respective concentration points.

The following establishes the Rational Method equation and the basic input data required:

$$Q = C_{u_1} * I * A$$

Where: Q = Peak discharge in cubic feet per second

 $C_{wt}$  = Weighted runoff coefficient

I" = Rainfall intensity in inches per hour

A = Drainage area in acres

A summary for the peak flows for the 10-year  $(Q_{10})$  and 100-year  $(Q_{100})$  storm events for the developed onsite drainage conditions are shown on the next page in Table 4.1. Appendix D contains detailed calculation sheets that establish the input data and estimated peak flow values for the developed conditions.

Summary of Peak Flows Table 4.1

| Area Label | Q <sub>100</sub> (cfs) | Q <sub>100</sub> (cfs) |
|------------|------------------------|------------------------|
| 1          | 0                      | 0                      |
| 2          | 0                      | 11                     |
| 3          | 0                      | J                      |
| 4          | 0                      | 0 -                    |
| 5          | 111                    | 3                      |
| 6.1        | 1                      | 2                      |
| 6          | 1                      | 1                      |
| 7          | 0                      | 0                      |
| <u>8</u> . | 0                      | 0                      |
| 99         | 0                      | 0                      |
| 10         | 0                      | 0                      |
| 11         | 11                     | 1                      |
| 12.1       | 0                      | 1                      |
| 12         | 11                     | 2                      |
| 13         | 1                      | 1                      |
| 14         | 3                      | 66                     |
| 15         | 1                      | 2                      |
| 16         | 0                      | 0                      |
| 17         | 0                      | l                      |
| 18         | 0                      | 0                      |
| 19         | 0                      | 1                      |
| 20         | 1                      | 1                      |
| · 21       | 1                      | 1                      |
| 22         | 0                      | 1                      |
| 23         | 0                      | 11                     |
| 24         | 0                      | 11                     |
| 25         | 0                      | 1                      |
| 26         | 0                      | 1                      |
| 27         |                        | 111                    |
| 28         | 0                      | 11                     |
| 29         | 0                      | 11                     |
| 30         | 1                      | 1                      |
| 31         | J                      | . 2                    |
| 32         | 0                      | 1                      |
| 33         | 1                      | 1                      |

"0" value stands for Peak flow of less than 0.5 cfs.

#### 5.0 HYDRAULIC ANALYSIS

The hydraulic analyses of the proposed storm water management facilities are based on the City of Scottsdale's Supplement to MAG Uniform Standard Specifications for Public Works Construction and the Drainage Design Manuals for Maricopa County, Arizona, Volume II Hydraulics.

StormCAD (Reference #6), a Haestad computer program, has been utilized to analyze the curb inlets and the drainage pipes. The hydraulic grade line was kept below the ponding depth that is caused by the inlet capacities at different locations onsite. Refer to Appendix D for detailed input and output data sheets.

FlowMaster (Reference #7), a Haestad computer program, has been utilized to analyze the hydraulic capacity for the adjacent street section and channels to determine the 100-year high water surface elevations based on the determined offsite runoff. FlowMaster analysis is based on Manning's equation. Refer to Appendix D for detailed input and output data sheets.

Scottsdale Road has a half street capacity adjacent to the site of approximately 160 cfs. The remainder of the 189 cfs (half the 378 cfs mentioned previously) will weir into the Safari Drive site. To compensate for not allowing the 29 cfs from entering the site, two catch basins are proposed along Coolidge Road that captures approximately 70 cfs from the street flow in Scottsdale Road.

The 8'x6' culvert was designed for runoff generated during a 100-year storm event using the Rational method. The tailwater condition was used as the weir elevation during the 100-year 24 hour storm event. For a lesser storm, the worst case scenario was used by assuming that the tailwater is at the ground elevation. However, the storm drain can be assumed to be designed for the 25-24 hour storm event because it is the capacity of the downstream receiving system (although the culvert has excess hydraulic capacity)..

The existing inlets capacity along the western portion of the Arizona Canal will be replaced with new inlets. The new inlets have capacity equal or greater than the existing inlet capacity. Refer to Appendix D for hydraulic calculations of the proposed inlets.

#### 6.0 CONCLUSIONS

Based on the results of this study, it can be concluded that:

- The site is developed according to the City of Scottsdale Design Standards and Policies Manual.
- The proposed buildings will should be free from inundation during a 100-year storm event.
- Although the site retains the majority of the runoff generated onsite, the site has a retention waiver and portion of the site will direct discharge into the conveyance system along the western side of the Arizona Canal.
- The ultimate outfall is located at the southeast corner of the project site maintaining the historic outfall condition.

#### 7.0 REFERENCES

- 1. City of Scottsdale Design Standards and Policies Manual, December 1999
- 2. City of Scottsdale Supplement to MAG Uniform Standard Specifications for Public Works Construction, October 2003.
- 3. Drainage Design Manuals for Maricopa County, Arizona, Volume I, Hydrology, April 2002.
- 4. Drainage Design Manuals for Maricopa County, Arizona, Volume II, Hydraulics, April 2002.
- 5. City of Scottsdale Stormwater Master Plan and Management Program, KVL, 1994.
- 6. StormCAD Version 5.06.007, Haestad Methods, Inc. 2005.
- 7. FlowMaster Version 7.0005, Haestad Methods, Inc. 2005.
- 8. Drainage Report Scottsdale Riverwalk Center Hotel prepared by CVL dated April 9, 1999. Revised March 28, 2001.
- 9. Master Drainage Report Scottsdale Portales prepared by DMJM dated April 13, 1999.
- 10. Drainage Report For Safari Drive prepared by Pentacor dated 2-7-06.
- 11. CulvertMaster a Bently program V3.1, dated 2006.

## Appendix D

**404 Certificate** 



### **Section 404 Certification**

Before the City issues development permits for a project, the developer's Engineer or the property owner must certify that it complies with, or is exempt from, Section 404 of the Clean Water Act of the United States. Section 404, administered by the U.S. Army Corps of Engineers (COE), regulates the discharge of dredged or fill material into a wetland, lake, (including dry lakes), river, stream (including intermittent streams, ephemeral washes, and arroyos), or other waters of the United States.

Prior to submittal of improvement plans to Project Review the form below must be completed (and submitted with the improvement plans) as evidence of compliance

| Owner's Name: ANGUMPO CIN HOME Phone No. 480-993-0472   |  |  |  |
|---|--|--|--|
| Project Name/Description: SAFARI DRIVE Case No. 45 DR ZOOS  |  |  |  |
| Project Location/Address: NW OF INTERSECTIONS OF CHINELBARK ROAD  # Scotts up to ROAD   |  |  |  |
| A registered Engineer or the property Owner must check the applicable condition and certify by signing below that:  |  |  |  |
| <ol> <li>Section 404 <u>does</u> apply to the project because there will be a discharge of dredged or fill material to<br/>waters of the U.S., and:</li> </ol>          |  |  |  |
| A Section 404 Permit has already been obtained for this project.  |  |  |  |
| -or-  |  |  |  |
| This project qualifies for a "Nationwide Permit," and this project will meet all terms and conditions of the applicable nationwide permit.                              |  |  |  |
| 2. Section 404 does not apply to the project because:   |  |  |  |
| No watercourses or other waters of the U.S. exist on the property.  |  |  |  |
| No jurisdictional waters of the U.S. exist on the property. Attached is a copy of the COE's<br>Jurisdictional Determination.  |  |  |  |
| Watercourses or other waters of the U.S. do exist on the property, but the project will not involve the discharge of dredged or fill material into any of these waters. |  |  |  |
| I certify that the above statement is true.   |  |  |  |
| 8-09-05   |  |  |  |
| Engineer's Signature and Seal, or Owner's Signature Date  |  |  |  |
| Title Company   |  |  |  |
|   |  |  |  |

## DRAINAGE REPORT SCOTTSDALE RIVERWALK CENTRE HOTEL SCOTTSDALE, ARIZONA

April 9, 1999 1<sup>st</sup> Revision: March 28, 2001



Coe & Van Loo Consultants, Inc. 4550 North 12th Street Phoenix, Arizona 85014

CVL Project No. 98-0121-01

## DRAINAGE REPORT SCOTTSDALE RIVERWALK CENTRE HOTEL SCOTTSDALE, ARIZONA

April 9, 1999 1<sup>st</sup> Revision: March 28, 2001

# DRAINAGE REPORT SCOTTSDALE RIVERWALK CENTRE HOTEL SCOTTSDALE, ARIZONA

April 9, 1999 1<sup>st</sup> Revision: March 28, 2001

Prepared for:

Ganos Associates Architects 1940 E. Camelback Road, Suite #202 Phoenix, AZ 85016

Prepared by:

Coe & Van Loo Consultants, Inc. 4550 North 12th Street Phoenix, AZ 85014 (602) 264-6831



#### Drainage Report for Scottsdale Riverwalk Centre Hotel Scottsdale, Arizona

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Plate 1 Drainage Map



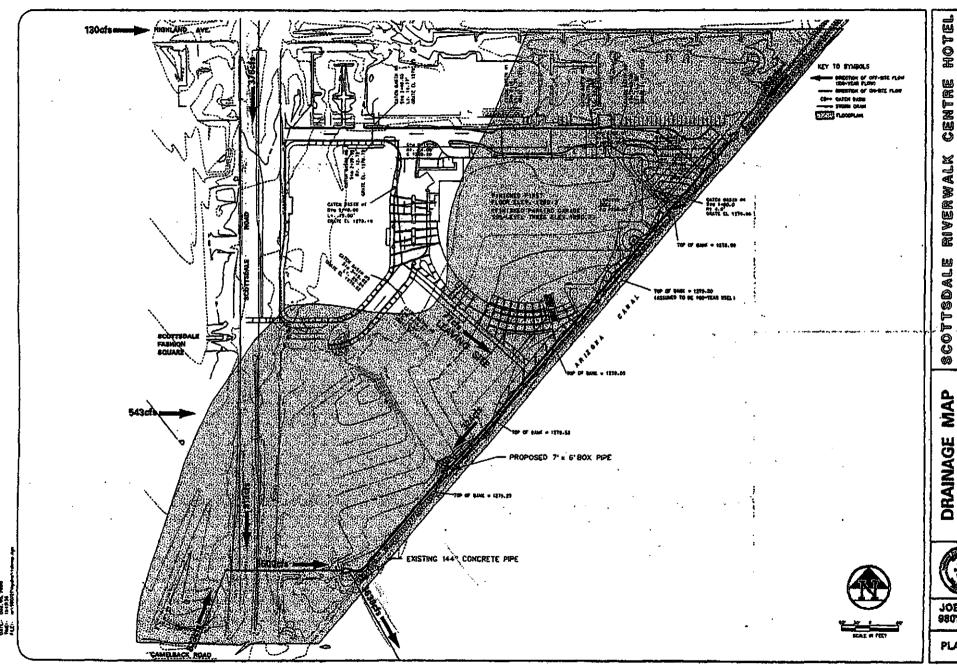
#### 3.0 MANAGEMENT OF OFF-SITE STORMWATER RUNOFF

The general direction of drainage flow in the area of this site is from northwest to southeast, with an outfall to the Indian Bend Wash. The City of Scottsdale Storm Water Master Plan and Management Program (Reference 1), identifies drainage area boundaries and estimated runoff rates throughout the developed areas of Scottsdale. This report was used as a basis for estimation of off-site discharges within the vicinity of the site.

Drainage north of Chaparral Road collects behind the Arizona Canal embankment and is intercepted by a large grate structure which outlets to a storm drainage system within Chaparral Road. Actording to the Storm Water Master Plan Chaparral Road represents a northern boundary for drainage that approaches the site. It was considered that this assumption was correct in developing the off-site discharges that approach this site.

A fully-developed area north of Highland Avenue and east of Scottsdale Road drains toward the Arizona Canal, and from there southwest within a drainage channel along the Arizona Canal. An existing office building and a two-level parking structure lie immediately north of the site. This office-building site provides some on-site retention within landscaped areas and on the parking surfaces. Drainage of retention areas is through the use of drywells. In the capacity of the site streetention is exceeded, drainage would be directed to the east with an outfall to the directed to the east with an outfall to the directed to the east with an outfall to the directed to the east with an outfall to the streetention is exceeded.

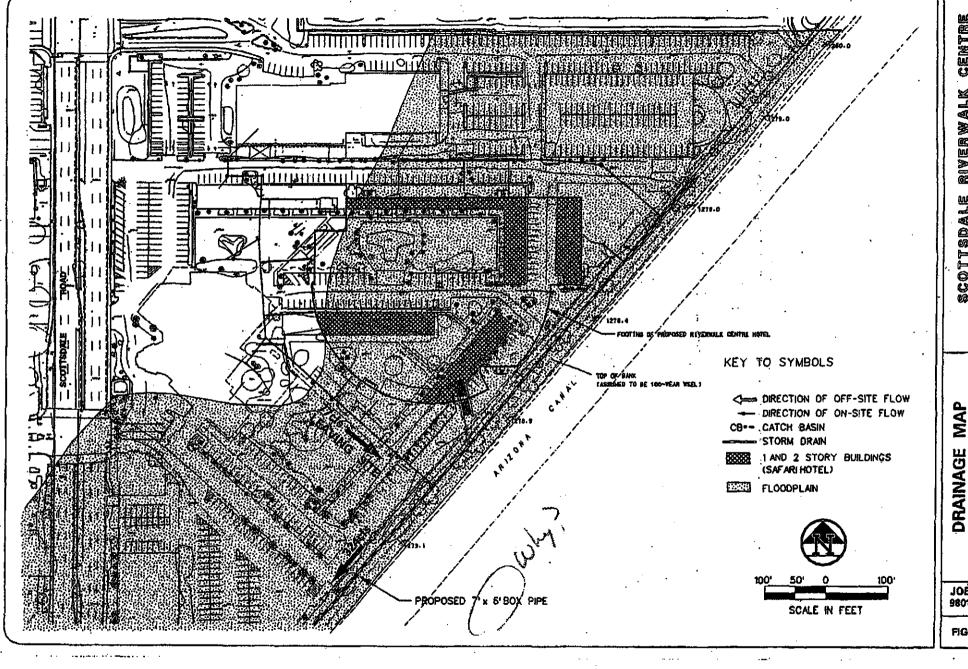
Runoff from the areas north of the property and west of Scottsdale Road flows south within Scottsdale Road, either within the street cross-section, or within an existing 42-inch storm drain system. These areas are currently under construction and it is anticipated that with future drainage improvements in place, the runoff reaching Scottsdale Road will be reduced. This storm drain interconnects with a 144-inch storm drain pipe structure which outfalls to the Indian Bend Wash along Camelback Road. According to the Storm Water Master Plans, under existing conditions during a 100-year, 6-hour storm event, approximately 3,638 cfs approaches the intersection of Scottsdale Road and Camelback Road. The box culvert outfall has capacity for approximately 1,000 cfs. Planned future drainage improvements include an additional storm drainage outfall along Camelback Road.



HAINAGE MAP
4550 MARTH 12TH STREET
PHOENX, ARZOWN 85014

JOB NO. 980121-03

PLATE 1



**DRAINAGE** 

CERTRE

RIVERWALK

SCOTTSDALE

JOB I 980121

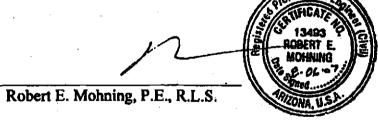
FIGUE

## **SCOTTSDALE FASHION SQUARE** PHASE 10

#### PRELIMINARY GRADING AND DRAINAGE REPORT

PREPARED FOR:

WESTCOR 1411 North Tatum Boulevard Phoenix, Arizona 85028 (602) 953-6379



August 7, 2007

RICK ENGINEERING COMPANY 6150 North 16<sup>TH</sup> Street Phoenix, Arizona 85016-1705

**JOB NUMBER 3750** 

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#### 1.0 INTRODUCTION

Scottsdale Fashion Square is located at the northwest corner of Scottsdale Road and Camelback Road. This preliminary drainage report addresses drainage for redevelopment of the easterly portion of Scottsdale Fashion Square bounded on the east by Scottsdale Road, on the south by Camelback Road, on the west by Goldwater Boulevard, and on the north by Highland Avenue, see vicinity map Appendix A

The total net area of this area within the four street rights of way is 35.33 acres. The purpose of this report is to discuss the existing and proposed onsite and offsite drainage for the redevelopment. The redevelopment will remove the former Robinson's-May store and adjoining parking structure, and add two new anchors, new retail and restaurant spaces, and underground parking.

#### 2.0 EXISTING DRAINAGE CONDITIONS AND CHARACTERISTICS

The Scottsdale Fashion Square site is fully developed with the retail mall, restaurants, a Days Inn Motel, office, and parking structures, see aerial photograph, Map Pocket 1.

Onsite drainage flows are generally from northwest to southeast. Onsite flows are intercepted by onsite catch basins or perimeter catch basins and are discharged into an existing 84 inch storm drain in Camelback Road and an existing 42 inch storm drain in Scottsdale Road. These two storm drain pipes connect to a 144 inch storm drain which drains east to the Indian Bend Wash.

All but a small portion of the site lies within Flood Zone "X" (textured) according to map number 04013C1695H of the FEMA Flood Information Map, dated September 30, 2005. A small area at the southeast corner of the site is within Flood Zone "A" because of the ponding of offsite flows against The Arizona Canal. An office building is located in this area and its finish floor is above the depth of the ponding.

Offsite drainage is from northwest to southeast toward the Arizona Canal. The site is higher than the elevation of the ponding at The Arizona Canal as described above.

#### 3.0 PROPOSED DRAINAGE PLAN

The drainage patterns of the redevelopment will be consistent with the existing drainage. No retention will be provided per the approved <u>Master Drainage Plan for Scottsdale Fashion Square</u>, Appendix C, and the site's location within the City of <u>Scottsdale Downtown Infrastructure Master Plan Volume 3 Drainage Study</u>. This study was prepared in December 1986 by Boyle Engineering Corporation and concludes that no detention/retention be provided for the downtown study area. The proposed redevelopment will not alter the amount of impervious area nor the volume or direction of storm water flows. See Preliminary Grading and Drainage Plan in Map Pocket 2.

#### 4.0 SPECIAL CONDITIONS

There are no special site conditions or need for a 404 permit. A Storm Water Pollution Prevention Plan will be prepared

#### MASTER DRAINAGE PLAN FOR SCOTTSDALE FASHION SQUARE C.V.W. No. 831114-21

Prepared for: THE WESTCOR COMPANY II, LIMITED PARTMERSHIP 11411 North Tatum Boulevard Phoenix, Arizona 85028

Prepared by: COLLAR, WILLIAMS & WHITE ENGINEERING 2702 North 44th Street, Suite 205-B Phoenix, Arizona 85008

RECEIVED
MASTER PLANNING

MAY 19 1988

BY FIRST ROVIDU

April, 1986 Approved by City of Scottsdale, August 18, 1986 Revised May 10, 1988

COLLAR, WILLIAMS & WHITE ENGINEERING

#### Drainage System

Scottsdale Fashion Square is an existing 35.0 acre shopping center located at the northwest corner of Camelback Road and Scottsdale Road in the City of Scottsdale, Arizona.

New development will occur on this site in multiple phases. These phases will include the demolition of some existing buildings, renovations to existing buildings, new office and commercial building construction, construction of new underground and elevated parking levels, and construction of a new retail bridge to connect Scottsdale Fashion Square to Camelview Plaza to the west. In addition, the proposed "West Couplet Roadway" alignment will be along the westerly boundary of the project.

Existing on-site surface drainage flows are, in general, from the northwest towards the south and east. All existing drainage flows are intercepted by existing on-site catch basins and discharged into an existing 84 inch diameter storm drain in Camelback Road and an existing 42 inch diameter storm drain in Scottsdale Road. These two storm drains connect at the intersection of Camelback and Scottsdale Roads and empty into an existing 144 inch diameter storm drain which conveys the water under the Arizona Canal and to the East towards Indian Bend Wash.

Existing building roof drainage is presently routed via vertical roof drain leader. lines to either existing on-site underground storm drainage systems or is discharged at existing grade and directed through existing curbing to the adjacent asphalt paved surfaces, where it sheet flows to existing storm drain inlets bordering the site.

As a part of the remodeling/renovating of existing buildings, additional floors will be added to the buildings. As additional floors are constructed, the existing vertical roof drain leader lines will be extended to the new roof levels. Future roof drainage from all new and renovated buildings will be connected

to on-site underground storm drainage systems, and all ongrade discharges will be eliminated.

There are no existing on-site storm water retention/detention facilities presently provided, and the new site development and modifications will not necessitate new on-site storm water retention/detention facilities (See attached letter from the City of Scottsdale dated December 8, 1987). Since the site is essentially impervious at this time, and will remain so after the redevelopment, no additional drainage flows will be generated.

A field survey made by Collar, Williams & White Engineering, of the top of the existing west bank of the Arizona Canal, indicates the elevations along the top of the existing west bank presently vary from 1378.0 feet to 1375.4 feet between the canal crossing at Highland Avenue and 500 feet south of the intersection of Scottsdale and Camelback Roads. With one foot of freeboard required above the maximum top of existing canal bank elevations, all new first floor building elevations have been established at no less than 1379.0. All existing building elevations are above this elevation. Both Camelback Road and Scottsdale Road are lower than elevation 1379.0.

New site development and modifications have incorporated adequate design measures to assure that no overflow of the Arizona Canal from a 100 year flood event will inundate any existing or proposed on-site building.

In addition, the new development has made adequate provisions to prevent any storm water from a 100 year event, which would flood the intersection of Camelback Raod and Scottsdale Road from entering any underground basement or lower parking level.

This assurance has been achieved by denying direct driveway access from Scottsdale Road or Camelback Road to the new underground parking levels, and by construction of walls around the office building at the southeast corner of the site to prevent flooding of the basement area.

APPENDIX G CLOMR-F

## **CLOMR-F**

## SCOTTSDALE BLUESKY

NOVEMBER 2011 DEA PROJECT NO. GRYD00001

## CLOMR-F APPLICATION FOR SCOTTSDALE BLUESKY

#### PREPARED FOR

## GRAY DEVELOPMENT 1400 E. CAMELBACK ROAD, SUITE 275 PHOENIX, AZ 85018

#### PREPARED BY

Paul Pal, P.E
Ramzi Georges, P.E, CFM
DAVID EVANS AND ASSOCIATES, INC.
4600 E WASHINGTON STREET, SUITE 430
PHOENIX, AZ 85034
(602) 678-5151

November 2011 DEA PROJECT NO. GRYD00001

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| 3.0          | FEMA FORMS                              |            |          |
| 4.0          | EXHIBITS                                |            | 2        |
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|              |   |            |          |
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#### 1.0 INTRODUCTION

This Conditional Letter of Map Revision based on Fill (CLOMR-F) has been prepared under a contract with Gray Development, LLC, owner and developer of the Blue Sky Scottsdale project.

The Blue Sky Scottsdale project is comprised of 3± acres within Section 23, Township 2 North, Range 4 East of the Gila and Salt River Base and Meridian. The current improvements include fill material to remove the site from the flood plain. The future Blue Sky Scottsdale project will be a mixed use development consist of 749 multi-family residential apartments with 91,000SF of commercial space, the commercial space will consists of 30,000SF grocery store, 15,000SF Restaurant, 13,000SF Retail, 28,000SF Club/fitness house, and 5,000SF office. There will be 4-levels of below grade parking that will provide approximately 1,511 parking spaces.

The area surrounding the site varies in use. The site is bounded by Coolidge Street to the North, Safari Drive condominium to the northeast, Arizona Canal to the east, Renaissance Center (commercial development) to the south and Scottsdale Road to the West. See Exhibit 1 Vicinity Map, in Appendix A. Access to the site will be provided via two entrances from Scottsdale Road along 72nd Place and Coolidge Street.

Site grading is designed to elevate the site above the base flood elevation, during the local 100-year storm event. This will allow for the site to be removed from the flood plain.

#### 2.0 FIRM PANEL

Based on the effective FEMA Flood Insurance Rate Map at the time of design (FIRM Map Number 04013C1695H, Map Revised September 30, 2005, see Appendix D, Exhibits 2 and 3), the site is located in flood hazard Zone "A" and Zone "X". Zone A is defined as the flood insurance rate zone that corresponds to the 100-year floodplains that are determined in the Flood Insurance Study by approximate methods. Because detailed hydraulic analyses are not performed for such areas, no Base Flood Elevations or depths are shown within this zone. Zone X is defined as "areas of 500-year flood; areas of 100-year flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from the 100-year flood."

#### 3.0 FEMA FORMS

The following documentation is enclosed as part of the CLOMR-F application:

a) FEMA Payment – FEMA Form 81-107 provides documentation of payment from Gray Development (see Appendix A). A check in the amount of \$800 is made out to the National Flood Insurance Program (NFIP) and enclosed for the Scottsdale BlueSky CLOMR-F application.

- b) **FEMA CLOMR-F Application** The FEMA MT-1 application is comprised of three forms (see Appendix B). The three forms include:
  - i) Property Information Form (MT-1 Form 1)
    - Documents the type of application and specific property information.
  - ii) Elevation Form (MT-1 Form 2)
    - Lists pad and top of curb elevations for lots of concern.
  - iii) Community Acknowledgment Form (MT-1 Form 3)
    - Provides documentation of local community consent.

#### 4.0 EXHIBITS

- 1. Vicinity Map This exhibit shows the site and area surrounding this project.
- 2. FIRM Panel FEMA Flood Insurance Rate Map encompassing the project site.
- 3. Firmette Focused exhibit addressing the locale of interest. The Firmette is a portion of the above mentioned FIRM panel and indicates the BlueSky project boundaries.
- 4. **FEMA TB10-01** FEMA guidelines for ensuring that structures on fill in or near special flood hazard areas are reasonably safe from flooding (provided for reference).

#### 5.0 PRELIMINARY DRAINAGE REPORT

The purpose of the preliminary drainage report is to provide hydraulic analysis, in support of the improvement plans raising the site above the floodplain as required by the City of Scottsdale. It is enclosed here in support of the CLOMR-F application and has been prepared in accordance with procedures detailed in the City of Scottsdale Design Standards and Policies Manual along with the City of Scottsdale Supplement to MAG Uniform Standard Specifications For Public Works Construction and Drainage Design Manuals for Maricopa County, Arizona, Volumes II See the Preliminary Drainage Report Table of Contents for a detailed list of contents and listed references.

**APPENDIX A: FEMA FORM 81-107** 

## FEDERAL EMERGENCY MANAGEMENT AGENCY PAYMENT INFORMATION FORM

| Community Name: City of Sco  | ttsdale, Arizona                  |                  |  |                  | <del></del>   |      |
|--|-----------------------------------|------------------|--|------------------|---------------|------|
| Project Identifier: BlueSky Sc   |                                   |                  |  |                  |               |      |
| THIS FORM MUST BE MAILED, AI   | <del>,=</del>                     | PRIATE FEE       | TO THE ADDRESS BELOW OF  | R FAXED TO THE F | AX NUMBER BEI | OW.  |
| Type of Request:   |                                   | 1 100 11 2 1 22, | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,  |                  |               |      |
| ·  | MT-1 application MT-2 application | }                | Company Compan |                  |               |      |
|  | ☐ EDR application                 | }                | FEMA Project Library<br>847 South Pickett St.<br>Alexandria, VA 22304<br>FAX (703) 212-4090  |                  |               |      |
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| ADDRESS: (for your credit card receipt-please print or type)                                 |                                   |                  | -<br>-   |                  |               |      |
| DAYTIME PHONE:   | <del></del>                       | _                |  |                  |               |      |

**APPENDIX B: FEMA FORM MT-1** 

## DEPARTMENT OF HOMELAND SECURITY - FEDERAL EMERGENCY MANAGEMENT AGENCY ELEVATION FORM

O.M.B. NO. 1660-0015 Expires February 28, 2014

#### PAPERWORK BURDEN DISCLOSURE NOTICE

Public reporting burden for this data collection is estimated to average 1.25 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing and submitting the form. This collection is required to obtain or retain benefits. You are not required to respond to this collection of information unless a valid OMB control number is displayed on this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, Department of Homeland Security, Federal Emergency Management Agency, 1800 South Bell Street, Arlington, VA 20598-3005, Paperwork Reduction Project (1660-0015). NOTE: Do not send your completed form to this address.

| or, if the request involves an an rounded to nearest tenth of a fresult in processing delays.  1. NFIP Community Numb  2. Are the elevations liste  3. For the existing or prop  | p Elevation Certificate ure on natural grade O including an attached ea described by metes boot. In order to proces  per: 045012 Prope d below based on  osed structures liste e  slab on grade [ ied this area as subject date of the current r atum? NGVD 29 listed below were co | rty Name or A  existing or  dect to land sub- ect to land | d fill from the Special File. For requests to remove ovide the lowest elevate all information on this faddress: 4601 N SCO  proposed condition to the condition of the condition | for single structure relood Hazard Area (SFI lood Hazard Hazard  TTSDALE RD, SCOT lood Hazard  TTSDALE RD, SCOT lood Hazard  TTSDALE RD, SCOT lood Hazard  TTSDALE RD, SCOT  Instructions? (Check one)  Instructions? (check (explain)  Lood Hazard  Lood | requests.  HA), submit the lowest if land from the SFHA, properties and bounds description eted in its entirety. Incomplete in its entirety.  TSDALE, AZ- 85251  all that apply)  Yes \( \sum \) No | adjacent grade (the lowest<br>rovide the lowest lot elevation;<br>n. All measurements are to be<br>omplete submissions will |
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| If yes, what is the  | listed below were co  | omputed using  | g a datum different t  | -   | d for the effective Fl  | ood Insurance Rate Map  |
| What is the elevation datum? NGVD 29 NAVD 88 Other (explain) If any of the elevations listed below were computed using a datum different than the datum used for the effective Flood Insurance Rate Map (FIRM) (e.g., NGVD 29 or NAVD 88), what was the conversion factor?   |   |  |  |   |   |   |
| Local Elevation +/- ft. = FIRM Datum  5. Please provide the Latitude and Longitude of the most upstream edge of the <i>structure</i> (in decimal degrees to the nearest fifth decimal place):  Indicate Datum: WGS84 NAD83 NAD27 Lat. 33 . 504996 Long. 111 . 925655  Please provide the Latitude and Longitude of the most upstream edge of the <i>property</i> (in decimal degrees to the nearest fifth decimal place):  Indicate Datum: WGS84 NAD83 NAD27 Lat. 33 . 505384 Long. 111 . 925053 |   |  |  |   |   |   |
| Address  | Lot Number  | Block<br>Number  | 1  |   | Base Flood<br>Elevation   | BFE Source  |
| 4601 N SCOTTSDALE RD,<br>SCOTTSDALE  | Commercial  | n/a  | 72.35  | n/a   | 79.50   | Survey Information  |
|  |   |  |  |   | <u> </u>  |   |
| This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001.  |   |  |  |   |   |   |
| Certifier's Name: Ramzi Georges, P.E, CFM License No.: 37287 Expiration Date: March 31, 2014   |   |  |  |   | March 31, 2014  |   |
| ompany Name: David Evans & Associates Telephone No.: 602-474-9223  |   |  |  |   |   |   |
| naìl: ryg@deainc.com Fax No.   |   |  |  |   |   |   |
| Signature:   | nature: Date:   |  |  |   |   |   |
| * For requests involving a portion of property, include the lowest ground elevation within the metes and bounds description.  Please note: If the Lowest Adjacent Grade to Structure is the only elevation provided, a determination will be issued for the structure only.  |   |  |  |   |   | eal (optional)  |

|   |              | (            | Continued from Page      | 1.                                       |                         |                                       |
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| Address   | Lot Number   | Block Number | Lowest Lot<br>Elevation* | Lowest Adjacent<br>Grade To<br>Structure | Base Flood<br>Elevation | BFE Source                            |
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| This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001. |              |              |                          |  |                         |                                       |
| Certifier's Name:   | <del>-</del> |              | License No.:             | · · · · · · · · · · · · · · · · · · ·    | Expiration Date:        |                                       |
| Company Name:   |              |              | Telephone Na.:           |  |                         | 1                                     |
| Email:  |              | ,            | Fax No.                  | <del>.</del>                             | <b></b>                 | ` I                                   |
| Signature:  |              |              | Date:                    |  |                         | ,                                     |
| * For requests involving a portion of property, include the lowest ground elevation within the metes and bounds description.  Please note: If the Lowest Adjacent Grade to Structure is the only elevation provided, a determination will be issued for the structure only.   |              |              |                          |  | al (optional)           |                                       |

## DEPARTMENT OF HOMELAND SECURITY - FEDERAL EMERGENCY MANAGEMENT AGENCY PROPERTY INFORMATION FORM

O.M.B. NO. 1660-0015 Expires February 28, 2014

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| Lett<br>Rev              | er of Map Amend<br>ision Based on Fill                       | ment (LOMA), Conditional Let<br>(CLOMR-F) for existing or pro                                 | ter of Map Amendment (CLOM/<br>posed, single or multiple lots/st | ed land surveyor, or registered professionals), Letter of Map Revision Based on Fill (LOF ructures. In order to process your request, esult in processing delays. Please check the | MR-F), or Conditional Letter of Map<br>all information on this form must be |  |  |
|                          | LOMA .   |   |  | tating that an existing structure or par<br>ade) would not be inundated by the ba  |   |  |  |
|                          | CLOMA  |   |  | tating that a proposed structure that is dated by the base flood if built as prop  |   |  |  |
|                          | LOMR-F   | ·   | A letter from DHS-FEMA s<br>fill would not be inundate           | tating that an existing structure or pard by the base flood.   | cel of land that has been elevated by                                       |  |  |
| ☒                        | CLOMR-F  |   |  | tating that a parcel of land or <b>propose</b> od by the base flood if fill is placed on tised.  |   |  |  |
| con<br>pra<br><b>Pro</b> | struction practice<br>ctice does not alte<br>gram (NFIP) map | of removing unsuitable existing the existing (natural grade) of showing the area in a Special | ng material (topsoil) and backfilli                              | nat raises the ground to or above the Base Fing with select structural material is not conne BFE. Fill that is placed before the date on sidered natural grade.                    | sidered the placement of fill if the  |  |  |
|                          |  | on your property to raise eviously below the BFE?   | Yes No   | If yes, when was fill placed?  | /<br>month/year   |  |  |
|                          | Il fill be placed on   | n your property to raise<br>w the BFE?  |  | If yes, when will fill be placed?<br>cies Act (ESA) compliance must be doc<br>nation (please refer page 4 to the MT-1  | 01/2012<br>month/year<br>umented to FEMA prior to issuance                  |  |  |
| 1.                       | street names b   |   | ·  | units, please attach additional sheet re   | eferencing each address and enter   |  |  |
| 2.                       | A PORTION  | OF TRACK 'A' OF PARA  |  | lescription from the Deed):<br>CORDED IN BOOK 46, PAGE 26, F<br>WNSHIP 2 NORTH, RANGE 4 EAS  |   |  |  |
| 3.                       | Are you reque  | sting that a flood zone dete  | ermination be completed for                                      | (check one):   |   |  |  |
|                          |  | Structures on the proper  | ty? What are the dates of co                                     | onstruction? 07/2012 (MM/YYYY)   | •   |  |  |
|                          |  | removed, certified by a li  |  | (A certified metes and bounds descript<br>stered professional engineer, are requi<br>T-1 Form 1 Instructions.)   |   |  |  |
|                          | $\boxtimes$  | The entire legally records  | ed property?   |  | •   |  |  |
| 4.                       | Is this request  | for a (check one): Single structure   |  |  |   |  |  |
|                          | $\boxtimes$  | Single lot  |  |  |   |  |  |
| :<br>İ                   |  | •   | •  | d in your request? List the number: 3)   |   |  |  |
|                          |  | Multiple lots (How many lots are involved in your request? List the number:                   |  |  |   |  |  |

| ion to this form (MT-1 Form 1), please complete the checklist below. ALL requests must include one copy of the following:  |
|--|
| Copy of the effective FIRM panel on which the structure and/or property location has been accurately plotted (property inadvertently located in the NFIP regulatory floodway will require Section B of MT-1 Form 3)  |
| Copy of the Subdivision Plat Map for the propert <b>y (with recordation data and stamp of the Recorder's Office)</b> OR  |
| Copy of the Property Deed (with recordation data and stamp of the Recorder's Office), accompanied by a tax assessor's map or other certified map showing the surveyed location of the property relative to local streets and watercourses. The map should include at least one street intersection that is shown on the FIRM panel.  |
| Form 2 – Elevation Form. If the request is to remove the structure, and an Elevation Certificate has already been completed for this property, it may be submitted in lieu of Form 2. If the request is to remove the entire legally recorded property, or a portion thereof, the lowest lot elevation must be provided on Form 2.   |
| Please include a map scale and North arrow on all maps submitted.  |
| 1R-Fs and CLOMR-Fs, the following must be submitted in addition to the items listed above:   |
| Form 3 – Community Acknowledgment Form   |
| MR-Fs, the following must be submitted in addition to the items listed above:  |
| Documented ESA compliance, which may include a copy of an Incidental Take Permit, an Incidental Take Statement, a "not likely to adversely affect" determination from the National Marine Fisheries Service (NMFS) or the U.S. Fish and Wildlife Service (USFWS), or an official letter from NMFS or USFWS concurring that the project has "No Effect" on proposed or listed species or designated critical habitat. Please refer to the MT-1 instructions for additional information. |
| Please do not submit original documents. Please retain a copy of all submitted documents for your records.   |
| DHS-FEMA encourages the submission of all required data in a digital format (e.g. scanned documents and images on Compact Disc (CD)). Digital submissions help to further DHS-FEMA's Digital Vision and also may facilitate the processing of your request.  |
| complete submissions will result in processing delays. For additional information regarding this form, including where to obtain the supporting documents ted above, please refer to the MT-1 Form instructions located at <a href="http://www.fema.gov/plan/prevent/fhm/dl">http://www.fema.gov/plan/prevent/fhm/dl</a> mt-1.shtm.  |
| ֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜֜  |

## DEPARTMENT OF HOMELAND SECURITY - FEDERAL EMERGENCY MANAGEMENT AGENCY ELEVATION FORM

O.M.B. NO. 1660-0015 Expires February 28, 2014

#### PAPERWORK BURDEN DISCLOSURE NOTICE

Public reporting burden for this data collection is estimated to average 1.25 hours per response. The burden estimate includes the time for reviewing instructions, searching existing data sources, gathering and maintaining the needed data, and completing and submitting the form. This collection is required to obtain or retain benefits. You are not required to respond to this collection of information unless a valid OMB control number is displayed on this form. Send comments regarding the accuracy of the burden estimate and any suggestions for reducing this burden to: Information Collections Management, Department of Homeland Security, Federal Emergency Management Agency, 1800 South Bell Street, Arlington, VA 20598-3005, Paperwork Reduction Project (1660-0015). NOTE: Do not send your completed form to this address.

This form must be completed for requests and must be completed and signed by a registered professional engineer or licensed land surveyor. A DHS - FEMA National Flood Insurance Program (NFIP) Elevation Certificate may be submitted in lieu of this form for single structure requests.

For requests to remove a structure on natural grade OR on engineered fill from the Special Flood Hazard Area (SFHA), submit the lowest adjacent grade (the lowest ground touching the structure), *including an attached deck or garage*. For requests to remove an entire parcel of land from the SFHA, provide the lowest lot elevation; or, if the request involves an area described by metes and bounds, provide the lowest elevation within the metes and bounds description. All measurements are to be rounded to nearest tenth of a foot. In order to process your request, all information on this form must be completed *in its entirety*. Incomplete submissions will result in processing delays.

| resu  | sult in processing delays.   |   |               |                          |                  |                       |                       |
|---|--|---|---------------|--------------------------|------------------|-----------------------|-----------------------|
| 1.  | NFIP Community Number:   | 045012 Prope  | rty Name or A | ddress: 4601 N SCOTT     | SDALE RD, SCOTTS | DALE, AZ- 85251       |                       |
| 2.  | Are the elevations listed below based on existing or proposed conditions? (Check one)  |   |               |                          |                  |                       |                       |
| 3.  | For the existing or proposed structures listed below, what are the types of construction? (check all that apply)  ☐ crawl space ☐ slab on grade ☐ basement/enclosure ☐ other (explain)   |   |               |                          |                  |                       |                       |
| 4.  | Has DHS - FEMA identified this area as subject to land subsidence or uplift? (see instructions)  |   |               |                          |                  |                       |                       |
| 5.  | What is the elevation datur<br>If any of the elevations liste<br>(FIRM) (e.g., NGVD 29 or NA   | d below were co   | omputed using | g a datum different tha  |                  | for the effective Flo | od insurance Rate Map |
|   |  |   | Local         | Elevation +/- ft. = FIRM | /I Datum         |                       |                       |
| 6.  | 6. Please provide the Latitude and Longitude of the most upstream edge of the <i>structure</i> (in decimal degrees to the nearest fifth decimal place):  Indicate Datum: WGS84 NAD83 NAD27 Lat. 33 . 504996 Long. 111 . 925655 |   |               |                          |                  |                       |                       |
|   | Please provide the Latitude and Longitude of the most upstream edge of the <i>property</i> (in decimal degrees to the nearest fifth decimal place):  Indicate Datum: WGS84 NAD83 NAD27 Lat. 33 . 505384 Long. 111 . 925053     |   |               |                          |                  |                       |                       |
|   | Address  | Lowest  Block Lowest Lot Adjacent  Lot Number Number Elevation* Grade To  Structure |               | Base Flood<br>Elevation  | BFE Source       |                       |                       |
|   | 1 N SCOTTSDALE RD,<br>TTSDALE  | Commercial  | n/a           | 72.35                    |                  | 79.50                 | Survey Information    |
|   |  |   |               |                          |                  |                       |                       |
| This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1001. |  |   |               |                          |                  |                       |                       |
| Certifler's Name: Ramzi Georges, P.E, CFM License No.: 37287 Expiration Date: March 31, 2014  |  |   |               |                          | March 31, 2014   |                       |                       |
| Con   | Company Name: David Evans & Associates Telephone No.: 602-474-9223   |   |               |                          | 4-9223           |                       |                       |
| Ema   | mail: ryg@deainc.com Fax No.   |   |               |                          |                  |                       |                       |
| Sign  | ignature: Date:  |   |               |                          |                  |                       | L                     |
|   | * For requests involving a portion of property, include the lowest ground elevation within   |   |               |                          |                  |                       |                       |
| P   | the metes and bounds description.  Please note: If the Lowest Adjacent Grade to Structure is the only elevation provided, a determination will be issued for the structure only.   |   |               |                          | Se               | al (optional)         |                       |

| Address Lot Number Block Number Clevest Lot Clevest Lot Grade To Structure Bese Flood Elevention    Lot Number   Block Number   Lovest Lot Grade To Structure   Bese Flood Elevention  |  |            |              | continued from Page | 1.          |                  |            |
|--|--|------------|--------------|---------------------|-------------|------------------|------------|
| This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or imprisonment under Title 18 of the United States Code, Section 1021.  Certifier's Name:  License No.  Email:  Fax No.  Signature:  Date:                                    | Address  | Lot Number | Block Number |                     | Grade To    |                  | 8FE Source |
| This certification is to be signed and sealed by a licensed land surveyor, registered professional engineer, or architect authorized by law to certify elevation information. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable by fine or improment under Title 18 of the United States Code, Section 1001.  Certifier's Name:  Usense No:  Expiration Date:  Usense No:  Expiration Date:                            |  |            |              |                     |             |                  |            |
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| Company Name: Telephone No.:  Email: Fax No.  Signature: Date:   | information. All documents submitted in support of this request are correct to the best of my knowledge. I understand that any false statement may be punishable |            |              |                     |             |                  |            |
| Email: Fax No. Signature: Date:  | Certifier's Name:  |            |              | License No.:        |             | Expiration Date: |            |
| Signature: Date:   | Company Name:  | -          |              | Telephone No.:      |             |                  | 1          |
|  | Email:   |            |              | Fax No.             |             | 7                |            |
|  |  |            |              |                     |             | <b></b>          |            |
| * For requests involving a portion of property, include the lowest ground elevation within the metes and bounds description.  Please note: If the Lowest Adjacent Grade to Structure is the only elevation provided, a determination will be issued for the structure only.  | l (optional)   |            |              |                     |             |                  |            |

## DEPARTMENT OF HOMELAND SECURITY - FEDERAL EMERGENCY MANAGEMENT AGENCY COMMUNITY ACKNOWLEDGMENT FORM

O.M.B. NO. 1660-0015 Expires February 28, 2014

#### **PAPERWORK BURDEN DISCLOSURE NOTICE**

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This form must be completed for requests involving the existing or proposed placement of fill (complete Section A) **OR** to provide acknowledgment of this request to remove a property from the SFHA which was previously located within the regulatory floodway (complete Section B).

This form must be completed and signed by the official responsible for floodplain management in the community. The six digit NFIP community number and the subject property address must appear in the spaces provided below. Incomplete submissions will result in processing delays. Please refer to the MT-1 instructions for additional information about this form.

Community Number: \_

Community Comments:

**Property Name or Address:** 4601 N SCOTTSDALE RD, SCOTTSDALE 85251

#### A. REQUESTS INVOLVING THE PLACEMENT OF FILL

As the community official responsible for floodplain management, I hereby acknowledge that we have received and reviewed this Letter of Map Revision Based on Fill (LOMR-F) or Conditional LOMR-F request. Based upon the community's review, we find the completed or proposed project meets or is designed to meet all of the community floodplain management requirements, including the requirement that no fill be placed in the regulatory floodway, and that all necessary Federal, State, and local permits have been, or in the case of a Conditional LOMR-F, will be obtained. For Conditional LOMR-F requests, the applicant has or will document Endangered Species Act (ESA) compliance to FEMA prior to issuance of the Conditional LOMR-F determination. For LOMR-F requests, I acknowledge that compliance with Sections 9 and 10 of the ESA has been achieved independently of FEMA's process. Section 9 of the ESA prohibits anyone from "taking" or harming an endangered species. If an action might harm an endangered species, a permit is required from U.S. Fish and Wildlife Service or National Marine Fisheries Service under Section 10 of the ESA. For actions authorized, funded, or being carried out by Federal or State agencies, documentation from the agency showing its compliance with Section 7(a)(2) of the ESA will be submitted. In addition, we have determined that the land and any existing or proposed structures to be removed from the SFHA are or will be reasonably safe from flooding as defined in 44CFR 65.2(c), and that we have available upon request by DHS-FEMA, all analyses and documentation used to make this determination. For LOMR-F requests, we understand that this request is being forwarded to DHS-FEMA for a possible map revision.

Community Official's Name and Title: (Please Print or Type)

C. Ashley Couch, PE, CFM, Stormwork Manager and Pleadplan Administrator 480-312-4317

Community Name:

City of Scottsdale, Arizona

Community Official's Signature: (required)

Date:

1/12/2012

#### **B. PROPERTY LOCATED WITHIN THE REGULATORY FLOODWAY**

As the community official responsible for floodplain management, I hereby acknowledge that we have received and reviewed this request for a LOMA. We understand that this request is being forwarded to DHS-FEMA to determine if this property has been inadvertently included in the regulatory floodway. We acknowledge that no fill on this property has been or will be placed within the designated regulatory floodway. We find that the completed or proposed project meets or is designed to meet all of the community floodplain management requirements.

Community Comments: N/A

| Community Official's Name and Title: (Please Print or | Туре)                                      | Telephone No.: |
|---|--|----------------|
| Community Name:                                       | Community Official's Signature (required): | Date:          |
|   |  |                |

## APPENDIX H WARNING AND DISCLAIMER LIABILITY FORM



# Appendix 4-C Warning and Disclaimer of Liability

The Drainage and Floodplain Regulations and Ordinances of the City of Scottsdale are intended to "minimize the occurrence of losses, hazards and conditions adversely affecting the public health, safety and general welfare which might result from flooding caused by the surface runoff of rainfail" (Scottsdale Revised Code §37-16).

As defined in S.R.C. §37-17, a flood plain or "Special flood hazard area means an area having flood and/or flood related erosion hazards as shown on a FHBM or FiRM as zone A. AO, A1-30, AE, A99, AH, or E, and those areas identified as such by the floodplain administrator, delineated in accordance with subsection 37-18(b) and adopted by the floodplain board." It is possible that a property could be inundated by greater frequency flood events or by a flood greater in magnitude than a 100-year flood. Additionally, much of the Scottadale area is a dynamic flood area; that is, the floodplains may shift from one location to another, over time, due to natural processes.

WARNING AND DISCLAIMER OF LIABILITY PURSUANT TO S.R.C §37-22

The degree of flood protection provided by the requirements in this article is considered researable for regulatory purposes and is based on scientific and engineering considerations. Floods larger than the base flood can and will occur on rare occasions. Floodwater heights may be increased by manmade or natural causes. This article (Chapter 37, Article II) shall not create liability on the part of the city, any officer or employee thereof, or the federal government for any flood damages that result from reliance on this article or any administrative decision lawfully made thereunder."

Compilance with Drainage and Floodplain Regulations and Ordinances does not insure complete protection from flooding. The Floodplain Regulations and Ordinances meet established local and federal standards for floodplain management, but neither this review nor the Regulations and Ordinances take into account such flood related problems as natural erosion, streambed meander or man-made obstructions and diversions, all of which may have an adverse affect in the event of a flood. You are advised to consult your own engineer or other expert regarding these considerations.

| I have read and ur | iderstand the above. If | l am en ag | ent for an own | <b>er I have made the</b> | OWNE |
|--------------------|-------------------------|------------|----------------|---------------------------|------|
| aware of and expla | ained this disclaimer.  |            |                | · .                       |      |
|                    | •                       | <i>7</i> · |                |                           |      |

Plan Check No.

11/21/11 Date

### APPENDIX I 404 CERTIFICATION



### **Section 404 Certification**

Before the City issues development permits for a project, the developer's Engineer or the property owner must certify that it complies with, or is exempt from, Section 404 of the Clean Water Act of the United States. Section 404, administered by the U.S. Army Corps of Engineers (COE), regulates the discharge of dredged or fill material into a wetland, lake, (including dry lakes), river, stream (including intermittent streams, ephemeral washes, and arroyos), or other waters of the United States.

Prior to submittel of improvement plans to Project Review the form below must be completed (and submitted with

| the improvement plans) as evidence of compliance   |
|--|
| Certification of Section 404 Permit Status   |
| Owner's Name: Gray Development Phone No. 602-508-7/41  Project Name/Description: Blue sky Scotts date. Case No. 396-PA-2010  Project Location/Address: South east Corner of Casticlye Rd & Scotts date. Rd  A registered Engineer or the property Owner must check the applicable condition and certify by signing |
| below that:  |
| <ol> <li>Section 404 <u>does</u> apply to the project because there will be a discharge of dredged or fill material to<br/>waters of the U.S., and:</li> </ol>   |
| A Section 404 Permit has already been obtained for this project.   |
| -or-   |
| This project qualifies for a "Nationwide Permit," and this project will meet all terms and conditions of the applicable nationwide permit.   |
| 2. Section 404 does not apply to the project because:  |
| No watercourses or other waters of the U.S. exist on the property.   |
| No jurisdictional waters of the U.S. exist on the property. Attached is a copy of the COE's Jurisdictional Determination.  |
| Watercourses or other waters of the U.S. do exist on the property, but the project will not involve the discharge of dredged or fill material into any of these waters.  |
| I cartify that the above statement is true.  |
| Engineer's Signature and Seal, or Owner's Signature  |
| Title Company Exp: 3-31-2614   |
| Planning & Development Services Department   |

7447 E Indian School Road, Suite 100, Scottsdale, AZ 85251 • Phone: 480-312-2500 • Fax: 480-312-7088