Exterior Building Color & Material Samples
Color Drawdowns
Archaeological Resources
Airport Vicinity Development Checklist
Parking Study
Trip Generation Comparison
Parking Master Plan



# CERTIFICATE OF NO EFFECT ARCHAEOLOGICAL RESOURCES

# 11-ZN-2017 7676 E Pinnacle Peak

#### APPLICATION INFORMATION

LOCATION: 7676 E Pinnacle Peak Rd

APPLICANT: Nick Wood

PARCEL:

212-04-001C

Snell & Wilmer L.L.P.

Q.S.:

45-46

ADDRESS:

COMPANY:

400 E Van Buren St Phoenix, AZ 85004

PHONE:

602-382-6269

Request by owner for a Zoning District Map Amendment from Service Residential, Environmentally Sensitive Lands (S-R ESL) zoning district, to Single-family Residential, Environmentally Sensitive Lands (R1-10 ESL) zoning district, on a +/- 19.7-acre site, located at 7676 E. Pinnacle Peak Road (incudes parcels 212-04-001B, 212-04-001C, 212-04-001D, and 212-04-001E).

#### **Certificate of No Effect Criteria:**

In accordance with Chapter 46, Article VI, of the Scottsdale Revised City Code, the Historic Preservation Officer finds that:

 No archaeological resources are located on the property according to the archaeological survey and report and based upon the city's review of the report.

#### **STIPULATIONS**

 Any development on the property is subject to the requirements of Scottsdale Revised Code, Chapter 46, Article VI, Protection of Archaeological Resources, Section 46-134 - Discoveries of archaeological resources during construction.

SIGNATURE:

DATE:

August 29, 2017

Steve Venker, City Archaeologist 480-312-2831

Steve Venker



# Class III Cultural Resources Survey of 20 Acres at the Northeast Corner of Pinnacle Peak Road and Miller Road for Wok HoldCo, LLC, in Scottsdale, Maricopa County, Arizona

Submitted to:

Wok HoldCo, LLC 7676 E. Pinnacle Peak Rd Scottsdale, AZ 85255

Prepared by: Jordan Myers, M.A., RPA

Technical Report 17-119 August 9, 2017

602.261.7253 | paleowest.com | 319 E. Palm Lane | Phoenix, AZ 85004

11-ZN-2017 08/18/2017

3-GP-2017 08/18/2017

Section 1. Report Title

1a. Report Title: Class III Cultural Resources Survey of 20 Acres at the

Northeast Corner of Pinnacle Peak Road and Miller Road for Wok HoldCo, LLC, in Scottsdale, Maricopa

County, Arizona

1b. Report Author(s):

Jordan Myers, M.A., RPA

1c. Date:

8/9/2017

1d. Report No.:

17-119

Section 2. Project Registration/Permits

2a. ASM Accession Number:

N/A

2b. AAA Permit No.:

2017-12bl

2c. ASLD Lease Application No.: N/A

2d. Other Permit Number(s): N/A

Section 3. Organization/Consulting Firm

3a. Name:

PaleoWest Archaeology

3b. Internal Project Number:

17-205

3c. Internal Project Name:

PF Chang's Class III Scottsdale

3d. Contact Name:

Chris North

3e. Contact Address:

319 E. Palm Lane, Phoenix AZ 85004

3f. Contact Phone:

602 261-7253

3g. Contact Email:

cnorth@paleowest.com

Section 4. Sponsor/Lead Agency

4a. Sponsor:

Wok HoldCo, LLC

4b. Lead Agency:

City of Scottsdale

4c. Agency Project Number(s):

N/A

4d. Agency Project Name:

N/A

4e. Funding Source(s):

Private

4f. Other Involved Agencies:

N/A

4g. Applicable Regulations:

COS Revised Code, Ord. No. 3243, § 2, 7-13-99

# Section 5. Description of Project or Undertaking:

Wok HoldCo, LLC, requested that PaleoWest conduct a Class III pedestrian survey of 20 acres of private land on the northeast corner of Pinnacle Peak Road and Miller Road for a proposed commercial development in Scottsdale, Maricopa County, Arizona.

# Section 6. Project Area/Area of Potential Effects:

The project area consists of 20 acres of privately-owned land at the northeast corner of Pinnacle Peak Road and Miller Road in Scottsdale, AZ. The project area measures a maximum of 395 meters by 185 meters.

| Section 7. | <b>Project</b> | Area In | formation: |
|------------|----------------|---------|------------|
|------------|----------------|---------|------------|

7a. Address:

7676 E. Pinnacle Peak Rd

7b. Route:

7c. Mileposts Limits: -

7d. Nearest City/Town: Scottsdale

7e. County: Maricopa

415154

7f. Project Locator UTMs: (NAD 83, Zone

mE

372930

mN

12)

7h. USGS

**7g. Baseline &** G&SRB&M **Meridian:** 

Quadrangle(s) Currys Corner

7i. Legal Description(s):SW ¼ of the SE ¼ of Section 11, T4N, R4E, Salt and Gila River
Baseline and Meridian

# Section 8. Survey Area

8a. Total Acres:

20

8b. Survey Area.

| 1. Land      | 2. Total Acres Surveyed | 3. Total Acres Not | 4. Justification for Areas Not |
|--------------|-------------------------|--------------------|--------------------------------|
| Jurisdiction |                         | Surveyed           | Surveyed                       |
| Private      | 15.6                    | 4.4                | Developed area                 |

# Section 9. Environmental Contexts

9a. Landform:

Alluvial floodplain

9b. Elevation:

1,902 feet above mean sea level

9c. Surrounding Topographic Features:

2.9 miles west of McDowell Mountains and

7.2 miles south of Black Mountain

| 9d. Nearest Drainag        | ge (Distance/Direction):             | Cave Creek is 7.66 miles to the northwest of the project area.                                |
|----------------------------|--------------------------------------|---|
| 9e. Local Geology:         |                                      | Holocene Surficial deposits (Arizona  |
| 06. 1/                     |                                      | Geological Survey 2013).  |
| 9f. Vegetation:            |                                      | Sonoran Desertscrub (Brown 1994): saguaro, barrel cactus, stag cholla,                        |
|                            |                                      | creosote, mesquite trees, paloverde, sage,  |
| 0 0 11 / 12 - 111          |                                      | grasses.  |
| 9g. Soils/Depositio        | n:                                   | Momoli gravelly sandy loam (USDA Natural Resources Conservation Service 2016)                 |
| 9h. Buried Deposits        | S:                                   | Not likely  |
| 9i. Justification:         |                                      | Few documented sites in vicinity, no  |
|                            |                                      | artifacts or features were observed within the project area.                                  |
|                            |                                      | the project area.   |
| Castian 10 Duile           | For decomposite                      |   |
| Section 10. Built          |                                      | Milley Deed, the court has Dispersely Deels Deed  |
|                            |                                      | Miller Road, the south by Pinnacle Peak Road<br>elopments. Within the project area is a large |
|                            |                                      | lots and sidewalks constructed in 1998.   |
|                            |                                      | ljacent to the project area.  |
|                            |                                      |   |
| Section 11. Inve           | ntory Class Compl                    | leted   |
| 11a. Class I Invent        | tory:                                | $\boxtimes$   |
| 11b. Researcher(s          | ):                                   | Jordan Myers, M.A., RPA   |
| 11c. Class II Surve        | ey:                                  | N/A   |
| 11d Sampling Stra          | tegy:                                | N/A   |
| 11e. Class III Inve        | entory:                              |   |
|                            |                                      |   |
| Section 12. Back           | ground Research                      | Sources   |
| 12a. AZSITE:               |                                      | $\boxtimes$   |
| 12b. ASM Archaeol          | ogical Records                       |   |
| Office:                    |                                      |   |
| 12c. SHPO Invento Library: | ries and/or SHPO                     |   |
| 12d. NRHP Databa           | se:                                  | $\boxtimes$   |
| 12e. ADOT Portal:          |                                      |   |
| 12f. GLO Maps:             | Plat 109520, filed 10/2              | 21/1915 depicts 10 separate roads, only one   |
|                            | of which is inside the p direction). | project area (running in an east/west   |
| 12a Land Managin           | ,                                    | N/A   |
| 12g. Land-Managir          | ig Agelicy Files:                    | N/A   |

12h. Tribal Cultural Resources Files: N/A

12i. Local Government Websites: City of Scottsdale Historic Register

(Scottsdale City Council 2013)

12j. Other: USGS maps: Currys Corner, Ariz. (1964) depicts 16 roads and three

transmission lines, all of which are outside the project area.

# Section 13. Background Research Results

| 13a. Previou                      | us Projects Within Study Are                    | a.                    |         |
|-----------------------------------|---|-----------------------|---------|
| 1. Project<br>Reference<br>Number | 2. Project Name                                 | 3. Author(s)          | 4. Year |
| 1987-                             | North Scottsdale                                | Recon                 | 1987    |
| 243.ASM                           | Reconnaissance                                  |                       |         |
| 1988-<br>39.ASM                   | Pinnacle Peak Substation<br>Extension           | Hoffman               | 1988    |
| 1989-<br>208.ASM                  | Core North Project                              | Breternitz and Landis | 1989    |
| 1993-<br>110.ASM                  | Landmark Land/Scottsdale<br>Road                | Woodall               | 1993    |
| 1994-<br>303.ASM                  | Ethan Bindelglas State Land<br>Survey, 53-53753 | Foster                | 1994    |
| 1996-<br>228.ASM                  | Scottsdale LaVista<br>Subdivision               | DeMaagd               | 1996    |
| 1997-<br>185.ASM                  | Pinnacle Peak and Miller<br>Roads               | Aguila                | 1997    |
| 1997-<br>221.ASM                  | Silverado Survey                                | Ryden                 | 1997    |
| 1998-<br>585.ASM                  | Desierto Vida II Survey                         | Ellis and Smith       | 1998    |
| 1999-<br>10.ASM                   | APS: Scottsdale Road and Happy Valley Road      | Moreno                | 1999a   |
| 1999-<br>130.ASM                  | Pinnacle Peak-Rawhide 69kV                      | Moreno                | 1999b   |
| 2000-<br>84.ASM                   | Alameda and 76th Survey                         | Hackbarth             | 2000    |
| 2000-<br>238.ASM                  | Mardian Archaeology Survey                      | Bushée                | 2000    |
| 2000-<br>731.ASM                  | Pinnacle Cemetery Project                       | Giacobbe and Geller   | 2000    |
| 2001-3.ASM                        | Scottsdale: Williams Dr & Scottsdale Rd         | DeMaagd               | 2001    |
| 2001-<br>392.ASM                  | Arroyo Paradise<br>Archaeological Project       | Schroeder             | 2001    |
| 2001-<br>603.ASM                  | Happy Valley LLC Survey                         | Lundin                | 2001    |

# Section 13. Background Research Results

|                                   | us Projects Within Study Are   | d.                        |         |
|-----------------------------------|--|---------------------------|---------|
| 1. Project<br>Reference<br>Number | 2. Project Name  | 3. Author(s)              | 4. Year |
| 2001-<br>611.ASM                  | Cox Communications 2   | Webb                      | 2001    |
| 2002-<br>222.ASM                  | Hayden/Santa Catalina<br>Survey  | Hart                      | 2002    |
| 2003-<br>422.ASM                  | Adobe Development  | Hackbarth                 | 2002    |
| 2004-<br>114.ASM                  | 160ac SEC Scottsdale & Pinnacle Peak   | North, Ryden, and Schmidt | 2003    |
| 2004-<br>455.ASM                  | Deer Valley and Scottsdale<br>Road Survey  | Hackbarth                 | 2003    |
| 2004-<br>1721.ASM                 | Happy Valley Road and<br>Hayden Roads Survey   | Cogswell                  | 2004    |
| 2004-<br>671.ASM                  | COS Arsenic Pipeline   | Lausten                   | 2004    |
| 2004-<br>705.ASM                  | 75th Street and Pinnacle<br>Peak Road Survey   | Hart                      | 2003    |
| 2005-<br>951.ASM                  | Scottsdale and Pinnacle Peak<br>Roads Survey   | Marshall                  | 2005    |
| 2005-<br>984.ASM                  | Jomax & Hayden Roads<br>Survey   | Gage                      | 2004    |
| 2006-<br>217.ASM                  | Pinnacle Peak and Miller<br>Roads Survey   | Stahman                   | 2005    |
| 2006-<br>475.ASM                  | Miller Road and Williams<br>Drive Survey   | Gage                      | 2006    |
| 2006-<br>944.ASM                  | Pinnacle Peak Road   | Rapp                      | 2007    |
| 2007-<br>465.ASM                  | Line 2223 Year 2008 PIP  | Hesse                     | 2007    |
| 2008-<br>15.ASM                   | Scottsdale Sewer Main  | Jaime                     | 2008    |
| 2009-<br>488.ASM                  | Scottsdale Road<br>Improvement Project<br>(Thompson Peak Parkway to<br>Pinnacle Peak Road) | Hyman                     | 2009    |
| 2010-<br>333.ASM                  | AT&T H080-02   | Luchetta and Moses        | 2010    |
| 2010-<br>389.ASM                  | AT&T Mobility H075-01  | Moses and Luchetta        | 2010    |
| 2011-8.ASM                        | Scottsdale ARRA Survey   | Stubing                   | 2011    |
| 2011-<br>628.ASM                  | Sonoran Hills School Site in<br>Scottsdale   | Breternitz                | 2011    |

Section 13. Background Research Results

| 13a. Previo                       | us Projects Within Study A                       | rea.         |         |
|-----------------------------------|--|--------------|---------|
| 1. Project<br>Reference<br>Number | 2. Project Name                                  | 3. Author(s) | 4. Year |
| 2012-<br>528.ASM                  | Scottsdale Rd, Thompson<br>Peak to Pinnacle Peak | Cox          | 2012    |

13b. Previously Recorded Cultural Resources Within Study Area.

| 13b. I Teviously Recorded Cultural Resources Within Study Area. |   |  |                          |                            |                      |
|---|---|--|--------------------------|----------------------------|----------------------|
| 1. Site No./<br>Name  | 2. Affiliation  | 3. Site Type                             | 4. Eligibility<br>Status | 5. Associated Reference(s) | 6.<br>Inside<br>APE? |
| AZ U:5:238(ASM)   | Unknown   | Unknown                                  | Unknown                  | AZSITE                     | No                   |
| AZ U:5:253(ASM)   | Archaic (8000<br>B.CA.D. 200);<br>Hohokam (A.D.<br>200-1500);<br>Historic (A.D.<br>1500-1950) | Rock features<br>and artifact<br>scatter | Recommended eligible     | AZSITE                     | No                   |
| AZ U:5:280(ASM)   | Unknown   | Unknown                                  | Unknown                  | AZSITE                     | No                   |

13c. Historic Buildings/Districts/Neighborhoods.

| 1. Property Name or Address | 2. Year | 3. Eligibility<br>Status | 4.<br>Inside<br>APE? |
|-----------------------------|---------|--------------------------|----------------------|
| N/A                         | _       | _                        | _                    |

13d. Historic USGS Map and GLO Properties Within Study Area.

| 1. Property Description                                   | 2. Map Year | 3. Inside APE? |
|---|-------------|----------------|
| 1 GLO Road  | 1915        | Yes            |
| 9 GLO Roads   | 1915        | No             |
| 16 roads on USGS Currys Corner, Ariz. Map                 | 1964        | No             |
| Three transmission lines on USGS Currys Corner, Ariz. Map | 1964        | No             |

# Section 14. Cultural Contexts

**14a. Prehistoric Culture:** Paleoindian, Archaic, Hohokam

**14b. Protohistoric Culture:** Akimel O'odham (Pima), Xalychidom Piipash

(Maricopa), Yavapai

**14c. Indigenous Historic Culture:** Akimel O'Odham (Pima), Xalychidom Piipash

(Maricopa), and Yavapai

**14d. Euro-American Culture:** A.D. 1880-present

# Section 15. Field Survey Personnel

**15a. Principal Investigator:** Chris North, M.A., RPA **15b. Field Supervisor:** Jordan Myers, M.A., RPA

**15c. Crew:** Jordan Myers, M.A., RPA

**15d. Fieldwork Date(s):** 06/01/2017

# Section 16. Survey Methods

16a. Transect Intervals: \_\_20\_ m apart

**16b. Coverage (%):** 100 percent

**16c. Site Recording Criteria:** ASM (Fish 1995)

16d. Ground Surface Visibility: 76-99 percent

**16e. Observed Disturbances:** Commercial development and scattered modern

trash

# Section 17. Field Survey Results

17a. No Cultural Resources

17b. Isolated Occurrences (IOs)

Only:

17c. Number of IOs Recorded: N/A

#### 17d. Table of IOs.

| 1. IO                 | . IO 2 Description | 2 Data Banca | 4. UTMs  |   |
|-----------------------|--------------------|--------------|----------|---|
| Number 2. Description | 3. Date Range      | Easting      | Northing |   |
| N/A                   | _                  | _            | _        | _ |

# Section 18. Comments/Recommendations:

This Class III cultural resources survey was completed in compliance with COS Revised Code, Chapter 46, Article VI. Background research indicated that small portions along the project area margins were previously surveyed for projects related to the LaVista Subdivision (DeMaagd 1996), the COS Arsenic Pipeline (Lausten 2004), and a pavement preservation project (Stubing 2011). However, these surveys are more than 5 years old and do not meet current COS Historic Preservation Office standards. Wok HoldCo, LLC, therefore requested that PaleoWest conduct a full pedestrian survey of the 20-acre parcel of private land for proposed commercial development. Background research also identified one historic road that crosses in the project area; however, no evidence of the road was observed during the survey, and it was not evident on aerial images. No IOs were identified and no sites were encountered within the project area. It is recommended that the project proceed with a Certificate of No Effect.

| Section 19. Attachments  |  |  |
|--|--|--|
| 19a. Project Location Map:   |  |  |
| 19b. Land Jurisdiction Map:  |  |  |
| 19c. Background Research Map(s):   | ☐ (Figure 2)   |  |
| 19d. GLO Map(s):   | ☑ (Figure 2)   |  |
| 19e. Project Area Photograph(s):   |  |  |
| 19f. References:   |  |  |
| Section 20. Consultant Certifica   |  |  |
| I certify the information provided herein<br>all work meets applicable agency standa | n has been reviewed for content and accuracy and ards. |  |
| 0114   |  |  |
| Che Nor-   | Date: 6/7/2017   |  |
| Signature  |  |  |
|  |  |  |
| Principal Investigator   |  |  |
| Title  |  |  |

# Section 21. Discovery Clause

If previously unreported cultural resources are encountered during ground disturbing activities, all work must immediately cease within 30 m (100 ft) until the COS Historic Preservation Office has been notified and the nature and significance of the discovery is evaluated by a qualified archaeologist. Work must not resume in this area without approval of the COS Historic Preservation Office.

If human remains are encountered during ground-disturbing activities, all work must immediately cease within 30 m (100 ft) of the discovery and the area must be secured. The Arizona State Museum (ASM), COS Historic Preservation Office, and appropriate Tribes must be notified of the discovery. All discoveries will be treated in accordance Arizona Revised Statute (A.R.S. § 41-865 and work must not resume in this area without authorization from the ASM.

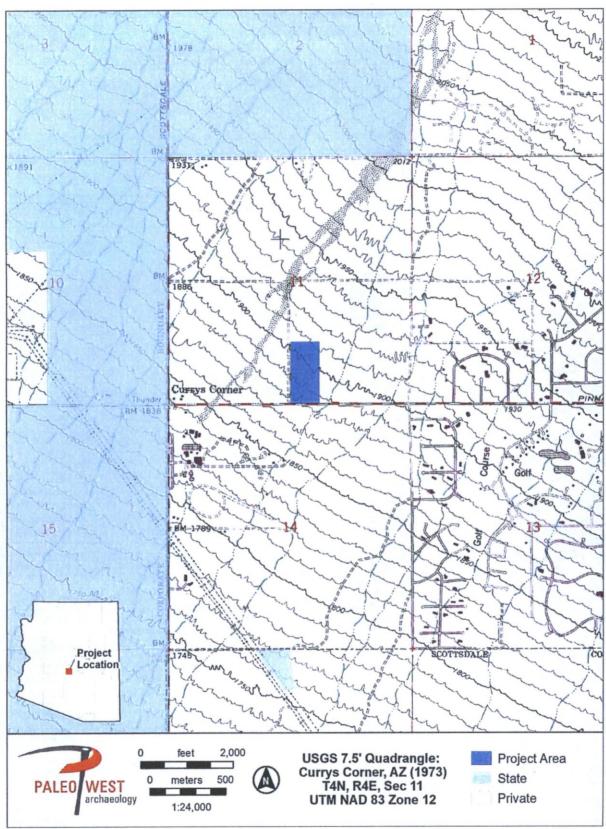


Figure 1. Project location map showing land jurisdiction.



# **Native Plant Inventory**

Pinnacle Peak & Miller 7676 E. Pinnacle Peak Road Scottsdale, AZ

6/2/2017

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 1       | Blue Palo Verde      | 7                            | S      | 经营业的 医二甲基甲基甲基  |
| 2       | Blue Palo Verde      | 6                            | NS     | Cambium Damage / Leaning   |
| 3       | Foothills Palo Verde | 14                           | S      | 一一一一一 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2  |
| 4       | Barrel               | 3                            | S      | No. of the second secon |
| 5       | Foothills Palo Verde | 6                            | NS     | Wash / On Slope  |
| 6       | Foothills Palo Verde | 7                            | S      |  |
| 7       | Mesquite             | 7                            | S      |  |
| 8       | Mesquite             | 5                            | S      | and the second second second   |
| 9       | Mesquite             | 14                           | S      |  |
| 10      | Saguaro              | 6                            | S      |  |
| 11      | Blue Palo Verde      | 14                           | NS     | Mistletoe  |
| 12      | Blue Palo Verde      | 20                           | NS     | Witches Broom  |
| 13      | Mesquite             | 16                           | S      |  |
| 14      | Barrel               | 3                            | S      |  |
| 15      | Blue Palo Verde      | 16                           | S      |  |
| 16      | Blue Palo Verde      | 9                            | S      | 是一个人的人,但是一个人的人的人,但是一个人的人的人的人,但是一个人的人的人的人的人的人的人的人的人的人的人的人的人的人的人的人的人的人的人的  |
| 17      | Barrel               | 4                            | S      |  |
| 18      | Blue Palo Verde      | 12                           | NS     | Witches Broom  |
| 19      | Barrel               | 5                            | S      |  |
| 20      | Foothills Palo Verde | 5                            | NS     | Proximity to Water Valve   |
| 21      | Mesquite             | 6                            | S      | AT THE SERVICE OF THE SERVICE SERVICE  |
| 22      | Foothills Palo Verde | 10                           | NS     | Cambium Damage   |
| 23      | Barrel               | 3                            | S      | The second second  |
| 24      | Mesquite             | 9                            | S      | 10000000000000000000000000000000000000   |
| 25      | Foothills Palo Verde | 4                            | S      |  |
| 26      | Barrel               | 3                            | S      | 4 3 4 4 4 4 4 4  |
| 27      | Foothills Palo Verde | 14                           | S      | the second second  |
| 28      | Foothills Palo Verde | 12                           | S      | TO THE STATE OF TH |
| 29      | Blue Palo Verde      | 6                            | S      |  |
| 30      | Foothills Palo Verde | 7                            | NS     | Trunk Form / Leaning   |
| 31      | Ocotillo             | 14                           | S      | Town I have  |
| 32      | Blue Palo Verde      | 8                            | S      |  |
| 33      | Foothills Palo Verde | 7                            | S      | and the second second  |
| 34      | Foothills Palo Verde | 4                            | S      | nv 1 3   |
| 35      | Barrel               | 3                            | S      | and the second of the second o |
| 36      | Foothills Palo Verde | 10                           | S      |  |
| 37      | Barrel               | 3                            | S      |  |

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 38      | Foothills Palo Verde | 8                            | NS     | Proximity to Headwall  |
| 39      | Foothills Palo Verde | 8                            | S      | Prune Mistletoe  |
| 40      | Barrel               | 4                            | S      |  |
| 41      | Foothills Palo Verde | 20                           | NS     | Cambium Damage   |
| 42      | Mesquite             | 20                           | NS     | Trunk Form / Cambium Damage  |
| 43      | Mesquite             | 18                           | S      |  |
| 44      | Saguaro              | 72                           | S      | 6 arms   |
| 45      | Mesquite             | 4                            | S      |  |
| 46      | Foothills Palo Verde | 16                           | NS     | Leaning / Cambium Damage   |
| 47      | Saguaro              | 134                          | NS     | 7 arms / Declining   |
| 48      | Mesquite             | 8                            | S      |  |
| 49      | Mesquite             | 7                            | S      | Control to the Control of the Contro |
| 50      | Whitethorn Acacia    | 7                            | NS     | Proximity to Headwall  |
| 51      | Whitethorn Acacia    | 7                            | S      |  |
| 52      | Whitethorn Acacia    | 9                            | NS     | Trunk Form / Leaning   |
| 53      | Whitethorn Acacia    | 8                            | NS     | Trunk Form / Leaning   |
| 54      | Mesquite             | 10                           | S      | 500 200 200 200 200 200 200 200 200 200  |
| 55      | Desert Willow        | 8                            | NS     | Cambium Damage   |
| 56      | Mesquite             | 6                            | NS     | Trunk Form / Leaning   |
| 57      | Whitethorn Acacia    | 10                           | NS     | Trunk Form / Poor Structure  |
| 58      | Mesquite             | 4                            | NS     | Trunk Form / Leaning   |
| 59      | Mesquite             | 10                           | S      |  |
| 60      | Blue Palo Verde      | 6                            | NS     | Cluster / Sucker Growth  |
| 61      | Mesquite             | 14                           | S      |  |
| 62      | Mesquite             | 10                           | S      |  |
| 63      | Mesquite             | 4                            | NS     | Trunk Form / Leaning   |
| 64      | Whitethorn Acacia    | 20                           | NS     | Leaning / Poor Structure   |
| 64      | Mesquite             | 14                           | S      |  |
| 65      | Mesquite             | 8                            | S      |  |
| 66      | Foothills Palo Verde | 20                           | NS     | Branch Dieback   |
| 67      | Foothills Palo Verde | 12                           | NS     | Cambium Damage / Leaning   |
| 68      | Foothills Palo Verde | 5                            | S      | AND THE RESERVE AND THE RESERV |
| 69      | Foothills Palo Verde | 8                            | NS     | Branch Dieback   |
| 70      | Foothills Palo Verde | 4                            | S      | The state of the s |
| 71      | Whitethorn Acacia    | 12                           | NS     | Trunk Form / Poor Structure  |
| 72      | Foothills Palo Verde | 18                           | S      |  |
| 73      | Whitethorn Acacia    | 6                            | NS     | Trunk Form / Leaning   |
| 74      | Mesquite             | 16                           | S      |  |
| 75      | Whitethorn Acacia    | 11                           | NS     | Trunk Form / Leaning   |
| 76      | Whitethorn Acacia    | 8                            | NS     | Trunk Form / Leaning   |
| 77      | Whitethorn Acacia    | 8                            | NS     | Exposed Roots / Leaning  |
| 78      | Mesquite             | 6                            | NS     | Trunk Form / Leaning   |
| 79      | Blue Palo Verde      | 7                            | NS     | Leaning / Poor Structure   |
| 80      | Catclaw Acacia       | 8                            | NS     | Leaning / Poor Structure   |
| 81      | Foothills Palo Verde | 4                            | S      |  |
| 82      | Foothills Palo Verde | 5                            | S      |  |
| 83      | Catclaw Acacia       | 6                            | S      |  |
| 84      | Foothills Palo Verde | 4                            | NS     | Cambium Damage   |
| 85      | Whitethorn Acacia    | 10                           | NS     | Branch Dieback / Cambium Damage  |

| Plant# | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|--------|----------------------|------------------------------|--------|--|
| 86     | Foothills Palo Verde | 4                            | S      |  |
| 87     | Foothills Palo Verde | 4                            | S      | Market Control of the |
| 88     | Foothills Palo Verde | 4                            | S      |  |
| 89     | Foothills Palo Verde | 4                            | NS     | Proximity to Wall  |
| 90     | Foothills Palo Verde | 4                            | NS     | Proximity to Wall  |
| 91     | Whitethorn Acacia    | 12                           | NS     | Leaning / Poor Structure   |
| 92     | Whitethorn Acacia    | 6                            | NS     | Leaning / Poor Structure   |
| 93     | Whitethorn Acacia    | 16                           | NS     | Leaning / Poor Structure   |
| 95     | Whitethorn Acacia    | 14                           | NS     | Leaning / Poor Structure   |
| 96     | Whitethorn Acacia    | 7                            | S      | VALUE OF THE PROPERTY OF THE P |
| 97     | Blue Palo Verde      | 4                            | S      |  |
| 98     | Mesquite             | 7                            | S      | A A Comment of the Co |
| 99     | Foothills Palo Verde | 14                           | NS     | Mistletoe / Declining  |
| 100    | Foothills Palo Verde | 12                           | S      |  |
| 101    | Foothills Palo Verde | 9                            | NS     | Proximity to #100  |
| 102    | Barrel               | 4                            | S      |  |
| 103    | Foothills Palo Verde | 4                            | S      |  |
| 104    | Foothills Palo Verde | 14                           | NS     | Mistletoe  |
| 105    | Foothills Palo Verde | 8                            | S      | · · · · · · · · · · · · · · · · · · ·  |
| 106    | Saguaro              | 33                           | S      | 2 arms   |
| 107    | Foothills Palo Verde | 8                            | S      |  |
| 108    | Mesquite             | 10                           | S      | Trade and the second   |
| 109    | Mesquite             | 6                            | S      |  |
| 110    | Desert Willow        | 16                           | NS     | Form / Poor Structure  |
| 111    | Foothills Palo Verde | 12                           | NS     | Cambium Damage / Poor Structure  |
| 112    | Mesquite             | 20                           | S      | 723 724 727 73   |
| 113    | Whitethorn Acacia    | 8                            | NS     | Form / Poor Structure  |
| 114    | Mesquite             | 10                           | NS     | Exposed Roots / Leaning  |
| 115    | Whitethorn Acacia    | 8                            | NS     | Trunk Form / Leaning   |
| 116    | Whitethorn Acacia    | 14                           | NS     | Trunk Form / Cambium Damage  |
| 117    | Mesquite             | 22                           | NS     | Exposed Roots  |
| 118    | Blue Palo Verde      | 5                            | NS     | Trunk Form / Leaning   |
| 119    | Whitethorn Acacia    | 12                           | NS     | Trunk Form / Leaning   |
| 120    | Whitethorn Acacia    | 16                           | NS     | Trunk Form / Poor Structure  |
| 121    | Foothills Palo Verde | 14                           | S      | Trainer offire con dudataro  |
| 122    | Mesquite             | 16                           | S      |  |
| 123    | Mesquite             | 12                           | NS     | Leaning / Poor Structure   |
| 124    | Whitethorn Acacia    | 8                            | NS     | Cambium Damage   |
| 125    | Mesquite             | 9                            | NS     | Trunk Form / Leaning   |
| 126    | Mesquite             | 8                            | S      |  |
| 127    | Mesquite             | 7                            | S      |  |
| 128    | Foothills Palo Verde | 5                            | S      |  |
| 129    | Mesquite             | 20                           | S      | 37 16856   |
| 130    | Mesquite             | 14                           | S      |  |
| 131    | Saguaro              | 90                           | S      | 10 arms  |
| 132    | Foothills Palo Verde | 8                            | S      | To diffic  |
| 133    | Saguaro              | 40                           | S      | 5 arms   |
|        | Jaguaru              |                              |        |  |
| 134    | Foothills Palo Verde | 18                           | NS     | Mistletoe  |

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 136     | Ironwood             | 8                            | S      |  |
| 137     | Foothills Palo Verde | 12                           | S      | A CONTRACTOR OF THE STATE OF TH |
| 138     | Ironwood             | 10                           | S      | the state of the s |
| 139     | Hackberry            | 24                           | NS     | Wide Base  |
| 140     | Foothills Palo Verde | 16                           | S      |  |
| 141     | Saguaro              | 12                           | S      |  |
| 142     | Ocotillo             | 16                           | NS     | Dead   |
| 143     | Foothills Palo Verde | 6                            | S      | A CONTRACTOR OF THE STATE OF TH |
| 144     | Foothills Palo Verde | 16                           | S      | A 100 (A) 100  |
| 145     | Foothills Palo Verde | 14                           | S      |  |
| 146     | Foothills Palo Verde | 5                            | S      | 5.39   |
| 146     | Saguaro              | 20                           | S      | A CONTRACTOR OF THE PROPERTY O |
| 148     | Mesquite             | 14                           | S      |  |
| 149     | Mesquite             | 8                            | S      |  |
| 150     | Saguaro              | 11                           | S      |  |
| 151     | Barrel               | 3                            | S      | at the same of   |
| 152     | Ironwood             | 24                           | S      |  |
| 153     | Saguaro              | 51                           | S      | 5 arms   |
| 154     | Ocotillo             | 14                           | S      |  |
| 155     | Barrel               | 3                            | S      |  |
| 156     | Foothills Palo Verde | 16                           | S      |  |
| 157     | Barrel               | 3                            | S      |  |
| 158     | Saguaro              | 11                           | S      |  |
| 159     | Ironwood             | 18                           | S      |  |
| 160     | Barrel               | 3                            | S      |  |
| 161     | Barrel               | 3                            | S      |  |
| 162     | Mesquite             | 12                           | NS     | Exposed Roots / Leaning  |
| 163     | Barrel               | 4                            | S      |  |
| 164     | Barrel               | 3                            | S      |  |
| 164     | Ironwood             | 24                           | S      |  |
| 166     | Ironwood             | 34                           | S      |  |
| 167     | Ocotillo             | 19                           | S      |  |
| 168     | Barrel               | 3                            | S      |  |
| 169     | Saguaro              | 8                            | S      |  |
| 170     | Foothills Palo Verde | 16                           | S      |  |
| 171     | Foothills Palo Verde | 14                           | S      |  |
| 172     | Saguaro              | 20                           | S      |  |
| 173     | Foothills Palo Verde | 12                           | NS     | Cambium Damage / Leaning   |
| 174     | Saguaro              | 35                           | S      | 3 arms   |
| 175     | Foothills Palo Verde | 22                           | NS     | Branch Dieback   |
| 176     | Barrel               | 3                            | S      |  |
| 177     | Barrel               | 3                            | S      | - 1 1000 - 11200   |
| 178     | Foothills Palo Verde | 12                           | NS     | Cambium Damage / Poor Structure  |
| 179     | Foothills Palo Verde | 16                           | NS     | Cambium Damage / Poor Structure  |
| 180     | Blue Palo Verde      | 6                            | NS     | Witches Broom  |
| 181     | Blue Palo Verde      | 6                            | NS     | Trunk Form / Leaning   |
| 182     | Barrel               | 4                            | S      | Trunk Form / Leaning   |
| 183     | Saguaro              | 13                           | S      |  |
| 184     | Ironwood             | 24                           | S      |  |

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 185     | Foothills Palo Verde | 20                           | NS     | Cambium Damage   |
| 186     | Ironwood             | 22                           | S      | the other self and the accomplishments   |
| 187     | Foothills Palo Verde | 12                           | S      | and the second second second   |
| 188     | Foothills Palo Verde | 14                           | NS     | Cambium Damage   |
| 189     | Foothills Palo Verde | 10                           | NS     | Cambium Damage   |
| 190     | Foothills Palo Verde | 18                           | S      |  |
| 191     | Ocotillo             | 13                           | S      | San  |
| 192     | Saguaro              | 31                           | NS     | 1 arm / Declining  |
| 193     | Foothills Palo Verde | 18                           | NS     | Cambium Damage   |
| 194     | Ironwood             | 14                           | S      |  |
| 195     | Saguaro              | 29                           | S      | 7 arms   |
| 196     | Ironwood             | 18                           | S      |  |
| 197     | Saguaro              | 18                           | S      | 1 arm  |
| 198     | Saguaro              | 55                           | S      | 6 arms   |
| 199     | Saguaro              | 16                           | S      |  |
| 200     | Ironwood             | 20                           | S      | 7 30.6   |
| 201     | Saguaro              | 9                            | S      | THE PROPERTY OF THE PARTY OF TH |
| 202     | Mesquite             | 4                            | S      | Charles and the second  |
| 203     | Foothills Palo Verde | 6                            | S      | The state of the s |
| 204     | Saguaro              | 101                          | S      | 11 arms  |
| 205     | Graythorn            | 7                            | S      | The Contract of the Contract of  |
| 206     | Foothills Palo Verde | 10                           | NS     | Cambium Damage   |
| 207     | Foothills Palo Verde | 16                           | S      | The state of the s |
| 208     | Foothills Palo Verde | 14                           | NS     | Cambium Damage   |
| 209     | Saguaro              | 54                           | S      | 8 arms   |
| 210     | Foothills Palo Verde | 22                           | S      | A THE RESIDENCE OF THE PARTY OF |
| 211     | Saguaro              | 15                           | S      | The second secon |
| 212     | Ironwood             | 10                           | S      |  |
| 213     | Foothills Palo Verde | 4                            | S      | AND SHAPE OF THE STATE OF THE S |
| 214     | Foothills Palo Verde | 4                            | S      |  |
| 215     | Foothills Palo Verde | 5                            | S      | White Act and the Company of the   |
| 216     | Blue Palo Verde      | 7                            | NS     | Cambium Damage   |
| 217     | Blue Palo Verde      | 14                           | S      | The water of the other all the   |
| 218     | Ocotillo             | 15                           | S      |  |
| 219     | Saguaro              | 40                           | S      | 2 arms   |
| 220     | Barrel               | 3                            | S      |  |
| 221     | Ocotillo             | 14                           | S      |  |
| 222     | Foothills Palo Verde | 18                           | S      |  |
| 223     | Blue Palo Verde      | 15                           | NS     | Cambium Damage / Poor Structure  |
| 224     | Barrel               | 3                            | S      |  |
| 225     | Blue Palo Verde      | 18                           | NS     | Cambium Damage / Poor Structure  |
| 226     | Blue Palo Verde      | 16                           | S      | A CAMPAGA A CAMP |
| 227     | Saguaro              | 35                           | S      | 2 arms   |
| 228     | Ironwood             | 20                           | NS     | Proximity to Structure   |
| 229     | Saguaro              | 25                           | NS     | Declining  |
| 230     | Mesquite             | 7                            | S      |  |
| 231     | Ocotillo             | 11                           | S      |  |
| 232     | Mesquite             | 13                           | NS     | Proximity to Asphalt / Structure   |
| 233     | Foothills Palo Verde | 16                           | S      | A CONTROL OF THE PROPERTY OF T |
|         | . Commo i dio voido  |                              | -      |  |

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 234     | Foothills Palo Verde | 20                           | NS     | Proximity to Structure   |
| 235     | Foothills Palo Verde | 20                           | S      |  |
| 236     | Mesquite             | 24                           | NS     | Cambium Damage / Access Issue  |
| 237     | Catclaw Acacia       | 14                           | NS     | Form / Access Issue  |
| 238     | Catclaw Acacia       | 12                           | NS     | Form / Access Issue  |
| 239     | Catclaw Acacia       | 8                            | NS     | Form / Access Issue  |
| 240     | Hackberry            | 20                           | NS     | Wide Base  |
| 241     | Hackberry            | 20                           | NS     | Wide Base  |
| 242     | Blue Palo Verde      | 18                           | S      |  |
| 243     | Saguaro              | 9                            | S      |  |
| 244     | Mesquite             | 17                           | S      |  |
| 245     | Saguaro              | 11                           | S      |  |
| 246     | Barrel               | 3                            | S      |  |
| 247     | Mesquite             | 5                            | S      |  |
| 248     | Barrel               | 3                            | S      | and the second s |
| 249     | Mesquite             | 28                           | NS     | Proximity to Asphalt / Structure   |
| 250     | Mesquite             | 16                           | NS     | Cambium Damage / Poor Structure  |
| 251     | Barrel               | 3                            | S      |  |
| 252     | Saguaro              | 12                           | S      | The second of the second of the  |
| 253     | Mesquite             | 8                            | S      |  |
| 254     | Mesquite             | 18                           | NS     | Exposed Roots / Poor Structure   |
| 255     | Saguaro              | 4                            | S      | AND REAL PROPERTY OF THE PARTY  |
| 256     | Mesquite             | 8                            | NS     | Trunk Form / Leaning   |
| 257     | Saguaro              | 5                            | S      |  |
| 258     | Barrel               | 3                            | S      |  |
| 259     | Barrel               | 4                            | S      |  |
| 260     | Barrel               | - 4                          | S      | and the second s |
| 261     | Mesquite             | 18                           | S      | 0.00   |
| 262     | Barrel               | 3                            | S      | West Control of the C |
| 263     | Mesquite             | 20                           | S      |  |
| 264     | Barrel               | 3                            | S      | The Walley Control of the Control  |
| 265     | Barrel               | 3                            | S      |  |
| 266     | Mesquite             | 18                           | S      |  |
| 267     | Barrel               | 3                            | S      |  |
| 268     | Mesquite             | 8                            | NS     | Exposed Roots  |
| 269     | Barrel               | 3                            | S      | Multiple heads   |
| 270     | Barrel               | 3                            | S      | AND THE RESERVE OF THE PARTY OF |
| 271     | Barrel               | 5                            | S      |  |
| 272     | Mesquite             | 13                           | NS     | Exposed Roots / Leaning  |
| 273     | Mesquite             | 14                           | S      |  |
| 274     | Ocotillo             | 10                           | S      |  |
| 275     | Mesquite             | 18                           | S      | The state of the state of the state of   |
| 276     | Saguaro              | 6                            | S      | all and the second seco |
| 277     | Foothills Palo Verde | 18                           | NS     | Proximity to Sidewalk  |
| 278     | Ironwood             | 22                           | NS     | Trunk Form / Access Issue  |
| 279     | Foothills Palo Verde | 16                           | NS     | Cambium Damage / Access Issue  |
| 280     | Foothills Palo Verde | 8                            | NS     | Proximity to Wall / Curb   |
| 281     | Blue Palo Verde      | 18                           | NS     | Cambium Damage / Proximity to Wal  |
| 282     | Ironwood             | 9                            | NS     | Form / Poor Structure  |

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 283     | Foothills Palo Verde | 24                           | NS     | Cambium Damage / Access Issue  |
| 284     | Ironwood             | 18                           | S      |  |
| 285     | Blue Palo Verde      | 14                           | NS     | Exposed Roots  |
| 286     | Foothills Palo Verde | 8                            | NS     | Cambium Damage / Poor Structure  |
| 287     | Foothills Palo Verde | 6                            | S      | The second secon |
| 288     | Mesquite             | 5                            | S      |  |
| 289     | Mesquite             | 15                           | S      |  |
| 290     | Mesquite             | 14                           | S      | and the second of the second o |
| 291     | Blue Palo Verde      | 14                           | S      | 23-11-26-2   |
| 292     | Blue Palo Verde      | 5                            | S      |  |
| 293     | Foothills Palo Verde | 6                            | S      |  |
| 294     | Foothills Palo Verde | 4                            | S      |  |
| 295     | Foothills Palo Verde | 5                            | S      | Kerist and the second  |
| 296     | Foothills Palo Verde | 4                            | S      | The state of the s |
| 297     | Foothills Palo Verde | 5                            | S      |  |
| 298     | Foothills Palo Verde | 6                            | S      | The second second  |
| 299     | Blue Palo Verde      | 5                            | S      | Serio de Maria de Caracteria d |
| 300     | Blue Palo Verde      | 9                            | S      |  |
| 301     | Blue Palo Verde      | 4                            | S      |  |
| 302     | Blue Palo Verde      | 12                           | S      | San Carlotte Control of the Control  |
| 303     | Blue Palo Verde      | 7                            | NS     | Cambium Damage / Leaning   |
| 304     | Blue Palo Verde      | 6                            | NS     | Cambium Damage / Leaning   |
| 305     | Ocotillo             | 13                           | S      |  |
| 306     | Saguaro              | 5                            | S      |  |
| 307     | Blue Palo Verde      | 14                           | NS     | Cambium Damage / Leaning   |
| 308     | Foothills Palo Verde | 5                            | S      |  |
| 309     | Yucca elata          | 10                           | NS     | 3 arms / Leaning / Form  |
| 310     | Yucca elata          | 10                           | NS     | 3 arms / Leaning / Declining   |
| 311     | Yucca elata          | 16                           | NS     | 2 heads / Declining  |
| 312     | Foothills Palo Verde | 7                            | S      | 4 2 10 20 20 20 20 20 20 20 20 20 20 20 20 20  |
| 313     | Blue Palo Verde      | 8                            | NS     | Cambium Damage / Leaning   |
| 314     | Foothills Palo Verde | 9                            | NS     | Trunk Form / Access Issue  |
| 315     | Blue Palo Verde      | 8                            | NS     | Exposed Roots / Cambium Damage   |
| 316     | Blue Palo Verde      | 5                            | S      | A STATE OF THE STA |
| 317     | Foothills Palo Verde | 5                            | S      | The state of the s |
| 318     | Mesquite             | 26                           | NS     | Exposed Roots  |
| 319     | Blue Palo Verde      | 15                           | S      |  |
| 320     | Mesquite             | 12                           | S      | The second secon |
| 321     | Blue Palo Verde      | 7                            | NS     | Leaning / Cambium Damage   |
| 322     | Ocotillo             | 16                           | S      | -  |
| 323     | Saguaro              | 5                            | S      | 8 10 10 10 10 10 10 10 10 10 10 10 10 10   |
| 324     | Saguaro              | 11                           | S      | 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1  |
| 325     | Foothills Palo Verde | 7                            | S      | The second second  |
| 325     | Ocotillo             | 9                            | S      | The state of the s |
| 326     | Blue Palo Verde      | 10                           | NS     | Cambium Damage / Access Issue  |
| 327     | Mesquite             | 8                            | S      |  |
| 329     | Mesquite             | 5                            | NS     | Leaning / Cambium Damage   |
| 330     | Catclaw Acacia       | 9                            | NS     | Leaning / Access Issue   |
| 331     | Catclaw Acacia       | 12                           | NS     | Leaning / Access Issue   |

| Plant #    | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|------------|----------------------|------------------------------|--------|--|
| 332        | Hackberry            | 12                           | NS     | Wide Base  |
| 333        | Blue Palo Verde      | 14                           | NS     | Cambium Damage   |
| 334        | Mesquite             | 30                           | S      |  |
| 335        | Foothills Palo Verde | 5                            | S      |  |
| 336        | Foothills Palo Verde | 8                            | NS     | Branch Dieback / Cambium Damage  |
| 337        | Mesquite             | 6                            | NS     | Trunk Form / Leaning   |
| 338        | Mesquite             | 6                            | S      |  |
| 339        | Foothills Palo Verde | 8                            | S      | The second secon |
| 340        | Blue Palo Verde      | 18                           | NS     | Proximity to Wall / On Slope   |
| 341        | Ironwood             | 28                           | S      |  |
| 342        | Foothills Palo Verde | 5                            | S      | and the second second  |
| 343        | Foothills Palo Verde | 7                            | NS     | Proximity to Wall / On Slope   |
| 344        | Foothills Palo Verde | 7                            | NS     | Proximity to Wall / On Slope   |
| 345        | Foothills Palo Verde | 14                           | NS     | Proximity to Wall / On Slope   |
| 346        | Blue Palo Verde      | 14                           | NS     | Proximity to Wall / On Slope   |
| 347        | Mesquite             | 4                            | S      |  |
| 348        | Mesquite             | 6                            | S      |  |
| 349        | Foothills Palo Verde | 9                            | NS     | Exposed Roots  |
| 350        | Foothills Palo Verde | 14                           | NS     | Exposed Roots  |
| 351        | Foothills Palo Verde | 7                            | NS     | Exposed Roots  |
| 352        | Saguaro              | 46                           | NS     | 4 arms / Declining   |
| 353        | Saguaro              | 39                           | NS     | 6 arms / Declining   |
| 354        | Foothills Palo Verde | 15                           | NS     | Cambium Damage   |
| 355        | Hackberry            | 8                            | NS     | Branch Dieback / Cambium Damage  |
| 356        | Saguaro              | 4                            | NS     | Damaged  |
| 357        | Saguaro              | 85                           | S      | 10 arms  |
| 358        | Saguaro              | 3                            | S      | TO arms  |
| 359        | Foothills Palo Verde | 12                           | S      |  |
| 360        | Foothills Palo Verde | 8                            | NS     | Branch Dieback / Cambium Damage  |
| 361        | Barrel               | 3                            | S      | Branch Dieback / Cambium Damage  |
| 362        | Barrel               | 4                            | NS     | Damaged  |
| 363        |                      | 63                           | NS     | 5 arms / Damaged   |
| 364        | Saguaro<br>Barrel    | 4                            | S      | 5 airiis / Dairiageu   |
| 365        |                      | 3                            | S      |  |
| 366        | Saguaro<br>Saguaro   | 4                            | S      |  |
| 367        |                      | 5                            | S      | 2 arms   |
| 368        | Saguaro<br>Saguaro   | 5                            | S      | 2 dillis   |
| 369        | Foothills Palo Verde | 13                           | S      |  |
| 370        | Foothills Palo Verde | 12                           | NS     | Cambium Damage   |
|            |                      | 7                            | S      | Cambium Damage   |
| 371        | Foothills Palo Verde |                              |        | Eveneed Posts  |
| 372        | Foothills Palo Verde | 8                            | NS     | Exposed Roots  |
| 373        | Foothills Palo Verde | 6                            | S      | Evened Bests / Counting Bests  |
| 374        | Foothills Palo Verde | 8                            | NS     | Exposed Roots / Cambium Damage   |
| 375        | Foothills Palo Verde | 6                            | NS     | Exposed Roots / Cambium Damage   |
| 376        | Foothills Palo Verde | 12                           | NS     | Branch Dieback / Cambium Damage  |
| 377        | Foothills Palo Verde | 8                            | NS     | Exposed Roots / Cambium Damage   |
|            | Ironwood             | 30                           | NS     | Branch Dieback / Cambium Damage  |
| 378<br>379 | Ironwood             | 50                           | NS     | Wide Base / Cambium Damage   |

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 381     | Barrel               | 4                            | S      |  |
| 382     | Foothills Palo Verde | 4                            | S      |  |
| 383     | Foothills Palo Verde | 8                            | NS     | Leaning / On Slope   |
| 384     | Foothills Palo Verde | 6                            | S      |  |
| 385     | Mesquite             | 16                           | S      | The second secon |
| 386     | Mesquite             | 4                            | S      | The state of the s |
| 387     | Ironwood             | 12                           | NS     | Trunk Form / Leaning   |
| 388     | Foothills Palo Verde | 8                            | NS     | Cambium Damage   |
| 389     | Blue Palo Verde      | 4                            | S      |  |
| 390     | Foothills Palo Verde | 12                           | NS     | Trunk Form / Leaning   |
| 391     | Foothills Palo Verde | 8                            | NS     | Trunk Form / Leaning   |
| 392     | Foothills Palo Verde | 6                            | NS     | Trunk Form / Leaning   |
| 393     | Blue Palo Verde      | 10                           | NS     | Branch Dieback / Leaning   |
| 394     | Saguaro              | 43                           | S      | 5 arms   |
| 395     | Barrel               | 4                            | S      | The table of the second of the |
| 396     | Foothills Palo Verde | 4                            | S      |  |
| 397     | Barrel               | 5                            | NS     | Damaged  |
| 398     | Barrel               | 3                            | S      | · · · · · · · · · · · · · · · · · · ·  |
| 399     | Saguaro              | 4                            | S      | Police March 199   |
| 400     | Barrel               | 4                            | S      |  |
| 401     | Foothills Palo Verde | 4                            | NS     | Leaning / On Slope   |
| 402     | Foothills Palo Verde | 22                           | NS     | Branch Dieback / Cambium Damage  |
| 403     | Foothills Palo Verde | 12                           | NS     | Branch Dieback / Cambium Damage  |
| 404     | Foothills Palo Verde | 6                            | NS     | Exposed Roots / Cambium Damage   |
| 405     | Foothills Palo Verde | 14                           | S      |  |
| 406     | Foothills Palo Verde | 20                           | S      | the section of the se |
| 407     | Foothills Palo Verde | 8                            | S      | 果 上 建 张 二 二 一  |
| 408     | Foothills Palo Verde | 10                           | NS     | Cambium Damage   |
| 409     | Foothills Palo Verde | 7                            | NS     | Cambium Damage   |
| 410     | Foothills Palo Verde | 16                           | NS     | Branch Dieback / Cambium Damage  |
| 411     | Foothills Palo Verde | 4                            | NS     | Exposed Roots / Cambium Damage   |
| 412     | Ironwood             | 10                           | NS     | Branch Dieback / Cambium Damage  |
| 413     | Foothills Palo Verde | 10                           | NS     | Branch Dieback / Cambium Damage  |
| 414     | Foothills Palo Verde | 4                            | S      | Endline and the second of the  |
| 415     | Saguaro              | 70                           | S      | 5 arms   |
| 416     | Saguaro              | 3                            | S      | The state of the s |
| 417     | Saguaro              | 3                            | S      | 2.4  |
| 418     | Saguaro              | 6                            | S      | The state of the s |
| 419     | Saguaro              | 43                           | NS     | 3 arms / Damaged   |
| 420     | Foothills Palo Verde | 5                            | NS     | Trunk Form / Leaning   |
| 421     | Foothills Palo Verde | 7                            | NS     | Branch Dieback / Cambium Damage  |
| 422     | Foothills Palo Verde | 6                            | NS     | Branch Dieback / Cambium Damage  |
| 423     | Foothills Palo Verde | 14                           | NS     | Branch Dieback / Cambium Damage  |
| 424     | Foothills Palo Verde | 7                            | NS     | Branch Dieback / Cambium Damage  |
| 425     | Foothills Palo Verde | 8                            | NS     | Trunk Form / Cambium Damage  |
| 426     | Foothills Palo Verde | 8                            | NS     | Trunk Form / Cambium Damage  |
| 427     | Foothills Palo Verde | 4                            | NS     | Trunk Form / Cambium Damage  |
| 428     | Foothills Palo Verde | 14                           | NS     | Branch Dieback / Cambium Damage  |
| 429     | Foothills Palo Verde | 7                            | NS     | Exposed Roots  |

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 430     | Foothills Palo Verde | 10                           | NS     | Branch Dieback / Cambium Damage  |
| 431     | Barrel               | 3                            | S      |  |
| 432     | Saguaro              | 14                           | S      |  |
| 433     | Saguaro              | 72                           | S      | 6 arms   |
| 434     | Saguaro              | 42                           | S      | 4 arms   |
| 435     | Saguaro              | 102                          | S      | 10 arms  |
| 436     | Saguaro              | 4                            | S      |  |
| 437     | Saguaro              | 4                            | S      | and the second second second   |
| 438     | Saguaro              | 4                            | S      |  |
| 439     | Barrel               | 5                            | NS     | Damaged  |
| 440     | Foothills Palo Verde | 24                           | S      |  |
| 441     | Foothills Palo Verde | 7                            | NS     | Leaning / On Slope   |
| 442     | Foothills Palo Verde | 4                            | S      | The state of the s |
| 443     | Foothills Palo Verde | 4                            | S      |  |
| 444     | Saguaro              | 3                            | S      |  |
| 445     | Saguaro              | 3                            | S      |  |
| 446     | Barrel               | 4                            | S      |  |
| 447     | Barrel               | 4                            | S      |  |
| 448     | Ironwood             | 24                           | S      | A CONTRACTOR OF THE CONTRACTOR |
| 449     | Barrel               | 4                            | S      |  |
| 450     | Barrel               | 4                            | S      | Company Track that was a second of the   |
| 451     | Barrel               | 4                            | S      | Multiple heads   |
| 452     | Barrel               | 4                            | S      | A PLANT OF THE STATE OF THE STA |
| 453     | Barrel               | 7                            | S      |  |
| 454     | Saguaro              | 3                            | S      |  |
| 455     | Barrel               | 3                            | S      | The state of the s |
| 456     | Ironwood             | 60                           | NS     | Wide Base / Cambium Damage   |
| 457     | Ironwood             | 18                           | NS     | Mistletoe / Cambium Damage   |
| 458     | Foothills Palo Verde | 9                            | NS     | Branch Dieback / Cambium Damage  |
| 459     | Foothills Palo Verde | 9                            | NS     | Branch Dieback / Cambium Damage  |
| 460     | Barrel               | 5                            | NS     | Damaged  |
| 461     | Saguaro              | 4                            | S      | Charles the latest the second of the   |
| 462     | Barrel               | 3                            | S      |  |
| 463     | Foothills Palo Verde | 4                            | S      |  |
| 464     | Foothills Palo Verde | 7                            | S      |  |
| 465     | Foothills Palo Verde | 8                            | S      |  |
| 466     | Saguaro              | 13                           | S      | Water State of the Control of the Co |
| 467     | Saguaro              | 3                            | S      |  |
| 468     | Ironwood             | 36                           | NS     | Exposed Roots / Mistletoe  |
| 469     | Ironwood             | 30                           | NS     | Exposed Roots / Cambium Damage   |
| 470     | Foothills Palo Verde | 16                           | S      |  |
| 471     | Saguaro              | 7                            | S      | THE STATE OF THE S |
| 472     | Saguaro              | 7                            | S      | 2 heads  |
| 473     | Foothills Palo Verde | 4                            | S      |  |
| 474     | Blue Palo Verde      | 4                            | S      |  |
| 475     | Foothills Palo Verde | 22                           | NS     | Branch Dieback / Cambium Damage  |
| 476     | Barrel               | 3                            | S      |  |
| 477     | Saguaro              | 10                           | S      |  |
| 478     | Saguaro              | 8                            | S      |  |

| Plant # | Common Name          | Caliper (in)/<br>Height (ft) | Status | Comments   |
|---------|----------------------|------------------------------|--------|--|
| 479     | Foothills Palo Verde | 20                           | NS     | Branch Dieback / Cambium Damage  |
| 480     | Blue Palo Verde      | 8                            | NS     | Witches Broom  |
| 481     | Blue Palo Verde      | 8                            | NS     | Witches Broom  |
| 482     | Blue Palo Verde      | 12                           | S      | A STATE OF THE STA |
| 483     | Blue Palo Verde      | 10                           | NS     | Branch Dieback   |
| 484     | Blue Palo Verde      | 4                            | S      |  |
| 485     | Mesquite             | 14                           | S      |  |
| 486     | Mesquite             | 4                            | S      |  |
| 487     | Foothills Palo Verde | 6                            | NS     | Proximity to #488  |
| 488     | Foothills Palo Verde | 6                            | S      |  |
| 489     | Blue Palo Verde      | 10                           | S      | Part of the second seco |

| Summary         | Trees | Cacti |  |
|-----------------|-------|-------|--|
| Salvageable     | 170   | 128   |  |
| Non-Salvageable | 175   | 16    |  |
| Remain-In-Place | 0     | 0     |  |
| Total           | 345   | 144   |  |

S = Salvageable
NS = Non-Salvageable
RIP = Remain-In-Place

# PRELIMINARY WATER CAPACITY REPORT

NEC Pinnacle Peak Rd. & Miller Rd. Scottsdale, AZ

**Prepared For:** 



7676 E. Pinnacle Peak Road Scottsdale, AZ 85255 P: 480.888.3000 City of Scottsdale
Water Resources Administration
9379 E. San Salvador
Scottsdale, AZ 85258

Prepared by:



Sustainability Engineering Group

8280 E. Gelding Drive, Suite 101 Scottsdale, AZ 85260 480.588.7226 <u>www.azSEG.com</u>

Project Number: 170566

Original Submittal Date: June 22, 2017 (Zoning) Revised: August 18,2017

Case No.: 3-GP-2017; 11-ZN-2017 Plan Check No.: TBD



EXPIRES 9/30/2017



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APPENDIX 2 - WaterCAD Results

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#### 1. EXECUTIVE SUMMARY

The subject project is the proposed redevelopment of the existing P.F. Chang's office complex located at the NEC of North Miller Road and East of Pinnacle Peak Road into a residential development. The parcels are currently zoned S-R ESL (Service Residential Environmentally Sensitive Lands) and will be developed with a maximum of fifty-five (55) residences fronting on a proposed internal 46' wide tract with 28' wide private cul-de-sacs with rezoning to R1-10.

Water service for the development is to be provided by the City of Scottsdale. Connections will be from an existing 16" DIP main that runs north and south in North Miller Road and an 8" water main in North 77<sup>th</sup> Street which then connects to the 12" water main south of the center line in East Pinnacle Peak Road.

There will be no off-site improvements required of public mains to serve the domestic service, irrigation, and fire protection to the proposed residential lots.

Certified fire hydrant flow testing was performed on May 22, 2017 at 7:00 AM by Arizona Flow Testing, LLC at locations as shown on the provided reports. The results are as follows:

|   |                    | Raw Test Data | Data w/58 PSI Safety Factor |
|---|--------------------|---------------|-----------------------------|
| • | Static Pressure    | 130.0 PSI     | 72.0 PSI                    |
| • | Residual Pressure: | 108.0 PSI     | 50.0 PSI                    |
| • | Flow:              | 3,087 GPM     | 3,087 GPM                   |
| • | GPM @ 20 PSI:      | 7,361 GPM     | 4,912 GPM                   |

The actual flow test documentation is included in Appendix I.

#### 2. INTRODUCTION

#### 2.1 PLAN OBJECTIVE:

The purpose of this report is to provide discussions and calculations defining the water system concepts necessary to comply with the requirements outlined in the City of Scottsdale Design Standards & Policy Manual. Preparation of this report has been done in accordance with the requirements of the City's Design Standards & Policy Manual.

#### 2.2 SITE LOCATION

The project property consists of four (4) parcels of land located at the NEC of North Miller Road and East Pinnacle Peak Road. The total project area contains approximately 855,802.3 SF (19.647 AC) gross; 749,876.2 SF (17.215 AC) net. It is further defined as follows:

• Parcel Description: The west half of Section 11, Township 4 North, Range 4 East of

the Gila and Salt River Base and Meridian, Maricopa County,

Scottsdale, Arizona

Parcel ID numbers: APN: 212-04-001B, 212-04-001C, 212-04-001D and 212-04

001E.

Parcel Address: 7676 E. Pinnacle Peak Road



The site is bounded by North Miller Road on the west, East Pinnacle Peak Road on the south, a portion of North 77<sup>th</sup> Street on the east near the SEC and the La Vista single family subdivision to the east and north.

Refer to FIGURE 1 - Vicinity Map for the project's location with respect to major cross streets

#### 2.3 PROPOSED DEVELOPMENT

#### 2.3.1 Existing Site Description:

Land ownership includes 17.22 +/- net acres over four (4) parcels of developed and undeveloped land designated as S-R ESL. There are existing designated and recorded N.A.O.S. areas along the south, west and north portions of the proposed project site area. The project is proposed to rezone the parcel to R1-10.

The site is both undeveloped natural desert and a developed office component roughly in the south 2/3 of the project site. Contour elevations range from approximately 1916 in the northeast corner to 1879 in the southwest corner, with a slope at approximately 2.5% from northeast to southwest.

FIRM Map Number 04013C1310L dated October 16, 2013 indicates this site is designated as Zone "AO", however there has been a Letter of Map Revision (LOMR) 15-09-1857P with an effective date of June 10, 2016 which removed the project site from the Rawhide Wash Floodplain area and re-designated as **Zone "X"**, having a 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile.

Refer to **FIGURE 2** for an aerial of the overall project existing conditions.

#### **EXISTING WATER (COS QS45-46)**

- Miller Road: Two existing 16" and one 36" water mains run north and south in North Miller Road. One 16" (unknown type) is located approximately 3' east, one 36" (unknown type) is located approximately 10' east and one 16" C900 / DIP is located approximately 39' east of the North Miller Road center line respectively. The 16" water main located approximately 39' east of the center line serves the existing office complex.
- E. Pinnacle Peak Road: Two 12" water mains run east and west in East Pinnacle Peak Road. One 12" DIP (non-potable unknown type, connected to a well site) water main is located approximately 44' north and one 12" water main (potable type) is located approximately 42' south of the East Pinnacle Peak Road center line. No service taps to the site are indicated.
- <u>77<sup>th</sup> Street:</u> An 8" ACP potable water main is located near the easterly ROW line of 77<sup>th</sup> Street. The on-site water loop ties into this main.
- On-site: There is an 8" diameter water line, per city mapping records, in a 12' public water easement that bisects the project site from North Miller Road to North 77<sup>th</sup>



Street. If the entire line cannot be utilized based on size and location then the line will need to be abandoned and removed.

Refer to Figure 3 for the COS Water Quarter Section Map (QS 45-46).

#### 2.3.2 Proposed Site Development:

Proposed development consists of a maximum of fifty-five (55) residences fronting on a proposed internal 46' wide tract with 28' wide private cul-de-sac. Main access is provided near the center of the parcel off North Miller Road which connects to East Pinnacle Peak Road to the south.

An 8" main is proposed to tie into the existing 16" City of Scottsdale main in Miller Road and loop through the site and tie into the existing 8" main in 77<sup>th</sup> Street. Domestic and irrigation services to the units will be tapped off this new 8" water main.

Refer to FIGURE 4 for the proposed site layout.

#### 3. DESIGN CRITERIA

### 3.1 UTILITY DEVELOPER GUIDE CRITERIA

This project is designed using 55 du / 19.65 gross acres = 2.89 du/ac. Refer to **Table 1** below for applicable "Design Criteria for Water Systems" based on Figure 6.1-2 (2-2.9 du/ac) in accordance with the City of Scottsdale DS&PM.

Table 1 - COS Design Criteria by demand type

| Land Use                     | Average Day<br>Demand<br>(gal/day/unit) | Max Day<br>Peaking<br>Factor | Peak Hour Peaking Factor |
|------------------------------|---|------------------------------|--------------------------|
| Residential<br>(2-2.9 DU/ac) | 470.4                                   | 2.0                          | 3.5                      |

The system pressures, velocities, head losses and fire flow are in accordance with the COS DS&PM as follows:

#### Minimum Pressures:

Final water modeling will demonstrate a minimum of 50 psi residual pressure is available at the highest delivery point within a structure based on data within the 2015 IPC Appendix "B" under maximum system demand AND a minimum 30 psi is available at all fire hydrants with 15 psi available at the highest delivery point within a structure.

#### **Maximum Pressures:**

Maximum Pressure =120 psi

The City of Scottsdale operates its system from wells and pumps that commonly have pressures exceeding 80 psi. Therefore, the city requires all metered services to have a pressure-regulating valve installed on the private service line per DS&PM 6-1.402.



#### Velocity & Head loss:

- 10 ft. head loss maximum per 1,000 linear feet of pipe for pipes less than 16 inches in diameter with a
- Hazen-Williams Coefficient = 130

#### Fire Flows:

This site is under the jurisdiction of the City of Scottsdale Fire Department. Fire flows must be in accordance with the 2015 International Fire Code which, for one- and two-family dwellings, is determined as follows:

 Dwellings having a fire-flow calculation area that does not exceed 3,600 s.f. that have automatic sprinklers shall be 500 gpm for 1/2 hour.

#### 4. DEMANDS

#### 4.1 PROJECT USE DESCRIPTION

Proposed demands for this project are based on a Residential Demand per Dwelling Unit for a density 2-2.9 DU/ac. Refer to **Table 2** below for the proposed water demand calculations based on the design criteria established in *Section 3.1* above

| Table 2: Water Dei           | mand Co | alculations                    |                              |                                |                             |                             |                       |
|------------------------------|---------|--------------------------------|------------------------------|--------------------------------|-----------------------------|-----------------------------|-----------------------|
|                              | Units   | Avg. Day<br>Flow<br>(gpd/unit) | Max Day<br>Peaking<br>Factor | Peak Hour<br>Peaking<br>Factor | Avg. Day<br>Demand<br>(GPD) | Max. Day<br>Demand<br>(GPD) | Peak<br>Hour<br>(GPD) |
| Res. (2-2.9 DU/ac)           | 55      | 470.4                          | 2                            | 3.5                            | 25,872                      | 51,744                      | 90,552                |
| TOTAL PROPOSED<br>BLDG UNITS | 55      |                                |                              |                                |                             |                             |                       |
| 5 7 7 7 7 7                  |         | 1                              | OTAL DEM                     | ANDS (GPD):                    | 25,872                      | 51,744                      | 90,552                |
|                              |         | TOTAL DEMANDS (gpm):           |                              |                                | 18.0                        | 35.9                        | 62.9                  |

#### 4.2 ZONING

This site is in Zone 6 according to Figure 6.1-3 Pressure Zone Map in DS&PM.

#### 4.3 PHASING OF DEMANDS

This residential project may be phased as dictated by unit demand. The infrastructure will be built in a single phase.

#### 4.4 SUMMARY NARRATIVE OF DEMANDS

The demand scenario that governs the design was the peak hour demand.



### 5. EXISTING FACILITIES / CONDITIONS

#### 5.1 PREVIOUS MASTER PLANS

No existing master plan or water report is available from COS for this site.

#### 6. PROPOSED FACILITIES

#### 6.1 DISTRIBUTION SYSTEM PIPING

#### 6.1.1 Onsite:

The proposed water supply will consist of new 8" public water line and new fire hydrants. The proposed 8" water main will be DIP in accordance with COS requirements. Domestic service will be provided by 1" copper service connections to each lot, including meter and backflow prevention and PRV. Irrigation will be tapped from the domestic service after the BFP and require a separate/second BFP.

Irrigation for common areas will be provided by a separate system tapped from the 8" water main and maintained by the Home Owners Association.

#### 6.1.2 Offsite Infrastructure:

No offsite infrastructure is anticipated.

#### 7. WATER MODEL

#### 7.1 DESCRIPTION OF MODEL

The final model of the proposed water system is designed to meet the criteria of COS Water, the Arizona Department of Environmental Quality ("ADEQ"), and Maricopa County Environmental Services Department ("MCESD").

Bentley WaterCAD\* Version 8i is the computer modeling tool used in this study.

Network analysis input parameters included the following:

- 1. Pipe diameters (inches)
- 2. Pipe lengths (feet)
- 3. Pipes invert elevations (feet)
- 4. General Purpose Valve to model Water Meter and Double Check Valve Assembly
- 5. A reservoir and a pump to model the fire flow test performed
- 6. System demands (gpm)
- 7. Fire flows (gpm)
- 8. Model piping is ductile iron pipe using Hazen-Williams frictional losses (C = 130)

Output parameters included but were not limited to:

- 1. Pressure (psig)
- 2. Flow rates (gpm)
- 3. Velocities (fps)
- 4. Head loss (feet)



#### 7.2 ASSUMPTIONS

Please refer to Section 3.1 for the design criteria.

The general methodology used to design this public water infrastructure consists of modeling a network of water distribution mains to meet COS pressure, head loss, and water demand requirements during daily demands and fire events. The connection to the water system is modeled as a reservoir and pump. The pump will simulate the pressure drop and the available flow from the existing water system as depicted by the fire flow test. Refer to **Appendix I** for a copy of the fire flow test results.

#### 7.3 SUMMARY OF RESULTS

A summary of the modeling results is presented below in **Table 3**. Detailed WaterCAD\* results are presented in **Appendix II**.

Table 3 - WaterCAD® Analysis Results

| Demand            | Water<br>Demand<br>(GMP) | Pressure (PSIG) |      |      |      | Maximum            |         |
|-------------------|--------------------------|-----------------|------|------|------|--------------------|---------|
| Scenario          |                          | Min.            | Node | Max. | Node | Velocity<br>(ft/s) | Pipe ID |
| Average Day       | 18.0                     | 66              | J-7  | 79   | J-11 | 0.07               | P-17    |
| Maximum<br>Day    | 35.9                     | 66              | J-7  | 79   | J-11 | 0.14               | P-9     |
| Peak Hour         | 62.9                     | 66              | J-7  | 79   | J-11 | 0.24               | P-9     |
| 500 +<br>Max. day | 500 +<br>Max. day        | 41              | J-7  | N/A  | N/A  | N/A                | N/A     |



# 8. SUMMARY / CONCLUSIONS

#### 8.1 CONFORMANCE TO DESIGN GOALS

- The proposed water main is designed in accordance with COS design standards and policies<sup>1</sup>. The following summary is based on the above analysis summary.
  - Minimum 50 psi residual @ highest delivery point required, 65 psi minimum provided.
  - o Minimum 30 psi @ max+ fire flow required, 38 psi provided.
  - 10 fps maximum velocity is not exceeded.
  - The system supports the minimum 500 gpm fire flow requirements.
- The results shown in the modeling summary (refer to Section 7.3) indicate that the
  proposed water system meets the COS criteria for Daily water usage and fire flow events as
  described in Section 3.1.
- PRV's at each building are required per COS design criteria.

#### 8.2 REQUIRED FACILITIES AND PHASING

- Proposed facility improvements for this project are limited to a new 8" water main, new fire hydrants, and 1" domestic service connections for each lot.
- This project will be constructed in a single phase.

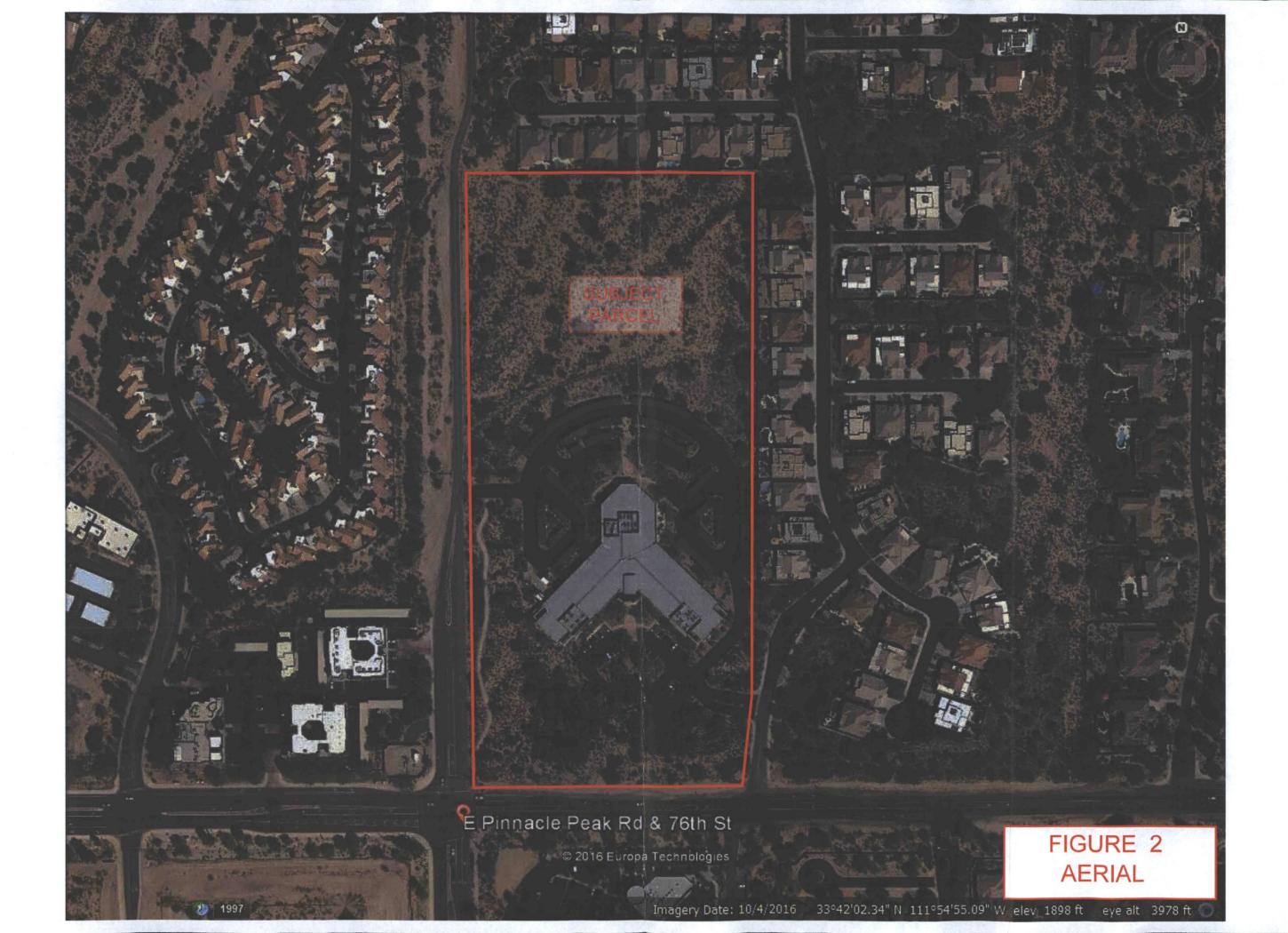


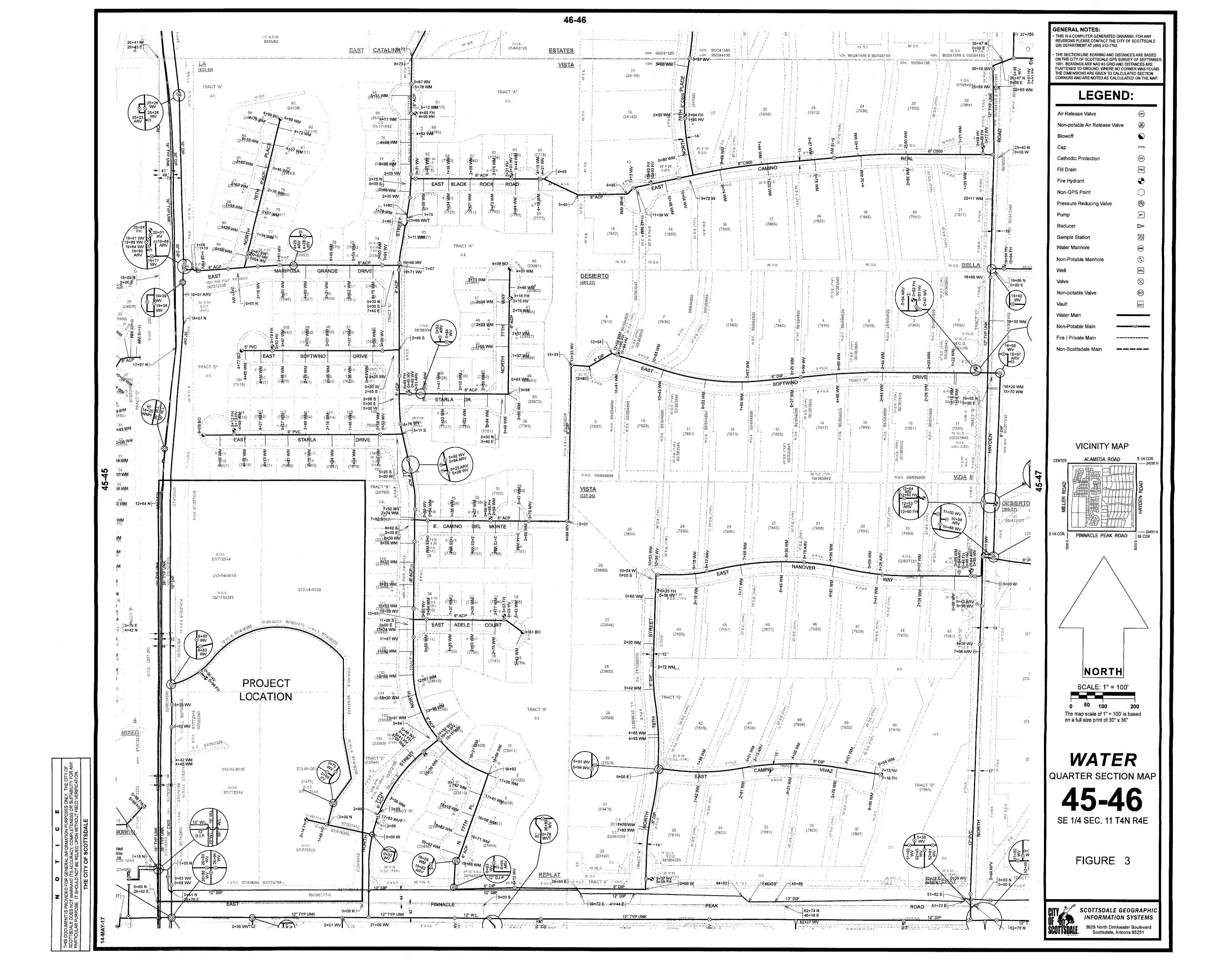
• The final plans will show water and sewer vertical clearances compliant with City and State separation or protection provisions.

# **REFERENCES**

1. City of Scottsdale Design Standards & Policies Manual-Chapter 6, Water

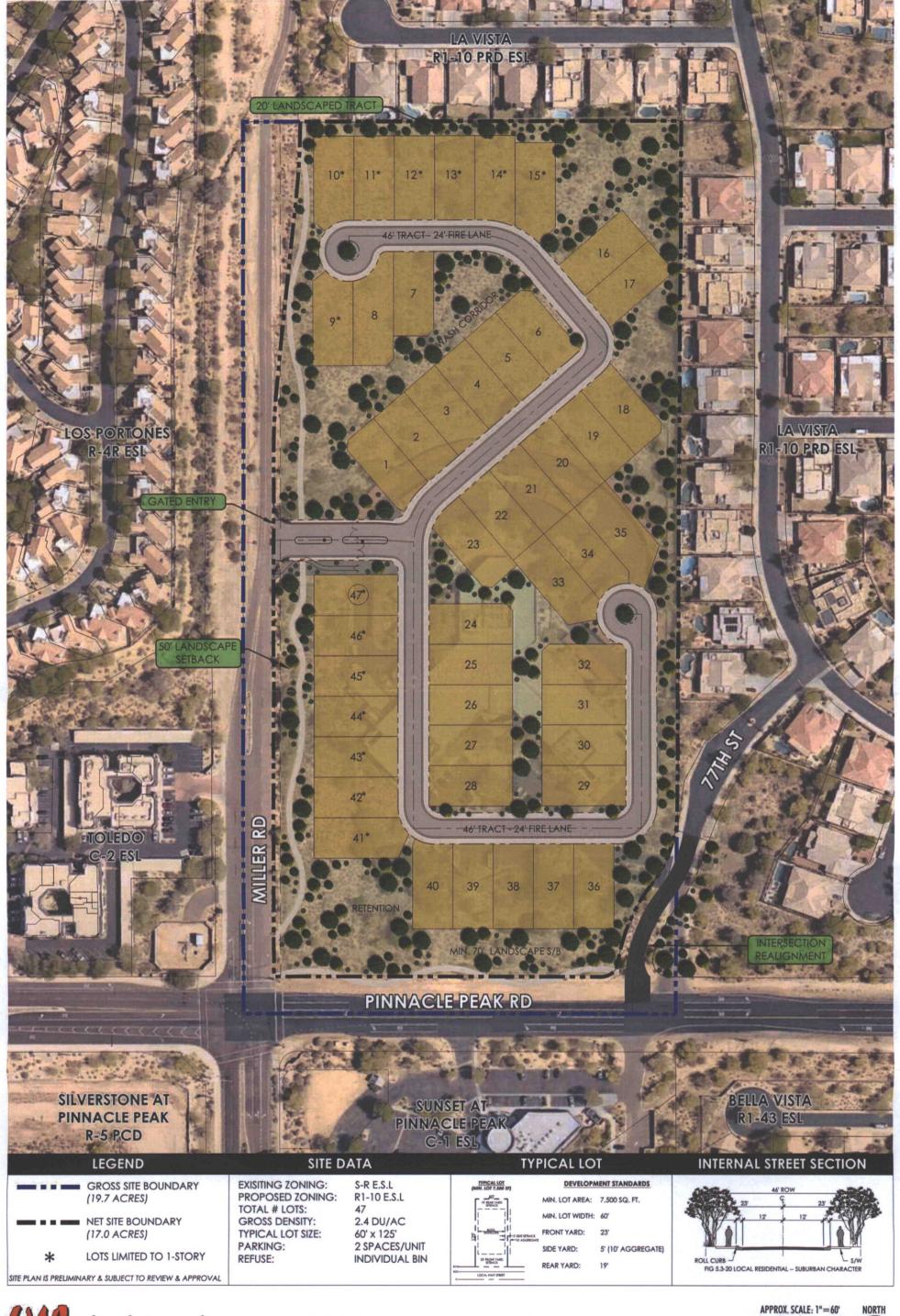








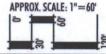
# APPENDIX I Flow Test Data

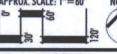




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### PINNACLE PEAK & MILLER





**CONCEPTUAL SITE PLAN** 



# APPENDIX I Calculations

| <b>Worksheet for</b> | 8" | sewer ( | 0 5=     | 1%  | for | 6000 | and |
|----------------------|----|---------|----------|-----|-----|------|-----|
| MOINSHIEL TO         | •  | 2CAAC!  | <b>-</b> | / . |     | 0000 | 904 |

| WOIKS                       | silection o sev | VCI @ 0-  | 70 101 0000 gpu |  |
|-----------------------------|-----------------|-----------|-----------------|--|
| Project Description         |                 |           |                 |  |
| Friction Method             | Manning Formula |           |                 |  |
| Solve For                   | Normal Depth    |           |                 |  |
| Input Data                  |                 |           |                 |  |
| Roughness Coefficient       |                 | 0.013     |                 |  |
| Channel Slope               |                 | 0.01000   | ft/ft           |  |
| Diameter                    |                 | 8.00      | in              |  |
| Discharge                   |                 | 6000.00   | gal/day         |  |
| Results                     |                 |           |                 |  |
| Normal Depth                |                 | 0.50      | in              |  |
| Flow Area                   |                 | 0.01      | ft²             |  |
| Wetted Perimeter            |                 | 0.34      | ft              |  |
| Hydraulic Radius            |                 | 0.32      | in              |  |
| Top Width                   |                 | 0.32      | ft              |  |
| Critical Depth              |                 | 0.04      | ft              |  |
| Percent Full                |                 | 6.3       | %               |  |
| Critical Slope              |                 | 0.00849   | ft/ft           |  |
| Velocity                    |                 | 1.02      | ft/s            |  |
| Velocity Head               |                 | 0.02      | ft              |  |
| Specific Energy             |                 | 0.06      | ft              |  |
| Froude Number               |                 | 1.07      |                 |  |
| Maximum Discharge           |                 | 1.30      | ft³/s           |  |
| Discharge Full              |                 | 780975.01 | gal/day         |  |
| Slope Full                  |                 | 0.00000   | ft/ft           |  |
| Flow Type                   | SuperCritical   |           |                 |  |
| GVF Input Data              |                 |           |                 |  |
| Downstream Depth            |                 | 0.00      | in              |  |
| Length                      |                 | 0.00      | ft              |  |
| Number Of Steps             |                 | 0         |                 |  |
| GVF Output Data             |                 |           |                 |  |
| Upstream Depth              |                 | 0.00      | in              |  |
| Profile Description         |                 |           |                 |  |
| Profile Headloss            |                 | 0.00      | ft              |  |
| Average End Depth Over Rise |                 | 0.00      | %               |  |
| Normal Depth Over Rise      |                 | 6.26      | %               |  |
| Downstream Velocity         |                 | Infinity  | ft/s            |  |

#### Worksheet for 8" sewer @ S=1% for 6000 gpd

#### **GVF Output Data**

| Upstream Velocity | Infinity | ft/s  |
|-------------------|----------|-------|
| Normal Depth      | 0.50     | in    |
| Critical Depth    | 0.04     | ft    |
| Channel Slope     | 0.01000  | ft/ft |
| Critical Slope    | 0.00849  | ft/ft |

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#### Worksheet for 8" sewer at S=1%, 65% full

#### **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 5.20 in

 Critical Depth
 0.45 ft

 Channel Slope
 0.01000 ft/ft

 Critical Slope
 0.00882 ft/ft



# APPENDIX II Preliminary Utility Plan





### PINNACLE PEAK & MILLER

FIGURE 4



1731



CONCEPTUAL SITE PLAN

### **Arizona Flow Testing LLC**

#### HYDRANT FLOW TEST REPORT

Project Name:

Not Provided

Project Address:

Miller and Pinnacle Peak, Scottsdale, Arizona 85255

Client Project No.:

Not Provided

Arizona Flow Testing Project No.:

17110

Flow Test Permit No.:

C53126

Date and time flow test conducted:

May 22, 2017 at 7:00 AM

Data is current and reliable until:

November 12, 2017

Conducted by: Witnessed by: Floyd Vaughan - Arizona Flow Testing, LLC (480-250-8154)

Larry Frandle – City of Scottsdale-Inspector (602-828-0847)

#### **Raw Test Data**

Static Pressure:

130.0 PSI

72.0 PSI

(Measured in pounds per square inch)

Static Pressure: (Measured in pounds per square inch)

Data with 58 PSI Safety Factor

Scottsdale requires a maximum Static Pressure of 72 PSI for AFES Design.

Residual Pressure:

108.0 PSI

(Measured in pounds per square inch)

Residual Pressure:

50.0 PSI

(Measured in pounds per square inch)

Pitot Pressure:

24.0 PSI (4 inch H.M.)

55.0 PSI (2 ½ inch)

(Measured in pounds per square inch)

Diffuser Orifice Diameter:

Distance between hydrants: Approx. 1150 Feet

(Measured in inches)

Main size: Not Provided

Coefficient of Diffuser: Big Boy Hose Monster

Flowing GPM:

3,087 GPM

One (4 inch)

(Measured in gallons per minute) 1,842 GPM + 1,245 GPM = 3,087 GPM Flowing GPM:

3.087 GPM

GPM @ 20 PSI:

7.361 GPM

GPM @ 20 PSI:

4,912 GPM

#### **Flow Test Location**

North



North Miller Street

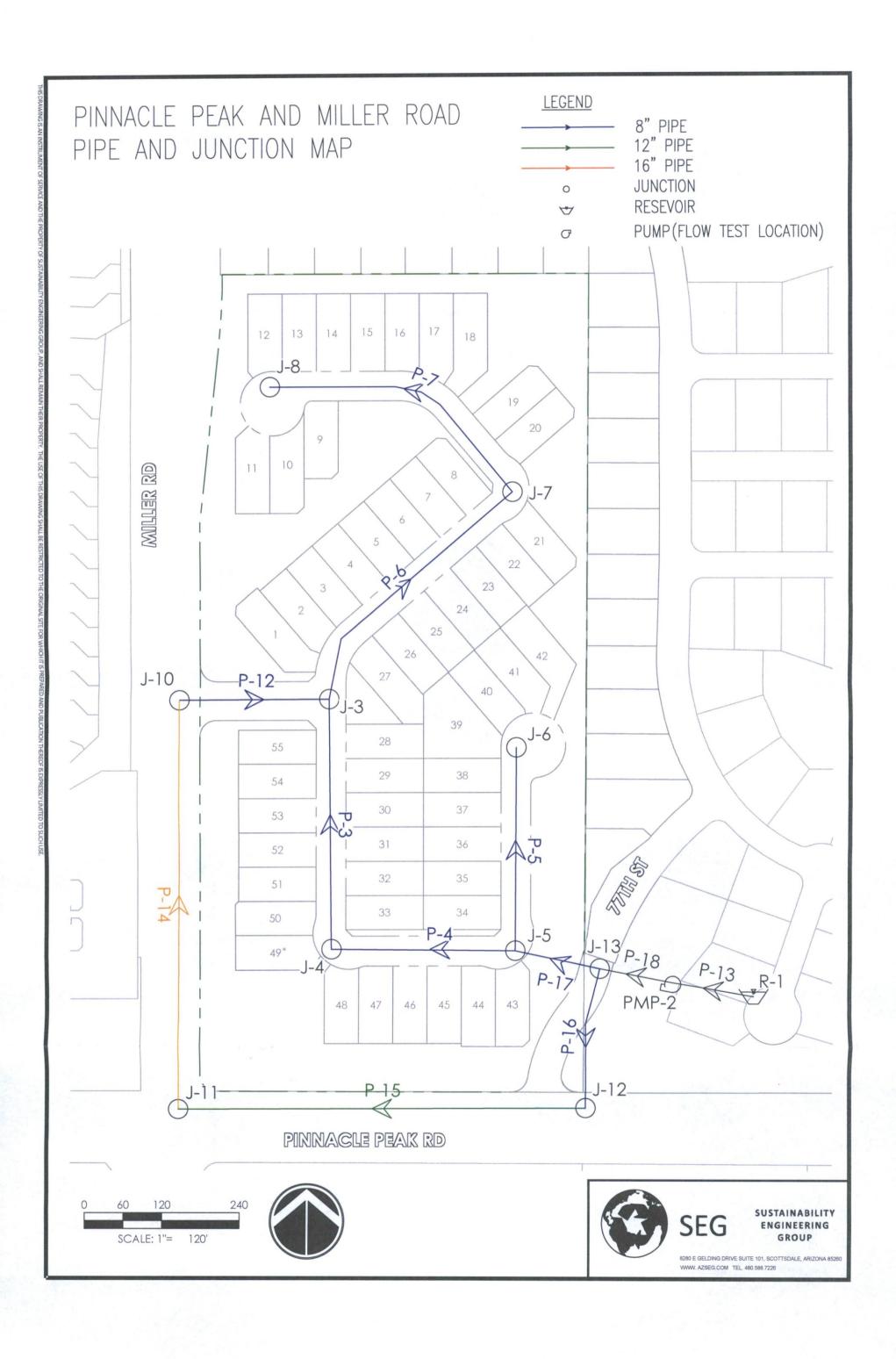
East Pinnacle Peak Road

Pressure Fire Hydrant

Flow Fire Hydrant



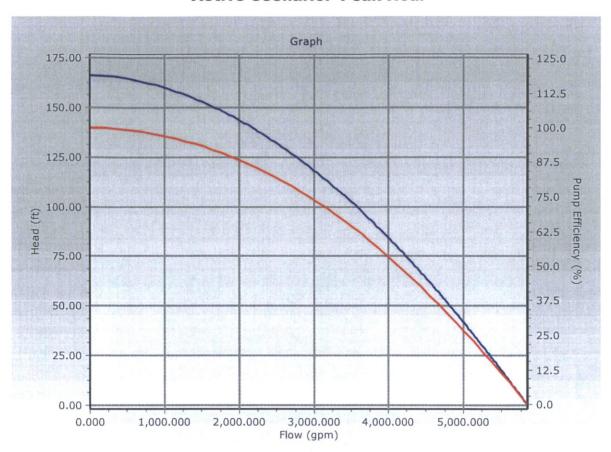
# APPENDIX II Water Model Results



## Pump Definition Detailed Report: Fire Flow Test Active Scenario: Peak Hour

| Element Details          |                             |                          |                   |
|--------------------------|-----------------------------|--------------------------|-------------------|
| ID                       | 59                          | Notes                    |                   |
| Label                    | Fire Flow Test              |                          |                   |
| Pump Definition Type     |                             |                          |                   |
| Pump Definition Type     | Standard (3<br>Point)       | Design Head              | 115.50 ft         |
| Shutoff Flow             | 0.000 gpm                   | Maximum Operating Flow   | 4,912.000 gpm     |
| Shutoff Head             | 166.32 ft                   | Maximum Operating Head   | 46.20 ft          |
| Design Flow              | 3,087.000 gpm               |                          |                   |
| Pump Efficiency Type     |                             |                          |                   |
| Pump Efficiency Type     | Best<br>Efficiency<br>Point | Motor Efficiency         | 100.0 %           |
| BEP Efficiency           | 100.0 %                     | Is Variable Speed Drive? | False             |
| BEP Flow                 | 0.000 gpm                   |                          |                   |
| Transient (Physical)     |                             |                          |                   |
| Inertia (Pump and Motor) | 0.000 lb·ft²                | Specific Speed           | SI=25,<br>US=1280 |
| Speed (Full)             | 0 rpm                       | Reverse Spin Allowed?    | True              |

## Pump Definition Detailed Report: Fire Flow Test Active Scenario: Peak Hour



## FlexTable: Junction Table Active Scenario: Average Day

| Label | Elevation<br>(ft) | Demand<br>(gpm) | Hydraulic Grade<br>(ft) | Pressure<br>(psi) |
|-------|-------------------|-----------------|-------------------------|-------------------|
| J-3   | 1,896.00          | 3.920           | 2,059.32                | 71                |
| J-4   | 1,882.00          | 3.267           | 2,059.32                | 77                |
| J-5   | 1,885.50          | 1.960           | 2,059.32                | 75                |
| J-6   | 1,895.50          | 1.960           | 2,059.32                | 71                |
| J-7   | 1,906.00          | 3.920           | 2,059.31                | 66                |
| J-8   | 1,900.50          | 2.940           | 2,059.31                | 69                |
| J-10  | 1,899.50          | 0.000           | 2,059.32                | 69                |
| J-11  | 1,876.00          | 0.000           | 2,059.32                | 79                |
| J-12  | 1,884.00          | 0.000           | 2,059.32                | 76                |
| J-13  | 1,888.00          | 0.000           | 2,059.32                | 74                |

## FlexTable: Pipe Table Active Scenario: Average Day

| Label | Length (Scaled)<br>(ft) | Start Node | Stop Node | Diameter<br>(in) | Hazen-Williams<br>C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------|-------------------------|------------|-----------|------------------|---------------------|---------------|--------------------|---------------------------------|
| P-3   | 387                     | J-3        | J-4       | 8.0              | 130.0               | -3.649        | 0.02               | 0.000                           |
| P-4   | 336                     | J-4        | J-5       | 8.0              | 130.0               | -6.916        | 0.04               | 0.000                           |
| P-5   | 313                     | J-5        | J-6       | 8.0              | 130.0               | 1.960         | 0.01               | 0.000                           |
| P-6   | 444                     | J-3        | J-7       | 8.0              | 130.0               | 6.860         | 0.04               | 0.000                           |
| P-7   | 446                     | J-7        | J-8       | 8.0              | 130.0               | 2.940         | 0.02               | 0.000                           |
| P-12  | 232                     | J-3        | J-10      | 8.0              | 130.0               | -7.131        | 0.05               | 0.000                           |
| P-13  | 129                     | R-1        | PMP-2     | 24.0             | 130.0               | 17.967        | 0.01               | 0.000                           |
| P-14  | 634                     | J-10       | J-11      | 16.0             | 130.0               | -7.131        | 0.01               | 0.000                           |
| P-15  | 632                     | J-11       | J-12      | 12.0             | 130.0               | -7.131        | 0.02               | 0.000                           |
| P-16  | 220                     | J-12       | J-13      | 8.0              | 130.0               | -7.131        | 0.05               | 0.000                           |
| P-17  | 85                      | J-13       | J-5       | 8.0              | 130.0               | 10.836        | 0.07               | 0.000                           |
| P-18  | 113                     | J-13       | PMP-2     | 24.0             | 130.0               | -17.967       | 0.01               | 0.000                           |

## FlexTable: Reservoir Table Active Scenario: Average Day

| Label | Elevation<br>(ft) | Zone          | Flow (Out net)<br>(gpm) | Hydraulic Grade<br>(ft) |  |
|-------|-------------------|---------------|-------------------------|-------------------------|--|
| R-1   | 1,893.00          | <none></none> | 17.967                  | 1,893.00                |  |

#### FlexTable: Pump Table

#### **Active Scenario: Average Day**

| Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade<br>(Suction)<br>(ft) | Hydraulic Grade<br>(Discharge)<br>(ft) | Flow (Total)<br>(gpm) | Pump Head<br>(ft) |
|-------|----------------|-----------------|------------------|--------------------------------------|--|-----------------------|-------------------|
| PMP-2 | 1,893.00       | Fire Flow Test  | On               | 1,893.00                             | 2,059.32                               | 17.967                | 166.32            |

#### FlexTable: Junction Table **Active Scenario: Max Day**

| Label | Elevation (ft) | Demand<br>(gpm) | Hydraulic Grade<br>(ft) | Pressure<br>(psi) |
|-------|----------------|-----------------|-------------------------|-------------------|
| J-3   | 1,896.00       | 7.840           | 2,059.30                | 71                |
| J-4   | 1,882.00       | 6.533           | 2,059.30                | 77                |
| J-5   | 1,885.50       | 3.920           | 2,059.31                | 75                |
| J-6   | 1,895.50       | 3.920           | 2,059.31                | 71                |
| J-7   | 1,906.00       | 7.840           | 2,059.30                | 66                |
| J-8   | 1,900.50       | 5.888           | 2,059.30                | 69                |
| J-10  | 1,899.50       | 0.000           | 2,059.30                | 69                |
| J-11  | 1,876.00       | 0.000           | 2,059.30                | 79                |
| J-12  | 1,884.00       | 0.000           | 2,059.31                | 76                |
| J-13  | 1,888.00       | 0.000           | 2,059.31                | 74                |

## FlexTable: Pipe Table Active Scenario: Max Day

| Label | Length (Scaled)<br>(ft) | Start Node | Stop Node | Diameter<br>(in) | Hazen-Williams<br>C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------|-------------------------|------------|-----------|------------------|---------------------|---------------|--------------------|---------------------------------|
| P-3   | 387                     | J-3        | ]-4       | 8.0              | 130.0               | -7.303        | 0.05               | 0.000                           |
| P-4   | 336                     | J-4        | J-5       | 8.0              | 130.0               | -13.836       | 0.09               | 0.000                           |
| P-5   | 313                     | J-5        | J-6       | 8.0              | 130.0               | 3.920         | 0.03               | 0.000                           |
| P-6   | 444                     | J-3        | J-7       | 8.0              | 130.0               | 13.728        | 0.09               | 0.000                           |
| P-7   | 446                     | J-7        | J-8       | 8.0              | 130.0               | 5.888         | 0.04               | 0.000                           |
| P-12  | 232                     | J-3        | J-10      | 8.0              | 130.0               | -14.265       | 0.09               | 0.000                           |
| P-13  | 129                     | R-1        | PMP-2     | 24.0             | 130.0               | 35.941        | 0.03               | 0.000                           |
| P-14  | 634                     | J-10       | J-11      | 16.0             | 130.0               | -14.265       | 0.02               | 0.000                           |
| P-15  | 632                     | J-11       | J-12      | 12.0             | 130.0               | -14.265       | 0.04               | 0.000                           |
| P-16  | 220                     | J-12       | J-13      | 8.0              | 130.0               | -14.265       | 0.09               | 0.000                           |
| P-17  | 85                      | J-13       | J-5       | 8.0              | 130.0               | 21.676        | 0.14               | 0.000                           |
| P-18  | 113                     | J-13       | PMP-2     | 24.0             | 130.0               | -35.941       | 0.03               | 0.000                           |

## FlexTable: Reservoir Table Active Scenario: Max Day

| Label | Elevation (ft) | Zone          | Flow (Out net)<br>(gpm) | Hydraulic Grade<br>(ft) |
|-------|----------------|---------------|-------------------------|-------------------------|
| R-1   | 1,893.00       | <none></none> | 35.941                  | 1,893.00                |

## FlexTable: Pump Table Active Scenario: Max Day

| Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade<br>(Suction)<br>(ft) | Hydraulic Grade<br>(Discharge)<br>(ft) | Flow (Total)<br>(gpm) | Pump Head<br>(ft) |
|-------|----------------|-----------------|------------------|--------------------------------------|--|-----------------------|-------------------|
| PMP-2 | 1,893.00       | Fire Flow Test  | On               | 1,893.00                             | 2,059.31                               | 35.941                | 166.31            |

#### Fire Flow Node FlexTable: Fire Flow Report Active Scenario: Max Day plus Fire Flow

| Label | Fire<br>Flow<br>(Needed<br>)<br>(gpm) | Fire Flow<br>(Available)<br>(gpm) | Flow<br>(Total<br>Needed)<br>(gpm) | Flow (Total<br>Available)<br>(gpm) | Pressure<br>(Residual<br>Lower<br>Limit)<br>(psi) | Pressure<br>(Calculated<br>Residual)<br>(psi) | Junction w/<br>Minimum<br>Pressure<br>(System) | Design<br>Velocity of<br>Maximum<br>Pipe<br>(ft/s) | Pipe w/<br>Maximum<br>Design<br>Velocity |
|-------|---------------------------------------|-----------------------------------|------------------------------------|------------------------------------|---|---|--|--|--|
| J-3   | 500.000                               | 2,881.643                         | 507.840                            | 2,889.483                          | 30  | 41  | J-7  | 10.00  | P-12                                     |
| J-4   | 500.000                               | 2,477.982                         | 506.533                            | 2,484.515                          | 30  | 55  | J-7  | 10.00  | P-17                                     |
| J-5   | 500.000                               | 1,913.295                         | 503.920                            | 1,917.215                          | 30  | 64  | J-7  | 10.00  | P-17                                     |
| J-6   | 500.000                               | 1,562.796                         | 503.920                            | 1,566.716                          | 30  | 58  | J-7  | 10.00  | P-5                                      |
| J-7   | 500.000                               | 1,552.988                         | 507.840                            | 1,560.828                          | 30  | 49  | J-8  | 10.00  | P-6                                      |
| J-8   | 500.000                               | 1,552.988                         | 505.888                            | 1,558.876                          | 30  | 43  | J-7  | 10.00  | P-6                                      |
| J-10  | 500.000                               | 2,411.292                         | 500.000                            | 2,411.292                          | 30  | 49  | J-7  | 10.00  | P-16                                     |
| J-11  | 500.000                               | 2,370.778                         | 500.000                            | 2,370.778                          | 30  | 60  | J-7  | 10.00  | P-16                                     |
| J-12  | 500.000                               | 2,205.603                         | 500.000                            | 2,205.603                          | 30  | 60  | J-7  | 10.00  | P-16                                     |
| J-13  | 500.000                               | 3,500.000                         | 500.000                            | 3,500.000                          | 30  | 46  | J-7  | 2.51   | P-18                                     |

# FlexTable: Junction Table Active Scenario: Max Day plus Fire Flow

| Label | Elevation<br>(ft) | Demand (gpm) | Hydraulic Grade<br>(ft) | Pressure<br>(psi) |
|-------|-------------------|--------------|-------------------------|-------------------|
| J-3   | 1,896.00          | 6.530        | 2,059.31                | 71                |
| J-4   | 1,882.00          | 4.570        | 2,059.31                | 75                |
| J-5   | 1,885.50          | 3.260        | 2,059.31                | 73                |
| J-6   | 1,895.50          | 4.570        | 2,059.31                | 70                |
| J-7   | 1,906.00          | 5.880        | 2,059.31                | 67                |
| J-8   | 1,900.50          | 5.880        | 2,059.30                | 68                |
| J-10  | 1,899.50          | 0.000        | 2,059.31                | 72                |
| J-11  | 1,876.00          | 0.000        | 2,059.31                | 78                |
| J-12  | 1,884.00          | 0.000        | 2,059.31                | 75                |
| J-13  | 1,888.00          | 0.000        | 2,059.31                | 72                |

## FlexTable: Pipe Table Active Scenario: Max Day plus Fire Flow

| Label | Length (Scaled)<br>(ft) | Start Node | Stop Node | Diameter<br>(in) | Hazen-Williams<br>C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------|-------------------------|------------|-----------|------------------|---------------------|---------------|--------------------|---------------------------------|
| P-3   | 387                     | J-3        | J-4       | 8.0              | 130.0               | -6.073        | 0.04               | 0.000                           |
| P-4   | 336                     | J-4        | J-5       | 8.0              | 130.0               | -10.643       | 0.07               | 0.000                           |
| P-5   | 313                     | J-5        | J-6       | 8.0              | 130.0               | 4.570         | 0.03               | 0.000                           |
| P-6   | 444                     | J-3        | J-7       | 8.0              | 130.0               | 11.760        | 0.08               | 0.000                           |
| P-7   | 446                     | J-7        | J-8       | 8.0              | 130.0               | 5.880         | 0.04               | 0.000                           |
| P-12  | 232                     | J-3        | J-10      | 8.0              | 130.0               | -12.217       | 0.08               | 0.000                           |
| P-13  | 129                     | R-1        | PMP-2     | 24.0             | 130.0               | 30.690        | 0.02               | 0.000                           |
| P-14  | 634                     | J-10       | J-11      | 16.0             | 130.0               | -12.217       | 0.02               | 0.000                           |
| P-15  | 632                     | J-11       | J-12      | 12.0             | 130.0               | -12.217       | 0.03               | 0.000                           |
| P-16  | 220                     | J-12       | J-13      | 8.0              | 130.0               | -12.217       | 0.08               | 0.000                           |
| P-17  | 85                      | J-13       | J-5       | 8.0              | 130.0               | 18.473        | 0.12               | 0.000                           |
| P-18  | 113                     | J-13       | PMP-2     | 24.0             | 130.0               | -30.690       | 0.02               | 0.000                           |

## FlexTable: Reservoir Table Active Scenario: Max Day plus Fire Flow

| Label | Elevation (ft) | Zone          | Flow (Out net)<br>(gpm) | Hydraulic Grade<br>(ft) |
|-------|----------------|---------------|-------------------------|-------------------------|
| R-1   | 1,893.00       | <none></none> | 30.690                  | 1,893.00                |

#### FlexTable: Pump Table

#### **Active Scenario: Max Day plus Fire Flow**

| Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade<br>(Suction)<br>(ft) | Hydraulic Grade<br>(Discharge)<br>(ft) | Flow (Total)<br>(gpm) | Pump Head<br>(ft) |
|-------|----------------|-----------------|------------------|--------------------------------------|--|-----------------------|-------------------|
| PMP-2 | 1,893.00       | Fire Flow Test  | On               | 1,893.00                             | 2,059.31                               | 30.690                | 166.31            |

## FlexTable: Junction Table Active Scenario: Peak Hour

| Label | Elevation (ft) | Demand<br>(gpm) | Hydraulic Grade<br>(ft) | Pressure<br>(psi) |
|-------|----------------|-----------------|-------------------------|-------------------|
| J-3   | 1,896.00       | 13.720          | 2,059.27                | 71                |
| J-4   | 1,882.00       | 11.433          | 2,059.27                | 77                |
| J-5   | 1,885.50       | 6.860           | 2,059.28                | 75                |
| J-6   | 1,895.50       | 6.860           | 2,059.28                | 71                |
| J-7   | 1,906.00       | 13.720          | 2,059.26                | 66                |
| J-8   | 1,900.50       | 10.292          | 2,059.26                | 69                |
| J-10  | 1,899.50       | 0.000           | 2,059.28                | 69                |
| J-11  | 1,876.00       | 0.000           | 2,059.28                | 79                |
| J-12  | 1,884.00       | 0.000           | 2,059.28                | 76                |
| J-13  | 1,888.00       | 0.000           | 2,059.28                | 74                |

### FlexTable: Pipe Table Active Scenario: Peak Hour

| Label | Length (Scaled)<br>(ft) | Start Node | Stop Node | Diameter<br>(in) | Hazen-Williams<br>C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------|-------------------------|------------|-----------|------------------|---------------------|---------------|--------------------|---------------------------------|
| P-3   | 387                     | J-3        | ]-4       | 8.0              | 130.0               | -12.775       | 0.08               | 0.000                           |
| P-4   | 336                     | J-4        | J-5       | 8.0              | 130.0               | -24.208       | 0.15               | 0.000                           |
| P-5   | 313                     | J-5        | J-6       | 8.0              | 130.0               | 6.860         | 0.04               | 0.000                           |
| P-6   | 444                     | J-3        | J-7       | 8.0              | 130.0               | 24.012        | 0.15               | 0.000                           |
| P-7   | 446                     | J-7        | J-8       | 8.0              | 130.0               | 10.292        | 0.07               | 0.000                           |
| P-12  | 232                     | J-3        | J-10      | 8.0              | 130.0               | -24.957       | 0.16               | 0.000                           |
| P-13  | 129                     | R-1        | PMP-2     | 24.0             | 130.0               | 62.885        | 0.04               | 0.000                           |
| P-14  | 634                     | J-10       | J-11      | 16.0             | 130.0               | -24.957       | 0.04               | 0.000                           |
| P-15  | 632                     | J-11       | J-12      | 12.0             | 130.0               | -24.957       | 0.07               | 0.000                           |
| P-16  | 220                     | J-12       | J-13      | 8.0              | 130.0               | -24.957       | 0.16               | 0.000                           |
| P-17  | 85                      | J-13       | J-5       | 8.0              | 130.0               | 37.928        | 0.24               | 0.000                           |
| P-18  | 113                     | J-13       | PMP-2     | 24.0             | 130.0               | -62.885       | 0.04               | 0.000                           |

## FlexTable: Reservoir Table Active Scenario: Peak Hour

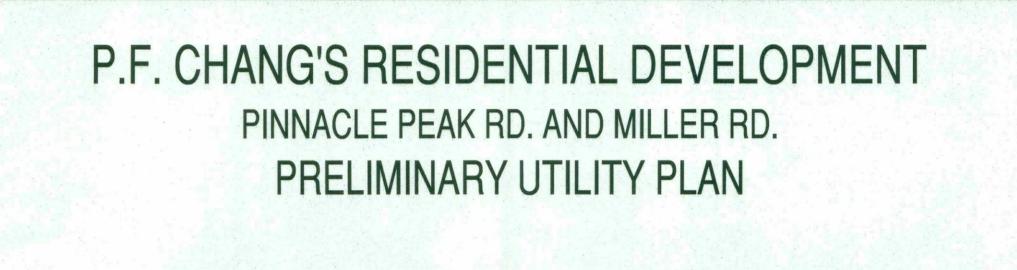
| Label | Elevation (ft) | Zone          | Flow (Out net)<br>(gpm) | Hydraulic Grade<br>(ft) |
|-------|----------------|---------------|-------------------------|-------------------------|
| R-1   | 1,893.00       | <none></none> | 62.885                  | 1,893.00                |

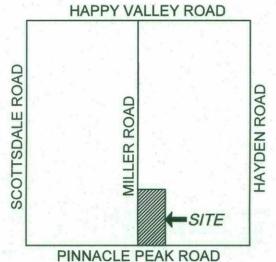
## FlexTable: Pump Table Active Scenario: Peak Hour

| Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade<br>(Suction)<br>(ft) | Hydraulic Grade<br>(Discharge)<br>(ft) | Flow (Total)<br>(gpm) | Pump Head<br>(ft) |
|-------|----------------|-----------------|------------------|--------------------------------------|--|-----------------------|-------------------|
| PMP-2 | 1,893.00       | Fire Flow Test  | On               | 1,893.00                             | 2,059.28                               | 62.885                | 166.28            |



# APPENDIX III Preliminary Utility Plan





APPLICANT/DEVELOPER

PFCCB PINNACLE PEAK LLC SNELL & WILMER 7676 E. PINNACLE PEAK RD. 400 E. VAN BUREN ST. #1900 PHOENIX, AZ 85004 PHONE: 602-328-6269 ATTN: NICK WOOD, ESQ

**OWNER** 

SCOTTSDALE, AZ 85255

ATTN: ZACH SHIRK

CIVIL ENGINEER

PLANNER

SUSTAINABILITY ENGINEERING GROUP VICINITY MAP

BASIS OF BEARING

THE BASIS OF BEARING AND ALL MONUMENTATION SHOWN



MALONEY

EXPIRES 9/30/2017

1. UTILITY CROSSINGS WILL BE DESIGNED FOR PROTECTION IN ACCORDANCE WITH MAG AND C.O.S. DESIGN CRITERIA.

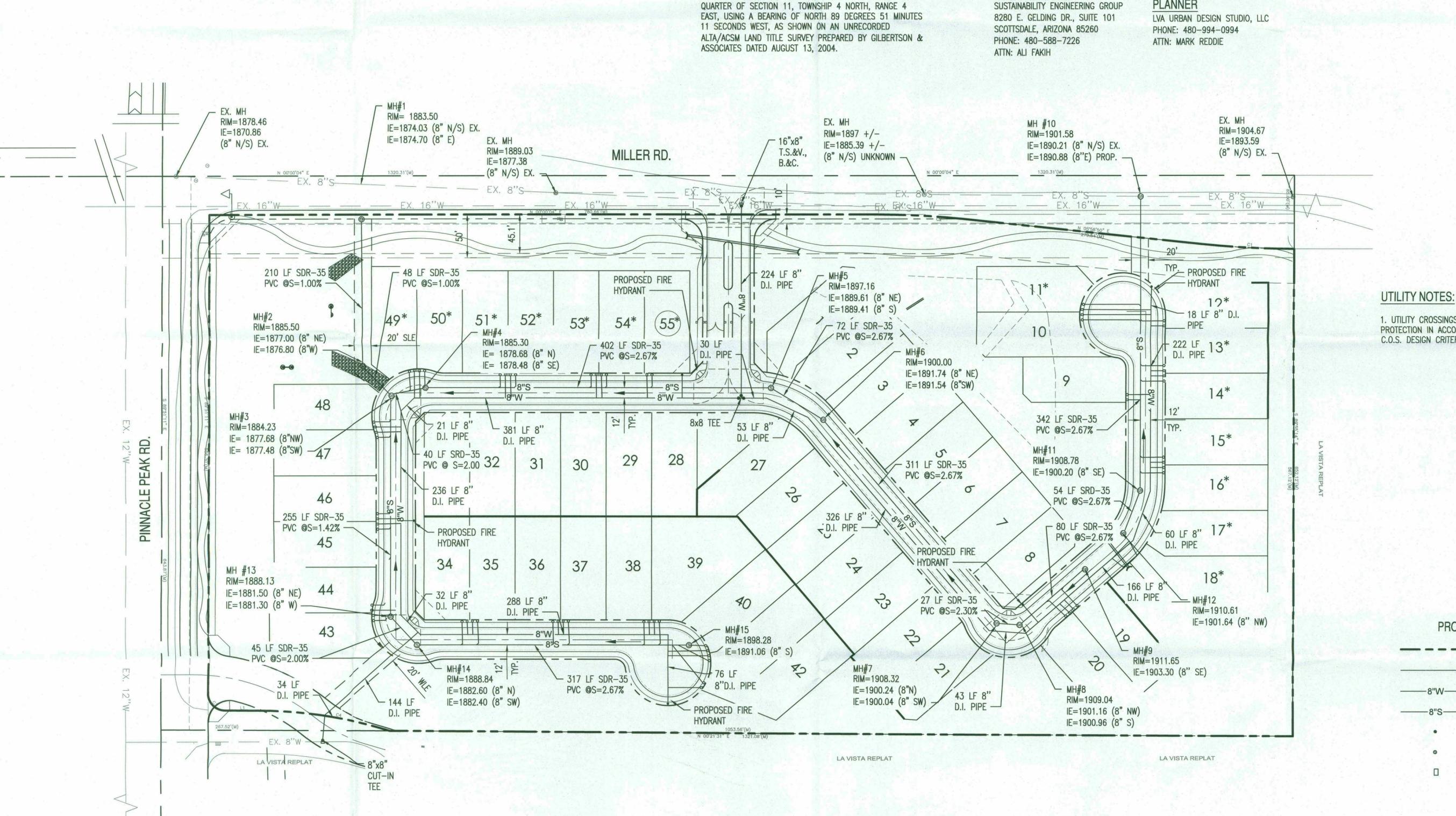
PROPOSED LEGEND PROPERTY LINE -----8"W------ WATER LINE 8"S—— SEWER LINE FIRE HYDRANT SEWER MANHOLE I" WATER METER

SANTIAGO MALONEY CHECKED -COUNSELL PROJ. MGR. — MALONEY 08/18/2017 ISSUED FOR: ZONING

REVISION NO .: JOB NO.: 170566

PRELIMINARY UTILITY PLAN

C4.00



SCALE: 1" = 60'

# PRELIMINARY SEWER CAPACITY REPORT NEC Pinnacle Peak Rd. & Miller Rd. Scottsdale, AZ

#### **Prepared For:**



7676 E. Pinnacle Peak Road Scottsdale, AZ 85255 P: 480.888.3000

Prepared by:



**Sustainability Engineering Group** 

8280 E. Gelding Drive, Suite 101 Scottsdale, AZ 85260 480.588.7226 www.az\$EG.com

Project Number: 170566

Original Submittal Date: June 22, 2017 (Zoning)

Case No.: 362-PA-2017 Plan Check No.: TBD

Accepted FOR ZNCATE

City of Scottsdale
Water Resources Administration
9379 E. San Salvador
Scottsdale, AZ 85258

Adolless nindr connents (Atlached) & submitin Ap CASE, LPillon 7-18-17



EXPIRES 9/30/2017



#### **PROJECT TRACKING SHEET**

|                     |                      |                            | STAFF CONTACT | TS                     |                |                |
|---------------------|----------------------|----------------------------|---------------|------------------------|----------------|----------------|
| CURRENT<br>PLANNING | DESIGN<br>CONSULTANT | ENGINEERING<br>Land Survey | FIRE          | LONG RANGE<br>PLANNING | STORM<br>WATER | TRANSPORTATION |
|                     | Steve V.             | DGue/dwayne                | R. King       | T. Reynolds            |                |                |

PROJECT NAME: 7676 E PINNACLE PEAK

Coordinator: Jesus Murillo Case#: 11-ZN-2017

ALL COMMENTS <u>MUST</u> INCLUDE THE ORDINANCE, POLICY, OR DSPM SECTION NUMBERS; PLEASE INITIAL AND DATE AT THE END OF EACH OF YOUR COMMENTS.

Tracking sheet boiler comments that are not applicable shall be struck out to indicate the reviewer has considered those particular comments; please do not delete comments from the Tracking Sheet in case if they become relevant in the resubmittal.

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|---|------|-------|------|-----|---------|--|
| W | AIER | OL OF | VVER | CON | MMEN 15 |  |

| SUBSTANTIVE | REVIEW: |
|-------------|---------|
|-------------|---------|

| <b>1</b> <sup>ST</sup>  | REVIEW COMPLETED BY LDILLON ON 07/18/17. | READY TO BE DETERMINED? | No 🗆 | YES 🗵 |
|---|--|-------------------------|------|-------|
| ADDRESS MINOR COMMENTS AND RESUBMIT FINAL BODS DURING PP CASE |  |                         |      |       |
| 2 <sup>ND</sup>   | REVIEW COMPLETED BY ????? ON ??/??/??.   | READY TO BE DETERMINED? | No 🗆 | YES   |
| 3 <sup>RD</sup>   | REVIEW COMPLETED BY ?????? ON ??/??/??.  | READY TO BE DETERMINED? | No 🗆 | YES 🗌 |

ALL COMMENTS <u>MUST</u> INCLUDE THE ORDINANCE, POLICY, OR DSPM SECTION NUMBERS; PLEASE INITIAL AND DATE AT THE END OF EACH OF YOUR COMMENTS.

#### **Ordinance Issues:**

1. None

#### Policy and Design Related Issues:

2. None

Technical Corrections to be resolved prior the next application or final plans submittal:

- Prelim water BOD, LDillon7/18/17:
  - a. Section 2.3.1,page 2: under Pinnacle Peak Road should read "unknown 44' north" and "potable 42' south". Note that the unknown line is a well line.
  - b. Section 2.3.1page 2: under Onsite note that this line is shown as 8" in our map system.
  - c. Section 3.1, section on Minimum pressure. These are two separate scenarios. Please model as such and update calculations.
    - Requirement is to have 50psi at highest finished floor with actual projected flow at worst case hydraulic node. The flow to be used in this scenario should be based on IPC 2015 Appendix B demand table, apply max day flows to other nodes.
    - ii. Model fire flow at worst case hydrant and ensure 30psi at hydrant tee with max day flows applied to all nodes and 15 psi min pressure to highest finished floor (or min required for sprinkler system).



# **PROJECT TRACKING SHEET**

- d. Utility Plan: several sewer/waterline crossing are indicated. Note that these must be handled per MAG and City design criteria.
- e. Utility plan: indicate distances between water and sewer lines where running parallel.
  - i. Calculation Table "Fire Flow Node Flex Table: Fire Flow Report, Active Scenario: Max Day plus Fire Flow" includes various data columns that are not clear. Description of what is being presented here is required.
- 4. Prelim wastewater BOD, LDillon7/18/17:
  - a. Section 4.2 should state 47 lots.
  - b. Section 5.5: Is 6,000 gpm the flow from half of the lots? Total average day flow is 11,750 per previous page. 6,000 gpm is also presented in Appendix I. where was the 1% drawn from. The utility plan shows various slopes, some exceeding 3.5%.
    - Calcs are not presented clearly, present velocity and depth for average and peak flows and then for hypothetical "full" pipe flow capacity i.e. d/D=0.65. Shows calcs for most relevant slopes/flows.
  - c. Utility Plan: several sewer/waterline crossings are indicated. Note that these must be handled per MAG and City design criteria. Note in final BOD.
  - d. Utility plan: indicate distances in final BOD between water and sewer lines where running in parallel. Conform to necessary separation/protection.

|--|

| Cinn | CTA | NTIV         | r D  | P1 // | F14/-    |
|------|-----|--------------|------|-------|----------|
| 311H | SIA | $\mathbf{n}$ | F 15 | rvi.  | F 1/1/ : |

| <b>1</b> <sup>ST</sup> | REVIEW COMPLETED BY PHIL K ON 7/17/17. | READY TO BE DETERMINED? | No ⊠ | YES 🗌 |
|------------------------|--|-------------------------|------|-------|
| 2 <sup>ND</sup>        | REVIEW COMPLETED BY ????? ON ??/??/??. | READY TO BE DETERMINED? | No 🗆 | YES 🗌 |
| 3 <sup>RD</sup>        | REVIEW COMPLETED BY ????? ON ??/??/??. | READY TO BE DETERMINED? | No 🗆 | YES   |

<u>Tracking sheet comments are not to be pasted in to the stipulations.</u> The comment need to be rewritten into the stipulation format in accordance with the direction provided in the stipulation.

# TRANSPORTATION STAFF COMMENTS:

5. The Transportation Department does not support the rezoning to residential due to the placement of residential homes in close proximity to two major streets, Miller Road and Pinnacle Peak Road, which are both planned to be four lane streets, and the major intersection of the two streets. Neither street is built out adjacent to the site, and the City is creating a situation where we will be allowing residents to purchase homes in this area who will then likely oppose future roadway construction. The site location should be conducive to S-R zoning, or a mixture of zoning that would keep non-residential on the corner.

#### Ordinance Issues:

- 6. Dedicate a minimum 50 feet of right-of-way along the Miller Road site frontage. There is currently insufficient right-of-way for signage and utilities. DSPM Sec. 5-3.100; Scottsdale Revised Code Sec. 47-10.
- 7. Complete the Pinnacle Peak Road minor arterial half street along the site frontage. Match the existing cross section to the west of Miller Road. The cross section shall include an 8 foot wide sidewalk. The improvements shall include appropriate transition to the existing pavement section to the east. DSPM Sec. 5-3.100; Scottsdale Revised Code Sec. 47-21 and 47-22.





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FIGURE 2 - Aerial

FIGURE 3 - COS Sewer Quarter Section Map

FIGURE 4 - Conceptual Site Plan

# APPENDIX:

Appendix I - Calculations

Appendix II - Preliminary Utility Plan



# 1. INTRODUCTION

# 1.1 SUMMARY OF PROPOSED DEVELOPMENT:

Proposed development consists of a maximum of forty-seven (47) residences fronting on a proposed internal 46' wide tract with 28' wide private roadways / cul-de-sacs. Main access is provided off North Miller Road which connects to East Pinnacle Peak Road to the south. Emergency access drives are proposed near the northwest corner from Miller Road and near the southeast corner onto 77th Street.

The purpose of this sewer capacity design report is to provide preliminary analysis of the impact that this development will have on the City's sewer system.

# 1.2 LEGAL DESCRIPTION:

The project property consists of four (4) parcels of land located at the NEC of North Miller Road and East Pinnacle Peak Road. The total project area contains approximately 855,802.3 SF (19.647 AC) gross; 749,876.2 SF (17.215 AC) net. It is further defined as follows:

• Parcel Description: The west half of Section 11, Township 4 North, Range 4 East of

the Gila and Salt River Base and Meridian, Maricopa County,

Scottsdale, Arizona

Parcel ID numbers: APN: 212-04-001B, 212-04-001C, 212-04-001D and 212-04

001E.

Parcel Address: 7676 E. Pinnacle Peak Road

The site is bounded by North Miller Road on the west, East Pinnacle Peak Road on the south, a portion of North 77<sup>th</sup> Street on the east near the SEC and the La Vista single family subdivision to the east and north.

Refer to FIGURE 1 - Vicinity Map for the project's location with respect to major cross streets

#### 1.3 EXISTING AND PROPOSED SITE ZONING AND LAND USES:

The project parcel is zoned S-R ESL (Service Residential Environmentally Sensitive Lands and falls under Zoning District Commercial and Industrial) per the City of Scottsdale Zoning Map 31 and is currently developed with a 50,728 SF office building, parking canopies and asphalt parking. There are existing designated and recorded N.A.O.S. areas along the south, west and north portions of the proposed project site area.

#### 1.4 REFERENCES:

The project site is shown in the City's General Plan Conceptual Land Use Map as Rural Neighborhoods.



# 2. DESIGN DOCUMENTATION

# 2.1 DESIGN COMPLIANCE:

The analysis of the proposed and existing sewer system is done in compliance with Chapter 7 – Wastewater of the City of Scottsdale 2010 update of the Design Standards & Policies Manual (DS&PM). Design flow calculations for the on-site system will be based on the recommendations in Section 7-1.403 of the DS&PM.

# 3. EXISTING CONDITIONS

#### 3.1 EXISTING ZONING & LAND USE:

Land ownership includes 17.22 +/- net acres over four (4) parcels of developed (office) and undeveloped land designated as S-R ESL. There are existing designated and recorded N.A.O.S. areas along the south, west and north portions of the proposed project site area. The project is proposed to rezone the parcel to R1-10.

# 3.2 EXISTING TOPOGRAPHY, VEGETATION AND LANDFORM FEATURES:

The site is both undeveloped natural desert and a developed office component roughly in the middle of the project site. Contour elevations range from approximately 1916 in the northeast corner to 1879 in the southwest corner, with an average slope at approximately 2.5% from northeast to southwest.

FIRM Map Number 04013C1310L dated October 16, 2013 indicates this site is designated as Zone "AO", however there has been a Letter of Map Revision (LOMR) 15-09-1857P with an effective date of June 10, 2016 which removed the project site from the Rawhide Wash Floodplain area and re-designated as "X", having a 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile.

Refer to **FIGURE 2** for an aerial of the overall project existing conditions.

# 3.3 EXISTING UTILITIES:

Sanitary Sewer: QS 45-46 City of Scottsdale

- North Miller Road: A City of Scottsdale public 8" PVC sewer main is shown in North Miller Road for the full length of the sites boundary with an existing manhole at the intersection of North Miller Road and East Pinnacle Peak Road, one existing manhole at the NWC of the project site and 2 additional existing manholes spaced approximately evenly between those. The invert elevation for the existing manhole at the intersection North Miller Road and East Pinnacle Peak Road is 1868.92 and a rim at 1878.35. The sewer main is located east of the center line on North Miller Road with the exception of the manhole at the intersection of North Miller Road and East Pinnacle Peak Road where the manhole is located west of the center line.
- <u>E. Pinnacle Peak Road:</u> A City of Scottsdale public 8" PVC sewer main is shown in East Pinnacle Peak Road for the full length of the sites boundary with two existing manholes

Sewer Capacity Report Page 2



in the intersection of North Miller Road and East Pinnacle Peak Road. A manhole located near the center of the parcel has an unspecified diameter sewer stub out to the project site. The invert of the stub out to the north is indicated as 1971.85 but it is assumed that the invert is more likely 1871.85 since the rim is indicated as 1883.70. A third manhole is located at the SEC of the project site. The sewer main is located approximately 24' south of the East Pinnacle Peak Road center line.

• 77<sup>th</sup> Street: No sewer mains are indicated in 77<sup>th</sup> Street.

Refer to FIGURE 3 for the City quarter section map (QS 45-46)

# 4. PROPOSED CONDITIONS

# 4.1 SITE PLAN:

Proposed development consists of a maximum of forty-seven (47) residences fronting on a proposed internal 46' wide tract with 28' wide private cul-de-sac. Main access is provided near the center of the parcel off North Miller Road which connects to East Pinnacle Peak Road to the south. Emergency access drives are proposed near the northwest corner from Miller Road and near the southeast corner onto the re-alignment of 77th Street, as proposed with this development.

Refer to **FIGURE 4** for proposed site layout.

# 4.2 PROPOSED SEWER SYSTEM:

It is proposed to construct a new 8" PVC sewer main in the new roadway to service the 48 lots. This service will then tie into the existing 8" PVC main in Miller Road approximately 200' north of Pinnacle Peak Road with a new manhole. Refer to Sheet C4.00 in **Appendix II** for the Preliminary Utility Plan.

#### 4.3 MAINTENANCE RESPONSIBILITIES:

The on-site sewer line for the proposed development will be public and located within right-of-way or easements to the City of Scottsdale. Therefore, the on-site and off-site sanitary sewer will be maintained by the City.

# 5. SANITARY SYSTEM COMPUTATIONS

#### 5.1. SEWER FLOW DEMANDS:

DS&PM, Chapter 7 Section 7-1.403 – Wastewater specifies that for residential uses, sanitary sewer lines 8 to 12 inches in diameter will be designed using 100 gallons per person per day and a peaking factor of 4. Residential densities are to assume 2.5 persons per dwelling unit.

Therefore, the average design flow is: 47 du x 100 gpcpd x 2.5 people/du = **11,750** gpd (Average Proposed)



#### 5.2. VARIANCE FROM STATED DESIGN FLOWS:

Stated design flows for the on-site system will be used as recommended.

#### 5.3. **DEMAND FACTORS:**

DS&PM requires a peak factor of 4.0 for residential usages. Therefore, from Section 5.1: 11,750 gpd x 4 = 47,000 gpd (Peak)

# 5.4. SEWER SYSTEM ANALYSIS (Existing On-Site):

As a comparison, the existing site has a 50,728 SF office building. The calculated average design flow is 50,728 SF x 0.4 per SF = 20,291 gpd (Average Existing).

DS&PM requires a peak factor of 3.0 for office use. Therefore, from Section 5.1, the existing peak demand is 20.291 gpd x 3 = 60.873 gpd (Peak).

The proposed sanitary sewer demands that will contribute to the intersection of North Miller Road and East Pinnacle Peak Road are approximately a 21% reduction from the existing contribution to the same point of the existing public sewer system. This will allow additional capacity in the main downstream from this point by providing a reduction of approximately, 8,541 gpd (Average) and 13,873 gpd (Peak) to the sewer demand. 11,750 ON pg.3

#### SEWER CAPACITY CALCULATIONS

SEWER CAPACITY CALCULATIONS

8.16 gp m

The site layout approximately splits the units to two sewer laterals. Therefore, to provide a minimum 1 fps under average flow conditions (6,000 gpd), an 8" diameter sanitary sewer pipe at S=1.0% (n=0.013) is proposed. This provides a velocity of 1.02 fps at a depth of 0.50" and has a flow capacity at 65% full of approximately 590,736 gpd, providing adequate 26 Eps @ 0.72" LEpth @ 3 3 gpm = \$ 1,36" capacity for the on-site system. Refer to Appendix I for Flowmaster calculations.

# 6. SUMMARY

#### 6 1 SUMMARY OF PROPOSED IMPROVEMENTS:

- The proposed wastewater improvement was designed based on the current Cit Scottsdale's design standards and policies.
- The existing sanitary main being tied into is capable of supporting the projected average flow for the development.
- The proposed development provides a reduction in sewer capacity demand compared to the existing development.

#### 6.2 PROJECT SCHEDULE:

As a residential development, the infrastructure is proposed to be constructed in a single phase to accommodate dwelling unit growth. The dwelling units may be phased based on consumer demand.

Sewer Capacity Report

Page 4



# **7 SUPPORTING MAPS**

# 7.1 PRELIMINARY UTILITY PLAN

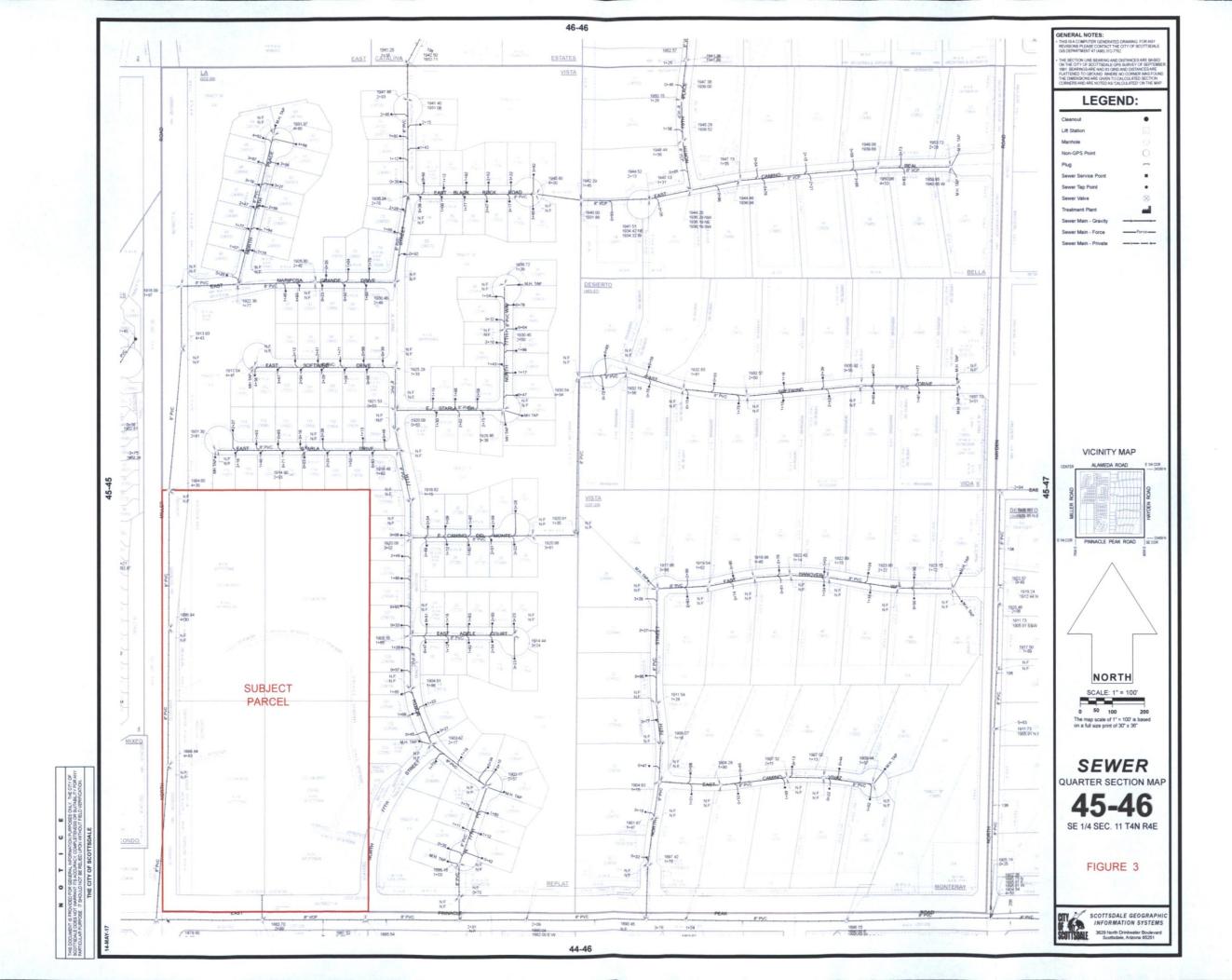
Refer to Preliminary Utility Plan (C4.00)

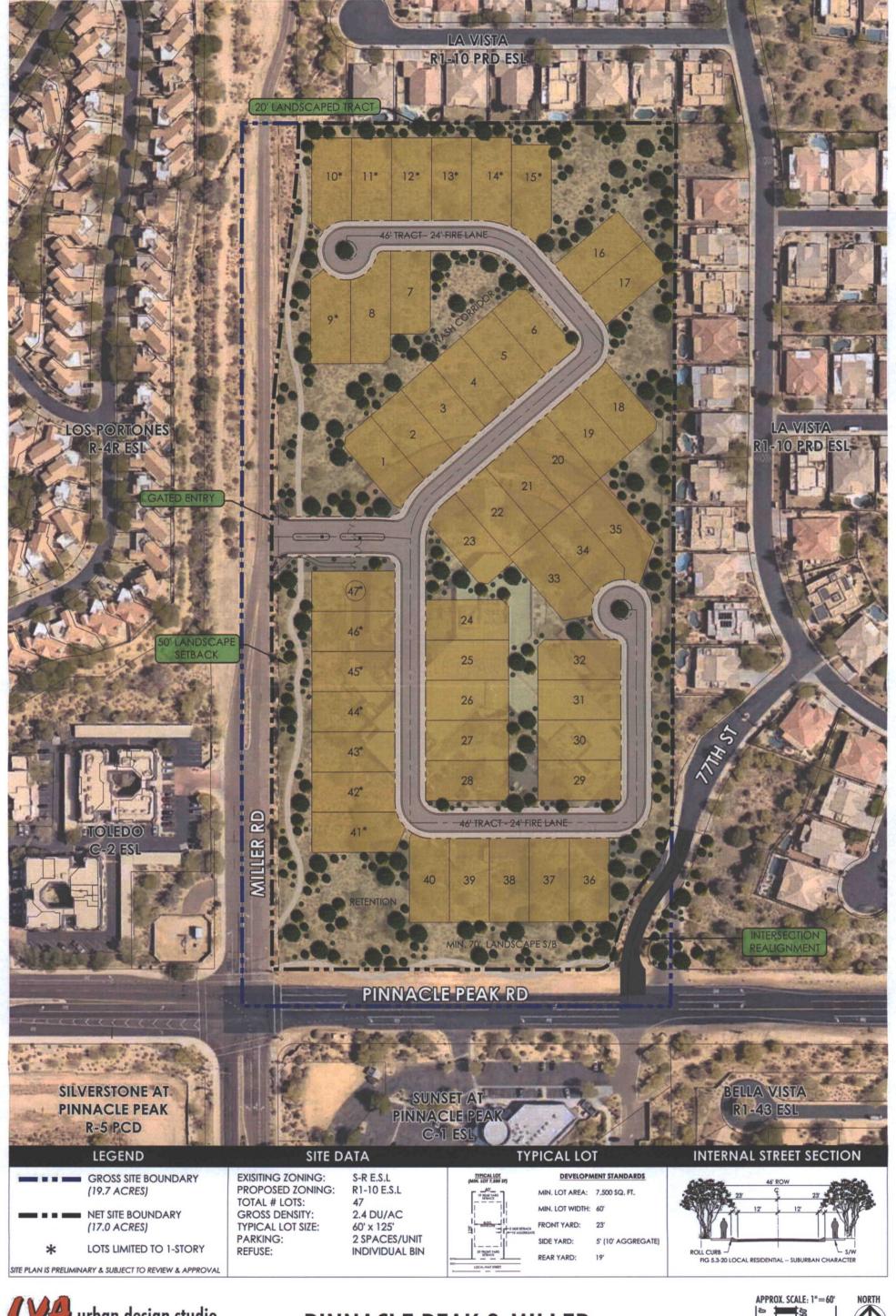
# 8 REFERENCES

- 1. COS QS Sewer Plan number 45-46
- 2. City of Scottsdale Design Standards & Policies Manual, 2010 (Chapter 7 Wastewater)











120 south ash avenue • tempe, arizona 85281 • 480.994.0994

# PINNACLE PEAK & MILLER



DRAWN BY: PR



# APPENDIX I Calculations

# Worksheet for 8" sewer @ S=1% for 6000 gpd

| Wor                         | ksheet for 8" sev | wer @ S=1 | l% for 6000 gpd |
|-----------------------------|-------------------|-----------|-----------------|
| Project Description         |                   |           |                 |
| Friction Method             | Manning Formula   |           |                 |
| Solve For                   | Normal Depth      |           |                 |
| Input Data                  |                   |           |                 |
| Roughness Coefficient       |                   | 0.013     |                 |
| Channel Slope               |                   | 0.01000   | ft/ft           |
| Diameter                    |                   | 8.00      | in              |
| Discharge                   |                   | 6000.00   | gal/day         |
| Results                     |                   |           |                 |
| Normal Depth                |                   | 0.50      | in              |
| Flow Area                   |                   | 0.01      | ft²             |
| Wetted Perimeter            |                   | 0.34      | ft              |
| Hydraulic Radius            |                   | 0.32      | in              |
| Top Width                   |                   | 0.32      | ft              |
| Critical Depth              |                   | 0.04      | ft              |
| Percent Full                |                   | 6.3       | %               |
| Critical Slope              |                   | 0.00849   | ft/ft           |
| Velocity                    |                   | 1.02      | ft/s            |
| Velocity Head               |                   | 0.02      | ft              |
| Specific Energy             |                   | 0.06      | ft              |
| Froude Number               |                   | 1.07      |                 |
| Maximum Discharge           |                   | 1.30      | ft³/s           |
| Discharge Full              |                   | 780975.01 | gal/day         |
| Slope Full                  |                   | 0.00000   | ft/ft           |
| Flow Type                   | SuperCritical     |           |                 |
| GVF Input Data              |                   |           |                 |
| Downstream Depth            |                   | 0.00      | in              |
| Length                      |                   | 0.00      | ft              |
| Number Of Steps             |                   | 0         |                 |
| GVF Output Data             |                   |           |                 |
| Upstream Depth              |                   | 0.00      | in              |
| Profile Description         |                   |           |                 |
| Profile Headloss            |                   | 0.00      | ft              |
| Average End Depth Over Rise |                   | 0.00      | %               |
| Normal Depth Over Rise      |                   | 6.26      | %               |
|                             |                   |           |                 |

Infinity ft/s

Downstream Velocity

# Worksheet for 8" sewer @ S=1% for 6000 gpd

# **GVF Output Data**

| Upstream Velocity | Infinity | ft/s  |
|-------------------|----------|-------|
| Normal Depth      | 0.50     | in    |
| Critical Depth    | 0.04     | ft    |
| Channel Slope     | 0.01000  | ft/ft |
| Critical Slope    | 0.00849  | ft/ft |

| Wo                          | orksheet for 8" s | ewer at S | =1%, 65% full |     |
|-----------------------------|-------------------|-----------|---------------|-----|
| Project Description         |                   |           |               |     |
| Friction Method             | Manning Formula   |           |               |     |
| Solve For                   | Discharge         |           |               |     |
| Input Data                  |                   |           |               |     |
| Roughness Coefficient       |                   | 0.013     |               |     |
| Channel Slope               |                   | 0.01000   | ft/ft         |     |
| Normal Depth                |                   | 5.20      | in            |     |
| Diameter                    |                   | 8.00      | in            |     |
| Results                     |                   |           |               |     |
| Discharge                   |                   | 590736.08 | gal/day       |     |
| Flow Area                   |                   | 0.24      | ft²           |     |
| Wetted Perimeter            |                   | 1.25      | ft            |     |
| Hydraulic Radius            |                   | 2.31      | in            |     |
| Top Width                   |                   | 0.64      | ft            |     |
| Critical Depth              |                   | 0.45      | ft            |     |
| Percent Full                |                   | 65.0      | %             |     |
| Critical Slope              |                   | 0.00882   | ft/ft         |     |
| Velocity                    |                   | 3.81      | ft/s          |     |
| Velocity Head               |                   | 0.23      | ft            |     |
| Specific Energy             |                   | 0.66      | ft            |     |
| Froude Number               |                   | 1.09      |               |     |
| Maximum Discharge           |                   | 1.30      | ft³/s         |     |
| Discharge Full              |                   | 780975.01 | gal/day       |     |
| Slope Full                  |                   | 0.00572   | ft/ft         |     |
| Flow Type                   | SuperCritical     |           |               |     |
| GVF Input Data              |                   |           |               | 466 |
| Downstream Depth            |                   | 0.00      | in            |     |
| Length                      |                   | 0.00      | ft            |     |
| Number Of Steps             |                   | 0         |               |     |
| GVF Output Data             |                   |           |               |     |
| Upstream Depth              |                   | 0.00      | in            |     |
| Profile Description         |                   |           |               |     |
| Profile Headloss            |                   | 0.00      | ft            |     |
| Average End Depth Over Rise |                   | 0.00      | %             |     |
| 275 M                       |                   |           |               |     |

65.00 %

Infinity ft/s

Normal Depth Over Rise Downstream Velocity

# Worksheet for 8" sewer at S=1%, 65% full

# **GVF Output Data**

**Upstream Velocity** Infinity ft/s Normal Depth 5.20 in Critical Depth 0.45 ft Channel Slope 0.01000 ft/ft Critical Slope 0.00882 ft/ft



# APPENDIX II Preliminary Utility Plan

# P.F. CHANG'S RESIDENTIAL DEVELOPMENT

# PINNACLE PEAK RD. AND MILLER RD. PRELIMINARY UTILITY PLAN

THE BASIS OF BEARING AND ALL MONUMENTATION SHOWN

QUARTER OF SECTION 11, TOWNSHIP 4 NORTH, RANGE 4 EAST, USING A BEARING OF NORTH 89 DEGREES 51 MINUTES

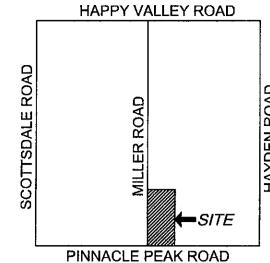
11 SECONDS WEST, AS SHOWN ON AN UNRECORDED

ASSOCIATES DATED AUGUST 13, 2004.

HEREON IS BASED ON THE SOUTH LINE OF THE SOUTHEAST

ALTA/ACSM LAND TITLE SURVEY PREPARED BY GILBERTSON &

BASIS OF BEARING



VICINITY MAP

**OWNER** 

PFCCB PINNACLE PEAK LLC 7676 E. PINNACLE PEAK RD. SCOTTSDALE, AZ 85255 ATTN:ZACH SHIRK

# CIVIL ENGINEER

SUSTAINABILITY ENGINEERING GROUP 8280 E. GELDING DR., SUITE 101 SCOTTSDALE, ARIZONA 85260 PHONE: 480-588-7226 ATTN: ALI FAKIH

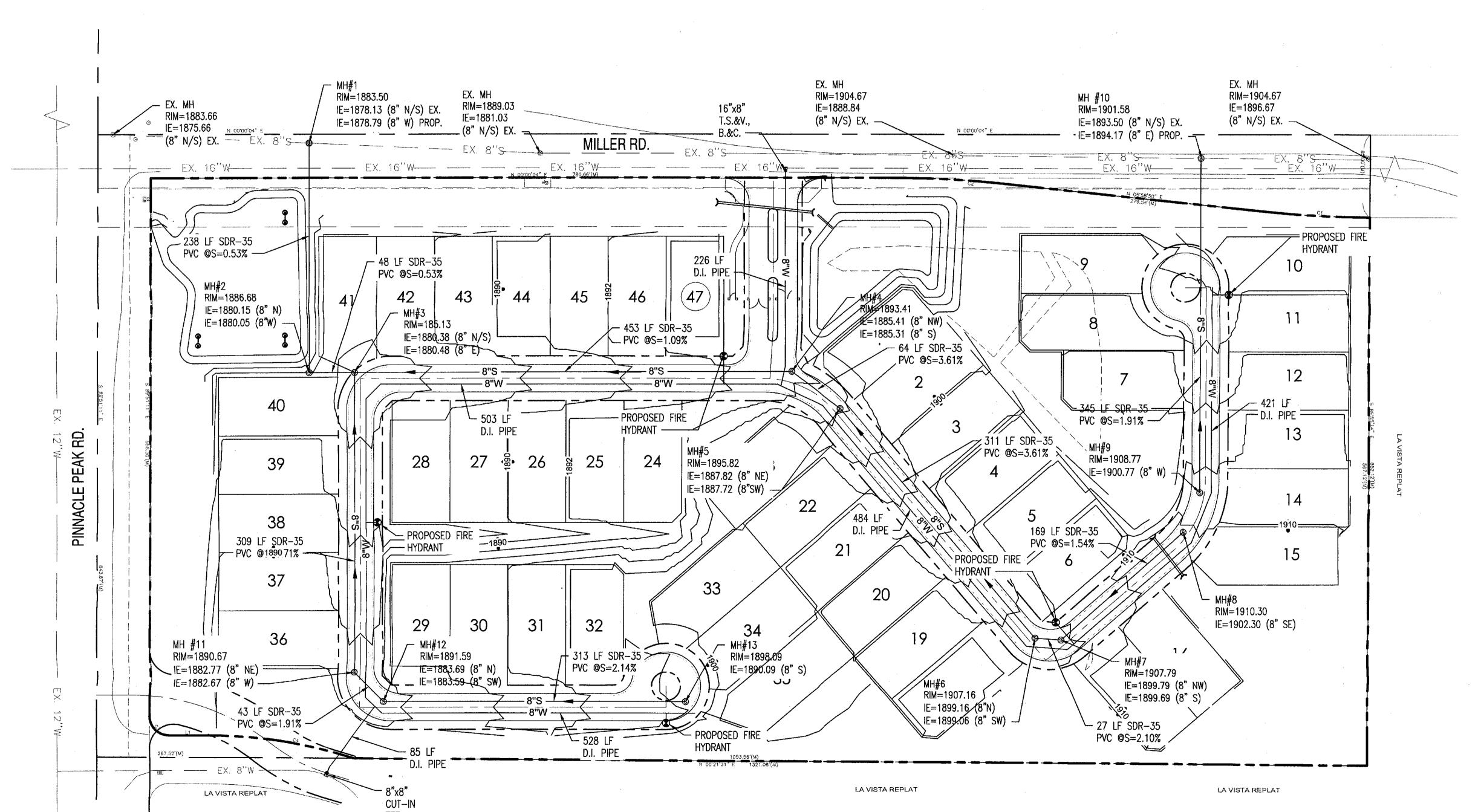
SNELL & WILMER

APPLICANT/DEVELOPER

400 E. VAN BUREN ST. #1900 PHOENIX, AZ 85004 PHONE: 602-328-6269 ATTN: NICK WOOD, ESQ

# **PLANNER**

LVA URBAN DESIGN STUDIO, LLC PHONE: 480-994-0994 ATTN: MARK REDDIE



SCALE: 1" = 60'

# PROPOSED LEGEND

|     | PROPERTY LIN |
|-----|--------------|
| 8"W | WATER LINE   |
| 8"S | SEWER LINE   |
| •   | FIRE HYDRANT |
|     |              |

SEWER MANHOLE

ISSUED FOR:

DESIGNED -

PROJ. MGR. —

CHECKED — COUNSELL

06/21/2017

MALONEY

DATE:

JOB NO.: 170566

PRELIMINARY UTILITY PLAN

C4.00

Dial 8-1-1 or 1-800-STAKE-IT (782-534 In Maricopa County: (602) 263-1100

SUSTAINABILITY
ENGINEERING

EXPIRES 9/30/2017

# PRELIMINARY WATER CAPACITY REPORT NEC Pinnacle Peak Rd. & Miller Rd. Scottsdale, AZ

# **Prepared For:**



7676 E. Pinnacle Peak Road Scottsdale, AZ 85255 P: 480.888.3000 Accepted FOR ZN CASE

City of Scottsdale

City of Scottsdale
Water Resources Administration
9379 E. San Salvador

Scottsdale, AZ 85258
Addless MINOR CORNEW & (4th

& SUBNIT IN PPLASE LDILLON

Prepared by:



**Sustainability Engineering Group** 

8280 E. Gelding Drive, Suite 101 Scottsdale, AZ 85260 480.588.7226 www.azSEG.com

Project Number: 170566

Original Submittal Date: June 22, 2017 (Zoning)

Case No.: 362-PA-2017 Plan Check No.: TBD



EXPIRES 9/30/2017



# PROJECT TRACKING SHEET

|                                    |          |                            | STAFF CONTACT | S                               |  |                |
|------------------------------------|----------|----------------------------|---------------|---------------------------------|--|----------------|
| CURRENT DESIGN PLANNING CONSULTANT |          | ENGINEERING<br>Land Survey | FIRE          | LONG RANGE STORM PLANNING WATER |  | TRANSPORTATION |
|                                    | Steve V. | DGue/dwayne                | R. King       | T. Reynolds                     |  |                |

PROJECT NAME: 7676 E PINNACLE PEAK

Coordinator: Jesus Murillo Case#: 11-ZN-2017

ALL COMMENTS <u>MUST</u> INCLUDE THE ORDINANCE, POLICY, OR DSPM SECTION NUMBERS; PLEASE INITIAL AND DATE AT THE END OF EACH OF YOUR COMMENTS.

Tracking sheet boiler comments that are not applicable shall be struck out to indicate the reviewer has considered those particular comments; please do not delete comments from the Tracking Sheet in case if they become relevant in the resubmittal.

# **WATER & SEWER COMMENTS:**

SUBSTANTIVE REVIEW:

| <b>1</b> <sup>ST</sup> | REVIEW COMPLETED BY LDILLON ON 07/18/17.          | READY TO BE DETERMINED? | No 🗆 | YES 🗵 |
|------------------------|---|-------------------------|------|-------|
| ADI                    | DRESS MINOR COMMENTS AND RESUBMIT FINAL BODS DURI | NG PP CASE              |      |       |
| 2 <sup>ND</sup>        | REVIEW COMPLETED BY ????? ON ??/??/??.            | READY TO BE DETERMINED? | No 🗆 | YES 🗆 |
| 3 <sup>RD</sup>        | REVIEW COMPLETED BY ????? ON ??/??/??.            | READY TO BE DETERMINED? | No 🗆 | YES   |

ALL COMMENTS <u>MUST</u> INCLUDE THE ORDINANCE, POLICY, OR DSPM SECTION NUMBERS; PLEASE INITIAL AND DATE AT THE END OF EACH OF YOUR COMMENTS.

#### Ordinance Issues:

1. None

# **Policy and Design Related Issues:**

None

# Technical Corrections to be resolved prior the next application or final plans submittal:

- Prelim water BOD, LDillon7/18/17:
  - a. Section 2.3.1,page 2: under Pinnacle Peak Road should read "unknown 44' north" and "potable 42' south". Note that the unknown line is a well line.
  - b. Section 2.3.1page 2: under Onsite note that this line is shown as 8" in our map system.
  - Section 3.1, section on Minimum pressure. These are two separate scenarios. Please model as such and update calculations.
    - Requirement is to have 50psi at highest finished floor with actual projected flow at worst case hydraulic node. The flow to be used in this scenario should be based on IPC 2015 Appendix B demand table, apply max day flows to other nodes.
    - Model fire flow at worst case hydrant and ensure 30psi at hydrant tee with max day flows applied to all nodes and 15 psi min pressure to highest finished floor (or min required for sprinkler system).



# **PROJECT TRACKING SHEET**

- d. Utility Plan: several sewer/waterline crossing are indicated. Note that these must be handled per MAG and City design criteria.
- e. Utility plan: indicate distances between water and sewer lines where running parallel.
  - Calculation Table "Fire Flow Node Flex Table: Fire Flow Report, Active Scenario: Max Day plus Fire Flow" includes various data columns that are not clear. Description of what is being presented here is required.
- Prelim wastewater BOD, LDillon7/18/17:
  - a. Section 4.2 should state 47 lots.
  - b. Section 5.5: Is 6,000 gpm the flow from half of the lots? Total average day flow is 11,750 per previous page. 6,000 gpm is also presented in Appendix I. where was the 1% drawn from. The utility plan shows various slopes, some exceeding 3.5%.
    - Calcs are not presented clearly, present velocity and depth for average and peak flows and then for hypothetical "full" pipe flow capacity i.e. d/D=0.65. Shows calcs for most relevant slopes/flows.
  - c. Utility Plan: several sewer/waterline crossings are indicated. Note that these must be handled per MAG and City design criteria. Note in final BOD.
  - d. Utility plan: indicate distances in final BOD between water and sewer lines where running in parallel. Conform to necessary separation/protection.

|                | -         |
|----------------|-----------|
| TRANSPORTATION | COMMENTS: |

| -    | 2000 |         | -   |      |
|------|------|---------|-----|------|
| STID | CTAI | NITINIE | DEV | IEW: |
|      |      |         |     |      |

|                        |  | · ·                     |      |       |
|------------------------|--|-------------------------|------|-------|
| <b>1</b> <sup>ST</sup> | REVIEW COMPLETED BY PHIL K ON 7/17/17. | READY TO BE DETERMINED? | No 🗵 | YES 🗌 |
| 2 <sup>ND</sup>        | REVIEW COMPLETED BY ????? ON ??/??/??. | READY TO BE DETERMINED? | No 🗆 | YES 🗌 |
| 3 <sup>RD</sup>        | REVIEW COMPLETED BY ????? ON ??/??/??. | READY TO BE DETERMINED? | No 🗆 | YES   |

Tracking sheet comments are not to be pasted in to the stipulations. The comment need to be rewritten into the stipulation format in accordance with the direction provided in the stipulation.

# **TRANSPORTATION STAFF COMMENTS:**

5. The Transportation Department does not support the rezoning to residential due to the placement of residential homes in close proximity to two major streets, Miller Road and Pinnacle Peak Road, which are both planned to be four lane streets, and the major intersection of the two streets. Neither street is built out adjacent to the site, and the City is creating a situation where we will be allowing residents to purchase homes in this area who will then likely oppose future roadway construction. The site location should be conducive to S-R zoning, or a mixture of zoning that would keep non-residential on the corner.

#### Ordinance Issues:

- 6. Dedicate a minimum 50 feet of right-of-way along the Miller Road site frontage. There is currently insufficient right-of-way for signage and utilities. DSPM Sec. 5-3.100; Scottsdale Revised Code Sec. 47-10.
- 7. Complete the Pinnacle Peak Road minor arterial half street along the site frontage. Match the existing cross section to the west of Miller Road. The cross section shall include an 8 foot wide sidewalk. The improvements shall include appropriate transition to the existing pavement section to the east. DSPM Sec. 5-3.100; Scottsdale Revised Code Sec. 47-21 and 47-22.



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# 1. EXECUTIVE SUMMARY

The subject project is the proposed redevelopment of the existing P.F. Chang's office complex located at the NEC of North Miller Road and East of Pinnacle Peak Road into a residential development. The parcels are currently zoned S-R ESL (Service Residential Environmentally Sensitive Lands) and will be developed with a maximum of forty-seven (47) residences fronting on a proposed internal 46' wide tract with 28' wide private cul-de-sacs with rezoning to R1-10.

Water service for the development is to be provided by the City of Scottsdale. Connections will be from an existing 16" DIP main that runs north and south in North Miller Road and an 8" water main in North 77<sup>th</sup> Street which then connects to the 12" water main south of the center line in East Pinnacle Peak Road.

There would be no off-site improvements required of public mains to serve the domestic service, irrigation, and fire protection to the proposed residential lots.

Certified fire hydrant flow testing was performed on May 22, 2017 at 7:00 AM by Arizona Flow Testing, LLC at locations as shown on the provided reports. The results are as follows:

|   |                    | Raw Test Data | Data w/58 PSI Safety Factor |          |
|---|--------------------|---------------|-----------------------------|----------|
| • | Static Pressure    | 130.0 PSI     | 72.0 PSI                    |          |
| • | Residual Pressure: | 108.0 PSI     | 50.0 PSI                    | (1.1     |
| • | Flow:              | 3,087 GPM     | 3,087 GPM                   | Actual 2 |
| • | GPM @ 20 PSI:      | 7,361 GPM     | 4,912 GPM                   | 175/1285 |
|   |                    |               |                             | 117      |

The actual flow test documentation is included in Appendix I.

# 2. INTRODUCTION

# 2.1 PLAN OBJECTIVE:

The purpose of this report is to provide discussions and calculations defining the water system concepts necessary to comply with the requirements outlined in the City of Scottsdale Design Standards & Policy Manual. Preparation of this report has been done in accordance with the requirements of the City's Design Standards & Policy Manual.

# 2.2 SITE LOCATION

The project property consists of four (4) parcels of land located at the NEC of North Miller Road and East Pinnacle Peak Road. The total project area contains approximately 855,802.3 SF (19.647 AC) gross; 749,876.2 SF (17.215 AC) net. It is further defined as follows:

Parcel Description: The west half of Section 11, Township 4 North, Range 4 East of

the Gila and Salt River Base and Meridian, Maricopa County,

Scottsdale, Arizona

Parcel ID numbers: APN: 212-04-001B, 212-04-001C, 212-04-001D and 212-04

001F

Parcel Address: 7676 E. Pinnacle Peak Road

Water Capacity Report

Page 1



The site is bounded by North Miller Road on the west, East Pinnacle Peak Road on the south, a portion of North 77<sup>th</sup> Street on the east near the SEC and the La Vista single family subdivision to the east and north.

Refer to FIGURE 1 - Vicinity Map for the project's location with respect to major cross streets

# 2.3 PROPOSED DEVELOPMENT

# 2.3.1 Existing Site Description:

Land ownership includes 17.22 +/- net acres over four (4) parcels of developed and undeveloped land designated as S-R ESL. There are existing designated and recorded N.A.O.S. areas along the south, west and north portions of the proposed project site area. The project is proposed to rezone the parcel to R1-10.

The site is both undeveloped natural desert and a developed office component roughly in the middle of the project site. Contour elevations range from approximately 1916 in the northeast corner to 1879 in the southwest corner, with a slope at approximately 2.5% from northeast to southwest.

FIRM Map Number 04013C1310L dated October 16, 2013 indicates this site is designated as Zone "AO", however there has been a Letter of Map Revision (LOMR) 15-09-1857P with an effective date of June 10, 2016 which removed the project site from the Rawhide Wash Floodplain area and re-designated as **Zone "X"**, having a 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile.

Refer to **FIGURE 2** for an aerial of the overall project existing conditions.

# **EXISTING WATER (COS QS45-46)**

- Miller Road: Two existing 16" and one 36" water mains run north and south in
  North Miller Road. One 16" unknown type is located approximately 3' east, one 36"
  unknown type is located approximately 10' east and one 16" C900 / DIP is located
  approximately 39' east of the North Miller Road center line respectively. The 16"
  water main located approximately 39' east of the center line serves the existing
  office complex.
- Pinnacle Peak Road: Two 12" water mains run east and west in East Pinnacle Peak Road. One 12" DIP water main is located approximately 44' north and one 12" water main type unknown is located approximately 42' south of the East Pinnacle Peak Road center line. No service taps to the site are indicated.
- 77<sup>th</sup> Street: An 8" ACP water main is located near the easterly ROW line of 77<sup>th</sup> Street. The on-site water loop ties into this main.
- On-site: There is an unspecified diameter water line in a 12' public water easement that bisects the project site from North Miller Road to North 77<sup>th</sup> Street. If the entire line cannot be utilized based on size and location then the line will need to be abandoned and removed.

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Refer to Figure 3 for the COS Water Quarter Section Map (QS 45-46).

# 2.3.2 Proposed Site Development:

Proposed development consists of a maximum of forty-seven (47) residences fronting on a proposed internal 46' wide tract with 28' wide private cul-de-sac. Main access is provided near the center of the parcel off North Miller Road which connects to East Pinnacle Peak Road to the south. Emergency access drives are proposed near the northwest corner from Miller Road and near the southeast corner onto the re-alignment of 77<sup>th</sup> Street, as proposed with this development.

An 8" main is proposed to tie into the existing 16" City of Scottsdale main in Miller Road and loop through the site and tie into the existing 8" main in 77th Street. Domestic and irrigation services to the units will be tapped off this new 8" water main.

Refer to **FIGURE 4** for the proposed site layout.

#### 3. **DESIGN CRITERIA**

#### UTILITY DEVELOPER GUIDE CRITERIA 3.1

This project is designed using 47 du / 17.22 net acres = 2.79 du/ac. Refer to Table 1 below for applicable "Design Criteria for Water Systems" based on Figure 6.1-2 (2-2.9 du/ac) in accordance with the City of Scottsdale DS&PM.

Table 1 - COS Design Criteria by demand type

| Land Use                     | Average Day<br>Demand<br>(gal/day/unit) | Max Day<br>Peaking<br>Factor | Peak Hour Peaking Factor |  |  |  |
|------------------------------|---|------------------------------|--------------------------|--|--|--|
| Residential<br>(2-2.9 DU/ac) | 470.4                                   | 2.0                          | 3.5                      |  |  |  |

The system pressures, velocities, head losses and fire flow are in accordance with the COS DS&PM as follows:

#### Minimum Pressures:

50 psi residual pressure at the highest delivery point and 30 psi @ max day +fire flow under what flow e anditions!

**Maximum Pressures:** 

Maximum Pressure =120 psi

In accordance with the Uniform Plumbing Code, any structure experiencing pressures greater than 80 psi shall have an individual pressure reducing valve (PRV) on the customer side of the meter. The City of Scottsdale operates its system from wells and pumps that commonly have pressures exceeding 80 psi. Therefore, the city requires all metered services to have a pressureregulating valve installed on the private service line per DS&PM 6-1.402.

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# Velocity & Head loss:

• 10 ft. head loss maximum per 1,000 linear feet of pipe for pipes less than 16 inches in diameter.

Hazen-Williams Coefficient 130

# Fire Flows:

This site is under the jurisdiction of the City of Scottsdale Fire Department. Fire flows must be in accordance with the 2015 International Fire Code which, for one- and two-family dwellings, is determined as follows:

• Dwellings having a fire-flow calculation area that does not exceed 3,600 s.f. that have automatic sprinklers shall be 500 gpm for 1/2 hour.

# 4. DEMANDS

# 4.1 PROJECT USE DESCRIPTION

Proposed demands for this project are based on a Residential Demand per Dwelling Unit for a density 2-2.9 DU/ac. Refer to **Table 2** below for the proposed water demand calculations based on the design criteria established in *Section 3.1* above

| Table 2: Water Demand Calculations |       |                                |                              |                                   |                             |                             |                    |  |  |
|------------------------------------|-------|--------------------------------|------------------------------|-----------------------------------|-----------------------------|-----------------------------|--------------------|--|--|
|                                    |       |                                |                              |                                   |                             |                             |                    |  |  |
|                                    | Units | Avg. Day<br>Flow<br>(gpd/unit) | Max Day<br>Peaking<br>Factor | Peak<br>Hour<br>Peaking<br>Factor | Avg. Day<br>Demand<br>(GPD) | Max. Day<br>Demand<br>(GPD) | Peak Hour<br>(GPD) |  |  |
| Res. (2-2.9 DU/ac)                 | 47    | 470.4                          | 2                            | 3.5                               | 22,108.8                    | 44,217.6                    | 77,380.8           |  |  |
|                                    |       |                                |                              |                                   |                             |                             |                    |  |  |
| TOTAL PROPOSED BLDG UNITS          | 47    |                                |                              |                                   |                             |                             |                    |  |  |
|                                    |       | TO                             | DTAL DEMAI                   | NDS (GPD):                        | 22,108.8                    | 44,217.6                    | 77,380.8           |  |  |
|                                    |       | TC                             | TOTAL DEMANDS (gpm):         |                                   |                             | 30.71                       | 53.74              |  |  |

# 4.2 **ZONING**

This site is in Zone 6 according to Figure 6.1-3 Pressure Zone Map in DS&PM.

# 4.3 PHASING OF DEMANDS

This residential project may be phased as dictated by unit demand. The infrastructure will be built in a single phase.

# 4.4 SUMMARY NARRATIVE OF DEMANDS

The demand scenario that governs the design was the peak hour demand.

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# 5. EXISTING FACILITIES / CONDITIONS

#### 5.1 PREVIOUS MASTER PLANS

No existing master plan or water report is available from COS for this site.

# 6. PROPOSED FACILITIES

# 6.1 **DISTRIBUTION SYSTEM PIPING**

# 6.1.1 Onsite:

The proposed water supply will consist of new 8" public water line and new fire hydrants. The proposed 8" water main will be DIP in accordance with COS requirements. Domestic service will be provided by 1" copper service connections to each lot, including meter and backflow prevention and PRV. Irrigation will be tapped from the domestic service after the BFP and require a separate/second BFP.

Irrigation for common areas will be provided by a separate system tapped from the 8" water main and maintained by the Home Owners Association.

#### 6.1.2 Offsite Infrastructure:

No offsite infrastructure is anticipated.

# 7. WATER MODEL

# 7.1 **DESCRIPTION OF MODEL**

The final model of the proposed water system is designed to meet the criteria of COS Water, the Arizona Department of Environmental Quality ("ADEQ"), and Maricopa County Environmental Services Department ("MCESD").

Bentley WaterCAD® Version 8i is the computer modeling tool used in this study.

Network analysis input parameters included the following:

- 1. Pipe diameters (inches)
- 2. Pipe lengths (feet)
- 3. Pipes invert elevations (feet)
- 4. General Purpose Valve to model Water Meter and Double Check Valve Assembly
- 5. A reservoir and a pump to model the fire flow test performed
- 6. System demands (gpm)
- 7. Fire flows (gpm)
- 8. Model piping is ductile iron pipe using Hazen-Williams frictional losses (C = 130)

Output parameters included but were not limited to:

- 1. Pressure (psig)
- 2. Flow rates (gpm)
- 3. Velocities (fps)
- 4. Head loss (feet)

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# 7.2 **ASSUMPTIONS**

Please refer to Section 3.1 for the design criteria.

The general methodology used to design this public water infrastructure consists of modeling a network of water distribution mains to meet COS pressure, head loss, and water demand requirements during daily demands and fire events. The connection to the water system is modeled as a reservoir and pump. The pump will simulate the pressure drop and the available flow from the existing water system as depicted by the fire flow test. Refer to **Appendix I** for a copy of the fire flow test results.

# 7.3 **SUMMARY OF RESULTS**

A summary of the modeling results is presented below in **Table 3**. Detailed WaterCAD\* results are presented in **Appendix II**.

| 1 | Table | 3 | - | WaterC/ | AD A | Analysis | Results |
|---|-------|---|---|---------|------|----------|---------|
| г |       |   |   |         |      |          |         |

| Demand               | Water             | Pressure (PSIG) |      |           |      | Maximum            |         |
|----------------------|-------------------|-----------------|------|-----------|------|--------------------|---------|
| Scenario             | Demand<br>(GMP)   | Min.            | Node | Max. Node |      | Velocity<br>(ft/s) | Pipe ID |
| Average Day          | 15.4              | 67              | J-7  | 78        | J-11 | 0.06               | P-17    |
| Maximum<br>Day       | 30.7              | 67              | J-7  | 78        | J-11 | 0.12               | P-17    |
| Peak Hour            | 53.7              | 67              | J-7  | 78        | J-11 | 0.21               | P-17    |
| PEAK. + Fire<br>Flow | 500 +<br>Max. day | 42              | J-3  | N/A       | N/A  | 10.0               | N/A     |

# 8. **SUMMARY / CONCLUSIONS**

# 8.1 CONFORMANCE TO DESIGN GOALS

- The proposed water main is designed in accordance with COS design standards and policies<sup>1</sup>. The following summary is based on the above analysis summary.
  - Minimum 50 psi residual @ highest delivery point required, 67 psi minimum provided.
  - Minimum 30 psi @ max+ fire flow required, 42 psi provided.
  - o 10 fps maximum velocity is not exceeded.
  - The system supports the minimum 500 gpm fire flow requirements.
- The results shown in the modeling summary (refer to Section 7.3) indicate that the
  proposed water system meets the COS criteria for Daily water usage and fire flow events as
  described in Section 3.1.
- PRV's at each building are required per COS design criteria.

#### 8.2 REQUIRED FACILITIES AND PHASING

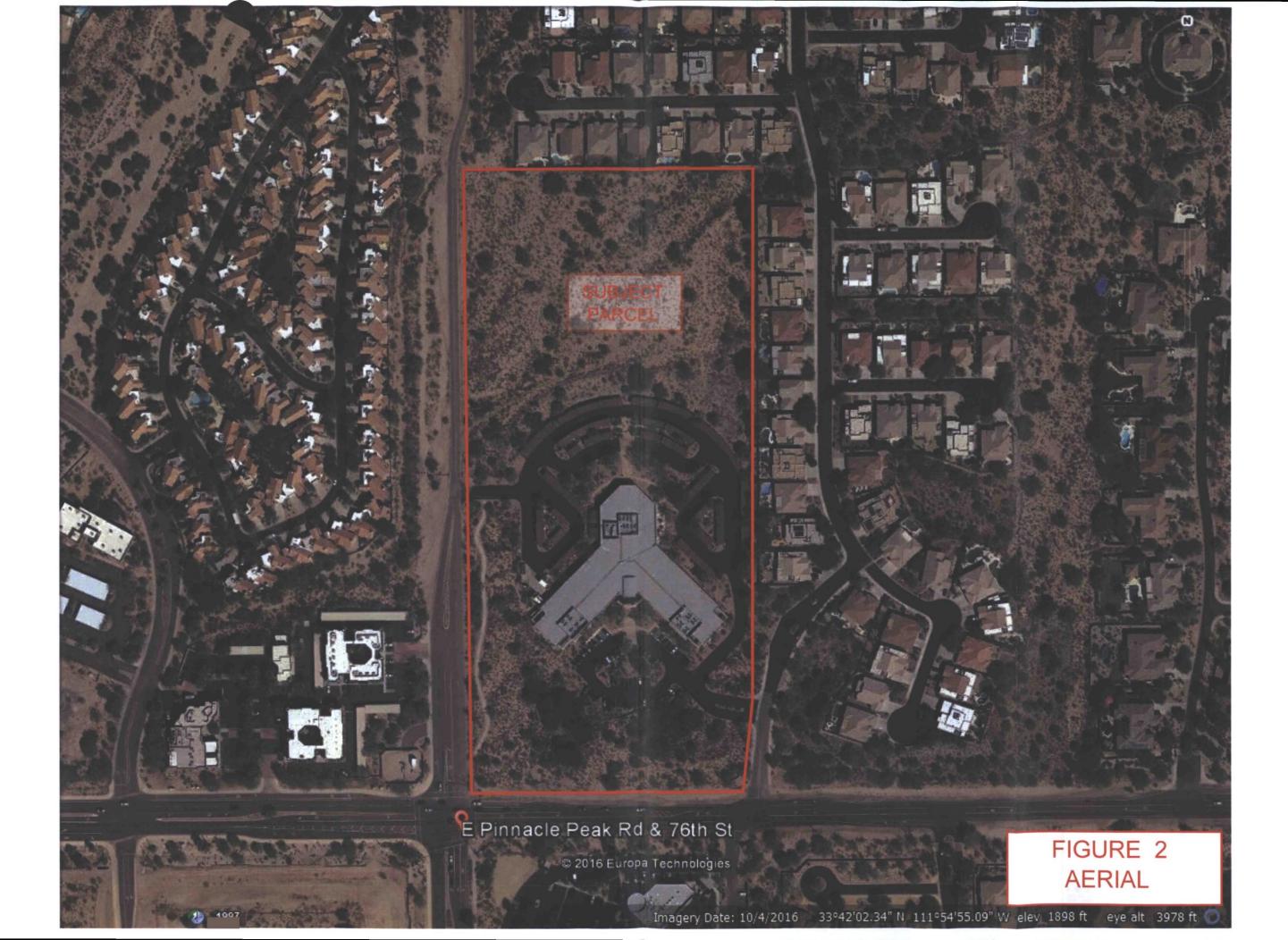
- Proposed facility improvements for this project are limited to a new 8" water main, new fire hydrants, and 1" domestic service connections for each lot.
- This project will be constructed in a single phase.

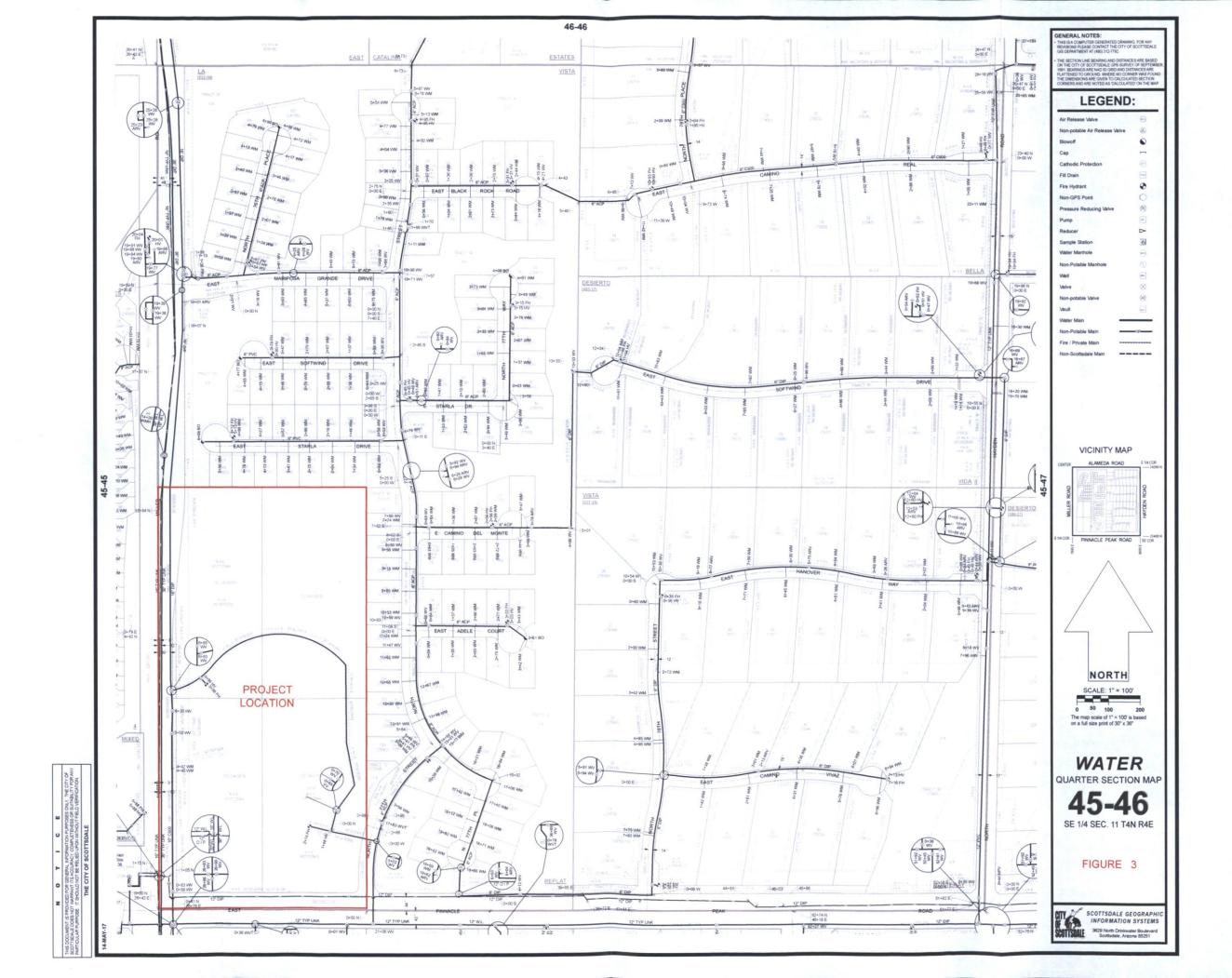


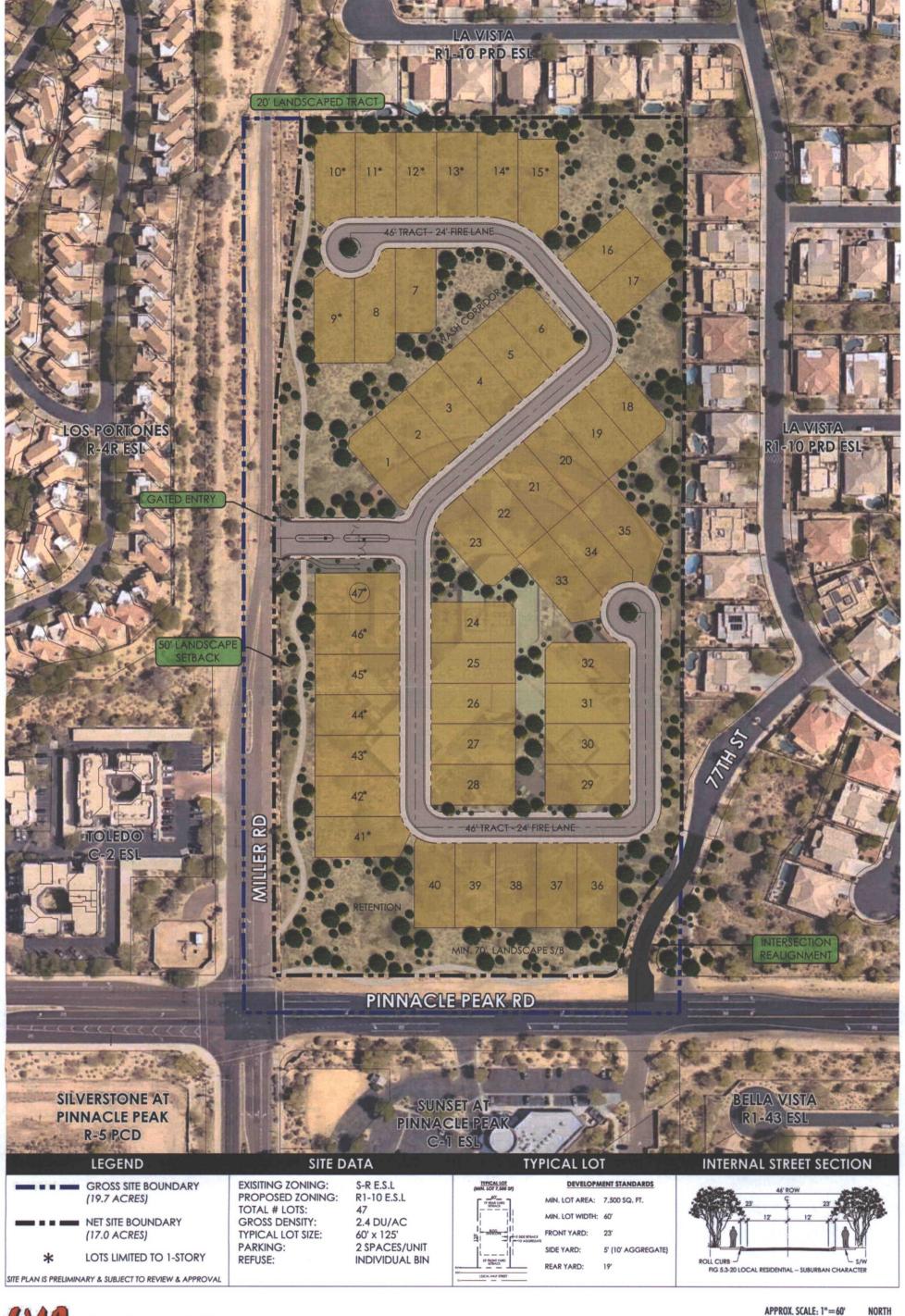
# **REFERENCES**

1. City of Scottsdale Design Standards & Policies Manual-Chapter 6, Water





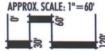






120 south ash avenue - tempe, arizona 85281 - 480.994.0994

# PINNACLE PEAK & MILLER





# APPENDIX I Flow Test Data

## **Arizona Flow Testing LLC**

### HYDRANT FLOW TEST REPORT

Project Name:

Not Provided

Project Address:

Miller and Pinnacle Peak, Scottsdale, Arizona 85255

Client Project No.:

Not Provided

Arizona Flow Testing Project No.:

17110

Flow Test Permit No.:

C53126

Date and time flow test conducted:

May 22, 2017 at 7:00 AM

Data is current and reliable until:

November 12, 2017

Conducted by:

Witnessed by:

Floyd Vaughan - Arizona Flow Testing, LLC (480-250-8154) Larry Frandle -City of Scottsdale-Inspector (602-828-0847)

#### **Raw Test Data**

Static Pressure:

130.0 PSI

(Measured in pounds per square inch)

Residual Pressure:

108.0 PSI

(Measured in pounds per square inch)

Pitot Pressure:

24.0 PSI (4 inch H.M.) 55.0 PSI (2 ½ inch)

(Measured in pounds per square inch)

Diffuser Orifice Diameter:

One (4 inch)

(Measured in inches)

Coefficient of Diffuser: Big Boy Hose Monster

Flowing GPM:

3,087 GPM

(Measured in gallons per minute) 1,842 GPM + 1,245 GPM = 3,087 GPM

GPM @ 20 PSI:

7,361 GPM

**Data with 58 PSI Safety Factor** 

Static Pressure:

72.0 PSI

(Measured in pounds per square inch)

Residual Pressure:

50.0 PSI

(Measured in pounds per square inch)

Scottsdale requires a maximum Static Pressure of 72 PSI for AFES Design.

Distance between hydrants: Approx. 1150 Feet

Main size: Not Provided

Flowing GPM:

3,087 GPM

GPM @ 20 PSI:

4,912 GPM

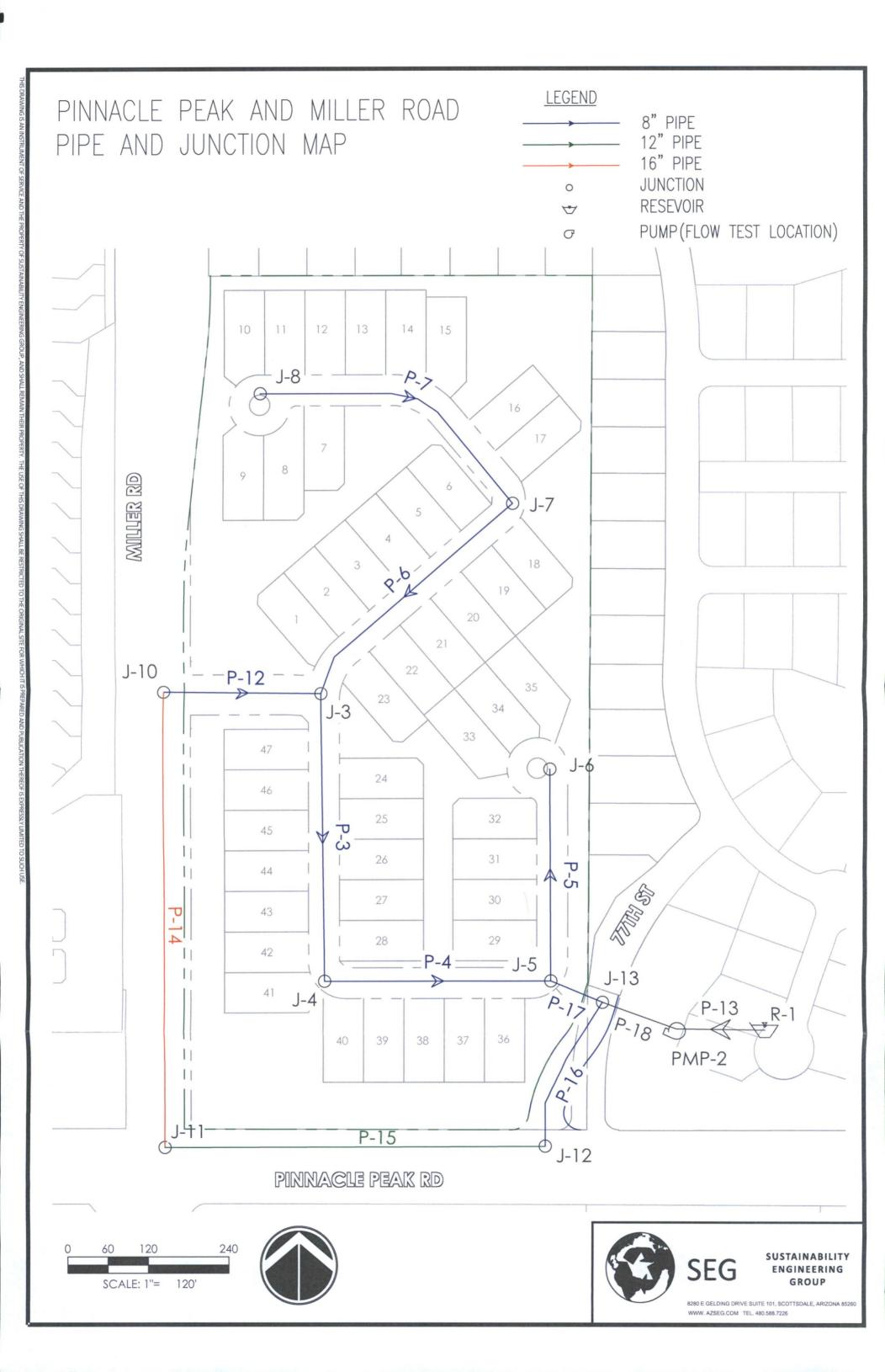
#### Flow Test Location

North





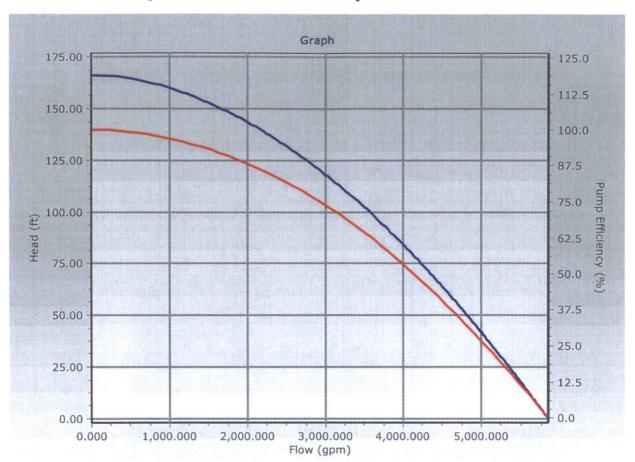
# APPENDIX II Water Model Results



## **Pump Definition Detailed Report: Fire Flow Test**

| Element Details          |                             |                          |                   |
|--------------------------|-----------------------------|--------------------------|-------------------|
| ID                       | 59                          | Notes                    |                   |
| Label                    | Fire Flow Test              |                          |                   |
| Pump Definition Type     |                             |                          |                   |
| Pump Definition Type     | Standard (3<br>Point)       | Design Head              | 115.50 ft         |
| Shutoff Flow             | 0.000 gpm                   | Maximum Operating Flow   | 4,912.000 gpm     |
| Shutoff Head             | 166.32 ft                   | Maximum Operating Head   | 46.20 ft          |
| Design Flow              | 3,087.000 gpm               |                          |                   |
| Pump Efficiency Type     |                             |                          |                   |
| Pump Efficiency Type     | Best<br>Efficiency<br>Point | Motor Efficiency         | 100.0 %           |
| BEP Efficiency           | 100.0 %                     | Is Variable Speed Drive? | False             |
| BEP Flow                 | 0.000 gpm                   |                          |                   |
| Transient (Physical)     |                             |                          |                   |
| Inertia (Pump and Motor) | 0.000 lb·ft²                | Specific Speed           | SI=25,<br>US=1280 |
| Speed (Full)             | 0 rpm                       | Reverse Spin Allowed?    | True              |

## **Pump Definition Detailed Report: Fire Flow Test**



# FlexTable: Junction Table Active Scenario: Average Day

| Label | Elevation (ft) | Demand<br>(gpm) | Hydraulic Grade<br>(ft) | Pressure (psi) |
|-------|----------------|-----------------|-------------------------|----------------|
| J-3   | 1,895.00       | 3.270           | 2,059.32                | 71             |
| J-4   | 1,886.00       | 2.290           | 2,059.32                | 75             |
| J-5   | 1,891.50       | 1.633           | 2,059.32                | 73             |
| J-6   | 1,897.50       | 2.290           | 2,059.32                | 70             |
| J-7   | 1,903.50       | 2.940           | 2,059.32                | 67             |
| J-8   | 1,902.00       | 2.940           | 2,059.32                | 68             |
| J-10  | 1,892.50       | 0.000           | 2,059.32                | 72             |
| J-11  | 1,879.00       | 0.000           | 2,059.32                | 78             |
| J-12  | 1,887.00       | 0.000           | 2,059.32                | 75             |
| J-13  | 1,893.00       | 0.000           | 2,059.32                | 72             |

# FlexTable: Pipe Table Active Scenario: Average Day

| Label | Length (Scaled)<br>(ft) | Start Node | Stop Node | Diameter<br>(in) | Hazen-Williams<br>C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------|-------------------------|------------|-----------|------------------|---------------------|---------------|--------------------|---------------------------------|
| P-3   | 426                     | J-3        | J-4       | 8.0              | 130.0               | -3.036        | 0.02               | 0.000                           |
| P-4   | 336                     | J-4        | J-5       | 8.0              | 130.0               | -5.326        | 0.03               | 0.000                           |
| P-5   | 313                     | J-5        | J-6       | 8.0              | 130.0               | 2.290         | 0.01               | 0.000                           |
| P-6   | 407                     | J-3        | J-7       | 8.0              | 130.0               | 5.880         | 0.04               | 0.000                           |
| P-7   | 446                     | J-7        | J-8       | 8.0              | 130.0               | 2.940         | 0.02               | 0.000                           |
| P-12  | 230                     | J-3        | J-10      | 8.0              | 130.0               | -6.114        | 0.04               | 0.000                           |
| P-13  | 129                     | R-1        | PMP-2     | 24.0             | 130.0               | 15.363        | 0.01               | 0.000                           |
| P-14  | 666                     | J-10       | J-11      | 16.0             | 130.0               | -6.114        | 0.01               | 0.000                           |
| P-15  | 632                     | J-11       | J-12      | 12.0             | 130.0               | -6.114        | 0.02               | 0.000                           |
| P-16  | 220                     | J-12       | J-13      | 8.0              | 130.0               | -6.114        | 0.04               | 0.000                           |
| P-17  | 85                      | J-13       | J-5       | 8.0              | 130.0               | 9.249         | 0.06               | 0.000                           |
| P-18  | 113                     | J-13       | PMP-2     | 24.0             | 130.0               | -15.363       | 0.01               | 0.000                           |

\$53;+V MAX 1,200

# FlexTable: Reservoir Table Active Scenario: Average Day

| Label | Elevation (ft) | Zone          | Flow (Out net)<br>(gpm) | Hydraulic Grade<br>(ft) |
|-------|----------------|---------------|-------------------------|-------------------------|
| R-1   | 1,893.00       | <none></none> | 15.363                  | 1,893.00                |

## FlexTable: Pump Table

## **Active Scenario: Average Day**

| Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade<br>(Suction)<br>(ft) | Hydraulic Grade<br>(Discharge)<br>(ft) | Flow (Total)<br>(gpm) | Pump Head<br>(ft) |
|-------|----------------|-----------------|------------------|--------------------------------------|--|-----------------------|-------------------|
| PMP-2 | 1,893.00       | Fire Flow Test  | On               | 1,893.00                             | 2,059.32                               | 15.363                | 166.32            |

# FlexTable: Junction Table Active Scenario: Max Day

| Label | Elevation (ft) | Demand<br>(gpm) | Hydraulic Grade<br>(ft) | Pressure (psi) |
|-------|----------------|-----------------|-------------------------|----------------|
| J-3   | 1,895.00       | 6.530           | 2,059.31                | 71             |
| J-4   | 1,886.00       | 4.570           | 2,059.31                | 75             |
| J-5   | 1,891.50       | 3.260           | 2,059.31                | 73             |
| J-6   | 1,897.50       | 4.570           | 2,059.31                | 70             |
| J-7   | 1,903.50       | 5.880           | 2,059.31                | 67             |
| J-8   | 1,902.00       | 5.880           | 2,059.30                | 68             |
| J-10  | 1,892.50       | 0.000           | 2,059.31                | 72             |
| J-11  | 1,879.00       | 0.000           | 2,059.31                | 78             |
| J-12  | 1,887.00       | 0.000           | 2,059.31                | 75             |
| J-13  | 1,893.00       | 0.000           | 2,059.31                | 72             |

# FlexTable: Pipe Table Active Scenario: Max Day

| Label | Length (Scaled)<br>(ft) | Start Node | Stop Node | Diameter<br>(in) | Hazen-Williams<br>C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------|-------------------------|------------|-----------|------------------|---------------------|---------------|--------------------|---------------------------------|
| P-3   | 426                     | J-3        | J-4       | 8.0              | 130.0               | -6.073        | 0.04               | 0.000                           |
| P-4   | 336                     | J-4        | J-5       | 8.0              | 130.0               | -10.643       | 0.07               | 0.000                           |
| P-5   | 313                     | J-5        | J-6       | 8.0              | 130.0               | 4.570         | 0.03               | 0.000                           |
| P-6   | 407                     | J-3        | J-7       | 8.0              | 130.0               | 11.760        | 0.08               | 0.000                           |
| P-7   | 446                     | J-7        | J-8       | 8.0              | 130.0               | 5.880         | 0.04               | 0.000                           |
| P-12  | 230                     | J-3        | J-10      | 8.0              | 130.0               | -12.217       | 0.08               | 0.000                           |
| P-13  | 129                     | R-1        | PMP-2     | 24.0             | 130.0               | 30.690        | 0.02               | 0.000                           |
| P-14  | 666                     | J-10       | J-11      | 16.0             | 130.0               | -12.217       | 0.02               | 0.000                           |
| P-15  | 632                     | J-11       | J-12      | 12.0             | 130.0               | -12.217       | 0.03               | 0.000                           |
| P-16  | 220                     | J-12       | J-13      | 8.0              | 130.0               | -12.217       | 0.08               | 0.000                           |
| P-17  | 85                      | J-13       | J-5       | 8.0              | 130.0               | 18.473        | 0.12               | 0.000                           |
| P-18  | 113                     | J-13       | PMP-2     | 24.0             | 130.0               | -30.690       | 0.02               | 0.000                           |

# FlexTable: Reservoir Table Active Scenario: Max Day

| Label | Elevation (ft) | Zone          | Flow (Out net)<br>(gpm) | Hydraulic Grade<br>(ft) |
|-------|----------------|---------------|-------------------------|-------------------------|
| R-1   | 1,893.00       | <none></none> | 30.690                  | 1,893.00                |

## FlexTable: Pump Table

## **Active Scenario: Max Day**

| Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade<br>(Suction)<br>(ft) | Hydraulic Grade<br>(Discharge)<br>(ft) | Flow (Total)<br>(gpm) | Pump Head<br>(ft) |
|-------|----------------|-----------------|------------------|--------------------------------------|--|-----------------------|-------------------|
| PMP-2 | 1,893.00       | Fire Flow Test  | On               | 1,893.00                             | 2,059.31                               | 30.690                | 166.31            |

# Fire Flow Node FlexTable: Fire Flow Report Active Scenario: Max Day plus Fire Flow

| Label | Fire<br>Flow<br>(Needed<br>)<br>(gpm) | Fire Flow<br>(Available)<br>(gpm) | Flow<br>(Total<br>Needed)<br>(gpm) | Flow (Total<br>Available)<br>(gpm) | Pressure<br>(Residual<br>Lower<br>Limit)<br>(psi) | Pressure<br>(Calculated<br>Residual)<br>(psi) | Pressure<br>(Calculated<br>Zone Lower<br>Limit)<br>(psi) | Junction w/<br>Minimum<br>Pressure<br>(Zone) | Pressure<br>(Calculated<br>System Lower<br>Limit)<br>(psi) | Junction w/<br>Minimum<br>Pressure<br>(System) | Velocity of<br>Maximum<br>Pipe<br>(ft/s) | Pipe w/<br>Maximum<br>Velocity |
|-------|---------------------------------------|-----------------------------------|------------------------------------|------------------------------------|---|---|--|--|--|--|--|--------------------------------|
| J-3   | 500.000                               | 2,798.143                         | 506.530                            | 2,804.673                          | 30  | 42  | 39   | J-7  | 39   | J-7  | 10.00                                    | P-12                           |
| J-4   | 500.000                               | 2,529.901                         | 504.570                            | 2,534.471                          | 30  | 52  | 47   | J-7  | 47   | J-7  | 10.00                                    | P-17                           |
| J-5   | 500.000                               | 1,903.547                         | 503.260                            | 1,906.807                          | 30  | 62  | 57   | J-7  | 57   | J-7  | 10.00                                    | P-17                           |
| J-6   | 500.000                               | 1,562.146                         | 504.570                            | 1,566.716                          | 30  | 57  | 60   | J-7  | 60   | J-7  | 10.00                                    | P-5                            |
| J-7   | 500.000                               | 1,554.956                         | 505.880                            | 1,560.836                          | 30  | 50  | 51   | J-8  | 51   | J-8  | 10.00                                    | P-6                            |
| J-8   | 500.000                               | 1,554.956                         | 505.880                            | 1,560.836                          | 30  | 43  | 50   | J-7  | 50   | J-7  | 10.00                                    | P-6                            |
| J-10  | 500.000                               | 2,376.935                         | 500.000                            | 2,376.935                          | 30  | 52  | 49   | J-7  | 49   | J-7  | 10.00                                    | P-16                           |
| J-11  | 500.000                               | 2,337.059                         | 500.000                            | 2,337.059                          | 30  | 59  | 50   | J-7  | 50   | J-7  | 10.00                                    | P-16                           |
| J-12  | 500.000                               | 2,181.138                         | 500.000                            | 2,181.138                          | 30  | 59  | 53   | J-7  | 53   | J-7  | 10.00                                    | P-16                           |
| J-13  | 500.000                               | 3,500.000                         | 500.000                            | 3,500.000                          | 30  | 44  | 39   | J-7  | 39   | J-7  | 2.50                                     | P-18                           |

# FlexTable: Junction Table Active Scenario: Max Day plus Fire Flow

| Label | Elevation (ft) | Demand<br>(gpm) | Hydraulic Grade<br>(ft) | Pressure<br>(psi) |
|-------|----------------|-----------------|-------------------------|-------------------|
| J-3   | 1,895.00       | 6.530           | 2,059.31                | 71                |
| J-4   | 1,886.00       | 4.570           | 2,059.31                | 75                |
| J-5   | 1,891.50       | 3.260           | 2,059.31                | 73                |
| J-6   | 1,897.50       | 4.570           | 2,059.31                | 70                |
| J-7   | 1,903.50       | 5.880           | 2,059.31                | 67                |
| J-8   | 1,902.00       | 5.880           | 2,059.30                | 68                |
| J-10  | 1,892.50       | 0.000           | 2,059.31                | 72                |
| J-11  | 1,879.00       | 0.000           | 2,059.31                | 78                |
| J-12  | 1,887.00       | 0.000           | 2,059.31                | 75                |
| J-13  | 1,893.00       | 0.000           | 2,059.31                | 72                |

FlexTable: Pipe Table
Active Scenario: Max Day plus Fire Flow

| Label | Length (Scaled)<br>(ft) | Start Node | Stop Node | Diameter<br>(in) | Hazen-Williams<br>C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------|-------------------------|------------|-----------|------------------|---------------------|---------------|--------------------|---------------------------------|
| P-3   | 426                     | J-3        | J-4       | 8.0              | 130.0               | -6.073        | 0.04               | 0.000                           |
| P-4   | 336                     | J-4        | J-5       | 8.0              | 130.0               | -10.643       | 0.07               | 0.000                           |
| P-5   | 313                     | J-5        | J-6       | 8.0              | 130.0               | 4.570         | 0.03               | 0.000                           |
| P-6   | 407                     | J-3        | J-7       | 8.0              | 130.0               | 11.760        | 0.08               | 0.000                           |
| P-7   | 446                     | J-7        | J-8       | 8.0              | 130.0               | 5.880         | 0.04               | 0.000                           |
| P-12  | 230                     | J-3        | J-10      | 8.0              | 130.0               | -12.217       | 0.08               | 0.000                           |
| P-13  | 129                     | R-1        | PMP-2     | 24.0             | 130.0               | 30.690        | 0.02               | 0.000                           |
| P-14  | 666                     | J-10       | J-11      | 16.0             | 130.0               | -12.217       | 0.02               | 0.000                           |
| P-15  | 632                     | J-11       | J-12      | 12.0             | 130.0               | -12.217       | 0.03               | 0.000                           |
| P-16  | 220                     | J-12       | J-13      | 8.0              | 130.0               | -12.217       | 0.08               | 0.000                           |
| P-17  | 85                      | J-13       | J-5       | 8.0              | 130.0               | 18.473        | 0.12               | 0.000                           |
| P-18  | 113                     | J-13       | PMP-2     | 24.0             | 130.0               | -30.690       | 0.02               | 0.000                           |

# FlexTable: Reservoir Table Active Scenario: Max Day plus Fire Flow

| Label | Elevation<br>(ft) | Zone          | Flow (Out net)<br>(gpm) | Hydraulic Grade<br>(ft) |
|-------|-------------------|---------------|-------------------------|-------------------------|
| R-1   | 1,893.00          | <none></none> | 30.690                  | 1,893.00                |

## FlexTable: Pump Table

## **Active Scenario: Max Day plus Fire Flow**

| Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade<br>(Suction)<br>(ft) | Hydraulic Grade<br>(Discharge)<br>(ft) | Flow (Total)<br>(gpm) | Pump Head<br>(ft) |
|-------|----------------|-----------------|------------------|--------------------------------------|--|-----------------------|-------------------|
| PMP-2 | 1,893.00       | Fire Flow Test  | On               | 1,893.00                             | 2,059.31                               | 30.690                | 166.31            |

# FlexTable: Junction Table Active Scenario: Peak Hour

| Label | Elevation (ft) | Demand<br>(gpm) | Hydraulic Grade<br>(ft) | Pressure<br>(psi) |
|-------|----------------|-----------------|-------------------------|-------------------|
| J-3   | 1,895.00       | 11.430          | 2,059.28                | 71                |
| J-4   | 1,886.00       | 8.000           | 2,059.29                | 75                |
| J-5   | 1,891.50       | 5.717           | 2,059.29                | 73                |
| J-6   | 1,897.50       | 8.000           | 2,059.29                | 70                |
| J-7   | 1,903.50       | 10.290          | 2,059.28                | 67                |
| J-8   | 1,902.00       | 10.290          | 2,059.28                | 68                |
| J-10  | 1,892.50       | 0.000           | 2,059.29                | 72                |
| J-11  | 1,879.00       | 0.000           | 2,059.29                | 78                |
| J-12  | 1,887.00       | 0.000           | 2,059.29                | 75                |
| J-13  | 1,893.00       | 0.000           | 2,059.29                | 72                |

# FlexTable: Pipe Table Active Scenario: Peak Hour

| Label | Length (Scaled)<br>(ft) | Start Node | Stop Node | Diameter<br>(in) | Hazen-Williams<br>C | Flow<br>(gpm) | Velocity<br>(ft/s) | Headloss<br>Gradient<br>(ft/ft) |
|-------|-------------------------|------------|-----------|------------------|---------------------|---------------|--------------------|---------------------------------|
| P-3   | 426                     | J-3        | J-4       | 8.0              | 130.0               | -10.626       | 0.07               | 0.000                           |
| P-4   | 336                     | J-4        | J-5       | 8.0              | 130.0               | -18.626       | 0.12               | 0.000                           |
| P-5   | 313                     | J-5        | J-6       | 8.0              | 130.0               | 8.000         | 0.05               | 0.000                           |
| P-6   | 407                     | J-3        | J-7       | 8.0              | 130.0               | 20.580        | 0.13               | 0.000                           |
| P-7   | 446                     | J-7        | J-8       | 8.0              | 130.0               | 10.290        | 0.07               | 0.000                           |
| P-12  | 230                     | J-3        | J-10      | 8.0              | 130.0               | -21.384       | 0.14               | 0.000                           |
| P-13  | 129                     | R-1        | PMP-2     | 24.0             | 130.0               | 53.727        | 0.04               | 0.000                           |
| P-14  | 666                     | J-10       | J-11      | 16.0             | 130.0               | -21.384       | 0.03               | 0.000                           |
| P-15  | 632                     | J-11       | J-12      | 12.0             | 130.0               | -21.384       | 0.06               | 0.000                           |
| P-16  | 220                     | J-12       | J-13      | 8.0              | 130.0               | -21.384       | 0.14               | 0.000                           |
| P-17  | 85                      | J-13       | J-5       | 8.0              | 130.0               | 32.343        | 0.21               | 0.000                           |
| P-18  | 113                     | J-13       | PMP-2     | 24.0             | 130.0               | -53.727       | 0.04               | 0.000                           |

# FlexTable: Reservoir Table Active Scenario: Peak Hour

| Label | Elevation (ft) | Zone          | Flow (Out net)<br>(gpm) | Hydraulic Grade<br>(ft) |
|-------|----------------|---------------|-------------------------|-------------------------|
| R-1   | 1,893.00       | <none></none> | 53.727                  | 1,893.00                |

## FlexTable: Pump Table

### **Active Scenario: Peak Hour**

| Label | Elevation<br>(ft) | Pump Definition | Status (Initial) | Hydraulic Grade<br>(Suction)<br>(ft) | Hydraulic Grade<br>(Discharge)<br>(ft) | Flow (Total)<br>(gpm) | Pump Head<br>(ft) |
|-------|-------------------|-----------------|------------------|--------------------------------------|--|-----------------------|-------------------|
| PMP-2 | 1,893.00          | Fire Flow Test  | On               | 1,893.00                             | 2,059.29                               | 53.727                | 166.29            |



# APPENDIX III Preliminary Utility Plan

# P.F. CHANG'S RESIDENTIAL DEVELOPMENT PINNACLE PEAK RD. AND MILLER RD. PRELIMINARY UTILITY PLAN

HAPPY VALLEY ROAD PINNACLE PEAK ROAD

APPLICANT/DEVELOPER SNELL & WILMER 400 E. VAN BUREN ST. #1900 PHOENIX, AZ 85004 PHONE: 602-328-6269 ATTN: NICK WOOD, ESQ

**PLANNER** 

PFCCB PINNACLE PEAK LLC

SCOTTSDALE, AZ 85255

**CIVIL ENGINEER** 

ATTN:ZACH SHIRK

7676 E. PINNACLE PEAK RD.

SUSTAINABILITY ENGINEERING GROUP

8280 E. GELDING DR., SUITE 101

- 27 LF SDR-35 PVC @S=2.10%

LA VISTA REPLAT

SCOTTSDALE, ARIZONA 85260

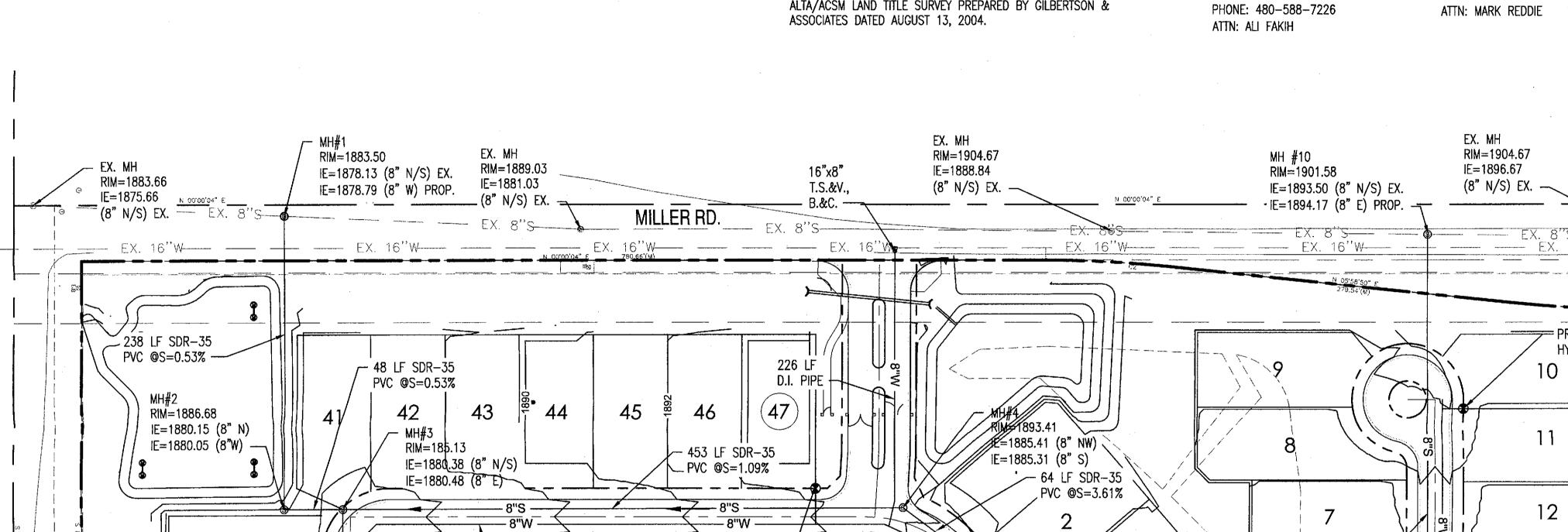
LVA URBAN DESIGN STUDIO, LLC PHONE: 480-994-0994 ATTN: MARK REDDIE

VICINITY MAP

## BASIS OF BEARING

THE BASIS OF BEARING AND ALL MONUMENTATION SHOWN HEREON IS BASED ON THE SOUTH LINE OF THE SOUTHEAST EAST, USING A BEARING OF NORTH 89 DEGREES 51 MINUTES 11 SECONDS WEST, AS SHOWN ON AN UNRECORDED ALTA/ACSM LAND TITLE SURVEY PREPARED BY GILBERTSON &

LA VISTA REPLAT



PROPOSED FIRE 311 LF SDR-35 PVC @S=3.61% 39 (E=1900.77 (8" W) IE=1887.82 (8" NE) IE=1887.72 (8"SW) PINNACLE 1910 \_\_\_\_\_ 169 LF SDR-35 PVC @S=1.54% --PROPOSED FIRE -1890-309 LF SDR-35 PVC @189071% --15 IE=1902.30 (8" SE) 313 LF SDR-35 RIM=1891.59 RIM = 1890.67PVC @S=2.14% TE≡1883.69 (8" N) \_ IE=1882.77 (8" NE) : IE=1882.67 (8" W) IE=1899.79 (8" NW) IE=1899.69 (8" S) RIM=1907.16

# PROPOSED LEGEND

-----8"W ----- WATER LINE -8"S---- SEWER LINE FIRE HYDRANT SEWER MANHOLE

| PROJECHA DEVELOP LOCATI   |  |  |  |  |  |
|---|--|--|--|--|--|
| DRAWN TALU DESIGNED MALONEY CHECKED COUNSELL PROJ. MGR. MALONEY |  |  |  |  |  |
| DATE: 06/21/2017  |  |  |  |  |  |
| ISSUED FOR: ZONING  |  |  |  |  |  |
| REVISION NO.: DATE:   |  |  |  |  |  |
| $\triangle$   |  |  |  |  |  |
| <u>^2</u>   |  |  |  |  |  |
| <u></u>   |  |  |  |  |  |
| 4   |  |  |  |  |  |
| JOB NO.: 170566   |  |  |  |  |  |

EXPIRES 9/30/2017

PRELIMINARY UTILITY PLAN

C4.00

SCALE: 1" = 60'

43 LF SDR-35

PVC @S=1.91%

LA VISTA REPLAT



## PRELIMINARY SEWER CAPACITY REPORT

NEC Pinnacle Peak Rd. & Miller Rd. Scottsdale, AZ

Prepared For:



7676 E. Pinnacle Peak Road Scottsdale, AZ 85255 P: 480.888.3000

LDillon 9-7-17

## Prepared by:



## Sustainability Engineering Group

8280 E. Gelding Drive, Suite 101 Scottsdale, AZ 85260 480.588.7226 www.azSEG.com

Project Number: 170566

Original Submittal Date: June 22, 2017 (Zoning)
Revised: August 18, 2017

Case No.: 3-GP-2017; 11-ZN-2017 Plan Check No.: TBD

52743 MARKA. MALONEY

EXPIRES 9/30/2017



"LEEDing and Developing Smart Projects"

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#### 1. INTRODUCTION

#### 1.1 SUMMARY OF PROPOSED DEVELOPMENT:

Proposed development consists of a maximum of fifty-five (55) residences fronting on a proposed internal 46' wide tract with 28' wide private roadways / cul-de-sacs. Main access is provided off North Miller Road which connects to East Pinnacle Peak Road to the south.

The purpose of this sewer capacity design report is to provide preliminary analysis of the impact that this development will have on the City's sewer system.

#### 1.2 LEGAL DESCRIPTION:

The project property consists of four (4) parcels of land located at the NEC of North Miller Road and East Pinnacle Peak Road. The total project area contains approximately 855,802.3 SF (19.647 AC) gross; 749,876.2 SF (17.215 AC) net. It is further defined as follows:

• Parcel Description: The west half of Section 11, Township 4 North, Range 4 East of

the Gila and Salt River Base and Meridian, Maricopa County,

Scottsdale, Arizona

Parcel ID numbers: APN: 212-04-001B, 212-04-001C, 212-04-001D and 212-04

001E.

• Parcel Address: 7676 E. Pinnacle Peak Road

The site is bounded by North Miller Road on the west, East Pinnacle Peak Road on the south, a portion of North 77<sup>th</sup> Street on the east near the SEC and the La Vista single family subdivision to the east and north.

Refer to FIGURE 1 - Vicinity Map for the project's location with respect to major cross streets

#### 1.3 EXISTING AND PROPOSED SITE ZONING AND LAND USES:

The project parcel is zoned S-R ESL (Service Residential Environmentally Sensitive Lands and falls under Zoning District Commercial and Industrial) per the City of Scottsdale Zoning Map 31 and is currently developed with a 50,728 SF office building, parking canopies and asphalt parking. There are existing designated and recorded N.A.O.S. areas along the south, west and north portions of the proposed project site area.

#### 1.4 REFERENCES:

The project site is shown in the City's General Plan Conceptual Land Use Map as Rural Neighborhoods.

#### 2. DESIGN DOCUMENTATION

#### 2.1 DESIGN COMPLIANCE:

The analysis of the proposed and existing sewer system is done in compliance with Chapter 7 – Wastewater of the City of Scottsdale 2010 update of the Design Standards & Policies Manual



(DS&PM). Design flow calculations for the on-site system will be based on the recommendations in Section 7-1.403 of the DS&PM.

#### 3. EXISTING CONDITIONS

#### 3.1 EXISTING ZONING & LAND USE:

Land ownership includes 17.22 +/- net acres over four (4) parcels of developed (office) and undeveloped land designated as S-R ESL. There are existing designated and recorded N.A.O.S. areas along the south, west and north portions of the proposed project site area. The project is proposed to rezone the parcel to R1-10.

#### 3.2 EXISTING TOPOGRAPHY, VEGETATION AND LANDFORM FEATURES:

The site is both undeveloped natural desert and a developed office component roughly in the middle of the project site. Contour elevations range from approximately 1916 in the northeast corner to 1879 in the southwest corner, with an average slope at approximately 2.5% from northeast to southwest.

FIRM Map Number 04013C1310L dated October 16, 2013 indicates this site is designated as Zone "AO", however there has been a Letter of Map Revision (LOMR) 15-09-1857P with an effective date of June 10, 2016 which removed the project site from the Rawhide Wash Floodplain area and re-designated as "X", having a 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile.

Refer to FIGURE 2 for an aerial of the overall project existing conditions.

#### 3.3 EXISTING UTILITIES:

Sanitary Sewer: QS 45-46 City of Scottsdale

- North Miller Road: A City of Scottsdale public 8" PVC sewer main is shown in North Miller Road for the full length of the sites boundary with an existing manhole at the intersection of North Miller Road and East Pinnacle Peak Road, one existing manhole at the NWC of the project site and 2 additional existing manholes spaced approximately evenly between those. The invert elevation for the existing manhole at the intersection North Miller Road and East Pinnacle Peak Road is 1868.92 and a rim at 1878.35. The sewer main is located east of the center line on North Miller Road with the exception of the manhole at the intersection of North Miller Road and East Pinnacle Peak Road where the manhole is located west of the center line.
- E. Pinnacle Peak Road: A City of Scottsdale public 8" PVC sewer main is shown in East Pinnacle Peak Road for the full length of the sites boundary with two existing manholes in the intersection of North Miller Road and East Pinnacle Peak Road. A manhole located near the center of the parcel has an unspecified diameter sewer stub out to the project site. The invert of the stub out to the north is indicated as 1971.85 but it is assumed that the invert is more likely 1871.85 since the rim is indicated as 1883.70. A



third manhole is located at the SEC of the project site. The sewer main is located approximately 24' south of the East Pinnacle Peak Road center line.

• 77<sup>th</sup> Street: No sewer mains are indicated in 77<sup>th</sup> Street.

Refer to FIGURE 3 for the City quarter section map (QS 45-46)

#### 4. PROPOSED CONDITIONS

#### 4.1 SITE PLAN:

Proposed development consists of a maximum of fifty-five (55) residences fronting on a proposed internal 46' wide tract with 28' wide private cul-de-sac. Main access is provided near the center of the parcel off North Miller Road which connects to East Pinnacle Peak Road to the south. Refer to **FIGURE 4** for proposed site layout.

#### 4.2 PROPOSED SEWER SYSTEM:

It is proposed to construct a new 8" PVC sewer main in the new roadway to service the 55 lots. This service will then tie into the existing 8" PVC main in Miller Road approximately 200' north of Pinnacle Peak Road with a new manhole. Refer to Sheet C4.00 in **Appendix II** for the Preliminary Utility Plan.

#### 4.3 MAINTENANCE RESPONSIBILITIES:

The on-site sewer line for the proposed development will be public and located within right-of-way or easements to the City of Scottsdale. Therefore, the on-site and off-site sanitary sewer will be maintained by the City.

#### 5. SANITARY SYSTEM COMPUTATIONS

#### 5.1. SEWER FLOW DEMANDS:

DS&PM, Chapter 7 Section 7-1.403 – Wastewater specifies that for residential uses, sanitary sewer lines 8 to 12 inches in diameter will be designed using 100 gallons per person per day and a peaking factor of 4. Residential densities are to assume 2.5 persons per dwelling unit.

Therefore, the average design flow is: 55 du x 100 gpcpd x 2.5 people/du = 13,750 gpd (Average Day Proposed)

#### 5.2. VARIANCE FROM STATED DESIGN FLOWS:

Stated design flows for the on-site system will be used as recommended.

#### 5.3. DEMAND FACTORS:

DS&PM requires a peak factor of 4.0 for residential usages. Therefore, from Section 5.1:  $13,750 \text{ gpd } \times 4 = 55,000 \text{ gpd (Peak)}$ 



#### 5.4. SEWER SYSTEM ANALYSIS (Existing On-Site):

As a comparison, the existing site has a 50,728 SF office building. The calculated average design flow is  $50,728 \text{ SF} \times 0.4 \text{ per SF} = 20,291 \text{ gpd (Average Existing)}$ .

DS&PM requires a peak factor of 3.0 for office use. Therefore, from Section 5.1, the existing peak demand is  $20,291 \text{ gpd} \times 3 = 60,873 \text{ gpd}$  (Peak).

The proposed sanitary sewer demands that will contribute to the intersection of North Miller Road and East Pinnacle Peak Road are approximately a 9.6% reduction from the existing peak contribution to the same point of the existing public sewer system. This will allow additional capacity in the main downstream from this point by providing a reduction of approximately, 6,541 gpd (average day) and 5,873 gpd (peak day) from the sewer demand.

#### 5.5. SEWER CAPACITY CALCULATIONS

The site layout splits the units into two sewer laterals. Ten (10) lots will discharge to the north lateral connection at Miller Road and 45 lots will discharge to the southern lateral connection at Miller Road. A minimum velocity of 1 fps under average flow conditions is required.

#### **NORTH LATERAL:**

For the north lateral the calculated flow is 10 du x 100 gpcpd x 2.5 people/du = **2,500 gpd** ADD or **7,500 gpd PDD**.

• An 8" diameter sanitary sewer pipe at S=2.67% (n=0.013) is proposed. This provides a velocity of 1.12 fps at a depth of 0.26" ADD, a velocity of 1.54 fps at a depth of 0.44" PDD, and "full" flow capacity (d/D = 0.65) of approximately 965,270 gpd at a velocity of 6.22 fps, providing adequate capacity for the on-site system. Refer to Appendix I for Flowmaster calculations.

For the south lateral the calculated flow is  $45 \text{ du} \times 100 \text{ gpcpd} \times 2.5 \text{ people/du} = 11,250 \text{ gpd}$  ADD or 33,750 gpd PDD.

• An 8" diameter sanitary sewer pipe at S=2.67% (n=0.013) is proposed for the upstream reach of the system, see above for calculation summary. An 8" diameter pipe at S=1.00% (n=0.013) is proposed for the downstream reach. This provides a velocity of 1.25 fps at a depth of 0.67" ADD, a velocity of 1.73 fps at a depth of 1.13" PDD, and "full" flow capacity (d/D = 0.65) of approximately 590,736 gpd at a velocity of 3.81 fps, providing adequate capacity for the on-site system. Refer to Appendix I for Flowmaster calculations.



#### 6. SUMMARY

#### 6.1 SUMMARY OF PROPOSED IMPROVEMENTS:

- The proposed wastewater improvement was designed based on the current City of Scottsdale's design standards and policies.
- The existing sanitary main being tied into is capable of supporting the projected average flow for the development.
- The proposed development provides a reduction in sewer capacity demand compared to the existing development.
- The final plans will show water and sewer vertical clearances compliant with City and State separation or protection provisions.

#### 6.2 PROJECT SCHEDULE:

As a residential development, the infrastructure is proposed to be constructed in a single phase to accommodate dwelling unit growth. The dwelling units may be phased based on consumer demand.

#### 7 SUPPORTING MAPS

#### 7.1 PRELIMINARY UTILITY PLAN

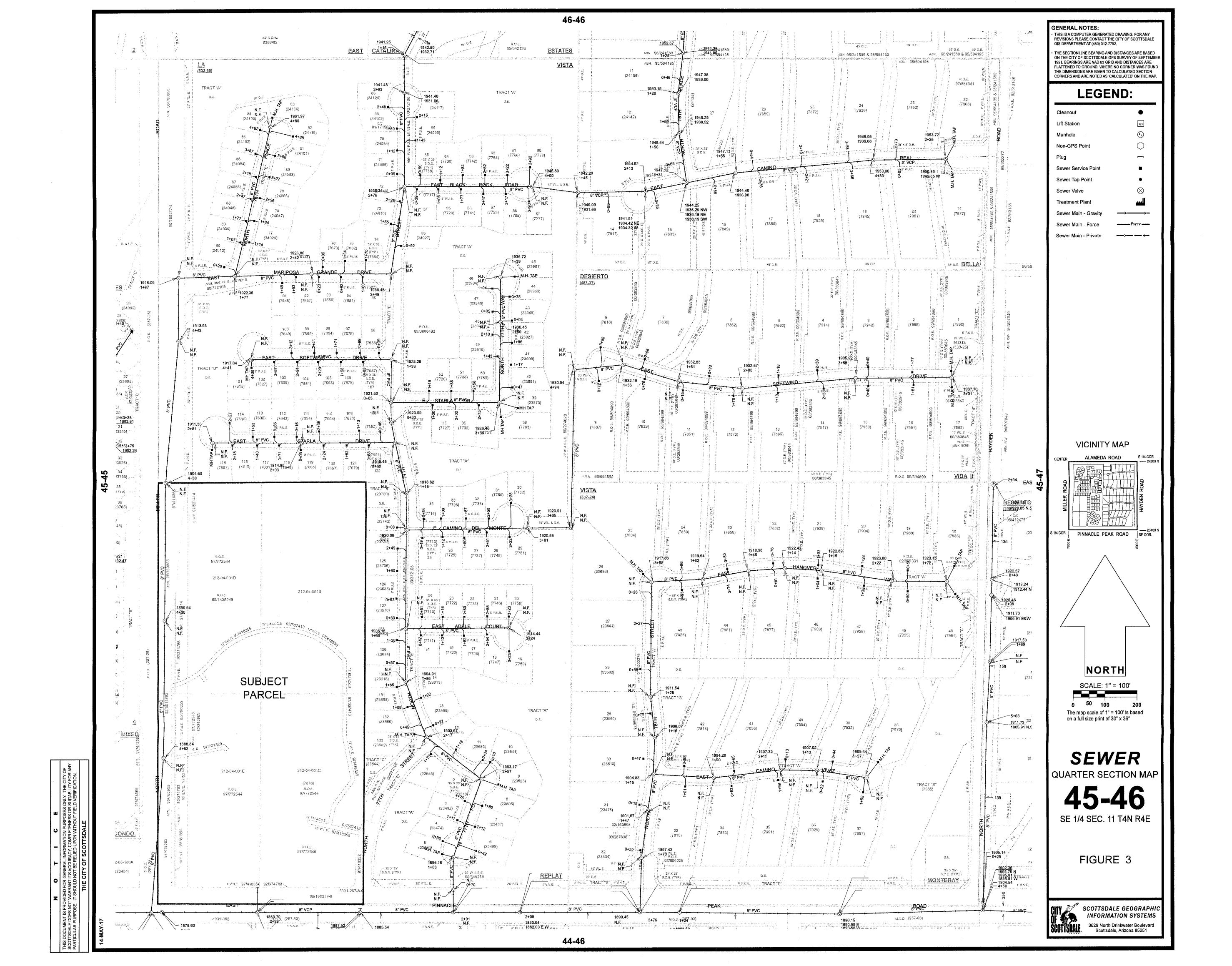
Refer to Preliminary Utility Plan (C4.00)

#### 8 REFERENCES

- COS OS Sewer Plan number 45-46
- 2. City of Scottsdale Design Standards & Policies Manual, 2010 (Chapter 7 Wastewater)





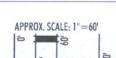






# PINNACLE PEAK & MILLER

FIGURE 4





1731



# APPENDIX I Calculations

# 8" Sanitary at S=2.67% - 2500 gpd ADD

| 8 3                         | sanitary at 5=2. | 01% - 2                               | SOU gpa ADD |
|-----------------------------|------------------|---------------------------------------|-------------|
| Project Description         |                  |                                       |             |
| Friction Method             | Manning Formula  |                                       |             |
| Solve For                   | Normal Depth     |                                       |             |
| Input Data                  |                  |                                       |             |
|                             |                  | 0.013                                 |             |
| Roughness Coefficient       |                  | 0.02670                               | ft/ft       |
| Channel Slope<br>Diameter   |                  | 8.00                                  | in          |
|                             |                  | 2500.00                               |             |
| Discharge                   |                  | 2300.00                               | gal/day     |
| Results                     |                  |                                       |             |
| Normal Depth                |                  | 0.26                                  | in          |
| Flow Area                   |                  | 0.00                                  | ft²         |
| Wetted Perimeter            |                  | 0.24                                  | ft          |
| Hydraulic Radius            |                  | 0.17                                  | in          |
| Top Width                   |                  | 0.24                                  | ft          |
| Critical Depth              |                  | 0.03                                  | ft          |
| Percent Full                |                  | 3.3                                   | %           |
| Critical Slope              |                  | 0.00994                               | ft/ft       |
| Velocity                    |                  | 1.12                                  | ft/s        |
| Velocity Head               |                  | 0.02                                  | ft          |
| Specific Energy             |                  | 0.04                                  | ft          |
| Froude Number               |                  | 1.64                                  |             |
| Maximum Discharge           |                  | 2.12                                  | ft³/s       |
| Discharge Full              |                  | 1.97                                  | ft³/s       |
| Slope Full                  |                  | 0.00000                               | ft/ft       |
| Flow Type                   | SuperCritical    |                                       |             |
| GVF Input Data              |                  |                                       |             |
| Downstream Depth            |                  | 0.00                                  | in          |
| Length                      |                  | 0.00                                  | ft          |
| Number Of Steps             |                  | 0                                     |             |
| GVF Output Data             |                  |                                       |             |
| Upstream Depth              |                  | 0.00                                  | in          |
| Profile Description         |                  | 2.30                                  |             |
| Profile Headloss            |                  | 0.00                                  | ft          |
| Average End Depth Over Rise |                  | 0.00                                  | %           |
| Normal Depth Over Rise      |                  | 3.26                                  | %           |
| Downstream Velocity         |                  | Infinity                              | ft/s        |
| Downstiean velocity         |                  | · · · · · · · · · · · · · · · · · · · | 100         |

# 8" Sanitary at S=2.67% - 2500 gpd ADD

# **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.26 in
 in

 Critical Depth
 0.03 ft
 Channel Slope
 0.02670 ft/ft

 Critical Slope
 0.00994 ft/ft
 0.00994 ft/ft

# 8" Sanitary at S=2.67% - 7500 gpd PDD

| 0 3                         | banitary at 3-2 | .01/0-1  | 300 gpa PDD |
|-----------------------------|-----------------|----------|-------------|
| Project Description         |                 |          |             |
| Friction Method             | Manning Formula |          |             |
| Solve For                   | Normal Depth    |          |             |
| Input Data                  |                 |          |             |
| Roughness Coefficient       |                 | 0.013    |             |
| Channel Slope               |                 | 0.02670  | ft/ft       |
| Diameter                    |                 | 8.00     | in          |
| Discharge                   |                 | 7500.00  | gal/day     |
| Results                     |                 |          |             |
| Normal Depth                |                 | 0.44     | in          |
| Flow Area                   |                 | 0.01     | ft²         |
| Wetted Perimeter            |                 | 0.32     | ft          |
| Hydraulic Radius            |                 | 0.29     | in          |
| Top Width                   |                 | 0.30     | ft          |
| Critical Depth              |                 | 0.05     | ft          |
| Percent Full                |                 | 5.5      | %           |
| Critical Slope              |                 | 0.00829  | ft/ft       |
| Velocity                    |                 | 1.54     | ft/s        |
| Velocity Head               |                 | 0.04     | ft          |
| Specific Energy             |                 | 0.07     | ft          |
| Froude Number               |                 | 1.73     |             |
| Maximum Discharge           |                 | 2.12     | ft³/s       |
| Discharge Full              |                 | 1.97     | ft³/s       |
| Slope Full                  | 00              | 0.00000  | ft/ft       |
| Flow Type                   | SuperCritical   |          |             |
| GVF Input Data              |                 |          |             |
| Downstream Depth            |                 | 0.00     | in          |
| Length                      |                 | 0.00     | ft          |
| Number Of Steps             |                 | 0        |             |
| GVF Output Data             |                 |          |             |
| Upstream Depth              |                 | 0.00     | in          |
| Profile Description         |                 |          |             |
| Profile Headloss            |                 | 0.00     | ft          |
| Average End Depth Over Rise |                 | 0.00     | %           |
| Normal Depth Over Rise      |                 | 5.51     | %           |
| Downstream Velocity         |                 | Infinity | ft/s        |

# 8" Sanitary at S=2.67% - 7500 gpd PDD

# **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.44 in
 in

 Critical Depth
 0.05 ft
 t

 Channel Slope
 0.02670 ft/ft
 t

 Critical Slope
 0.00829 ft/ft

# 8" Sanitary at \$=2.67% - Full Flow (65%)

| 0 3                         | anitary at 3-2  | 4.0/70 - FU | III Flow (65 %) |
|-----------------------------|-----------------|-------------|-----------------|
| Project Description         |                 |             |                 |
| Friction Method             | Manning Formula |             |                 |
| Solve For                   | Discharge       |             |                 |
| Input Data                  |                 |             |                 |
| Roughness Coefficient       |                 | 0.013       |                 |
| Channel Slope               |                 | 0.02670     | ft/ft           |
| Normal Depth                |                 | 5.20        | in              |
| Diameter                    |                 | 8.00        | in              |
| Results                     |                 |             |                 |
| Discharge                   |                 | 965270.71   | gal/day         |
| Flow Area                   |                 | 0.24        | ft²             |
| Wetted Perimeter            |                 | 1.25        | ft              |
| Hydraulic Radius            |                 | 2.31        | in              |
| Top Width                   |                 | 0.64        | ft              |
| Critical Depth              |                 | 0.57        | ft              |
| Percent Full                |                 | 65.0        | %               |
| Critical Slope              |                 | 0.01421     | ft/ft           |
| Velocity                    |                 | 6.22        | ft/s            |
| Velocity Head               |                 | 0.60        | ft              |
| Specific Energy             |                 | 1.03        | ft              |
| Froude Number               |                 | 1.78        |                 |
| Maximum Discharge           |                 | 2.12        | ft³/s           |
| Discharge Full              |                 | 1.97        | ft³/s           |
| Slope Full                  |                 | 0.01528     | ft/ft           |
| Flow Type                   | SuperCritical   |             |                 |
| GVF Input Data              |                 |             |                 |
| Downstream Depth            |                 | 0.00        | in              |
| Length                      |                 | 0.00        | ft              |
| Number Of Steps             |                 | 0           |                 |
| GVF Output Data             |                 |             |                 |
| Upstream Depth              |                 | 0.00        | in              |
| Profile Description         |                 |             |                 |
| Profile Headloss            |                 | 0.00        | ft              |
| Average End Depth Over Rise |                 | 0.00        | %               |
| Normal Depth Over Rise      |                 | 65.00       | %               |
| Downstream Velocity         |                 | Infinity    | ft/s            |
|                             |                 |             |                 |

# 8" Sanitary at S=2.67% - Full Flow (65%)

### **GVF** Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 5.20 in

 Critical Depth
 0.57 ft

 Channel Slope
 0.02670 ft/ft

 Critical Slope
 0.01421 ft/ft

# 8" Sanitary at S=1.00% - 11.250 gpd ADD

| 8 2                         | anitary at S=1.0 | 00% - 11 | ,250 gpa ADD |
|-----------------------------|------------------|----------|--------------|
| Project Description         |                  |          |              |
| Friction Method             | Manning Formula  |          |              |
| Solve For                   | Normal Depth     |          |              |
| Input Data                  |                  |          |              |
| Roughness Coefficient       |                  | 0.013    |              |
| Channel Slope               |                  | 0.01000  | ft/ft        |
| Diameter                    |                  | 8.00     | in           |
| Discharge                   |                  | 11250.00 | gal/day      |
| Results                     |                  |          |              |
| Normal Depth                |                  | 0.67     | in           |
| Flow Area                   |                  | 0.01     | ft²          |
| Wetted Perimeter            |                  | 0.39     | ft           |
| Hydraulic Radius            |                  | 0.43     | in           |
| Top Width                   |                  | 0.37     | ft           |
| Critical Depth              |                  | 0.06     | ft           |
| Percent Full                |                  | 8.4      | %            |
| Critical Slope              |                  | 0.00770  | ft/ft        |
| Velocity                    |                  | 1.25     | ft/s         |
| Velocity Head               |                  | 0.02     | ft           |
| Specific Energy             |                  | 0.08     | ft           |
| Froude Number               |                  | 1.13     |              |
| Maximum Discharge           |                  | 1.30     | ft³/s        |
| Discharge Full              |                  | 1.21     | ft³/s        |
| Slope Full                  |                  | 0.00000  | ft/ft        |
| Flow Type                   | SuperCritical    |          |              |
| GVF Input Data              |                  |          |              |
| Downstream Depth            |                  | 0.00     | in           |
| Length                      |                  | 0.00     | ft           |
| Number Of Steps             |                  | 0        |              |
| GVF Output Data             |                  |          |              |
| Upstream Depth              |                  | 0.00     | in           |
| Profile Description         |                  | 2.30     |              |
| Profile Headloss            |                  | 0.00     | ft           |
| Average End Depth Over Rise |                  | 0.00     | %            |
| Normal Depth Over Rise      |                  | 8.37     | %            |
| Downstream Velocity         |                  | Infinity | ft/s         |

# 8" Sanitary at S=1.00% - 11,250 gpd ADD

# **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 0.67 in

 Critical Depth
 0.06 ft

 Channel Slope
 0.01000 ft/ft

 Critical Slope
 0.00770 ft/ft

# 8" Sanitary at S=1.00% - 33,750 gpd PDD

| 8 5                         | anitary at 5=1. | 00% - 33 | , rou gpa Puu |
|-----------------------------|-----------------|----------|---------------|
| Project Description         |                 |          |               |
| Friction Method             | Manning Formula |          |               |
| Solve For                   | Normal Depth    |          |               |
| Input Data                  |                 |          |               |
| Roughness Coefficient       |                 | 0.013    |               |
| Channel Slope               |                 | 0.01000  | ft/ft         |
| Diameter                    |                 | 8.00     | in            |
| Discharge                   |                 | 33750.00 | gal/day       |
| Results                     |                 |          |               |
| Normal Depth                |                 | 1.13     | in            |
| Flow Area                   |                 | 0.03     | ft²           |
| Wetted Perimeter            |                 | 0.51     | ft            |
| Hydraulic Radius            |                 | 0.70     | in            |
| Top Width                   |                 | 0.46     | ft            |
| Critical Depth              |                 | 0.10     | ft            |
| Percent Full                |                 | 14.2     | %             |
| Critical Slope              |                 | 0.00682  | ft/ft         |
| Velocity                    |                 | 1.73     | ft/s          |
| Velocity Head               |                 | 0.05     | ft            |
| Specific Energy             |                 | 0.14     | ft            |
| Froude Number               |                 | 1.20     |               |
| Maximum Discharge           |                 | 1.30     | ft³/s         |
| Discharge Full              |                 | 1.21     | ft³/s         |
| Slope Full                  |                 | 0.00002  | ft/ft         |
| Flow Type                   | SuperCritical   |          |               |
| GVF Input Data              |                 |          |               |
| Downstream Depth            |                 | 0.00     | in            |
| Length                      |                 | 0.00     | ft            |
| Number Of Steps             |                 | 0        |               |
| GVF Output Data             |                 |          |               |
| Upstream Depth              |                 | 0.00     | in            |
| Profile Description         |                 |          |               |
| Profile Headloss            |                 | 0.00     | ft            |
| Average End Depth Over Rise |                 | 0.00     | %             |
| Normal Depth Over Rise      |                 | 14.16    | %             |
| Downstream Velocity         |                 | Infinity | ft/s          |
| ,                           |                 |          |               |

# 8" Sanitary at S=1.00% - 33,750 gpd PDD

# **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 1.13
 in

 Critical Depth
 0.10
 ft

 Channel Slope
 0.01000
 ft/ft

 Critical Slope
 0.00682
 ft/ft

# 8" Sanitary at S=1.00% - Full Flow (65%)

| 0 3                         | anitary at 5-1   | .00 /o - I-u | 11 Flow (03 /6) |
|-----------------------------|--|--------------|-----------------|
| Project Description         |  |              |                 |
| Friction Method             | Manning Formula  |              |                 |
| Solve For                   | Discharge  |              |                 |
| Input Data                  |  |              |                 |
| Roughness Coefficient       | er for the second s | 0.013        |                 |
| Channel Slope               |  | 0.01000      | ft/ft           |
| Normal Depth                |  | 5.20         | in              |
| Diameter                    |  | 8.00         | in              |
| Results                     |  |              |                 |
| Discharge                   |  | 590736.08    | gal/day         |
| Flow Area                   |  | 0.24         | ft²             |
| Wetted Perimeter            |  | 1.25         | ft              |
| Hydraulic Radius            |  | 2.31         | in              |
| Top Width                   |  | 0.64         | ft              |
| Critical Depth              |  | 0.45         | ft              |
| Percent Full                |  | 65.0         | %               |
| Critical Slope              |  | 0.00882      | ft/ft           |
| Velocity                    |  | 3.81         | ft/s            |
| Velocity Head               |  | 0.23         | ft              |
| Specific Energy             |  | 0.66         | ft              |
| Froude Number               |  | 1.09         |                 |
| Maximum Discharge           |  | 1.30         | ft³/s           |
| Discharge Full              |  | 1.21         | ft³/s           |
| Slope Full                  |  | 0.00572      | ft/ft           |
| Flow Type                   | SuperCritical  |              |                 |
| GVF Input Data              |  |              |                 |
| Downstream Depth            |  | 0.00         | in              |
| Length                      |  | 0.00         | ft              |
| Number Of Steps             |  | 0            |                 |
| GVF Output Data             |  |              |                 |
| Upstream Depth              |  | 0.00         | in              |
| Profile Description         |  |              |                 |
| Profile Headloss            |  | 0.00         | ft              |
| Average End Depth Over Rise |  | 0.00         | %               |
| Normal Depth Over Rise      |  | 65.00        | %               |
| Downstream Velocity         |  | Infinity     | ft/s            |

# 8" Sanitary at S=1.00% - Full Flow (65%)

# **GVF** Output Data

| Upstream Velocity | Infinity | ft/s  |
|-------------------|----------|-------|
| Normal Depth      | 5.20     | in    |
| Critical Depth    | 0.45     | ft    |
| Channel Slope     | 0.01000  | ft/ft |
| Critical Slope    | 0.00882  | ft/ft |



# APPENDIX II Preliminary Utility Plan

# P.F. CHANG'S RESIDENTIAL DEVELOPMENT PINNACLE PEAK RD. AND MILLER RD. PRELIMINARY UTILITY PLAN **OWNER** PFCCB PINNACLE PEAK LLC 7676 E. PINNACLE PEAK RD. SCOTTSDALE, AZ 85255 ATTN: ZACH SHIRK BASIS OF BEARING THE BASIS OF BEARING AND ALL MONUMENTATION SHOWN **CIVIL ENGINEER** SUSTAINABILITY ENGINEERING GROUP QUARTER OF SECTION 11, TOWNSHIP 4 NORTH, RANGE 4 EAST, USING A BEARING OF NORTH 89 DEGREES 51 MINUTES 8280 E. GELDING DR., SUITE 101 11 SECONDS WEST, AS SHOWN ON AN UNRECORDED SCOTTSDALE, ARIZONA 85260 ALTA/ACSM LAND TITLE SURVEY PREPARED BY GILBERTSON &

MH#1 RIM= 1883.50

IE=1874.70 (8" E)

IE=1874.03 (8" N/S) EX.

- 48 LF SDR-35

PVC @S=1.00%

50\*

D.I. PIPE

l 十 236 LF 8"

40 LF SRD-35 PVC @ S=2.00 32

- PROPOSED FIRE

IE=1882.60 (8" N)

IE=1882.40 (8" SW)

RIM = 1889.03

52\*

IE= 1878.68 (8" N)

IE= 1878.48 (8" SE)

D.I. PIPE

31

36

288 LF 8"

D.I. PIPE -

SCALE: 1" = 60'

IE=1877.38 \_(8" N/S) EX MILLER RD.

PROPOSED FIRE

 $(55^*)$ 

28

8x8 TEE -

D.I. PIPE

8"D.I. PIPE

HYDRANT ----

54\*

/- 402 LF SDR-35

PVC @S=2.67%

29

- 317 LF SDR-35

PVC @S=2.67%

53\*

RIM = 1878.46

IE=1870.86

(8" N/S) EX.

PVC @S=1.00% -

IE=1877.00 (8" NE)

IE=1876.80 (8"W) -

IE= 1877.68 (8"NW)

RIM = 1888.13

IE=1881.50 (8" NE)

IE=1881.30 (8" W) ---

45 LF SDR-35

~ PVC @S=2.00%

LA VISTA REPLAT

IE= 1877.48 (8"SW) -47

\_255 LF SDR-35 PVC @S=1.42% —

PEAK RD.

ASSOCIATES DATED AUGUST 13, 2004.

T.S.&V.,

D.I. PIPE

EX. MH

RIM=1897 +/-

IE=1885.39 +/-

RIM=1897.16

326 LF 8" >

RIM=1908.32

LA VISTA REPLAT

IE=1900.24 (8"N)

E=1889.61 (8" NE) IE=1889.41 (8" S)

∕- 72 ĹF SDR-35

/ PVC @S=2.67%

RIM = 1900.00

/- 311 LF SDR-35

PVC @S=2.67%

PROPOSED FIRE

27 LF SDR-35 PVC @S=2.30% -

IE=1891.74 (8" NE) IE=1891.54 (8"SW)

(8" N/S) UNKNOWN

APPLICANT/DEVELOPER PINNACLE PEAK ROAD SNELL & WILMER 400 E. VAN BUREN ST. #1900

PHOENIX, AZ 85004 PHONE: 602-328-6269 ATTN: NICK WOOD, ESQ

EX. MH

TYP. PROPOSED FIRE

222 LF 13\*

RIM = 1910.61

IE=1901.64 (8" NW)

RIM=1904.67

(8" N/S) EX. -

IE=1893.59

PLANNER LVA URBAN DESIGN STUDIO, LLC PHONE: 480-994-0994 PHONE: 480-588-7226 ATTN: MARK REDDIE ATTN: ALI FAKIH

MH #10 RIM=1901.58

IE=1890.21 (8" N/S) EX.

IE=1890.88 (8"E) PROP.

342 LF SDR-35

PVC @S=2.67% -

IE=1900.20 (8" SE) —

54 LF SRD-35 ∠ PVC @S=2.67% ·

- 80 LF SDR-35

PVC @S=2.67% 🦎

RIM=1909.04

IE=1901.16 (8" NW)

IE=1900.96 (8" S)

D.I. PIPE

IE=1903.30 (8" SE)

LA VISTA REPLAT

RIM=1908.78

VICINITY MAP

EXPIRES 9/30/2017



**UTILITY NOTES:** 

HAPPY VALLEY ROAD

PROTECTION IN ACCORDANCE WITH MAG AND C.O.S. DESIGN CRITERIA.

1. UTILITY CROSSINGS WILL BE DESIGNED FOR

PROPOSED LEGEND

- PROPERTY LINE ----8"W----- WATER LINE

-----8"S------ SEWER LINE FIRE HYDRANT

SEWER MANHOLE

I" WATER METER

- SANTIAGO MALONEY COUNSELL COUNSELL PROJ. MGR. — MALONEY 08/18/2017 ISSUED FOR: ZONING REVISION NO .:

JOB NO.: 170566

PRELIMINARY UTILITY PLAN

C4.00

SHEET TITLE: