Color Drawdowns
Archaeological Resources
Airport Vicinity Development Checklist
Parking Study
Trip Generation Comparison
Parking Master Plan

CASE FILE 05 21.44 22-2N-2016



COTTONWOODS RESORT & SUITES SEWER SYSTEM ASSESSMENT August 2016

Project Description:

The existing site was developed with a one-story building serving as the Cottonwoods Resort lobby and a restaurant. The building that once served as the lobby and restaurant was recently demolished however, the existing sewer service lines remain in place. There is currently an 8-inch sewer main in Rose Lane that discharges to another 8-inch sewer in Scottsdale Road at a slope of 0.33%, which serves the Cottonwoods Resort, Alamos, the Marriot, and the Borgata. This sewer system assessment evaluates the future demand for development of the existing Cottonwoods Resort lobby and restaurant property.

Site Information:

APN#:

174-65-012G

Site Address:

6160 N Scottsdale Rd

Paradise Valley, AZ 85253

Site Area:

115,782 sq. ft. (2.6 acres)

City of Scottsdale

Water Resources Administration

Accepted w/Commenter

9379 E. San Salvador Scottsdale, AZ 85258

Duy WANN 9.7.16

Sewer Demand Calculations:

To determine the unit wastewater loads, the following references were used:

City of Scottsdale Digital Zoning Map

 Table 8-22: "Unit Daily Design Flow For Sewer – Per Land Use" in the Town of Gilbert Public Works And Engineering Standards 2015.

Table 8-23: "Wastewater Flow Peaking Factor" in the Town of Gilbert Public Works And Engineering Standards 2015.

ADEQ Bulletin No. 11

weighted Aug = 553 gra/d.

In accordance with the City of Scottsdale Zoning Map, the subject property is currently located within Zone R-R4, Resort/Townhouse Residential District. The property is in the process of being re-zoned to Zone C-1, Neighborhood Commercial. There currently is not a plan in place for the development of the subject property, so assumptions were made to determine future sewer flows based on acreage of the site and zoning designation. Since the City of Scottsdale does not have a sewer demand for gallons per acre per day, a sewer demand from the Town of Gilbert Public Works and Engineering Standards was used. Utilizing this information, it can be determined from Table 8-22 of the Town of Gilbert Public Works and Engineering Standards 2015 manual that the design unit wastewater load for property zoned with a commercial land use is 707 gallons per acre per day.



The existing Average Daily Flow is:

Total Average Daily Flow = (707 gal. per acre per day) x (2.6 acres) = 1,838 gal/day (1.28 gal/min)

A peaking factor of 2.9 was determined per Town of Gilbert Design Standards & Policies Manual.

Total Peak Factor = (2.9) x (1,838 gal/day) = 5,331 gal/day (3.70 gal/min)

Pipe Velocity and Capacity Calcu	lations:	6	Sapra Grimveson
Sewer Size (D):	8	inches + (Salph (Firm reson
Mannings n-value (n):	0.013	76	M CVP PO
Slope (S):	0.0033	ft./ft.	, ,
Hydraulic Radius (R):	0.167	ft.	R=D/4 (full pipe)
Manning Equation:	V=(k/n) x	$(R)^{2/3} \times (S)^{1/2}$	k = 1.486
Velocity (V), full pipe:	2.0	ft./sec	Min. = 2.0 ft./sec Per ADEQ Bulletin No. 11 Max. = 10.0 ft./sec
Pipe Capacity: 0.65	0.69	cfs	$Q = V \times A$

Note: Upon final development of the subject property, a new sewer design report shall be prepared and submitted in accordance with City of Scottsdale design guidelines and requirements.

gal/day

448,629

OK

SWC Scottsdale Road & Rose Lane Scottsdale, Arizona

Traffic Impact Analysis – FIRST REVISION

May 2017

Prepared for:

PV HOTEL VENTURE, SPE LLC

For Submittal to:

CITY OF SCOTTSDALE

EPS Group Project Number: 16-228

Prepared by: Eric R. Maceyko, P.E., PTOE

Bryan A. Martin, P.E.

CITY OF SCOTTSDALE
TRANSPORTATION DEPARTMENT

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Expires:6/30/2017

DATE: June 20, 2017

REVIEWER: Man Rud

EPS

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Executive Summary

Introduction

PV Hotel Venture, SPE LLC is proposing a new restaurant development on the southwest corner of Scottsdale Road and Rose Lane in Scottsdale, Arizona. The proposed development encompasses an existing parcel of land on approximately 2.7 acres that previously contained an 8,000 square foot building with 2,000 square feet of patio space. This previous building contained hotel lobby and restaurant uses and was recently demolished.

The existing parcel is being planned for redevelopment to contain either one (1) single-story restaurant pad or two (2) separate two-story restaurant pads, with either option providing a total of 9,000 square feet of indoor building area and 3,000 square feet of outdoor patio area.

Results

The proposed development is anticipated to generate the following weekday traffic volumes.

Time Period	Day		AM Peak Hour			PM Peak Hour			
Time Period	Enter	Exit	Total	Enter	Exit	Total	Enter	Exit	Tota
Weekday	572	572	1,144	54	50	104	59	41	100

Recommendations without Proposed Development

The existing Scottsdale Road / Rose Lane intersection is operating at a level-of-service "B" during both peak hours with some individual movements operating at level-of-service "D" or "E". All instances of level-of-service "D" or "E" occurred on Rose Lane. These levels-of-service are anticipated to continue for ambient 2018 traffic conditions with minor additional delay.

It is also recommended to provide new lane striping on the eastbound Rose Lane approach at its intersection with Scottsdale Road to improve visibility of lane separation.

Recommendations with Proposed Development

All intersections are anticipated to operate at a level-of-service "B" or better under the 2018 with proposed site traffic conditions. The Scottsdale Road / Rose Lane intersection is anticipated to continue to have some individual movements operating at level-of-service "D" or "E". All instances of level-of-service "D" or "E" occurred on Rose Lane.

It is recommended to implement a revised lane configuration on the eastbound and westbound Rose Lane approaches consisting of separate left-turn and shared through / right-turn lanes.

No significant change in intersection level-of-service is anticipated with the addition of the proposed site traffic.

No additional turn lanes are warranted or recommended.

Introduction

PV Hotel Venture, SPE LLC is proposing a new restaurant development on the southwest corner of Scottsdale Road and Rose Lane in Scottsdale, Arizona. The proposed development encompasses an existing parcel of land on approximately 2.7 acres that previously contained an 8,000 square foot building with 2,000 square feet of patio space. This previous building contained hotel lobby and restaurant uses and was recently demolished.

The existing parcel is being planned for redevelopment to contain either one (1) single-story restaurant pad or two (2) separate two-story restaurant pads, with either option providing a total of 9,000 square feet of indoor building area and 3,000 square feet of outdoor patio area.

Scope of Study

There are eight (8) purposes for this analysis:

- Evaluate existing traffic conditions
- Estimate future ambient 2018 traffic volumes
- Evaluate ambient 2018 traffic conditions
- Estimate new traffic generated by proposed development
- Assign and distribute new traffic to surrounding street system
- Determine need for auxiliary lanes at all study intersections
- Evaluate operation of adjacent streets and intersections with proposed development
- Determine need for modified traffic control at all study intersections

Proposed Development

The site is located on the southwest corner of Scottsdale Road and Rose Lane. Figure 1 provides a vicinity map proximate to the proposed site. Figure 2 provides an initial site plan for the proposed development representing the two-building option.

The primary road used to access the site is Rose Lane which connects to Scottsdale Road. Rose Lane does not provide through access east or west of Scottsdale Road. Scottsdale Road is the main arterial providing regional access. The existing site has two full access driveways on Rose Lane west of Scottsdale Road, both of which are planned to be utilized by the proposed development. The driveways are labeled as Access A and Access B for the purposes of this analysis.



Figure 1: Vicinity Map

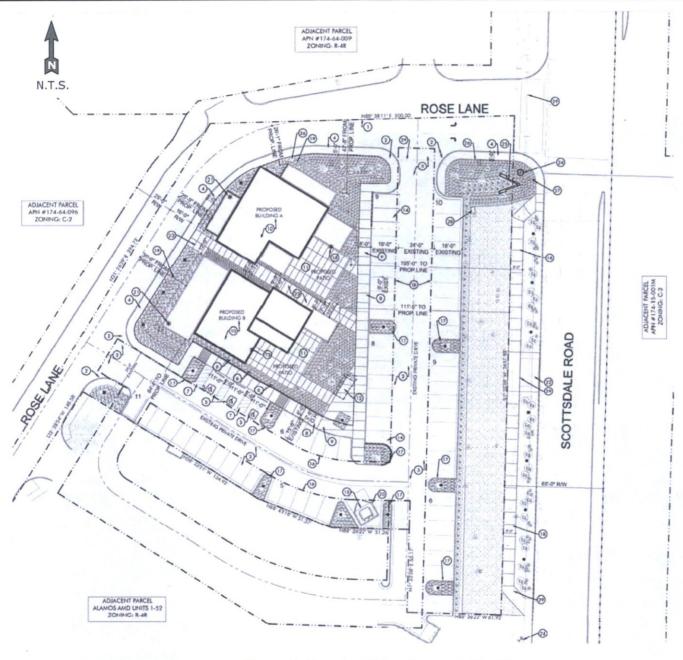


Figure 2: Proposed Development Site Plan

Surrounding Land Use and Transportation System

The proposed development is served primarily by Scottsdale Road and is located adjacent to various residential and mixed-use commercial and office properties. The site is located approximately one-quarter mile south of Lincoln Drive and north of McDonald Drive. Lincoln Drive provides additional west regional access and McDonald Drive provides additional east and west regional access. The Loop 101 freeway is located approximately 2 miles to the east of the proposed development with an interchange at McDonald Drive.

Scottsdale Road is a north-south Major Arterial Road that currently provides three lanes in each direction adjacent to the site with a posted speed limit of 45 mph. Rose Lane is an east-west local road west of Scottsdale Road adjacent to the site providing one lane in each direction with a posted speed limit of 25 mph. The alignment curves to the southwest and terminates shortly west of the proposed development.

Study Intersections

The existing Scottsdale Road / Rose Lane intersection will be analyzed for existing and ambient 2018 conditions for both weekday morning and evening peak hour conditions.

The following additional intersections will only be analyzed for 2018 with the proposed development conditions:

Access A and Rose Lane Rose Lane and Access B

Figure 3 depicts the existing lane configurations at the study intersections.

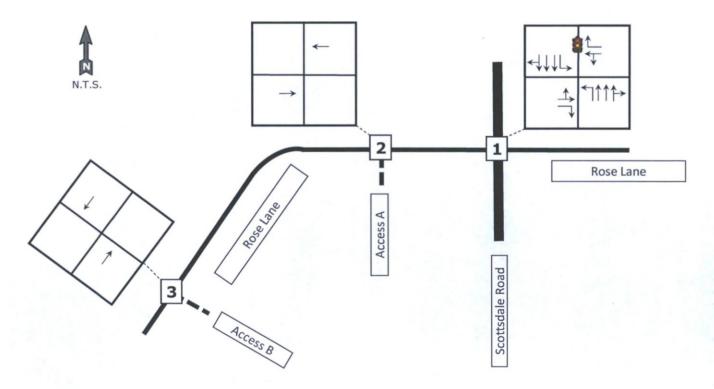


Figure 3: Existing Lane Configurations and Traffic Control

Existing Traffic Counts

Approach and departure traffic volumes were collected on Thursday, 28 July 2016 for 24 hours in 15-minute intervals on the following road segments:

- Scottsdale Road, north of Rose Lane
- · Scottsdale Road, south Rose Lane
- · Rose Lane, east of Scottsdale Road
- Rose Lane, west of Scottsdale Road

Four-hour turning movement traffic counts were also obtained at the Scottsdale Road / Rose Lane intersection on Thursday, 28 July 2016 from 7:00 AM to 9:00 AM, and from 4:00 PM to 6:00 PM. Since July is historically a low traffic volume month, the counts were increased by a monthly adjustment factor. The monthly adjustment factor for July, as provided by the City of Scottsdale, is 1.08. **Figure 4** depicts the adjusted existing weekday traffic volumes. **Figure 5** and **Figure 6** respectively depict the adjusted existing weekday morning and evening peak hour traffic volumes.

The existing traffic volumes are provided in **Appendix A** to this report. Also included in **Appendix A** are tables providing the hourly counts by time of day, and graphs plotting the hourly traffic counts. **Appendix A.1** contains the approach and departure volumes. Also included in this appendix are tables determining the maximum morning and evening hourly volumes and peak hour factors as determined from the approach counts, and graphs plotting the hourly traffic counts. **Appendix A.2** contains the turning movement counts.

Historical traffic data on Scottsdale Road between Lincoln Drive and McDonald Drive is provided by the City of Scottsdale. The volumes were reviewed to determine an appropriate average annual growth rate to obtain predicted 2018 traffic volumes. The City provides historic traffic count data every other year from 1998 to 2014. The current adjusted 2016 traffic volumes collected on Scottsdale Road are also included.

Table 1 provides the historic traffic volumes by year.

Table 1: Historic Traffic Volumes Summary

AVERA	AGE DAILY TRAFFIC VO	LUMES	
YEARS	YEARS SCOTTSDALE ROAD		
1998	70,500	-	
2000	70,300	0%	
2002	50,200	-14%	
2004	51,400	1%	
2006	47,700	-4%	
2008	43,900	-4%	
2010	42,400	-2%	
2012	43,200	1%	
2014	40,700	-3%	
2016	43,383	3%	
AVERAG	E ANNUAL GROWTH	-2%	

As can be seen in **Table 1**, growth has been inconsistent with some years reporting increases and other years reporting decreases in traffic volume. Therefore, it was determined that a conservative nominal annual growth rate of 2%, applied linearly to all existing traffic volumes, was appropriate to estimate ambient 2018 traffic volumes. **Figure 7** depicts the ambient 2018 weekday traffic volumes. **Figure 8** and **Figure 9** respectively depict the ambient 2018 weekday morning and evening peak hour traffic volumes.

The existing Cottonwoods Resort, located west of the proposed development with primary access on Rose Lane, is currently undergoing redevelopment. As part of the planning for the redevelopment the Cottonwoods Resort Traffic and Parking Impact Analysis, was prepared by Kimley-Horn & Associates in February 2014. Included in this report are the anticipated morning and evening peak hour traffic volumes anticipated with the new development. These traffic volumes were added to the estimated ambient 2018 traffic volumes and are included in **Figure 8** and **Figure 9**. **Appendix B** contains the pertinent excerpts from the previous report.



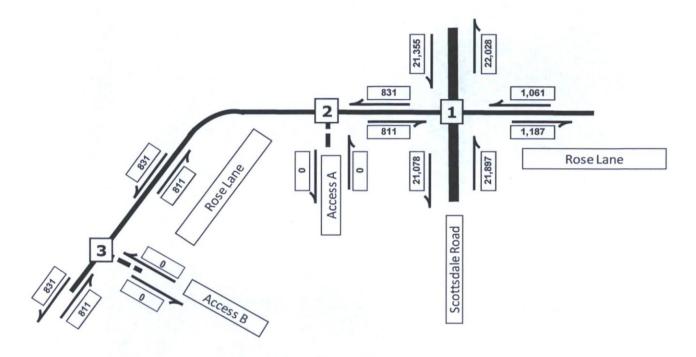


Figure 4: Existing Traffic Volumes - Day

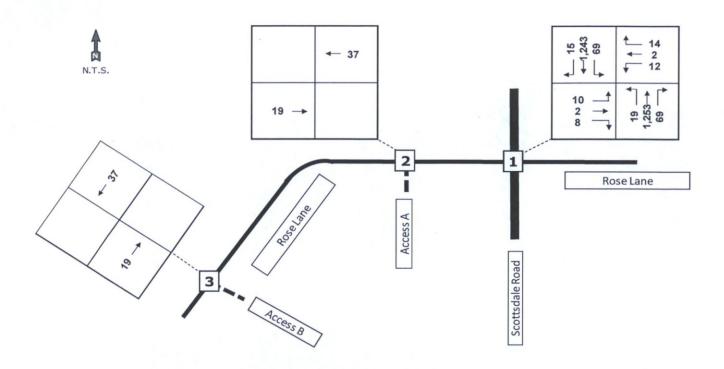


Figure 5: Existing Traffic Volumes - AM Peak Hour

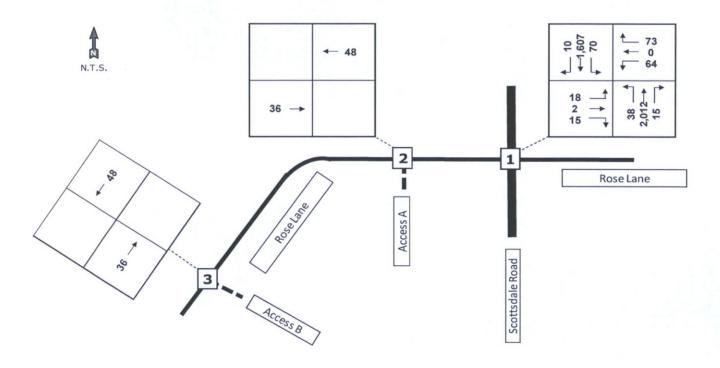


Figure 6: Existing Traffic Volumes - PM Peak Hour



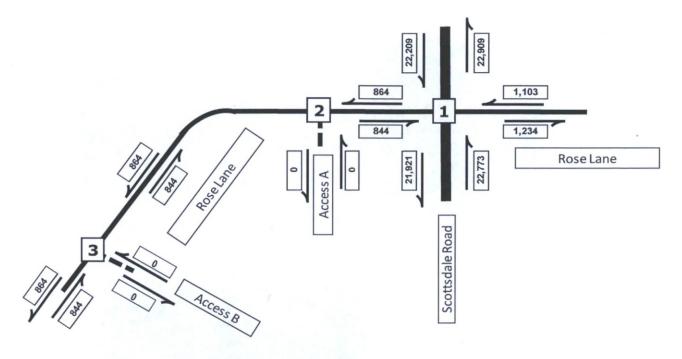


Figure 7: Ambient 2018 Traffic Volumes - Day

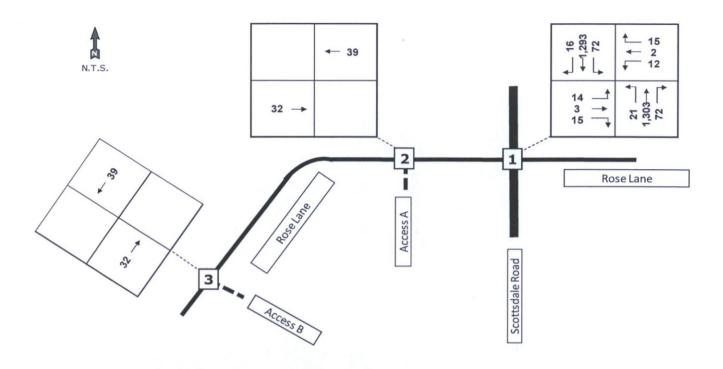


Figure 8: Ambient 2018 Traffic Volumes - AM Peak Hour

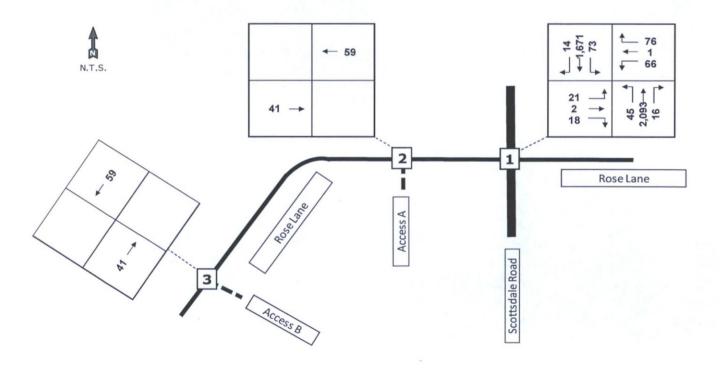


Figure 9: Ambient 2018 Traffic Volumes - PM Peak Hour

Level-of-Service Analysis without Site

The ability of a transportation system to transmit the transportation demand is characterized as its level-of-service (LOS). Level-of-service is a rating system from "A", representing the best operation with the least delay, to "F", representing the worst operation with the greatest delay. Typically, level-of-service "D" is considered the minimum acceptable operation. The appropriate reference for level-of-service operation is the *Highway Capacity Manual*, published by the Transportation Research Board in 2010.

This manual considers the average delay per vehicle as the measure to determine the level-of-service for both signalized and unsignalized intersections. For signalized intersections and for multi-way stop intersections, the delay and level-of-service are calculated for the intersection, each approach, and each turning movement. For unsignalized intersections the level-of-service is defined for each minor movement for two-way stop controls, and is not defined for the major street approaches or for the entire intersection. **Figure 10** provides a diagram and **Table 2** lists the level-of-service criteria for both signalized and unsignalized intersections as stated in the *Highway Capacity Manual*.

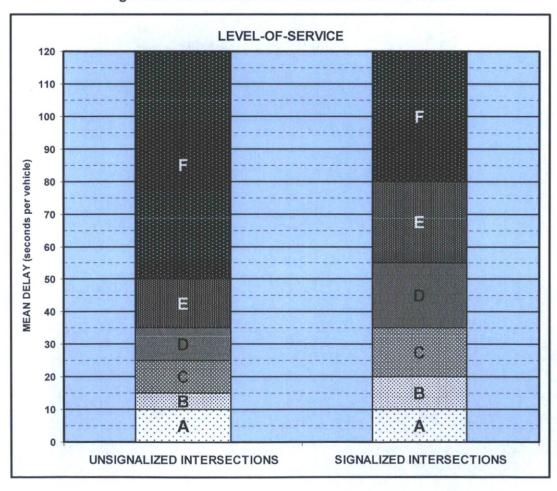


Figure 10: Level-of-Service Criteria for Intersections

Table 2: Level-of-Service Criteria for Intersections

LEVEL OF SERVICE	AVERAGE DELAY (seconds per vehicle)			
LEVEL-OF-SERVICE	UNSIGNALIZED	SIGNALIZED		
Α	≤ 10	≤ 10		
В	> 10 to 15	> 10 to 20		
С	> 15 to 25	> 20 to 35		
D	> 25 to 35	> 35 to 55		
E	> 35 to 50	> 55 to 80		
F	> 50	> 80		

Synchro software was utilized to calculate the average delay and level-of-service. The input and output for these analyses are provided as **Appendix C** to this report. **Appendix C.1** provides the results for existing traffic volumes, and **Appendix C.2** provides the results for ambient 2018 traffic volumes. **Figure 11** and **Figure 12** respectively provide the weekday morning and evening peak hour existing level-of-service for the study intersection. **Figure 13** and **Figure 14** respectively provide the weekday morning and evening peak hour ambient 2018 level-of-service for the study intersection.

The existing traffic signal timing plans for the Scottsdale Road / Rose Lane intersection were utilized in the analysis. A copy of these plans is provided in **Appendix D**. The existing Scottsdale Road / Rose Lane intersection is operating at a level-of-service "B" during both peak hours with some individual movements operating at level-of-service "D" or "E". All instances of level-of-service "D" or "E" occurred on Rose Lane. These levels-of-service are anticipated to continue for ambient 2018 traffic conditions with minor additional delay.

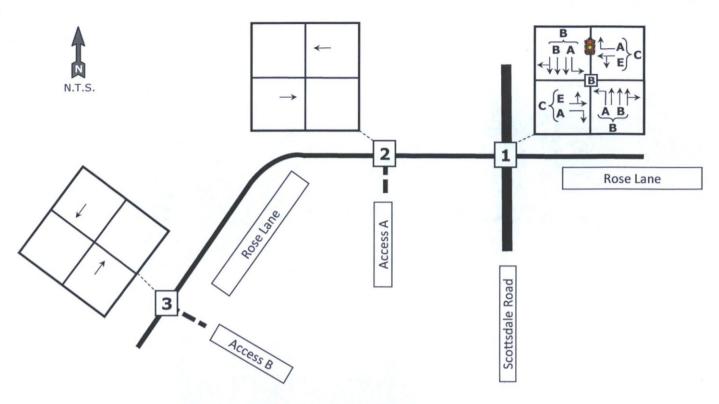


Figure 11: Existing Level-of-Service - AM Peak Hour

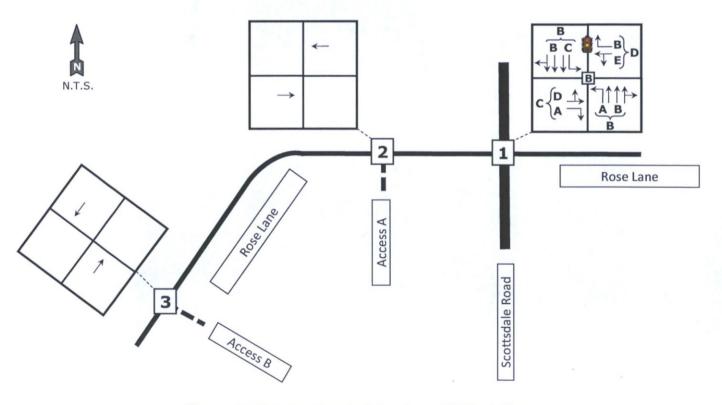


Figure 12: Existing Level-of-Service - PM Peak Hour

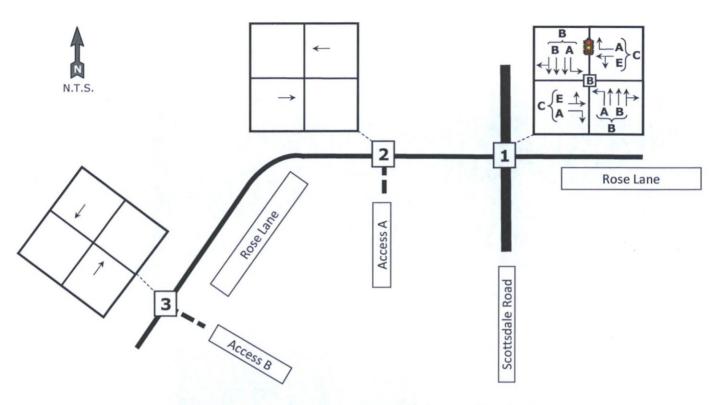


Figure 13: Ambient 2018 Level-of-Service - AM Peak Hour

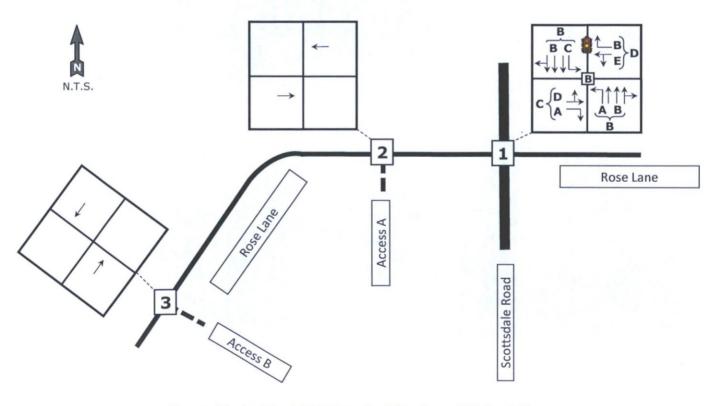


Figure 14: Ambient 2018 Level-of-Service - PM Peak Hour

Proposed Site - Trip Generation

The estimated trip generation for the proposed development was determined through the procedures and data contained within the Institute of Transportation Engineers (ITE) Trip Generation, 9th Edition, published in 2012. This document provides traffic volume data from existing developments throughout North America that can be utilized to estimate vehicle trips that might be generated from proposed developments. The traffic data are provided for 172 different categories. The estimated traffic volume is dependent upon independent variables defined by the characteristics and size of each land use category.

There is considerable data for restaurant developments. The exact nature of the restaurants is currently unknown. Therefore, ITE Land Use Code 931 – Quality Restaurant, and ITE Land Use Code 932 – High Turnover (Sit-Down) Restaurant were utilized for the trip generation analysis. The largest trip generation values from both land use codes were utilized. The independent variable available to predict trips for this land use category is 1,000 Square Feet of Gross Floor Area. It should be noted that ITE specifies that outdoor seating area is not included in the gross floor area for the purposes of calculating trip generation.

The trip generation calculation results for the proposed development are summarized in **Table 3**.

AM Peak Hour PM Peak Hour Day Time Period Enter Exit Total Enter Exit Total Enter Exit **Total** Weekday 572 572 1,144 54 50 104 59 41 100

Table 3: Proposed Development Trip Generation Summary

The same methodology was utilized to determine the estimated trip generation for the previous site. The operation of the previous restaurant use was most similar to the description contained in ITE Land Use Code 931 – Quality Restaurant. Therefore, the data from this land use was utilized for the trip generation analysis. The independent variable available to predict trips for this land use category is 1,000 Square Feet of Gross Floor Area. As previously noted, ITE specifies that outdoor seating area is not included in the gross floor area for the purposes of calculating trip generation.

The trip generation calculation results for the previous development are summarized in **Table 4**.

PM Peak Hour Day AM Peak Hour Time Period Exit Enter Enter Exit Enter Total Exit Total Total Weekday 360 360 720 20 60

Table 4: Previous Development Trip Generation Summary

Table 5 summarizes the two (2) trip generation calculations and compares the differences between the trip generation calculations for the previous development and the proposed development. The proposed development is estimated to generate less daily and evening peak hour trips and more morning peak hour trips than the previously approved development.

Table 5: Trip Generation Comparison Summary

TIME PERIOD	PREVIOUS	PROPOSED	COMPARISON
WEEKDAY			
Day	720	1,144	424
AM Peak Hour	6	104	98
PM Peak Hour	60	100	40

Appendix E contains the complete trip generation calculations.

Proposed Site - Trip Distribution

The final determination related to site traffic is the direction the generated traffic utilizes to enter and exit the site. The existing traffic count data and the Maricopa County Association of Governments (MAG) 2020 population estimates were utilized to determine the likely aggregate direction of travel for a radius of 5 miles. **Table 6** provides the anticipated aggregate trip distribution for the proposed development.

Table 6: Trip Distribution

DIRECTION OF TRAVEL	% OF TRIPS
Scottsdale Road, North	50%
Scottsdale Road, South	45%
Rose Lane, West	5%

The anticipated site traffic generated by the proposed development was assigned to the adjacent roadway network according to the trip distribution and site layout. Figure 15 provides the site weekday traffic volumes. Figure 16 and Figure 17 respectively provide the site weekday morning and evening peak hour turning movement volumes. Figure 18 provides the total of the ambient 2018 and proposed site weekday traffic volumes. Figure 19 and Figure 20 respectively provide the total of the ambient 2018 and proposed site weekday morning and evening peak hour turning movement volumes.



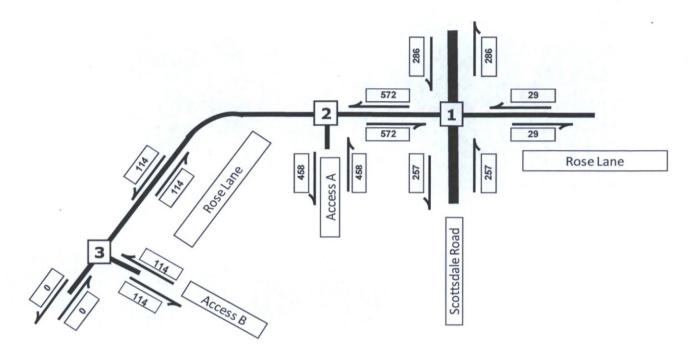


Figure 15: Site Traffic Volumes - Day

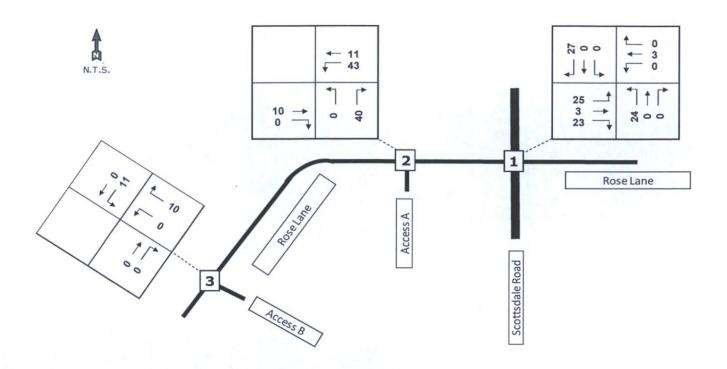


Figure 16: Site Traffic Volumes - AM Peak Hour

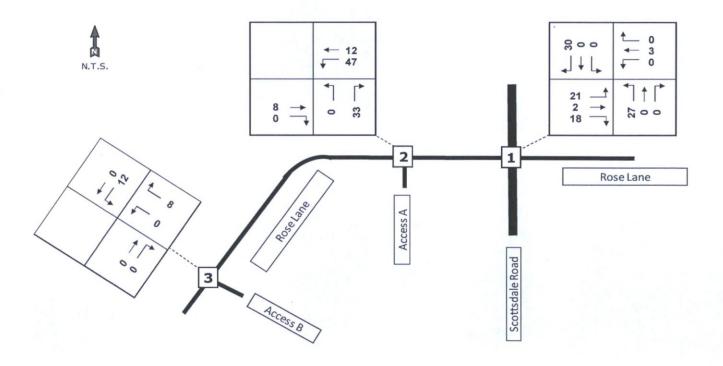


Figure 17: Site Traffic Volumes - PM Peak Hour



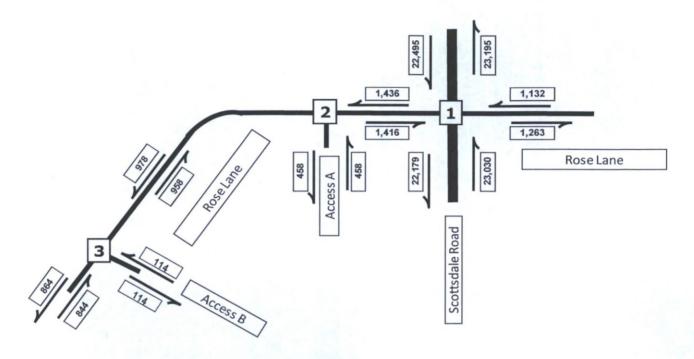


Figure 18: 2018 with Site Traffic Volumes - Day

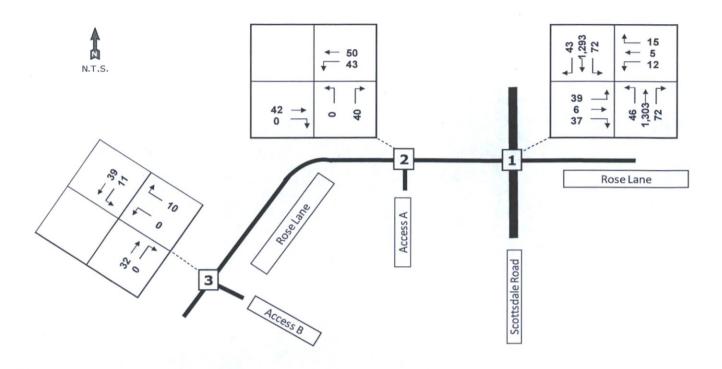


Figure 19: 2018 with Site Traffic Volumes - AM Peak Hour

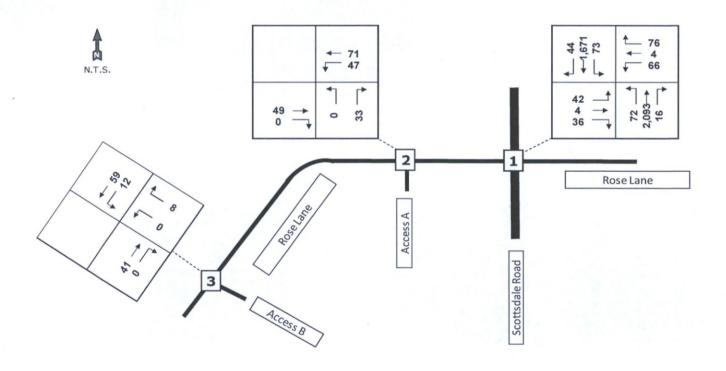


Figure 20: 2018 with Site Traffic Volumes - PM Peak Hour

Level-of-Service Analysis with Site

The level-of-service for the 2018 with site traffic volumes was analyzed for the study intersections and site accesses. Synchro software was utilized to calculate the average delay and level-of-service. All intersections are anticipated to operate at a level-of-service "B" or better under the 2018 with proposed site traffic conditions. The Scottsdale Road / Rose Lane intersection is anticipated to continue to have some individual movements operating at level-of-service "D" or "E". All instances of level-of-service "D" or "E" occurred on Rose Lane.

The average increase in intersection delay with the addition of the proposed site traffic is below:

- Scottsdale Road / Rose Lane
 - o Morning Peak Hour: + 0.7 seconds
 - o Evening Peak Hour: + 0.6 seconds

No significant change in intersection level-of-service is anticipated with the addition of the proposed site traffic.

Discussions with City staff yielded a request for the inclusion of alternate Rose Lane intersection lane configuration analyses. Two (2) alternate configurations were considered for the eastbound and westbound Rose Lane approaches:

- Alternative 1 separate left-turn, through, and right-turn lanes
- Alternative 2 separate left-turn and shared through / right-turn lanes

Figure 21 and **Figure 22** respectively provide the schematic revised striping layouts with the approximate roadway widths available. Synchro software was also utilized to calculate the average increase in intersection delay with the addition of the proposed site traffic for these two alternative lane configurations. The following results were obtained:

- Scottsdale Road / Rose Lane (Alternative 1)
 - Morning Peak Hour: + 0.5 seconds
 - Evening Peak Hour: + 0.2 seconds
- Scottsdale Road / Rose Lane (Alternative 2)
 - Morning Peak Hour: + 0.8 seconds
 - Evening Peak Hour: + 0.4 seconds

The results of all three analyses yielded only slight differences in intersection level-of-service or average delay. Therefore, it is recommended to implement the Alternative 2 lane configurations as this provides a slightly better overall average delay than the existing configuration, requires only striping modifications, and eliminates the eastbound and westbound through traffic deflection that occurs within the intersection under the existing or Alternative 1 configurations.

The input and output for all three analyses are provided as **Appendix F** to this report. **Figure 23** and **Figure 24** respectively provide the 2018 with site traffic weekday morning and evening peak hour level-of-service for the study intersections utilizing the recommended Alternative 2 lane configurations.

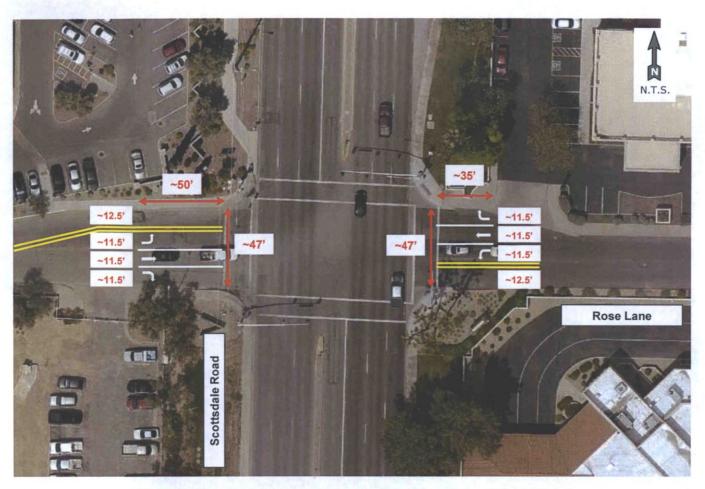


Figure 21: Rose Lane Alternate Lane Configuration – Alternative 1

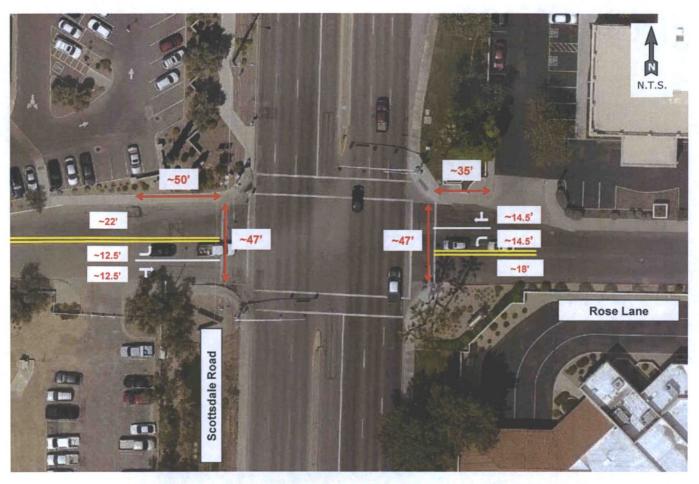


Figure 22: Rose Lane Alternate Lane Configuration – Alternative 2

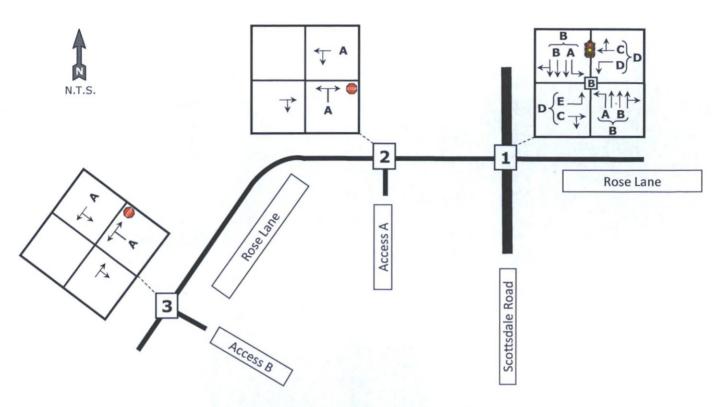


Figure 23: 2018 with Site Levels-of-Service - AM Peak Hour

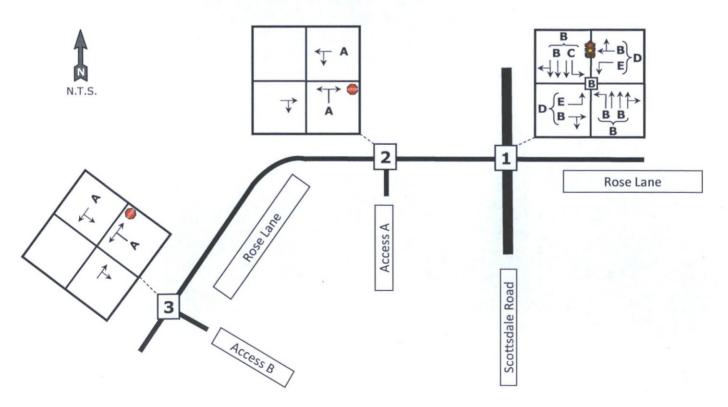


Figure 24: 2018 with Site Levels-of-Service - PM Peak Hour

Turn Lane Analysis

The current edition of the *City of Scottsdale Design Standards & Policies Manual* contains criteria regarding the need for deceleration lanes. Per the manual, the following criteria are provided:

"Deceleration lanes are required at all new driveways on major arterials and at new commercial/retail driveways on minor arterials. Deceleration lanes for driveways may also be required on collector streets and for non-commercial/retail driveways on minor arterials. The lane length should be based on the distance needed to allow the vehicle to exit the through lane and slow to a 15 mph travel speed. To determine the need for a deceleration lane on streets classified as a minor arterial or collector, see the following criteria:

- At least 5,000 vehicles per day are expected to use the street;
- The 85th percentile traffic speed on the street is at least 35 mph; or 45 mph for a 2 lane (1 lane each direction) roadway;
- At least 30 vehicles will make right turns into the driveway during a 1-hour period."

It was determined that a right-turn deceleration lane is not warranted at any of the site access intersections as neither access meets the above criteria. Additionally, right-turn lanes would have been included at intersections where necessary to provide level-of-service "D" or better. There were no circumstances where this criterion was satisfied.

Synchro also calculates the 95th percentile queue lengths. **Table 7** provides the maximum 95th percentile queue lengths for left-turn and right-turn lanes for the ambient 2018 and 2018 with proposed site traffic conditions during the weekday peak morning and evening hours.

	EXISTING	AMBIEI	NT 2018	2018 W	ITH SITE
	TURN-LANE	AM	PM	AM	PM
MOVEMENT	STORAGE	PEAK	PEAK	PEAK	PEAK
	1 - SCOTTSDALE	ROAD and F	ROSE LANE		
NORTHBOUND					
Northbound Left	165'	6'	16'	12'	24'
SOUTHBOUND					
Southbound Left	170'	15'	62'	18'	63'
EASTBOUND					
Eastbound Right (Left)	50'	0'	0'	(70')	(71')
WESTBOUND					
Westbound Right (Left)	35'	0'	46'	(30')	(100')

Table 7: 95th Percentile Queue Length Calculations

The calculated 95th percentile queue lengths generally lie within the turn-lane storage length available where turn lanes already exist. Some excessive queuing is anticipated for the eastbound and westbound turn lanes at the Scottsdale Road / Rose Lane intersection during ambient 2018 and 2018 with proposed site traffic conditions. This condition is primarily due to the minimal turn lane storage length provided or available on the Rose Lane approaches. It was observed that the excess queue did not impede overall intersection operation.

It was also noted that the existing eastbound Rose Lane approach at its intersection with Scottsdale Road does currently provide a dedicated through / left-turn lane and dedicated right-turn lane. However, due to the poor condition of the striping this separation may be difficult for drivers to discern and may contribute to instances of excess queuing. It is recommended to refresh the striping to maintain adequate separation of turn movements.

Collision Analysis

Collision experience from 2013 through 2015 was provided by the City of Scottsdale for the intersection of Scottsdale Road / Rose Lane and for the Scottsdale Road segment immediately north and south of Rose Lane. A copy of the data is provided as **Appendix G**.

At the Scottsdale Road / Rose Lane intersection there were a total of 12 collisions from 2013 to 2015. There were a total of 4 sideswipe (same direction) collisions, 3 rear-end collisions, 3 left-turn collisions, 1 angle collision, and 1 head-on collision. There were no fatal collisions and 1 incapacitating injury collision. All collisions, with one exception, involved vehicles traveling northbound and / or southbound on Scottsdale Road. The one exception involved a vehicle traveling westbound on Rose Lane. The Year 2015 contained the most reported collisions with a total of 6 collisions. There were not a significant number of crashes at this intersection nor was there a discernable pattern in the collision manner or direction of travel.

For the Scottsdale Road segment north and south of Rose Lane there were a total of 9 collisions from 2013 to 2015. There were 7 rear-end collisions, and 2 sideswipe (same direction) collisions. There were no fatal collisions and 2 incapacitating injury collisions, one of which involved alcohol. There were not a significant number of crashes on this road segment nor was there a discernable pattern in the collision manner or direction of travel.

Recommendations without Proposed Development

The existing Scottsdale Road / Rose Lane intersection is operating at a level-of-service "B" during both peak hours with some individual movements operating at level-of-service "D" or "E". All instances of level-of-service "D" or "E" occurred on Rose Lane. These levels-of-service are anticipated to continue for ambient 2018 traffic conditions with minor additional delay.

It is also recommended to provide new lane striping on the eastbound Rose Lane approach at its intersection with Scottsdale Road to improve visibility of lane separation.

Recommendations with Proposed Development

All intersections are anticipated to operate at a level-of-service "B" or better under the 2018 with proposed site traffic conditions. The Scottsdale Road / Rose Lane intersection is anticipated to continue to have some individual movements operating at level-of-service "D" or "E". All instances of level-of-service "D" or "E" occurred on Rose Lane.

It is recommended to implement a revised lane configuration on the eastbound and westbound Rose Lane approaches consisting of separate left-turn and shared through / right-turn lanes.

No significant change in intersection level-of-service is anticipated with the addition of the proposed site traffic.

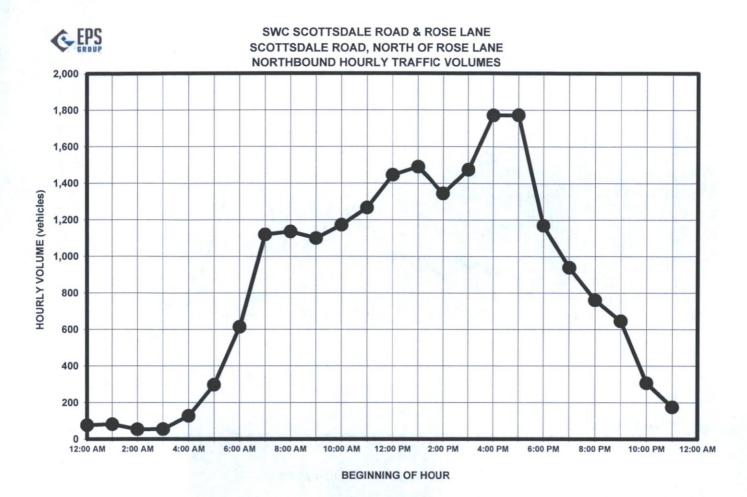
No additional turn lanes are warranted or recommended.

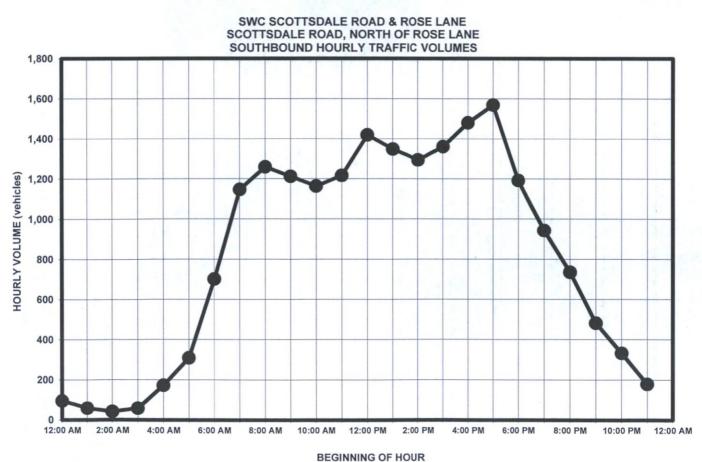
APPENDIX A
EXISTING TRAFFIC COUNTS

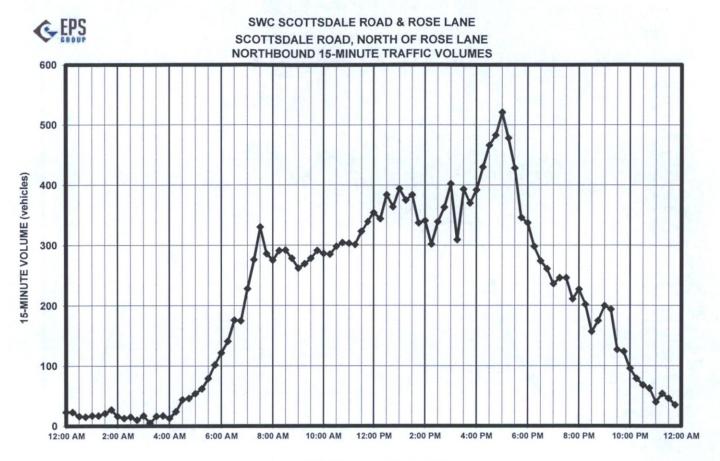


APPENDIX A.1
APPROACH AND DEPARTURE

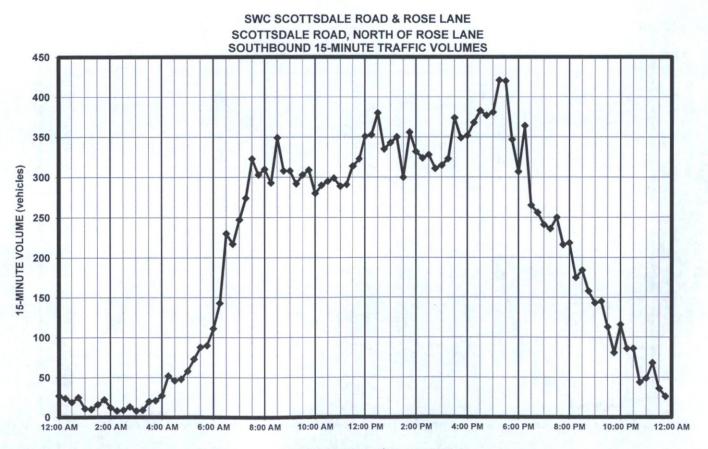












BEGINNING OF 15-MINUTE PERIOD

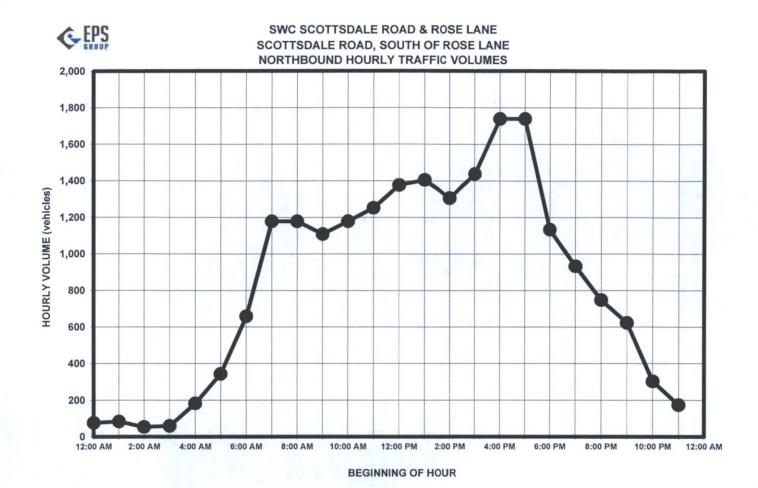
SWC SCOTTSDALE ROAD & ROSE LANE SCOTTSDALE ROAD, NORTH OF ROSE LANE APPROACH AND DEPARTURE

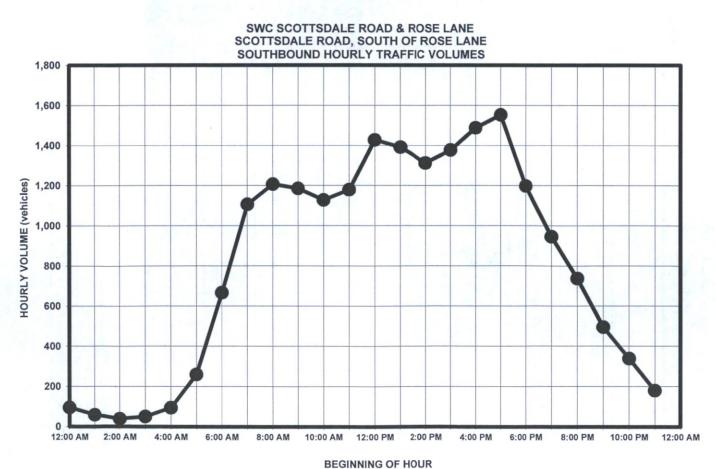
BEGIN	NORTI	HBOUND	SOUT	HBOUND I	I в	ОТН
PERIOD	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES
12:00 AM	23	77	27	95	50	172
12:15 AM	23	71	24	79	47	150
12:30 AM	16	65	19	65	35	130
12:45 AM	15	70	25	62	40	132
1:00 AM	17	82	11	59	28	141
1:15 AM	17	81	10	60	27	141
1:30 AM	21	77	16	58	37	135
1:45 AM	27	71	22	51	49	122
2:00 AM	16	54	12	42	28	96
2:15 AM	13	55	8	38	21	93
2:30 AM	15	47	9	39	24	86
2:45 AM	10	48	13	50	23	98
3:00 AM	17	55	8	58	25	113
3:15 AM	5	51	9	77	14	128
3:30 AM	16	70	20	120	36	190
3:45 AM	17	98	21	146	38	244
4:00 AM	13	127	27	173	40	300
4:15 AM	24	168	52	204	76	372
4:30 AM	44	206	46	225	90	431
4:45 AM	46	241	48	267	94	508
5:00 AM	54	297	58	309	112	606
5:15 AM	62	365	73	362	135	727
5:30 AM	79	444	88	432	167	876
5:45 AM	102	541	90	574	192	1,115
6:00 AM	122	614	111	701	233	1,315
6:15 AM	141	720	143	837	284	1,557
6:30 AM	176	855	230	968	406	1,823
6:45 AM	175	1,009	217	1,061	392	2,070
7:00 AM	228	1,120	247	1,147	475	2,267
7:15 AM	276	1,167	274	1,210	550	2,377
7:30 AM	330	1,182	323	1,229	653	2,411
7:45 AM	286	1,144	303	1,255	589	2,399
8:00 AM	275	1,136	310	1,260	585	2,396
8:15 AM	291	1,123	293	1,258	584	2,381
8:30 AM	292	1,101	349	1,257	641	2,358
8:45 AM	278	1,087	308	1,211	586	2,298
9:00 AM	262	1,100	308	1,212	570	2,312
9:15 AM	269	1,124	292	1,184	561	2,308
9:30 AM	278	1,140	303	1,182	581	2,322
9:45 AM	291	1,160	309	1,174	600	2,334
10:00 AM	286	1,173	280	1,164	566	2,337
10:15 AM	285	1,190	290	1,173	575	2,363
10:30 AM	298	1,206	295	1,174	593	2,380
10:45 AM	304	1,231	299	1,193	603	2,424
11:00 AM	303	1,266	289	1,217	592	2,483
11:15 AM	301	1,317	291	1,279	592	2,596
11:30 AM	323	1,360	314	1,341	637	2,701
11:45 AM	339	1,421	323	1,407	662	2,828
MAXIMUM	384	1,421	380	1,407	764	2,828
PHF and TIME	0.93	1,421 11:45 AM	0.93	11:45 AM	0.93	11:45 AM
TTII AIIU TIIVIL	0.33	TT.45 AIVI	0.93	11.40 AIVI	0.33	11.40 AW

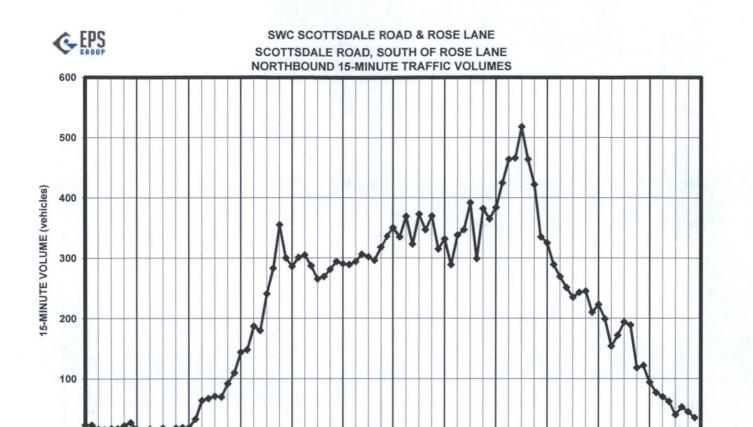


SWC SCOTTSDALE ROAD & ROSE LANE SCOTTSDALE ROAD, NORTH OF ROSE LANE APPROACH AND DEPARTURE

BEGIN	NORTH	BOUND	SOUTH	BOUND	BC	TH
PERIOD	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES
12:00 PM	354	1,446	351	1,419	705	2,865
12:15 PM	344	1,486	353	1,411	697	2,897
12:30 PM	384	1,517	380	1,408	764	2,925
12:45 PM	364	1,517	335	1,328	699	2,845
1:00 PM	394	1,490	343	1,349	737	2,839
1:15 PM	375	1,437	350	1,338	725	2,775
1:30 PM	384	1,364	300	1,312	684	2,676
1:45 PM	337	1,319	356	1,340	693	2,659
2:00 PM	341	1,345	332	1,295	673	2,640
2:15 PM	302	1,406	324	1,278	626	2,684
2:30 PM	339	1,413	328	1,277	667	2,690
2:45 PM	363	1,467	311	1,323	674	2,790
3:00 PM	402	1,474	315	1,361	717	2,835
3:15 PM	309	1,464	323	1,398	632	2,862
3:30 PM	393	1,585	374	1,443	767	3,028
3:45 PM	370	1,658	349	1,452	719	3,110
4:00 PM	392	1,771	352	1,480	744	3,251
4:15 PM	430	1,900	368	1,509	798	3,409
4:30 PM	466	1,948	383	1,562	849	3,510
4:45 PM	483	1,910	377	1,599	860	3,509
5:00 PM	521	1,773	381	1,569	902	3,342
5:15 PM	478	1,589	421	1,495	899	3,084
5:30 PM	428	1,409	420	1,438	848	2,847
5:45 PM	346	1,255	347	1,283	693	2,538
6:00 PM	337	1,170	307	1,192	644	2,362
6:15 PM	298	1,069	364	1,126	662	2,195
6:30 PM	274	1,017	265	998	539	2,015
6:45 PM	261	989	256	983	517	1,972
7:00 PM	236	939	241	943	477	1,882
7:15 PM	246	930	236	920	482	1,850
7:30 PM	246	886	250	859	496	1,745
7:45 PM	211	797	216	793	427	1,590
8:00 PM	227	761	218	735	445	1,496
8:15 PM	202	734	175	660	377	1,394
8:30 PM	157	726	184	630	341	1,356
8:45 PM	175	696	158	559	333	1,255
9:00 PM	200	645	143	482	343	1,127
9:15 PM	194	541	145	455	339	996
9:30 PM	127	426	113	396	240	822
9:45 PM	124	367	81	369	205	736
10:00 PM	96	306	116	332	212	638
10:15 PM	79	250	86	265	165	515
10:30 PM	68	225	86	247	154	472
10:45 PM	63	203	44	197	107	400
11:00 PM	40	175	49	179	89	354
11:15 PM	54	-	68	-	122	- 004
11:30 PM	46		36		82	
11:45 PM	35	-	26	The second second	61	
		-				-
MAXIMUM DUE and TIME	521	1,948	421	1,599 4:45 PM	902	3,510
PHF and TIME	0.93	4:30 PM	0.95	4:45 PW	0.97	4:30 PM
		NORTHBOUND		SOUTHBOUND		вотн
DAILY TOTAL	VOLUME	20,396		19,773		40,169







BEGINNING OF 15-MINUTE PERIOD

12:00 PM

2:00 PM

4:00 PM

6:00 PM

8:00 PM

10:00 PM

12:00 AM

12:00 AM

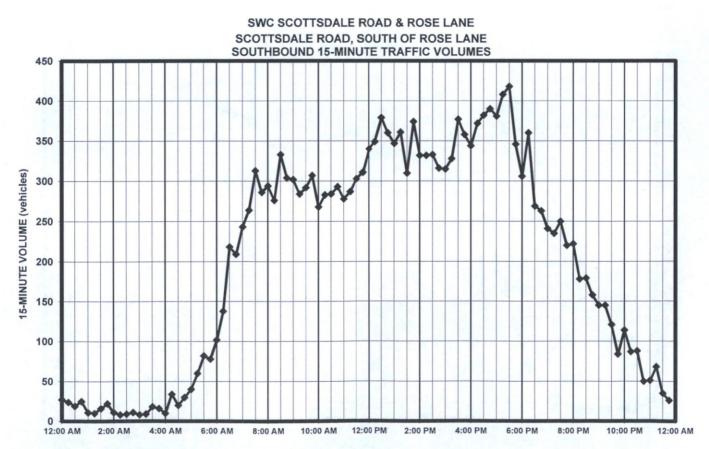
2:00 AM

4:00 AM

6:00 AM

8:00 AM

10:00 AM



BEGINNING OF 15-MINUTE PERIOD

SWC SCOTTSDALE ROAD & ROSE LANE SCOTTSDALE ROAD, SOUTH OF ROSE LANE APPROACH AND DEPARTURE

BEGIN	NORTH	HBOUND	SOUTH	BOUND	ВС	OTH													
PERIOD	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES													
12:00 AM	23	77	27	95	50	172													
12:15 AM	23	71	24	79	47	150													
12:30 AM	16	65	19	65	35	130													
12:45 AM	15	71	25	62	40	133													
1:00 AM	17	83	11	59	28	142													
1:15 AM	17	82	10	59	27	141													
1:30 AM	22	78	16	57	38	135													
1:45 AM	27	72	22	50	49	122													
2:00 AM	16	54	11	39	27	93													
2:15 AM	13	56	8	36	21	92													
2:30 AM	16	48	9	37	25	85													
2:45 AM	9	50	11	46	20	96													
3:00 AM	18	60	8	51	26	111													
3:15 AM	5	61	9	53	14	114													
3:30 AM	18	89	18	78	36	167													
3:45 AM	19	135	16	80	35	215													
4:00 AM	19	183	10	94	29	277													
4:15 AM		235 34 124 67				235 34 124 67				3 235 34 124 67		33 235 34 124 67		34 124 67		359			
4:30 AM	64	272 20 150 84				422													
4:45 AM	67					300 30 212 97						300 30 212 97					30 212 97		512
5:00 AM	71	343	40		111	603													
5:15 AM	70	416	60	322	130	738													
5:30 AM	92	494	82	400	174	894													
5:45 AM	110	589	78	536	188	1,125													
6:00 AM	144	659	102	667	246	1,326													
6:15 AM	148	756	138	808	286	1,564													
6:30 AM	187	891	218		405	1,825													
6:45 AM	180	1,059	209	1,029	389	2,088													
7:00 AM	241	1,179	243	1,106	484	2,285													
7:15 AM	283	1,224	264	1,157	547	2,381													
7:30 AM	355	1,242	313	1,169	668	2,411													
7:45 AM	300	1,192	286	1,189	586	2,381													
8:00 AM	286	1,179	294	1,207	580	2,386													
8:15 AM	301	1,158	276	1,215	577	2,373													
8:30 AM	305	1,126	333	1,223	638	2,349													
8:45 AM	287	1,102	304	1,182	591	2,284													
9:00 AM	265	1,109	302	1,185	567	2,294													
9:15 AM	269	1,134	284	1,151	553	2,285													
9:30 AM	281	1,154	292	1,150	573	2,304													
9:45 AM	294	1,167	307	1,142	601	2,309													
10:00 AM	290	1,179	268	1,128	558														
10:15 AM	289	1,191	283	1,138	572	2,307 2,329													
10:30 AM	294		284	1,142	578														
10:45 AM	306	1,198 1,222	293	1,161	599	2,340 2,383													
	302				580														
11:00 AM 11:15 AM		1,252	278	1,179	583	2,431													
11:30 AM	296	1,300	287	1,241	621	2,541													
11:45 AM	318 336	1,339	303	1,303 1,379	647	2,642													
	330	1,390	311	1,378	047	2,769													
MAXIMUM	369	1,390	379	1,379	748	2,769													
PHF and TIME	0.94	11:45 AM	0.91	11:45 AM	0.93	11:45 AM													

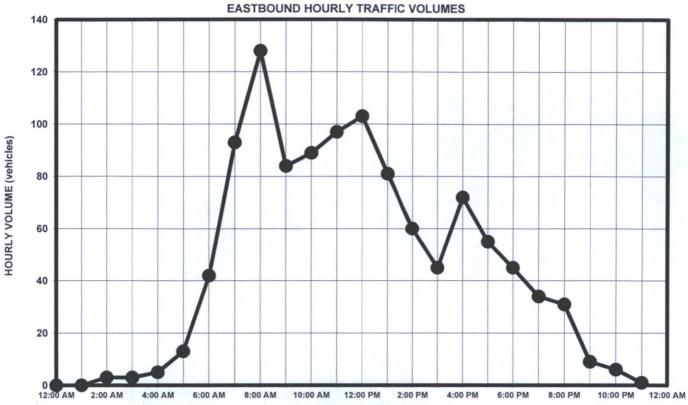


SWC SCOTTSDALE ROAD & ROSE LANE SCOTTSDALE ROAD, SOUTH OF ROSE LANE APPROACH AND DEPARTURE

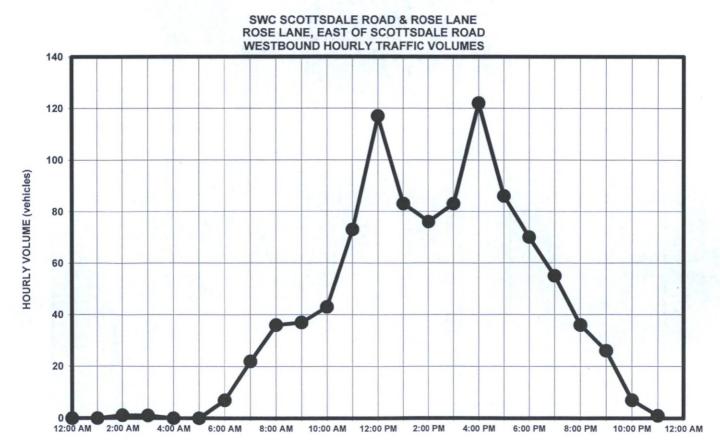
BEGIN	NORTH	IBOUND	SOUTH	HBOUND	BC	TH
PERIOD	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES
12:00 PM	350	1,377	340	1,428	690	2,805
12:15 PM	335	1,400	349	1,435	684	2,835
12:30 PM	369	1,412	379	1,447	748	2,859
12:45 PM	323	1,413	360	1,378	683	2,791
1:00 PM	373	1,405	347	1,392	720	2,797
1:15 PM	347	1,364	361	1,377	708	2,741
1:30 PM	370	1,306	310	1,348	680	2,654
1:45 PM	315	1,274	374	1,371	689	2,645
2:00 PM	332	1,306	332	1,313	664	2,619
2:15 PM	289	1,366	332	1,296	621	2,662
2:30 PM	338	1,376	333	1,292	671	2,668
2:45 PM	347	1,420	316	1,336	663	2,756
3:00 PM	392	1,438	315	1,378	707	2,816
3:15 PM	299	1,430	328	1,407	627	2,837
3:30 PM	382	1,556	377	1,451	759	3,007
3:45 PM	365	1,638	358	1,456	723	3,094
4:00 PM	384	1,739	344	1,488	728	3,227
4:15 PM	425	1,873	372	1,525	797	3,398
4:30 PM	464	1,912	382	1,561	846	3,473
4:45 PM	466	1,870	390	1,597	856	3,467
5:00 PM	518	1,739	381	1,553	899	3,292
5:15 PM	464	1,546	408	1,478	872	3,024
5:30 PM	422	1,371	418	1,430	840	2,801
5:45 PM	335	1,218	346	1,281	681	2,499
6:00 PM	325	1,134	306	1,198	631	2,332
6:15 PM	289	1,044	360	1,133	649	2,177
6:30 PM	269	998	269	1,008	538	2,006
6:45 PM	251	974	263	989	514	1,963
7:00 PM	235	933	241	946	476	1,879
7:15 PM	243	921	235	927	478	1,848
7:30 PM	245	877	250	870	495	1,747
7:45 PM	210	786	220	799	430	1,747
	223	748	222	737	445	
8:00 PM		719	178	660	377	1,485 1,379
8:15 PM	199		179	627	333	
8:30 PM	154	709				1,336
8:45 PM	172	673	158	569	330	1,242
9:00 PM	194	623	145	495	339	1,118
9:15 PM	189	523	145	464	334	987
9:30 PM	118	411	121	406	239	817
9:45 PM	122	363	84	373	206	736
10:00 PM	94	303	114	339	208	642
10:15 PM	77	249	87	276	164	525
10:30 PM	70	225	88	257	158	482
10:45 PM	62	200	50	204	112	404
11:00 PM	40	173	51	180	91	353
11:15 PM	53	-	68	-	121	-
11:30 PM	45	-	35	Parket - The second	80	1 1/2 -
11:45 PM	35	-	26	-	61	-
MAXIMUM	518	1,912	418	1,597	899	3,473
PHF and TIME	0.92	4:30 PM	0.96	4:45 PM	0.97	4:30 PM
		NORTHBOUND		SOUTHBOUND		вотн
				· · · · · · · · · · · · · · · · · · ·		



SWC SCOTTSDALE ROAD & ROSE LANE ROSE LANE, EAST OF SCOTTSDALE ROAD



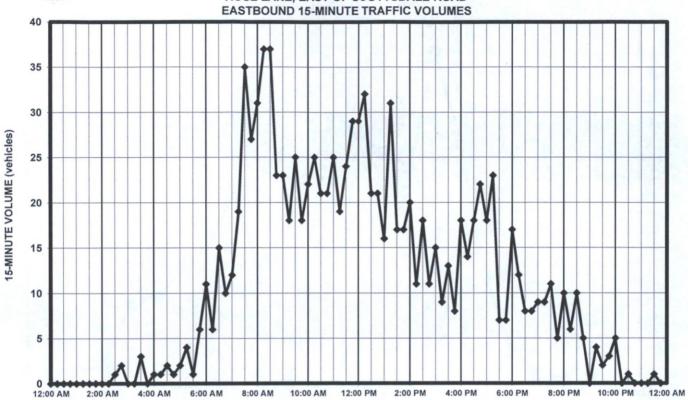
BEGINNING OF HOUR



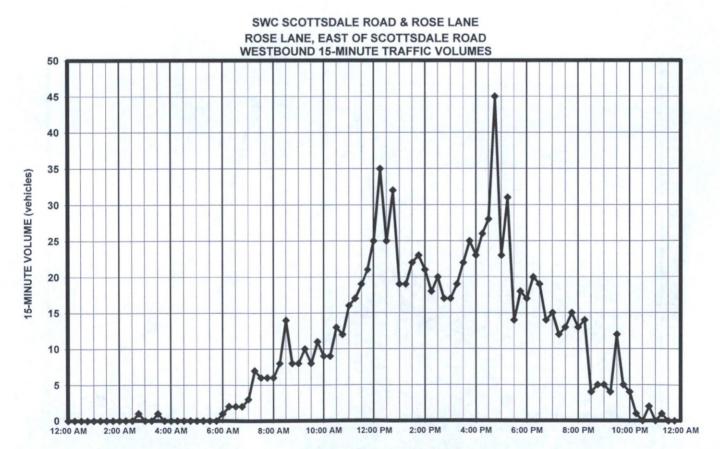
BEGINNING OF HOUR



SWC SCOTTSDALE ROAD & ROSE LANE ROSE LANE, EAST OF SCOTTSDALE ROAD



BEGINNING OF 15-MINUTE PERIOD



BEGINNING OF 15-MINUTE PERIOD

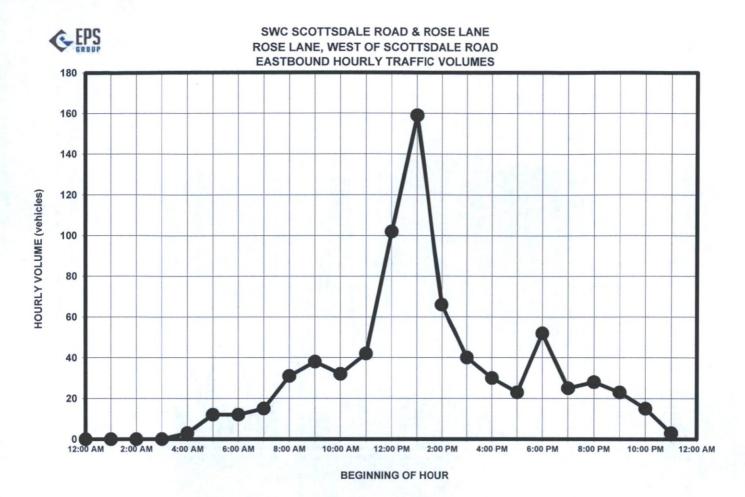
SWC SCOTTSDALE ROAD & ROSE LANE ROSE LANE, EAST OF SCOTTSDALE ROAD APPROACH AND DEPARTURE

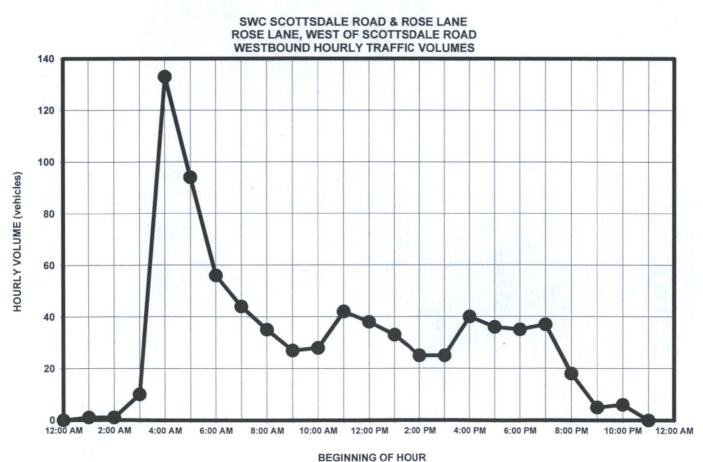
BEGIN	EASTB		I WEST	BOUND	В	ОТН
PERIOD	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES
12:00 AM	0	0	0	0	0	0
12:15 AM	0	0	0	0	0	0
12:30 AM	0	0	0	0	0	0
12:45 AM	0	0	0	0	0	0
1:00 AM	0	0	0	0	0	0
1:15 AM	0	0	0	0	0	0
1:30 AM	0	0	0	0	0	0
1:45 AM	0	1	0	0	0	1
2:00 AM	0	3	0	1	0	4
2:15 AM	0	3	0	1	0	4
2:30 AM	1	3	0	1	1	4
2:45 AM	2	5	1	2	3	7
3:00 AM	0	3	0	1	0	4
3:15 AM	0	4	0	1	0	5
3:30 AM	3	5	1	1	4	6
3:45 AM	0	4	0	0	0	4
4:00 AM	1	5	0	0	1	5
4:15 AM	1	6	0	0	1	6
4:30 AM	2	9	0	0	2	9
4:45 AM	1	8	0	0	1	8
5:00 AM	2	13	0	0	2	13
5:15 AM	4	22	0	1	4	23
5:30 AM	1	24	0	3	1	27
	6	38	0	5	6	
5:45 AM	11	42	1	7	12	43
6:00 AM	6	43	2	9	8	49
6:15 AM	15	56	2	14	17	52
6:30 AM						70
6:45 AM	10 12	76	2	18	12	94
7:00 AM		93	7	22	15	115
7:15 AM	19	112		25	26	137
7:30 AM	35	130	6	26	41	156
7:45 AM	27	132	6	34	33	166
8:00 AM	31	128	6	36	37	164
8:15 AM	37	120	8	38	45	158
8:30 AM	37	101	14	40	51	141
8:45 AM	23	89	8	34	31	123
9:00 AM	23	84		37	31	121
9:15 AM	18	83	10	38	28	121
9:30 AM	25	90	8	37	33	127
9:45 AM	18	86	11	42	29	128
10:00 AM	22	89	9	43	31	132
10:15 AM	25	92	9	50	34	142
10:30 AM	21	86	13	58	34	144
10:45 AM	21	89	12	64	33	153
11:00 AM	25	97	16	73	41	170
11:15 AM	19	101	17	82	36	183
11:30 AM	24	114	19	100	43	214
11:45 AM	29	111	21	106	50	217
MAXIMUM	37	132	35	106	67	217
PHF and TIME	0.89	7:45 AM	0.76	11:45 AM	0.81	11:45 AM



SWC SCOTTSDALE ROAD & ROSE LANE ROSE LANE, EAST OF SCOTTSDALE ROAD APPROACH AND DEPARTURE

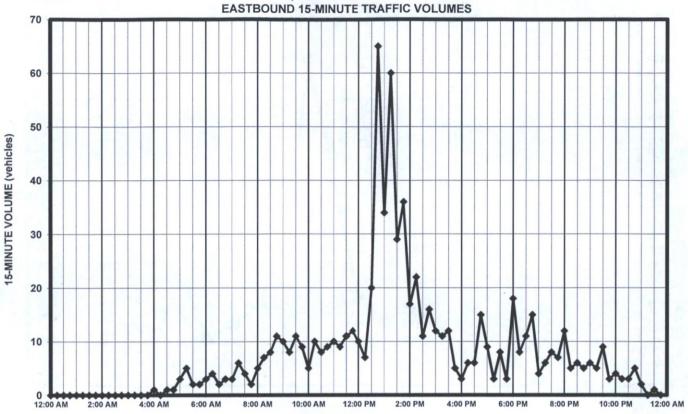
BEGIN	EASTE	BOUND	WEST	BOUND	BC	TH
PERIOD	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES
12:00 PM	29	103	25	117	54	220
12:15 PM	32	90	35	111	67	201
12:30 PM	21	89	25	95	46	184
12:45 PM	21	85	32	92	53	177
1:00 PM	16	81	19	83	35	164
1:15 PM	31	85	19	85	50	170
1:30 PM	17	65	22	84	39	149
1:45 PM	17	66	23	82	40	148
2:00 PM	20	60	21	76	41	136
2:15 PM	11	55	18	72	29	127
2:30 PM	18	53	20	73	38	126
2:45 PM	11	48	17	75	28	123
3:00 PM	15	45	17	83	32	128
3:15 PM	9	48	19	89	28	137
3:30 PM	13	53	22	96	35	149
3:45 PM	8	58	25	102	33	160
4:00 PM	18	72	23	122	41	194
4:15 PM	14	72	26	122	40	194
4:30 PM	18	81	28	127	46	208
4:45 PM	22	70	45	113	67	183
5:00 PM	18	55	23	86	41	141
5:15 PM	23	54	31	80	54	134
5:30 PM	7	43	14	69	21	112
5:45 PM	7	44	18	74	25	118
6:00 PM	17	45	17	70	34	115
6:15 PM	12	37	20	68	32	105
6:30 PM	8	34	19	60	27	94
6:45 PM	8	37	14	54	22	91
7:00 PM	9	34	15	55	24	89
7:15 PM	9	35	12	53	21	88
7:30 PM	11	32	13	55	24	87
7:45 PM	5	31	15	46	20	77
8:00 PM	10	31	13	36	23	67
8:15 PM	6	21	14	28	20	49
8:30 PM	10	19	4	18	14	37
8:45 PM	5	11	5	26	10	37
9:00 PM	0	9	5	26	5	35
9:15 PM	4	14	4	25	8	39
9:30 PM	2	10	12	22	14	32
9:45 PM	3	9	5	10	8	19
10:00 PM	5	6	4	7	9	13
10:15 PM	0	1	1	3	1	4
10:30 PM	1	1	0	3	1	4
10:45 PM	0	1	2	3	2	4
11:00 PM	0	1	0	1	0	2
11:15 PM	0	-	1	- 4	1	-
11:30 PM	1	_	0		1	-
11:45 PM	0	-	0	S115 - 38 15	0	-
MAXIMUM	32	103	45	127	67	220
PHF and TIME	0.80	12:00 PM	0.71	4:30 PM	0.82	12:00 PM
		EASTBOUND	MARKET WILLIAM	WESTBOUND	217,75	вотн
DAILY TOTAL	VOLUME			982		
DAILY TOTAL	VOLUME	1,099		302		2,081



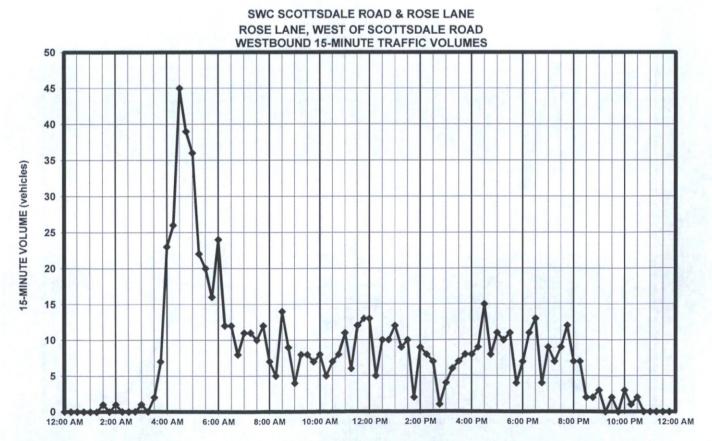




SWC SCOTTSDALE ROAD & ROSE LANE ROSE LANE, WEST OF SCOTTSDALE ROAD EASTROLING AS MINUTE TRAFFIC VOLUMES



BEGINNING OF 15-MINUTE PERIOD



BEGINNING OF 15-MINUTE PERIOD

SWC SCOTTSDALE ROAD & ROSE LANE ROSE LANE, WEST OF SCOTTSDALE ROAD APPROACH AND DEPARTURE

BEGIN	l FAST	BOUND	WEST	BOUND	I в	ОТН
PERIOD	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES
12:00 AM	0	0	0	0	0	0
12:15 AM	0	0	0	0	0	0
12:30 AM	0	0	0	0	0	0
12:45 AM	0	0	0	1	0	1
1:00 AM	0	0	0	1	0	1
1:15 AM	0	0	0	2	0	2
1:30 AM	0	0	1	2	1	2
1:45 AM	0	0	0	1	0	1
2:00 AM	0	0	1	1	1	1
2:15 AM	0	0	0	1	0	1
2:30 AM	0	0	0	1	0	1
2:45 AM	0	0	0	3	0	3
	0	0	1	10	1	10
3:00 AM				32	0	
3:15 AM	0	1	2			33
3:30 AM	0	1		58	7	59
3:45 AM	0	2	7	101		103
4:00 AM	1	3	23	133	24	136
4:15 AM	0	5	26	146	26	151
4:30 AM	1	10	45	142	46	152
4:45 AM	1	11	39	117	40	128
5:00 AM	3	12	36	94	39	106
5:15 AM	5	12	22	82	27	94
5:30 AM	2	11	20	72	22	83
5:45 AM	2	11	16	64	18	75
6:00 AM	3	12	24	56	27	68
6:15 AM	4	12	12	43	16	55
6:30 AM	2	14	12	42	14	56
6:45 AM	3	16	8	40	11	56
7:00 AM	3	15	11	44	14	59
7:15 AM	6	17	11	40	17	57
7:30 AM	4	18	10	34	14	52
7:45 AM	2	22	12	38	14	60
8:00 AM	5	31	7	35	12	66
8:15 AM	7	36	5	32	12	68
8:30 AM	8	37	14	35	22	72
8:45 AM	11	40	9	29	20	69
9:00 AM	10	38	4	27	14	. 65
9:15 AM	8	33	8	31	16	64
9:30 AM	11	35	8	28	19	63
9:45 AM	9	32	7	27	16	59
10:00 AM	5	32	8	28	13	60
10:15 AM	10	37	5	31	15	68
10:30 AM	8	36	7	32	15	68
10:45 AM	9	39	8	37	17	76
11:00 AM	10	42	11	42	21	84
11:15 AM	9	42	6	44	15	86
11:30 AM	11	40	12	43	23	83
11:45 AM	12	49	13	41	25	90
MAXIMUM	20	49	45	146	46	152
PHF and TIME	0.61	11:45 AM	0.81	4:15 AM	0.83	4:30 AM
THE WAY THE	0.01	11.40 AW	0.01	7. 10 AW	0.00	7.50 AW



SWC SCOTTSDALE ROAD & ROSE LANE ROSE LANE, WEST OF SCOTTSDALE ROAD APPROACH AND DEPARTURE

BEGIN	EASTE	BOUND	WEST	BOUND	BC	OTH
PERIOD	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES	15 MINUTES	60 MINUTES
12:00 PM	10	102	13	38	23	140
12:15 PM	7	126	5	37	12	163
12:30 PM	20	179	10	41	30	220
12:45 PM	65	188	10	41	75	229
1:00 PM	34	159	12	33	46	192
1:15 PM	60	142	9	30	69	172
1:30 PM	29	104	10	29	39	133
1:45 PM	36	86	2	26	38	112
2:00 PM	17	66	9	25	26	91
2:15 PM	22	61	8	20	30	81
2:30 PM	11	50	7	18	18	68
2:45 PM	16	51	1	18	17	69
3:00 PM	12	40	4	25	16	65
3:15 PM	11	31	6	29	17	60
3:30 PM	12	26	7	32	19	58
3:45 PM	5	20	8	40	13	60
4:00 PM	3	30	8	40	11	70
4:15 PM	6	36	9	43	15	79
4:30 PM	6	33	15	44	21	77
4:45 PM	15	35	8	40	23	75
5:00 PM	9	23	11	36	20	59
5:15 PM	3	32	10	32	13	64
5:30 PM	8	37	11	33	19	70
5:45 PM	3	40	4	35	7	75
6:00 PM	18	52	7	35	25	87
6:15 PM	8	38	11	37	19	75
6:30 PM	11	36	13	33	24	69
6:45 PM	15	33	4	29	19	62
7:00 PM	4	25	9	37	13	62
7:15 PM	6	33	7	35	13	68
7:30 PM	8	32	9	35	17	67
	7	30	12	28	19	58
7:45 PM	12	28	7	18	19	46
8:00 PM 8:15 PM	5	22	7	14	12	36
	6	22	2	7	8	29
8:30 PM 8:45 PM	5	25	2	7	7	32
			3	5	9	28
9:00 PM	6	23 21	0	5	5	26
9:15 PM	5		2	6	11	25
9:30 PM	9	19	0	6	3	19
9:45 PM	3	13	3		7	21
10:00 PM	4	15		6		
10:15 PM	3	13	2	3 2	5	16 12
10:30 PM	3	10				
10:45 PM	5	8	0	0	5	8
11:00 PM	2	3	0	0	2	3
11:15 PM	0	-	0	STATE OF THE STATE	0	- ATT -
11:30 PM	1	-	0		1	
11:45 PM	0	-	0	-	0	Stickt-
MAXIMUM	65	188	15	44	75	229
PHF and TIME	0.72	12:45 PM	0.73	4:30 PM	0.76	12:45 PN
Tan Andrew		EASTBOUND	THE REAL PROPERTY.	WESTBOUND	a to the second	вотн
	VOLUME	751		769		1,520

APPENDIX A.2
TURNING MOVEMENTS





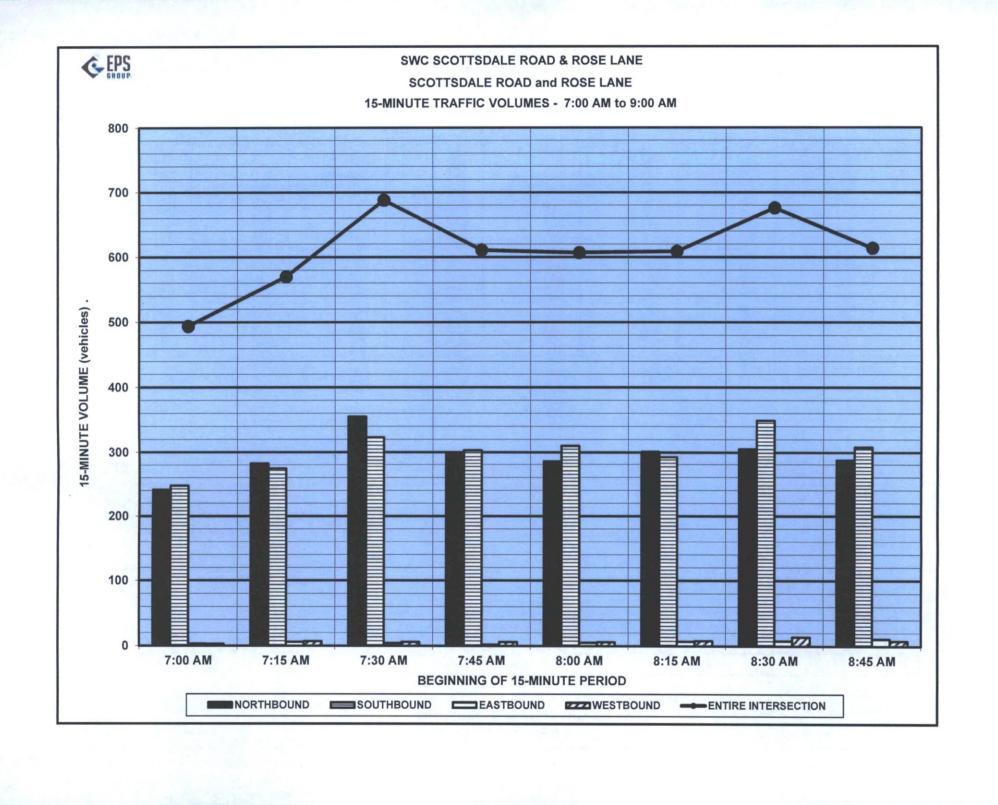
SWC SCOTTSDALE ROAD & ROSE LANE SCOTTSDALE ROAD and ROSE LANE

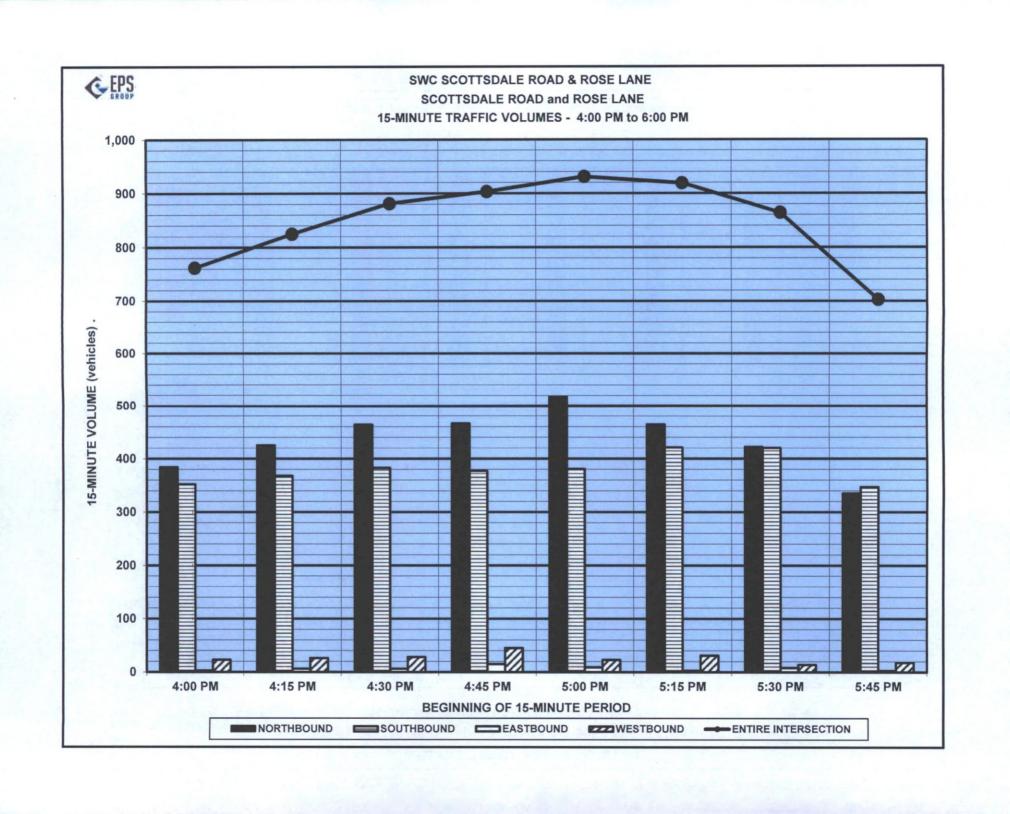
EXISTING 4-HOUR TURNING MOVEMENT COUNTS

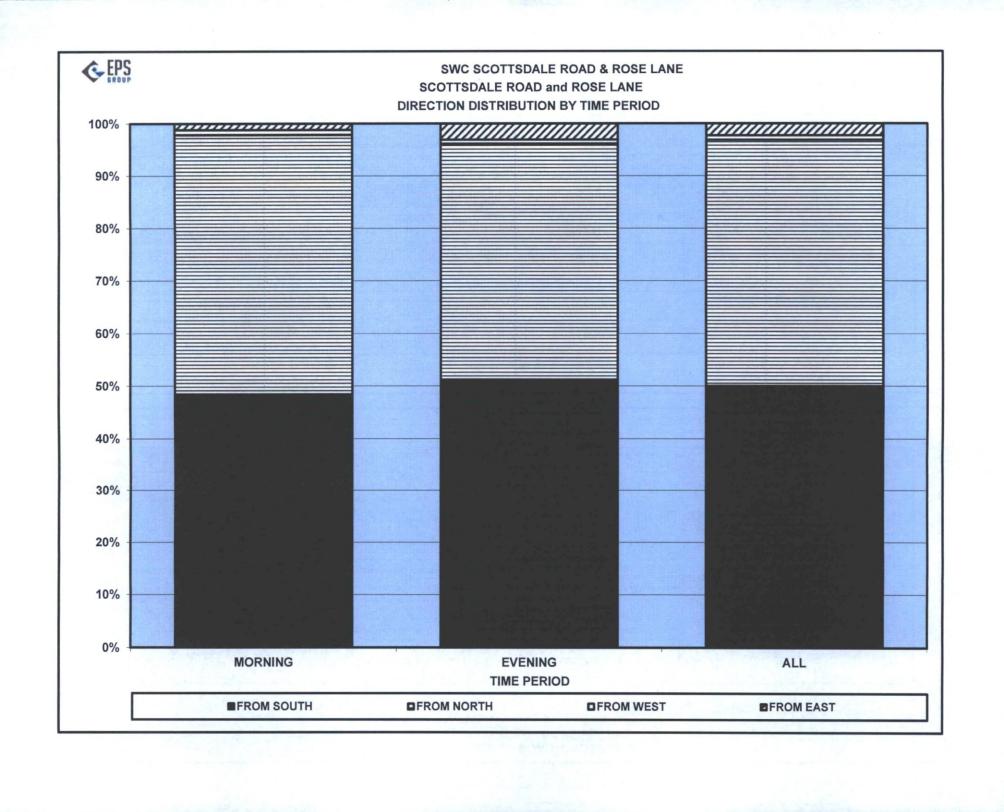
	SC	COTTSD	ALE RO	AD		ROSE	LANE		SC	OTTSD	ALE RO	AD		ROSE	LANE			60
BEGIN		FROM	NORTH			FROM	EAST			FROM	SOUTH			FROM	WEST		ALL	MIN.
TIME	LEFT	THRU	RIGHT	TOTAL	LEFT	THRU	RIGHT	TOTAL	LEFT	THRU	RIGHT	TOTAL	LEFT	THRU	RIGHT	TOTAL	TOTAL	TOTA
7:00 AM	5	239	3	247	1	0	2	3	8	226	7	241	0	0	3	3	494	2,363
7:15 AM	11	257	6	274	1	0	6	7	5	270	8	283	0	0	6	6	570	2,476
7:30 AM	11	308	4	323	1	0	5	6	6	325	24	355	0	0	4	4	688	2,515
7:45 AM	15	283	5	303	3	1	2	6	6	282	12	300	2	0	0	2	611	2,503
8:00 AM	19	289	2	310	4	1	1	6	4	271	11	286	3	1	1	5	607	2,506
8:15 AM	19	271	3	293	3	0	5	8	2	282	17	301	4	1	2	7	609	
8:30 AM	19	324	6	349	5	0	9	14	8	280	17	305	3	1	4	8	676	
8:45 AM	13	292	3	308	5	0	3	8	6	272	9	287	3	1	7	11	614	MAX
AM PEAK	64	1,151	14	1,229	11	2	13	26	18	1,160	64	1,242	9	2	7	18	2,515	2,515
PHF	0.84	0.93	0.70	0.95	0.69	0.50	0.65	0.81	0.75	0.89	0.67	0.87	0.56	0.50	0.44	0.64	0.91	
4:00 PM	14	335	3	352	7	0	16	23	5	375	4	384	1	0	2	3	762	3,371
4:15 PM	6	359	3	368	13	0	13	26	6	412	7	425	5	1	0	6	825	3,540
4:30 PM	12	367	4	383	11	0	17	28	11	447	6	464	2	0	4	6	881	3,634
4:45 PM	16	359	2	377	26	0	19	45	6	456	4	466	8	2	5	15	903	3,617
5:00 PM	16	364	1	381	13	0	10	23	10	506	2	518	5	0	4	9	931	3,417
5:15 PM	21	398	2	421	9	0	22	31	8	454	2	464	2	0	1	3	919	-
5:30 PM	7	411	2	420	5	0	9	14	9	413	0	422	6	0	2	8	864	-
5:45 PM	7	337	3	347	7	0	11	18	1	334	0	335	1	0	2	3	703	MAX
PM PEAK	65	1,488	9	1,562	59	0	68	127	35	1,863	14	1,912	17	2	14	33	3,634	3,634
PHF	0.77	0.93	0.56	0.93	0.57	0.00	0.77	0.71	0.80	0.92	0.58	0.92	0.53	0.25	0.70	0.55	0.98	

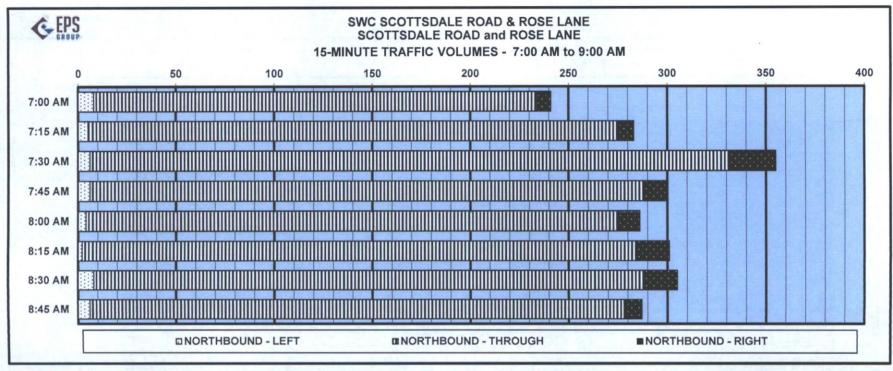
							Mark the second					100						
								TTSDAL										
								DALE R										
	SC	COTTSD	ALE RO	AD		ROSE	LANE		SC	OTTSD		AD	100		LANE			60
BEGIN		FROM I	NORTH			FROM	EAST			FROM	SOUTH				WEST		ALL	MIN.
TIME	LEFT	THRU	RIGHT	TOTAL	LEFT	THRU	RIGHT	TOTAL	LEFT	THRU	RIGHT	TOTAL	LEFT THRU RIGHT TOTAL				TOTAL	TOTA
						2000	A	PPROA	CH VOL	UMES								
7:00 AM	42	1,087	18	1,147	6	1	15	22	25	1,103	51	1,179	2	0	13	15		2,363
8:00 AM	70	1,176	14	1,260	17	1	18	36	20	1,105	54	1,179	13	4	14	31		2,506
4:00 PM	48	1,420	12	1,480	57	0	65	122	28	1,690	21	1,739	16	3	11	30		3,371
5:00 PM	51	1,510	8	1,569	34	0	52	86	28	1,707	4	1,739	14	0	9	23		3,417
							- Carlon											
AM TOTAL	112	2,263	32	2,407	23	2	33	58	45	2,208	105	2,358	15	4	27	46		4,869
AM %	5%	94%	1%	100%	40%	3%	57%	100%	2%	94%	4%	100%	33%	9%	59%	100%		
PM TOTAL	99	2,930	20	3,049	91	0	117	208	56	3,397	25	3,478	30	3	20	53		6,788
PM %	3%	96%	1%	100%	44%	0%	56%	100%	2%	98%	1%	100%	57%	6%	38%	100%		
ALL TOTAL	211	5,193	52	5,456	114	2	150	266	101	5,605	130	5,836	45	7	47	99		11,657
ALL %	4%	95%	1%	100%	43%	1%	56%	100%	2%	96%	2%	100%	45%	7%	47%	100%		
		100													• /			
AM TOTAL		49	, -				%				3%				%			100%
PM TOTAL		45					%				1%				%			100%
ALL TOTAL		47	%			2	%			50)%			1	%			100%
	1						D	EPARTL	IRF VOI	UMES		MAGNE						
	SC	COTTSD	ALFRO	OAD		ROSE	LANE	LIANTE	_	and the second second second	ALERO	AD		ROSE	LANE			60
1503		TON		,,,,,			EAST		SCOTTSDALE ROAD TO SOUTH						VEST		ALL	MIN.
	EB	NB	WB	1	SB	EB	NB		WB	SB	EB		NB	WB	SB			
TIME	LEFT			TOTAL	LEFT	a la constitución de la constitu	Mark was an arranged	TOTAL		THRU	The second second	TOTAL	LEFT	THRU	The second second	TOTAL	TOTAL	TOTAL
AM TOTAL	15	2.208	33	2.256	112	4	105	221	23	2.263	27	2,313	45	2	32	79	101712	4,869
AM %	1%	98%	1%	100%	51%	2%	48%	100%	1%	98%	1%	100%	57%	3%	41%	100%	7 7 7	1,000
PM TOTAL	30	3.397	117	3,544	99	3	25	127	91	2,930	20	3.041	56	0	20	76		6,788
PM %	1%	96%	3%	100%	78%	2%	20%	100%	3%	96%	1%	100%	74%	0%	26%	100%		0,700
ALL TOTAL	45	5,605	150	5,800	211	7	130	348	114	5,193	47	5,354	101	2	52	155		11,657
TOTAL %	1%	97%	3%	100%	61%	2%	37%	100%	2%	97%	1%	100%	65%	1%	34%	100%	1000	11,007
															100			
AM TOTAL		46	%				%			48	3%	W			%	50 - 1 L		100%
					2%				45%			1%					10001	
PM TOTAL	100	52 50	2%				%			45	%				%	3		100%

EPS GROUP

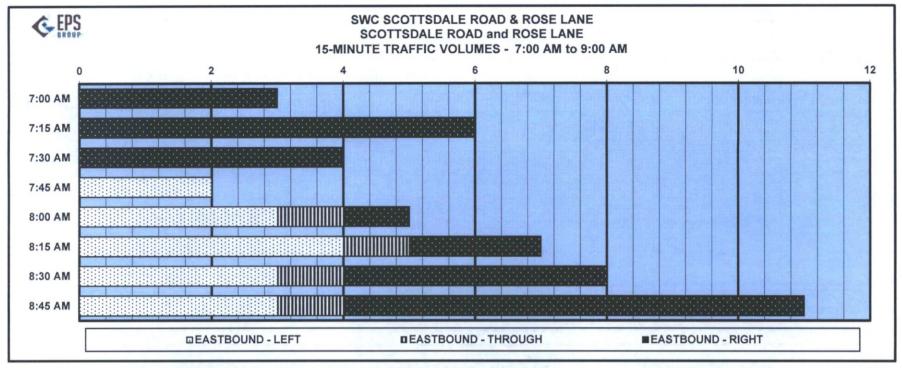


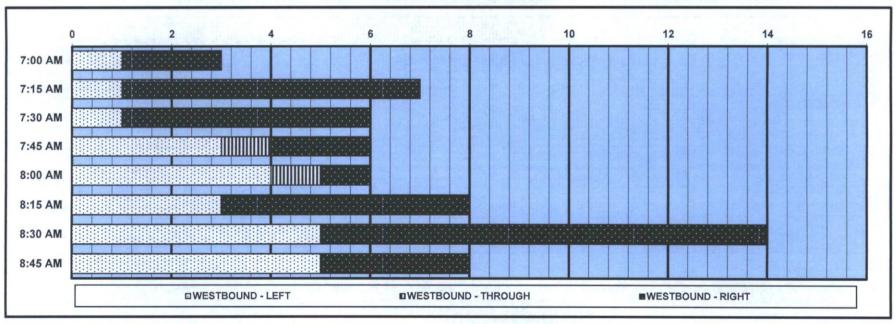


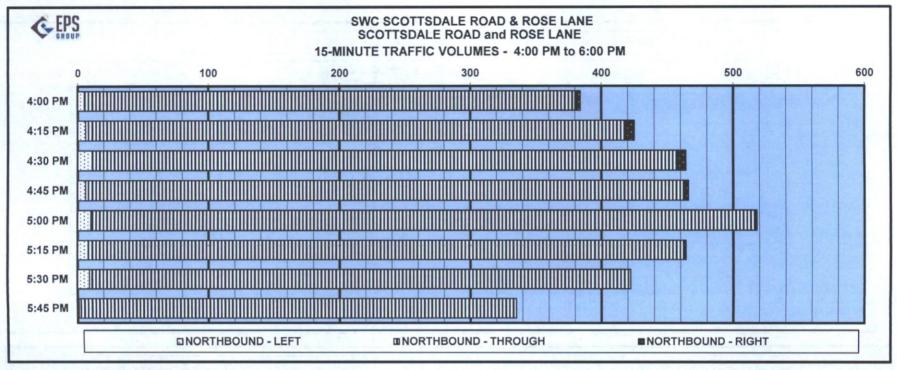


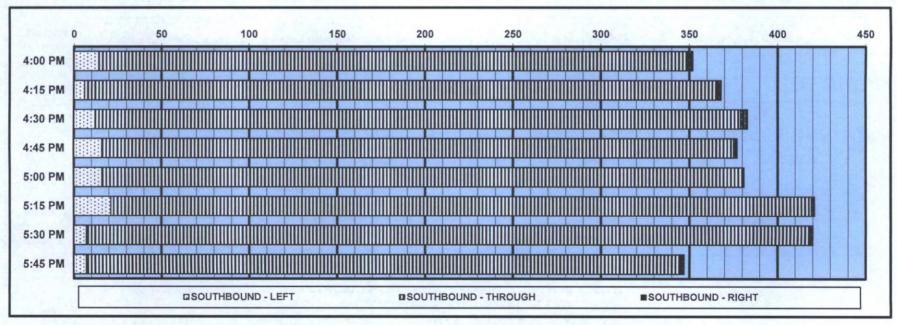


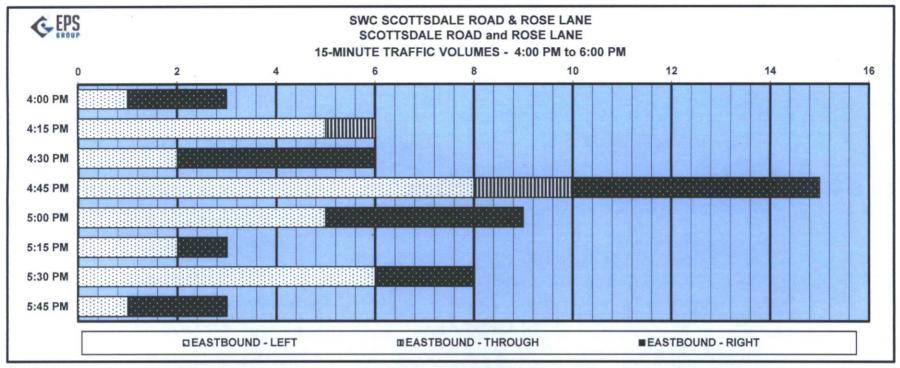


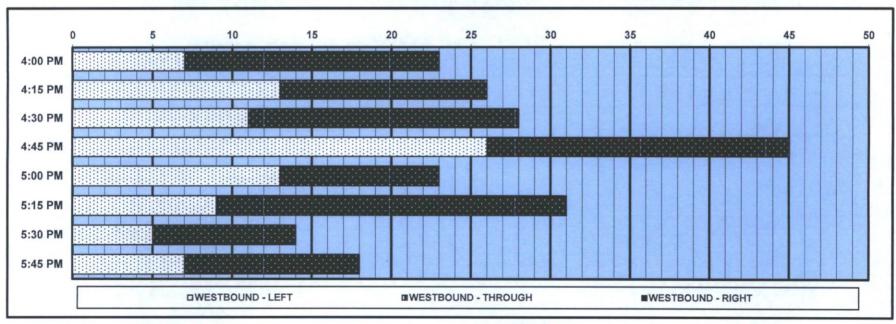








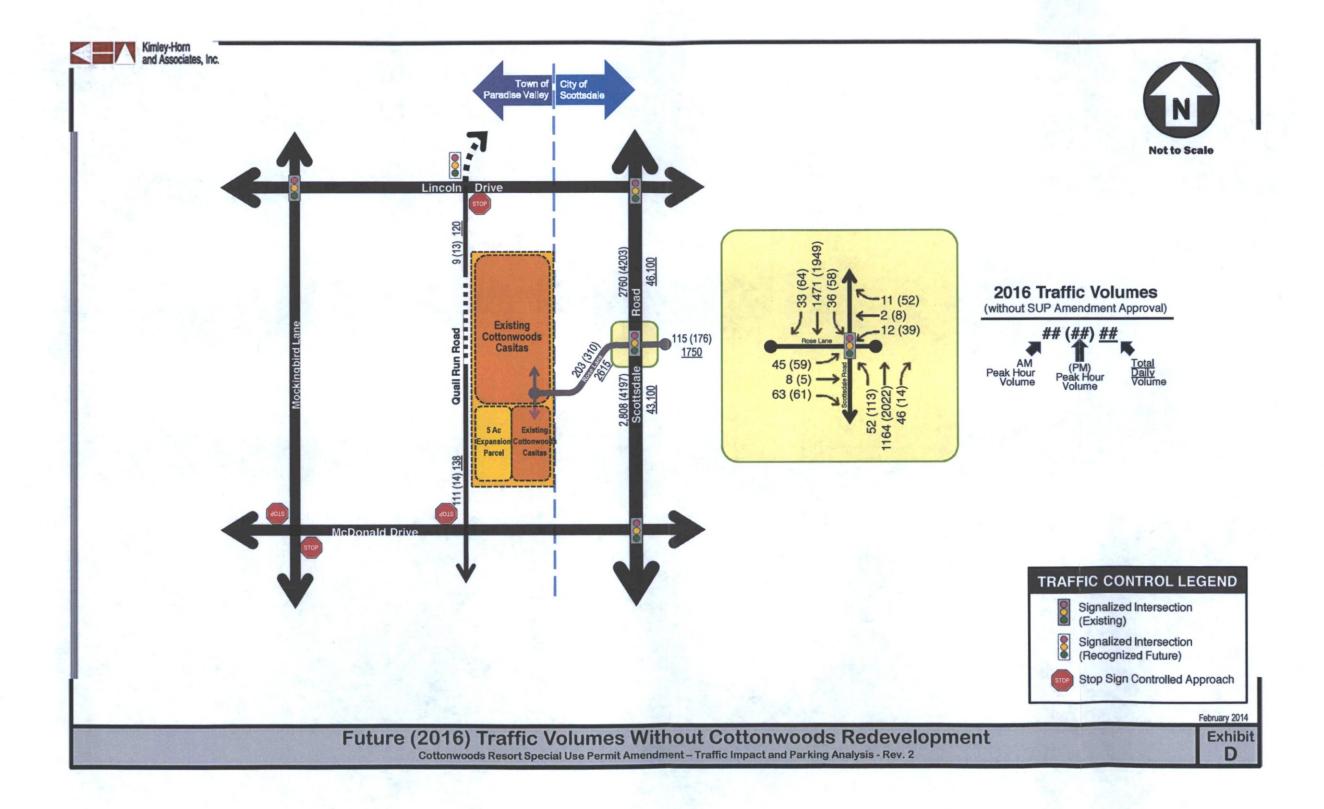


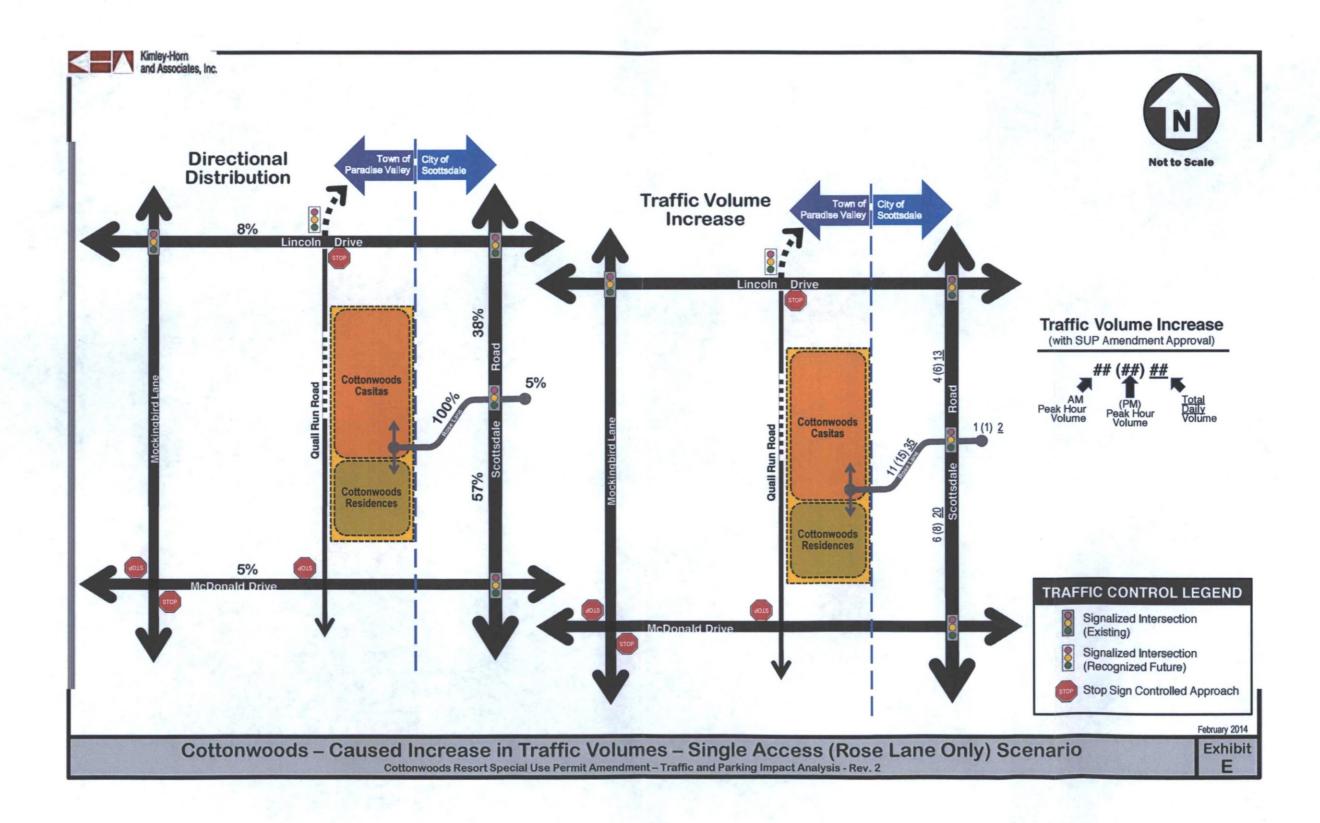


APPENDIX B
PERTINENT EXCERPTS FROM PREVIOUS REPORT

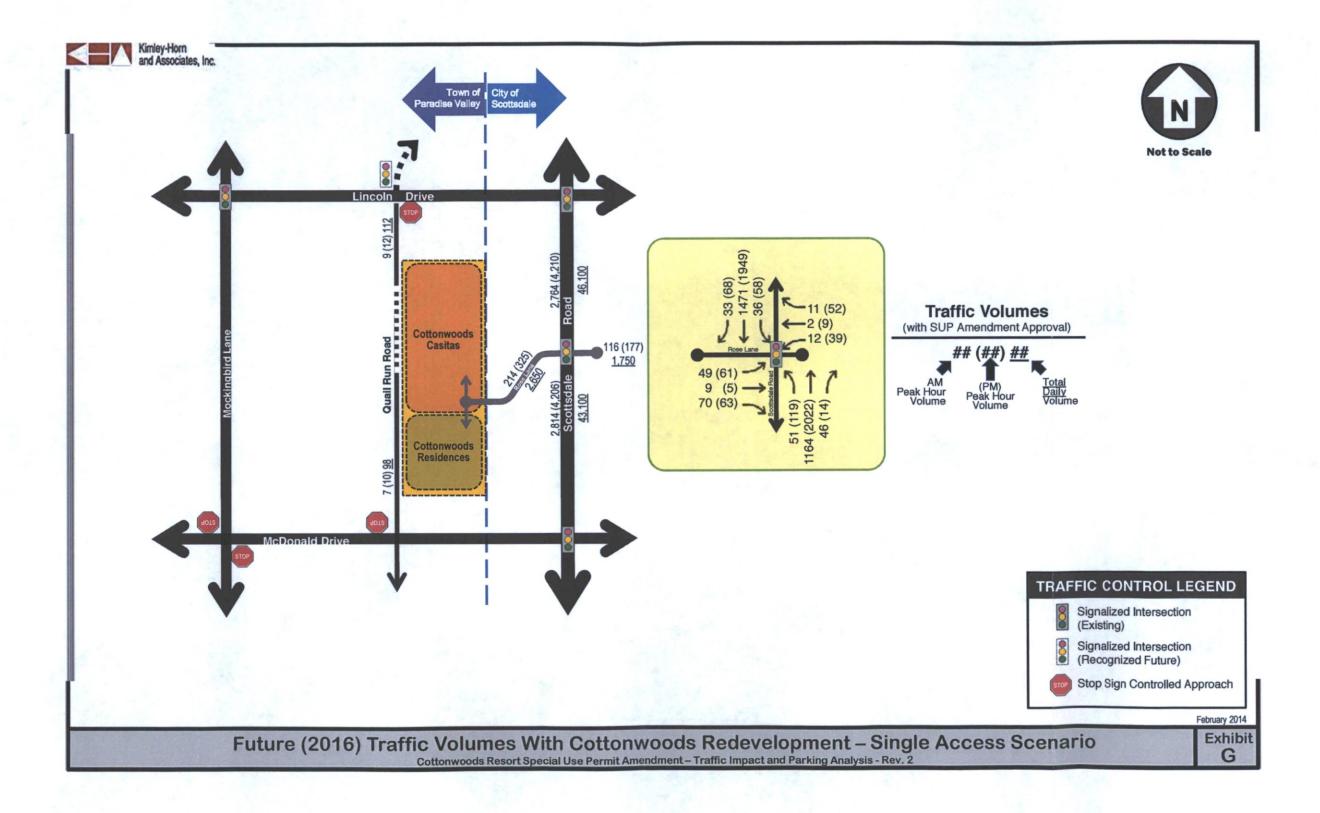


TRAFFIC





TRAFFIC





February 25, 2014

Mr. James Shano, P.E. Public Works Director Town of Paradise Valley 6401 E. McDonald Drive Paradise Valley, AZ 85253

e: Cottonwoods Resort - Paradise Valley, Arizona
Special Use Permit (SUP) Amendment
Traffic and Parking Impact Analysis – Revision No. 2

Dear Mr. Shano:

This letter discusses the anticipated traffic and parking impacts of updated redevelopment plans for the Cottonwoods Resort, and a resort-adjacent vacant 5.0 acre residential parcel. The Cottonwoods Resort is operating under an existing Special Use Permit (SUP) that covers 22.5 acres (the main resort site) located south of Lincoln Drive; west of Scottsdale Road; north of McDonald Drive; and east of Quail Run Road. Cottonwoods (the applicant) is proposing to expand the existing SUP coverage area by 5.0 acres, through an amendment to the existing SUP. The 5.0-acre "expansion" parcel the applicant is proposing to add to the SUP coverage area is located on the east side of Quail Run Road; approximately 320 feet north of McDonald Drive.

Suite 300 7740 N 16th Street

85020

27781

TOVE CHRISTIN

Phoenix, Arizona

Overview

There are currently 22.5 acres within the existing SUP coverage area. Previously considered redevelopment plans for the Cottonwoods Resort proposed three (3) traffic impacting changes to the SUP: (1) an increase in the size of the SUP coverage (land) area; (2) a change in the composition of dwelling units within the SUP coverage area; and (3) an increase in the number of dwelling units allowed within the SUP coverage area. Currently proposed changes to the SUP include an increase in land area and dwelling unit composition; but no longer include an increase in the allowable number of dwelling units.

A Vicinity Map and Context Plan identifying the main resort site and proposed expansion parcel, respectively; is presented in **Exhibit A.** A conceptual site plan for the entire 27.5 acres is presented in **Exhibit B.** Also attached to this letter are five additional exhibits (**Exhibits C through G**) displaying traffic impact information in a graphic format; and three pages of tables (**Tables 1 through 13**) that summarize the quantitative

TEL 602 944 5500 FAX 602 944 7423



Mr. James Shano, P.E., February 25, 2014, Page 2

information and opinions discussed below.

Executive Summary

The information provided with this letter demonstrates the following:

- Cottonwoods redevelopment will add fewer than 20 trips to Rose Lane during either peak hour. Rose Lane and the Scottsdale/Rose intersection have enough capacity remaining to accommodate all of this trip generation, as well as all of the traffic anticipated to come from the recently approved "commercial to residential" land use conversion of the rear portion of the Borgata property, which is located adjacent to the Cottonwoods property.
- Daily traffic volumes on Rose Lane will be lower, after the Cottonwoods and Borgata sites have been redeveloped than it would have been if the Borgata site remained commercial.
- Peak hour level of service at the Scottsdale/Rose intersection is expected to remain in the acceptable level of service (LOS) range ("D" or better) after Cottonwoods is completely redeveloped, without any traffic impact mitigation on Rose Lane, and regardless of whether or not any access to the Cottonwoods is provided on Quail Run Road.
- Approval of the Cottonwoods application will add no traffic to Quail Run Road, except during emergencies, as required by the Town. In fact, by adding the 5.0-acre expansion parcel to the existing SUP, approval of the SUP amendment will actually reroute to Rose Lane (City of Scottsdale) traffic that would otherwise be using Quail Run Road.
- Even if Cottonwoods residential (and not resort) access was to be provided along Quail Run Road (later referred to as the "dual access scenario"), the amount of Cottonwoods traffic that would use Quail Run would be minimal (approximately 39 vehicles per day, and fewer than 5 vehicles during either peak hour).
- The proposed redevelopment of the Cottonwoods property should not be the basis for determining when or how to close the existing "gap" in Quail Run Road because, regardless of which the above cited access scenarios is implemented, the amount of traffic this project would add to Quail Run Road would be minimal.
- The determination as to how and when to complete the rest of Quail Run Road between Lincoln and McDonald, should not occur without the following:
 - Specific consideration of the potential future use of the eight acres of undeveloped Sunchase property located to the west of the Cottonwoods site:
 - support of an alignment from existing owners of property along this segment of Quail Run Road; and

TRAFFIC







Conceptual Site Plan
Cottonwoods Resort Special Use Permit Amendment – Traffic and Parking Impact Analysis - Rev. 2

Exhibit B

APPENDIX C
LEVEL-OF-SERVICE ANALYSIS WITHOUT SITE



	•	→	*	•	—	4	1	1	-	1	1	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ર્ન	7		4	14	1	ተተጉ		N.	444	
Traffic Volume (vph)	10	2	8	12	2	14	19	1253	69	69	1243	15
Future Volume (vph)	10	2	8	12	2	14	19	1253	69	69	1243	15
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt		at its	0.850	alife of		0.850	19.55	0.992			0.998	
Flt Protected		0.959			0.958		0.950			0.950		
Satd. Flow (prot)	0	1786	1583	0	1785	1583	1770	5045	0	1770	5075	0
Flt Permitted		0.803			0.812		0.152			0.138		
Satd. Flow (perm)	0	1496	1583	0	1513	1583	283	5045	0	257	5075	0
Satd. Flow (RTOR)			64			64		17			3	
Adj. Flow (vph)	11	2	9	13	2	16	21	1392	77	77	1381	17
Lane Group Flow (vph)	0	13	9	0	15	16	21	1469	0	77	1398	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	4.11	pm+pt	NA	
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3		3	3		3	1			1		72-1
Total Split (s)	18.0	18.0	18.0	18.0	18.0	18.0	12.0	90.0		12.0	90.0	
Total Lost Time (s)		6.0	6.0		6.0	6.0	4.0	6.0		4.0	6.0	
Act Effct Green (s)		6.9	6.9		6.9	6.9	103.8	75.0		103.8	75.0	
Actuated g/C Ratio		0.06	0.06	A 4	0.06	0.06	0.86	0.62		0.86	0.62	
v/c Ratio		0.15	0.06		0.17	0.11	0.04	0.46		0.14	0.44	
Control Delay		56.9	0.8		57.6	1.4	1.7	12.0		2.7	11.9	
Queue Delay		0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	
Total Delay		56.9	0.8	egy so S	57.6	1.4	1.7	12.0		2.7	11.9	
LOS		E	Α		E	A	Α	В		Α	В	
Approach Delay		33.9			28.6			11.9			11.4	
Approach LOS		C			C			В			В	
Queue Length 50th (ft)		10	0		11	0	2	189		6	179	
Queue Length 95th (ft)		31	0		34	0	5	163		14	154	
Internal Link Dist (ft)		57			222			269			300	
Turn Bay Length (ft)			50			35	165			170		
Base Capacity (vph)		149	215		151	215	576	3586		559	3604	
Starvation Cap Reductn		0	0		0	0	0	0		0	0	
Spillback Cap Reductn		0	0		0	0	0	0		0	0	
Storage Cap Reductn		0	0	25.3	0	0	0	0		0	0	
Reduced v/c Ratio		0.09	0.04		0.10	0.07	0.04	0.41		0.14	0.39	

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.46

Intersection Signal Delay: 12.0
Intersection Capacity Utilization 50.3%

Intersection LOS: B
ICU Level of Service A

Analysis Period (min) 15

Splits and Phases: 1: Scottsdale Road & Rose Lane



No. 1	1	→	7	1	+	1	1	1	-	1	1	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		ર્ન	7"		र्स	7	7	ተተጉ		7	ተተጉ	3316
Traffic Volume (vph)	18	2	15	64	0	73	38	2012	15	70	1607	10
Future Volume (vph)	18	2	15	64	0	73	38	2012	15	70	1607	10
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt			0.850			0.850	ALE IN	0.999	1	17 17 17	0.999	A DE
Flt Protected		0.957			0.950		0.950			0.950		BUNG
Satd. Flow (prot)	0	1783	1583	0	1770	1583	1770	5080	0	1770	5080	0
Flt Permitted		0.695			0.743		0.094			0.049		
Satd. Flow (perm)	0	1295	1583	0	1384	1583	175	5080	0	91	5080	0
Satd. Flow (RTOR)			64			81		2			1	
Adj. Flow (vph)	20	2	17	71	0	81	42	2236	17	78	1786	11
Lane Group Flow (vph)	0	22	17	0	71	81	42	2253	0	78	1797	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3		3	3		.3	1			1	1.13 1.10	
Total Split (s)	26.0	26.0	26.0	26.0	26.0	26.0	12.0	82.0		12.0	82.0	
Total Lost Time (s)	A CONTRACTOR OF THE PARTY OF TH	6.0	6.0		6.0	6.0	4.0	6.0		4.0	6.0	STEW.
Act Effct Green (s)		11.5	11.5		11.5	11.5	94.5	81.3		94.5	81.3	
Actuated g/C Ratio		0.10	0.10		0.10	0.10	0.79	0.68		0.79	0.68	ojeuja)
v/c Ratio		0.18	0.08		0.54	0.36	0.15	0.65		0.34	0.52	
Control Delay		51.2	0.7		65.6	14.8	5.3	12.4		25.5	10.3	AN AL
Queue Delay		0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	
Total Delay		51.2	0.7		65.6	14.8	5.3	12.4		25.5	10.3	14 30
LOS		D	Α		E	В	Α	В		C	В	
Approach Delay		29.2			38.5			12.2			11.0	9000
Approach LOS		C			D			В			В	
Queue Length 50th (ft)		16	0		53	0	5	304		9	208	TO STILL
Queue Length 95th (ft)		41	0		99	46	14	403		58	280	
Internal Link Dist (ft)		57			222			269			300	
Turn Bay Length (ft)		MIN SE	50			35	165	ife sa		170		
Base Capacity (vph)	1	215	317		230	331	287	3441		228	3441	37
Starvation Cap Reductn		0	0		0	0	0	0		0	0	
Spillback Cap Reductn		0	0		0	0	0	0		0	0	
Storage Cap Reductn		0	0		0	0	0	0		0	0	
Reduced v/c Ratio		0.10	0.05		0.31	0.24	0.15	0.65		0.34	0.52	Carlotte.

Intersection Summary

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.65

Intersection Signal Delay: 12.8
Intersection Capacity Utilization 66.6%

Intersection LOS: B
ICU Level of Service C

Analysis Period (min) 15

Splits and Phases: 1: Scottsdale Road & Rose Lane



APPENDIX C.2
AMBIENT 2018



	•	→	*	1	←	4	1	1	-	1	Į.	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4	7		4	1	7	ተተጉ		7	444	13.11
Traffic Volume (vph)	14	3	15	12	2	15	21	1303	72	72	1293	16
Future Volume (vph)	14	3	15	12	2	15	21	1303	72	72	1293	16
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt		44	0.850		1	0.850	Red Link	0.992			0.998	
Flt Protected	**	0.960			0.958		0.950			0.950		
Satd. Flow (prot)	0	1788	1583	0	1785	1583	1770	5045	0	1770	5075	0
Flt Permitted		0.752	6		0.762		0.144			0.131		
Satd. Flow (perm)	0	1401	1583	0	1419	1583	268	5045	0	244	5075	0
Satd. Flow (RTOR)		TATES	64			64		17			3	
Adj. Flow (vph)	16	3	17	13	2	17	23	1448	80	80	1437	18
Lane Group Flow (vph)	0	19	17	0	15	17	23	1528	0	80	1455	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3		3	3		3	1			1		
Total Split (s)	18.0	18.0	18.0	18.0	18.0	18.0	12.0	90.0		12.0	90.0	
Total Lost Time (s)		6.0	6.0		6.0	6.0	4.0	6.0		4.0	6.0	
Act Effct Green (s)		7.2	7.2		7.2	7.2	103.5	77.8		103.5	77.8	
Actuated g/C Ratio	4	0.06	0.06	1/1	0.06	0.06	0.86	0.65		0.86	0.65	
v/c Ratio		0.23	0.11		0.18	0.11	0.04	0.47		0.16	0.44	
Control Delay		59.4	1.4	8, 79	57.4	1.4	1.9	10.8		3.1	10.6	
Queue Delay		0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	
Total Delay		59.4	1.4		57.4	1.4	1.9	10.8		3.1	10.6	
LOS		E	A		E	A	A	В		Α	В	
Approach Delay	1 1/4 - 1	32.0		1200	27.7			10.7			10.2	
Approach LOS		C			C			В			В	
Queue Length 50th (ft)		14	0		11	0	2	168		6	158	100
Queue Length 95th (ft)		39	0		34	0	6	176		15	166	
Internal Link Dist (ft)		57			222			269			300	
Turn Bay Length (ft)			50			35	165			170		
Base Capacity (vph)		140	215		141	215	527	3581		511	3599	
Starvation Cap Reductn		0	0		0	0	0	0		0	0	
Spillback Cap Reductn		0	0		0	0	0	0		0	0	
Storage Cap Reductn		0	0		0	0	0	0		0	0	
Reduced v/c Ratio		0.14	0.08		0.11	0.08	0.04	0.43		0.16	0.40	

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.47

Intersection Signal Delay: 10.9
Intersection Capacity Utilization 51.7%

Intersection LOS: B
ICU Level of Service A

Analysis Period (min) 15



	1	→	*	1	+	1	1	1	-	1	+	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4	77		4	7	1	ተተጉ		7	ተተጉ	Mark.
Traffic Volume (vph)	21	2	18	66	1	76	45	2093	16	73	1671	14
Future Volume (vph)	21	2	18	66	1	76	45	2093	16	73	1671	14
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt			0.850			0.850	12.10	0.999			0.999	
Flt Protected		0.956			0.953		0.950			0.950		
Satd. Flow (prot)	0	1781	1583	0	1775	1583	1770	5080	0	1770	5080	0
Flt Permitted		0.690			0.711		0.085			0.049		
Satd. Flow (perm)	0	1285	1583	0	1324	1583	158	5080	0	91	5080	0
Satd. Flow (RTOR)			64			84		2			2	
Adj. Flow (vph)	23	2	20	73	1	84	50	2326	18	81	1857	16
Lane Group Flow (vph)	0	25	20	0	74	84	50	2344	0	81	1873	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3		3	3	100	3	1			1		1107
Total Split (s)	26.0	26.0	26.0	26.0	26.0	26.0	12.0	82.0		12.0	82.0	
Total Lost Time (s)		6.0	6.0		6.0	6.0	4.0	6.0		4.0	6.0	
Act Effct Green (s)		12.0	12.0		12.0	12.0	94.0	81.4		94.0	81.4	
Actuated g/C Ratio		0.10	0.10		0.10	0.10	0.78	0.68		0.78	0.68	
v/c Ratio		0.20	0.09		0.56	0.36	0.19	0.68		0.37	0.54	
Control Delay		51.1	0.8		66.6	14.2	7.1	12.9		27.3	10.6	
Queue Delay		0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	
Total Delay		51.1	0.8		66.6	14.2	7.1	12.9		27.3	10.6	
LOS		D	Α		E	В	Α	В		C	В	
Approach Delay		28.8			38.8			12.8			11.3	
Approach LOS		C			D			В			В	
Queue Length 50th (ft)		18	0		56	0	6	332		9	226	
Queue Length 95th (ft)		44	0		103	46	16	443		62	305	
Internal Link Dist (ft)		57			222			269			300	
Turn Bay Length (ft)			50			35	165			170		
Base Capacity (vph)		214	317		220	333	266	3445		219	3445	11
Starvation Cap Reductn		0	0		0	0	0	0		0	0	
Spillback Cap Reductn		0	0		0	0	0	0		0	0	Sec. Marie
Storage Cap Reductn		0	0		0	0	0	0	TE TOTAL	0	0	
Reduced v/c Ratio		0.12	0.06		0.34	0.25	0.19	0.68		0.37	0.54	

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.68

Intersection Signal Delay: 13.2

Intersection Capacity Utilization 68.5%

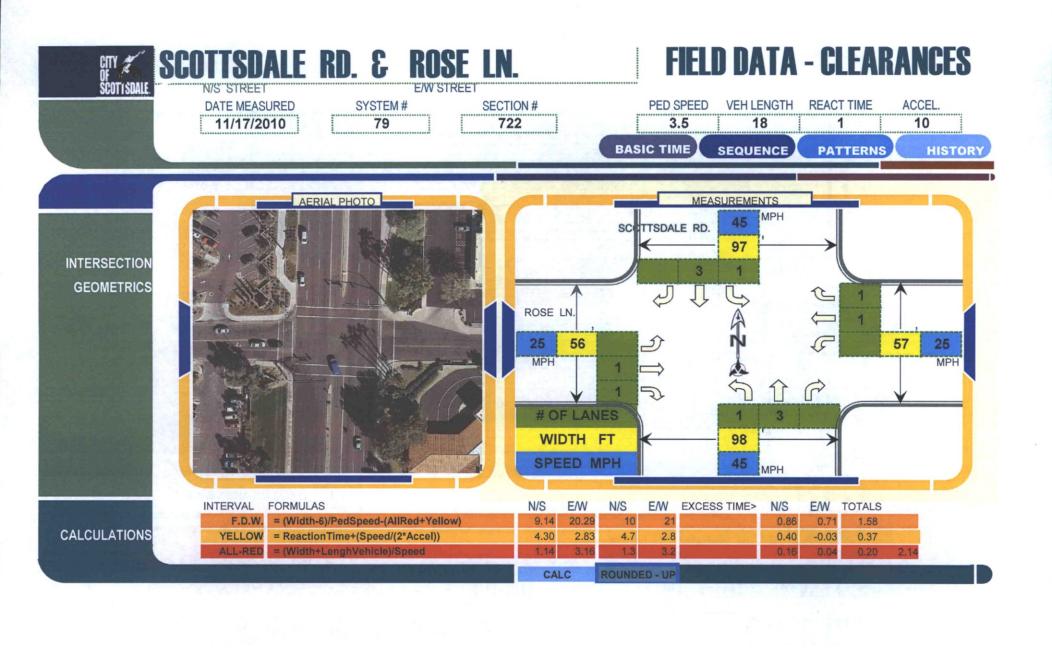
Intersection LOS: B
ICU Level of Service C

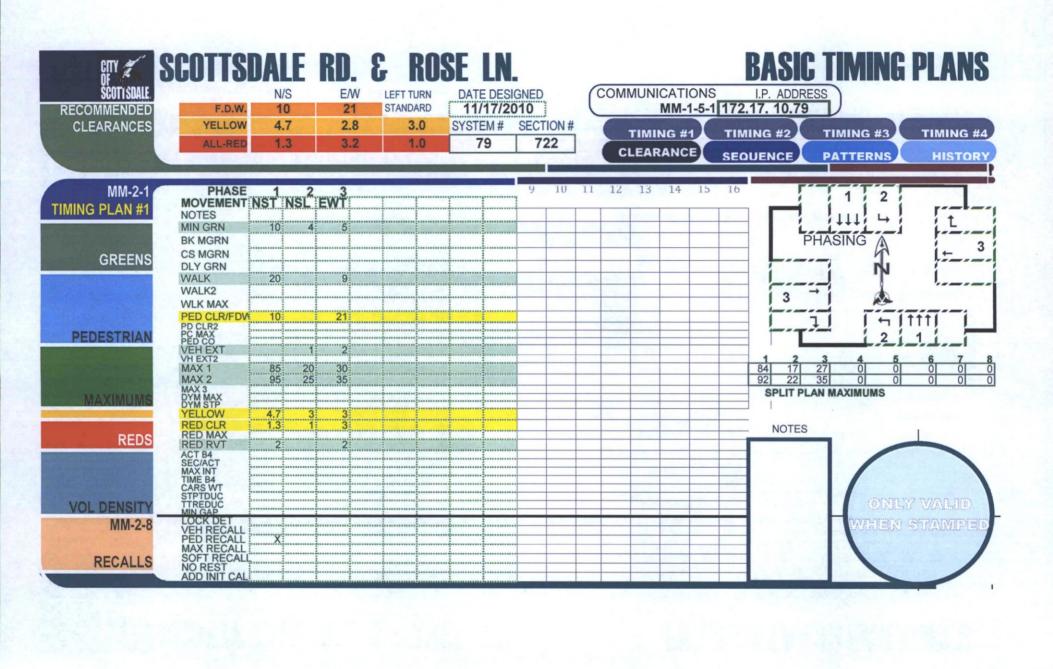
Analysis Period (min) 15

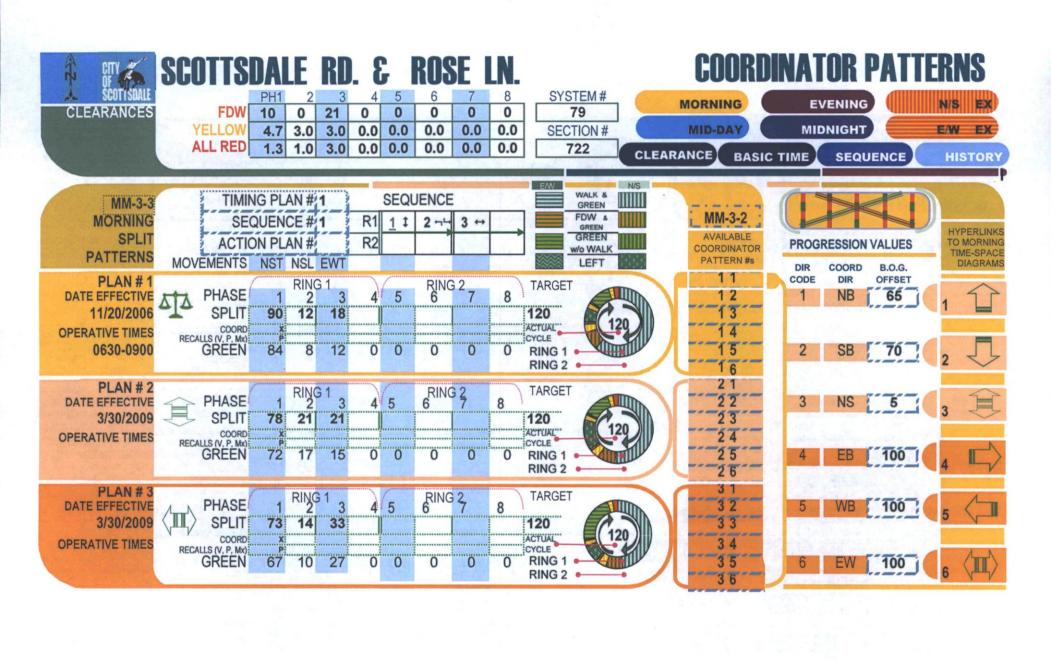


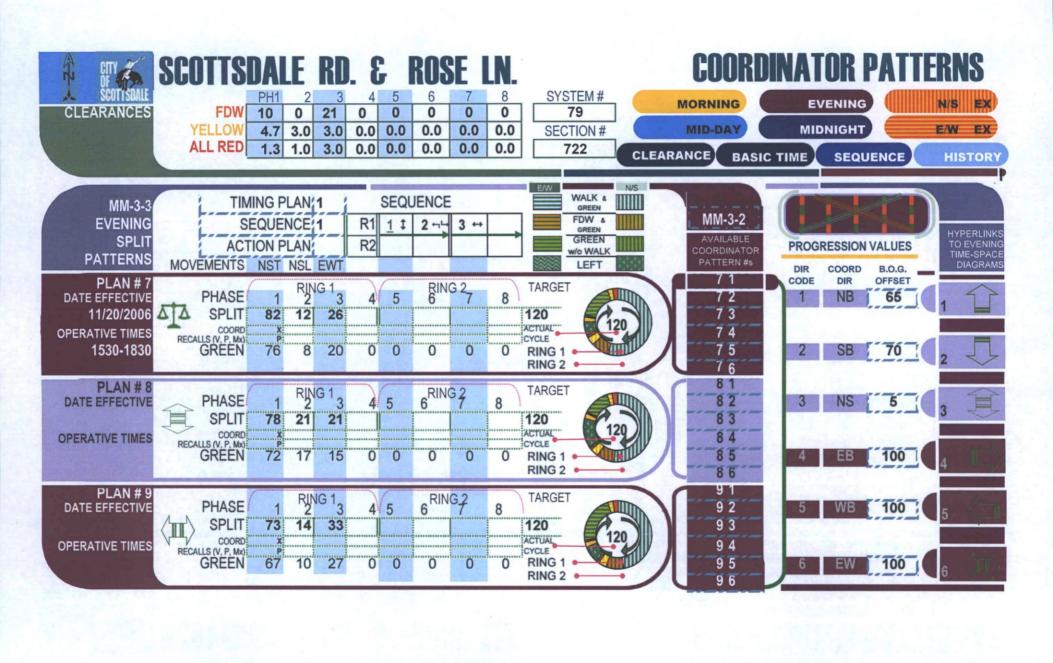
APPENDIX D
TRAFFIC SIGNAL TIMING PLANS











APPENDIX E
TRIP GENERATION



PROJECT	SW	C SCOTTSDALE F	ROAD & ROSE L	ANE
PARCEL		RESTAL	JRANT	
ITE LAND USE CATEGORY AND CODE		QUALITY REST	AURANT - 931	
INDEPENDENT VARIABLE		1,000 SQU/	ARE FEET	
SIZE		9.0	00	
			TRIPS	
and the same of th		ENTERING	EXITING	TOTAL
WEEKDAY DAILY	7	50%	50%	
NUMBER OF STUDIES	15	100		
AVERAGE SIZE	9			Electronic Control
MINIMUM RATE	33.41	151	150	301
AVERAGE RATE	89.95	405	405	810
MAXIMUM RATE	139.80	629	629	1,258
STANDARD DEVIATION	36.81			
EQUATION: NOT PROVIDED	NA	NA	NA	NA
LARGEST OF AVERAGE OR EQUATION	Contract of the second	405	405	810
AM PEAK HOUR ADJACENT STREET	-	50%	50%	
NUMBER OF STUDIES	11			17 76.7
AVERAGE SIZE	9			- 3
MINIMUM RATE	0.25	1	1	2
AVERAGE RATE	0.81	4	3	7
MAXIMUM RATE	1.60	7	7	14
STANDARD DEVIATION	0.93			
EQUATION: NOT PROVIDED	NA	NA	NA	NA
LARGEST OF AVERAGE OR EQUATION		4	3	7
AM PEAK HOUR GENERATOR	Contract to the	82%	18%	
NUMBER OF STUDIES	14			
AVERAGE SIZE	9			
MINIMUM RATE	0.87	7	1	8
AVERAGE RATE	5.57	41	9	50
MAXIMUM RATE	10.37	76	17	93
STANDARD DEVIATION	3.79			
EQUATION: NOT PROVIDED	NA	NA	NA	NA
LARGEST OF AVERAGE OR EQUATION		41	9	50
PM PEAK HOUR ADJACENT STREET		67%	33%	
NUMBER OF STUDIES	24			
AVERAGE SIZE	9			
MINIMUM RATE	2.42	15	7	22
AVERAGE RATE	7.49	45	22	67
MAXIMUM RATE	18.64	113	55	168
STANDARD DEVIATION	4.89			
EQUATION: NOT PROVIDED	NA	NA	NA	NA
LARGEST OF AVERAGE OR EQUATION		45	22	67
PM PEAK HOUR GENERATOR		62%	38%	
NUMBER OF STUDIES	16			
AVERAGE SIZE	9			
MINIMUM RATE	3.24	18	11	29
AVERAGE RATE	9.02	50	31	81
MAXIMUM RATE	15.89	89	54	143
STANDARD DEVIATION	4.55			
EQUATION: NOT PROVIDED	NA	NA	NA	NA
LARGEST OF AVERAGE OR EQUATION		50	31	81

PROJECT	SWC SCOTTSDALE ROAD & ROSE LANE								
PARCEL	RESTAURANT QUALITY RESTAURANT - 931								
ITE LAND USE CATEGORY AND CODE									
INDEPENDENT VARIABLE		1,000 SQU	ARE FEET	3 () () ()					
SIZE	in the same	9.0	00						
the best of the state of the st			TRIPS						
	RATE	ENTERING	EXITING	SUM					
SATURDAY DAILY		50%	50%						
NUMBER OF STUDIES	11								
AVERAGE SIZE	9								
MINIMUM RATE	53.63	242	241	483					
AVERAGE RATE	94.36	425	424	849					
MAXIMUM RATE	156.67	705	705	1,410					
STANDARD DEVIATION	34.42								
EQUATION: LN (T) = 1.04 * LN(X) + 4.41	$R^2 = 0.54$	54	53	107					
LARGEST OF AVERAGE OR EQUATION		425	424	849					
PEAK HOUR GENERATOR		59%	41%						
NUMBER OF STUDIES	11	9 11 2							
AVERAGE SIZE	9								
MINIMUM RATE	5.75	31	21	52					
AVERAGE RATE	10.82	57	40	97					
MAXIMUM RATE	15.28	81	57	138					
STANDARD DEVIATION	4.38			7,5					
EQUATION: T = 10.87 * (X) - 0.46	$R^2 = 0.64$	11	7	18					
LARGEST OF AVERAGE OR EQUATION		57	40	97					
SUNDAY DAILY		50%	50%						
NUMBER OF STUDIES	11			1					
AVERAGE SIZE	9	1							
MINIMUM RATE	34.09	154	153	307					
AVERAGE RATE	72.16	325	324	649					
MAXIMUM RATE	137.78	620	620	1,240					
STANDARD DEVIATION	32.35								
EQUATION: NOT PROVIDED	NA	NA	NA	NA					
LARGEST OF AVERAGE OR EQUATION		325	324	649					
PEAK HOUR GENERATOR	4 1	63%	37%	F 74/23					
NUMBER OF STUDIES	10								
AVERAGE SIZE	9								
MINIMUM RATE	4.56	26	15	41					
AVERAGE RATE	8.38	47	28	75					
MAXIMUM RATE	12.07	69	40	109					
STANDARD DEVIATION	3.88								
EQUATION: LN (T) = 0.94 * LN(X) + 2.21	$R^2 = 0.55$	6	4	10					
LARGEST OF AVERAGE OR EQUATION	., 0.00	47	28	75					

PROJECT	SW	C SCOTTSDALE F	ROAD & ROSE L	ANE						
PARCEL		RESTAL								
ITE LAND USE CATEGORY AND CODE	HIGH TU	JRNOVER (SIT-DO		ANT - 932						
INDEPENDENT VARIABLE		1,000 SQU/		10.00						
SIZE	9.000									
			TRIPS	and the second						
		ENTERING	EXITING	TOTAL						
WEEKDAY DAILY		50%	50%							
NUMBER OF STUDIES	14									
AVERAGE SIZE	7									
MINIMUM RATE	73.51	331	331	662						
AVERAGE RATE	127.15	572	572	1,144						
MAXIMUM RATE	246.00	1,107	1,107	2,214						
STANDARD DEVIATION	41.77	1,107	1,101	2,217						
EQUATION: NOT PROVIDED	NA	NA	NA	NA						
LARGEST OF AVERAGE OR EQUATION	14/3	572	572	1,144						
AM PEAK HOUR ADJACENT STREET		52%	48%	1,1						
NUMBER OF STUDIES	18	0270	10 / 0							
AVERAGE SIZE	6	1	× 1							
MINIMUM RATE	2.83	13	12	25						
AVERAGE RATE	11.52	54	50	104						
MAXIMUM RATE	25.60	120	110	230						
STANDARD DEVIATION	6.75	120	110	230						
EQUATION: NOT PROVIDED	NA	NA	NA	NA						
LARGEST OF AVERAGE OR EQUATION	INA	54	50	104						
AM PEAK HOUR GENERATOR		52%	48%	104						
NUMBER OF STUDIES	21	5270	4070							
AVERAGE SIZE	7									
MINIMUM RATE	3.00	14	13	27						
AVERAGE RATE	13.53	63	59	122						
MAXIMUM RATE	54.09	253	234	487						
STANDARD DEVIATION	10.05	255	234	407						
EQUATION: NOT PROVIDED	NA	NA	NA	NA						
LARGEST OF AVERAGE OR EQUATION	INA	63	59							
PM PEAK HOUR ADJACENT STREET		59%	41%	122						
	46	59%	4170							
NUMBER OF STUDIES	6	-								
AVERAGE SIZE		15	10	2F						
MINIMUM RATE	2.80 11.15	15 59	10	25						
AVERAGE RATE MAXIMUM RATE			41	100						
STANDARD DEVIATION	62.00	329	229	558						
	9.13	NIA	NIA	NIA						
EQUATION: NOT PROVIDED	NA	NA F0	NA 44	NA 400						
LARGEST OF AVERAGE OR EQUATION		59	41	100						
PM PEAK HOUR GENERATOR	04	54%	46%							
NUMBER OF STUDIES	31									
AVERAGE SIZE	5	07	20							
MINIMUM RATE	5.60	27	23	50						
AVERAGE RATE	18.49	90	76	166						
MAXIMUM RATE	69.20	336	287	623						
STANDARD DEVIATION	13.32									
EQUATION: NOT PROVIDED	NA	NA	NA	NA						
LARGEST OF AVERAGE OR EQUATION		90	76	166						

PROJECT	SW	C SCOTTSDALE F	ROAD & ROSE LA	ANE					
PARCEL		RESTAL	JRANT						
ITE LAND USE CATEGORY AND CODE	HIGH TURNOVER (SIT-DOWN) RESTAURANT - 932								
INDEPENDENT VARIABLE	1,000 SQUARE FEET								
SIZE	9.000								
the second secon			TRIPS						
	RATE	ENTERING	EXITING	SUM					
SATURDAY DAILY		50%	50%						
NUMBER OF STUDIES	2	Mark Market	en date by						
AVERAGE SIZE	5								
MINIMUM RATE	144.60	651	650	1,301					
AVERAGE RATE	158.37	713	712	1,425					
MAXIMUM RATE	172.71	777	777	1,554					
STANDARD DEVIATION	NA								
EQUATION: NOT PROVIDED	NA	NA	NA	NA					
LARGEST OF AVERAGE OR EQUATION		713	712	1,425					
PEAK HOUR GENERATOR		53%	47%						
NUMBER OF STUDIES	8								
AVERAGE SIZE	4								
MINIMUM RATE	4.44	21	19	40					
AVERAGE RATE	14.07	67	60	127					
MAXIMUM RATE	50.40	241	213	454					
STANDARD DEVIATION	12.19			111111111111111111111111111111111111111					
EQUATION: NOT PROVIDED	NA	NA	NA	NA					
LARGEST OF AVERAGE OR EQUATION		67	60	127					
SUNDAY DAILY		50%	50%						
NUMBER OF STUDIES	2			17/19					
AVERAGE SIZE	5	1							
MINIMUM RATE	119.38	537	537	1,074					
AVERAGE RATE	131.84	594	593	1,187					
MAXIMUM RATE	143.80	647	647	1,294					
STANDARD DEVIATION	NA			1-1-2					
EQUATION: NOT PROVIDED	NA	NA	NA	NA					
LARGEST OF AVERAGE OR EQUATION		594	593	1,187					
PEAK HOUR GENERATOR		55%	45%	The state of the					
NUMBER OF STUDIES	3		The state of the s						
AVERAGE SIZE	4								
MINIMUM RATE	9.79	48	40	88					
AVERAGE RATE	18.46	91	75	166					
MAXIMUM RATE	43.20	214	175	389					
STANDARD DEVIATION	13.74			000					
EQUATION: NOT PROVIDED	NA NA	NA	NA	NA					
LARGEST OF AVERAGE OR EQUATION		91	75	166					
ENTOLOT OF ATELWAL ON ENGATION				€ El					

PROJECT	SW	C SCOTTSDALE F	ROAD & ROSE L	ANE
PARCEL		RESTAURANT -		
ITE LAND USE CATEGORY AND CODE		QUALITY REST		
INDEPENDENT VARIABLE		1,000 SQU/		
SIZE		8.0		
		The second secon	TRIPS	
		ENTERING	EXITING	TOTAL
WEEKDAY DAILY		50%	50%	The state of the s
NUMBER OF STUDIES	15	43 1 1	THE SAME REPORTED	ed and had been
AVERAGE SIZE	9			
MINIMUM RATE	33.41	134	133	267
AVERAGE RATE	89.95	360	360	720
MAXIMUM RATE	139.80	559	559	1,118
STANDARD DEVIATION	36.81			
EQUATION: NOT PROVIDED	NA	NA	NA	NA
LARGEST OF AVERAGE OR EQUATION	Section 1	360	360	720
AM PEAK HOUR ADJACENT STREET		50%	50%	
NUMBER OF STUDIES	11		197	
AVERAGE SIZE	9			
MINIMUM RATE	0.25	1	1	2
AVERAGE RATE	0.81	3	3	6
MAXIMUM RATE	1.60	7	6	13
STANDARD DEVIATION	0.93	7. 187		
EQUATION: NOT PROVIDED	NA	NA	NA	NA
LARGEST OF AVERAGE OR EQUATION	And Address	3	3	6
AM PEAK HOUR GENERATOR		82%	18%	1
NUMBER OF STUDIES	14	1 72 11		
AVERAGE SIZE	9	1000		
MINIMUM RATE	0.87	6	1	7
AVERAGE RATE	5.57	37	8	45
MAXIMUM RATE	10.37	68	15	83
STANDARD DEVIATION	3.79			
EQUATION: NOT PROVIDED	NA	NA	NA	NA
LARGEST OF AVERAGE OR EQUATION		37	8	45
PM PEAK HOUR ADJACENT STREET		67%	33%	
NUMBER OF STUDIES	24	4		
AVERAGE SIZE	9	40		- 10
MINIMUM RATE	2.42	13	6	19
AVERAGE RATE	7.49	40	20	60
MAXIMUM RATE	18.64	100	49	149
STANDARD DEVIATION	4.89	NIA	NIA	NIA
EQUATION: NOT PROVIDED	NA	NA 40	NA 20	NA CO
LARGEST OF AVERAGE OR EQUATION		40	20 38%	60
PM PEAK HOUR GENERATOR	16	62%	38%	
NUMBER OF STUDIES AVERAGE SIZE	16 9			
	3.24	16	10	26
MINIMUM RATE AVERAGE RATE	9.02	45	27	72
MAXIMUM RATE	15.89	79	48	127
		79	40	127
STANDARD DEVIATION	4.55 NA	NIA	NA	NIA
EQUATION: NOT PROVIDED LARGEST OF AVERAGE OR EQUATION	INA	NA 45	NA 27	NA 72
LANGEST OF AVERAGE OR EQUATION		45	21	72

PROJECT	SW	C SCOTTSDALE R		ANE						
PARCEL	I Carry Control	RESTAURANT - I		May 19 1						
ITE LAND USE CATEGORY AND CODE	QUALITY RESTAURANT - 931									
INDEPENDENT VARIABLE	1,000 SQUARE FEET									
SIZE	and the state of the state of	8.00								
the same of part of the same o			TRIPS							
and the last of th	RATE	ENTERING	EXITING	SUM						
SATURDAY DAILY		50%	50%							
NUMBER OF STUDIES	11									
AVERAGE SIZE	9									
MINIMUM RATE	53.63	215	214	429						
AVERAGE RATE	94.36	378	377	755						
MAXIMUM RATE	156.67	627	626	1,253						
STANDARD DEVIATION	34.42			17						
EQUATION: LN (T) = 1.04 * LN(X) + 4.41	$R^2 = 0.54$	48	48	96						
LARGEST OF AVERAGE OR EQUATION		378	377	755						
PEAK HOUR GENERATOR	The same	59%	41%							
NUMBER OF STUDIES	11		1 X 7 33							
AVERAGE SIZE	9			1						
MINIMUM RATE	5.75	27	19	46						
AVERAGE RATE	10.82	51	36	87						
MAXIMUM RATE	15.28	72	50	122						
STANDARD DEVIATION	4.38									
EQUATION: T = 10.87 * (X) - 0.46	$R^2 = 0.64$	10	7	17						
LARGEST OF AVERAGE OR EQUATION		51	36	87						
SUNDAY DAILY		50%	50%							
NUMBER OF STUDIES	11									
AVERAGE SIZE	9									
MINIMUM RATE	34.09	137	136	273						
AVERAGE RATE	72.16	289	288	577						
MAXIMUM RATE	137.78	551	551	1,102						
STANDARD DEVIATION	32.35									
EQUATION: NOT PROVIDED	NA	NA	NA	NA						
LARGEST OF AVERAGE OR EQUATION		289	288	577						
PEAK HOUR GENERATOR		63%	37%	E Part of						
NUMBER OF STUDIES	10									
AVERAGE SIZE	9									
MINIMUM RATE	4.56	23	13	36						
AVERAGE RATE	8.38	42	25	67						
MAXIMUM RATE	12.07	61	36	97						
STANDARD DEVIATION	3.88									
EQUATION: LN (T) = 0.94 * LN(X) + 2.21	$R^2 = 0.55$	6	3	9						
LARGEST OF AVERAGE OR EQUATION		42	25	67						

APPENDIX F
LEVEL-OF-SERVICE ANALYSIS WITH SITE



	•	-	-	1	←	4	1	1	-	1	ļ	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		4	14		र्स	7	N.	ተተጉ		7	ተተጉ	
Traffic Volume (vph)	39	6	37	12	5	15	46	1303	72	72	1293	43
Future Volume (vph)	39	6	37	12	5	15	46	1303	72	72	1293	43
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt			0.850			0.850	14 1	0.992	100		0.995	
Flt Protected		0.959			0.967		0.950			0.950		
Satd. Flow (prot)	0	1786	1583	0	1801	1583	1770	5045	0	1770	5060	0
Flt Permitted		0.742			0.764		0.138	4011		0.131		
Satd. Flow (perm)	0	1382	1583	0	1423	1583	257	5045	0	244	5060	0
Satd. Flow (RTOR)			64			64		17			10	
Adj. Flow (vph)	43	7	41	13	6	17	51	1448	80	80	1437	48
Lane Group Flow (vph)	0	50	41	0	19	17	51	1528	0	80	1485	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA	7	pm+pt	NA	1
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3		3	3		3	1			1		
Total Split (s)	18.0	18.0	18.0	18.0	18.0	18.0	12.0	90.0		12.0	90.0	
Total Lost Time (s)		6.0	6.0		6.0	6.0	4.0	6.0		4.0	6.0	
Act Effct Green (s)		9.3	9.3		9.3	9.3	99.0	77.5		99.0	77.5	
Actuated g/C Ratio		0.08	0.08		0.08	0.08	0.82	0.65		0.82	0.65	
v/c Ratio		0.47	0.23		0.17	0.09	0.11	0.47		0.18	0.45	
Control Delay	10.33	66.3	8.1		54.0	1.0	3.2	11.0		4.3	10.9	
Queue Delay		0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	Sales I
Total Delay		66.3	8.1		54.0	1.0	3.2	11.0		4.3	10.9	
LOS		E	Α		D	A	A	В		Α	В	
Approach Delay		40.1			29.0			10.7			10.5	
Approach LOS		D			C			В			В	
Queue Length 50th (ft)		38	0	7.	14	0	5	161		8	156	
Queue Length 95th (ft)		79	18		38	0	12	191		18	185	
Internal Link Dist (ft)		57			222			269			300	
Turn Bay Length (ft)			50			35	165			170		
Base Capacity (vph)		138	215		142	215	458	3546		449	3555	
Starvation Cap Reductn		0	0		0	0	0	0		0	0	
Spillback Cap Reductn		0	0		0	0	0	0		0	0	
Storage Cap Reductn		0	0		0	0	0	0		0	0	
Reduced v/c Ratio		0.36	0.19		0.13	0.08	0.11	0.43		0.18	0.42	

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.47

Intersection Signal Delay: 11.7
Intersection Capacity Utilization 53.2%

Intersection LOS: B
ICU Level of Service A

Analysis Period (min) 15



	-	-	*	-	+	1	1	1	-	1	+	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations		र्स	14		र्स	7	1	ተተጉ	The same	7	ተተጉ	
Traffic Volume (vph)	42	4	36	66	4	76	72	2093	16	73	1671	44
Future Volume (vph)	42	4	36	66	4	76	72	2093	16	73	1671	44
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt		AT E	0.850	13,4		0.850		0.999			0.996	
Flt Protected		0.956			0.955		0.950			0.950		
Satd. Flow (prot)	0	1781	1583	0	1779	1583	1770	5080	0	1770	5065	0
FIt Permitted		0.688			0.700		0.081			0.049		192
Satd. Flow (perm)	0	1282	1583	0	1304	1583	151	5080	0	91	5065	0
Satd. Flow (RTOR)			64			84		2			6	15 5
Adj. Flow (vph)	47	4	40	73	4	84	80	2326	18	81	1857	49
Lane Group Flow (vph)	0	51	40	0	77	84	80	2344	0	81	1906	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3		3	3		3	1			1	MORE THE	Shows !
Total Split (s)	26.0	26.0	26.0	26.0	26.0	26.0	12.0	82.0		12.0	82.0	
Total Lost Time (s)	1 1	6.0	6.0	-	6.0	6.0	4.0	6.0		4.0	6.0	SHAT
Act Effct Green (s)		12.5	12.5		12.5	12.5	93.5	81.0		93.5	81.0	
Actuated g/C Ratio		0.10	0.10		0.10	0.10	0.78	0.68		0.78	0.68	1617
v/c Ratio		0.38	0.18		0.57	0.35	0.31	0.68		0.37	0.56	
Control Delay		56.6	6.0		66.1	13.7	14.6	13.2		27.9	11.0	
Queue Delay		0.0	0.0		0.0	0.0	0.0	0.0		0.0	0.0	
Total Delay		56.6	6.0		66.1	13.7	14.6	13.2		27.9	11.0	
LOS		E	A		E	В	В	В		C	В	
Approach Delay		34.4			38.7			13.3			11.7	
Approach LOS		C			D			В			В	
Queue Length 50th (ft)		38	0		58	0	10	336		10	235	
Queue Length 95th (ft)		75	15		104	46	25	462		63	326	
Internal Link Dist (ft)		57			222			269			300	
Turn Bay Length (ft)			50			35	165			170		
Base Capacity (vph)		213	317		217	333	259	3427		217	3419	15.2
Starvation Cap Reductn		0	0	100	0	0	0	0		0	0	
Spillback Cap Reductn		0	0	F. C.	0	0	0	0		0	0	Stell !
Storage Cap Reductn		0	0		0	0	0	0		0	0	
Reduced v/c Ratio		0.24	0.13		0.35	0.25	0.31	0.68		0.37	0.56	1016

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.68

Intersection Signal Delay: 13.9

Intersection Capacity Utilization 68.7%

Intersection LOS: B
ICU Level of Service C

Analysis Period (min) 15



Intersection	0.5745.8		de jas					
Int Delay, s/veh	3.8					Ç I		
Movement		EBT	EBR	W	BL	WBT	NBL	NBR
Lane Configurations		12				4	W	
Traffic Vol, veh/h		42	0		43	50	0	40
Future Vol, veh/h		42	0		43	50	0	40
Conflicting Peds, #/hr		0	0		0	0	0	0
Sign Control	MICHIGAN STATE	Free	Free	Fr	ee	Free	Stop	Stop
RT Channelized		1100	None			None	Otop	None
Storage Length			-		NA SE	-	0	IVOITO
Veh in Median Storage, #		0		Sales as		0	0	NAME OF THE
Grade, %		0				0	0	
Peak Hour Factor		90	90		90	90	90	90
Heavy Vehicles, %	MONTH STREET	2	2		2	2	2	2
Mvmt Flow		47	0		48	56	0	44
IVIVIIIL F IOW		41	U	NEW THEFALE	40	50	U	44
Major/Minor	1	//ajor1		Majo	r2		Minor1	
Conflicting Flow All	1 1000	0	0		47	0	198	47
Stage 1						MEAN	47	
Stage 2	NAME OF THE OWNER, OWNE	-	-		-	- HORSELDWINGSHICKE	151	-
Critical Hdwy				4.	12		6.42	6.22
Critical Hdwy Stg 1	and the little parties.	-	-	THE REAL PROPERTY AND ADDRESS OF THE PERSON NAMED IN COLUMN TWO IS NOT THE PERSON NAMED IN COLUMN TO THE PERSON NAMED IN COLUM	-	-	5.42	-
Critical Hdwy Stg 2					-		5.42	
Follow-up Hdwy		-	-	2.2	18		3.518	3.318
Pot Cap-1 Maneuver				150			791	1022
Stage 1	manufacturi (1821)	-		.0	-		975	TOLL
Stage 2	a ya e				1		877	
Platoon blocked, %		THE PERSON NAMED IN	-		HE STA		resimulation and Williams	
Mov Cap-1 Maneuver	YOU WELL THE			15	60		766	1022
Mov Cap-2 Maneuver		NEW RIANG	-	THE REAL PROPERTY.	-		766	1022
Stage 1	4455 <u>4</u> 654				NO.	Laborer L	975	
Stage 2				with the state of the state of			849	
Olage 2							043	
Approach	1256	EB		M	VB		NB	
HCM Control Delay, s		0	N. S. S. S.	3	3.4		8.7	
HCM LOS				The state of the s	Carlo Ball		A	9/
Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL WE	BT.			
Capacity (veh/h)	1022	-		1560				
HCM Lane V/C Ratio	0.043	-	-	0.031	-		9 9 4 7 5	1 6 5 5
HCM Control Delay (s)	8.7			7.4	0			
HCM Lane LOS	Α		-	Α	Α		A CONTRACTOR	
HCM 95th %tile Q(veh)	0.1			0.1			CONTRACTOR OF THE PARTY OF THE	SAN ASSESSMENT OF THE PARTY OF

Intersection			HE PATE							
Int Delay, s/veh	3.1									1 5 6 kg d
Movement		EBT	EBR		WBL	WBT	NB	L N	BR	
Lane Configurations		1				4	*	1		W. Berten
Traffic Vol, veh/h		49	0		47	71		0	33	
Future Vol, veh/h		49	0		47	71		0	33	
Conflicting Peds, #/hr		0	0		0	0		0	0	
Sign Control		Free	Free		Free	Free	Sto	p S	top	
RT Channelized			None		-	None			ne	
Storage Length		-	-		-	-		0	-	
Veh in Median Storage, #		0			-	0		0	-	
Grade, %		0	-		-	0		0	-	
Peak Hour Factor		90	90		90	90			90	
Heavy Vehicles, %		2	2		2	2		2	2	
Mvmt Flow		54	0		52	79		0	37	
Major/Minor	N	Najor1		N	lajor2		Minor	1		
Conflicting Flow All		0	0	The state of	54	0	23	7	54	100
Stage 1		-	-		-		5	4		
Stage 2		-	-		-	-	18	3	-	
Critical Hdwy		-			4.12		6.4	2 6.	.22	
Critical Hdwy Stg 1		-	-		-	-	5.4	2	-	
Critical Hdwy Stg 2		-			-		5.4	2	-	
Follow-up Hdwy		-	-		2.218	-	3.51	8 3.3	18	
Pot Cap-1 Maneuver		-			1551	-	75	1 10	113	
Stage 1		-	-		-	-	96	9	-	n in the sol
Stage 2		-	-		-		84	8	-	
Platoon blocked, %		-	-			-				THE REPORT OF
Mov Cap-1 Maneuver		-	1		1551	-	72	5 10	113	
Mov Cap-2 Maneuver		-	-		-	-	72	5	-	
Stage 1		-			-		96	9		
Stage 2		-	-		-	-	81	8	-	and Early
Approach	registion.	EB			WB		N	В		
HCM Control Delay, s		0			2.9		8.	7		
HCM LOS								A		
										140
Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT					ZVIA
Capacity (veh/h)	1013			1551						
HCM Lane V/C Ratio	0.036	-	-	0.034	-			100	The second	
HCM Control Delay (s)	8.7	-		7.4	0					
HCM Lane LOS	Α	-	-	Α	Α			100		
HCM 95th %tile Q(veh)	0.1			0.1	-					
HOW 95th %tile Q(veh)	0.1	12-14		0.1						TRANSPORT OF THE PARTY OF THE P

Intersection							
	1.8						
Movement	WBL	WBR		NBT	NBR	SBL	SBT
Lane Configurations	W	man market		7			4
Traffic Vol, veh/h	0	10		32	0	11	39
Future Vol, veh/h	0	10		32	0	11	39
Conflicting Peds, #/hr	0	0		0	0	0	0
Sign Control	Stop	Stop	MATERIAL PROPERTY.	Free	Free	Free	Free
RT Channelized		None			AND DESIGNATION OF THE PERSON		None
Storage Length	0	-		-	-		-
Veh in Median Storage, #				0	STREET STREET		0
Grade, %	0	-		0	-	**************************************	0
Peak Hour Factor	90	90		90	90	90	90
Heavy Vehicles, %	2	2	Warnes Sale	2	2	2	2
Mvmt Flow	0	11		36	0	12	43
Major/Minor	Minor1			Major1		Major2	(SS)
Conflicting Flow All	104	36		0	0	36	0
Stage 1	36		F3.54				
Stage 2	68	-	· · · · · · · · · · · · · · · · · · ·		-	-	-
Critical Hdwy	6.42	6.22				4.12	
Critical Hdwy Stg 1	5.42	-	NAME OF TAXABLE PARTY.	-	-	-	-
Critical Hdwy Stg 2	5.42						
Follow-up Hdwy	3.518	3.318	-7102 CA	-	-	2.218	-
Pot Cap-1 Maneuver	894	1037				1575	
Stage 1	986	-		-	-	-	-
Stage 2	955				16.512		
Platoon blocked, %			THE RESERVE	-	-		-
Mov Cap-1 Maneuver	887	1037				1575	
Mov Cap-2 Maneuver	887	-		-	-	-	-
Stage 1	986					BOST NO.	
Stage 2	947	-	- Anna Colonia	-	-	-	-
Approach	WB			NB		SB	
HCM Control Delay, s	8.5		1	0		1.6	
HCM LOS	Α					The state of the s	
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT			
Capacity (veh/h)		- 1037	1575				
HCM Lane V/C Ratio	-	- 0.011	0.008	- 1.1	- 3 8		
HCM Control Delay (s)	-	- 8.5	7.3	0			
HCM Lane LOS	-	- A	Α	Α			7 4 2
HCM 95th %tile Q(veh)		- 0	0	-			
, ,							-

Intersection							N.S.D.A.	
	1.3			17.74				1 7/12 - 1/12
Movement	WBL	WBR		NBT	NBR	SBL	SBT	
ane Configurations	W	THE I		1	13613		4	
raffic Vol, veh/h	0	8	DESIGNATION OF THE PARTY OF THE	41	0	12	59	
uture Vol, veh/h	0	8		41	0	12	59	
conflicting Peds, #/hr	0	0		0	0	0	0	
sign Control	Stop	Stop		Free	Free	Free	Free	
RT Channelized	Otop -	None		1100	None	1100	None	
storage Length	0	None	I STEWARD		140116	-	None	
eh in Median Storage, #	0			0			0	
	0	N. Sulfa M. Majik		0	-		0	
rade, % eak Hour Factor	90	90	SHEAT	90	90	90	90	
	2	2		2	2	2	2	
leavy Vehicles, %	0	9	THE REAL PROPERTY.	46	0	13	66	
lvmt Flow	U	9	OR SERVICE	40	U	13	00	
1-1-18 11	10 1			11.1.1		Helena		
lajor/Minor	Minor1		10	Major1		Major2		
Conflicting Flow All	138	46	The Parket of th	0	0	46	0	ON ADDRESS OF THE PARTY OF THE
Stage 1	46							
Stage 2	92	-	and Comment	-	-	- 140	-	
ritical Hdwy	6.42	6.22			-	4.12		
ritical Hdwy Stg 1	5.42	-		-	-	-	-	
ritical Hdwy Stg 2	5.42				-		-	
ollow-up Hdwy	3.518	3.318		-	-	2.218	-	
ot Cap-1 Maneuver	855	1023				1562		
Stage 1	976	-		-	-	-	-	West of the second
Stage 2	932			Research				
Platoon blocked, %				1 -	-		-	The Mark State
Nov Cap-1 Maneuver	847	1023				1562		
Nov Cap-2 Maneuver	847	-		1	-	-	-	
Stage 1	976							
Stage 2	924			-		-	-	
Approach	WB			NB		SB		
ICM Control Delay, s	8.6			0		1.2		
ICM LOS	А							
linor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT				
Capacity (veh/h)		- 1023	1562					
ICM Lane V/C Ratio	-	- 0.009	0.009	-				
ICM Control Delay (s)		- 8.6	7.3	0				
HCM Lane LOS	-	- A	Α	Α				
HCM 95th %tile Q(veh)		- 0	0					
, ,		The second secon					-	

	•	→	*	1	—	4	1	1	-	-	ļ	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	19	1	7	7	↑	7	19	ተተጉ		7	ተተጐ	
Traffic Volume (vph)	39	6	37	12	5	15	46	1303	72	72	1293	43
Future Volume (vph)	39	6	37	12	5	15	46	1303	72	72	1293	43
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt			0.850			0.850	1	0.992			0.995	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1863	1583	1770	1863	1583	1770	5045	0	1770	5060	0
Flt Permitted	0.754			0.753			0.138			0.131		
Satd. Flow (perm)	1405	1863	1583	1403	1863	1583	257	5045	0	244	5060	0
Satd. Flow (RTOR)			64			64		17			10	
Adj. Flow (vph)	43	7	41	13	6	17	51	1448	80	80	1437	48
Lane Group Flow (vph)	43	7	41	13	6	17	51	1528	0	80	1485	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA		pm+pt	NA	
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3		3	3		3	1			1		
Total Split (s)	18.0	18.0	18.0	18.0	18.0	18.0	12.0	90.0		12.0	90.0	
Total Lost Time (s)	6.0	6.0	6.0	6.0	6.0	6.0	4.0	6.0		4.0	6.0	
Act Effct Green (s)	8.9	8.9	8.9	8.9	8.9	8.9	99.4	77.6		99.4	77.6	
Actuated g/C Ratio	0.07	0.07	0.07	0.07	0.07	0.07	0.83	0.65		0.83	0.65	
v/c Ratio	0.41	0.05	0.23	0.12	0.04	0.10	0.11	0.47		0.18	0.45	
Control Delay	64.1	50.7	8.3	53.1	50.4	1.1	3.1	10.9		4.2	10.8	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	
Total Delay	64.1	50.7	8.3	53.1	50.4	1.1	3.1	10.9	100	4.2	10.8	
LOS	E	D	A	D	D	A	A	В		Α	В	
Approach Delay		37.9			28.1			10.7			10.5	
Approach LOS		D			C			В			В	
Queue Length 50th (ft)	32	5	0	10	4	0	5	161		8	156	
Queue Length 95th (ft)	70	20	18	30	18	0	12	191		18	185	
Internal Link Dist (ft)		57			222			269			300	1
Turn Bay Length (ft)			50			35	165			170		
Base Capacity (vph)	140	186	215	140	186	215	462	3553		453	3562	A STATE OF THE PARTY OF THE PAR
Starvation Cap Reductn	0	0	0	0	0	0	0	0	X BOOK	0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0		0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0		0	0	
Reduced v/c Ratio	0.31	0.04	0.19	0.09	0.03	0.08	0.11	0.43		0.18	0.42	· 1

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.47

Intersection Signal Delay: 11.5
Intersection Capacity Utilization 52.9%

Intersection LOS: B
ICU Level of Service A

Analysis Period (min) 15



40	1	-	-	1	+	*	1	1	-	1	1	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	1	↑	7"	7	^	7	1	ተተጉ		7	444	The same
Traffic Volume (vph)	42	4	36	66	4	76	72	2093	16	73	1671	44
Future Volume (vph)	42	4	36	66	4	76	72	2093	16	73	1671	44
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt		Albert	0.850			0.850		0.999			0.996	T.
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1863	1583	1770	1863	1583	1770	5080	0	1770	5065	0
Flt Permitted	0.755			0.755			0.081			0.049		
Satd. Flow (perm)	1406	1863	1583	1406	1863	1583	151	5080	0	91	5065	0
Satd. Flow (RTOR)			64			84		2			6	
Adj. Flow (vph)	47	4	40	73	4	84	80	2326	18	81	1857	49
Lane Group Flow (vph)	47	4	40	73	4	84	80	2344	0	81	1906	0
Turn Type	Perm	NA	Perm	Perm	NA	Perm	pm+pt	NA		pm+pt	NA	1 1
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3	4 7 3 1	3	3	11000	3	1			1	- Pari	May.
Total Split (s)	26.0	26.0	26.0	26.0	26.0	26.0	12.0	82.0		12.0	82.0	
Total Lost Time (s)	6.0	6.0	6.0	6.0	6.0	6.0	4.0	6.0		4.0	6.0	
Act Effct Green (s)	11.7	11.7	11.7	11.7	11.7	11.7	94.3	81.5		94.3	81.5	
Actuated g/C Ratio	0.10	0.10	0.10	0.10	0.10	0.10	0.79	0.68		0.79	0.68	
v/c Ratio	0.34	0.02	0.19	0.53	0.02	0.37	0.30	0.68		0.36	0.55	
Control Delay	55.7	46.0	6.3	64.4	46.0	14.4	13.8	12.8		27.1	10.7	
Queue Delay	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0		0.0	0.0	
Total Delay	55.7	46.0	6.3	64.4	46.0	14.4	13.8	12.8		27.1	10.7	
LOS	E	D	Α	E	D	В	В	В		C	В	
Approach Delay		33.5			37.8			12.9			11.4	
Approach LOS		C			D			В			В	
Queue Length 50th (ft)	35	3	0	55	3	0	9	327		9	229	
Queue Length 95th (ft)	71	14	16	100	14	46	24	445		62	315	
Internal Link Dist (ft)		57			222			269			300	
Turn Bay Length (ft)			50			35	165			170		
Base Capacity (vph)	234	310	317	234	310	333	264	3449		222	3441	
Starvation Cap Reductn	0	0	0	0	0	0	0	0		0	0	
Spillback Cap Reductn	0	0	0	0	0	0	0	0		0	0	
Storage Cap Reductn	0	0	0	0	0	0	0	0		0	0	
Reduced v/c Ratio	0.20	0.01	0.13	0.31	0.01	0.25	0.30	0.68		0.36	0.55	

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.68

Intersection Signal Delay: 13.5

Intersection Capacity Utilization 68.5%

Intersection LOS: B
ICU Level of Service C

Analysis Period (min) 15



nt Dolov olych	3.8								100000000000000000000000000000000000000
nt Delay, s/veh	3.8								
Movement		EBT	EBR		WBL	WBT	NBL	NBR	
ane Configurations		1				र्स	Y		Market Total
Traffic Vol, veh/h		42	0		43	50	0	40	
Future Vol, veh/h		42	0		43	50	0	40	WELL AND THE
Conflicting Peds, #/hr		0	0		0	0	0	0	
Sign Control		Free	Free		Free	Free	Stop	Stop	
RT Channelized			None			None		None	
Storage Length		-	-		-	-	0	-	
Veh in Median Storage, #		0	-			0	0		
Grade, %		0	-		-	0	0	-	
Peak Hour Factor		90	90		90	90	90	90	
Heavy Vehicles, %		2	2		2	2	2	2	A Spirite 1
Mvmt Flow		47	0		48	56	0	44	
Major/Minor	N	Najor1		٨	/lajor2		Minor1		
Conflicting Flow All		0	0		47	0	198	47	
Stage 1							47		
Stage 2		-	-		-		151	AUDITARIA DE SENTENTA DE	
Critical Hdwy				VI SUS	4.12		6.42	6.22	
Critical Hdwy Stg 1		-	-	ACCULATION .	-	-	5.42	-	DESIGNATION OF THE PERSON OF T
Critical Hdwy Stg 2				Park Tea			5.42		
Follow-up Hdwy	HISTORIA SIDEMERSION	-	-	SACTOR DESIGNATION	2.218	-	3.518	3.318	
Pot Cap-1 Maneuver					1560		791	1022	
Stage 1		-	-		-	-	975	-	
Stage 2							877		
Platoon blocked, %		-	-			-			
Mov Cap-1 Maneuver					1560		766	1022	
Mov Cap-2 Maneuver		-	-		-	-	766	-	
Stage 1		-	177 -				975	-	
Stage 2		-	-		-	-	849		
Approach	0.5314535	EB		(1)	WB		NB		
HCM Control Delay, s		0			3.4		8.7		
HCM LOS	OUR INIUPICATION TO		STATE OF STREET	resolved)	311		A	Manager And States	
Minor Lane/Major Mvmt	NBLn1	EBT	EBR	WBL	WBT				
Capacity (veh/h)	1022	LDI.		1560	4401				
HCM Lane V/C Ratio	0.043	-		0.031					
HCM Control Delay (s)	8.7			7.4	0	NISTERNIE		III THE STATE OF T	STATE OF THE PARTY
HCM Lane LOS	Α	-	-	Α Α	A				COLUMN TO SERVICE SERV
HCM 95th %tile Q(veh)	0.1			0.1	_	BALL SOLDIES		PROFESSION NO.	
TOTAL JOHN GUILL (VEIL)	0.1	SERVICE DE LA CONTRACTOR DE LA CONTRACTO	and the second	0,1	STATES OF				

ic Vol, veh/h re Vol, veh/h	9 0 9 0 0 0	WBL 47 47	WBT ← ↑ 71	NBL ¥	NBR	
ement EB e Configurations ic Vol, veh/h re Vol, veh/h dicting Peds, #/hr Control Fre	9 0 9 0 0 0	47 47	र्स		NBR	
e Configurations ic Vol, veh/h re Vol, veh/h dicting Peds, #/hr Control Control	9 0 9 0 0 0	47 47	र्स		NBR	Byggesen
c Configurations ic Vol, veh/h re Vol, veh/h licting Peds, #/hr Control Control	9 0 9 0 0 0	47		Y		
ic Vol, veh/h 4 re Vol, veh/h 4 licting Peds, #/hr Control Fre	9 0 9 0 0 0	47				
re Vol, veh/h 4 licting Peds, #/hr Control Fre	9 0			0	33	
licting Peds, #/hr Control Fre			71	0	33	
Control Fre	- Г	0	0	0	0	
	e Free	Free	Free	Stop	Stop	
	- None		None		None	
age Length		-	-	0	-	
in Median Storage, #	0 -		0	0		
	0 -	-	0	0	-	
	0 90	90	90	90	90	
	2 2	2	2	2	2	. , .
	4 0	52	79	0	37	
	12// 15	14.5				
r/Minor Major	1	Major2		Minor1		1788
		54	0	237	54	
		-	-		_	
	-	4.12			6.22	
		-	_		-	a long to the long to
		2.218	-		3.318	
		-	-		-	
				848	The state of the s	900
			-			45
		1551		725	1013	
Cap-2 Maneuver		-	-	725	-	
Stage 1				969		
Stage 2		-	40.5	818	1685-01	
roach	В	WB		NB		
			THE PERSON			5600
	ACCOUNT OF THE	2.0			The second secon	TO LOUIS COMME
r Lane/Major Mymt NBLn1 EB	T EBR	WBL WBT		estivated		E
			CONTRACTOR OF STREET		/	
	140414					
	STREET, SQUARE, SALES	0.1 -				B380
Stage 1 Stage 2		4.12 - 2.218 1551 - - 1551 - - - WB 2.9 WBL WBT 1551 - 0.034 - 7.4 0 A A		54 183 6.42 5.42 5.42 3.518 751 969 848 725 725 969 818	6.22 - 3.318 1013 - - 1013	

Intersection	WE COLEM							
nt Delay, s/veh	1.8							
Movement	WBL	WBR		NBT	NBR	SBL	SBT	
Lane Configurations	Y			1>			4	
Traffic Vol, veh/h	0	10		32	0	11	39	
Future Vol, veh/h	0	10	CONCERNION OF THE PARTY OF	32	0	11	39	
Conflicting Peds, #/hr	0	0	E 180 YO	0		0	0	
Sign Control	Stop	Stop		Free	STREET, SQUARE,	Free	Free	
RT Channelized	Otop	None	HEAT 1	1100		1100	None	
Storage Length	0	-		-	-	-	-	
Veh in Median Storage, #			Market Service	0			0	
Grade, %	0			0			0	
Peak Hour Factor	90	90		90	90	90	90	
Heavy Vehicles, %	2	2	THE RESERVE	2	2	2	2	
Mymt Flow	0	11	May 15	36	0	12	43	
				30		12		
Major/Minor	Minor1			Major1		Major2		
Conflicting Flow All	104	36		0	0	36	0	
Stage 1	36						341	
Stage 2	68				-	-	-	
Critical Hdwy	6.42	6.22				4.12		
Critical Hdwy Stg 1	5.42	-			-	-	-	
Critical Hdwy Stg 2	5.42		HERE		-			
Follow-up Hdwy	3.518	3.318		- Manager Caracteristics	-	2.218	-	
Pot Cap-1 Maneuver	894	1037				1575		
Stage 1	986	-		-	-	-	-	· ·
Stage 2	955							
Platoon blocked, %				THE RESERVE OF THE PARTY OF THE	-		-	
Mov Cap-1 Maneuver	887	1037	TO SERVE	-		1575		
Mov Cap-2 Maneuver	887	-		-		-	-	
Stage 1	986							The second second
Stage 2	947		THE RESIDEN		-	-	-	
Approach	WB			NB		SB		
HCM Control Delay, s	8.5	有关 (10)		0		1.6		
HCM LOS	А				1 1			
								Later of Vice
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT	1351	Market Page		
Capacity (veh/h)		- 1037	1575					
HCM Lane V/C Ratio	-	- 0.011		-	1119	W. W. W.		SALE VIANALI
HCM Control Delay (s)		- 8.5	7.3	0				
HCM Lane LOS	-	- A	Α	Α				
HCM 95th %tile Q(veh)		- 0	0					

Movement WBL	Intersection								
Tarlic Vol, veh/h Tarlic Vol, v		1.3			18073	-		To the	
Tarlic Vol, veh/h Tarlic Vol, v	Movement	WBL	WBR		NBT	NBR	SBL	SBT	
rraffic Vol, veh/h									
Future Vol, veh/h Future Fut			8			0	12		
Conflicting Peds, #/hr									
Right Control Stop Stop Free Free Free Free Free Free Free Free		0	0			0		0	A
None		Stop	Stop		Free	Free	Free	Free	
Control Cont	RT Channelized	CONTRACTOR DESCRIPTION	CALL PROPERTY AND ADDRESS OF THE PARTY AND ADD	1937		None		None	
Veh in Median Storage, # 0		0	-		-	and the same of th		-	muqu
Stage Stag		0			0	-		0	
Peak Hour Factor 90 60 66 Algorithm Mallor Mallor Mallor Mallor Major Majo	Grade, %	0	-		0	-	-	0	
Any All Flow Alajor/Minor Minor Minor Major Major Major Major Conflicting Flow All	Peak Hour Factor	90	90		90	90	90	90	360
Anjor/Minor Minor1 Major1 Major2 Conflicting Flow All 138 46 0 0 0 46 0 Stage 1 46	Heavy Vehicles, %	2	2		2	2	2	2	
Stage 1	Mvmt Flow	0	9		46	0	13	66	TE AL
Stage 1									
Stage 1	Major/Minor	Minor1			Major1		Major2		Jan B
Stage 1	Conflicting Flow All		46			0		0	
Stage 2 92	-		THE RESERVE OF THE PERSON NAMED IN COLUMN 1			NAMES OF TAXABLE PARTY.	Annual Control of the		
### Critical Hollowy			-		-	-	-	-	
Critical Houry Stg 1 5.42	Critical Hdwy	6.42	6.22			_	4.12		1913
Critical Hdwy Stg 2		5.42	-		-	-	-	-	
Sollow-up Hdwy						-			TO THE
Stage 1			3.318		-	-	2.218	-	
Stage 1 976 -	Pot Cap-1 Maneuver	855	1023				1562	-	
Stage 2 932 - - - - - - - - -	THE RESIDENCE OF THE PROPERTY	976	-		-	-	-	-	
Platoon blocked, % Mov Cap-1 Maneuver 847 1023 1562 - Mov Cap-2 Maneuver 847 Stage 1 976 Stage 2 924 Stage 2 924 Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SBT Capacity (veh/h) - 1023 1562 - HCM Lane V/C Ratio - 0.009 0.009 - HCM Control Delay (s) - 8.6 7.3 0 HCM Lane LOS - A A A		932				-			
Mov Cap-1 Maneuver 847 1023 1562 - Mov Cap-2 Maneuver 847 Stage 1 976 Stage 2 924 Stage 2 924 Approach WB NB SB HCM Control Delay, s 8.6 0 1.2 HCM LOS A Minor Lane/Major Mvmt NBT NBRWBLn1 SBL SBT Capacity (veh/h) 1023 1562 - HCM Lane V/C Ratio 0.009 0.009 - HCM Control Delay (s) - 8.6 7.3 0 HCM Lane LOS - A A A	Platoon blocked, %				-	-		-	
Mov Cap-2 Maneuver	Mov Cap-1 Maneuver	847	1023				1562	-	
Stage 1 976 -	Mov Cap-2 Maneuver		-		-	-	-	-	
Stage 2 924 - - - - - - - - -		976			-				MA
NB		924	Mary Mary	7	20.64.	-	-	-	
CM Control Delay, s									
A A A A A A A A A A A A A A A A A A A	Approach	WB			NB		SB		
Alinor Lane/Major Mvmt NBT NBRWBLn1 SBL SBT Capacity (veh/h) - 1023 1562 - HCM Lane V/C Ratio - 0.009 0.009 - HCM Control Delay (s) - 8.6 7.3 0 HCM Lane LOS - A A A	HCM Control Delay, s	8.6			0		1.2		
Capacity (veh/h) 1023 1562 - HCM Lane V/C Ratio 0.009 0.009 - HCM Control Delay (s) 8.6 7.3 0 HCM Lane LOS - A A A	HCM LOS	Α		NE MONSONS					CHENTRA
Capacity (veh/h) 1023 1562 - HCM Lane V/C Ratio 0.009 0.009 - HCM Control Delay (s) 8.6 7.3 0 HCM Lane LOS - A A A									144
HCM Lane V/C Ratio 0.009 0.009 - HCM Control Delay (s) 8.6 7.3 0 HCM Lane LOS - A A A					SBT				
HCM Control Delay (s) 8.6 7.3 0 HCM Lane LOS A A A	Capacity (veh/h)				-				
HCM Lane LOS A A A	HCM Lane V/C Ratio	-							
	HCM Control Delay (s)								
ICM 95th %tile Q(veh) 0 0 -	HCM Lane LOS	-			Α	5.30			
	HCM 95th %tile Q(veh)		- 0	0					

	1	-	•	•	←	1	1	1	-	1	1	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	7	4		7	1		7	444		7	441	-a
Traffic Volume (vph)	39	6	37	12	5	15	46	1303	72	72	1293	43
Future Volume (vph)	39	6	37	12	5	15	46	1303	72	72	1293	43
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt	1 2 3	0.872			0.889			0.992			0.995	HE T
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1624	0	1770	1656	0	1770	5045	0	1770	5060	0
Flt Permitted	0.742			0.726		63954	0.138			0.131		
Satd. Flow (perm)	1382	1624	0	1352	1656	0	257	5045	0	244	5060	0
Satd. Flow (RTOR)		41			17			17			10	
Adj. Flow (vph)	43	7	41	13	6	17	51	1448	80	80	1437	48
Lane Group Flow (vph)	43	48	0	13	23	0	51	1528	0	80	1485	0
Turn Type	Perm	NA	- 4	Perm	NA		pm+pt	NA		pm+pt	NA	
Protected Phases		3			3		2	1		2	1	
Permitted Phases	3			3			1			1	1, 17, 24	
Total Split (s)	18.0	18.0		18.0	18.0		12.0	90.0		12.0	90.0	
Total Lost Time (s)	6.0	6.0		6.0	6.0		4.0	6.0		4.0	6.0	
Act Effct Green (s)	9.0	9.0		9.0	9.0		99.3	77.6		99.3	77.6	
Actuated g/C Ratio	0.08	0.08	100	0.08	0.08		0.83	0.65		0.83	0.65	
v/c Ratio	0.42	0.30		0.13	0.17		0.11	0.47		0.18	0.45	
Control Delay	64.4	23.7		53.2	28.8		3.1	10.9		4.2	10.8	
Queue Delay	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Total Delay	64.4	23.7		53.2	28.8		3.1	10.9		4.2	10.8	11-1
LOS	E	C		D	C		A	В		Α	В	
Approach Delay		42.9			37.6			10.7			10.5	
Approach LOS		D		No. of the last	D			В			В	
Queue Length 50th (ft)	32	5		10	4		5	161		8	156	
Queue Length 95th (ft)	70	43		30	31		12	191	ALC: N	18	185	
Internal Link Dist (ft)		57			222	-		269			300	
Turn Bay Length (ft)							165			170		
Base Capacity (vph)	138	199		135	180	Maria Sel personal de la companyone de l	461	3552		453	3561	aparago and appropri
Starvation Cap Reductn	0	0		0	0	NAME OF	0	0		0	0	
Spillback Cap Reductn	0	0		0	0		0	0		0	0	
Storage Cap Reductn	0	0		0	0		0	0		0	0	
Reduced v/c Ratio	0.31	0.24		0.10	0.13		0.11	0.43		0.18	0.42	

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.47

Intersection Signal Delay: 11.8

Intersection Capacity Utilization 52.9%

Intersection LOS: B ICU Level of Service A

Analysis Period (min) 15



	1	→	*	-	+	1	1	1	-	1	↓	1
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations	ħ	1		7	1		7	ተተጉ		7	11	18 8
Traffic Volume (vph)	42	4	36	66	4	76	72	2093	16	73	1671	44
Future Volume (vph)	42	4	36	66	4	76	72	2093	16	73	1671	44
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	0.91	0.91	1.00	0.91	0.91
Frt		0.864	14		0.857	144	3 3 3 3	0.999	10 10		0.996	
Flt Protected	0.950			0.950			0.950			0.950		
Satd. Flow (prot)	1770	1609	0	1770	1596	0	1770	5080	. 0	1770	5065	0
Flt Permitted	0.700			0.728			0.081			0.049		
Satd. Flow (perm)	1304	1609	0	1356	1596	0	151	5080	0	91	5065	0
Satd. Flow (RTOR)		40			84			2			6	
Adj. Flow (vph)	47	4	40	73	4	84	80	2326	18	81	1857	49
Lane Group Flow (vph)	47	44	0	73	88	0	80	2344	0	81	1906	0
Turn Type	Perm	NA		Perm	NA		pm+pt	NA		pm+pt	NA	
Protected Phases		3	-1-1-1		3		2	1		2	1	
Permitted Phases	3			3			1			1	le and be	
Total Split (s)	26.0	26.0		26.0	26.0		12.0	82.0		12.0	82.0	
Total Lost Time (s)	6.0	6.0		6.0	6.0		4.0	6.0		4.0	6.0	
Act Effct Green (s)	12.0	12.0		12.0	12.0		94.0	81.3		94.0	81.3	
Actuated g/C Ratio	0.10	0.10		0.10	0.10		0.78	0.68		0.78	0.68	5,
v/c Ratio	0.36	0.22		0.54	0.38		0.31	0.68		0.37	0.56	
Control Delay	56.6	18.7		65.0	15.6		14.1	13.0		27.3	10.8	2-12
Queue Delay	0.0	0.0		0.0	0.0		0.0	0.0		0.0	0.0	
Total Delay	56.6	18.7		65.0	15.6		14.1	13.0		27.3	10.8	
LOS	E	В		E	В		В	В		C	В	
Approach Delay		38.3			38.0			13.0			11.5	
Approach LOS		D			D			В			В	
Queue Length 50th (ft)	35	3		55	3		9	329		9	231	
Queue Length 95th (ft)	71	37		100	50		24	450		62	318	
Internal Link Dist (ft)		57			222			269			300	100
Turn Bay Length (ft)					44		165			170		
Base Capacity (vph)	217	301		226	336		262	3443		221	3434	
Starvation Cap Reductn	0	0		0	0		0	0		0	0	
Spillback Cap Reductn	0	0		- 0	0		0	0		0	0	
Storage Cap Reductn	0	0		0	0		0	0		0	0	
Reduced v/c Ratio	0.22	0.15		0.32	0.26		0.31	0.68		0.37	0.56	

Cycle Length: 120

Actuated Cycle Length: 120

Offset: 0 (0%), Referenced to phase 2:NBSBL and 6:, Start of Green, Master Intersection

Control Type: Actuated-Coordinated

Maximum v/c Ratio: 0.68 Intersection Signal Delay: 13.7 Intersection Capacity Utilization 68.5%

Intersection LOS: B
ICU Level of Service C

Analysis Period (min) 15



Intersection					100						
nt Delay, s/veh	3.8									3 8 3 7 7	24 A. V.
Movement		EBT	EBR		WBL	WBT		NBL	NBR		1-31-3
ane Configurations		1	No.			र्भ		W			
Traffic Vol, veh/h		42	0		43	50		0	40		
Future Vol, veh/h		42	0		43	50		0	40		A Long to the second
Conflicting Peds, #/hr		0	0		0	0		0	0		
Sign Control		Free	Free		Free	Free		Stop	Stop)	- Page
RT Channelized			None			None		THE SALE	None	NAME AND ADDRESS OF THE OWNER, THE PARTY OF THE OWNER, THE PARTY OF THE OWNER, THE PARTY OF THE OWNER, THE OWN	
Storage Length		-	-		-	4.5		0			
/eh in Median Storage, #		0	-			0		0			
Grade, %		0	-		-	0		0			
Peak Hour Factor		90	90		90	90		90	90		
Heavy Vehicles, %		2	2		2	2		2	2		a whisp
Nymt Flow		47	0		48	56		0	44		
Major/Minor		//ajor1		8.4	ajor2			Minor1			
	A STATE OF THE PARTY OF THE PAR		0	IVI		0	With the same of		47	CONTRACTOR OF STREET	E MENTAL L
Conflicting Flow All		0	0		47	0		198	47	NAS INCHES NAS INCHES	
Stage 1			-		-	-	Section 18	47		PARK BANK BANKS	
Stage 2	White the same of	-	ADDRESS OF	SISCENSION OF REAL PROPERTY.	1 12	and the same of th		151	6.00		
Critical Hdwy					4.12			6.42 5.42	6.22	The Control of the Co	200
Critical Howy Stg 1	TO STATE OF THE PARTY OF THE PA	SALUE AND A	acereno		-	-	MACHINE STATE				
Critical Hdwy Stg 2					2.218			5.42 3.518	2 210		
Follow-up Hdwy			I CONTRACTOR OF THE PARTY OF TH		1560		STATISTICS OF	791	3.318 1022		
Pot Cap-1 Maneuver				Neces III an	1300			975	1022		
Stage 1		-	-					877			
Stage 2 Platoon blocked, %				De to de la K	100		Take Tille	011			
Mov Cap-1 Maneuver					1560			766	1022		
Mov Cap-1 Maneuver					1000			766	1022		PERMIT
Stage 1				4.53	TO DE			975		NAME OF TAXABLE PARTY.	
Stage 2			Kole				SIGNATURE STATE OF	849			
Stage 2								043			
Approach		EB			WB			NB	25/25 F		
HCM Control Delay, s		0			3.4			8.7		THE YEAR	
HCM LOS			7-17				1,761	Α			
											PREMI
Minor Lane/Major Mvmt	NBLn1	EBT	EBR		WBT					DESCRIPTION OF	
Capacity (veh/h)	1022			1560	-						
HCM Lane V/C Ratio	0.043	-	-	0.031	-					1 1 1 200	CLARK
HCM Control Delay (s)	8.7		-	7.4	0						
HCM Lane LOS	Α	-	-	Α	Α						
HCM 95th %tile Q(veh)	0.1	-	-	0.1	-						

Intersection										(ABA-1510)	
Int Delay, s/veh	3.1										
Movement	9.35 64	EBT	EBR		WBL	WBT	N	IBL	NBR		
Lane Configurations		- ↑				લ		M		2 2 5	
Traffic Vol, veh/h		49	0		47	71		0	33		
Future Vol, veh/h		49	0		47	71		0	33		9
Conflicting Peds, #/hr		0	0		0	0		0	0		
Sign Control		Free	Free		Free	Free	S	top	Stop		
RT Channelized			None			None			None		
Storage Length		-	-		-	-		0	-		
/eh in Median Storage, #		0			-	0		0	-		
Grade, %		0	-		-	0		0	-		
Peak Hour Factor		90	90		90	90		90	90		
Heavy Vehicles, %		2	2		2	2		2	2		
Mvmt Flow		54	0		52	79		0	37		
Major/Minor	M	lajor1		Ma	ajor2		Min				
Conflicting Flow All		0	0		54	0	2	237	54		
Stage 1		-			-	-		54			
Stage 2		-	-		-	-		183	-		
Critical Hdwy			-		4.12			.42	6.22		
Critical Hdwy Stg 1		-	-		-	-		.42	-		
Critical Hdwy Stg 2		-			1			.42			
follow-up Hdwy		-	-		2.218	-		518	3.318		
Pot Cap-1 Maneuver					1551			751	1013		
Stage 1		-	-		-	-		969	-		
Stage 2		-			-		1	348			
Platoon blocked, %		-	-			-					
Mov Cap-1 Maneuver		-	630 50		1551			725	1013	TOTAL STATE	8
Mov Cap-2 Maneuver		-			-	-		725	-	1.00	
Stage 1		1						969	317		
Stage 2		-	V/2		-	-	8	318	-		
									i i sana		
Approach		EB			WB			NB			
HCM Control Delay, s		0			2.9			8.7			
HCM LOS		1		1777				Α		NAME AND ADDRESS OF THE OWNER, WHEN PERSON ADDRESS OF THE OWNER, WHEN PERSON AND ADDRESS OF THE OWNER, WHEN	
Minor Lane/Major Mvmt	NBLn1	EBT			WBT						
Capacity (veh/h)	1013			1551	-						
HCM Lane V/C Ratio	0.036	-	- 1	0.034	-		11-129-17	1 1		a their	
HCM Control Delay (s)	8.7	-	-	7.4	0					43.75	
HCM Lane LOS	Α	-	-	Α	Α				32.00	1500	
HCM 95th %tile Q(veh)	0.1	-		0.1	-						

Intersection							V.
Int Delay, s/veh	1.8			The second secon			
Movement	WBL	WBR		NBT	NBR	SBL	SBT
Lane Configurations	Ϋ́			1			4
Traffic Vol, veh/h	0	10		32	0	11	39
Future Vol, veh/h	0	10		32	0	11	39
Conflicting Peds, #/hr	0	0		0	0	0	0
Sign Control	Stop	Stop		Free	Free	Free	Free
RT Channelized		None	1000		The second second		None
Storage Length	0	-		_	-	-	_
Veh in Median Storage, #	0			0			0
Grade, %	0	-		0	-	-	0
Peak Hour Factor	90	90		90	90	90	90
Heavy Vehicles, %	2	2		2	2	2	2
Mvmt Flow	0	11		36	0	12	43
Major/Minor	Minor1	AAMST.		Major1		Major2	
Conflicting Flow All	104	36	3/1/1	0	0	36	0
Stage 1	36		Ten la				-
Stage 2	68		-	_	-	-	-
Critical Hdwy	6.42	6.22			200	4.12	
Critical Hdwy Stg 1	5.42			-	-	-	-
Critical Hdwy Stg 2	5.42				-		
Follow-up Hdwy	3.518	3.318		-	-	2.218	-
Pot Cap-1 Maneuver	894	1037			400	1575	
Stage 1	986	-		-	-	-	-
Stage 2	955				-		
Platoon blocked, %				-	-		-
Mov Cap-1 Maneuver	887	1037			-	1575	
Mov Cap-2 Maneuver	887	-		-	-	-	-
Stage 1	986				-		
Stage 2	947	-		-	-	-	-
						3000	
Approach	WB			NB		SB	
HCM Control Delay, s	8.5			0		1.6	
HCM LOS	Α			,			
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT	7.50		
Capacity (veh/h)		- 1037	1575				
HCM Lane V/C Ratio	-	- 0.011	0.008		- 13		11/1
HCM Control Delay (s)		- 8.5	7.3	0			
HCM Lane LOS	-	- A	Α	Α			
HCM 95th %tile Q(veh)		- 0	0	-			
now 95th %the Q(ven)		- 0	U	The state of			

ntersection	100 BE							
	1.3							Charles Tarks Vis
Movement	WBL	WBR		NBT	NBR	SBL	SBT	
ane Configurations	W			1>			4	
Traffic Vol, veh/h	0	8		41	0	12	59	
uture Vol, veh/h	0	8		41	0	12	59	
Conflicting Peds, #/hr	0	0		0	0	0	0	
Sign Control	Stop	Stop	Salari Salari Salari	Free	Free	Free	Free	The state of the s
RT Channelized		None			None		None	
Storage Length	0	-		-	-	-	-	
eh in Median Storage, #	0			0		-	0	
Grade, %	0	-	CHOICE STATE OF THE PARTY OF TH	0	-	-	0	
eak Hour Factor	90	90		90	90	90	90	
leavy Vehicles, %	2	2		2	2	2	2	7 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1
Nymt Flow	0	9	SSE	46	0	13	66	
							No Tea	de la
Major/Minor	Minor1		A SHEY	Major1	YAS ASS	Major2	FSS	the same and the same of the s
Conflicting Flow All	138	46	CALLEGE CO.	0	0	46	0	
Stage 1	46	40				40		
Stage 2	92				nenzirelen		-	antiga itusiga espanting parangan kanadan kanadan kanadan kanadan kanadan kanadan kanadan kanadan kanadan kanad
Critical Hdwy	6.42	6.22		1 5 2 D 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1		4.12		
Critical Hdwy Stg 1	5.42	0.22			-	-		EN BOOK HAI ON DE PROGRAMMENT DE PRESENTATION DE PRO
Critical Hdwy Stg 2	5.42	ARGISTINGE						
follow-up Hdwy	3.518	3.318	EMANGES OF		-	2.218	-	PER
ot Cap-1 Maneuver	855	1023			103.31	1562		以此地的政策和任何对对对自己的
Stage 1	976	-	RMANUSISA		-	-	-	NEW THE PROPERTY AND ASSESSMENT OF THE PROPERTY OF THE PARTY OF THE PA
Stage 2	932				111111			医结节性成功的第三人称形式
Platoon blocked, %	002			-	_		- Indian	Asset with the burner as a standard and an arministra
Nov Cap-1 Maneuver	847	1023			200	1562		
Nov Cap-2 Maneuver	847	-			autore res	-	-	
Stage 1	976			1000				
Stage 2	924	Anthe secondon to here of	EIRORE		_		-	normal me analysis for a surface about the second
Rail Market Control								
Innroach	WB			NB		SB		
Approach	8.6		Para de la	0	25 0000	1.2	(USALE)	
HCM Control Delay, s HCM LOS	6.6 A			U	Description of the last of the	1.2	Hersian.	
TOW LOS	A						THE REAL	
Minor Lane/Major Mvmt	NBT	NBRWBLn1	SBL	SBT			TO BE SEE	
	NDI	- 1023	1562	-			HO IS	
Capacity (veh/h) HCM Lane V/C Ratio		- 0.009		CONTROL MONITORING CONTROL CONTROL	STERNIE .			
		- 8.6	7.3	0	NAME OF THE			SINCE AND ADDRESS OF THE STATE
ICM Control Delay (s) ICM Lane LOS		AND DESCRIPTION OF THE PROPERTY OF	7.5 A	A				
IOINI FUILE FOO	-	- A	A	A				

APPENDIX G
HISTORIC COLLISION DATA



CITY OF SCOTTSDALE

'13 -'14 COLLISION SUMMARY

REPORT#	DATE TIME YYMMDD HHMM	NORTH / SOUTH ST.	TYPE	EAST WEST ST.	TYPE	DIR FROM	DIST	INJ. : #1	SEV. PI #2 #			VIOI #1	#2			TRAN		MANNER OF COLLISION	COMMENTS
14-21436	141005 1514	SCOTTSDALE	RD	ROSE	LN	AT		1	3	0	0	99	99	4	1	WB	NB	3	
14-18257	140824 1356	SCOTTSDALE	RD	ROSE	LN	AT		1	1	0	0	2	1	1	3	SB	SB	4	
14-15723	140721 1100	SCOTTSDALE	RD	ROSE	LN	N	50	1	1	0	0	2	1	1	3	SB	SB	4	
14-14627	140705 1044	SCOTTSDALE	RD	ROSE	LN	AT		1	1	0	0	12	1	8	1	SB	SB	6	
13-26293	131114 1806	SCOTTSDALE	RD	ROSE	LN	AT		3	3	97	0	97	1	4	1	SB	NB	3	
13-01811	130124 1920	SCOTTSDALE	RD	ROSE	LN	AT		1	1	0	0	6	1	5	1	NB	NB	2	

KEY

INJURY SEVERITY: 1=NO INJURY, 2=POSSIBLE INJURY, 3=NON-INCAPACITATING INJURY, 4=INCAPACITATING INJURY, 5=FATAL INJURY, 99=NOT REPORTED / UNKNOWN PHYSICAL CONDITION: 0=NO APPARENT INFLUENCE, 1=ILLNESS, 2=PHYSICAL IMPAIRMENT, 3=FELL ASLEEP / FATIGUED 4=ALCOHOL, 5=DRUGS, 6=MEDICATIONS. A=NO TEST GIVEN. B=TEST GIVEN. C=TEST REFUSED. D=TESTING UNKNOWN, 97=OTHER, 99=UNKNOWN

VIOLATION: 1=NO IMPROPER ACTION, 2=SPEED TOO FAST FOR CONDITIONS, 3=EXCEEDED LAWFUL SPEED 4=FOLLOWED TOO CLOSELY. 5=RAN STOP SIGN, 6=DISREGAREDED TRAFFIC SIGNAL7=MADE IMPROPER TURN, 8=DROVE/RODE IN OPPOSING TRAFFIC LANE, 9=KNOWINGLY OPERATED WITH FAULTY / MISSING EQUIPMENT, 10=REQUIRED MOTORCYCLE SAFETY EQUIPMENT NOT USED, 11=PASSED IN NO PASSING ZONE, 12=UNSAFE LANE CHANGE, 13=FAILED TO KEEP IN PROPER LANE, 14=DISREGARDED PAVEMENT MARKINGS, 15=OTHER UNSAFE PASSING, 16=INATTENTION/DISTRACTION, 17=DID NOT USE CROSSWALK, 18=WALKED ON WRONG SIDE OF ROAD, 19=ELECTRONIC COMMUNICATIONS DEVICE, 20=FAILED TO YIELD RIGHT OF WAY (added August 2014), 97=OTHER, 99 UNKNOWN

ACTION: 1=GOING STRAIGHT AHEAD, 2=SLOWING IN TRAFFICWAY, 3=STOPPED IN TRAFFICWAY, 4=MAKING LEFT TURN, 5=MAKING RIGHT TURN, 6=MAKING U-TURN, 7=OVERTAKING/PASSING, 8=CHANGING LANES, 9=NEGOTIATING A CURVE, 10=BACKING, 11=AVOIDING VEH/OBJ/PED/CYCLIST/ANIMAL, 12=ENTERING PARKING POSITION, 13=LEAVING PARKING POSITION, 14=PROPERLY PARKED, 15=IMPROPERLY PARKED, 16=DRIVERLESS MOVING VEHICLE, 17=CROSING ROAD, 18=WALKING WITH TRAFFIC, 19=WALKING AGAINST TRAFFIC, 20=STANDING, 21=LYING, 22=GETTING ON OR OFF VEHICLE, 23=WORKING ON/PUSHING VEHICLE, 24=WORKING ON ROAD, 97=OTHER, 99=UKNOWN

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CITY OF SCOTTSDALE

'15 -'16 COLLISION SUMMARY

REPORT#	DATE TIME YYMMDD HHMM	NORTH / SOUTH ST.	TYPE	EAST WEST ST.	TYPE	DIR FROM	DIST FROM	INJ. #1	SEV. P #2 #			VIOLA #1		ACTI #1		TRA		MANNER OF COLLISION	COMMENTS
15-27479	151215 1850	SCOTTSDALE	RD	ROSE	LN	AT		1	1	0	0		1	1	2	SB	SB	4	
15-23337	151026 1232	SCOTTSDALE	RD	ROSE	LN	AT		99	1	99	0	13	1	7	1	NB	NB	6	HIT AND RUN
15-21810	151006 1909	SCOTTSDALE	RD	ROSE	AV	AT		1	1	4	0	12	1	8	1	SB	SB	6	DUI
15-18347	150821 2105	SCOTTSDALE	RD	ROSE	AV	AT		99	1	99	0	15	1	5	4	NB	NB	6	HIT AND RUN
15-06554	150320 1312	SCOTTSDALE	RD	ROSE	LN	AT		4	2	0	0	20	1	4	1	SB	NB	5	
15-03412	150209 1453	SCOTTSDALE	RD	ROSE	LN	AT		2	3	0	0	7	1	4	1	SB	NB	3	MULTI VEH 3

KEY

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TOTAL

CITY OF SCOTTSDALE

'13 -'14 COLLISION SUMMARY

REPORT#	DATE TIME YYMMDD HHMM	NORTH / SOUTH ST.	TYPE	EAST WEST ST.	TYPE	DIR FROM	DIST FROM	INJ. #1	SEV. PH #2 #1				LATION #2			TRA #1		MANNER OF COLLISION	COMMENTS
14-05683	140311 1745	SCOTTSDALE	RD	ROSE	LN	S	300	1	1	0	0	2	1	2	3	SB	SB	4	
14-01919	140124 1231	SCOTTSDALE	RD	ROSE	LN	S	470	1	3	0	0	2	1	1	3	NB	NB	4	MULTI VEH 3
14-01918	140124 1304	SCOTTSDALE	RD	ROSE	LN	S	486		1	0	0	1	1	1	3	NB	NB	4	
13-28137	131207 1201	SCOTTSDALE	RD	ROSE	LN	N	277	1	3	0	0	97	1	8	1	SB	SB	6	
13-10788	130508 1805	SCOTTSDALE	RD	ROSE	LN	N	647	1	1	0	0	12	1	8	1	SB	SB	6	
13-02496	130201 1800	SCOTTSDALE	RD	ROSE	LN	S	200	1	1	0	0	2	1	1	1	NB	NB	4	MULTI VEH 3
13-00242	130104 0305	SCOTTSDALE	RD	ROSE	LN	S	350	1	4	4	0	2	1	1	97	NB	NB	4	PEDICAB

KEY

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CITY OF SCOTTSDALE

'15 -'16 COLLISION SUMMARY

REPORT#	DATE TIME YYMMDD HHMM	NORTH / SOUTH ST.	TYPE	EAST WEST ST.	TYPE		DIST		SEV. #2	PHYS. (COND. 2		TION #2	ACT #1	ION #2	TR/ #1	W. DIR	MANNER OF COLLISION	COMMENTS
15-19136	150901 1404	SCOTTSDALE	RD	ROSE	LN	N	250	1	2	0	0	2	1	1		3 SB	SB	4	
15-08319	150410 1900	SCOTTSDALE	RD	ROSE	LN	N	240	99	1	99	0	99	1	1		3 SB	SB	4	HITA ND RUN

KEY

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TOTAL

APPENDIX C.1
EXISTING



COTTONWOODS RESORT & SUITES MARICOPA, ARIZONA

LOCATED AT 6160 N SCOTTSDALE RD PARADISE VALLEY, ARIZONA 85253

MASTER DRAINAGE REPORT AUGUST 2017 Project No.: 16143

PREPARED FOR:

PV HOTEL VENTURES SPE, LLC 4858 E. BASELINE RD., SUITE 101 MESA, AZ 85206

PREPARED BY:

HUBBARD ENGINEERING
1201 S. ALMA SCHOOL Rd., SUITE 12000
MESA, ARIZONA 85210
(480) 892-3313
BRENT STEFFENHAGEN, PE



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Plan #		
Case # _ 22 - 3	ZN-2	016
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Accepted		
Viccepted		
Corrections		
	9/1	2/17

22-ZN-2016 08/24/2017

9-GP-2016 08/24/2017





WARNING & DISCLAIMER OF LIABILITY

The Drainage and Floodplain Regulations and Ordinances of the City of Scottsdale are intended to "minimize the occurrence of losses, hazards and conditions adversely affecting the public health, safety and general welfare which might result from flooding caused by the surface runoff of rainfall" (Scottsdale Revised Code §37-16).

As defined in S.R.C. §37-17, a flood plain or "Special flood hazard area means an area having flood and/or flood related erosion hazards as shown on a FHBM or FIRM as zone A, AO, A1-30, AE, A99, AH, or E, and those areas identified as such by the floodplain administrator, delineated in accordance with subsection 37-18(b) and adopted by the floodplain board." It is possible that a property could be inundated by greater frequency flood events or by a flood greater in magnitude than a 100-year flood. Additionally, much of the Scottsdale area is a dynamic flood area; that is, the floodplains may shift from one location to another, over time, due to natural processes.

WARNING AND DISCLAIMER OF LIABILITY PURSUANT TO S.R.C §37-22

"The degree of flood protection provided by the requirements in this article is considered reasonable for regulatory purposes and is based on scientific and engineering considerations. Floods larger than the base flood can and will occur on rare occasions. Floodwater heights may be increased by manmade or natural causes. This article (Chapter 37, Article II) shall not create liability on the part of the city, any officer or employee thereof, or the federal government for any flood damages that result from reliance on this article or any administrative decision lawfully made thereunder."

Compliance with Drainage and Floodplain Regulations and Ordinances does not insure complete protection from flooding. The Floodplain Regulations and Ordinances meet established local and federal standards for floodplain management, but neither this review nor the Regulations and Ordinances take into account such flood related problems as natural erosion, streambed meander or man-made obstructions and diversions, all of which may have an adverse affect in the event of a flood. You are advised to consult your own engineer or other expert regarding these considerations.

I have read and understand the above. If I am an agent for an owner I have made the owner aware of and explained this disclaimer.

Plan Check No.

Owner or Agent Date

AVANCIZED SIGNATURE

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APPENDICES

Appendix A Retention Calculations

Appendix B Rainfall data

EXHIBITS

Exhibit 1 Aerial Site Map

Exhibit 2 Pre Development Aerial Ground Cover Map Post Development Aerial Ground Cover Map Exhibit 3

Existing Site Drainage Map Exhibit 4 Existing Site Topographic Map Exhibit 5

Preliminary Grading Plan Exhibit 6



1. INTRODUCTION AND SCOPE OF WORK

This report presents the results of a *Master Drainage Study* conducted by Hubbard Engineering at the request of Delawie ("client"), for Cottonwoods Resort & Suites ("site"). The purpose of this report is to provide a hydrologic and hydraulic evaluation for the site so that the site can be rezoned. This report addresses on-site conditions as well as storm water runoff retention.

1.1 Site Description

The site is located in Section 10 of Township 2N, Range 4E of the Gila and Salt River Base and Meridian, Maricopa County, Arizona. The location of the site is shown on the site *Vicinity Map*, **FIGURE 1**, on the next page.

1.2 Project Description

The site was previously developed with an existing building with water service connections, sewer service connections, asphalt paved parking lot, concrete sidewalk, concrete curb, block site wall, landscape areas and a surface retention basin that has grass for ground cover. The adjacent half streets to the site are fully developed. The existing building on the site was demoed however, the existing paved parking lot remains along with the existing surface retention basin along Scottsdale Road. There are no offsite flows onto the existing site.

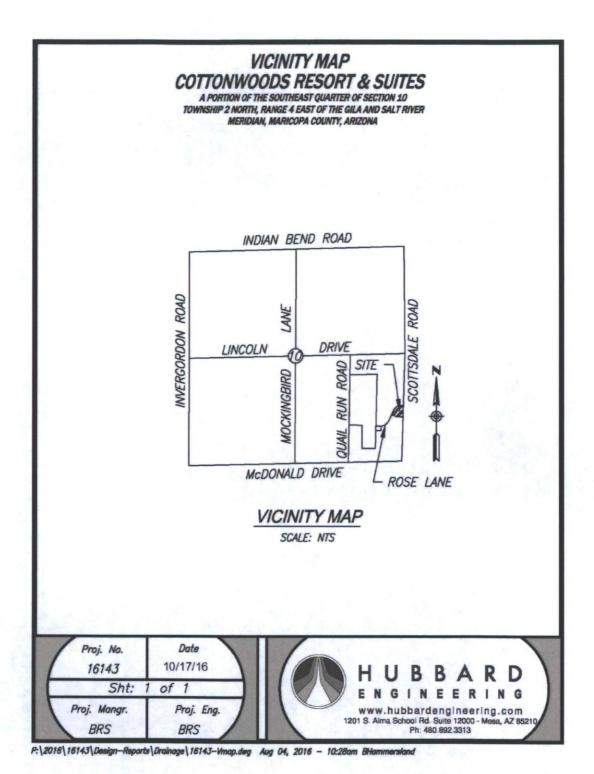


Figure 1 – Vicinity Map

1.3 Design Criteria

The criteria used in the drainage design and analysis of the site was established using the guidelines as described in the following:

- ➤ Design Standards & Policies Manual Chapter 4 Grading and Drainage, City of Scottsdale, Dated January, 2010. (Reference 1).
- Drainage Design Manual for Maricopa County, Arizona, Volume I, Hydrology (Reference 2).
- Drainage Design Manual for Maricopa County, Arizona, Volume II, Hydraulics (Reference 3).

2. DESCRIPTION OF EXIST. DRAINAGE COND. & CHARACTERISTICS

2.1 Onsite Drainage

As previously mentioned, the site was previously developed with an existing building with water service connections, sewer service connections, asphalt paved parking lot, concrete sidewalk, concrete curb, block site wall, desert landscape areas and a surface retention basin that has grass for ground cover. The adjacent half streets are fully developed. The existing building on the site was recently demoed however, the existing paved parking lot remains along with the existing surface retention basin along N. Scottsdale Road.

A pre-vs-post drainage analysis was done on the existing site. The analysis represents the previous site condition with the building and the post (future) site conditions with future buildings locations and proposed ground cover. The future conceptual site layout is very similar to pre-project site layout. All ground cover areas will stay the same as the pre site conditions. The existing site has one drainage area DA-A which is shown in **Exhibit 4**. DA-A drains to the existing retention basin along Scottsdale Rd via sheet flow. The demolition of the existing building included the concrete slab of the building. A C-value of 0.95 was used for impervious areas and a C-value of 0.30 was used for grass areas. See **Exhibits 2 & 6** for pre-vs-post ground cover delineation areas. See **Section 2.5** for additional information on pre-vs-post drainage analysis. See **Exhibit 1** for Aerial Site Map, **Exhibit 5** for existing site topography.

In accordance with the requirements of the City of Scottsdale Design Standards & Policies Manual, the subject property will be required to retain the 100-year, 2-hour runoff volume, which is determined by utilizing the following formula:

$$V = C * (P/12) * A$$

where,

V = Storage volume (acre-feet)

C = Watershed runoff coefficient

P = 100-year, 2-hour precipitation (inches)

A = Drainage area (acres)

According to the City of Scottsdale Design Standards & Policies Manual, the 100-year, 2-hour depth is 2.2 inches for the site area. See **Appendix B** for NOAA rainfall data.

A "weighted" C-value is determined for each drainage area by utilizing the formula:

$$Cw = A_1 * C_1 + A_2 * C_2 + A_3 * C_3 \dots A_n * C_n$$

$$A_1 + A_2 + A_3 \dots A_n$$

where,

 A_i = Area in the i_{th} sub-area (acres)

 C_i = Runoff coefficient in the i_{th} sub-area

As identified in Figure 4.1-4 of the City of Scottsdale Design Standards & Policies Manual, the following "C" values will be used in the retention calculations:

Land Use Category	100-year max. "C" value
Pavement and Rooftops (Impervious Areas)	0.95
Landscape (no impervious weed barrier)	0.45
Lawns, golf course & parks (grassed areas)	0.30

The volume provided in the proposed retention basins is calculated by using the prismoidal formula:

$$V = d/3 * (A_1 + A_2 + (A_1 * A_2)^{0.5})$$

where,

V = Storage volume (cu.ft.)

d = Depth(ft)

 A_1 = Area of upper contour (sq.ft.)

 A_2 = Area of lower contour (sq.ft.)

The volume of the existing retention basin was determined by using the prismoidal formula. See **Table 1** below for the existing retention basin volume.

Table 1: Existing Basin Volume

	EXISTING RETENTION BASIN										
Drainage Area	HW Elevation (ft)	HW Area	Bottom Elevation (ft)	Bottom ft ²	H ft	Volume Provided ft ³	Drainage Areas contributing to Basins				
RBI	1302.25	14,000.00	1300.25	680.00	2	11,844	DA-A				
					Total ->	11,844					

14,000.00

<= Total Area @ H.W.'s

Volume Provided = $H/3*(A_{H.W.} + A_{BOTTOM} + (A_{H.W.} * A_{BOTTOM})^{0.5})$

In accordance with the City of Scottsdale Drainage Ordinance, retention basins are required to be drained within a 36-hour period after the storm event.

There is an existing drywell located in the existing retention basin that currently assists in the dissipation of the water to drain within the required 36-hours. See **Exhibit 2 & 6** for drywell location. When the property is developed in the future a Final Drainage Report will need to be submitted along with the Improvement Plans to verify that the proposed site will not require additional storage than what is currently provided by the existing basin and if additional drywell or drywells need to be added to drain the water within the required 36-hours.

Drainage calculations can be found at the end of this drainage study.

2.2 Existing Off-Site Conditions Characteristics

There are no existing offsite flows that inundate the existing site.

2.3 Flood Zone Information

The Maricopa County, Arizona and Incorporated Areas Flood Insurance Rate Map (*F.I.R.M.*) number 04013C1770L panel number 1770 of 4425, dated October 16, 2013 indicates that the project falls within Zone X. A Copy of the FEMA Firmette map can be found in **FIGURE 2**.

Zone X is defined by the Federal Emergency Management Agency (FEMA) as:

"Areas determined to be outside the 0.2% annual chance floodplain."



Figure 2 – FIRM

2.4 Pre- and Post-Project Topography

The pre and post project topography will be very similar since they will maintain the same drainage scheme and drain to the same existing basin. See **Exhibit 5 & 6** for existing site topography map and the preliminary grading plan.

2.5 Pre- and Post-Project Stormwater Runoff

The entire drainage area DA-A shown in **Exhibit 4** will drain to the existing retention basin RB-1 located along Scottsdale Road. The site was determined to have one drainage area and **Exhibit 4** is labeled accordingly. The runoff from DA-A will drain to RB-1 via sheet flow. The existing basin RB-1 is 2 feet in depth and has a capacity of approximately 11,844 cubic feet. For the pre-condition drainage analysis, it was determined that the required volume that the retention basin must provide per City of Scottsdale's *Design Standards and Policies Manual* (Reference 1) was 7,646 cubic feet. The post-condition drainage analysis determined that the required volume the retention basin must also provide the same as the precondition 7,646 cubic feet of water. The sidewalk adjacent to N. Scottsdale Road will be realigned to the

west and take away a portion of the volume being provided by the existing RB-1. The existing retention will need to be regraded as shown in the preliminary grading plans. The proposed basin is designed to provide 7,656 cubic feet of storage. See **Appendix A** for retention calculations. The proposed basin volume being provided will be adequate for the proposed post site conditions. The existing basin also has an existing drywell incorporated in the bottom of the basin. With the existing RB-1 being reduced in size the existing drywell will need a catch basin or an interceptor located at the bottom of the new retention basin, so that the basin drains within the permitted time of 36 hours. See **Appendix A** pre vs post calculations.

3. SPECIAL CONDITIONS

3.1 Section 404 & 401

The site is not delineated as a 404 & 401 jurisdiction.

3.2 AZPDES

When the future site is regraded an AZPDES permit will be required for improvements since the land disturbed will be more than one acre. An NOI will be submitted to ADEQ prior to and an approved NOI Certification with an AZCON number. The approved AZCON will be provided to the City at the time of the final plan review.

3.3 ESL

The site does not qualify as an Environmentally Sensitive Land on the City of Scottsdale Environmentally Sensitive Land Inventories.

4. DATA ANALYSIS METHODS

4.1 Peak Flows and Stormwater Storage

Storage for the 100-year, 2-hour and peak flow for the 100-year storm was determined by rational method per COS Requirements. See the associated Appendices for the references and parameters that were used to calculate the storm water required retention.

5. SUMMARY AND CONCLUSION

- The project is bound by N. Scottsdale Rd to the east, Rose Ln. to the west and north and by condos on the south side.
- Any future development on the site must abide by the City of Scottsdale's Design Standards & Policies Manual.
- The proposed surface retention basin will provide adequate storage volume for the proposed post site condition per City of Scottsdale's Design Standards & Policies Manual.
- The site will covey the 100-yr storm event via surface flow into the existing retention basin along N. Scottsdale Road.
- The post conceptual site will have the same drainage area and drainage scheme.
- Subject site is currently located in Flood Plain Zone X per FEMA No. 04013C1770L.

6. REFERENCES

- 1. Design Standards & Policies Manual Chapter 4 Grading and Drainage, City of Scottsdale, Dated January, 2010.
- 2. Drainage Design Manual For Maricopa County, Arizona, Volume I, Hydrology, Flood Control District Of Maricopa County, February 2013.
- 3. Drainage Design Manual For Maricopa County, Arizona, Volume II, Hydraulics, Flood Control District Of Maricopa County, January 2013. Flood Insurance Rate Map (F.I.R.M.) Maricopa County, Arizona and Incorporated areas, Panel 1770 of 4425

7. LIMITATIONS

This report is focused on providing practical design information, evaluation, and calculations for statistical flood events up to and including the 100-year frequency flood. The procedures used herein are derived from, and performed with, currently accepted engineering methodologies and practices. Additionally, the criteria for this evaluation is designed to conform to currently applicable ordinances, regulations and policies effected by the appropriate jurisdictional regulatory authorities for the site.

The analysis presented herein focuses on developing design estimates of storm water runoff resulting from a statistical evaluation of storm events of particular duration and frequency up to and including a 100-year frequency event. A storm event exceeding the 100-year frequency event may cause or create the risk of greater flood impact than is addressed and presented herein. However, the scope of this assessment does not include evaluation of storm water runoff resulting from storm events exceeding the 100-year frequency event. Hubbard Engineering assumes no responsibility for actual flood damage, increased risks of flood damage, or increased construction or development cost resulting from or related to any such events. Nor shall Hubbard Engineering be responsible for any changes in, or additions to, regulatory requirements which may result from, or be related to, any such events or changes in hydrologic or hydraulic conditions within the watershed.

In performing the services contained herein, Hubbard Engineering has received or will receive information prepared or compiled by others. Hubbard Engineering, as engineering professionals, are not required to verify the information, but may rely on the information unless actual knowledge concerning the validity of the information is known or is obvious to the professional. Therefore, Hubbard Engineering is entitled to rely upon the accuracy and completeness of this information without independent evaluation or verification.

POST Composite "C" Calculation **Hubbard Engineering** Project No. 16143

Project Name: Cottonwoods Resort

Prepared By: BAH

Date: 08/22/17

Project No: 16143

Checked By:

Date:

Purpose: Calculate a weighted "C" Value for a drainage area.

Methodology: The weighted "C" value is determined by summing the products of each surface "C" value

times the suface area, and dividing by the sum of all of the surface areas.

References: 1. Scottsdale Drainage Design Policy

Calculation: $Cw = (C_{0.95} * A_{0.95} + C_{0.45} * A_{0.45})/A_{TOTAL}$

Surface	C	Area (Sq. Ft.)	C x Area
Landscape	0.45	10,423	4,690
Grassed Areas	0.30	7,200	2,160
Impervious	0.95	36,537	34,710
Total	N/A	54,160	41,561

" $Cw'' = 0.77$	Weighted Runoff Coefficient	

Post Retention Calculations Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort

Project No.: 16143

Prepared by: BAH Revised By:

Date: 08/22/17

Purpose: Evaluate the required and provided retention volumes in order to assess conformance to project criteria.

Methodology: Calculate the volume of stormwater required to be retained using City of Scottsdale criteria. Calculate the estimated volume of stormwater retained using retention basin geometry.

Criteria: Retain the calculated stormwater run-off for the 100-YEAR 2-HOUR duration storm event.

References: 1. Scottsdale Drainage Design Policy
2. Drainage Design Manual for Maricopa County, Arizona, Volume II: Hydraulics, August 2013.

Calculations: Volume Required = C_{Composite} *D/12* A [ft³]

(Reference 1)

D = 2.2

[in] (Paved Parking)

(Reference 1) (Reference 1)

C = 0.95 C = 0.30 C = 0.45

(Grassed Areas) (Desert Landscape) (Reference 1)

Composite C= (C1*A1 + C2*A2...+...)/(A1+A2+...)

Volume Required = Composite C*P/12*A

Results:

Identifiers	CALCULATE R	ETENTION VOLUME REQUIRED	Volu	me
Contributory	Area	C Post	Requi	ired
Area ID	[acres]		[acre-ft]	[ft³]
DA-A	1.24	0.77	0.18	7,646
Total Area:	1.24	TOTAL VOLUME REQUIRED:	0.18	7,646

Pre Composite "C" Calculation Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort Project No: 16143 Prepared By: BAH

Date: 08/22/17

Checked By:

Date:

Purpose: Calculate a weighted "C" Value for a drainage area.

Methodology: The weighted "C" value is determined by summing the products of each surface "C" value

times the suface area, and dividing by the sum of all of the surface areas.

References: 1. Scottsdale Drainage Design Policy

Calculation: $Cw = (C_{0.95} * A_{0.95} + C_{0.45} * A_{0.45})/A_{TOTAL}$

Surface	C	Area (Sq. Ft.)	C x Area
Grassed Areas	0.30	9,904	2971.20
Landscape	0.45	6,743	3034.35
Impervious	0.95	37,513	35637.35
Total	N/A	54,160	41642.90

"Cw" = 0.77	Weighted Runoff Coefficient	

Pre Retention Calculations Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort

Project No.: 16143

Prepared by: BAH

Revised By:

Date: 08/22/17

Purpose: Evaluate the required and provided retention volumes in order to assess conformance to project criteria.

Methodology: Calculate the volume of stormwater required to be retained using City of Scottsdale criteria. Calculate the estimated volume of stormwater retained using retention basin geometry.

Criteria: Retain the calculated stormwater run-off for the 100-YEAR 2-HOUR duration storm event.

References: 1. Scottsdale Drainage Design Policy
2. Drainage Design Manual for Maricopa County, Arizona, Volume II: Hydraulics, August 2013.

Calculations: Volume Required = C_{Composite} *D/12* A [ft³]

(Reference 1)

D = 2.2

(Reference 1)

C = 0.95 C = 0.30 C = 0.45

(Paved Parking)

(Reference 1)

(Grassed Areas)

(Reference 1)

(Desert Landscape)

Composite C= (C1*A1 + C2*A2...+...)/(A1+A2+...)

Volume Required = Composite C*P/12*A

Results:

Identifiers	CALCULATE RETENTION VOLUME REQUIRED		Volume	
Contributory	Area	C PRE	Required	
Area ID	[acres]		[acre-ft]	[ft³]
DA-A	1.24	0.77	0.18	7,646
Total Area:	1.24	TOTAL VOLUME REQUIRED:	0.18	7,646

Retention Basin

Retention Provided Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort

Project No.: 16143

Prepared By: BAH
Revised By:

Date: 08/22/17

Date:

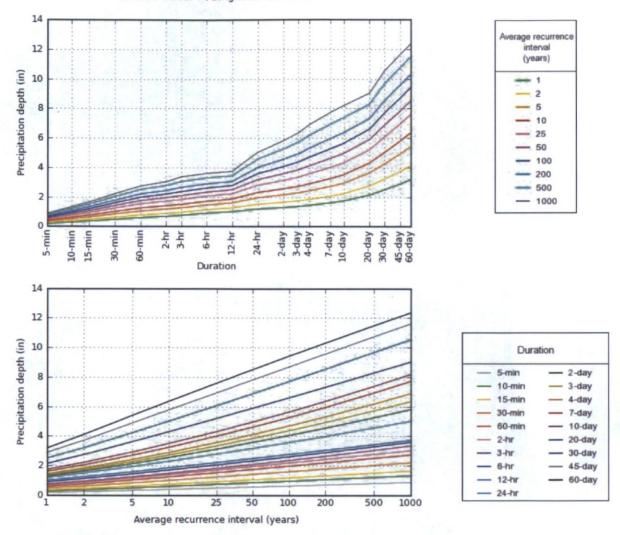
RETENTION BASINS						
Drainage Area	HW Area	Bottom ft²	H ft	Volume Provided ft ³	Drainage Areas contributing to Basins	
RB1	5,833.00	3,622.55	1	4,684	DA-A	
Samuel and	3,622.55	1,511.50	1	2,491	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	
	1,511.50	500.00	0.5	480		
			Total ->	7,656		

10,967.05 <= Total Area @ H.W.'s

Volume Provided = H/3* $(A_{H.W.} + A_{BOTTOM} + (A_{H.W.} * A_{BOTTOM})^{0.5})$

PF graphical



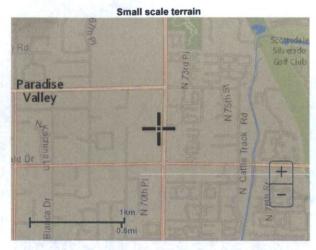


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Maps & aerials









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US Department of Commerce

National Oceanic and Atmospheric Administration

National Weather Service

National Water Center

1325 East West Highway

Silver Spring, MD 20910

QuestihbDhS:C:Questions@noaa.gov

Discl ai mer

22-ZN-2016 08/24/2017

9-GP-2016 08/24/2017





GROUND COVER DELINEATION

DRAINAGE AREA

DRAINAGE AREA ID DA-A

GROUND COVER TYPE "IMPERVIOUS"

GROUND COVER TYPE "GRASS"

GROUND COVER TYPE "LANDSCAPE"

Surface	C	Area (Sq. Ft.)	C x Area
Grassed Areas	0.30	9,904	2971.20
Landscape	0.45	6,743	3034.35
Impervious	0.95	37,513	35637.35
Total	N/A	54,160	41642.90

"Cw"= 0.77 Weighted Runoff Coefficient

Retention Volumes

Vrpre=7,646 C.F. Vp=11,844 C.F.





Proj. No. Date
16143 08/22/17
Sht: 1 of 1

PRE-DEVELOPMENT AERIAL GROUND COVER MAP EXHIBIT 2

A PORTION OF THE SOUTHEAST QUARTER OF SECTION 10 TOWNSHIP 2 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER MERIDIAN, MARICOPA COUNTY, ARIZONA



HUBBARD¹¹
ENGINEERING

1201 S. Alma School Rd. Suite 12000 Mesa, AZ 85210 Pb: 480 892 3313

www.hubbardengineering.com

GROUND COVER DELINEATION

DRAINAGE AREA

DRAINAGE AREA ID

DA-A



GROUND COVER TYPE "DESERT LANDSCAPE"

GROUND COVER TYPE "IMPERVIOUS"



GROUND COVER TYPE "GRASS"

Surface	C	Area (Sq. Ft.)	C x Area
Landscape	0.45	10,423	4,690
Grassed Areas	0.30	7,200	2,160
Impervious	0.95	36,537	34,710
Total	N/A	54,160	41,561

"Cw"= 0.77 Weighted Runoff Coefficient

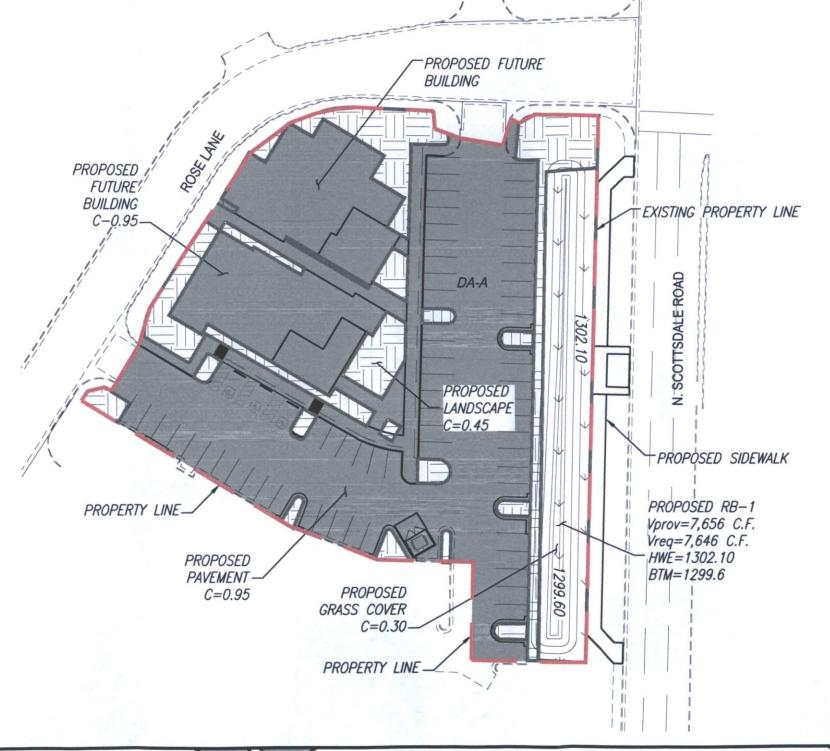
Retention Volumes

Vrpre=7,646 C.F.

Vrpost=7,646 C.F.

Vp=7,656 C.F.





Proj. No. Date

16143 08/22/17

Sht: 1 of 1

POST DEVELOPMENT AERIAL GROUND COVER MAP

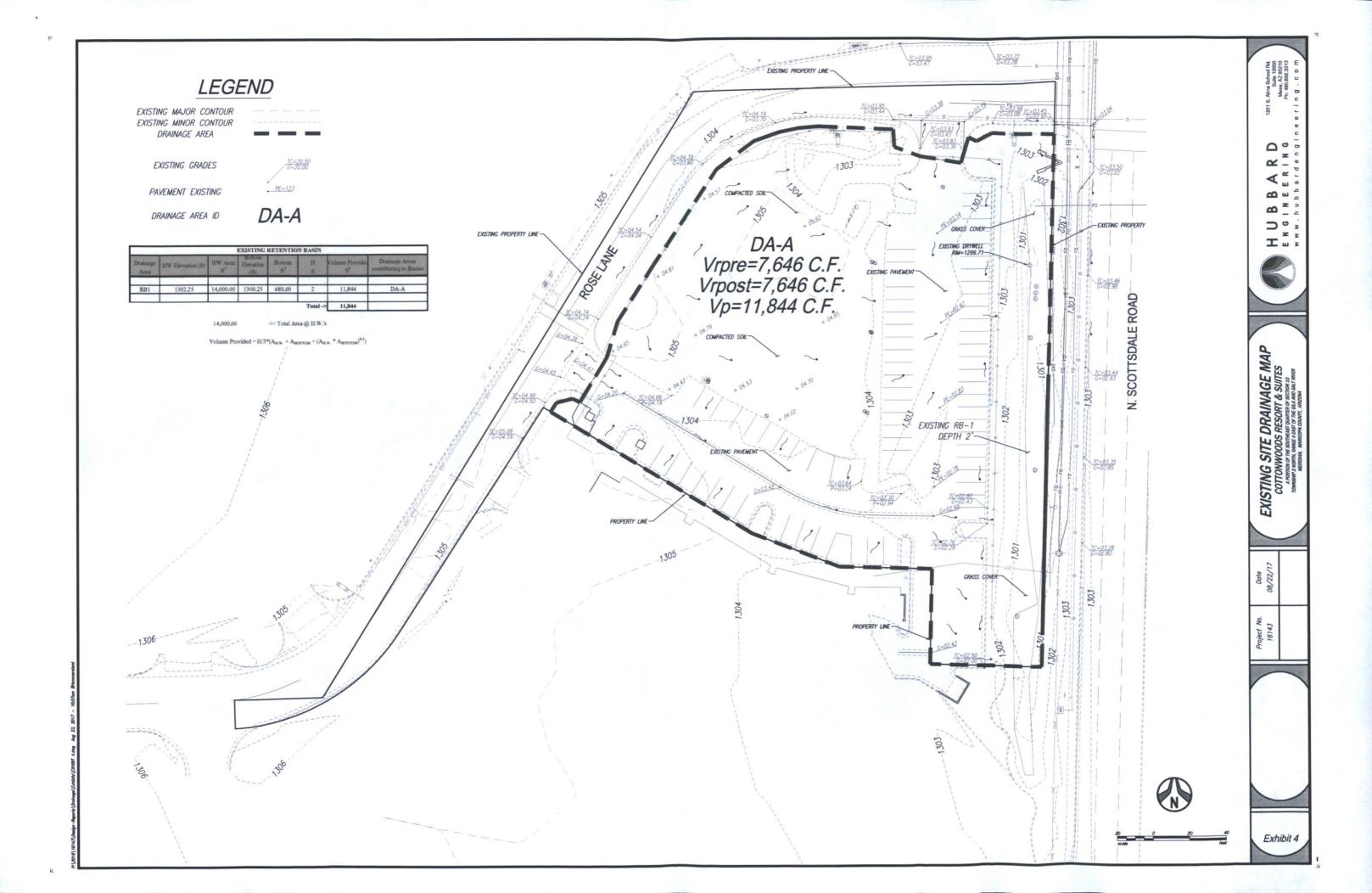
A PORTION OF THE SOUTHEAST QUARTER OF SECTION 10 TOWNSHIP 2 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER MERIDIAN, MARICOPA COUNTY, ARIZONA

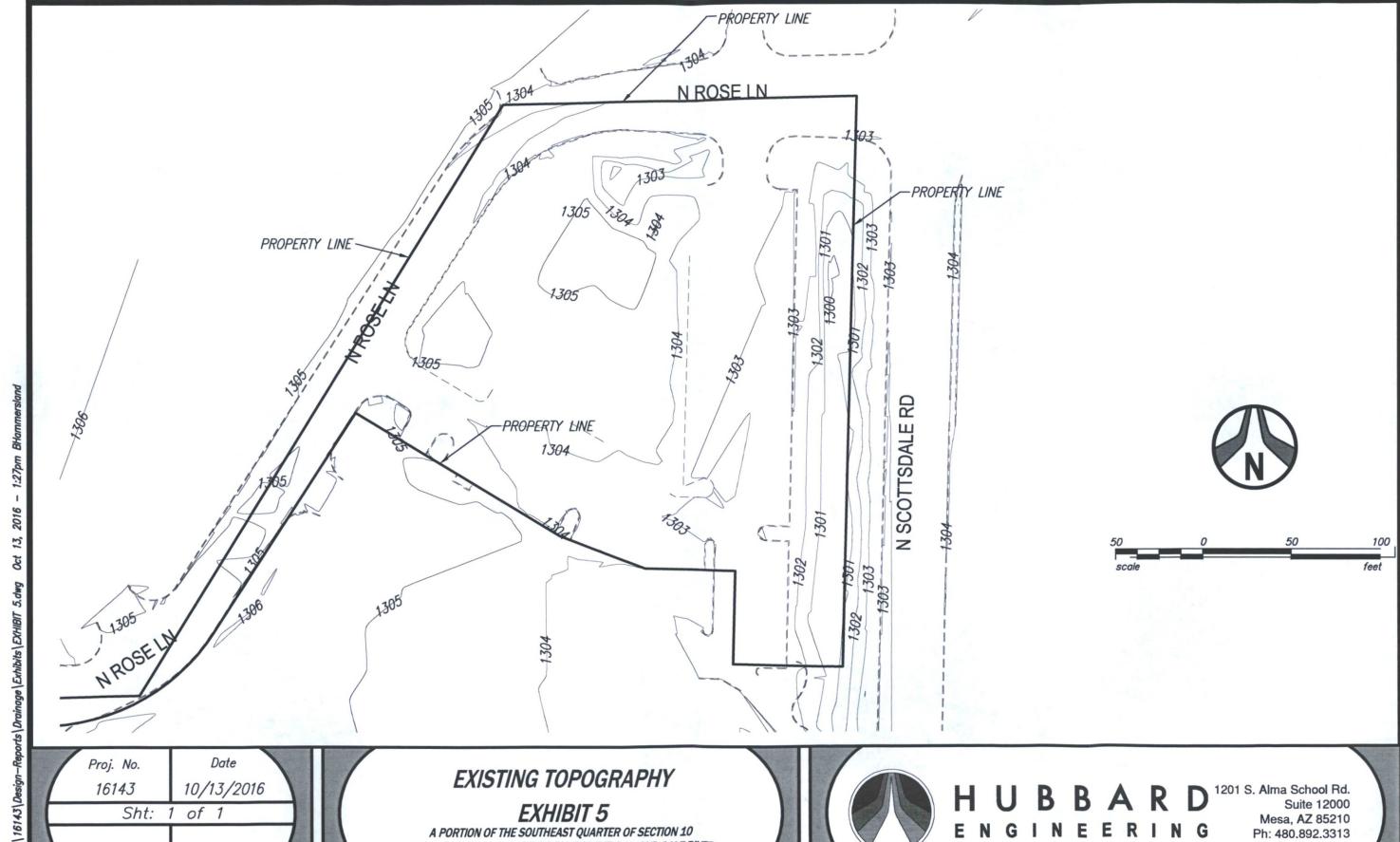


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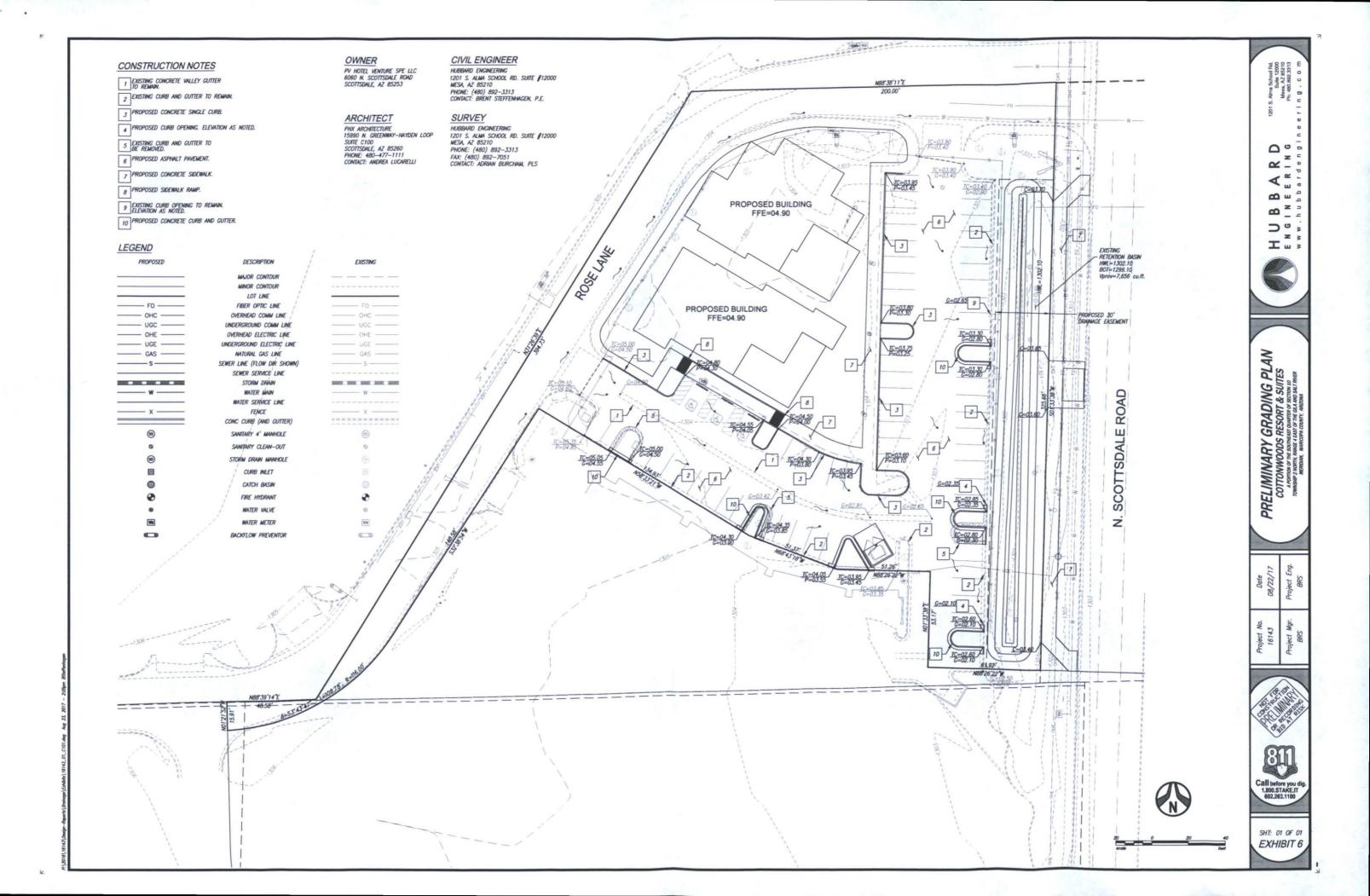


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TOWNSHIP 2 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER

MERIDIAN, MARICOPA COUNTY, ARIZONA

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Development Application: PC/CC, CC and DRB (← circle one) Date of application submittal: 5-31-17 Preapp #: 22-ZN-16 Coordinator: **Date Plans Were Routed:** Staff that Routed Plans: Please check the appropriate box of the Type(s) of Application(s) **Planning Commission and City Council Development Review** Other ☐ General Plan Amendment (GP) ☐ Development Review (Major) (DR) ☐ Annexation/De-annexation (AN) In-Lieu Parking (IP) (More than 5 spaces ☐ Text Amendment (TA) ☐ Subdivisions (Major) (PP) Rezoning (ZN) ☐ Historic Property (HP) ☐ Hardship Exemption (HE) ☐ Conditional Use Permit (UP) **Board of Adjustment** Other Application Type Not Listed ☐ In-fill Incentive (II) ☐ Variance (BA) ☐ Abandonment (AB) ☐ Zoning or DS&PM Appeal PC/CC Track - Not including major General Plan Amendment **DRB Track** BofA Track | White Other Coordinator, please complete the following: 1. Is this a resubmittal: Yes or No (circle one) Yes, this is a resubmittal. Indicate the Review Track that the application was resubmitted on: Review Team. Please indicate below, who and what are to be routed. Review Due Date. Please indicate the Comments Due Date below for the Review Track that the application was submitted on. Comments Due Date: _ Add other Archaeologica **3asis of Design** Water and/or **Nastewater** item(s) Report & D Plan below **Review Team** Design Review - Steve Venker qty 1 Ø Engineering Group—Eliana Hayes David 6. M V V Transportation Engineering - Phil Kercher qty 2 qty 2 qty 2 Transportation Planning - Greg Davies Water Resources - Chris Hassert qty 2 V Fire Group - Ricky King qty 2 Drainage - Richard Anderson Molymond M qty 2 GIS - (Street Names, PP Cases) - Tanya H. Airport - Sarah Ferrara Maps - (PP Cases) - Greg Williams Land Survey – (PP, Dedications) – Dwayne H. Historic Preserv. or Archaeological - Steve V. V 0 Long Range Planning (Taylor R.) Other:

1st Submittal (Resubmittal (← circle one)

<u>Case Review – Rose Lane Commercial Parcel (Cottonwoods</u> Resorts and Suites)

PROJECT NAME: ROSE LANE COMMERCIAL PARCEL

LOCATION: SOUTHEAST CORNER OF SCOTTSDALE ROAD AND ROSE LANE

CASE NUMBER: 22-ZN-2016

Review comments for case drainage report by Hubbard Engineering sealed May 24, 2017. The date of our review is June 20, 2017. Our review comments are as follows:

- The ground cover delineation for the pre-developed condition appears to designate some landscaped areas as impervious. This may overestimate pre-developed flow and under-estimate impacts during post-developed conditions. Delineate these landscaped areas and take this account when calculating the weighted runoff coefficient. [Reference: COS DSPM: Section 4-1.806]
- 2. Submit a preliminary grading and drainage plan on a folded 24"x36" sheet showing existing topo, proposed contours or finished grade elevations, and arrows indicating drainage patterns. Label the existing basin and indicate the proposed drainage easement for the basin. [Reference: COS DSPM: Section 4-1.804]
- 3. For redevelopment projects, the current policy is to preserve any existing stormwater storage and meet first flush treatment for the re-developed area. The proposed drainage concept for this project is acceptable if the Engineer can demonstrate that the existing basin has enough storage to accommodate both (a) the 100-year, 2-hour volume per NOAA Atlas 14 rainfall and (b) first flush (0.5 inch) [Reference: COS Ordinance: Section 37-1.804]
- 4. The area of disturbance during construction of this project will exceed 1 acre. Any disturbed area over 1 acre requires a Notice of Intent (NOI) Certification from the ADEQ prior to construction. Please add a section in the report stating that an NOI will be submitted to ADEQ and an approved NOI Certification from ADEQ with an AZCON number will be provided to the City during the improvement plans submittal. [Reference: COS DS&PM: Section 4-1.300]
- 5. Each drainage report should include a completed Warning and Disclaimer of Liability. [Reference: COS DSPM: Section 4-1A]

Alex Meñez, P.E., CFM Sr. Stormwater Engineer Stormwater Management City of Scottsdale Phone: 480-312-7278

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Exhibit 2	Pre Development Aerial Ground Cover Map	The Signed S. P. C.
Exhibit 3	Post Development Aerial Ground Cover Map	CARIZONA, U.S. 20
Exhibit 4	Existing Site Drainage Map	Expires 3/31/
Exhibit 5	Existing Site Topographic Map	
Exhibit 6	Conceptual Grading Plan	



1. INTRODUCTION AND SCOPE OF WORK

This report presents the results of a *Master Drainage Study* conducted by Hubbard Engineering at the request of Delawie ("client"), for Cottonwoods Resort & Suites ("site"). The purpose of this report is to provide a hydrologic and hydraulic evaluation for the site so that the site can be rezoned. This report addresses on-site conditions as well as storm water runoff retention.

1.1 Site Description

The site is located in Section 10 of Township 2N, Range 4E of the Gila and Salt River Base and Meridian, Maricopa County, Arizona. The location of the site is shown on the site *Vicinity Map*, **FIGURE 1**, on the next page.

1.2 Project Description

The site was previously developed with an existing building with water service connections, sewer service connections, asphalt paved parking lot, concrete sidewalk, concrete curb, block site wall, landscape areas and a surface retention basin that has grass for ground cover. The adjacent half streets to the site are fully developed. The existing building on the site was demoed however, the existing paved parking lot remains along with the existing surface retention basin along Scottsdale Road. There are no offsite flows onto the existing site.

Cottonwoods Resort & Suites Maricopa, Arizona

LOCATED AT 6160 N SCOTTSDALE RD PARADISE VALLEY, ARIZONA 85253

MASTER DRAINAGE REPORT

May 2017

Project No.: 16143

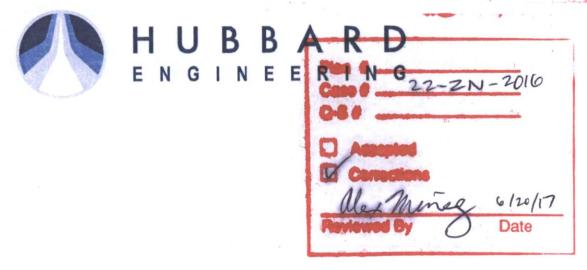
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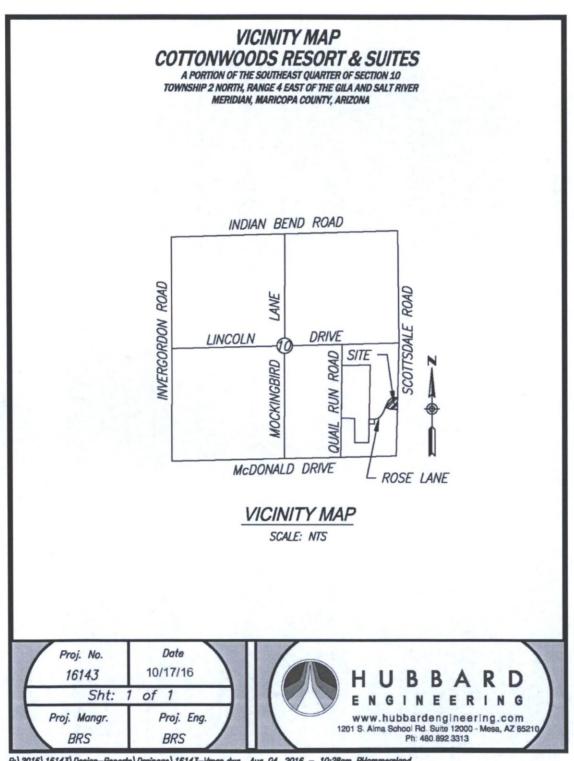
PV HOTEL VENTURES SPE, LLC 4858 E. BASELINE RD., SUITE 101 MESA, AZ 85206

PREPARED BY:

HUBBARD ENGINEERING
1201 S. ALMA SCHOOL RD., SUITE 12000
MESA, ARIZONA 85210
(480) 892-3313
BRENT STEFFENHAGEN, PE







P:\2016\16143\Design-Reports\Drainage\16143-Vmap.dwg Aug 04, 2016 - 10:28am BHammersland

Figure 1 - Vicinity Map

1.3 Design Criteria

The criteria used in the drainage design and analysis of the site was established using the guidelines as described in the following:

- ➤ Design Standards & Policies Manual Chapter 4 Grading and Drainage, City of Scottsdale, Dated January, 2010. (Reference 1).
- ➤ Drainage Design Manual for Maricopa County, Arizona, Volume I, Hydrology (Reference 2).
- Drainage Design Manual for Maricopa County, Arizona, Volume II, Hydraulics (Reference 3).

2. DESCRIPTION OF EXIST. DRAINAGE COND. & CHARACTERISTICS

2.1 Onsite Drainage

As previously mentioned, the site was previously developed with an existing building with water service connections, sewer service connections, asphalt paved parking lot, concrete sidewalk, concrete curb, block site wall, desert landscape areas and a surface retention basin that has grass for ground cover. The adjacent half streets are fully developed. The existing building on the site was recently demoed however, the existing paved parking lot remains along with the existing surface retention basin along N. Scottsdale Road.

A pre-vs-post drainage analysis was done on the existing site representing the previous site condition with the building and the post (future) site conditions with future buildings locations and proposed ground cover. The future conceptual site layout is very similar to pre-project site layout. All ground cover areas will stay the same as the pre site conditions. The existing site has one drainage area DA-A which is shown in **Exhibit 4**. DA-A drains to the existing retention basin along Scottsdale Rd via sheet flow. The demolition of the existing building included the concrete slab of the building therefore the impervious area of the demoed building. A C-value of 0.95 was used for impervious areas and a C-value of 0.30 was used for grass areas. See **Exhibits 2 & 6** for pre-vs-post ground cover delineation areas. See **Section 2.5** for additional information on pre-vs-post drainage analysis. See **Exhibit 1** for Aerial Site Map, **Exhibit 5** for existing site topography.

In accordance with the requirements of the City of Scottsdale Design Standards & Policies Manual, the subject property will be required to retain the 100-year, 2-hour runoff volume, which is determined by utilizing the following formula:

$$V = C * (P/12) * A$$

where,

V = Storage volume (acre-feet)

C = Watershed runoff coefficient

P = 100-year, 2-hour precipitation (inches)

A = Drainage area (acres)

According to the City of Scottsdale Design Standards & Policies Manual, the 100-year, 2-hour depth is 2.2 inches for the site area. See **Appendix B** for NOAA rainfall data.

A "weighted" C-value is determined for each drainage area by utilizing the formula:

$$Cw = A_1 * C_1 + A_2 * C_2 + A_3 * C_3 \dots A_n * C_n$$

$$A_1 + A_2 + A_3 \dots A_n$$

where,

 A_i = Area in the i_{th} sub-area (acres)

C_i = Runoff coefficient in the ith sub-area

As identified in Figure 4.1-4 of the City of Scottsdale Design Standards & Policies Manual, the following "C" values will be used in the retention calculations:

Land Use Category	100-year max. "C" value
Pavement and Rooftops (Impervious Areas)	0.95
Lawns, golf course & parks (grassed areas)	0.30

The volume provided in the proposed retention basins is calculated by using the prismoidal formula:

$$V = d/3 * (A_1 + A_2 + (A_1 * A_2)^{0.5})$$

where,

V = Storage volume (cu.ft.)

d = Depth(ft)

 A_1 = Area of upper contour (sq.ft.)

 A_2 = Area of lower contour (sq.ft.)

The volume of the existing retention basin was determined by using the prismoidal formula. See **Table 1** below for the existing retention basin volume.

Table 1: Existing Basin Volume

			EXISTING I	RETENTIO	N BASIN		
Drainage Area	HW Elevation (ft)	HW Area	Bottom Elevation (ft)	Bottom ft²	H ft	Volume Provided ft ³	Drainage Areas contributing to Basins
RB1	1302.25	14,000.00	1300.25	680.00	2	11,844	DA-A
		34			Total ->	11,844	

14,000.00

<= Total Area @ H.W.'s

Volume Provided = $H/3*(A_{H.W.} + A_{BOTTOM} + (A_{H.W.} * A_{BOTTOM})^{0.5})$

In accordance with the City of Scottsdale Drainage Ordinance, retention basins are required to be drained within a 36-hour period after the storm event.

There is an existing drywell located in the existing retention basin that currently assists in the dissipation of the water to drain within the required 36-hours. See **Exhibit 2 & 6** for drywell location. When the property is developed in the future a Final Drainage Report will need to be submitted along with the Improvement Plans to verify that the proposed site will not require additional storage than what is currently provided by the existing basin and if additional drywell or drywells need to be added to drain the water within the required 36-hours.

Drainage calculations can be found at the end of this drainage study.

2.2 Existing Off-Site Conditions Characteristics

There are no existing offsite flows that inundate the existing site.

2.3 Flood Zone Information

The Maricopa County, Arizona and Incorporated Areas Flood Insurance Rate Map (*F.I.R.M.*) number 04013C1770L panel number 1770 of 4425, dated October 16, 2013 indicates that the project falls within Zone X. A Copy of the FEMA Firmette map can be found in **FIGURE 2**.

Zone X is defined by the Federal Emergency Management Agency (FEMA) as:

"Areas determined to be outside the 0.2% annual chance floodplain."

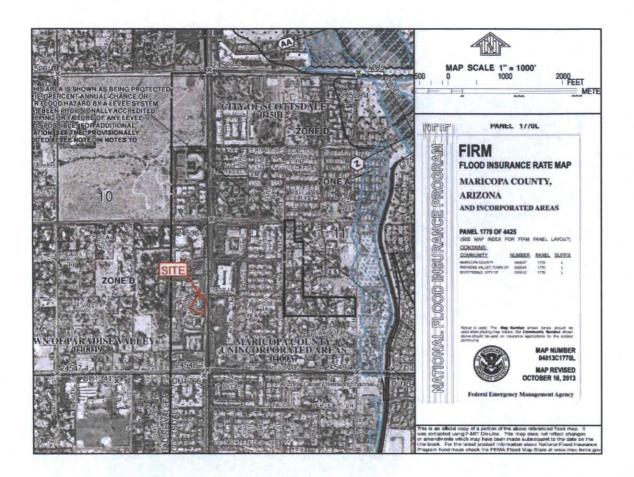


Figure 2 - FIRM

2.4 Pre- and Post-Project Topography

The pre and post project topography will be very similar since they will maintain the same drainage scheme and drain to the same existing basin. See **Exhibit 5 & 6** for existing site topography map and conceptual grading plan.

2.5 Pre- and Post-Project Stormwater Runoff

The entire drainage area DA-A shown in **Exhibit 4** will drain to the existing retention basin RB-1 located along Scottsdale Road. The site was determined to have one drainage area and **Exhibit 4** is labeled accordingly. The runoff from DA-A will drain to RB-1 via sheet flow. The existing basin RB-1 is 2 feet in depth and has a capacity of approximately 11,844 cubic feet. For the pre-condition drainage analysis, it was determined that the required volume that the retention basin must provide per City of Scottsdale's *Design Standards and Policies Manual* (Reference 1) was 8,241 cubic feet. The post-condition drainage analysis determined that the required volume the retention basin must also provide the same as the precondition 8,241 cubic feet of water. Therefore, the existing retention basin has adequate volume for the

current site condition. The existing basin also has an existing drywell incorporated in the bottom of the basin so that the basin drains within the permitted time of 36 hours. See **Appendix A** pre vs post calculations.

3. SPECIAL CONDIDITIONS

3.1 Section 404 & 401

The site is not delineated as a 404 & 401 jurisdiction.

3.2 AZPDES

If in the future the site regraded an AZPDES permit maybe required if the land disturbed is more than one acre.

3.3 **ESL**

The site does not qualify as an Environmentally Sensitive Land on the City of Scottsdale Environmentally Sensitive Land Inventories.

4. DATA ANALYSIS METHODS

4.1 Peak Flows and Stormwater Storage

Storage for the 100-year, 2-hour and peak flow for the 100-year storm was determined by rational method per COS Requirements. See the associated Appendices for the references and parameters that were used to calculate the storm water required retention.

5. SUMMARY AND CONCLUSION

- The project is bound by N. Scottsdale Rd to the east, Rose Ln. to the west and north and by condos on the south side.
- Any future development on the site must abide by the City of Scottsdale's Design Standards & Policies Manual.
- The pre vs post analysis determined that the existing retention basin provides the adequate volume for the current site conditions.
- The site will covey the 100-yr storm event via surface flow into the existing retention basin along N. Scottsdale Road.
- The post conceptual site will have the same drainage area and drainage scheme. It will also have the same ground cover areas as the pre-project condition.
- Subject site is currently located in Flood Plain Zone X per FEMA No. 04013C1770L.

6. REFERENCES

- 1. Design Standards & Policies Manual Chapter 4 Grading and Drainage, City of Scottsdale, Dated January, 2010.
- 2. Drainage Design Manual For Maricopa County, Arizona, Volume I, Hydrology, Flood Control District Of Maricopa County, February 2013.
- 3. Drainage Design Manual For Maricopa County, Arizona, Volume II, Hydraulics, Flood Control District Of Maricopa County, January 2013. Flood Insurance Rate Map (F.I.R.M.) Maricopa County, Arizona and Incorporated areas, Panel 1770 of 4425

7. LIMITATIONS

This report is focused on providing practical design information, evaluation, and calculations for statistical flood events up to and including the 100-year frequency flood. The procedures used herein are derived from, and performed with, currently accepted engineering methodologies and practices. Additionally, the criteria for this evaluation is designed to conform to currently applicable ordinances, regulations and policies effected by the appropriate jurisdictional regulatory authorities for the site.

The analysis presented herein focuses on developing design estimates of storm water runoff resulting from a statistical evaluation of storm events of particular duration and frequency up to and including a 100-year frequency event. A storm event exceeding the 100-year frequency event may cause or create the risk of greater flood impact than is addressed and presented herein. However, the scope of this assessment does not include evaluation of storm water runoff resulting from storm events exceeding the 100-year frequency event. Hubbard Engineering assumes no responsibility for actual flood damage, increased risks of flood damage, or increased construction or development cost resulting from or related to any such events. Nor shall Hubbard Engineering be responsible for any changes in, or additions to, regulatory requirements which may result from, or be related to, any such events or changes in hydrologic or hydraulic conditions within the watershed.

In performing the services contained herein, Hubbard Engineering has received or will receive information prepared or compiled by others. Hubbard Engineering, as engineering professionals, are not required to verify the information, but may rely on the information unless actual knowledge concerning the validity of the information is known or is obvious to the professional. Therefore, Hubbard Engineering is entitled to rely upon the accuracy and completeness of this information without independent evaluation or verification.

POST Composite "C" Calculation Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort

Project No: 16143

Prepared By: BAH

Checked By:

Date: 05/23/17

Date:

Purpose: Calculate a weighted "C" Value for a drainage area.

Methodology: The weighted "C" value is determined by summing the products of each surface "C" value

times the suface area, and dividing by the sum of all of the surface areas.

References: 1. Scottsdale Drainage Design Policy

Calculation: $Cw = (C_{0.95}*A_{0.95} + C_{0.45}*A_{0.45})/A_{TOTAL}$

Surface	C	Area (Sq. Ft.)	C x Area
Hardscape	0.95	19,463	18,490
Grassed Areas	0.30	9,904	2,971
Impervious	0.95	24,793	23,553
Total	N/A	54,160	45,014

1.243342516

1.03338843

"Cw" = 0.83	Weighted Runoff Coefficient	

Post Retention Calculations Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort

Project No.: 16143

Prepared by: BAH Revised By:

Date: 05/23/17 Date:

Purpose: Evaluate the required and provided retention volumes in order to assess conformance to project criteria.

Methodology: Calculate the volume of stormwater required to be retained using City of Scottsdale criteria. Calculate the estimated volume of stormwater retained using retention basin geometry.

Criteria: Retain the calculated stormwater run-off for the 100-YEAR 2-HOUR duration storm event.

References: 1. Scottsdale Drainage Design Policy

2. Drainage Design Manual for Maricopa County, Arizona, Volume II: Hydraulics, August 2013.

Calculations: Volume Required = C_{Composite} *D/12* A [ft³]

(Reference 1)

D = 2.2C = 0.95

(Reference 1) (Reference 1)

C = 0.30

[in] (Paved Parking) (Grassed Areas)

(Reference 1)

Composite C= (C1*A1 + C2*A2...+...)/(A1+A2+...)

Volume Required = Composite C*P/12*A

Results:

Identifiers	CALCULATE R	ETENTION VOLUME REQUIRED	Volume		
Contributory	Area	C Post	Requ	ired	
Area ID	[acres]		[acre-ft]	[ft ³]	
DA-A	1.24	0.83	0.19	8,241	
Total Area:	1.24	TOTAL VOLUME REQUIRED:	0.19	8,241	

Retention Basin

1 of 1

Pre Composite "C" Calculation Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort

Project No: 16143

Prepared By: BAH

Checked By:

Date: 10/13/16

Date:

Purpose: Calculate a weighted "C" Value for a drainage area.

Methodology: The weighted "C" value is determined by summing the products of each surface "C" value

times the suface area, and dividing by the sum of all of the surface areas.

References: 1. Scottsdale Drainage Design Policy

Calculation: $Cw = (C_{0.95} * A_{0.95} + C_{0.45} * A_{0.45}) / A_{TOTAL}$

Surface	C	Area (Sq. Ft.)	C x Area
Grassed Areas	0.30	9,904.00	2971.20
Impervious	0.95	44,256.00	42043.20
Total	N/A	54160.00	45014.40

1.243342516

1.03338843

Pre Retention Calculations Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort

Project No.: 16143

Prepared by: BAH Revised By:

Date: 10/13/16

Date:

Purpose: Evaluate the required and provided retention volumes in order to assess conformance to project criteria.

Methodology: Calculate the volume of stormwater required to be retained using City of Scottsdale criteria. Calculate the estimated volume

of stormwater retained using retention basin geometry.

Criteria: Retain the calculated stormwater run-off for the 100-YEAR 2-HOUR duration storm event.

References: 1. Scottsdale Drainage Design Policy

2. Drainage Design Manual for Maricopa County, Arizona, Volume II: Hydraulics, August 2013.

Calculations: Volume Required = C_{Composite} *D/12* A [ft³]

(Reference 1)

(Reference 1)

D = 2.2 C = 0.95 C = 0.30

(Paved Parking)

(Reference 1)

(Grassed Areas)

(Reference 1)

Composite C= (C1*A1 + C2*A2...+...)/(A1+A2+....)

Volume Required = Composite C*P/12*A

Results:

Identifiers	CALCULATE R	ETENTION VOLUME REQUIRED	Volume		
Contributory	Area	C PRE	Requ	ired	
Area ID	[acres]		[acre-ft]	[ft ³]	
DA-A	1.24	0.83	0.19	8,241	
Total Area:	1.24	TOTAL VOLUME REQUIRED:	0.19	8,241	

Retention Provided Hubbard Engineering Project No. 16143

Project Name: Cottonwoods Resort

Project No.: 16143

Prepared By: BAH

Revised By:

Date: 10/13/16

Date:

RETENTION BASINS						
Drainage Area	HW Area	Bottom ft ²	H	Volume Provided ft ³	Drainage Areas contributing to Basins	
RB1	14,000.00	680.00	2	11,844	DA-A	
			Total ->	11,844	and the second	

14,000.00 <= Total Area @ H.W.'s

Volume Provided = $H/3*(A_{H.W.} + A_{BOTTOM} + (A_{H.W.} * A_{BOTTOM})^{0.5})$



NOAA Atlas 14, Volume 1, Version 5 Location name: Scottsdale, Arizona, USA* Latitude: 33.5274°, Longitude: -111.9264° Elevation: 1300.55 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

PDS	-based po	oint preci	pitation fr	equency	estimates	with 90%	confiden	ce interva	als (in inc	hes) ¹
Duration				Averag	ge recurrence	e interval (/ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.185 (0.155-0.226)	0.242 (0.203-0.296)	0.329 (0.274-0.401)	0.395 (0.327-0.480)	0.485 (0.395-0.586)	0.554 (0.446-0.666)	0.625 (0.494-0.749)	0.697 (0.541-0.834)	0.794 (0.600-0.951)	0.868 (0.643-1.04)
10-min	0.282 (0.236-0.345)	0.369 (0.310-0.451)	0.500 (0.417-0.610)	0.602 (0.498-0.730)	0.738 (0.602-0.892)	0.844 (0.679-1.01)	0.951 (0.752-1.14)	1.06 (0.824-1.27)	1.21 (0.914-1.45)	1.32 (0.979-1.59)
15-min	0.350 (0.292-0.428)	0.457 (0.384-0.559)	0.620 (0.517-0.756)	0.746 (0.618-0.906)	0.915 (0.746-1.11)	1.05 (0.841-1.26)	1.18 (0.932-1.41)	1.32 (1.02-1.57)	1.50 (1.13-1.80)	1.64 (1.21-1.97)
30-min	0.471 (0.393-0.576)	0.616 (0.517-0.753)	0.836 (0.696-1.02)	1.00 (0.832-1.22)	1.23 (1.00-1.49)	1.41 (1.13-1.69)	1.59 (1.25-1.90)	1.77 (1.38-2.12)	2.02 (1.53-2.42)	2.20 (1.63-2.65)
60-min	0.583 (0.487-0.713)	0.762 (0.640-0.932)	1.03 (0.861-1.26)	1.24 (1.03-1.51)	1.53 (1.24-1.84)	1.74 (1.40-2.10)	1.97 (1.55-2.36)	2.19 (1.70-2.62)	2.50 (1.89-2.99)	2.73 (2.02-3.28)
2-hr	0.677 (0.575-0.810)	0.877 (0.744-1.05)	1.17 (0.990-1.40)	1.40 (1.17-1.67)	1.71 (1.41-2.02)	1.94 (1.58-2.29)	2.19 (1.75-2.58)	2.43 (1.92-2.86)	2.76 (2.13-3.26)	3.02 (2.27-3.58)
3-hr	0.743 (0.628-0.899)	0.952 (0.809-1.16)	1.25 (1.05-1.51)	1.49 (1.24-1.79)	1.82 (1.50-2.17)	2.08 (1.69-2.47)	2.35 (1.88-2.80)	2.64 (2.07-3.13)	3.03 (2.31-3.61)	3.35 (2.49-3.99)
6-hr	0.894 (0.772-1.06)	1.13 (0.979-1.34)	1.45 (1.25-1.71)	1.70 (1.45-2.00)	2.05 (1.72-2.39)	2.32 (1.92-2.69)	2.60 (2.12-3.02)	2.89 (2.31-3.36)	3.28 (2.56-3.82)	3.59 (2.74-4.19)
12-hr	0.997 (0.869-1.16)	1.26 (1.10-1.47)	1.59 (1.38-1.85)	1.86 (1.60-2.15)	2.21 (1.88-2.55)	2.48 (2.09-2.86)	2.77 (2.29-3.19)	3.05 (2.49-3.52)	3.43 (2.74-3.97)	3.73 (2.92-4.35)
24-hr	1.18 (1.04-1.36)	1.50 (1.33-1.73)	1.95 (1.71-2.23)	2.30 (2.02-2.63)	2.79 (2.43-3.19)	3.17 (2.74-3.62)	3.57 (3.07-4.08)	3.99 (3.40-4.55)	4.57 (3.84-5.21)	5.02 (4.18-5.74)
2-day	1.28 (1.13-1.46)	1.63 (1.44-1.87)	2.14 (1.89-2.45)	2.55 (2.24-2.91)	3.12 (2.72-3.56)	3.58 (3.10-4.08)	4.05 (3.49-4.63)	4.55 (3.89-5.20)	5.25 (4.44-6.01)	5.81 (4.86-6.66)
3-day	1.36 (1.20-1.55)	1.73 (1.53-1.98)	2.28 (2.01-2.60)	2.72 (2.39-3.10)	3.34 (2.92-3.81)	3.84 (3.33-4.37)	4.37 (3.76-4.98)	4.93 (4.21-5.62)	5.72 (4.82-6.51)	6.35 (5.30-7.25)
4-day	1.43 (1.26-1.64)	1.83 (1.62-2.09)	2.42 (2.13-2.75)	2.89 (2.54-3.29)	3.57 (3.11-4.05)	4.11 (3.56-4.67)	4.69 (4.04-5.32)	5.31 (4.52-6.04)	6.18 (5.20-7.02)	6.89 (5.74-7.84)
7-day	1.60 (1.41-1.83)	2.05 (1.80-2.34)	2.71 (2.38-3.09)	3.24 (2.84-3.70)	4.00 (3.48-4.56)	4.61 (3.98-5.24)	5.26 (4.51-5.98)	5.95 (5.06-6.78)	6.93 (5.81-7.89)	7.71 (6.41-8.80)
10-day	1.73 (1.53-1.98)	2.22 (1.96-2.53)	2.93 (2.58-3.33)	3.51 (3.07-3.98)	4.31 (3.76-4.88)	4.95 (4.29-5.60)	5.64 (4.85-6.38)	6.36 (5.43-7.21)	7.37 (6.22-8.35)	8.18 (6.84-9.29)
20-day	2.14 (1.89-2.42)	2.75 (2.43-3.11)	3.63 (3.21-4.10)	4.30 (3.79-4.85)	5.20 (4.56-5.87)	5.89 (5.15-6.65)	6.60 (5.74-7.45)	7.32 (6.33-8.27)	8.28 (7.10-9.38)	9.03 (7.68-10.2)
30-day	2.50 (2.20-2,83)	3.22 (2.84-3.64)	4.24 (3.74-4.79)	5.02 (4.41-5.66)	6.07 (5.31-6.84)	6.87 (5.99-7.74)	7.70 (6.68-8.66)	8.54 (7.37-9.60)	9.67 (8.29-10.9)	10.5 (8.96-11.9)
45-day	2.88 (2.56-3.26)	3.72 (3.30-4.19)	4.90 (4.34-5.52)	5.78 (5.10-6.51)	6.93 (6.10-7.80)	7.80 (6.85-8.78)	8.69 (7.58-9.78)	9.57 (8.32-10.8)	10.7 (9.26-12.1)	11.6 (9.96-13.1)
60-day	3.18 (2.83-3.58)	4.11 (3.66-4.62)	5.41 (4.81-6.07)	6.36 (5.63-7.14)	7.59 (6.71-8.51)	8.50 (7.48-9.53)	9.41 (8.25-10.6)	10.3 (9.00-11.6)	11.5 (9.97-12.9)	12.4 (10.7-14.0)

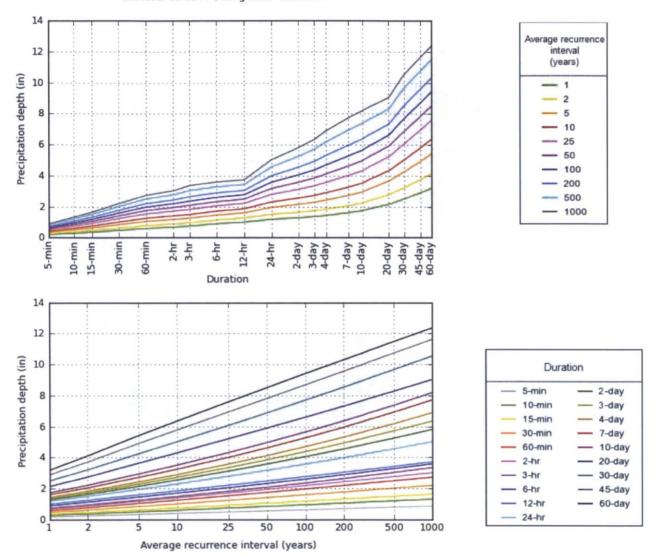
¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 33.5274°, Longitude: -111.9264°



NOAA Atlas 14, Volume 1, Version 5

Created (GMT): Thu Oct 13 22:13:01 2016

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Maps & aerials

Small scale terrain



Large scale terrain



Large scale map



Large scale aerial

Prescott

Arizona

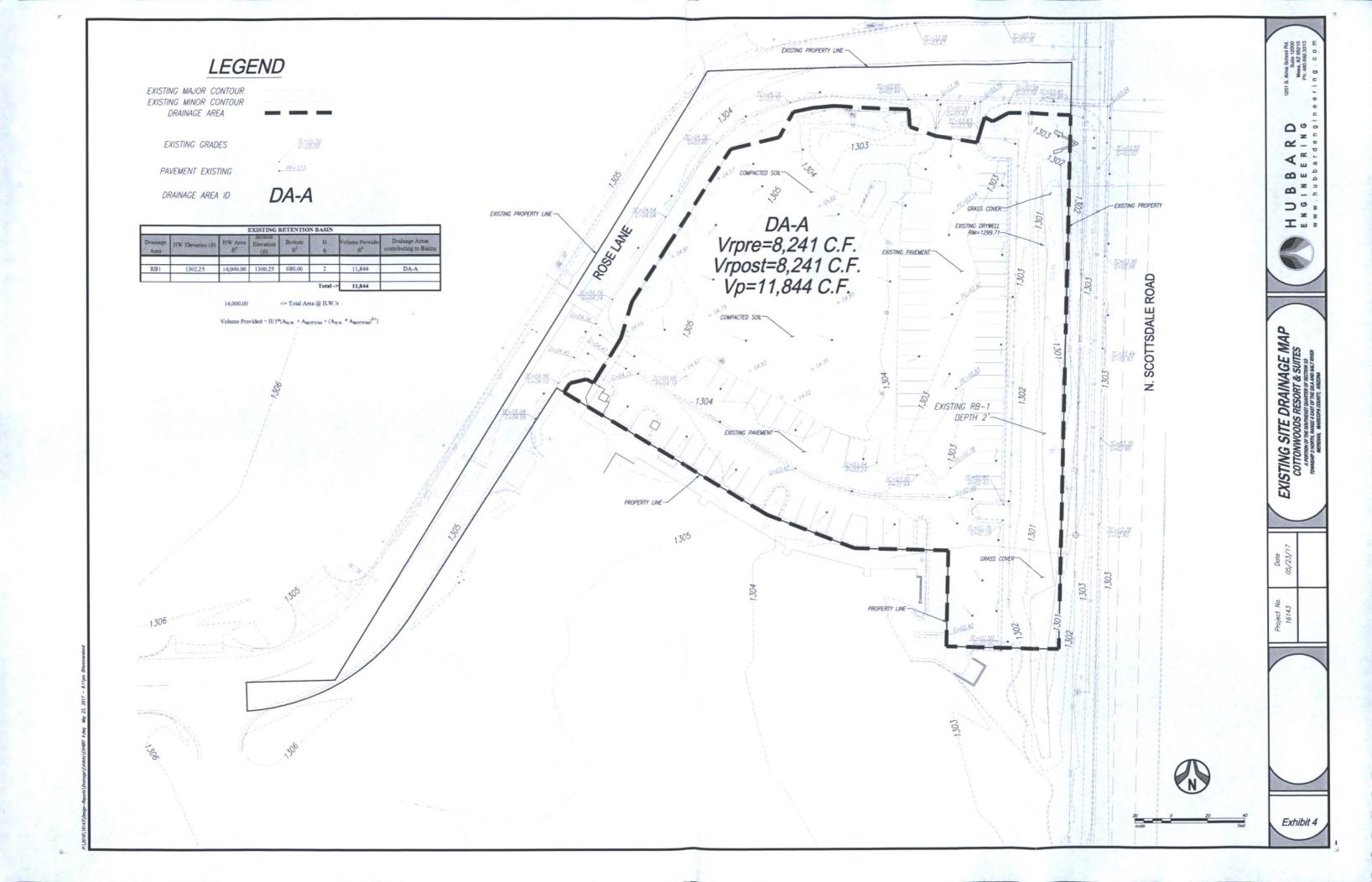
Phoenix

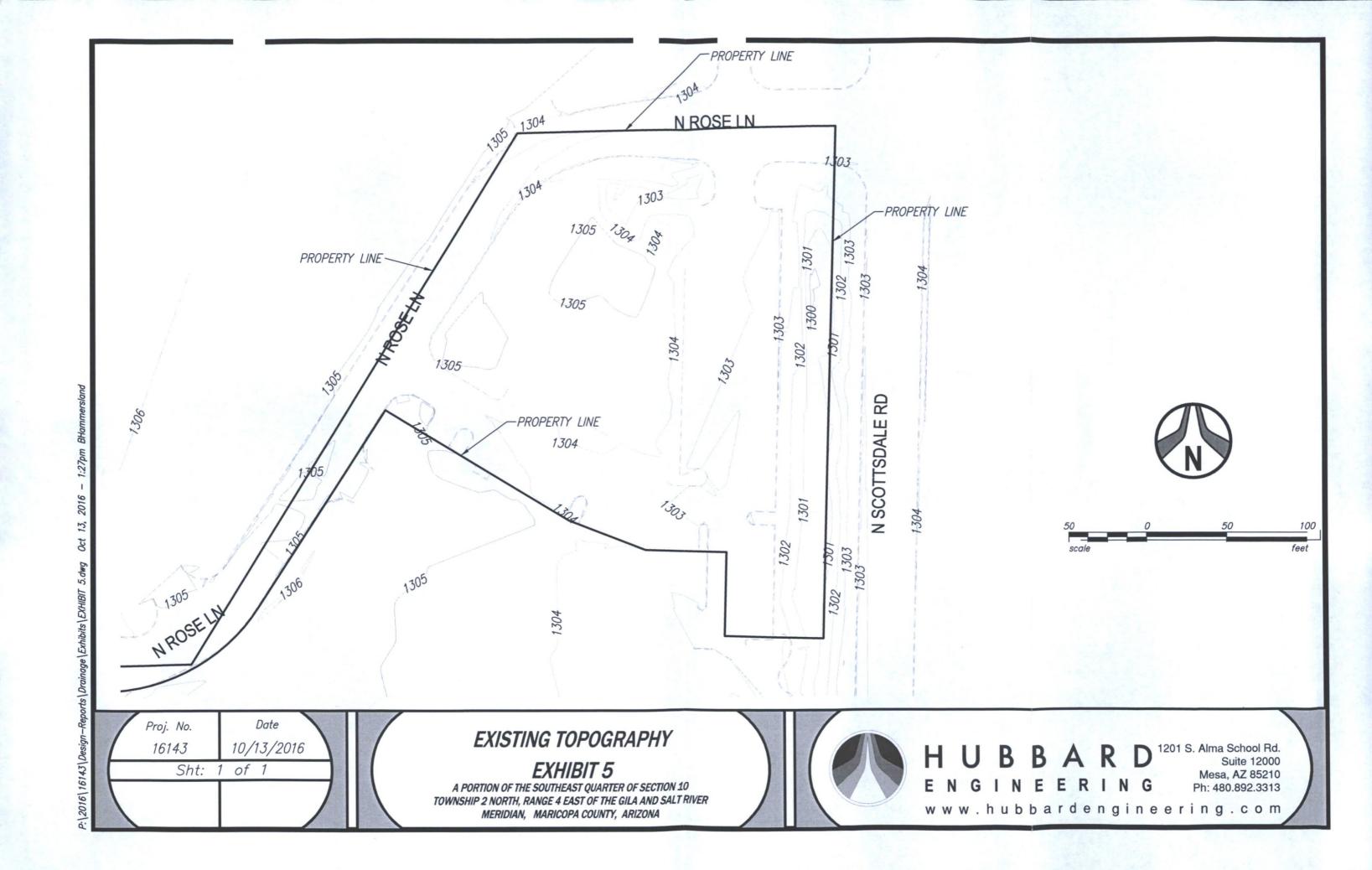
Mesa

Back to Top

US Department of Commerce
National Oceanic and Atmospheric Administration
National Weather Service
National Water Center
1325 East West Highway
Silver Spring, MD 20910
Questions?: HDSC.Questions@noaa.gov

Disclaimer





GROUND COVER DELINEATION

DRAINAGE AREA

DRAINAGE AREA ID

DA-A

GROUND COVER TYPE "BUIDLINGS & HARDSCAPE"

GROUND COVER TYPE "PAVEMENT"

GROUND COVER TYPE "GRASS"

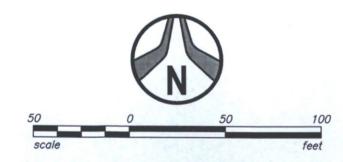
Surface	C	Area (Sq. Ft.)	C x Area
Hardscape	0.95	19,463	18,490
Grassed Areas	0.30	9,904	2,971
Impervious	0.95	24,793	23,553
Total	N/A	54,160	45,014

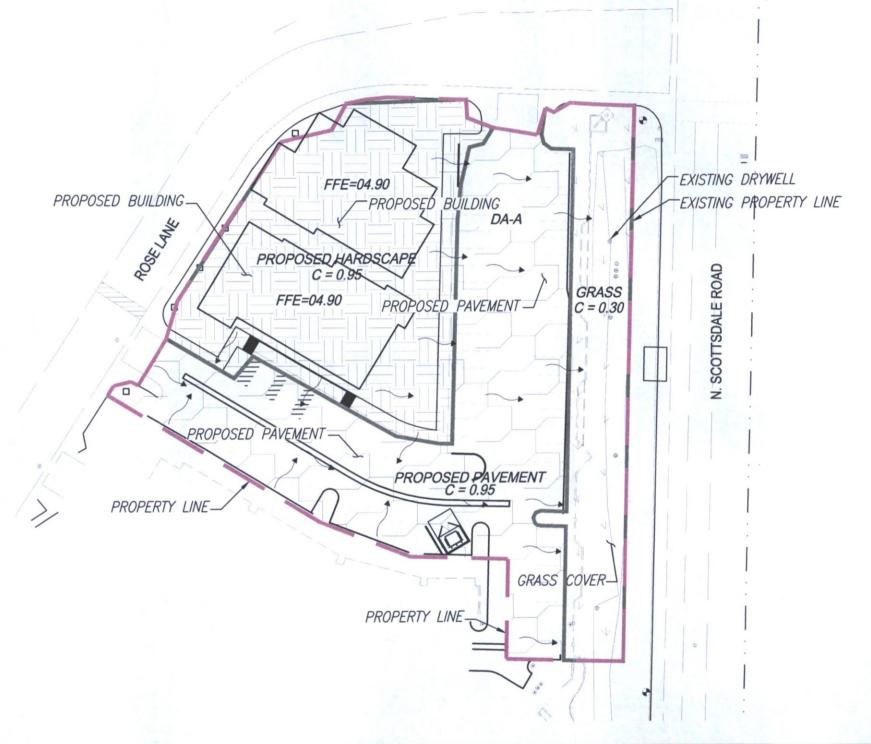
Retention Volumes

Vrpre=8,241 C.F.

Vrpost=8,241 C.F.

Vp=11,844 C.F.





Proj. No.	Date
16143	05/23/17
Sht:	1 of 1

CONCEPTUAL GRADING PLAN

EXHIBIT 6

A PORTION OF THE SOUTHEAST QUARTER OF SECTION 10 TOWNSHIP 2 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER MERIDIAN, MARICOPA COUNTY, ARIZONA



H U B B A R D' ENGINEERING

1201 S. Alma School Rd. Suite 12000 Mesa, AZ 85210 Ph: 480.892.3313

www.hubbardengineering.com

DRAINAGE AREA ID

DA-A

GROUND COVER TYPE "BUIDLINGS & HARDSCAPE"

GROUND COVER TYPE "PAVEMENT"

GROUND COVER TYPE "GRASS"

Surface	C	Area (Sq. Ft.)	C x Area
Hardscape	0.95	19,463	18,490
Grassed Areas	0.30	9,904	2,971
Impervious	0.95	24,793	23,553
Total	N/A	54,160	45,014

Retention Volumes

Vrpre=8,241 C.F.

Vrpost=8,241 C.F.

Vp=11,844 C.F.





Proj. No. Date

16143 05/23/17

Sht: 1 of 1

POST DEVELOPMENT AERIAL GROUND COVER MAP EXHIBIT 3

A PORTION OF THE SOUTHEAST QUARTER OF SECTION 10 TOWNSHIP 2 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER MERIDIAN, MARICOPA COUNTY, ARIZONA



H U B B A R D E N G I N E E R I N G

1201 S. Alma School Rd. Suite 12000 Mesa, AZ 85210 Ph: 480.892.3313

www.hubbardengineering.com

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B w



GROUND COVER DELINEATION

DRAINAGE AREA

DRAINAGE AREA ID DA-A

GROUND COVER TYPE "PAVEMENT" [GROUND COVER TYPE "GRASS"

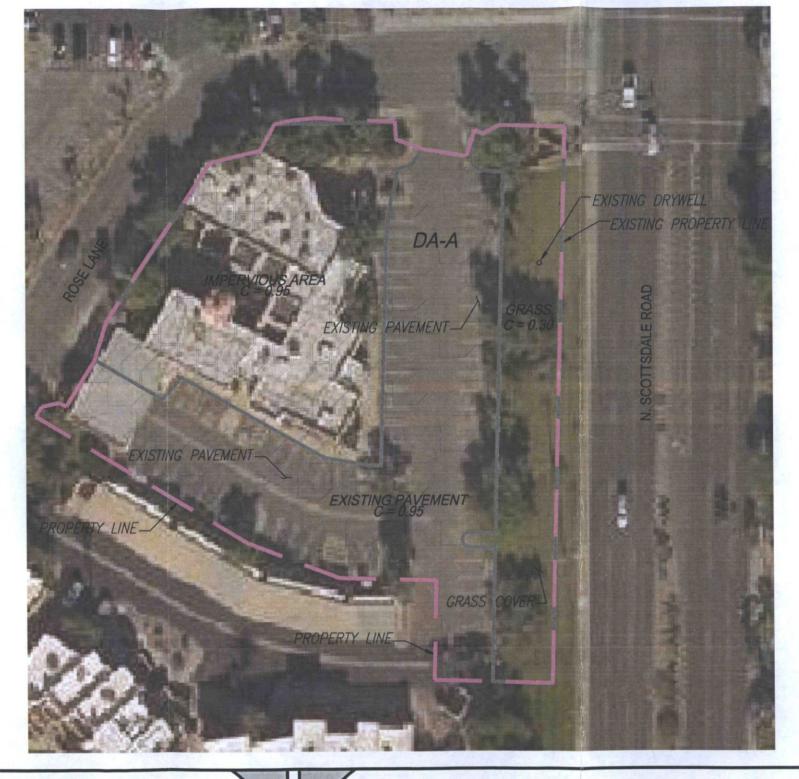
GROUND COVER TYPE "IMPERVIOUS"

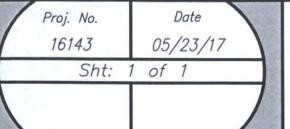
Surface	C	Area (Sq. Ft.)	C x Area
Grassed Areas	0.30	9,904.00	2971.20
Impervious	0.95	44,256.00	42043.20
Total	N/A	54160.00	45014.40

Retention Volumes

Vrpre=8,241 C.F. Vp=11,844 C.F.







PRE-DEVELOPMENT AERIAL GROUND COVER MAP EXHIBIT 2

A PORTION OF THE SOUTHEAST QUARTER OF SECTION 10 TOWNSHIP 2 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER MERIDIAN, MARICOPA COUNTY, ARIZONA



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Mesa, AZ 85210 Ph: 480.892.3313

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