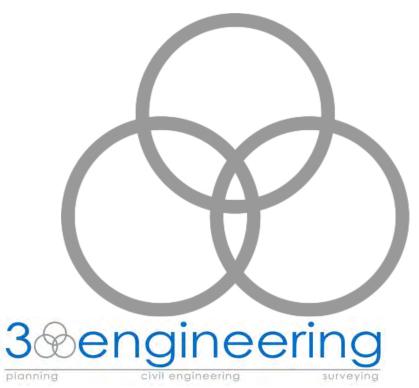
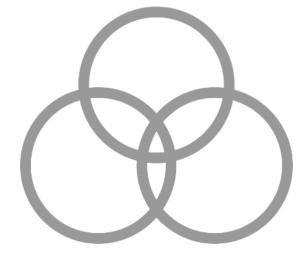


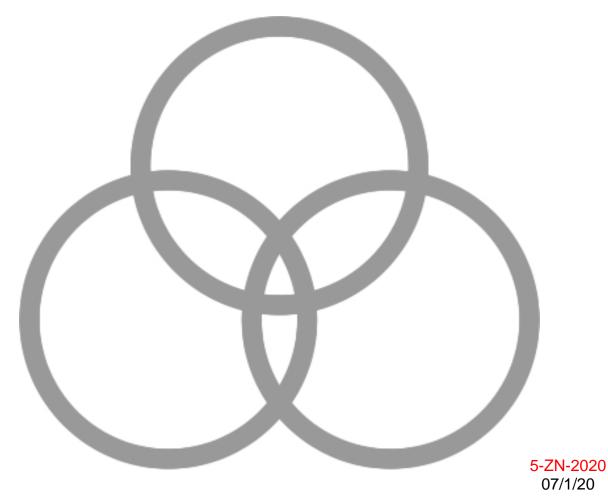
Drainage Reports





Planning civil engineering survey SOUTHDALE Preliminary Drainage Report

3 engineering Job #: 1872 June 29, 2020 COS #: 5-ZN-2020





# SOUTHDALE

# 7000 E. MCDOWELL ROAD, SCOTTSDALE, AZ 85257

# PRELIMINARY DRAINAGE REPORT

Prepared for:

Hawkins Companies LLC 4700 S. McClintock Drive #160 Scottsdale, Arizona 85257 Contact: Mark Mitchell Phone: (480) 223-8239



Daniel G. Mann, P.E.

June 29, 2020

### Submittal to:

City of Scottsdale 7447 E. Indian School Road, Suite 105 Scottsdale, AZ 85251

### Prepared by:

3 engineering, LLC 6370 E. Thomas Road, Suite #200 Scottsdale, Arizona 85251 Contact: Dan G. Mann, P.E.

Job Number 1872





### Table of Contents

### Page

| 1. | Introduction              | 1 |
|----|---------------------------|---|
| 2. | Site Description          | 1 |
| 3. | Drainage Design – Offsite | 1 |
| 4. | Drainage Design – Onsite  | 2 |
| 5. | Conclusions               | 4 |
| 6. | References                | 4 |

### Appendix

| Appendix A – Vicinity Map                             | A-1  |
|---|------|
| Appendix B – FEMA FIRM Map                            | A-2  |
| Appendix C – Warning and Disclaimer of Liability      | A-3  |
| Appendix D – Watershed Delineation and Topography Map | A-4  |
| Appendix E – Offsite Drainage Calculations            | A-5  |
| Appendix F – Aerial Site Photographs                  | A-6  |
| Appendix G – Offsite Aerial Photographs               | A-7  |
| Appendix H – Onsite Drainage Area Map                 | A-8  |
| Appendix I – Inlet Area Exhibit                       | A-9  |
| Appendix J – Onsite Drainage Calculations             | A-10 |
| Appendix K – Flo-2d Maps                              | A-11 |
| Appendix L - Preliminary Grading and Drainage Plans   | A-12 |





### 1. Introduction

The purpose of this report is to present the existing and proposed drainage plan for the project site, Southdale. It is our opinion the proposed grading and drainage concept is in accordance with the City of Scottsdale drainage requirements.

The project site, Southdale, is located in the southeast guarter of Section 34, Township 2 North, Range 4 East of the Gila and Salt River Meridian, Maricopa County, Arizona within the City of Scottsdale. The project is located at 7000 E. McDowell Road, Scottsdale, AZ 85257. The site is bounded on the north by an apartment complex, on the east by a commercial development, on the south by McDowell Road, and on the west by 70<sup>th</sup> Street. See Appendix A for a vicinity map and Appendix G for offsite aerial photographs.

The existing zoning is C-3. The land is currently used as a commercial development. The proposed zoning is PUD. The City of Scottsdale 2001 General Plan shows the site as a Mixed-Use Neighborhood. The proposed site is a 267-unit apartment complex with office and retail space. The site currently lies within the "Zone X" floodplain designation.

### 2. Site Description

### Existing

The project site currently consists of a fully developed commercial development with landscaping, drive aisles, parking, and utilities. The existing topography of the site generally slopes from northwest to southeast at approximately 1.0 percent (1.0%). The site currently does not retain stormwater and discharges flows to McDowell Road at the site outfall located at the southeast corner of the site. The site does not show any signs of containing waters of the US (404 washes). See Appendix F for an aerial photograph of the site.

### Federal Emergency Management Agency (FEMA) Designation

According to FEMA Flood Insurance Rate Map (FIRM) # 04013C2235L, dated October 16, 2013, the site is located within the "Zone X" floodplain designation.

"Zone X" is described as follows:

"Areas determined to be outside the 0.2% annual chance floodplain."

Refer to the updated Flood Insurance Rate Map information in Appendix B.

### Proposed

The proposed project includes constructing a 267-unit multi-family apartment complex with office and retail space. The site also includes drive aisles, surface parking, a parking structure, and landscape. See the proposed improvements in the Onsite Drainage Area Map in Appendix Η.

### 3. Drainage Design - Offsite

The site is not considered to be affected by offsite flows. The Maricopa County Flood Control District Flo-2d maps from the Lower Indian bend Wash Study show offsite flows entering the site from the west. See Appendix K for Flo-2d maps. The physical conditions of the site differ from the assumptions in the Flo-2d analysis. The site is blocked from offsite flows and is discussed below.

Flows are generated within an offsite drainage area west of the site that travel east toward 70th Street through Coronado Road, Almeria Road and an alley south of Almeria Road. See Watershed Delineation and Topography Map in Appendix D. The peak discharge for the

Page | 1 5-ZN-2020 07/1/20



drainage area was determined to be 23 cfs for the 100-year storm event using the FCDMC DDMSW HEC-1 Model, which is consistent with the flows shown in the Flo-2d map. The flow is conveyed to the west half of 70<sup>th</sup> Street which has a capacity of 18.15 cfs (cross section A). Therefore, 4.85 cfs breaks over to the east side of 70<sup>th</sup> Street. With a flow of 4.85 cfs, the water surface elevation in the east side of 70<sup>th</sup> street is at an elevation of 42.19 at the location of a 20-ft wide driveway to the apartment complex north of the site (cross section B). The back of the driveway has an elevation of 42.17. The breakover was modeled as a weir with a width of 20-ft and a depth of 0.02-ft, resulting in a flow of 0.17 cfs that enters the apartment complex (weir section B). The remaining 4.68 cfs travels south in the east half of 70<sup>th</sup> street, adjacent to the site, which has a capacity of 7.95 cfs (cross section C). There is a block wall/solid building walls that extend the entire property line between the project site and the apartment complex. There is an opening at a foot-gate along the wall, however it is 1.3-ft above the adjacent catch basin in the apartment complex drive aisle. Therefore, no offsite flows affect the site. There is a drywell in the alley behind the existing apartment complex to the northwest that dissipates any storm water in this area.

Refer to Appendix D for a Watershed Delineation and Topography map and Appendix E for Offsite Drainage Calculations including HEC-1 Results and Flowmaster Calculations. Cross section locations are shown in the Onsite Drainage Area Map, Appendix H.

#### Hydraulic Parameters

Bentley Flowmaster V8i was used to calculate the street capacity for sections in 70<sup>th</sup> Street for 100-year flows. The Flood Control District of Maricopa County Drainage Design Management System for Windows (DDMSW) was used to determine the flow for 100-year storm event . See results in Appendix E.

#### 4. Drainage Design - Onsite

The City of Scottsdale Design Standards and Policies Manual and the Drainage Design Manual for Maricopa County, Volume 1 was followed in designing on-site drainage facilities for the site.

Refer to the Preliminary Grading and Drainage Plan in Appendix L, the Onsite Drainage Map in Appendix H and Inlet Area Exhibit in Appendix I for the following discussion. The proposed site is required to provide retention for the pre- vs. post-project runoff for the 100-year, 2-hour storm or the 0.5" First Flush Storm (with weighted runoff coefficient), whichever is greater. The c value for the proposed site is less than the existing site, so the pre- vs. post- runoff method results in no required volume. Therefore, the First Flush Storm is used. There is no retention provided for the "true rooftop" areas with no amenities, see Appendix H for areas. See Appendix J for Onsite Drainage Calculations.

The required retention volume for Drainage Area A is 2,697 c.f. There is 2,764 c.f. provided in 220-L.F. of 48" storm drain pipe. Flows generated within this drainage area are conveyed via roof drains and surface flow to five catch basins that connect directly into the underground retention pipe. In a storm event greater than the 0.5" first flush the retention pipe will fill and overflow through the southernmost catch basin to McDowell Road. The system is modeled in Bentley StormCAD using a tail water elevation of 6" above the highpoint breakover at the driveway. A proposed dry-well will provide a dry up time of 36 hours with an infiltration rate of 0.02 cfs. Additionally, the two courtyard areas have secondary overflow catch basins elevated 0.25-ft above the primary catch basin. The overflow catch basins will not receive flow until the

Page | 2



planning

civil engineering

underground retention is full or the primary catch basins are clogged. The overflow catch basin in the north courtyard, area A-4, is conveyed to a bubble-up outlet in the fire lane west of the building. The bubble-up structure is connected to the underground retention with a bleed off pipe and does not require an additional drywell. The overflow catch basin for the south courtyard, area A-5, outlets to the right of way in McDowell Road.

The required retention volume for Drainage Area B is 517 c.f. There is 702 c.f. provided in 143-L.F. of 30" storm drain pipe. Flows generated within this drainage area are conveyed via surface flow to two catch basins that connect directly into the underground retention pipe. In a storm event greater than the 0.5" first flush the retention pipe will fill and overflow through the north catch basin to 70th Street. The system is modeled in Bentley StormCAD using a tail water elevation of 0.13-ft above the highpoint breakover at the driveway. A proposed dry-well will provide a dry up time of 36 hours with an infiltration rate of 0.01 cfs.

The proposed finish floor of the new building is 1243.00, which is 12" above the highest adjacent catch basin inlet elevation of 1242.00. Therefore, the finish floor meets the requirement of 12" above the adjacent high-water elevation per the Maricopa County Drainage Standards. Additionally, the proposed finish floor elevations are greater than 14" above the site outfall of 1237.85, exceeding the Maricopa County Drainage Standard requirement.

#### Hydraulic Parameters

For onsite peak flows, the Rational Method will be used as follows:

O=CiA

| where: C = Composite runoff coefficient = weighted by ground cover |
|--|
|--|

- i = Intensity corresponding to T<sub>c</sub>
- $T_c$  = Time of concentration (10 minute minimum used)
- A = Area in acres

The 100-year runoff coefficient for this development to be used is 0.95 for impervious areas and 0.45 for pervious areas per the Maricopa County Drainage Policies and Standards. The rainfall is based upon the NOAA Atlas 14, Volume 1, Version 5, dated 2011, 90% confidence interval, mean partial duration time series data.

Determination of Catch Basin capacity operating as a weir by using the following formula:  $Q = C_w x P x d^{1.5} x (1-CF)$ 

 $C_W$  = Weir coefficient (3.0) where: Q = Discharge Capacity (cfs) *P* = Inlet Perimeter

d = Flow depth

CF = Clogging Factor. 40% clogging (or 0.40) used

Please refer to APPENDIX J for catch basin computations.

The on-site storm drain pipes are designed to accommodate flows resulting from the 100year storm event. To calculate the capacity of the storm drain pipes, StormCAD V8i by Bentley Systems, Inc. was used, see results in Appendix J. The 100-year flow calculated for a given drainage area was assigned to the corresponding catch basin. Inlet areas are shown in the Inlet Area Exhibit in Appendix I. The tailwater for each outlet of the retention pipes were set above the adjacent driveway breakover elevations.



#### 5. Conclusions

The following is a summary of the Southdale Preliminary Drainage Report.

- The site currently lies within the "Zone X" floodplain designation.
  - Retention is provided for the 0.5" first flush storm for the site.
  - No offsite flows affect the site.
  - The finish floors are safe from the 100-year storm event.

#### 6. <u>References</u>

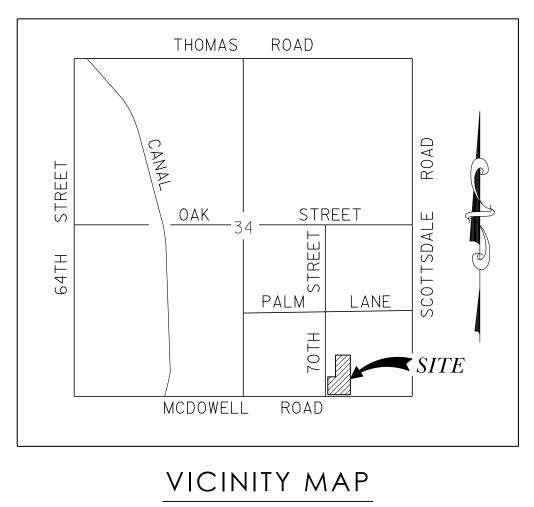
- 1. City of Scottsdale, Design Standards and Policies Manual, 2018.
- 2. Maricopa County, Drainage Policies and Standards, August 2018.
- 3. Maricopa County Flood Control District Flo-2d maps from the Lower Indian bend Wash Study

3 engineering surveying planning

# APPENDIX A

# Vicinity Map

Page | A1 5-ZN-2020 07/1/20







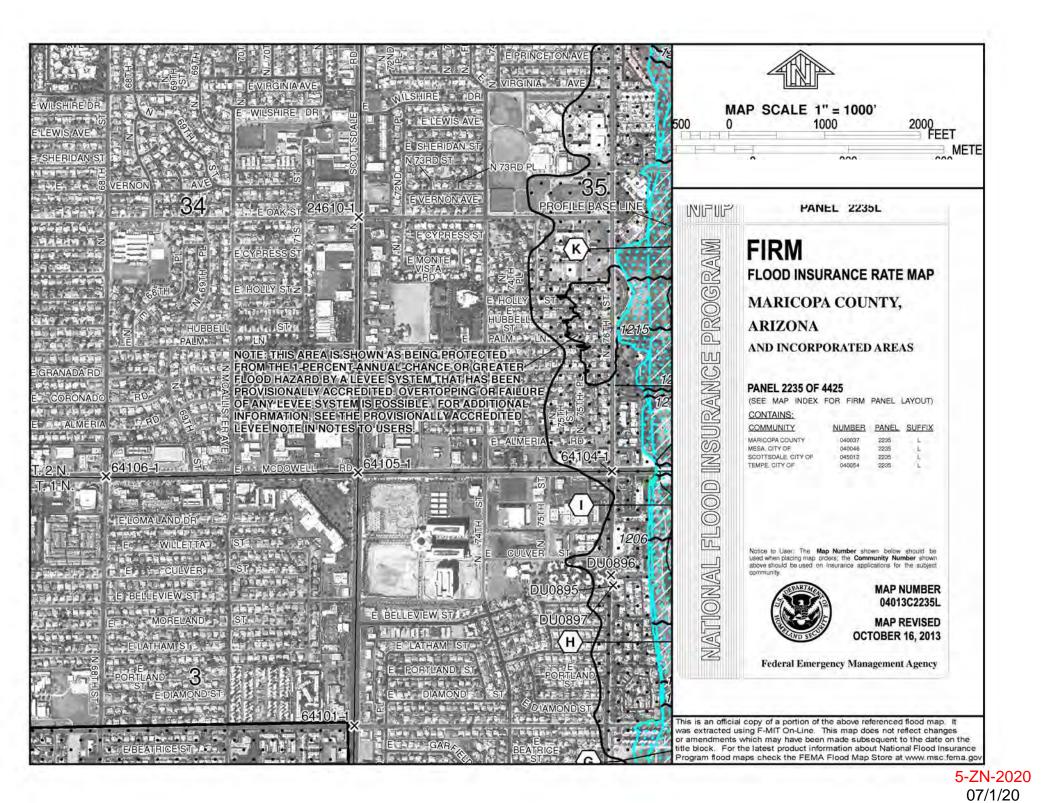
<u>3@engineering</u> civil engineering planning surveying

# APPENDIX B

# FEMA FIRM Map

Page | A2

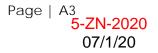
5-ZN-2020 07/1/20



<u>3@engineering</u> civil engineering surveying planning

# APPENDIX C

# Warning and Disclaimer of Liability



# GRADING & DRAINAGE GRADING & DRAINAGE LANGUAGE

### WARNING AND DISCLAIMER OF LIABILITY

The City's Stormwater and Floodplain Management Ordinance is intended to minimize the occurrence of losses, hazards and conditions adversely affecting the public health, safety and general welfare which might result from flooding. The Stormwater and Floodplain Management Ordinance identifies floodplains, floodways, flood fringes and special flood hazard areas. However, a property outside these areas could be inundated by floods. Also, much of the city is a dynamic flood area; floodways, floodplains, flood fringes and special flood hazard areas may shift from one location to another, over time, due to natural processes.

WARNING AND DISCLAIMER OF LIABILITY

The flood protection provided by the Stormwater and Floodplain Management Ordinance is considered reasonable for regulatory purposes and is based on scientific and engineering considerations. Floods larger than the base flood can and will occur on rare occasions. Floodwater heights may be increased by constructed or natural causes. The Stormwater and Floodplain Management Ordinance does not create liability on the part of the city, any officer or employee thereof, or the federal, state or county government for any flood damages that result from reliance on the Ordinance or any administrative decision lawfully made thereunder.

Compliance with the Stormwater and Floodplain Management Ordinance does not ensure complete protection from flooding. Flood-related problems such as natural erosion, streambed meander, or constructed obstructions and diversions may occur and have an adverse effect in the event of a flood. You are advised to consult your own engineer or other expert regarding these considerations. I have read and understand the above.

| 20    | ale | Ar . |
|-------|-----|------|
| Owner |     | Date |

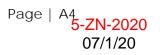
Plan Check #

Page **219 5-ZN-2020** 07/1/20

3<br/>
<br/>
<br/>
engineering civil engineering planning survevina

# APPENDIX D

# Watershed Delineation and Topography Map





securiSync\Projects\1872\_70th\_St\_McDowell\_Apartments\Reports\Preliminary Drainage\1872exb\_watershed\_delineation.dg

<u>3®engineering</u> civil engineering planning surveying

# APPENDIX E

# Offsite Drainage Calculations

Page | A5



| 1** | ******                           | *** | *** | ************                            | *** |
|-----|----------------------------------|-----|-----|---|-----|
| *   |                                  | *   | *   |   | *   |
| *   | FLOOD HYDROGRAPH PACKAGE (HEC-1) | *   | *   | U.S. ARMY CORPS OF ENGINEERS            | *   |
| *   | JUN 1998                         | *   | *   | HYDROLOGIC ENGINEERING CENTER           | *   |
| *   | VERSION 4.1                      | *   | *   | 609 SECOND STREET                       | *   |
| *   |                                  | *   | *   | DAVIS, CALIFORNIA 95616                 | *   |
| *   | RUN DATE 10JUN20 TIME 09:11:31   | *   | *   | (916) 756-1104                          | *   |
| *   |                                  | *   | *   |   | *   |
| **  | ************                     | *** | *** | *************************************** | *** |

| Х    | Х   | XXXXXXX | XXX | XXX |       | Х   |
|------|-----|---------|-----|-----|-------|-----|
| Х    | Х   | Х       | Х   | Х   |       | XX  |
| Х    | Х   | Х       | Х   |     |       | Х   |
| XXXX | XXX | XXXX    | Х   |     | XXXXX | Х   |
| Х    | Х   | Х       | Х   |     |       | Х   |
| Х    | Х   | Х       | Х   | Х   |       | Х   |
| Х    | Х   | XXXXXXX | XXX | XXX |       | XXX |

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

HEC-1 INPUT

1

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

PAGE 1

5-ZN-2020 07/1/20

| LINE | ID    | 1.  | 2            | 3       | 4         | 5678910         |
|------|-------|-----|--------------|---------|-----------|-----------------|
| 1    | ID    | F   | lood Contro  | ol Dist | rict of N | Naricopa County |
| 2    | ID    | 1   | .872 SOUTHDA | ALE -   |           |                 |
| 3    | ID    | 1   | .00 YEAR     |         |           |                 |
| 4    | ID    | e   | Hour Stor    | ۳m      |           |                 |
| 5    | ID    | ι   | Init Hydrog  | raph: C | lark      |                 |
| 6    | ID    |     | torm: Mult   |         |           |                 |
| 7    | ID    | e   | 6/10/2020    | •       |           |                 |
|      | *DIAG | RAM |              |         |           |                 |
| 8    | IT    | 5   | 1JAN99       | 0       | 2000      |                 |
| 9    | IO    | 5   |              |         |           |                 |
| 10   | IN    | 15  |              |         |           |                 |

|            |                                 | *       |                   |   |           |          |        |       |       |       |                   |   |           |
|------------|---------------------------------|---------|-------------------|---|-----------|----------|--------|-------|-------|-------|-------------------|---|-----------|
|            | 11                              | JD      | 2.540             | 0.0001                                  |           |          |        |       |       |       |                   |   |           |
|            | 12                              | PC      | 0.000             | 0.0001                                  | 0.016     | 0.025    | 0.033  | 0.041 | 0.050 | 0.058 | 0.066             | 0.074                                   |           |
|            | 13                              | PC      | 0.087             | 0.099                                   | 0.118     | 0.138    | 0.216  | 0.377 | 0.834 | 0.058 | 0.931             | 0.950                                   |           |
|            | 14                              | PC      | 0.962             | 0.972                                   | 0.983     | 0.991    | 1.000  | 0.5/7 | 0.054 | 0.911 | 0.991             | 0.000                                   |           |
|            | 15                              | JD      | 2.525             | 0.5000                                  | 01909     | 01332    | 1.000  |       |       |       |                   |   |           |
|            | 16                              | PC      | 0.000             | 0.008                                   | 0.016     | 0.025    | 0.033  | 0.041 | 0.050 | 0.058 | 0.066             | 0.074                                   |           |
|            | 17                              | PC      | 0.087             | 0.099                                   | 0.118     | 0.138    | 0.216  | 0.377 | 0.834 | 0.911 | 0.931             | 0.950                                   |           |
|            | 18                              | PC      | 0.962             | 0.972                                   | 0.983     | 0.991    | 1.000  |       |       |       |                   |   |           |
|            |                                 | *       |                   |   |           |          |        |       |       |       |                   |   |           |
|            |                                 |         |                   |   |           |          |        |       |       |       |                   |   |           |
|            | 19                              | KK      | 1                 | BASIN                                   |           |          |        |       |       |       |                   |   |           |
|            | 20                              | BA      | 0.021             |   |           |          |        |       |       |       |                   |   |           |
|            | 21                              | LG      | 0.25              | 0.25                                    | 3.95      | 0.59     | 45     |       |       |       |                   |   |           |
|            | 22                              | UC      | 0.338             | 0.453                                   |           |          |        |       |       |       |                   |   |           |
|            | 23                              | UA      | 0                 | 5.0                                     | 16.0      | 30.0     | 65.0   | 77.0  | 84.0  | 90.0  | 94.0              | 97.0                                    |           |
|            | 24                              | UA<br>* | 100               |   |           |          |        |       |       |       |                   |   |           |
|            | 25                              |         |                   |   |           |          |        |       |       |       |                   |   |           |
| 1          | 25                              | ZZ      |                   |   |           |          |        |       |       |       |                   |   |           |
| T          | сснем                           |         |                   | STREAM I                                |           |          |        |       |       |       |                   |   |           |
| INPUT      | SCHEM                           | ATIC DI |                   | JINLAH                                  |           |          |        |       |       |       |                   |   |           |
| LINE       | (V) ROUTIN                      | G       | (                 | >) DIVERS                               | STON OR I |          | M      |       |       |       |                   |   |           |
|            | (1)                             | •       | <b>`</b>          | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, |           |          |        |       |       |       |                   |   |           |
| NO.        | (.) CONNEC                      | TOR     | (<                | -) RETURI                               | N OF DIV  | ERTED OR | PUMPED | FLOW  |       |       |                   |   |           |
|            |                                 |         |                   |   |           |          |        |       |       |       |                   |   |           |
| 19         | 1                               |         |                   |   |           |          |        |       |       |       |                   |   |           |
|            |                                 |         |                   |   |           |          |        |       |       |       |                   |   |           |
| • •        | NOFF ALSO COM<br>********       |         |                   |   |           |          |        |       |       |       | * * * * * * * * * | *****                                   | * * * * * |
| 1********* | * * * * * * * * * * * * * * * * | ****    | * * * * * * * * * | ****                                    |           |          |        |       |       |       | *                 | * | *****     |
|            |                                 |         |                   | `*<br>`*                                |           |          |        |       |       |       |                   | . ARMY CORPS OF ENGINEERS               | *         |
| * FLOOI    | D HYDROGRAPH<br>JUN             | 1998    | (HEC-1            | *                                       |           |          |        |       |       |       | 0.5               | ROLOGIC ENGINEERING CENTER              |           |
| *          | VERSION                         |         |                   | *                                       |           |          |        |       |       |       | * חזטו<br>*       | 609 SECOND STREET                       | *         |
| *          | VERSION                         | 4.1     |                   | *                                       |           |          |        |       |       |       | * 1               | DAVIS, CALIFORNIA 95616                 | *         |
| * RUN DA   | ATE 1010020                     | TTMF    | 09:11:3           | 1 *                                     |           |          |        |       |       |       | *                 | (916) 756-1104                          | *         |
| *          | 10000020                        | 1 1112  |                   | *                                       |           |          |        |       |       |       | *                 | (310) 730 1104                          | *         |
| *******    | *****                           | ******  | ******            | ****                                    |           |          |        |       |       |       | ******            | ******                                  | ****      |
|            |                                 |         |                   |   |           |          |        |       |       |       |                   |   |           |

Flood Control District of Maricopa County 1872 SOUTHDALE -100 YEAR 6 Hour Storm Unit Hydrograph: Clark Storm: Multiple

5-ZN-2020 07/1/20

06/10/2020

9 IO OUTPUT CONTROL VARIABLES IPRNT 5 PRINT CONTROL IPLOT 0 PLOT CONTROL QSCAL 0. HYDROGRAPH PLOT SCALE

#### IT HYDROGRAPH TIME DATA

| NMIN   | 5      | MINUTES IN COMPUTATION INTERVAL |
|--------|--------|---------------------------------|
| IDATE  | 1JAN99 | STARTING DATE                   |
| ITIME  | 0000   | STARTING TIME                   |
| NQ     | 2000   | NUMBER OF HYDROGRAPH ORDINATES  |
| NDDATE | 7JAN99 | ENDING DATE                     |
| NDTIME | 2235   | ENDING TIME                     |
| ICENT  | 19     | CENTURY MARK                    |

| COMPUTATION | INTERVAL  | 0.08   | HOURS |
|-------------|-----------|--------|-------|
| TOTAL       | FIME BASE | 166.58 | HOURS |

#### ENGLISH UNITS

| DRAINAGE AREA       | SQUARE MILES          |
|---------------------|-----------------------|
| PRECIPITATION DEPTH | INCHES                |
| LENGTH, ELEVATION   | FEET                  |
| FLOW                | CUBIC FEET PER SECOND |
| STORAGE VOLUME      | ACRE-FEET             |
| SURFACE AREA        | ACRES                 |
| TEMPERATURE         | DEGREES FAHRENHEIT    |

#### 11 JD INDEX STORM NO. 1 STRM 2 54 PRECIPITATION DEPTH

| 21111 | 2.54 | PRECIPITATION DEPTH         |
|-------|------|-----------------------------|
| TRDA  | 0.00 | TRANSPOSITION DRAINAGE AREA |

#### 12 PI PRECIPITATION PATTERN

| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
|------|------|------|------|------|------|------|------|------|------|
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.03 |
| 0.03 | 0.03 | 0.05 | 0.05 | 0.05 | 0.15 | 0.15 | 0.15 | 0.03 | 0.03 |
| 0.03 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.00 | 0.00 |      |      |      |      |      |      |      |      |

#### 15 JD INDEX STORM NO. 2

| STRM | 2.53 | PRECIPITATION | DEPTH    |      |
|------|------|---------------|----------|------|
| TRDA | 0.50 | TRANSPOSITION | DRAINAGE | AREA |

#### 16 PI PRECIPITATION PATTERN

| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
|------|------|------|------|------|------|------|------|------|------|
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |

### 5-ZN-2020 07/1/20

| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
|------|------|------|------|------|------|------|------|------|------|
| 0.00 | 0.00 | 0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.03 |
| 0.03 | 0.03 | 0.05 | 0.05 | 0.05 | 0.15 | 0.15 | 0.15 | 0.03 | 0.03 |
| 0.03 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 0.00 | 0.00 | 0.00 |
| 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 | 0.00 |
| 0.00 | 0.00 |      |      |      |      |      |      |      |      |

1

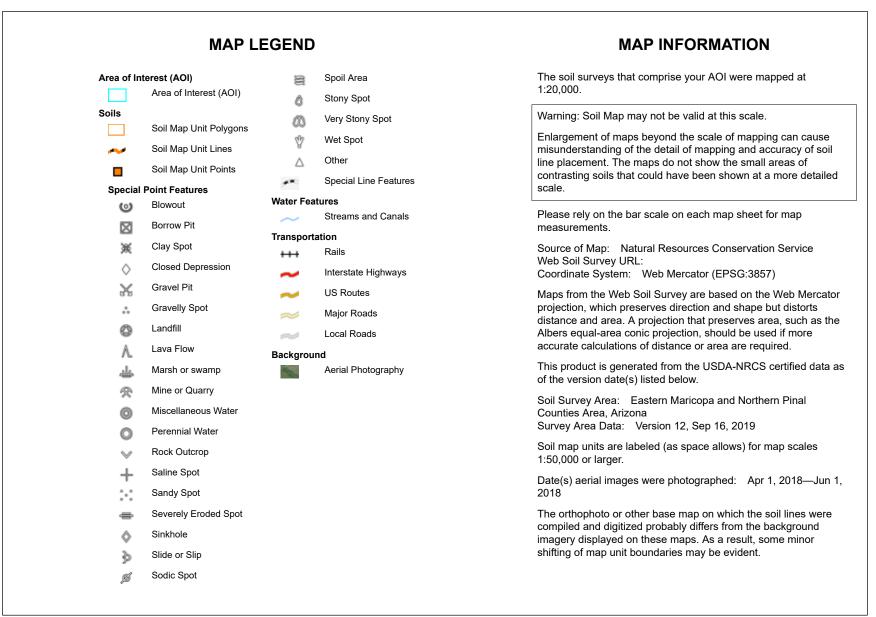
#### RUNOFF SUMMARY FLOW IN CUBIC FEET PER SECOND TIME IN HOURS, AREA IN SQUARE MILES

|   | OPERATION     | STATION | PEAK<br>FLOW | TIME OF<br>PEAK | AVERAGE FI | LOW FOR MAXIN | MUM PERIOD | BASIN<br>AREA | MAXIMUM<br>STAGE | TIME OF<br>MAX STAGE |
|---|---------------|---------|--------------|-----------------|------------|---------------|------------|---------------|------------------|----------------------|
| + |               |         | -            |                 | 6-HOUR     | 24-HOUR       | 72-HOUR    |               |                  |                      |
|   | HYDROGRAPH AT |         |              |                 |            |               |            |               |                  |                      |
| + |               | 1       | 23.          | 4.17            | 4.         | 1.            | 0.         | 0.02          |                  |                      |

\*\*\* NORMAL END OF HEC-1 \*\*\*



USDA Natural Resources Conservation Service Web Soil Survey National Cooperative Soil Survey <sup>6/10/202</sup> Page 1 of 3 07/1/20



Soil Map-Eastern Maricopa and Northern Pinal Counties Area, Arizona



USDA

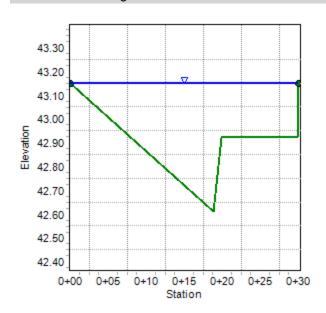
# Map Unit Legend

| Map Unit Symbol             | Map Unit Name                                | Acres in AOI | Percent of AOI |
|-----------------------------|--|--------------|----------------|
| LaA                         | Laveen loam, 0 to 1 percent slopes           | 1.9          | 14.2%          |
| RiA                         | Rillito gravelly loam, 0 to 1 percent slopes | 11.7         | 85.8%          |
| Totals for Area of Interest |  | 13.7         | 100.0%         |



# **Cross Section for 70th Street Section A**

| Project Description          |                              |       |
|------------------------------|------------------------------|-------|
| Friction Method<br>Solve For | Manning Formula<br>Discharge |       |
| Input Data                   |                              |       |
| Channel Slope                | 0.25000                      | %     |
| Normal Depth                 | 0.54                         | ft    |
| Discharge                    | 18.15                        | ft³/s |
| Cross Section Image          |                              |       |



# Worksheet for 70th Street Section A

|  | STRATECT IO                              | 70111 51100    |                     |                       |       |
|--|--|----------------|---------------------|-----------------------|-------|
| Project Description  |  |                |                     |                       |       |
| Friction Method  | Manning Formula                          |                |                     |                       |       |
| Solve For  | Discharge                                |                |                     |                       |       |
| Input Data   |  |                |                     |                       |       |
| Channel Slope  |  | 0.25000        | %                   |                       |       |
| Normal Depth   |  |                | <sup>70</sup><br>ft |                       |       |
| Section Definitions  |  | 0.01           | i.                  |                       |       |
|  |  |                |                     |                       |       |
|  |  |                |                     |                       |       |
| Station (ft)   |  | Elevation (ft) |                     |                       |       |
| Station (it)   |  |                |                     |                       |       |
|  | 0+00                                     |                | 43.15               |                       |       |
|  | 0+19                                     |                | 42.61               |                       |       |
|  | 0+20                                     |                | 42.92               |                       |       |
|  | 0+30                                     |                | 42.92               |                       |       |
|  | 0+30                                     |                | 43.15               |                       |       |
| Roughness Segment Definitions                                    |  |                |                     |                       |       |
|  |  |                |                     |                       |       |
|  |  |                |                     |                       |       |
| Start Station  |  | Ending Station |                     | Roughness Coefficient |       |
|  |  |                |                     |                       |       |
| (0+00,   | 43.15)                                   | (0+3           | 0, 43.15)           |                       | 0.013 |
| Options  |  |                |                     |                       |       |
| Current Roughness Weighted                                       |  |                |                     |                       |       |
| Method   | Pavlovskii's Metho<br>Pavlovskii's Metho |                |                     |                       |       |
| Open Channel Weighting Method<br>Closed Channel Weighting Method | Pavlovskii's Metho                       |                |                     |                       |       |
|  |  |                |                     |                       |       |
| Results  |  |                |                     |                       |       |
| Discharge  |  | 18.15          | ft³/s               |                       |       |
| Elevation Range  | 42.61 to 43.15 ft                        |                |                     |                       |       |
| Flow Area  |  | 7.83           | ft²                 |                       |       |
| Wetted Perimeter   |  | 30.28          | ft                  |                       |       |
| Hydraulic Radius   |  | 0.26<br>30.00  | ft<br>#             |                       |       |
| Top Width<br>Normal Depth  |  | 0.54           | ft<br>ft            |                       |       |
| Critical Depth   |  |                | ft                  |                       |       |
|  |  |                |                     |                       |       |

Bentley Systems, Inc. Haestad Methods SoBdidle CEnterMaster V8i (SELECTseries 1) [08.11.01.03]

4/7/2020 11:13:08 AM

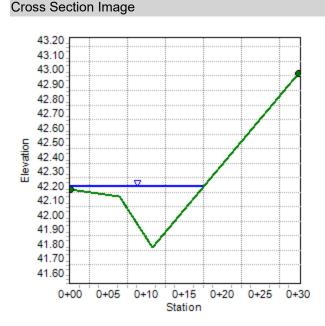
27 Siemons Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2

# Worksheet for 70th Street Section A

| Results             |             |          |       |
|---------------------|-------------|----------|-------|
| Critical Slope      |             | 0.00405  | ft/ft |
| Velocity            |             | 2.32     | ft/s  |
| Velocity Head       |             | 0.08     | ft    |
| Specific Energy     |             | 0.62     | ft    |
| Froude Number       |             | 0.80     |       |
| Flow Type           | Subcritical |          |       |
| GVF Input Data      |             |          |       |
| Downstream Depth    |             | 0.00     | ft    |
| Length              |             | 0.00     | ft    |
| Number Of Steps     |             | 0        |       |
| GVF Output Data     |             |          |       |
| Upstream Depth      |             | 0.00     | ft    |
| Profile Description |             |          |       |
| Profile Headloss    |             | 0.00     | ft    |
| Downstream Velocity |             | Infinity | ft/s  |
| Upstream Velocity   |             | Infinity | ft/s  |
| Normal Depth        |             | 0.54     | ft    |
| Critical Depth      |             | 0.50     | ft    |
| Channel Slope       |             | 0.25000  | %     |
| Critical Slope      |             | 0.00405  | ft/ft |

### **Cross Section for 70th Street Section B**

| Project Description |                 |         |       |
|---------------------|-----------------|---------|-------|
| Friction Method     | Manning Formula |         |       |
| Solve For           | Normal Depth    |         |       |
| Input Data          |                 |         |       |
| Channel Slope       |                 | 0.25000 | %     |
| Normal Depth        |                 | 0.42    | ft    |
| Discharge           |                 | 4.85    | ft³/s |



Bentley Systems, Inc. Haestad Methods SoBdittle CEnterMaster V8i (SELECTseries 1) [08.11.01.03] 6/10/2020 9:29:54 AM

# Worksheet for 70th Street Section B

|  | N KSHEEL IUI                               | 70th Shee  | L JEC                 |                       |       |
|--|--|--|-----------------------|-----------------------|-------|
| Project Description  |  |  |                       |                       |       |
| Friction Method  | Manning Formula                            |  |                       |                       |       |
| Solve For  | Normal Depth                               |  |                       |                       |       |
| Input Data   |  |  |                       |                       |       |
|  |  | 0.25000  | %                     |                       |       |
| Channel Slope<br>Discharge   |  | 4.85   | ∽₀<br>ft³/s           |                       |       |
| Section Definitions  |  | 4.00   | 11 /5                 |                       |       |
|  |  |  |                       |                       |       |
|  |  |  |                       |                       |       |
|  |  |  |                       |                       |       |
| Station (ft)   |  | Elevation (ft)                                   |                       |                       |       |
|  | 0+00                                       |  | 42.17                 |                       |       |
|  | 0+06                                       |  | 42.12                 |                       |       |
|  | 0+11                                       |  | 41.77                 |                       |       |
|  | 0+30                                       |  | 42.97                 |                       |       |
| Poughnoop Sogmont Definitions  |  |  |                       |                       |       |
| Roughness Segment Definitions  |  |  |                       |                       |       |
|  |  |  |                       |                       |       |
|  |  |  |                       |                       |       |
| Start Station  | E  | Ending Station                                   |                       | Roughness Coefficient |       |
| (0+00,   | 42.17)                                     | (0+3   | 0, 42.97)             |                       | 0.013 |
| (1-1-1)  | ,  |  | -,,                   |                       |       |
| Options  |  |  |                       |                       |       |
| •  |  |  |                       |                       |       |
| Current Roughness Weighted   | Pavlovskii's Methoo                        | t  |                       |                       |       |
|  | Pavlovskii's Methoo<br>Pavlovskii's Methoo |  |                       |                       |       |
| Current Roughness Weighted Method  |  | d  |                       |                       |       |
| Current Roughness Weighted<br>Method<br>Open Channel Weighting Method  | Pavlovskii's Methoo                        | d  |                       |                       |       |
| Current Roughness Weighted<br>Method<br>Open Channel Weighting Method<br>Closed Channel Weighting Method<br>Results  | Pavlovskii's Methoo                        | d<br>d   | ft                    |                       |       |
| Current Roughness Weighted<br>Method<br>Open Channel Weighting Method<br>Closed Channel Weighting Method   | Pavlovskii's Methoo                        | d  | ft                    |                       |       |
| Current Roughness Weighted<br>Method<br>Open Channel Weighting Method<br>Closed Channel Weighting Method<br>Results<br>Normal Depth  | Pavlovskii's Methoo<br>Pavlovskii's Methoo | d<br>d   | ft<br>ft²             |                       |       |
| Current Roughness Weighted<br>Method<br>Open Channel Weighting Method<br>Closed Channel Weighting Method<br>Results<br>Normal Depth<br>Elevation Range   | Pavlovskii's Methoo<br>Pavlovskii's Methoo | 0.42   |                       |                       |       |
| Current Roughness Weighted<br>Method<br>Open Channel Weighting Method<br>Closed Channel Weighting Method<br><b>Results</b><br>Normal Depth<br>Elevation Range<br>Flow Area   | Pavlovskii's Methoo<br>Pavlovskii's Methoo | 0.42   | ft²                   |                       |       |
| Current Koughness Weighted<br>Method<br>Open Channel Weighting Method<br>Closed Channel Weighting Method<br>Results<br>Normal Depth<br>Elevation Range<br>Flow Area<br>Wetted Perimeter                                  | Pavlovskii's Methoo<br>Pavlovskii's Methoo | d<br>d<br>0.42<br>2.85<br>17.61                  | ft²<br>ft             |                       |       |
| Current Roughness Weighted<br>Method<br>Open Channel Weighting Method<br>Closed Channel Weighting Method<br>Results<br>Normal Depth<br>Elevation Range<br>Flow Area<br>Wetted Perimeter<br>Hydraulic Radius              | Pavlovskii's Methoo<br>Pavlovskii's Methoo | d<br>d<br>0.42<br>2.85<br>17.61<br>0.16          | ft²<br>ft<br>ft       |                       |       |
| Current Koughness Weighted<br>Method<br>Open Channel Weighting Method<br>Closed Channel Weighting Method<br>Results<br>Normal Depth<br>Elevation Range<br>Flow Area<br>Wetted Perimeter<br>Hydraulic Radius<br>Top Width | Pavlovskii's Methoo<br>Pavlovskii's Methoo | d<br>d<br>0.42<br>2.85<br>17.61<br>0.16<br>17.56 | ft²<br>ft<br>ft<br>ft |                       |       |

Bentley Systems, Inc. Haestad Methods SoBdittle@EnderMaster V8i (SELECTseries 1) [08.11.01.03]

27 Siemons Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2

# Worksheet for 70th Street Section B

| Results             |             |          |       |  |
|---------------------|-------------|----------|-------|--|
| Velocity            |             | 1.70     | ft/s  |  |
| Velocity Head       |             | 0.04     | ft    |  |
| Specific Energy     |             | 0.47     | ft    |  |
| Froude Number       |             | 0.74     |       |  |
| Flow Type           | Subcritical |          |       |  |
| GVF Input Data      |             |          |       |  |
| Downstream Depth    |             | 0.00     | ft    |  |
| Length              |             | 0.00     | ft    |  |
| Number Of Steps     |             | 0        |       |  |
| GVF Output Data     |             |          |       |  |
| Upstream Depth      |             | 0.00     | ft    |  |
| Profile Description |             |          |       |  |
| Profile Headloss    |             | 0.00     | ft    |  |
| Downstream Velocity |             | Infinity | ft/s  |  |
| Upstream Velocity   |             | Infinity | ft/s  |  |
| Normal Depth        |             | 0.42     | ft    |  |
| Critical Depth      |             | 0.39     | ft    |  |
| Channel Slope       |             | 0.25000  | %     |  |
| Critical Slope      |             | 0.00471  | ft/ft |  |
|                     |             |          |       |  |

# **Cross Section for Section B Weir**

| Project Description    |           |      |       |         |
|------------------------|-----------|------|-------|---------|
| Solve For              | Discharge |      |       |         |
| Input Data             |           |      |       |         |
| Discharge              |           | 0.17 | ft³/s |         |
| Headwater Elevation    |           | 0.02 | ft    |         |
| Crest Elevation        |           | 0.00 | ft    |         |
| Tailwater Elevation    |           | 0.00 | ft    |         |
| Weir Coefficient       |           | 3.00 | US    |         |
| Crest Length           | 2         | 0.00 | ft    |         |
| Number Of Contractions | 0         |      |       |         |
| Cross Section Image    |           |      |       |         |
|                        | <b>v</b>  |      |       | 0.02 ft |

20.00 ft

V: 1 **N** H: 1



### Worksheet for Section B Weir

| Project Description          |           |       |       |
|------------------------------|-----------|-------|-------|
| Solve For                    | Discharge |       |       |
| Input Data                   |           |       |       |
| Headwater Elevation          |           | 0.02  | ft    |
| Crest Elevation              |           | 0.00  | ft    |
| Tailwater Elevation          |           | 0.00  | ft    |
| Weir Coefficient             |           | 3.00  | US    |
| Crest Length                 |           | 20.00 | ft    |
| Number Of Contractions       | 0         |       |       |
| Results                      |           |       |       |
| Discharge                    |           | 0.17  | ft³/s |
| Headwater Height Above Crest |           | 0.02  | ft    |
| Tailwater Height Above Crest |           | 0.00  | ft    |
| Flow Area                    |           | 0.40  | ft²   |
| Velocity                     |           | 0.42  | ft/s  |
| Wetted Perimeter             |           | 20.04 | ft    |
| Top Width                    |           | 20.00 | ft    |
|                              |           |       |       |

### **Cross Section for 70th Street Section C**

| Project Description          |                              |         |       |  |
|------------------------------|------------------------------|---------|-------|--|
| Friction Method<br>Solve For | Manning Formula<br>Discharge |         |       |  |
| Input Data                   |                              |         |       |  |
| Channel Slope                |                              | 0.25000 | %     |  |
| Normal Depth                 |                              | 0.62    | ft    |  |
| Discharge                    |                              | 7.95    | ft³/s |  |
| Cross Section Image          |                              |         |       |  |

#### 43.00 42.90 42.80 42.70 42.60 42.50 42.40 Elevation -42.30 42.20 42.10 42.00 41.90 41.80 41.70 41.60 41.50 0+05 0+00 0+10 0+15 0+20 0+25 0+30 Station

 Bentley Systems, Inc. Haestad Methods SoBdititie@Efitier/Master V8i (SELECTseries 1) [08.11.01.03]

 4/7/2020 11:15:05 AM
 27 Siemons Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666
 Page 1 of 1

5-ZN-2020 07/1/20

# Worksheet for 70th Street Section C

|   | JI KSHEET IOI                |                | 1 300              |                       |       |
|---|------------------------------|----------------|--------------------|-----------------------|-------|
| Project Description                     |                              |                |                    |                       |       |
| Friction Method<br>Solve For            | Manning Formula<br>Discharge |                |                    |                       |       |
|   | 2.000.00.90                  |                |                    |                       |       |
| Input Data                              |                              |                |                    |                       |       |
| Channel Slope                           |                              | 0.25000        | %                  |                       |       |
| Normal Depth                            |                              | 0.62           | ft                 |                       |       |
| Section Definitions                     |                              |                |                    |                       |       |
|   |                              |                |                    |                       |       |
|   |                              |                |                    |                       |       |
| Station (ft)                            |                              | Elevation (ft) |                    |                       |       |
|   |                              |                |                    |                       |       |
|   | 0+00                         |                | 42.35              |                       |       |
|   | 0+05<br>0+11                 |                | 42.27<br>42.23     |                       |       |
|   | 0+11                         |                | 42.23              |                       |       |
|   | 0+30                         |                | 42.79              |                       |       |
|   |                              |                |                    |                       |       |
| Roughness Segment Definitions           |                              |                |                    |                       |       |
|   |                              |                |                    |                       |       |
|   |                              |                |                    |                       |       |
| Start Station                           |                              | Ending Station |                    | Roughness Coefficient |       |
| (0+00,                                  | 42.35)                       | (0+3           | 0, 42.79)          |                       | 0.013 |
| , , , , , , , , , , , , , , , , , , ,   | ,                            | , ,            | . ,                |                       |       |
| Options                                 |                              |                |                    |                       |       |
| Current Roughness Weighted              | Pavlovskii's Metho           | d              |                    |                       |       |
| Method<br>Open Channel Weighting Method | Pavlovskii's Metho           | d              |                    |                       |       |
| Closed Channel Weighting Method         | Pavlovskii's Metho           | d              |                    |                       |       |
| Results                                 |                              |                |                    |                       |       |
| Discharge                               |                              | 7.95           | ft <sup>3</sup> /c |                       |       |
| Elevation Range                         | 41.73 to 42.79 ft            | 1.00           | 11/5               |                       |       |
| Flow Area                               |                              | 4.24           | ft²                |                       |       |
| Wetted Perimeter                        |                              | 22.55          | ft                 |                       |       |
| Hydraulic Radius                        |                              | 0.19           | ft                 |                       |       |
| Top Width                               |                              | 22.03          | ft                 |                       |       |
| Normal Depth                            |                              | 0.62           | ft                 |                       |       |
| Critical Depth                          |                              | 0.57           | ft                 |                       |       |
|   |                              |                |                    |                       |       |

Bentley Systems, Inc. Haestad Methods SoBdidle CEnterMaster V8i (SELECTseries 1) [08.11.01.03]

4/7/2020 11:15:22 AM

27 Siemons Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2

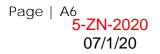
# Worksheet for 70th Street Section C

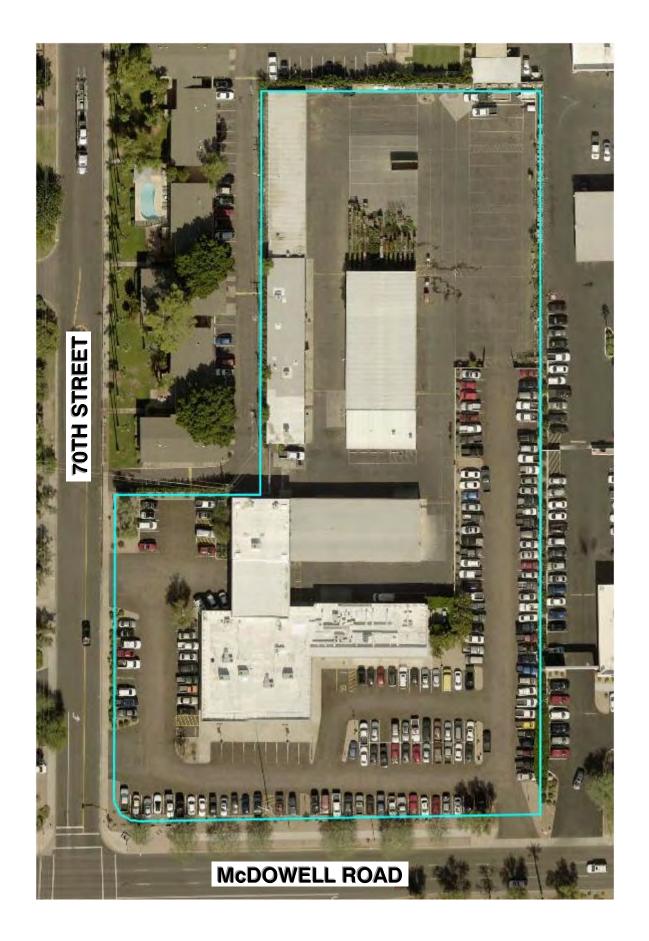
| Results             |             |          |       |
|---------------------|-------------|----------|-------|
| Critical Slope      |             | 0.00451  | ft/ft |
| Velocity            |             | 1.88     | ft/s  |
| Velocity Head       |             | 0.05     | ft    |
| Specific Energy     |             | 0.67     | ft    |
| Froude Number       |             | 0.75     |       |
| Flow Type           | Subcritical |          |       |
| GVF Input Data      |             |          |       |
| Downstream Depth    |             | 0.00     | ft    |
| Length              |             | 0.00     | ft    |
| Number Of Steps     |             | 0        |       |
| GVF Output Data     |             |          |       |
| Upstream Depth      |             | 0.00     | ft    |
| Profile Description |             |          |       |
| Profile Headloss    |             | 0.00     | ft    |
| Downstream Velocity |             | Infinity | ft/s  |
| Upstream Velocity   |             | Infinity | ft/s  |
| Normal Depth        |             | 0.62     | ft    |
| Critical Depth      |             | 0.57     | ft    |
| Channel Slope       |             | 0.25000  | %     |
| Critical Slope      |             | 0.00451  | ft/ft |

<u>3@engineering</u> civil engineering planning surveying

# APPENDIX F

# Aerial Site Photographs



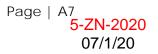


| 3@enaineerina | 157   | 3 ENGINEERING, LLC<br>6370 E, THOMAS ROAD, SUITE # 200- PHOENIX, ARIZONA 85251<br>PHONE: (602) 334-4357 - FAX; (602) 490-3230<br>TOA I/D9 / 707 1877 |    |
|---------------|---|--|----|
| SOUTHDALE     | 7000 E. MCDOWELL ROAD, SCOTTSDALE, AZ 85257 | AERIAL SITE PHOTOGRAPHS  |    |
| 1"=           | =80<br>5-Zľ                                 | ,<br><mark>N-202</mark><br>/1/20   | 20 |

<u>3@engineering</u> civil engineering planning surveying

# APPENDIX G

# Offsite Aerial Photographs



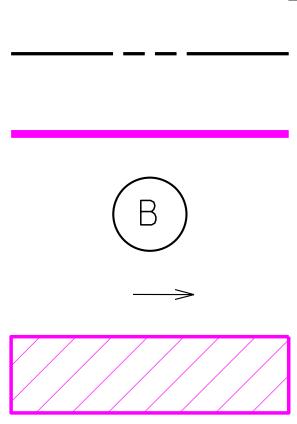


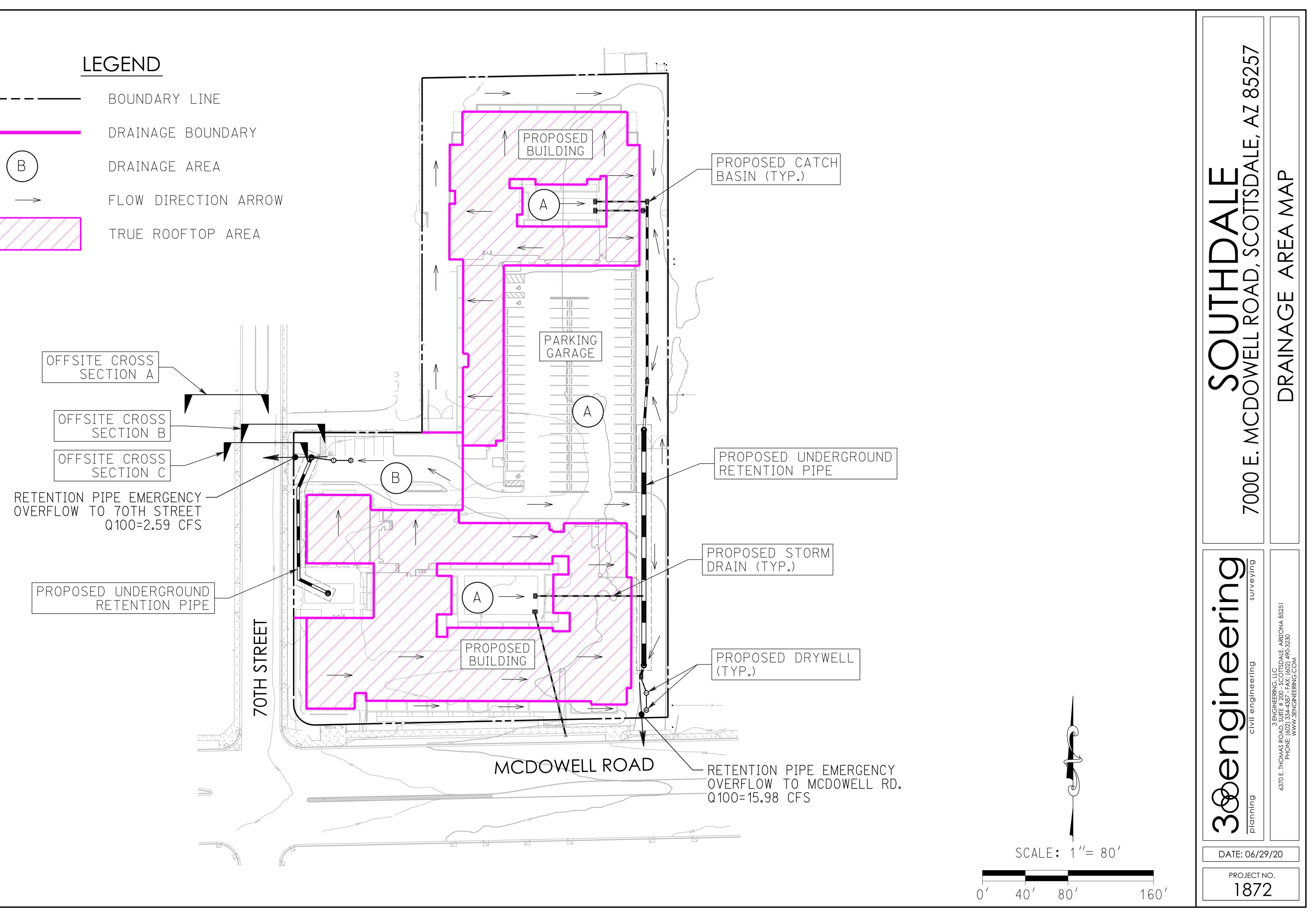
<u>3®engineering</u> civil engineering planning surveying

# APPENDIX H

## Onsite Drainage Area Map

Page | A8



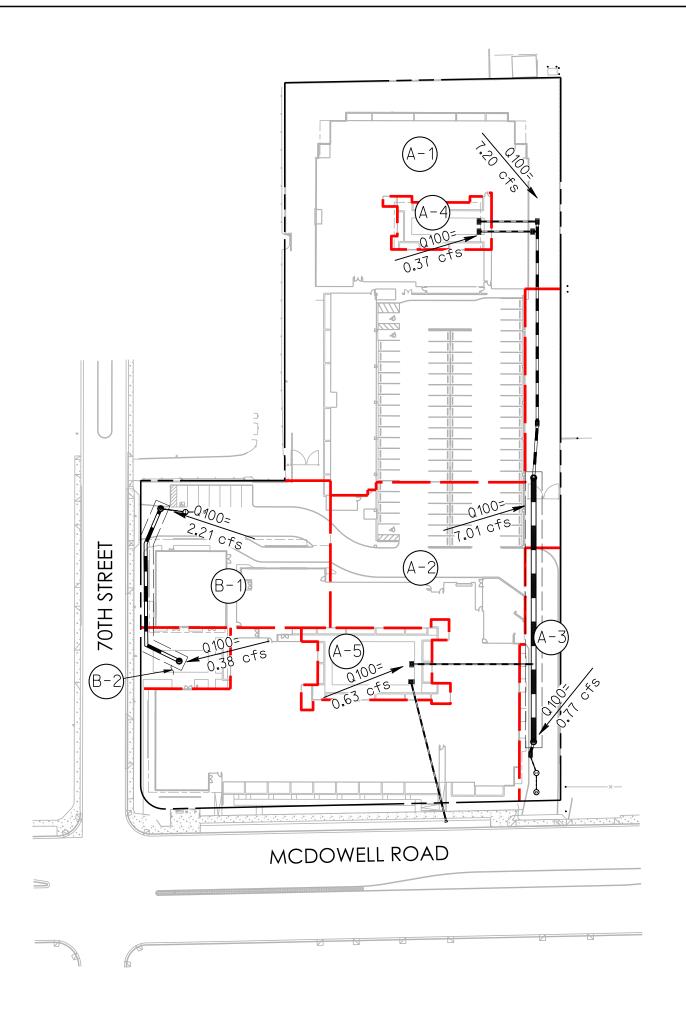


<u>3®engineering</u> civil engineering surveying planning

# APPENDIX I

# Inlet Area Exhibit

Page | A9



## LEGEND

(B-1)

BOUNDARY LINE

- DRAINAGE BOUNDARY
- DRAINAGE SUB-BOUNDARY
- DRAINAGE INLET SUB-AREA

AZ 85257

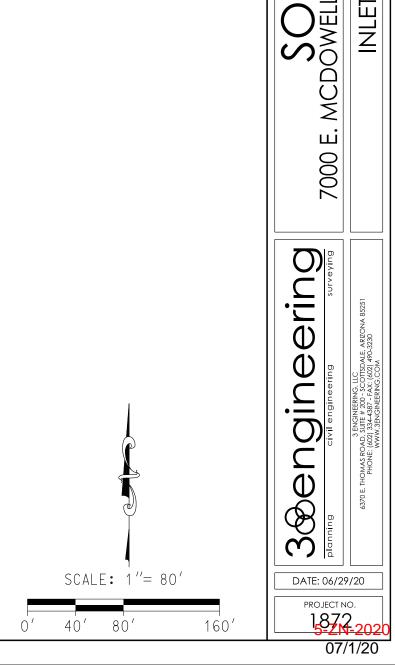
DALE Cottsdale,

) A V

2

AREA EXHIBIT

INLET



<u>3®engineering</u> civil engineering planning surveying

## APPENDIX J

# **Onsite Drainage Calculations**

Page | A10 5-ZN-2020 07/1/20

### Post-Development Rational Method Calculations

planning

| <u>1031-DCV</u> |        |             |              |       |             |              |             |              |  |  |  |
|-----------------|--------|-------------|--------------|-------|-------------|--------------|-------------|--------------|--|--|--|
| Sub-Area        | Area   | <b>C</b> 10 | <b>C</b> 100 | Tc    | <b>İ</b> 10 | <b>İ</b> 100 | <b>Q</b> 10 | <b>Q</b> 100 |  |  |  |
|                 | (acre) | (weighted)  | (weighted)   | (min) | (in/hr)     | (in/hr)      | (cfs)       | (cfs)        |  |  |  |
| A-1             | 1.59   | 0.76        | 0.81         | 10    | 3.53        | 5.6          | 4.26        | 7.20         |  |  |  |
| A-2             | 1.42   | 0.83        | 0.88         | 10    | 3.53        | 5.6          | 4.17        | 7.01         |  |  |  |
| A-3             | 0.16   | 0.83        | 0.88         | 10    | 3.53        | 5.6          | 0.46        | 0.77         |  |  |  |
| A-4             | 0.08   | 0.78        | 0.83         | 10    | 3.53        | 5.6          | 0.22        | 0.37         |  |  |  |
| A-5             | 0.15   | 0.69        | 0.74         | 10    | 3.53        | 5.6          | 0.37        | 0.63         |  |  |  |
| B-1             | 0.44   | 0.84        | 0.89         | 10    | 3.53        | 5.6          | 1.31        | 2.21         |  |  |  |
| B-2             | 0.09   | 0.73        | 0.78         | 10    | 3.53        | 5.6          | 0.22        | 0.38         |  |  |  |

civil engineering

engineering

surveying

### **On-Site Retention for the First Flush Storm**

|          |        |              |      |           |            | U.G.      |            |
|----------|--------|--------------|------|-----------|------------|-----------|------------|
|          |        |              |      | Total     | Surface    | Retention | Total      |
| Sub-Area | Area   | <b>C</b> 100 | Р    | Vol. Req. | Vol. Prov. | Provided  | Vol. Prov. |
|          | (acre) |              | (in) | (cf)      | (cf)       | (cf)      | (cf)       |
| А        | 1.96   | 0.76         | 0.50 | 2,697     | -          | 2,764     | 2,764      |
| В        | 0.35   | 0.82         | 0.50 | 517       | -          | 702       | 702        |

### PRE V. POST RETENTION CALCULATIONS

C = 0.95 (IMPERVIOUS), C = 0.45 (PERVIOUS) P = 2.14 IN AREA OF LOT = 171,290 SF PRE (EXISTING) AREA OF IMPERVIOUS = 161,857 SF AREA OF PERVIOUS = 9,433 SF (161,857 X 0.95) + (9,433 X 0.45) WEIGHTED C = 171,290 WEIGHTED C = 0.92POST (PROPOSED) AREA OF IMPERVIOUS = 134,825 SF AREA OF PERVIOUS = 36,465 SF WEIGHTED C =  $\begin{pmatrix} (134,825 \times 0.95) + (36,465 \times 0.45) \\ 171,290 \end{pmatrix}$ WEIGHTED C = 0.84(0.84-0.92)  $\left(\frac{2.14}{12}\right)$  (171,290) = [O CF REQUIRED

SOUTHDALE 6/29/2020

Dengineering surveying

### Grated Inlet Capacity - Weir Condition

planning

|                  |       |              | Inlet Capacity |      |    |       |
|------------------|-------|--------------|----------------|------|----|-------|
|                  |       |              | w/ 40%         |      |    |       |
| Inlet Type       | Inlet | <b>Q</b> 100 | Clogging       | d    | Cw | Р     |
|                  |       | (cfs)        | (cfs)          | (ft) |    | (ft)  |
| M.A.G. type "F"  | A-1   | 7.20         | 7.53           | 0.50 | 3  | 11.83 |
| M.A.G. type "F"  | A-2   | 7.01         | 7.53           | 0.50 | 3  | 11.83 |
| M.A.G. type "F"  | A-3   | 0.77         | 7.53           | 0.50 | 3  | 11.83 |
| M.A.G. type "F"  | A-4   | 0.37         | 2.66           | 0.25 | 3  | 11.83 |
| M.A.G. type "F"  | A-5   | 0.63         | 2.66           | 0.25 | 3  | 11.83 |
| 30" Grated Inlet | B-1   | 2.21         | 5.00           | 0.50 | 3  | 7.85  |
| 30" Grated Inlet | B-2   | 0.38         | 3.71           | 0.41 | 3  | 7.85  |

Q=Cw\*P\*d^1.5

Cw= 3.0 weir coefficient

Q = discharge capacity

P = inlet perimeterd = flow depth

SOUTHDALE 6/29/2020

#### Bengineering surveying planning

civil engineering

### Weighted C Coefficient Calculations

|     |             | Building &   |             |            |             |              |
|-----|-------------|--------------|-------------|------------|-------------|--------------|
|     | Overall     | Parking Area | Landscape   | Overall    |             |              |
|     | Area (s.f.) | (s.f.)       | Area (s.f.) | Area (Ac.) | <b>C</b> 10 | <b>C</b> 100 |
| A   | 85398       | 52,605       | 32,793      | 1.96       | 0.71        | 0.76         |
| В   | 15049       | 11,269       | 3,779       | 0.35       | 0.77        | 0.82         |
| A-1 | 69250       | 49,721       | 19,529      | 1.59       | 0.76        | 0.81         |
| A-2 | 61955       | 53,296       | 8,658       | 1.42       | 0.83        | 0.88         |
| A-3 | 6850        | 5,835        | 1,015       | 0.16       | 0.83        | 0.88         |
| A-4 | 3408        | 2,618        | 790         | 0.08       | 0.78        | 0.83         |
| A-5 | 6638        | 3,890        | 2,748       | 0.15       | 0.69        | 0.74         |
| B-1 | 19371       | 16,912       | 2,459       | 0.44       | 0.84        | 0.89         |
| B-2 | 3818        | 2,498        | 1,320       | 0.09       | 0.73        | 0.78         |

C=((Building & Hardscape Area x 0.95) + (Landscape Area x 0.45)) / Overall Area

**C**100 Building & Hardscape = 0.95

**C**100 Landscape = 0.45

> Page 1 of 1 5-ZN-2020 07/1/20

SOUTHDALE 6/29/2020

3 engineering surveying

### **Drywell Percolation Rates**

|          |            |        | # of     | Drywell   |
|----------|------------|--------|----------|-----------|
|          | Total      | Dry-Up | Drywells | Perc Rate |
| Sub-Area | Basin Vol. | Time   | Provided | Required  |
|          | (cf)       | (hr)   |          | (cf/s)    |
| A        | 2,764      | 36.00  | 1        | 0.02      |
| В        | 702        | 36.00  | 1        | 0.01      |
|          |            |        |          |           |

Page 1 of 1 5-ZN-2020 07/1/20

5-ZN-2020



NOAA Atlas 14, Volume 1, Version 5 Location name: Scottsdale, Arizona, USA\* Latitude: 33.4662°, Longitude: -111.93° Elevation: 1237.91 ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### **PF** tabular

| D        |                               |                               |                               | Averag                        | ge recurrenc                  | e interval (                  | /ears)                        |                               |                               |                             |
|----------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-------------------------------|-----------------------------|
| Duration | 1                             | 2                             | 5                             | 10                            | 25                            | 50                            | 100                           | 200                           | 500                           | 1000                        |
| 5-min    | <b>0.180</b><br>(0.152-0.218) | <b>0.235</b><br>(0.199-0.286) | <b>0.321</b><br>(0.269-0.387) | <b>0.386</b><br>(0.322-0.464) | <b>0.475</b><br>(0.390-0.567) | <b>0.544</b><br>(0.440-0.647) | <b>0.613</b><br>(0.487-0.727) | <b>0.684</b><br>(0.535-0.812) | <b>0.780</b><br>(0.594-0.926) | <b>0.853</b><br>(0.637-1.02 |
| 10-min   | <b>0.274</b><br>(0.231-0.332) | <b>0.359</b><br>(0.303-0.435) | <b>0.488</b><br>(0.410-0.589) | <b>0.588</b><br>(0.491-0.705) | <b>0.722</b><br>(0.593-0.864) | <b>0.827</b><br>(0.670-0.984) | <b>0.933</b><br>(0.742-1.11)  | <b>1.04</b><br>(0.815-1.24)   | <b>1.19</b><br>(0.904-1.41)   | <b>1.30</b><br>(0.969-1.55  |
| 15-min   | <b>0.340</b><br>(0.286-0.412) | <b>0.444</b><br>(0.376-0.538) | <b>0.606</b><br>(0.508-0.730) | <b>0.729</b><br>(0.608-0.874) | <b>0.895</b><br>(0.735-1.07)  | <b>1.02</b><br>(0.831-1.22)   | <b>1.16</b><br>(0.920-1.37)   | <b>1.29</b><br>(1.01-1.53)    | <b>1.47</b><br>(1.12-1.75)    | <b>1.61</b><br>(1.20-1.92   |
| 30-min   | <b>0.457</b><br>(0.385-0.555) | <b>0.598</b><br>(0.506-0.725) | <b>0.815</b><br>(0.684-0.983) | <b>0.982</b><br>(0.819-1.18)  | <b>1.21</b><br>(0.990-1.44)   | <b>1.38</b><br>(1.12-1.64)    | <b>1.56</b><br>(1.24-1.85)    | <b>1.74</b><br>(1.36-2.06)    | <b>1.98</b><br>(1.51-2.35)    | <b>2.17</b><br>(1.62-2.58   |
| 60-min   | <b>0.566</b><br>(0.477-0.686) | <b>0.740</b><br>(0.626-0.897) | <b>1.01</b><br>(0.847-1.22)   | <b>1.22</b><br>(1.01-1.46)    | <b>1.49</b><br>(1.23-1.78)    | <b>1.71</b><br>(1.39-2.03)    | <b>1.93</b><br>(1.53-2.29)    | <b>2.15</b><br>(1.68-2.55)    | <b>2.45</b><br>(1.87-2.91)    | <b>2.68</b><br>(2.00-3.19   |
| 2-hr     | <b>0.657</b><br>(0.563-0.781) | <b>0.851</b><br>(0.728-1.01)  | <b>1.14</b><br>(0.974-1.35)   | <b>1.36</b><br>(1.15-1.61)    | <b>1.67</b><br>(1.39-1.95)    | <b>1.90</b><br>(1.56-2.22)    | <b>2.14</b><br>(1.73-2.50)    | <b>2.38</b><br>(1.89-2.78)    | <b>2.71</b> (2.10-3.17)       | <b>2.96</b><br>(2.25-3.49   |
| 3-hr     | <b>0.712</b><br>(0.606-0.850) | <b>0.912</b><br>(0.781-1.10)  | <b>1.20</b><br>(1.02-1.44)    | <b>1.43</b><br>(1.21-1.70)    | <b>1.75</b><br>(1.46-2.07)    | <b>2.00</b><br>(1.65-2.36)    | <b>2.27</b><br>(1.83-2.68)    | <b>2.55</b><br>(2.02-3.00)    | <b>2.94</b><br>(2.26-3.46)    | <b>3.25</b><br>(2.43-3.84   |
| 6-hr     | <b>0.857</b><br>(0.745-1.00)  | <b>1.09</b><br>(0.949-1.27)   | <b>1.40</b><br>(1.21-1.63)    | <b>1.64</b><br>(1.42-1.91)    | <b>1.98</b><br>(1.68-2.29)    | <b>2.24</b><br>(1.88-2.58)    | <b>2.52</b><br>(2.07-2.90)    | <b>2.80</b><br>(2.26-3.23)    | <b>3.18</b> (2.51-3.68)       | <b>3.49</b><br>(2.68-4.05   |
| 12-hr    | <b>0.961</b><br>(0.843-1.11)  | <b>1.22</b><br>(1.07-1.41)    | <b>1.54</b><br>(1.35-1.78)    | <b>1.80</b><br>(1.56-2.07)    | <b>2.15</b><br>(1.84-2.47)    | <b>2.41</b><br>(2.05-2.77)    | <b>2.69</b><br>(2.25-3.08)    | <b>2.96</b><br>(2.44-3.41)    | <b>3.34</b><br>(2.68-3.85)    | <b>3.63</b><br>(2.86-4.22   |
| 24-hr    | <b>1.16</b> (1.04-1.30)       | <b>1.47</b><br>(1.32-1.65)    | <b>1.90</b><br>(1.70-2.13)    | <b>2.25</b> (2.00-2.51)       | <b>2.72</b> (2.41-3.04)       | <b>3.10</b><br>(2.73-3.45)    | <b>3.49</b><br>(3.05-3.89)    | <b>3.90</b><br>(3.38-4.34)    | <b>4.46</b> (3.82-4.97)       | <b>4.90</b><br>(4.16-5.47   |
| 2-day    | <b>1.25</b><br>(1.12-1.40)    | <b>1.60</b><br>(1.44-1.79)    | <b>2.10</b><br>(1.88-2.35)    | <b>2.50</b><br>(2.23-2.79)    | <b>3.06</b><br>(2.71-3.41)    | <b>3.50</b><br>(3.08-3.91)    | <b>3.97</b><br>(3.48-4.44)    | <b>4.45</b><br>(3.87-4.98)    | <b>5.14</b><br>(4.41-5.76)    | <b>5.68</b><br>(4.83-6.40   |
| 3-day    | <b>1.32</b><br>(1.19-1.48)    | <b>1.69</b><br>(1.52-1.90)    | <b>2.22</b> (1.99-2.49)       | <b>2.65</b> (2.37-2.96)       | <b>3.26</b><br>(2.89-3.63)    | <b>3.74</b> (3.30-4.17)       | <b>4.26</b> (3.73-4.75)       | <b>4.80</b><br>(4.17-5.36)    | <b>5.56</b> (4.77-6.21)       | <b>6.17</b><br>(5.24-6.92   |
| 4-day    | <b>1.39</b><br>(1.25-1.56)    | <b>1.78</b> (1.60-2.00)       | <b>2.35</b><br>(2.10-2.62)    | <b>2.81</b> (2.50-3.13)       | <b>3.46</b><br>(3.07-3.85)    | <b>3.98</b><br>(3.51-4.43)    | <b>4.55</b> (3.98-5.06)       | <b>5.14</b><br>(4.46-5.73)    | <b>5.98</b> (5.12-6.67)       | <b>6.66</b><br>(5.65-7.45   |
| 7-day    | <b>1.54</b><br>(1.38-1.73)    | <b>1.97</b><br>(1.77-2.20)    | <b>2.60</b><br>(2.32-2.90)    | <b>3.10</b> (2.77-3.47)       | <b>3.82</b> (3.39-4.27)       | <b>4.40</b> (3.88-4.91)       | <b>5.02</b> (4.39-5.60)       | <b>5.67</b><br>(4.92-6.33)    | <b>6.60</b> (5.65-7.36)       | <b>7.34</b><br>(6.22-8.21   |
| 10-day   | <b>1.68</b><br>(1.50-1.87)    | <b>2.14</b><br>(1.92-2.40)    | <b>2.83</b><br>(2.53-3.15)    | <b>3.38</b><br>(3.01-3.76)    | <b>4.14</b> (3.68-4.61)       | <b>4.76</b> (4.20-5.30)       | <b>5.42</b><br>(4.75-6.03)    | <b>6.11</b><br>(5.31-6.80)    | <b>7.07</b><br>(6.07-7.88)    | <b>7.85</b><br>(6.67-8.76   |
| 20-day   | <b>2.06</b><br>(1.85-2.29)    | <b>2.65</b><br>(2.38-2.94)    | <b>3.49</b><br>(3.13-3.88)    | <b>4.13</b><br>(3.70-4.58)    | <b>4.99</b><br>(4.45-5.54)    | <b>5.65</b><br>(5.02-6.27)    | <b>6.33</b> (5.59-7.03)       | <b>7.01</b><br>(6.16-7.79)    | <b>7.93</b> (6.91-8.84)       | <b>8.64</b><br>(7.47-9.64   |
| 30-day   | <b>2.40</b><br>(2.15-2.67)    | <b>3.09</b><br>(2.78-3.44)    | <b>4.07</b><br>(3.65-4.51)    | <b>4.82</b> (4.31-5.33)       | <b>5.82</b> (5.18-6.44)       | <b>6.59</b><br>(5.84-7.28)    | <b>7.37</b><br>(6.51-8.15)    | <b>8.17</b><br>(7.18-9.04)    | <b>9.25</b> (8.07-10.2)       | <b>10.1</b><br>(8.71-11.2   |
| 45-day   | <b>2.79</b><br>(2.51-3.10)    | <b>3.59</b><br>(3.24-3.99)    | <b>4.73</b> (4.26-5.25)       | <b>5.57</b> (5.00-6.18)       | <b>6.68</b> (5.98-7.41)       | <b>7.52</b> (6.70-8.33)       | <b>8.36</b> (7.42-9.27)       | <b>9.20</b> (8.13-10.2)       | <b>10.3</b> (9.04-11.5)       | <b>11.1</b> (9.72-12.4      |
| 60-day   | <b>3.09</b><br>(2.79-3.42)    | <b>3.99</b><br>(3.60-4.42)    | <b>5.25</b> (4.73-5.81)       | <b>6.16</b> (5.54-6.81)       | <b>7.35</b><br>(6.59-8.13)    | <b>8.23</b><br>(7.35-9.11)    | <b>9.11</b> (8.11-10.1)       | <b>9.97</b> (8.84-11.0)       | <b>11.1</b> (9.78-12.3)       | <b>11.9</b> (10.5-13.3      |

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values. Please refer to NOAA Atlas 14 document for more information.

Back to Top

5-ZN-2020



NOAA Atlas 14, Volume 1, Version 5 Location name: Scottsdale, Arizona, USA\* Latitude: 33.4662°, Longitude: -111.93° Elevation: 1237.91 ft\*\* \* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

#### **PF** tabular

| PDS-b    | PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches/hour) <sup>1</sup> |                            |                            |                            |                            |                            |                            |                            |                            |                            |  |  |  |
|----------|---|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|--|--|--|
| Duration |   |                            |                            | Avera                      | ge recurren                | ce interval (              | years)                     |                            |                            |                            |  |  |  |
| Duration | 1   | 2                          | 5                          | 10                         | 25                         | 50                         | 100                        | 200                        | 500                        | 1000                       |  |  |  |
| 5-min    | <b>2.16</b><br>(1.82-2.62)  | <b>2.82</b><br>(2.39-3.43) | <b>3.85</b><br>(3.23-4.64) | <b>4.63</b><br>(3.86-5.57) | <b>5.70</b><br>(4.68-6.80) | <b>6.53</b><br>(5.28-7.76) | <b>7.36</b><br>(5.84-8.72) | <b>8.21</b><br>(6.42-9.74) | <b>9.36</b><br>(7.13-11.1) | <b>10.2</b> (7.64-12.2)    |  |  |  |
| 10-min   | <b>1.64</b><br>(1.39-1.99)  | <b>2.15</b><br>(1.82-2.61) | <b>2.93</b><br>(2.46-3.53) | <b>3.53</b><br>(2.95-4.23) | <b>4.33</b><br>(3.56-5.18) | <b>4.96</b><br>(4.02-5.90) | <b>5.60</b><br>(4.45-6.64) | <b>6.25</b> (4.89-7.41)    | <b>7.12</b> (5.42-8.46)    | <b>7.79</b><br>(5.81-9.28) |  |  |  |
| 15-min   | <b>1.36</b>   | <b>1.78</b>                | <b>2.42</b>                | <b>2.92</b>                | <b>3.58</b>                | <b>4.10</b>                | <b>4.63</b>                | <b>5.16</b>                | <b>5.88</b>                | <b>6.44</b>                |  |  |  |
|          | (1.14-1.65)   | (1.50-2.15)                | (2.03-2.92)                | (2.43-3.50)                | (2.94-4.28)                | (3.32-4.88)                | (3.68-5.49)                | (4.04-6.12)                | (4.48-6.99)                | (4.80-7.66)                |  |  |  |
| 30-min   | <b>0.914</b>  | <b>1.20</b>                | <b>1.63</b>                | <b>1.96</b>                | <b>2.41</b>                | <b>2.76</b>                | <b>3.11</b>                | <b>3.48</b>                | <b>3.96</b>                | <b>4.34</b>                |  |  |  |
|          | (0.770-1.11)  | (1.01-1.45)                | (1.37-1.97)                | (1.64-2.36)                | (1.98-2.88)                | (2.24-3.29)                | (2.48-3.70)                | (2.72-4.12)                | (3.02-4.71)                | (3.24-5.16)                |  |  |  |
| 60-min   | <b>0.566</b>  | <b>0.740</b>               | <b>1.01</b>                | <b>1.22</b>                | <b>1.49</b>                | <b>1.71</b>                | <b>1.93</b>                | <b>2.15</b>                | <b>2.45</b>                | <b>2.68</b>                |  |  |  |
|          | (0.477-0.686)   | (0.626-0.897)              | (0.847-1.22)               | (1.01-1.46)                | (1.23-1.78)                | (1.39-2.03)                | (1.53-2.29)                | (1.68-2.55)                | (1.87-2.91)                | (2.00-3.19)                |  |  |  |
| 2-hr     | <b>0.328</b>  | <b>0.426</b>               | <b>0.571</b>               | <b>0.682</b>               | <b>0.832</b>               | <b>0.949</b>               | <b>1.07</b>                | <b>1.19</b>                | <b>1.35</b>                | <b>1.48</b>                |  |  |  |
|          | (0.282-0.390)   | (0.364-0.506)              | (0.487-0.676)              | (0.575-0.804)              | (0.694-0.977)              | (0.780-1.11)               | (0.866-1.25)               | (0.947-1.39)               | (1.05-1.59)                | (1.12-1.75)                |  |  |  |
| 3-hr     | <b>0.237</b>  | <b>0.304</b>               | <b>0.400</b>               | <b>0.476</b>               | <b>0.582</b>               | <b>0.667</b>               | <b>0.757</b>               | <b>0.849</b>               | <b>0.978</b>               | <b>1.08</b>                |  |  |  |
|          | (0.202-0.283)   | (0.260-0.365)              | (0.340-0.478)              | (0.402-0.566)              | (0.485-0.689)              | (0.548-0.787)              | (0.610-0.892)              | (0.673-0.999)              | (0.751-1.15)               | (0.811-1.28)               |  |  |  |
| 6-hr     | <b>0.143</b>  | <b>0.181</b>               | <b>0.233</b>               | <b>0.274</b>               | <b>0.330</b>               | <b>0.374</b>               | <b>0.420</b>               | <b>0.467</b>               | <b>0.532</b>               | <b>0.582</b>               |  |  |  |
|          | (0.124-0.168)   | (0.158-0.213)              | (0.203-0.272)              | (0.236-0.319)              | (0.281-0.382)              | (0.313-0.431)              | (0.346-0.484)              | (0.377-0.539)              | (0.419-0.615)              | (0.448-0.676)              |  |  |  |
| 12-hr    | <b>0.080</b>  | <b>0.101</b>               | <b>0.128</b>               | <b>0.150</b>               | <b>0.178</b>               | <b>0.200</b>               | <b>0.223</b>               | <b>0.246</b>               | <b>0.277</b>               | <b>0.301</b>               |  |  |  |
|          | (0.070-0.092)   | (0.089-0.117)              | (0.112-0.148)              | (0.130-0.172)              | (0.153-0.205)              | (0.170-0.229)              | (0.186-0.256)              | (0.203-0.283)              | (0.223-0.320)              | (0.237-0.350)              |  |  |  |
| 24-hr    | <b>0.048</b>  | <b>0.061</b>               | <b>0.079</b>               | <b>0.094</b>               | <b>0.113</b>               | <b>0.129</b>               | <b>0.145</b>               | <b>0.162</b>               | <b>0.186</b>               | <b>0.204</b>               |  |  |  |
|          | (0.043-0.054)   | (0.055-0.069)              | (0.071-0.089)              | (0.083-0.105)              | (0.100-0.127)              | (0.114-0.144)              | (0.127-0.162)              | (0.141-0.181)              | (0.159-0.207)              | (0.173-0.228)              |  |  |  |
| 2-day    | <b>0.026</b>  | <b>0.033</b>               | <b>0.044</b>               | <b>0.052</b>               | <b>0.064</b>               | <b>0.073</b>               | <b>0.083</b>               | <b>0.093</b>               | <b>0.107</b>               | <b>0.118</b>               |  |  |  |
|          | (0.023-0.029)   | (0.030-0.037)              | (0.039-0.049)              | (0.046-0.058)              | (0.056-0.071)              | (0.064-0.081)              | (0.072-0.092)              | (0.081-0.104)              | (0.092-0.120)              | (0.101-0.133)              |  |  |  |
| 3-day    | <b>0.018</b>  | <b>0.023</b>               | <b>0.031</b>               | <b>0.037</b>               | <b>0.045</b>               | <b>0.052</b>               | <b>0.059</b>               | <b>0.067</b>               | <b>0.077</b>               | <b>0.086</b>               |  |  |  |
|          | (0.016-0.021)   | (0.021-0.026)              | (0.028-0.035)              | (0.033-0.041)              | (0.040-0.050)              | (0.046-0.058)              | (0.052-0.066)              | (0.058-0.074)              | (0.066-0.086)              | (0.073-0.096)              |  |  |  |
| 4-day    | <b>0.015</b>  | <b>0.019</b>               | <b>0.024</b>               | <b>0.029</b>               | <b>0.036</b>               | <b>0.041</b>               | <b>0.047</b>               | <b>0.054</b>               | <b>0.062</b>               | <b>0.069</b>               |  |  |  |
|          | (0.013-0.016)   | (0.017-0.021)              | (0.022-0.027)              | (0.026-0.033)              | (0.032-0.040)              | (0.037-0.046)              | (0.041-0.053)              | (0.046-0.060)              | (0.053-0.069)              | (0.059-0.078)              |  |  |  |
| 7-day    | <b>0.009</b>  | <b>0.012</b>               | <b>0.015</b>               | <b>0.018</b>               | <b>0.023</b>               | <b>0.026</b>               | <b>0.030</b>               | <b>0.034</b>               | <b>0.039</b>               | <b>0.044</b>               |  |  |  |
|          | (0.008-0.010)   | (0.011-0.013)              | (0.014-0.017)              | (0.016-0.021)              | (0.020-0.025)              | (0.023-0.029)              | (0.026-0.033)              | (0.029-0.038)              | (0.034-0.044)              | (0.037-0.049)              |  |  |  |
| 10-day   | <b>0.007</b>  | <b>0.009</b>               | <b>0.012</b>               | <b>0.014</b>               | <b>0.017</b>               | <b>0.020</b>               | <b>0.023</b>               | <b>0.025</b>               | <b>0.029</b>               | <b>0.033</b>               |  |  |  |
|          | (0.006-0.008)   | (0.008-0.010)              | (0.011-0.013)              | (0.013-0.016)              | (0.015-0.019)              | (0.018-0.022)              | (0.020-0.025)              | (0.022-0.028)              | (0.025-0.033)              | (0.028-0.036)              |  |  |  |
| 20-day   | <b>0.004</b>  | <b>0.006</b>               | <b>0.007</b>               | <b>0.009</b>               | <b>0.010</b>               | <b>0.012</b>               | <b>0.013</b>               | <b>0.015</b>               | <b>0.017</b>               | <b>0.018</b>               |  |  |  |
|          | (0.004-0.005)   | (0.005-0.006)              | (0.007-0.008)              | (0.008-0.010)              | (0.009-0.012)              | (0.010-0.013)              | (0.012-0.015)              | (0.013-0.016)              | (0.014-0.018)              | (0.016-0.020)              |  |  |  |
| 30-day   | <b>0.003</b>  | <b>0.004</b>               | <b>0.006</b>               | <b>0.007</b>               | <b>0.008</b>               | <b>0.009</b>               | <b>0.010</b>               | <b>0.011</b>               | <b>0.013</b>               | <b>0.014</b>               |  |  |  |
|          | (0.003-0.004)   | (0.004-0.005)              | (0.005-0.006)              | (0.006-0.007)              | (0.007-0.009)              | (0.008-0.010)              | (0.009-0.011)              | (0.010-0.013)              | (0.011-0.014)              | (0.012-0.016)              |  |  |  |
| 45-day   | <b>0.003</b>  | <b>0.003</b>               | <b>0.004</b>               | <b>0.005</b>               | <b>0.006</b>               | <b>0.007</b>               | <b>0.008</b>               | <b>0.009</b>               | <b>0.010</b>               | <b>0.010</b>               |  |  |  |
|          | (0.002-0.003)   | (0.003-0.004)              | (0.004-0.005)              | (0.005-0.006)              | (0.006-0.007)              | (0.006-0.008)              | (0.007-0.009)              | (0.008-0.009)              | (0.008-0.011)              | (0.009-0.012)              |  |  |  |
| 60-day   | <b>0.002</b>  | <b>0.003</b>               | <b>0.004</b>               | <b>0.004</b>               | <b>0.005</b>               | <b>0.006</b>               | <b>0.006</b>               | <b>0.007</b>               | <b>0.008</b>               | <b>0.008</b>               |  |  |  |
|          | (0.002-0.002)   | (0.002-0.003)              | (0.003-0.004)              | (0.004-0.005)              | (0.005-0.006)              | (0.005-0.006)              | (0.006-0.007)              | (0.006-0.008)              | (0.007-0.009)              | (0.007-0.009)              |  |  |  |

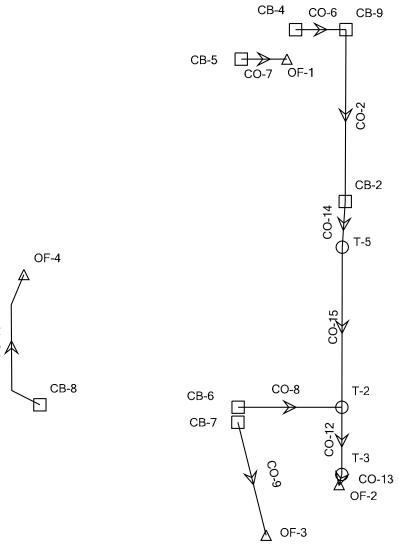
<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top

### Scenario: Base



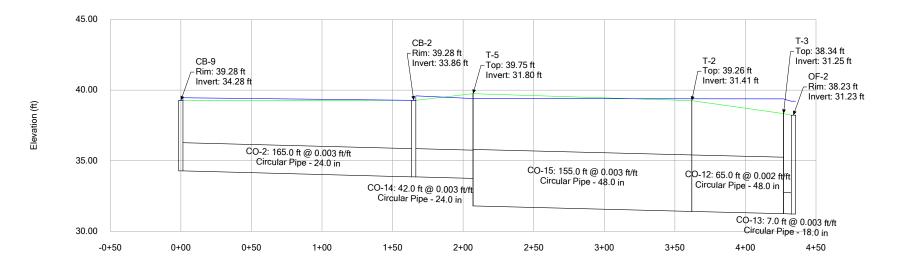
CO-11

1872.stc 6/29/2020

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1

Profile Report Engineering Profile - East Retention Pipe (1872.stc)

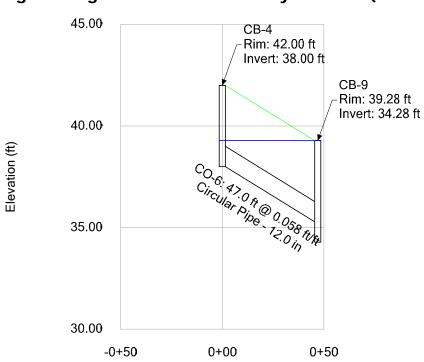


Station (ft)

Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1

> 5-ZN-2020 07/1/20

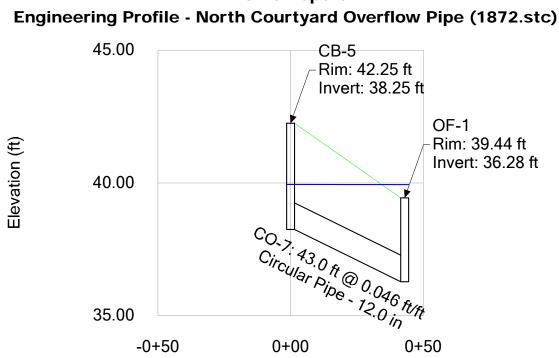
1872.stc 6/29/2020 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666



Profile Report Engineering Profile - North Courtyard Inlet (1872.stc)

Station (ft)

1872.stc 6/29/2020 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1

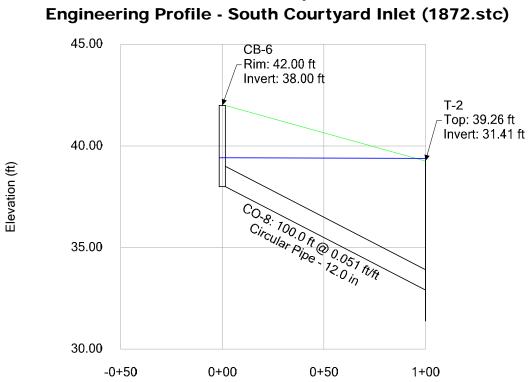


**Profile Report** 



1872.stc 6/29/2020 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1





Station (ft)

1872.stc 6/29/2020 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666

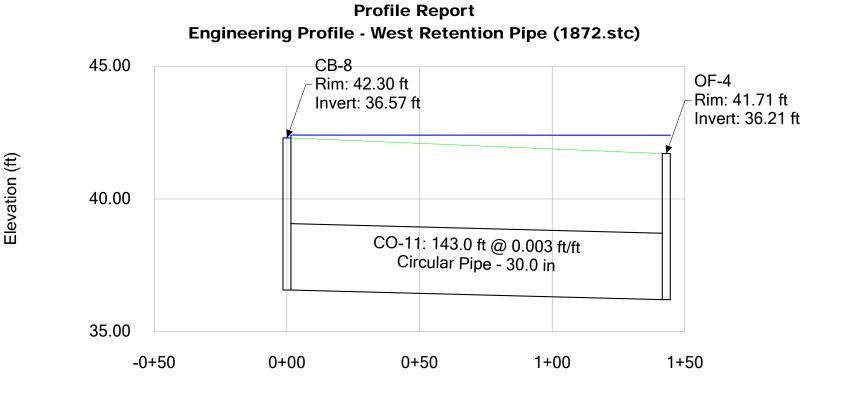
Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1

**Profile Report** Engineering Profile - South Courtyard Overflow Pipe (1872.stc) 45.00 CB-7 Rim: 42.25 ft Invert: 40.00 ft OF-3 Rim: 40.65 ft Invert: 38.90 ft 40.00 CO-9: 118.0 ft @ 0.009 ft/ft Circular Pipe - 12.0 in 35.00 0+50 1+00 1+50 -0+50 0+00

Station (ft)

1872.stc 6/29/2020 Elevation (ft)

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1



Station (ft)

1872.stc 6/29/2020 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1

| Label | Start<br>Node | Stop Node | Length<br>(Unified<br>)<br>(ft) | Total<br>Flow<br>(ft³/s) | Rise<br>(Unifie<br>d)<br>(in) | Capacity<br>(Full Flow)<br>(ft³/s) | Velocity<br>(Average)<br>(ft/s) | Invert<br>(Upstr<br>eam)<br>(ft) | Invert<br>(Downstr<br>eam)<br>(ft) | Slope<br>(ft/ft) | Mannin<br>g's n | Hydraulic Grade<br>Line (In)<br>(ft) | Hydraulic Grade<br>Line (Out)<br>(ft) |
|-------|---------------|-----------|---------------------------------|--------------------------|-------------------------------|------------------------------------|---------------------------------|----------------------------------|------------------------------------|------------------|-----------------|--------------------------------------|---------------------------------------|
| CO-9  | CB-7          | OF-3      | 118.0                           | 0.63                     | 12.0                          | 3.44                               | 3.33                            | 40.00                            | 38.90                              | 0.009            | 0.013           | 40.33                                | 39.19                                 |
| CO-7  | CB-5          | OF-1      | 43.0                            | 0.37                     | 12.0                          | 7.63                               | 0.47                            | 38.25                            | 36.28                              | 0.046            | 0.013           | 39.94                                | 39.94                                 |
| CO-11 | CB-8          | OF-4      | 143.0                           | 2.59                     | 30.0                          | 20.58                              | 0.53                            | 36.57                            | 36.21                              | 0.003            | 0.013           | 42.41                                | 42.40                                 |
| CO-8  | CB-6          | T-2       | 100.0                           | 0.63                     | 12.0                          | 8.04                               | 0.80                            | 38.00                            | 32.91                              | 0.051            | 0.013           | 39.42                                | 39.39                                 |
| CO-6  | CB-4          | CB-9      | 47.0                            | 0.37                     | 12.0                          | 8.57                               | 0.47                            | 38.00                            | 35.28                              | 0.058            | 0.013           | 39.29                                | 39.28                                 |
| CO-2  | CB-9          | CB-2      | 165.0                           | 7.57                     | 24.0                          | 11.41                              | 2.41                            | 34.28                            | 33.86                              | 0.003            | 0.013           | 39.46                                | 39.28                                 |
| CO-14 | CB-2          | T-5       | 42.0                            | 15.35                    | 24.0                          | 11.58                              | 4.89                            | 33.86                            | 33.75                              | 0.003            | 0.013           | 39.60                                | 39.41                                 |
| CO-15 | T-5           | T-2       | 155.0                           | 15.35                    | 48.0                          | 72.28                              | 1.22                            | 31.80                            | 31.41                              | 0.003            | 0.013           | 39.41                                | 39.39                                 |
| CO-12 | T-2           | T-3       | 65.0                            | 15.98                    | 48.0                          | 71.26                              | 1.27                            | 31.41                            | 31.25                              | 0.002            | 0.013           | 39.39                                | 39.38                                 |
| CO-13 | Т-3           | OF-2      | 7.0                             | 15.98                    | 18.0                          | 5.61                               | 9.04                            | 31.25                            | 31.23                              | 0.003            | 0.013           | 39.38                                | 39.22                                 |

### Conduit FlexTable: Combined Pipe/Node Report (1872.stc)

1872.stc 6/29/2020 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1

| Label                        | Station<br>(Calculated)<br>(ft) | Elevation<br>(Ground)<br>(ft) | Set Rim to<br>Ground<br>Elevation? | Elevation<br>(Rim)<br>(ft) | Elevation<br>(Invert)<br>(ft) | Flow<br>(Additional)<br>(ft³/s)    | Carryover<br>Additional<br>Flow<br>(ft³/s) | Flow<br>(Known)<br>(ft³/s) | Inlet Type      | Maximum Inflow<br>(ft³/s) |
|------------------------------|---------------------------------|-------------------------------|------------------------------------|----------------------------|-------------------------------|------------------------------------|--|----------------------------|-----------------|---------------------------|
| CB-2                         | 2+69                            | 39.28                         | True                               | 39.28                      | 33.86                         | 7.78                               | 0.00                                       | 0.00                       | Percent Capture | 0.00                      |
| CB-4                         | 4+81                            | 42.00                         | True                               | 42.00                      | 38.00                         | 0.37                               | 0.00                                       | 0.00                       | Percent Capture | 0.00                      |
| CB-5                         | 0+43                            | 42.25                         | True                               | 42.25                      | 38.25                         | 0.37                               | 0.00                                       | 0.00                       | Percent Capture | 0.00                      |
| CB-6                         | 1+72                            | 42.00                         | True                               | 42.00                      | 38.00                         | 0.63                               | 0.00                                       | 0.00                       | Percent Capture | 0.00                      |
| CB-7                         | 1+18                            | 42.25                         | True                               | 42.25                      | 40.00                         | 0.63                               | 0.00                                       | 0.00                       | Percent Capture | 0.00                      |
| CB-8                         | 1+43                            | 42.30                         | True                               | 42.30                      | 36.57                         | 2.59                               | 0.00                                       | 0.00                       | Percent Capture | 0.00                      |
| CB-9                         | 4+34                            | 39.28                         | True                               | 39.28                      | 34.28                         | 7.20                               | 0.00                                       | 0.00                       | Percent Capture | 0.00                      |
| Capture<br>Efficiency<br>(%) | Inlet Location                  | Desired Sump<br>Depth<br>(ft) | Depth (ft                          | • •                        | epth (Out)<br>(ft)            | Hydraulic Gra<br>Line (In)<br>(ft) | Line                                       | ic Grade<br>(Out)<br>ft)   |                 |                           |
| 10                           | 0.0 On Grade                    | 0.0                           | 00                                 | 5.42                       | 5.42                          | 39                                 | .28  | 39.28                      |                 |                           |
| 10                           | 0.0 On Grade                    | 0.0                           | 00                                 | 1.29                       | 1.29                          | 39                                 | .29  | 39.29                      |                 |                           |
| 10                           | 0.0 On Grade                    | 0.0                           | 00                                 | 1.69                       | 1.69                          | 39                                 | .94  | 39.94                      |                 |                           |
| 10                           | 0.0 On Grade                    | 0.0                           | 00                                 | 1.42                       | 1.42                          | 39                                 | .42  | 39.42                      |                 |                           |
| 10                           | 0.0 On Grade                    | 0.0                           | 00                                 | 0.33                       | 0.33                          | 40                                 | .33  | 40.33                      |                 |                           |
| 10                           | 0.0 On Grade                    | 0.0                           | 00                                 | 5.73                       | 5.73                          | 42                                 | .30  | 42.30                      |                 |                           |
| 10                           | 0.0 On Grade                    | 0.0                           | 00                                 | 5.00                       | 5.00                          | 39                                 | .28  | 39.28                      |                 |                           |

### FlexTable: Catch Basin Table (1872.stc)

1872.stc 6/29/2020 Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1

| Label | Station<br>(ft) | Elevation<br>(Ground)<br>(ft) | Set Rim to<br>Ground<br>Elevation | Elevation<br>(Invert)<br>(ft) | Boundary<br>Condition Type | Elevation<br>(Tailwater)<br>(ft) | Flow (Outfall)<br>(ft³/s) |
|-------|-----------------|-------------------------------|-----------------------------------|-------------------------------|----------------------------|----------------------------------|---------------------------|
| OF-1  | 0+00            | 39.44                         | True                              | 36.28                         | User Defined<br>Tailwater  | 39.94                            | 0.37                      |
| OF-2  | 0+00            | 38.23                         | True                              | 31.23                         | User Defined<br>Tailwater  | 39.22                            | 15.98                     |
| OF-3  | 0+00            | 40.65                         | True                              | 38.90                         | Free Outfall               | 0.00                             | 0.63                      |
| OF-4  | 0+00            | 41.71                         | True                              | 36.21                         | User Defined<br>Tailwater  | 42.40                            | 2.59                      |

### FlexTable: Outfall Table (1872.stc)

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1



| Label | Elevation<br>(Ground)<br>(ft) | Elevation<br>(Top)<br>(ft) | Elevation<br>(Invert)<br>(ft) | Transition<br>Length<br>(ft) | Headloss<br>Method | Hydraulic Grade<br>Line (Out)<br>(ft) |
|-------|-------------------------------|----------------------------|-------------------------------|------------------------------|--------------------|---------------------------------------|
| T-2   | 39.26                         | 39.26                      | 31.41                         | 0.0                          | Absolute           | 39.39                                 |
| T-3   | 38.34                         | 38.34                      | 31.25                         | 0.0                          | Absolute           | 39.38                                 |
| T-5   | 39.75                         | 39.75                      | 31.80                         | 0.0                          | Absolute           | 39.41                                 |

### FlexTable: Transition Table (1872.stc)

Bentley Systems, Inc. Haestad Methods Solution Center 27 Siemon Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Bentley StormCAD V8i (SELECTseries 2) [08.11.02.38] Page 1 of 1

5-ZN-2020 07/1/20

3<br/>
<br/>
<br/>
engineering civil engineering planning surveying

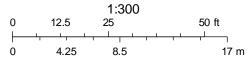
## APPENDIX K

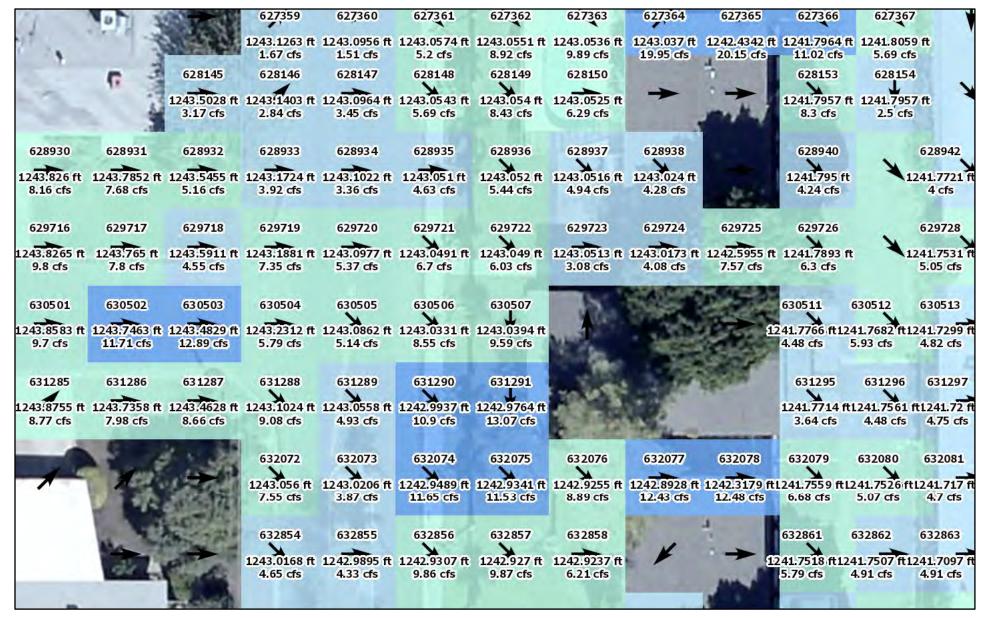
## Flo-2d Maps

Page | A11





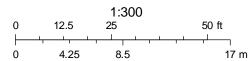




March 24, 2020

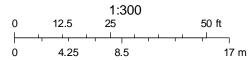


March 24, 2020

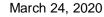


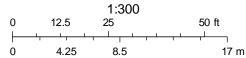










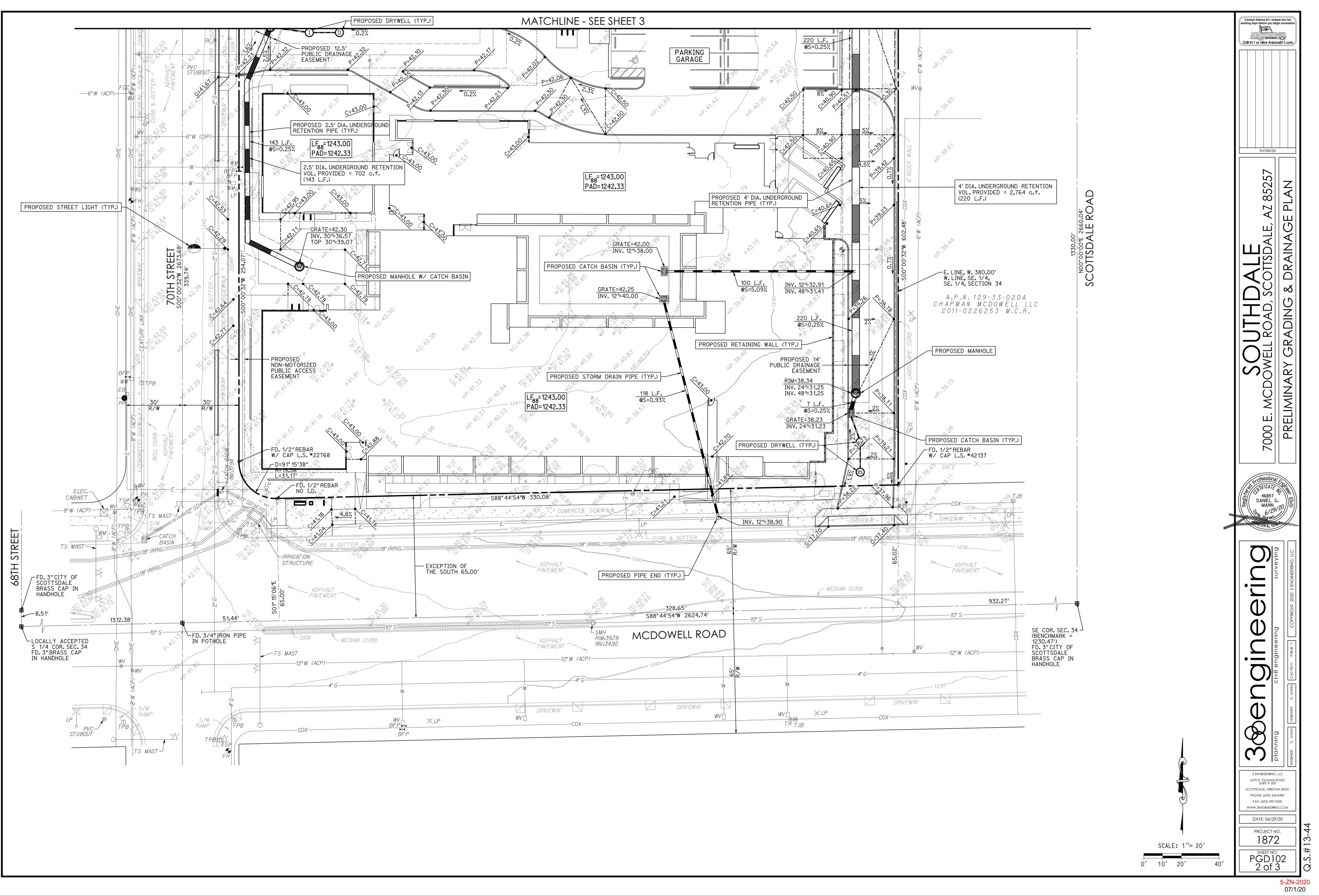


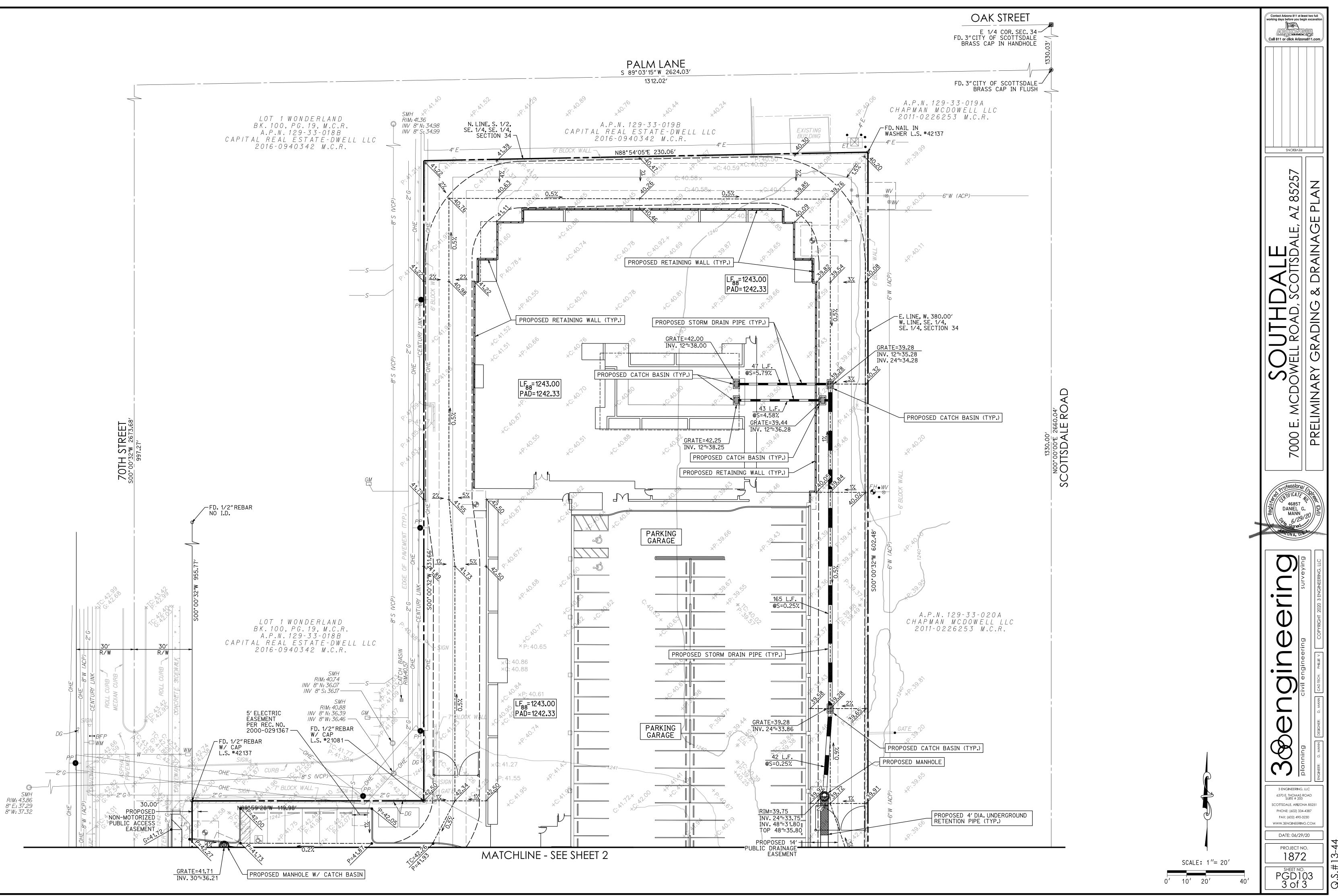
3<br/>
<br/>
planning civil engineering surveying

# APPENDIX L

## Preliminary Grading and Drainage Plans

Page | A12





y SecuriSync/Projects/1872\_70th\_St\_McDowell\_Apartments/1872pgrd03.dgn