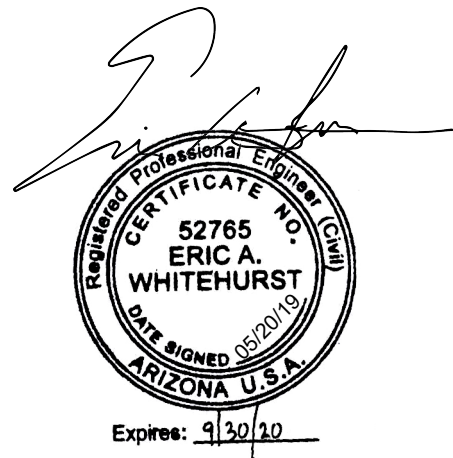


WATER AND WASTEWATER
BASIS OF DESIGN REPORT

2nd Street & Bishop Lane
Scottsdale, Arizona

Prepared for:

The Morgan Group, Inc.
3001 Brighton Blvd., Suite 445
Denver, CO 80216



Prepared by:



2ND STREET & BISHOP LANE

WATER AND WASTEWATER BASIS OF DESIGN REPORT

MAY 2019

Prepared By:

Kimley»»Horn

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Appendix C – Fire Flow Requirements from 2015 IFC

Appendix D – Fire Flow Test and Water CAD Results and Layout

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1.0 INTRODUCTION

Kimley-Horn and Associates, Inc. has prepared this Water and Wastewater Basis of Design Report for the proposed luxury apartment development at the southwest corner of 2nd Street and Bishop Lane in Scottsdale, Arizona. This report will demonstrate that the proposed project conforms to the City of Scottsdale design requirements.

2nd Street & Bishop Lane, the “project”, encompasses approximately 1.13 ± net acres and contains a 210,857 square foot, eight-story apartment with a 93,372 square foot two-level underground parking garage. The project lies within a portion of the Northeast Quarter of Section 27, Township 2 North, Range 4 East of the Gila and Salt River Baseline and Meridian in Maricopa County, Arizona. More specifically, the project is bounded by East 2nd Street to the north followed by North Bishop Lane to the east followed by Moe Tavassoli Oriental Rugs to the south, and a public alley followed by existing commercial buildings to the west. The site slopes from the northwest to the southeast at approximately 1.0%. See **Appendix A** for the Vicinity Map.

2.0 DOMESTIC WATER ANALYSIS

2.1 INTENT AND SCOPE

The intent of this section is to evaluate the potable water infrastructure for the proposed development. As a result of this analysis, it will be determined if the potable water infrastructure is capable of satisfying the projected water demands for the proposed development in accordance with the City of Scottsdale Design Standards & Policies Manual (**Reference 1**) and the 2015 International Fire Code (**Reference 2**) for fire prevention.

2.2 GENERAL THEORY

The water system modeling program Water CAD, developed by Haestad Methods, is used to model the water system servicing the proposed development. The program uses the fluid mechanic head loss theory known as the Hazen-Williams method. This is the typical method used to evaluate water distribution systems.

2.3 DOMESTIC WATER SUPPLY

There is an existing 8-inch ACP and 16-inch DIP water main located in East 2nd Street north of the site. The existing 8-inch ACP water main connects to an existing 6-inch ACP water main in North Bishop Lane east of the site and to an existing 4-inch DIP water main in the ally west of the site. There is an existing 8-inch ACP water main located in North Goldwater Boulevard approximately 310 feet south of the site.

A proposed 8-inch DIP private fire line will connect to the existing 8-inch ACP water main north of the site via an 8-inch by 8-inch tapping sleeve and valve. Two 2-inch domestic services that combine into a 3-inch onsite line will also connect to the existing 8-inch ACP water main north of the site. Refer to **Appendix B** for the Preliminary Utility Plan.

Residual and static pressures were obtained from a flow test performed on two fire hydrants (one flow and one pressure) in East 2nd Street, by EJ Flow Tests on May 5th, 2019. The tested fire hydrants were selected due to the proximity to the proposed building. See **Appendix D** for the Fire Flow Test results.

2.4 INTERNATIONAL FIRE CODE, 2015

According to the City of Scottsdale Fire Department, the 2015 International Fire Code (IFC) with City of Scottsdale Amendments is currently the governing code with respect to fire protection requirements. The IFC evaluates the building construction type, occupancy descriptions, and square footage to set minimum fire flow requirements with regards to a particular development.

The proposed building and garage are Construction Type I-B. Per Table B105.1(2) of **Reference 2**, the required fire flow is 6,000 gallons per minute. A reduction in fire-flow of 75% percent is allowed when the building is equipped with an approved fire sprinkler system. The apartment building and parking garage will be equipped with an approved fire sprinkler system. The minimum fire flow requirements per the IFC 2015 for the proposed building are shown in Table 1. Table 1 also shows the required building fire flow based upon a maximum fire flow reduction of 75% allowed by the IFC 2015. See **Appendix C** for IFC 2015 Appendix B.

Table 1 Required Building Fire Flows

Building	Building Construction Type	Building Area (sf)	Required Fire Flow per IFC 2015 (gpm)	Reduction	Actual Required Fire Flow with Reduction (gpm)
Apartment & Garage	I-B	304,229	6,000	75%	1,500

2.5 WATER DEMANDS

According to the guidelines provided in Figure 6-1.2 of **Reference 1**, the proposed development will add the following demands to the existing water system for Average Day Demand (ADD), Maximum Day Demand (MDD), and Peak Hour Demand (PHD):

Table 2: Domestic Water Demands

Building	Building Area (SF)	# DUs	Total Demand ¹ (GPM/DU)	ADD (GPM)	MDD ² (GPM)	PHD ³ (GPM)
Building 1 + Garage	304,229	199	0.27	53.73	107.46	188.06

Notes:

1. For high density condominium land use, average day demand is 185.3 gpd/du or 0.27 gpm/du.
2. Maximum day demand defined as 2 times the average day demand.
3. Peak hour demand defined as 3.5 times the average day demand.

Two water analyses were performed to evaluate the existing adjacent off-site water infrastructure and the proposed on-site water system:

1. Peak Hour
2. Maximum Day Demand + Fire Flow

The system was analyzed for the worst-case scenario to ensure that the existing and proposed public water infrastructure can maintain a minimum pressure of 50 psi for the Peak Hour demand, and 30 psi for the Maximum Day plus Fire Flow demand. See Appendix D for water model layout to identify nodes and pipes.

See **Appendix D** for the Fire Flow Test and Water CAD Analysis and Layout. A summary of the water analysis results for the project is tabulated below:

Table 3 Domestic Water Model Result Summary

Criteria	Peak Hour Demand	Constraint	Peak Hour Pressure at Demand	Node with Minimum Pressure
Minimum Pressure	188 gpm	50 psi	64.0 psi	BLDG DW
Meets Criteria?	-	-	Yes	

Table 4 Fire Flow Water Model Result Summary

Criteria	Max Day + Fire Flow Demand	Constraint	Max Day + Fire Flow Pressure at Demand	Node with Minimum Pressure
Minimum System Pressure	1,607 gpm	30 psi	58.0 psi	BLDG DW
Meets Criteria?	-	-	Yes	

Table 5 Fire Hydrant Flow Water Model Result Summary

Criteria	Fire Flow Demand	Constraint	Fire Flow Pressure at Demand	Meets Criteria?
Hydrant 1	1,500 gpm	20 psi	62.0 psi	YES
Hydrant 2	1,500 gpm	20 psi	66.0 psi	YES

3.0 WASTEWATER COLLECTION SYSTEM

3.1 INTENT AND SCOPE

The intent of this section is to evaluate the proposed sewer infrastructure and wastewater design flows for the development. As a result of this analysis, it will be determined if the sewer infrastructure is capable supporting the proposed development in accordance with the City of Scottsdale Design Standards & Policies Manual (**Reference 1**).

3.2 SEWER INFRASTRUCTURE

There is an existing 8-inch sewer main in the alley west of the site. An 8-inch VCP sewer main also exists in North Bishop Lane to the east of the site.

A proposed 6-inch PVC sewer service with a slope of 8.00% will connect to the existing 8-inch sewer main in the alley west of the site. Refer to **Appendix B** for the Preliminary Utility Plan.

3.3 WASTEWATER DESIGN FLOWS

The following calculations are based on information provided in Section 7-1.403 of **Reference 1**:

Table 3: Wastewater Design Flow

Building	Building Area (SF)	# Units	Average Daily Flow ¹ (GPD)	Peak Flow ² (GPD)	Peak Flow (GPM)	Peak Flow ³ w/ Pool Backwash (GPM)
Apartment and Garage	304,229	199	27,860	125,370	87	187

Notes:

1. Wastewater flows are based on 140 gallons per unit per day for high density condominium land use.
2. Design peaking factor for high density condominium is 4.5.
3. 100 GPM maximum design assumption. Backwash pump and pipe sizing will be done by the pool designer under separate permit.

3.4 ANALYSIS

Sanitary sewer lines will be designed to maintain a maximum depth to diameter ratio (d/D) of 0.65 and minimum full flow velocity of 2.5 ft/sec and a maximum full flow velocity of 10.0 ft/sec in the ultimate peak flow condition. To verify the proposed 6-inch sewer on-site has adequate capacity to serve the project, design flows were analyzed with Flow Master using minimum and maximum pipe design slopes. The sewer capacity for a six-inch pipe at the minimum design slope of 1.10% is 264 gpm. Pool backwash shall be connected to the sanitary sewer system and not discharge to the storm drain system. For the purpose of the design we have assumed a pool backwash flow rate of 100 gpm. Actual backwash discharge rate shall not exceed 100 gpm. Backwash pump and pipe sizing will be done by the pool designer under separate permit. Refer to **Appendix E** for the Sewer Capacity Calculations.

4.0 CONCLUSION

Water

The proposed and existing on-site water system as outlined by this analysis appears adequate and sufficient to meet the required fire flow demand for the proposed 2nd Street and Bishop Lane development near the southwest corner of 2nd Street and Bishop Lane in Scottsdale, Arizona.

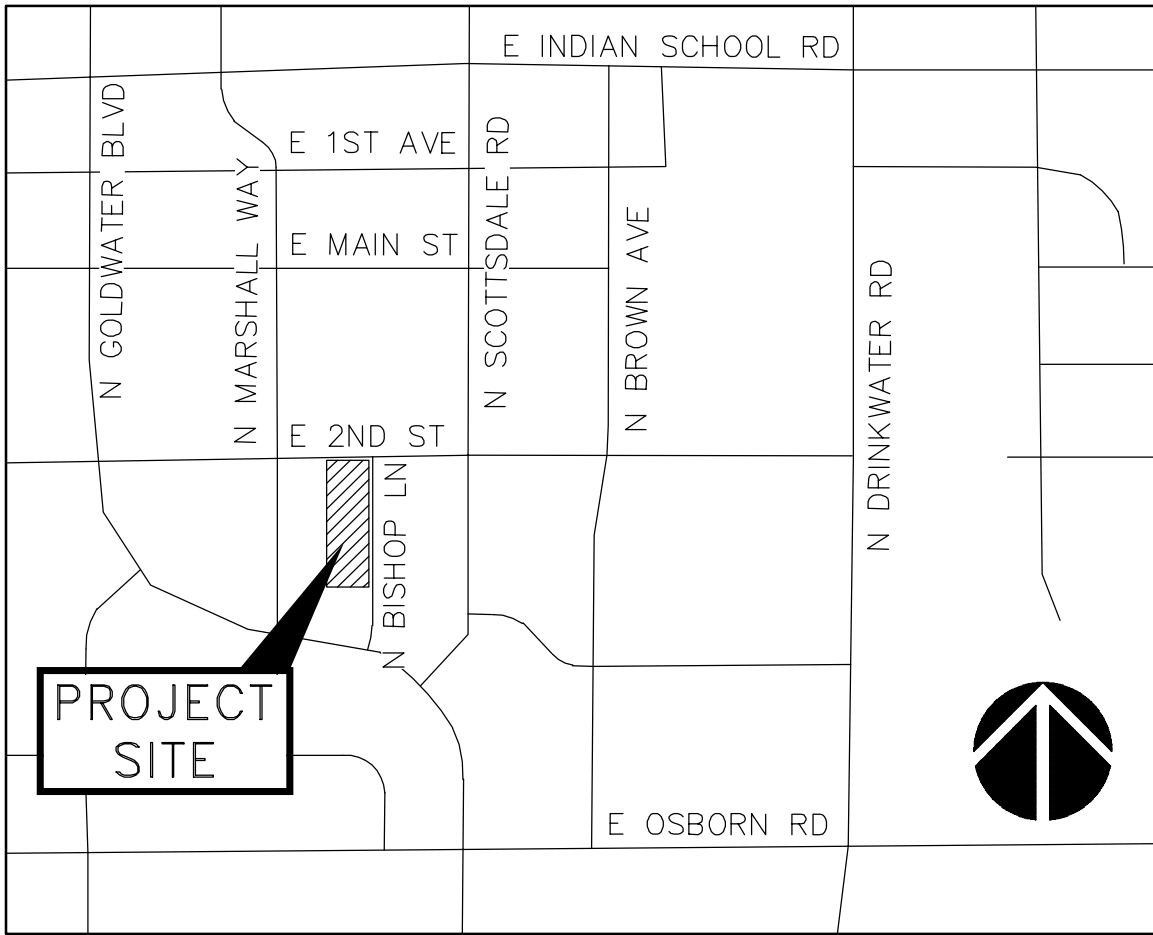
Wastewater

This development proposes to connect the building sewer services to the existing 8-inch sewer main in the alley west of the site. The proposed 6-inch PVC private sanitary sewer service has adequate capacity for the flows generated by the proposed building and its associated uses. Refer to Appendix B for the Sewer Capacity Calculations.

5.0 REFERENCES

1. City of Scottsdale, *Design Standards and Policies Manual*. 2018.
2. International Code Council, *2015 International Fire Code*. May 2014.

Appendix A – Vicinity Map



VICINITY MAP

SCOTTSDALE, AZ
N.T.S.

Appendix B –Utility Plan

Appendix C – Fire Flow Requirements from 2015 IFC

SECTION B105 FIRE-FLOW REQUIREMENTS FOR BUILDINGS

B105.1 One- and two-family dwellings.

The minimum fire-flow and flow duration requirements for one- and two-family *dwellings* having a fire-flow calculation area that does not exceed 3,600 square feet (344.5 m²) shall be 1,000 gallons per minute (3785.4 L/min) for 1 hour. Fire-flow and flow duration for *dwellings* having a fire-flow calculation area in excess of 3,600 square feet (344.5m²) shall not be less than that specified in Table B105.1.

Exception: A reduction in required fire-flow of 50 percent, as *approved*, is allowed when the building is equipped with an *approved automatic sprinkler system*.

TABLE B105.1 MINIMUM REQUIRED FIRE-FLOW AND FLOW DURATION FOR BUILDINGS

FIRE-FLOW CALCULATION AREA (square feet)					FIRE-FLOW (gallons per minute) ^b	FLOW DURATION (hours)
Type IA and IB ^a	Type IIA and IIIA ^a	Type IV and V-A ^a	Type IIB and IIIB ^a	Type V- B ^a		
0-22,700	0-12,700	0-8,200	0-5,900	0-3,600	1,500	2
22,701- 30,200	12,701- 17,000	8,201- 10,900	5,901-7,900	3,601- 4,800	1,750	
30,201- 38,700	17,001- 21,800	10,901- 12,900	7,901-9,800	4,801- 6,200	2,000	
38,701- 48,300	21,801- 24,200	12,901- 17,400	9,801-12,600	6,201- 7,700	2,250	
48,301- 59,000	24,201- 33,200	17,401- 21,300	12,601- 15,400	7,701- 9,400	2,500	
59,001- 70,900	33,201- 39,700	21,301- 25,500	15,401- 18,400	9,401- 11,300	2,750	
70,901- 83,700	39,701- 47,100	25,501- 30,100	18,401- 21,800	11,301- 13,400	3,000	3
83,701- 97,700	47,101- 54,900	30,101- 35,200	21,801- 25,900	13,401- 15,600	3,250	
97,701- 112,700	54,901- 63,400	35,201- 40,600	25,901- 29,300	15,601- 18,000	3,500	
112,701- 128,700	63,401- 72,400	40,601- 46,400	29,301- 33,500	18,001- 20,600	3,750	
128,701- 145,900	72,401- 82,100	46,401- 52,500	33,501- 37,900	20,601- 23,300	4,000	4
145,901- 164,200	82,101- 92,400	52,501- 59,100	37,901- 42,700	23,301- 26,300	4,250	
164,201-	92,401-	59,101-	42,701-	26,301-	4,500	

183,400	103,100	66,000	47,700	29,300	
183,401- 203,700	103,101- 114,600	66,001- 73,300	47,701- 53,000	29,301- 32,600	4,750
203,701- 225,200	114,601- 126,700	73,301- 81,100	53,001- 58,600	32,601- 36,000	5,000
225,201- 247,700	126,701- 139,400	81,101- 89,200	58,601- 65,400	36,001- 39,600	5,250
247,701- 271,200	139,401- 152,600	89,201- 97,700	65,401- 70,600	39,601- 43,400	5,500
271,201- 295,900	152,601- 166,500	97,701- 106,500	70,601- 77,000	43,401- 47,400	5,750
295,901- Greater	166,501- Greater	106,501- 115,800	77,001- 83,700	47,401- 51,500	6,000
—	—	115,801- 125,500	83,701- 90,600	51,501- 55,700	6,250
—	—	125,501- 135,500	90,601- 97,900	55,701- 60,200	6,500
—	—	135,501- 145,800	97,901- 106,800	60,201- 64,800	6,750
—	—	145,801- 156,700	106,801- 113,200	64,801- 69,600	7,000
—	—	156,701- 167,900	113,201- 121,300	69,601- 74,600	7,250
—	—	167,901- 179,400	121,301- 129,600	74,601- 79,800	7,500
—	—	179,401- 191,400	129,601- 138,300	79,801- 85,100	7,750
—	—	191,401- Greater	138,301- Greater	85,101- Greater	8,000

For SI: 1 square foot = 0.0929 m², 1 gallon per minute = 3.785 L/m, 1 pound per square inch = 6.895 kPa.

- a. Types of construction are based on the *International Building Code*.
- b. Measured at 20 psi residual pressure.

B105.2 Buildings other than one- and two-family dwellings.

The minimum fire-flow and flow duration for buildings other than one- and two-family dwellings shall be as specified in Table B105.1.

Exception: A reduction in required fire-flow of up to 75 percent, as *approved*, is allowed when the building is provided with an *approved automatic sprinkler system* installed in accordance with Section 903.3.1.1 or 903.3.1.2. The resulting fire-flow shall not be less than 1,500 gallons per minute (5678 L/min) for the prescribed duration as specified in Table B105.1.

Appendix D – Fire Flow Test and Water CAD Results and Layout



Flow Test Summary

Project Name: EJFT 19096
Project Address: 7125 E 2nd St, Scottsdale, AZ 85251
Date of Flow Test: 2019-05-03
Time of Flow Test: 7:34 AM
Data Reliable Until: 2019-11-03
Conducted By: Eder Cueva & Tayler Lynch (EJ Flow Tests) 602.999.7637
Witnessed By: Ray Padilla (City of Scottsdale) 602.541.0586
City Forces Contacted: City of Scottsdale (602.541.0586)
Permit Number: C58183

Note Scottsdale requires a max static pressure of 72 psi for safety factor

Raw Flow Test Data

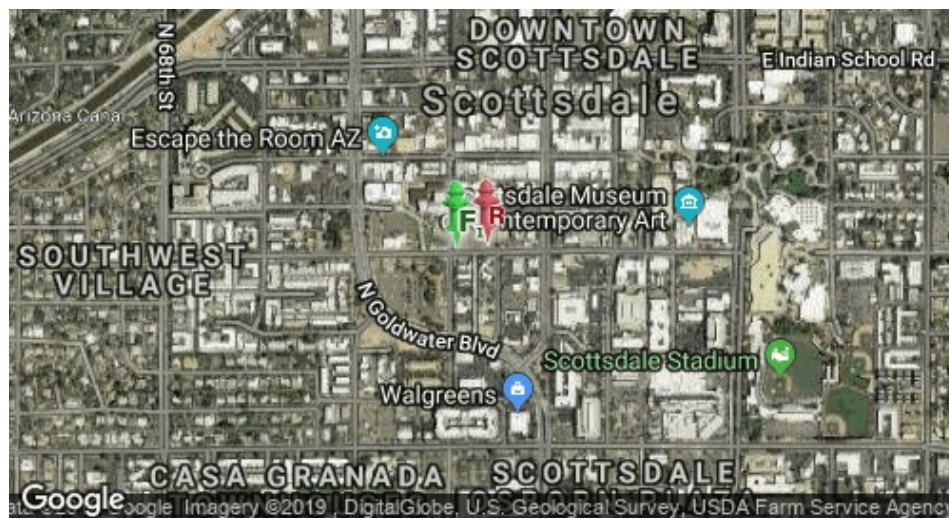
Static Pressure: 88.0 PSI
Residual Pressure: 82.0 PSI
Flowing GPM: 1,575
GPM @ 20 PSI: 5,841



Data with a 16 PSI Safety Factor

Static Pressure: 72.0 PSI
Residual Pressure: 66.0 PSI
Flowing GPM: 1,575
GPM @ 20 PSI: 5,054

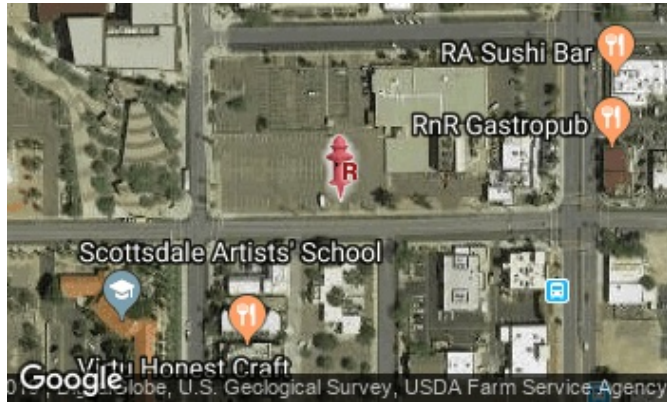
Hydrant F₁

Pitot Pressure (1): 22 PSI
Coefficient of Discharge (1): 0.9
Hydrant Orifice Diameter (1): 2.5 inches
Pitot Pressure (2): 22 PSI
Coefficient of Discharge (2): 0.9
Hydrant Orifice Diameter (2): 2.5 inches



 Static-Residual Hydrant
 Flow Hydrant
Distance Between F₁ and R
204 ft (measured linearly)
Static-Residual Elevation
1257 ft (above sea level)
Flow Hydrant (F₁) Elevation
1257 ft (above sea level)
Elevation & distance values are approximate

Static-Residual Hydrant



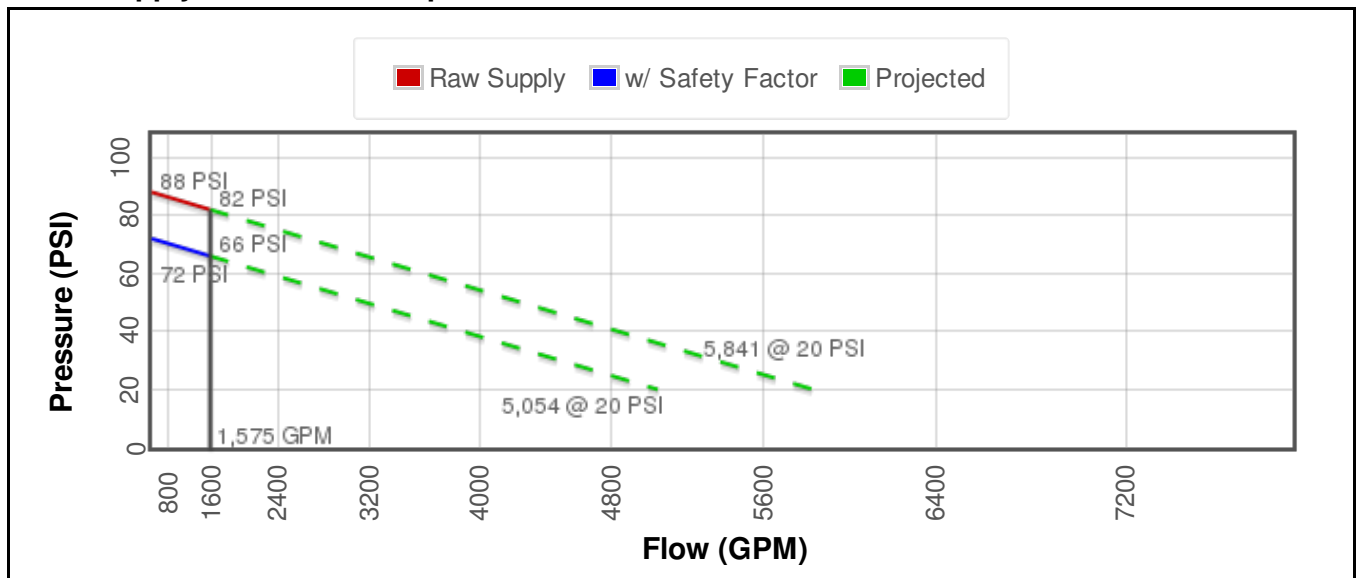
Flow Hydrant (only hydrant F1 shown for clarity)



Approximate Project Site



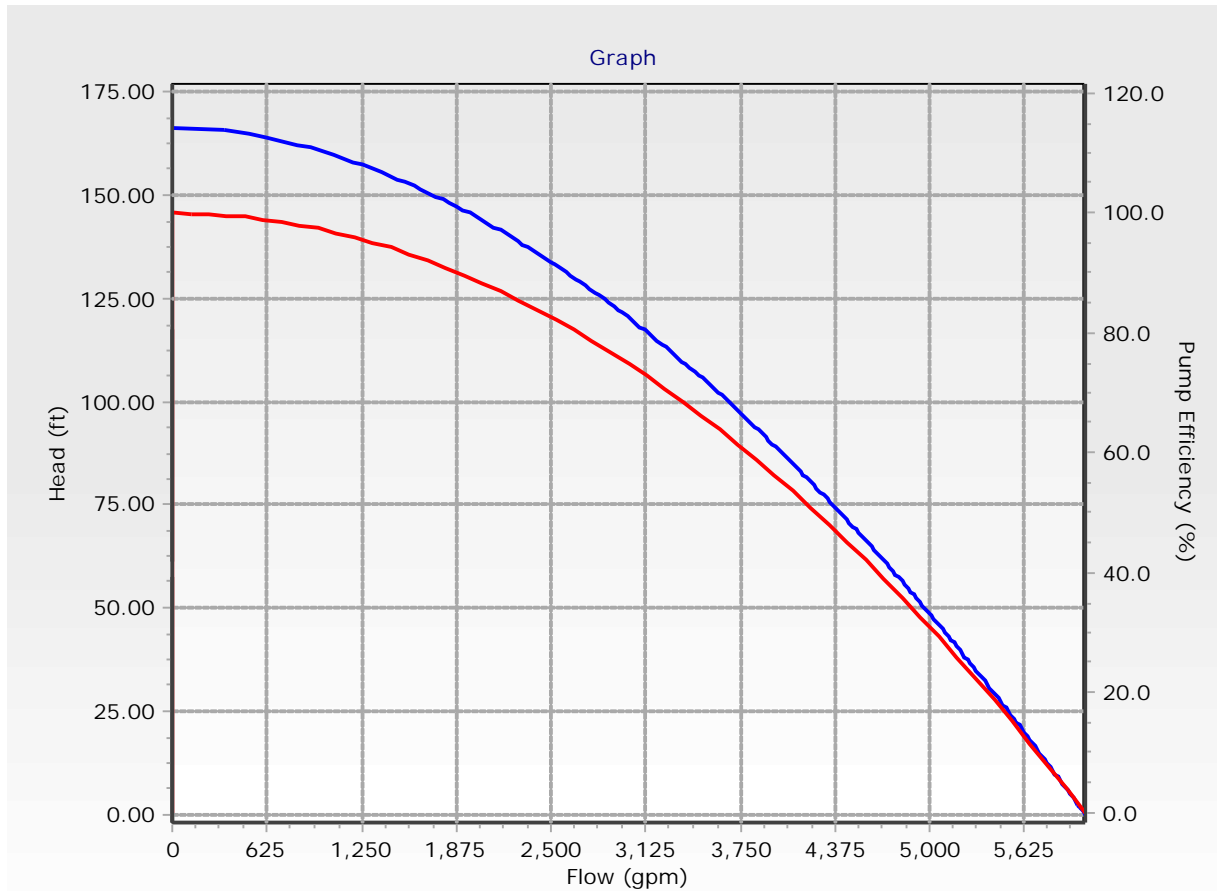
Water Supply Curve N^{1.85} Graph



Pump Definition Detailed Report: 2nd & Bishop

Element Details			
ID	64	Notes	
Label	2nd & Bishop		
Pump Definition Type			
Pump Definition Type	Standard (3 Point)	Design Head	152.46 ft
Shutoff Flow	0 gpm	Maximum Operating Flow	5,054 gpm
Shutoff Head	166.32 ft	Maximum Operating Head	46.20 ft
Design Flow	1,575 gpm		
Pump Efficiency Type			
Pump Efficiency Type	Best Efficiency Point	Motor Efficiency	100.0 %
BEP Efficiency	100.0 %	Is Variable Speed Drive?	False
BEP Flow	0 gpm		
Transient (Physical)			
Inertia (Pump and Motor)	0.000 lb·ft ²	Specific Speed	SI=25, US=1280
Speed (Full)	0 rpm	Reverse Spin Allowed?	True

Pump Definition Detailed Report: 2nd & Bishop



FlexTable: Junction Table

Active Scenario: Maximum Day Demand + Fire Flow

Label	Elevation (ft)	Demand (gpm)	Hydraulic Grade (ft)	Pressure (psi)	Pressure (Minimum) (psi)	Flow (Total Available) (gpm)	Flow (Total Needed) (gpm)	Fire Flow (Available) (gpm)
J-1	54.75	0	203.31	64	64	(N/A)	(N/A)	(N/A)
J-2	54.72	0	203.44	64	64	(N/A)	(N/A)	(N/A)
J-3	54.54	0	206.76	66	66	(N/A)	(N/A)	(N/A)
BLDG DW	55.37	107	189.71	58	58	(N/A)	(N/A)	(N/A)
FIRE	55.35	1,500	200.89	63	63	(N/A)	(N/A)	(N/A)
J-12	56.50	0	203.31	64	64	(N/A)	(N/A)	(N/A)

FlexTable: Pipe Table

Active Scenario: Maximum Day Demand + Fire Flow

Label	Start Node	Stop Node	Diameter (in)	Length (Scaled) (ft)	Material	Hazen-Williams C	Flow (gpm)	Velocity (ft/s)	Headloss (ft)
P-3	J-2	J-1	8.0	4	Asbestos Cement	140.0	1,500	9.57	0.14
P-4	J-3	J-2	8.0	86	Asbestos Cement	140.0	1,607	10.26	3.32
P-5	H-2	J-3	8.0	16	Ductile Iron	130.0	0	0.00	0.00
P-8	J-1	FIRE	8.0	62	Ductile Iron	130.0	1,500	9.57	2.42
P-9	PMP-1	J-3	100.0	15	Ductile Iron	130.0	1,607	0.07	0.00
P-10	R-1	PMP-1	100.0	18	Ductile Iron	130.0	1,607	0.07	0.00
P-6	J-2	GPV-1	3.0	52	Ductile Iron	130.0	107	4.88	1.81
P-7	GPV-1	BLDG DW	3.0	10	Ductile Iron	130.0	107	4.88	0.37
P-1	H-1	J-12	8.0	18	Ductile Iron	130.0	0	0.00	0.00
P-2	J-12	J-1	8.0	150	Asbestos Cement	140.0	0	0.00	0.00

FlexTable: Junction Table
Active Scenario: Peak Hour Demand

Label	Elevation (ft)	Demand (gpm)	Hydraulic Grade (ft)	Pressure (psi)	Pressure (Minimum) (psi)	Flow (Total Available) (gpm)	Flow (Total Needed) (gpm)	Fire Flow (Available) (gpm)
J-1	54.75	0	220.82	72	72	(N/A)	(N/A)	(N/A)
J-2	54.72	0	220.82	72	72	(N/A)	(N/A)	(N/A)
J-3	54.54	0	220.88	72	72	(N/A)	(N/A)	(N/A)
BLDG DW	55.37	188	203.13	64	64	(N/A)	(N/A)	(N/A)
FIRE	55.35	0	220.82	72	72	(N/A)	(N/A)	(N/A)
J-12	56.50	0	220.82	71	71	(N/A)	(N/A)	(N/A)

FlexTable: Pipe Table
Active Scenario: Peak Hour Demand

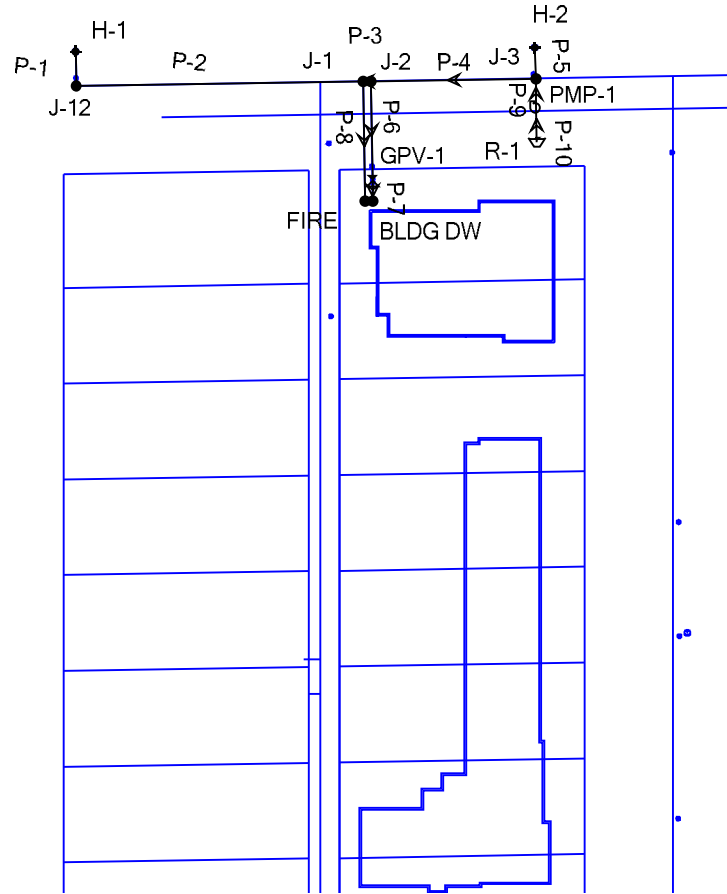
Label	Start Node	Stop Node	Diameter (in)	Length (Scaled) (ft)	Material	Hazen-Williams C	Flow (gpm)	Velocity (ft/s)	Headloss (ft)
P-3	J-2	J-1	8.0	4	Asbestos Cement	140.0	0	0.00	0.00
P-4	J-3	J-2	8.0	86	Asbestos Cement	140.0	188	1.20	0.06
P-5	H-2	J-3	8.0	16	Ductile Iron	130.0	0	0.00	0.00
P-8	J-1	FIRE	8.0	62	Ductile Iron	130.0	0	0.00	0.00
P-9	PMP-1	J-3	100.0	15	Ductile Iron	130.0	188	0.01	0.00
P-10	R-1	PMP-1	100.0	18	Ductile Iron	130.0	188	0.01	0.00
P-6	J-2	GPV-1	3.0	52	Ductile Iron	130.0	188	8.54	5.11
P-7	GPV-1	BLDG DW	3.0	10	Ductile Iron	130.0	188	8.54	1.03
P-1	H-1	J-12	8.0	18	Ductile Iron	130.0	0	0.00	0.00
P-2	J-12	J-1	8.0	150	Asbestos Cement	140.0	0	0.00	0.00

Fire Flow Node FlexTable: Fire Flow Report

Active Scenario: Fire Flow

Label	Elevation (ft)	Fire Flow (Needed) (gpm)	Fire Flow (Available) (gpm)	Pressure (Calculated Residual @ Total Flow Needed) (psi)	Pressure (Residual Lower Limit) (psi)	Junction w/ Minimum Pressure (System)	Satisfies Fire Flow Constraints?
H-1	57.00	1,500	1,567	62	20	BLDG DW	True
H-2	54.83	1,500	1,567	66	20	BLDG DW	True
J-1	54.75	1,500	(N/A)	(N/A)	20	(N/A)	False
J-2	54.72	1,500	(N/A)	(N/A)	20	(N/A)	False
J-3	54.54	1,500	(N/A)	(N/A)	20	(N/A)	False
BLDG DW	55.37	1,500	(N/A)	(N/A)	20	(N/A)	False
FIRE	55.35	1,500	1,567	64	20	BLDG DW	True
J-12	56.50	1,500	(N/A)	(N/A)	20	(N/A)	False

WaterCAD Layout



Appendix E – Sewer Capacity Calculations

Worksheet for 6" Service (min design slope)

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.01100	ft/ft
Normal Depth	6.00	in
Diameter	6.00	in

Results

Discharge	264.12	gal/min
Flow Area	0.20	ft ²
Wetted Perimeter	1.57	ft
Hydraulic Radius	1.50	in
Top Width	0.00	ft
Critical Depth	0.39	ft
Percent Full	100.0	%
Critical Slope	0.01209	ft/ft
Velocity	3.00	ft/s
Velocity Head	0.14	ft
Specific Energy	0.64	ft
Froude Number	0.00	
Maximum Discharge	0.63	ft ³ /s
Discharge Full	0.59	ft ³ /s
Slope Full	0.01100	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.00	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s

Worksheet for 6" Service (min design slope)

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	6.00	in
Critical Depth	0.39	ft
Channel Slope	0.01100	ft/ft
Critical Slope	0.01209	ft/ft

Worksheet for 6" Service (max design slope)

Project Description

Friction Method	Manning Formula
Solve For	Discharge

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.08000	ft/ft
Normal Depth	6.00	in
Diameter	6.00	in

Results

Discharge	712.28	gal/min
Flow Area	0.20	ft ²
Wetted Perimeter	1.57	ft
Hydraulic Radius	1.50	in
Top Width	0.00	ft
Critical Depth	0.50	ft
Percent Full	100.0	%
Critical Slope	0.07385	ft/ft
Velocity	8.08	ft/s
Velocity Head	1.02	ft
Specific Energy	1.52	ft
Froude Number	0.00	
Maximum Discharge	1.71	ft ³ /s
Discharge Full	1.59	ft ³ /s
Slope Full	0.08000	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.00	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.00	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	100.00	%
Downstream Velocity	Infinity	ft/s

Worksheet for 6" Service (max design slope)

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	6.00	in
Critical Depth	0.50	ft
Channel Slope	0.08000	ft/ft
Critical Slope	0.07385	ft/ft