

# PRELIMINARY DRAINAGE REPORT

## Residential Healthcare Facility 90<sup>th</sup> Street and Raintree Drive Scottsdale, AZ 85260

Prepared For:



The Global Leader in Rental Housing

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Reviewed By	Date

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Project Number: 200626

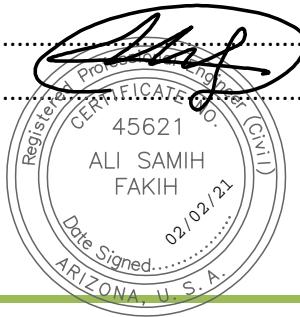
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## 1. INTRODUCTION

This Preliminary Drainage Report represents the storm water analysis for a proposed Residential Healthcare Facility located in Scottsdale, Arizona. The purpose of this report is to provide the hydrologic and hydraulic analysis, required by the City of Scottsdale, to support the proposed site plan for said development. This report includes discussions and calculations defining the storm water management concepts for the collection and conveyance necessary to comply with the drainage requirements of the City of Scottsdale and Maricopa County. Preparation of this report has been completed in accordance with the requirements of the City of Scottsdale Design Standards & Policies Manual (DS&PM) 2018 <sup>1</sup>, and the Drainage Design Manuals for Maricopa County, Arizona, Volumes I<sup>2</sup> and Volume II<sup>3</sup>.

## 2. LOCATION AND PROJECT DESCRIPTION

### 2.1 LOCATION:

The subject property consists of land located at the northwest corner of 90<sup>th</sup> Street and Raintree Circle Drive in Scottsdale, AZ:

- A portion of the Northwest 1/4 of Section 7, Township 3 North, Range 5 East of the Gila and Salt River Base and Meridian, Maricopa County, Scottsdale, Arizona.
- Parcel ID:      Parcel 217-15-033.

Refer to **FIGURE 1 - Vicinity Map** for the project's location with respect to major cross streets.

### 2.2 EXISTING AND PROPOSED DEVELOPMENTS SURROUNDING THE SITE:

- South: The site is bound by Raintree Circle Drive with the following across as follows:
  - Parcel 217-15-952; The Robinson Group; Zoning is I-1
  - Parcel 217-15-953; Wood Trust Bank; Zoning is I-1
  - Parcel 217-15-954; Epstein Schneider; Zoning is I-1
  - Parcel 217-15-955; GHA Technologies, Inc; Zoning is I-1
  - Parcel 217-15-944; Loanpal; Zoning is C-2
- North: Parcel 217-15-036E; Alliance Defending Freedom. 217-15-036J; Vanguard. Zoning is I-1.
- East: Directly adjacent is 90<sup>th</sup> Street. Across is a residential development; Zoning is R1-7
- West: Parcel 217-15-035A; Undeveloped; Zoning is I-1; Raintree & Pima Self Storage Partners LLC.

### 2.3 EXISTING SITE DESCRIPTION:

The project area includes approximately 203,311 sf. (4.67 acres) of land designated as R1-35 zoning. The proposed project will be a Residential Healthcare Facility and therefore will be rezoned to Commercial Office (C-O). The existing site consists of an undeveloped parcel. Per Topographic Survey prepared by AW Land Surveying LLC, a majority of the site slopes from northwest to southeast, while the western most portion flows from northeast to southwest at approximately 1.0%. Elevation varies from approximately 1480.66 at the northwest corner to approximately 1476.82 at the southeast corner.

Refer to **FIGURE 2** for an aerial map of the site.

#### **2.4 PROPOSED SITE DEVELOPMENT:**

The proposed development consists of a new residential healthcare facility with three and four story components, parking, and a common area with a pool. Refer to **Appendix III** - Preliminary Grading Plan for site layout.

#### **2.5 FLOOD HAZARD ZONE:**

FIRM Map Number 04013C1760L dated October 16, 2013 indicates the site is designated as Zone "X-Shaded", corresponding to 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile.

Refer to **FIGURE 3** for the current FIRM map.

### **3. EXISTING DRAINAGE CONDITIONS**

#### **3.1 OFF-SITE DRAINAGE PATTERNS**

The topographic survey and city quarter section maps, **FIGURES 4 and 5**, provide the following information for offsite drainage:

- **North:**
  - Parcels 217-15-036E and 217-15-036J are developed sites that retain their onsite runoff. The existing curb and gutter along the northwest portion of the property line and the existing retention basin along the northeast portion of the property boundary maintain runoff from northern parcels and do not affect the proposed site.
  - There is an existing 24" RGRCP storm pipe discharging onto the northeast corner of the site via a headwall (EX HW-1). This system conveys runoff from 90<sup>th</sup> Street and restricted discharge for a retention basin from the Raintree Corporate Center approximately 650' north. The flow discharging to the site is currently unknown. According to the Scottsdale Corporate Center, Phase 2 Grading Plan, CASE #86-DR-87, the existing 24" pipe has a slope of 0.005 ft/ft, assuming full capacity of the pipe, the maximum flow discharging to the site is 16 cfs.
- **West:**
  - There is a ridgeline within the west portion of the subject property that directs flows northeast to southwest prohibiting runoff from the western adjacent parcel from entering the site.
- **South:**
  - There is an elevation difference of +/- 3 feet from north to south throughout the site, as such, offsite drainage from the southern parcel does not affect the site.
- **East:**
  - There is an existing catch basin at 90<sup>th</sup> Street that drains to the property, approximately 60' north of the southeast corner of the site. A second catch basin is located on the northbound side of 90<sup>th</sup> Street. According to the Storm QS map 34-49, both basins are connected by a pipe of unknown size and material and discharge onsite through the existing headwall, EX HW-2. The calculated runoff from 90<sup>th</sup> Street was determined using the rational method based on the estimated drainage area. Refer to **Appendix II** for Existing Conditions Drainage Area Map.
  -

<b>Table 1: Offsite Flows Summary</b>		
Headwall ID	Description	Flow (CF)
EX-HW-1	24" RCP capturing runoff from north parcels	16.00
EX-HW-2	24" RCP capturing runoff from 90th Street	6.20
	<b>TOTAL:</b>	<b>22.20</b>

The offsite runoff from the north and from 90<sup>th</sup> Street exit the site through a headwall located near the southeast corner of the site, EX HW-3. Considering runoff from the offsite flows specified above and including an additional flow of 3.4 cfs from drainage area EX-1, the estimated flow,  $Q_{out}$ , leaving EX. HW-3 is 25.60 cfs. Refer to **Appendix II** for Offsite Existing Conditions Drainage Area Map.

### **3.2 ON-SITE DRAINAGE PATTERNS**

The site is currently undeveloped and slopes from northwest to southeast at approximately 0.5%. Elevation varies from approximately 1480.66 at the northwest corner to approximately 1476.82 at the southeast corner. All existing on-site runoff is assumed to sheet flow following the natural slope of the land. Existing drainage area EX-3 at the west of the site drains to HO-3 located exactly at the southwest corner of the property, where the corresponding flow of 3.1 cfs exits the site. EX-2 ultimately drains to HO-2 at the south boundary of the site with a flow of 9.6 cfs. As described above, drainage for EX-1 is provided by HO-1, where an estimated 25.60 cfs leave the site through existent headwall EX-HW-3 that connects to the public storm drain system.

## **4. PROPOSED STORM WATER MANAGEMENT**

### **4.1 DESIGN INTENT:**

On-site run-off from the east will be captured by catch basins directing flows to two above-ground retention basins. On-site runoff from the west will be directed to an underground CMP storage system located in the northeastern portion of the site. Three proposed drywells will treat and discharge captured stormwater runoff within 36 hours.

Refer to **Appendix II** for Proposed Conditions Drainage Area Map.

The site will be self-retaining for the 100-year, 2-hr storm event. Existing offsite drainage patterns will remain unchanged. Flows from Existing Headwall 1 (EX-HW-1) and Existing Headwall 2 (EX-HW-2) will be rerouted to the existing storm drain manhole (EX-MH-2) on the northwest corner of 90<sup>th</sup> Street and Raintree Circle Drive via a 24" storm pipe. Pipe hydraulic calculations were performed to size and design the required slopes for the pipes rerouting offsite flows.

Refer to **Appendix II** for Offsite pipe hydraulic calculations

Refer to **Appendix III** for Preliminary Grading and Drainage Plan.

### **4.2 DESIGN STORM REQUIREMENTS:**

In accordance with The City of Scottsdale requirements, stormwater storage for a 100-year 2-hour storm event is required.

#### **4.3 LAND CHARACTERISTICS:**

The proposed development consists of a multi-story commercial building with a main drive and minor landscape areas along the perimeter. Based on the DS&PM, the weighted runoff coefficient for a 100-year storm event used is as follows:

- C=0.95 for paved streets, parking lots (concrete or asphalt), roofs, driveways, etc.
- C=0.45 for undisturbed natural desert or desert landscaping (no impervious weed barrier).

**HYDROLOGIC ANALYSIS:** The hydrologic analysis is determined using the procedures in The City of Scottsdale Design Standards & Policies Manual and the Drainage Design Manual for Maricopa County, Arizona, Volume I. The Rational Method was utilized to compute the on-site peak discharges. The Rational Method equation is displayed as shown below:

$$Q=C_{wt}IA$$

Where:  $C_{wt}$  = The runoff coefficient relating runoff to rainfall

I = Average rainfall intensity in inches/hour, lasting for Tc

Tc = The time of concentration (Using Five minutes for the developed areas)

A = The contributing drainage area in acres

Q= Estimated peak discharge at inlet point, cfs.

Refer to the **Proposed Conditions Drainage Area Map** and Calculations in **Appendix II**.

#### **4.4 STORMWATER RETENTION:**

Based on a topographic survey there is no retention provided in existing conditions. Per the above equation, the proposed development storage requirements for the 100-yr, 2-hr storm event are shown below. A combination of underground stormwater storage tanks and open retention basins will be employed to retain the required stormwater volume. In the case of the open retention basins, an equalizer pipe will be installed between both basins to combine their retention capacity.

##### **4.4.1 STORAGE REQUIRED:**

Stormwater storage required for the 100-year, 2-hour event is calculated in accordance with The City of Scottsdale - DS&PM. Required Retention (Acre-Feet)  $V_R = (P/12)*A*C$

Where: P = 100-yr, 2-hr precipitation in inches (Ref: Isopluvial from DS&PM, Appendix 4-1D, pg.11 and NOAA Atlas 14 table). According to this reference, P = 2.27 in for the site location. Refer to **Appendix I** for rainfall data.

Based on the weighted runoff coefficient (Cwt) identified in Section 4.3, the following retention is required:

**Basin A (Open Retention):** 1.42 ac @ Cwt= 0.73

- 100-yr 2-hr.:

$$V_R = 2.27/12 * 1.42 * 0.73 = \mathbf{0.19 \text{ ac.ft. (8,637 c.f.) REQUIRED STORAGE}}$$

**Basin B (Underground Storage):** 3.28 ac @ Cwt= 0.86

- 100-yr 2-hr.:

$$V_R = 2.27/12 * 3.28 * 0.87 = \mathbf{0.53 \text{ ac.ft. (23,160 c.f.) REQUIRED STORAGE}}$$

#### 4.4.2 STORAGE PROVIDED:

The proposed retention consists of two open retention basins (Retention Basin A) and two connected 10-ft diameter corrugated metal pipes (Retention Basin B).

Retention A is proposed as an equalized hydraulic system, connecting both open retention basins with an 18" HDPE pipe at an elevation of 77.50', one-foot above the bottom of basin. The system discharges to a drywell with rims located above the bottom elevation of Basin A1. Equalizing the open retention basins provides additional retention volume to basin A2 that would otherwise not have sufficient storage capacity as an independent system.

- The proposed volume for the open retention was calculated using the area-sum method based on design contours.
- Storage volume of underground piping is calculated using  $V_p = \pi(R^2) * L$ . Table 2 summarizes the calculated volume provided and volume required and verifies that proposed basins are adequate to store the required volume for the 100-yr, 2-hr storm event.

Refer to **Appendix II** for **Provided Storage Calculations**.

**Table 2:**

<b>Proposed Retention Basin Summary</b>						
		Basin	TYPE	Vp	Vp total	Vr
		(ID)	(--)	(CF)	(CF)	(CF)
Basin A	Basin A1	OPEN		6,192	10,182	8,637
	Basin A2	OPEN		3,990		
Basin B		UG		25,133	25,133	23,160
				TOTAL	35,314	31,797

#### 4.4.3 STORMWATER DISCHARGE:

For Basins with no direct bleed-off available, drywells are proposed for the on-site storage facilities to empty all basins within thirty-six (36) hours. The calculation is as follows:

- Minimum percolating rate of a drywell (for planning purposes) = 0.1 cfs
- Volume to be drained in 36 hours = 0.1 cfs \* 36 hours \* 3600 sec/hour = 12,960 cf = 0.298 acre-feet.

- Basin A retention provided = 10,702 cf  
Therefore, 10,702 cf / 12,960 cf per drywell = 0.83= 1 drywell required.  
Basin B retention provided  
Therefore, 25,133 cf / 12,960 cf per drywell = 1.93= 2 drywells required.
- The drywells are to be installed according to FCDMC guidelines.
- The number of drywells may be reduced if geotechnical testing for percolation rates determine adequate infiltration is available in the native soils at lower depths. If the percolation rate of the drywells is less than 0.1 cfs the number of drywells may have to be increased.

#### 4.5 STORM DRAIN INLET CALCULATIONS

MAG 535 type "F" catch basins are proposed in the parking lot areas to capture on-site storm run-off.

Nyloplast 2'x3' Steel Bar/MAG Grate and Nyloplast 18" will be used to capture flows from the curb openings at the southwest of the site.

- A MAG 535 catch basin can convey a flow of 4.95 cfs, while considering a clogging factor of 0.50. The proposed catch basin inlets can adequately convey runoff for the maximum 100-year, 5-min event,  $Q_{100} = \mathbf{3.04 \text{ cfs (CB-3)}}$ .
- The Nyloplast 2'x3' Steel Bar/MAG Grate Nyloplast catch basin can convey a flow of 6.75 cfs, while considering a clogging factor of 0.50. The proposed catch basin inlets can adequately convey runoff for the maximum 100-year, 5-min event,  $Q_{100} = \mathbf{5.69 \text{ (CB-5)}}$ .
- The 18" Nyloplast catch basin can convey a flow of 1.35 cfs, while considering a clogging factor of 0.50. The proposed catch basin inlets can adequately convey runoff for the maximum 100-year, 5-min event,  $Q_{100} = \mathbf{0.96 \text{ (CB-4)}}$ .

**Table 3:**

100-yr Runoff Calculation Summary								
P=100-yr, 5-min=7.72 in/hr								
Drainage	Area	$C_w$	Intensity	Q	Qtotall	Structure	Structure	Capacity
Area ID	(acres)	(-)	(in/hr)	(cfs)	(cfs)	ID	Type	(cfs)
DA-1	0.40	0.84	7.72	2.59	2.59	CB-1A	MAG 535	4.95
DA-2	0.36	0.84	7.72	2.31	2.31	CB-1	MAG 535	4.95
DA-3	0.21	0.85	7.72	1.40	1.40	CO-1	Curb opening	-
DA-4	0.08	0.88	7.72	0.51	0.51	CO-2	Curb opening	-
DA-5	0.24	0.45	7.72	0.84	0.84	N/A	N/A	-
DA-6	0.21	0.87	7.72	1.41	1.41	CO-3	Curb opening	-
DA-7	0.16	0.45	7.72	0.54	0.54	N/A	N/A	-
DA-8	0.52	0.84	7.72	3.38	3.38	CO-4	Curb opening	-
DA-9	0.32	0.84	7.72	2.05	5.69	CB-6A	2' x 3' Nyloplast Steel Bar	6.75
DA-12	0.61	0.77	7.72	3.63				
DA-10	0.15	0.82	7.72	0.96	0.96	CB-5A	18" Nyloplast	1.35
DA-11	0.47	0.84	7.72	3.04	3.04	CB-4A	MAG 535	4.95
DA-13	0.97	0.95	7.72	7.11	7.11	R-1	Roof drain	-

#### **4.6 STREET CAPACITY CALCULATIONS**

Street capacity was verified using *Hydraflow Express Extension for Autodesk Civil 3D* to obtain the stormwater spread and depth at the edge of curb, ensuring at ultimate conditions, run-off will not overflow the street. CB-5 with the greatest flow of 6.16 cfs has a depth of 5.4" at the edge of curb under 100-yr, 2-hr ultimate conditions. All proposed inlets have a depth of less than 6" (curb height) evaluated at 100-yr, 2-hr ultimate conditions.

Refer to **Appendix II** for street capacity calculations for proposed inlets.

**Table 4:**

<b>100-yr STREET CAPACITY SUMMARY</b>									
P=100-yr, 5-min=7.72 in/hr									
Drainage	Area	C <sub>w</sub>	Intensity	Q	Qtotal	Structure	Structure	Depth at curb	Spread
Area ID	(acres)	(-)	(in/hr)	(cfs)	(cfs)	ID	Type	(in)	(ft)
DA-1	0.40	0.84	7.72	2.59	2.59	CB-1A	MAG 535	3.5	8.53
DA-2	0.36	0.84	7.72	2.31	2.31	CB-1	MAG 535	3.2	14.51
DA-11	0.47	0.84	7.72	3.04	3.04	CB-4A	MAG 535	3.8	12.74

#### **4.7 ADEQ WATER QUALITY REQUIREMENTS**

The total disturbed area of this site is approximately 4.67 acres. The Arizona Department of Environmental Quality requires that any site disturbance over one acre is required to submit an NOI. An NOI will be submitted to ADEQ for this site prior to approval of construction documents as site disturbance for this project exceeds one acre.

### **5. FLOOD SAFETY FOR DWELLINGS**

#### **5.1 FINISHED FLOOR ELEVATIONS**

This project lies in an "X-Shaded" Flood Zone. The ultimate outfall elevation for the site is 1479.72 and is located at the southeast corner of the site. Therefore, the proposed building finished floor elevations will be set a minimum of 12 inches above the 100-year high-water elevation of any adjacent streets and drainage paths and 14" above ultimate lot outfall. This will ensure that finished floor elevations will be set sufficiently above the 100-year water level so as to not be in danger of flooding during a 100 yr-2hr storm event.

## 6. CONCLUSIONS

### 6.1 OVERALL PROJECT:

1. The finish floor elevations will be designed a minimum of 12 inches above the 100-year water surface in adjacent streets and drainage paths and a minimum of 14 inches above the low top of curb of the lot.
2. All on-site storm water will be retained on-site and is provided for the 100-yr, 2-hr storm event with discharge within 36-hours. A combination of equalized underground tanks and open retention basins will be used to store the required stormwater volume.

### 6.2 PROJECT PHASING:

This project will be constructed in a single phase.

## 7. WARNING AND DISCLAIMER OF LIABILITY

GRADING & DRAINAGE	<b>GRADING &amp; DRAINAGE LANGUAGE</b>	APPENDIX 4-1C
<b>WARNING AND DISCLAIMER OF LIABILITY</b>		
<p>The City's Stormwater and Floodplain Management Ordinance is intended to minimize the occurrence of losses, hazards and conditions adversely affecting the public health, safety and general welfare which might result from flooding. The Stormwater and Floodplain Management Ordinance identifies floodplains, floodways, flood fringes and special flood hazard areas. However, a property outside these areas could be inundated by floods. Also, much of the city is a dynamic flood area; floodways, floodplains, flood fringes and special flood hazard areas may shift from one location to another, over time, due to natural processes.</p> <p><b>WARNING AND DISCLAIMER OF LIABILITY</b></p> <p>The flood protection provided by the Stormwater and Floodplain Management Ordinance is considered reasonable for regulatory purposes and is based on scientific and engineering considerations. Floods larger than the base flood can and will occur on rare occasions. Floodwater heights may be increased by constructed or natural causes. The Stormwater and Floodplain Management Ordinance does not create liability on the part of the city, any officer or employee thereof, or the federal, state or county government for any flood damages that result from reliance on the Ordinance or any administrative decision lawfully made thereunder.</p> <p>Compliance with the Stormwater and Floodplain Management Ordinance does not ensure complete protection from flooding. Flood-related problems such as natural erosion, streambed meander, or constructed obstructions and diversions may occur and have an adverse effect in the event of a flood. You are advised to consult your own engineer or other expert regarding these considerations.</p> <p>I have read and understand the above.</p>		
Plan Check #	Owner	Date

*From City of Scottsdale DPSM-2018. Page 219*

## 8. REFERENCES

1. *Design Standards & Policies Manual, City of Scottsdale – January 2018*
2. *Drainage Design Manual for Maricopa County, Arizona, Volume I, Hydrology, Flood Control District of Maricopa County, Fourth Edition, December 14, 2018*
3. *Drainage Design Manual for Maricopa County, Arizona, Volume II, Hydraulics, Flood Control District of Maricopa County, December 14, 2018*



## **FIGURE 1 – Vicinity Map**

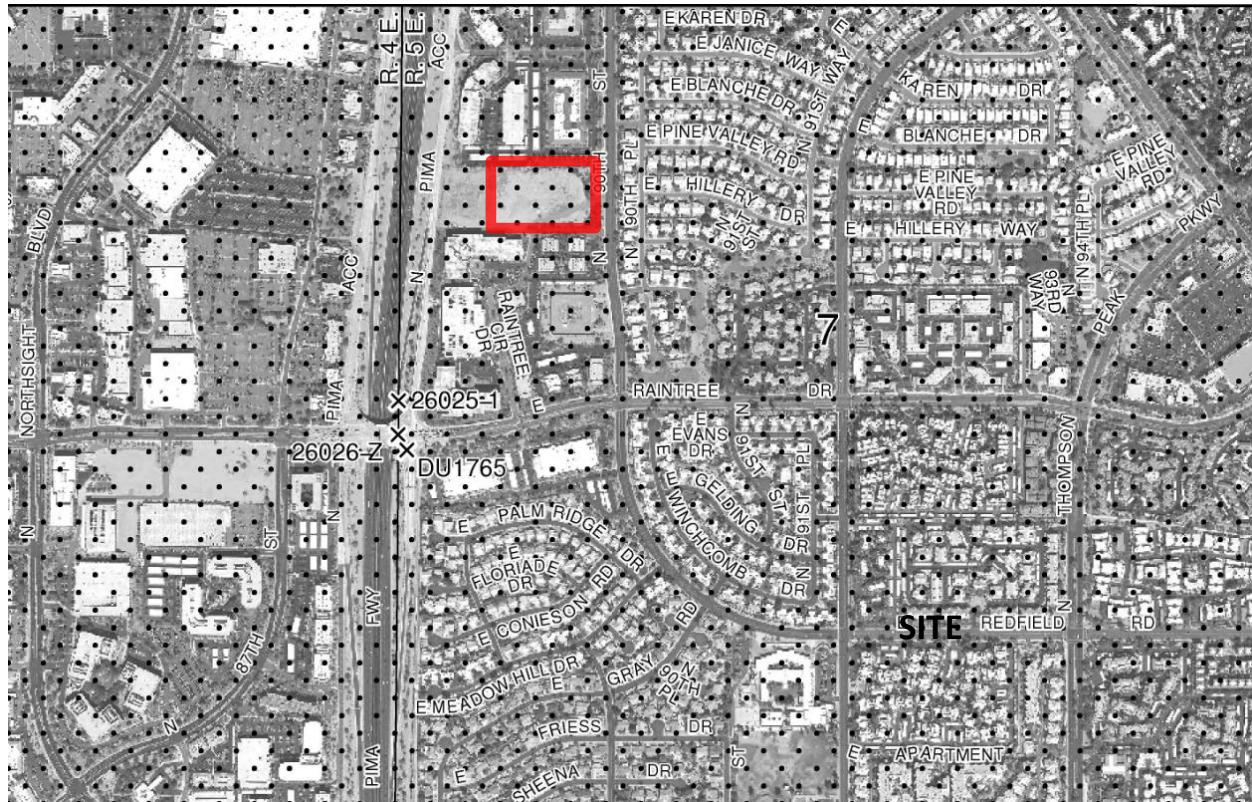
***FIGURE 2 - Aerial***

8280 E. Gelding Dr., Suite 101  
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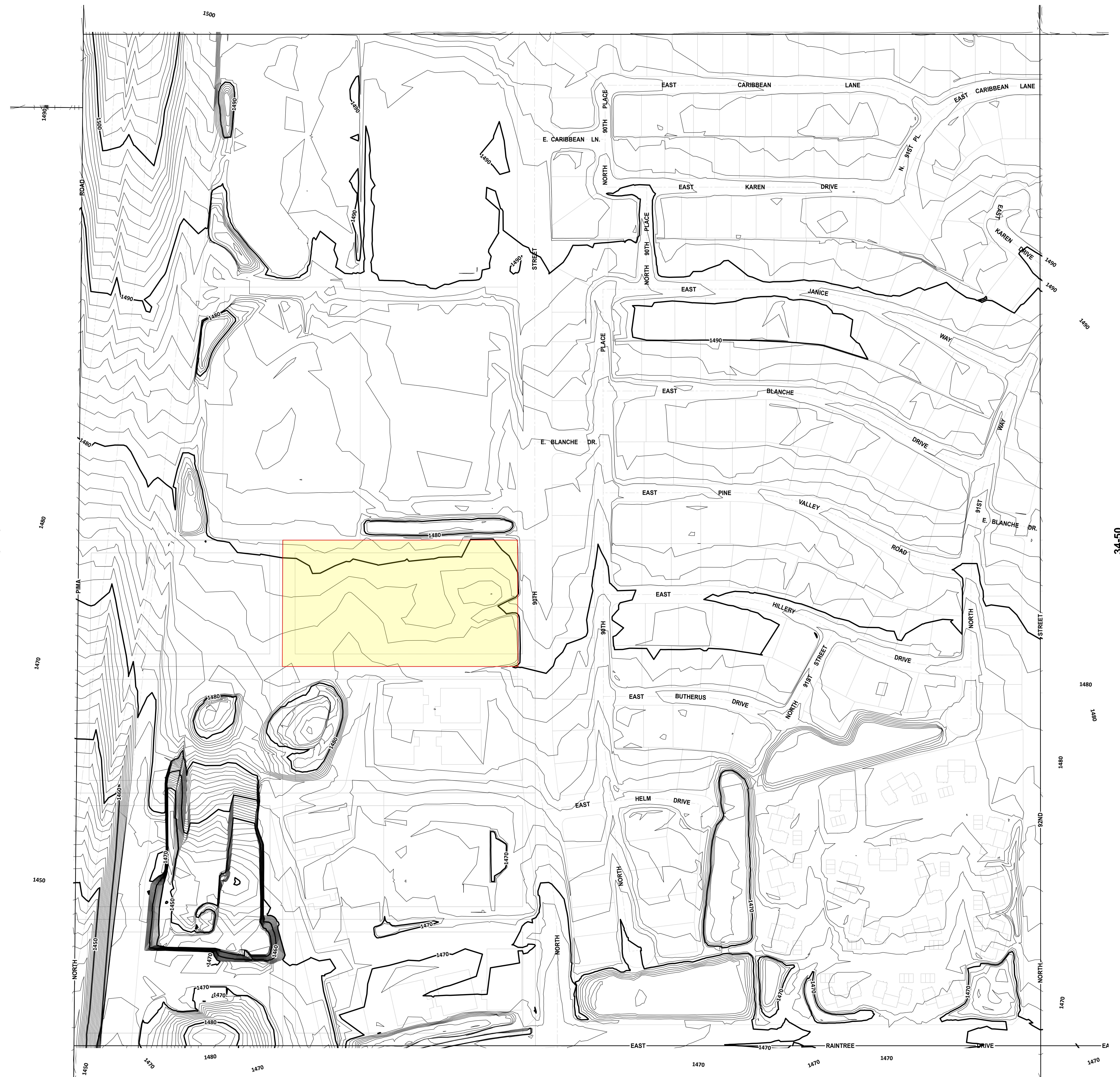
4-DR-2021  
2/8/2021



**FIGURE 3 – FEMA FIRM**  
*Excerpt from 04013C1760L*



34-48



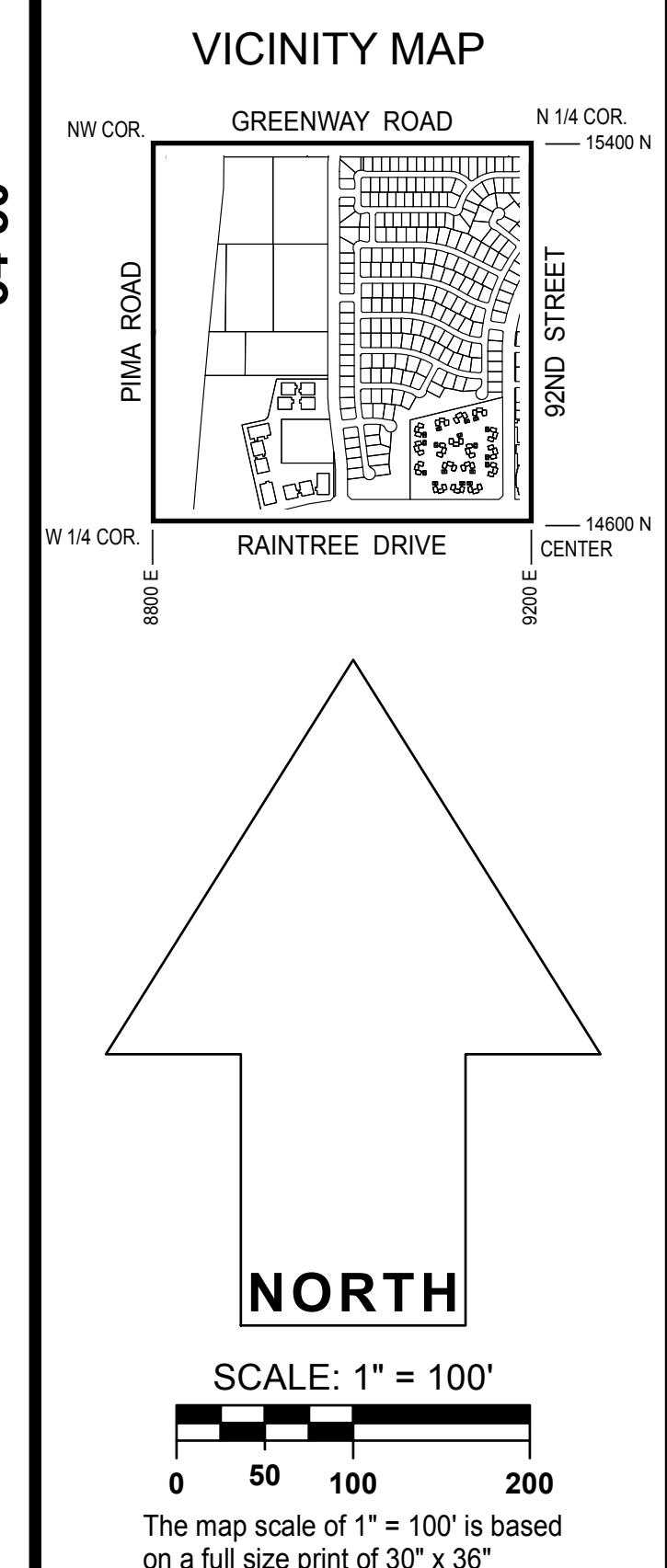
35-49

33-49

**GENERAL NOTES:**

- THIS IS A COMPUTER GENERATED DRAWING. FOR ANY REVISIONS PLEASE CONTACT THE CITY OF SCOTTSDALE GIS DEPARTMENT AT (480) 312-7792.
- THE SECTION LINE BEARING AND DISTANCES ARE BASED ON THE CITY OF SCOTTSDALE GPS SURVEY OF SEPTEMBER, 1991. BEARINGS ARE NAD 83 GRID AND DISTANCES ARE FLATTENED TO GROUND. WHERE NO CORNER WAS FOUND THE DIMENSIONS ARE GIVEN TO CALCULATED SECTION CORNERS AND ARE NOTED AS CALCULATED ON THE MAP.

### LEGEND:



**CONTOUR QUARTER SECTION MAP**  
**34-49**  
 NW 1/4 SEC. 7 T3N R5E

FIGURE 5

## *APPENDIX I*

### *Rainfall Data*

*8280 E. Gelding Dr., Suite 101  
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APPENDIX

4-DR-2021  
2/8/2021



### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

#### PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	<b>0.194</b> (0.161-0.238)	<b>0.253</b> (0.212-0.310)	<b>0.341</b> (0.283-0.417)	<b>0.410</b> (0.338-0.498)	<b>0.501</b> (0.406-0.607)	<b>0.571</b> (0.458-0.686)	<b>0.643</b> (0.506-0.772)	<b>0.714</b> (0.554-0.856)	<b>0.811</b> (0.613-0.974)	<b>0.885</b> (0.655-1.06)
10-min	<b>0.295</b> (0.245-0.362)	<b>0.385</b> (0.322-0.472)	<b>0.520</b> (0.431-0.634)	<b>0.623</b> (0.514-0.758)	<b>0.762</b> (0.618-0.924)	<b>0.868</b> (0.696-1.05)	<b>0.978</b> (0.771-1.18)	<b>1.09</b> (0.842-1.30)	<b>1.24</b> (0.933-1.48)	<b>1.35</b> (0.997-1.62)
15-min	<b>0.366</b> (0.304-0.448)	<b>0.478</b> (0.399-0.585)	<b>0.644</b> (0.533-0.786)	<b>0.772</b> (0.637-0.940)	<b>0.945</b> (0.766-1.15)	<b>1.08</b> (0.863-1.30)	<b>1.21</b> (0.955-1.46)	<b>1.35</b> (1.04-1.62)	<b>1.53</b> (1.16-1.84)	<b>1.67</b> (1.24-2.01)
30-min	<b>0.492</b> (0.409-0.603)	<b>0.643</b> (0.538-0.788)	<b>0.868</b> (0.718-1.06)	<b>1.04</b> (0.858-1.27)	<b>1.27</b> (1.03-1.54)	<b>1.45</b> (1.16-1.74)	<b>1.63</b> (1.29-1.96)	<b>1.81</b> (1.41-2.18)	<b>2.06</b> (1.56-2.48)	<b>2.25</b> (1.67-2.70)
60-min	<b>0.609</b> (0.506-0.746)	<b>0.796</b> (0.665-0.976)	<b>1.07</b> (0.889-1.31)	<b>1.29</b> (1.06-1.57)	<b>1.57</b> (1.28-1.91)	<b>1.79</b> (1.44-2.16)	<b>2.02</b> (1.59-2.43)	<b>2.25</b> (1.74-2.69)	<b>2.55</b> (1.93-3.06)	<b>2.78</b> (2.06-3.35)
2-hr	<b>0.713</b> (0.600-0.853)	<b>0.923</b> (0.780-1.11)	<b>1.23</b> (1.03-1.46)	<b>1.46</b> (1.21-1.74)	<b>1.78</b> (1.47-2.11)	<b>2.02</b> (1.64-2.39)	<b>2.27</b> (1.81-2.67)	<b>2.52</b> (1.98-2.97)	<b>2.86</b> (2.19-3.36)	<b>3.12</b> (2.34-3.69)
3-hr	<b>0.790</b> (0.666-0.969)	<b>1.01</b> (0.855-1.25)	<b>1.32</b> (1.11-1.62)	<b>1.57</b> (1.30-1.91)	<b>1.91</b> (1.56-2.31)	<b>2.19</b> (1.77-2.63)	<b>2.47</b> (1.96-2.96)	<b>2.77</b> (2.16-3.31)	<b>3.17</b> (2.40-3.80)	<b>3.50</b> (2.59-4.20)
6-hr	<b>0.953</b> (0.818-1.13)	<b>1.20</b> (1.03-1.43)	<b>1.53</b> (1.31-1.82)	<b>1.80</b> (1.52-2.12)	<b>2.16</b> (1.80-2.54)	<b>2.44</b> (2.00-2.85)	<b>2.73</b> (2.21-3.18)	<b>3.03</b> (2.41-3.54)	<b>3.43</b> (2.66-4.01)	<b>3.75</b> (2.84-4.39)
12-hr	<b>1.07</b> (0.922-1.26)	<b>1.35</b> (1.16-1.59)	<b>1.70</b> (1.46-2.00)	<b>1.98</b> (1.68-2.32)	<b>2.35</b> (1.98-2.75)	<b>2.64</b> (2.20-3.07)	<b>2.94</b> (2.41-3.41)	<b>3.24</b> (2.62-3.76)	<b>3.63</b> (2.87-4.24)	<b>3.94</b> (3.06-4.63)
24-hr	<b>1.25</b> (1.10-1.44)	<b>1.59</b> (1.40-1.83)	<b>2.05</b> (1.79-2.36)	<b>2.41</b> (2.11-2.78)	<b>2.93</b> (2.54-3.36)	<b>3.33</b> (2.86-3.82)	<b>3.75</b> (3.19-4.31)	<b>4.19</b> (3.53-4.81)	<b>4.80</b> (3.97-5.52)	<b>5.29</b> (4.31-6.10)
2-day	<b>1.35</b> (1.18-1.56)	<b>1.72</b> (1.50-1.99)	<b>2.26</b> (1.96-2.60)	<b>2.68</b> (2.33-3.08)	<b>3.27</b> (2.82-3.76)	<b>3.74</b> (3.19-4.29)	<b>4.23</b> (3.58-4.87)	<b>4.75</b> (3.98-5.47)	<b>5.46</b> (4.51-6.31)	<b>6.04</b> (4.91-7.01)
3-day	<b>1.45</b> (1.28-1.67)	<b>1.86</b> (1.63-2.13)	<b>2.45</b> (2.14-2.80)	<b>2.92</b> (2.55-3.34)	<b>3.59</b> (3.11-4.10)	<b>4.13</b> (3.55-4.71)	<b>4.70</b> (4.01-5.38)	<b>5.31</b> (4.48-6.09)	<b>6.16</b> (5.12-7.08)	<b>6.85</b> (5.63-7.91)
4-day	<b>1.56</b> (1.38-1.78)	<b>1.99</b> (1.76-2.27)	<b>2.64</b> (2.32-3.00)	<b>3.17</b> (2.78-3.60)	<b>3.91</b> (3.41-4.45)	<b>4.52</b> (3.92-5.14)	<b>5.17</b> (4.44-5.89)	<b>5.87</b> (4.99-6.70)	<b>6.85</b> (5.74-7.84)	<b>7.66</b> (6.34-8.81)
7-day	<b>1.76</b> (1.54-2.02)	<b>2.25</b> (1.97-2.58)	<b>2.98</b> (2.61-3.41)	<b>3.58</b> (3.12-4.09)	<b>4.43</b> (3.84-5.06)	<b>5.12</b> (4.41-5.85)	<b>5.86</b> (5.01-6.71)	<b>6.66</b> (5.63-7.64)	<b>7.78</b> (6.48-8.96)	<b>8.70</b> (7.16-10.1)
10-day	<b>1.91</b> (1.68-2.18)	<b>2.45</b> (2.15-2.79)	<b>3.24</b> (2.84-3.69)	<b>3.88</b> (3.39-4.41)	<b>4.79</b> (4.16-5.44)	<b>5.52</b> (4.76-6.27)	<b>6.30</b> (5.40-7.17)	<b>7.13</b> (6.05-8.13)	<b>8.30</b> (6.94-9.50)	<b>9.25</b> (7.64-10.6)
20-day	<b>2.36</b> (2.09-2.69)	<b>3.05</b> (2.69-3.46)	<b>4.03</b> (3.55-4.57)	<b>4.78</b> (4.19-5.42)	<b>5.79</b> (5.06-6.57)	<b>6.58</b> (5.72-7.47)	<b>7.39</b> (6.39-8.41)	<b>8.22</b> (7.06-9.38)	<b>9.34</b> (7.94-10.7)	<b>10.2</b> (8.61-11.8)
30-day	<b>2.78</b> (2.44-3.15)	<b>3.57</b> (3.15-4.06)	<b>4.72</b> (4.16-5.35)	<b>5.60</b> (4.92-6.33)	<b>6.78</b> (5.93-7.67)	<b>7.70</b> (6.70-8.71)	<b>8.64</b> (7.48-9.78)	<b>9.61</b> (8.26-10.9)	<b>10.9</b> (9.29-12.4)	<b>11.9</b> (10.1-13.6)
45-day	<b>3.24</b> (2.87-3.67)	<b>4.18</b> (3.70-4.73)	<b>5.52</b> (4.88-6.24)	<b>6.52</b> (5.75-7.37)	<b>7.85</b> (6.89-8.87)	<b>8.86</b> (7.75-10.0)	<b>9.90</b> (8.60-11.2)	<b>10.9</b> (9.45-12.4)	<b>12.3</b> (10.5-14.1)	<b>13.4</b> (11.4-15.4)
60-day	<b>3.60</b> (3.20-4.07)	<b>4.66</b> (4.13-5.25)	<b>6.14</b> (5.44-6.91)	<b>7.22</b> (6.38-8.14)	<b>8.64</b> (7.61-9.74)	<b>9.71</b> (8.51-11.0)	<b>10.8</b> (9.40-12.2)	<b>11.9</b> (10.3-13.4)	<b>13.3</b> (11.4-15.1)	<b>14.3</b> (12.2-16.4)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

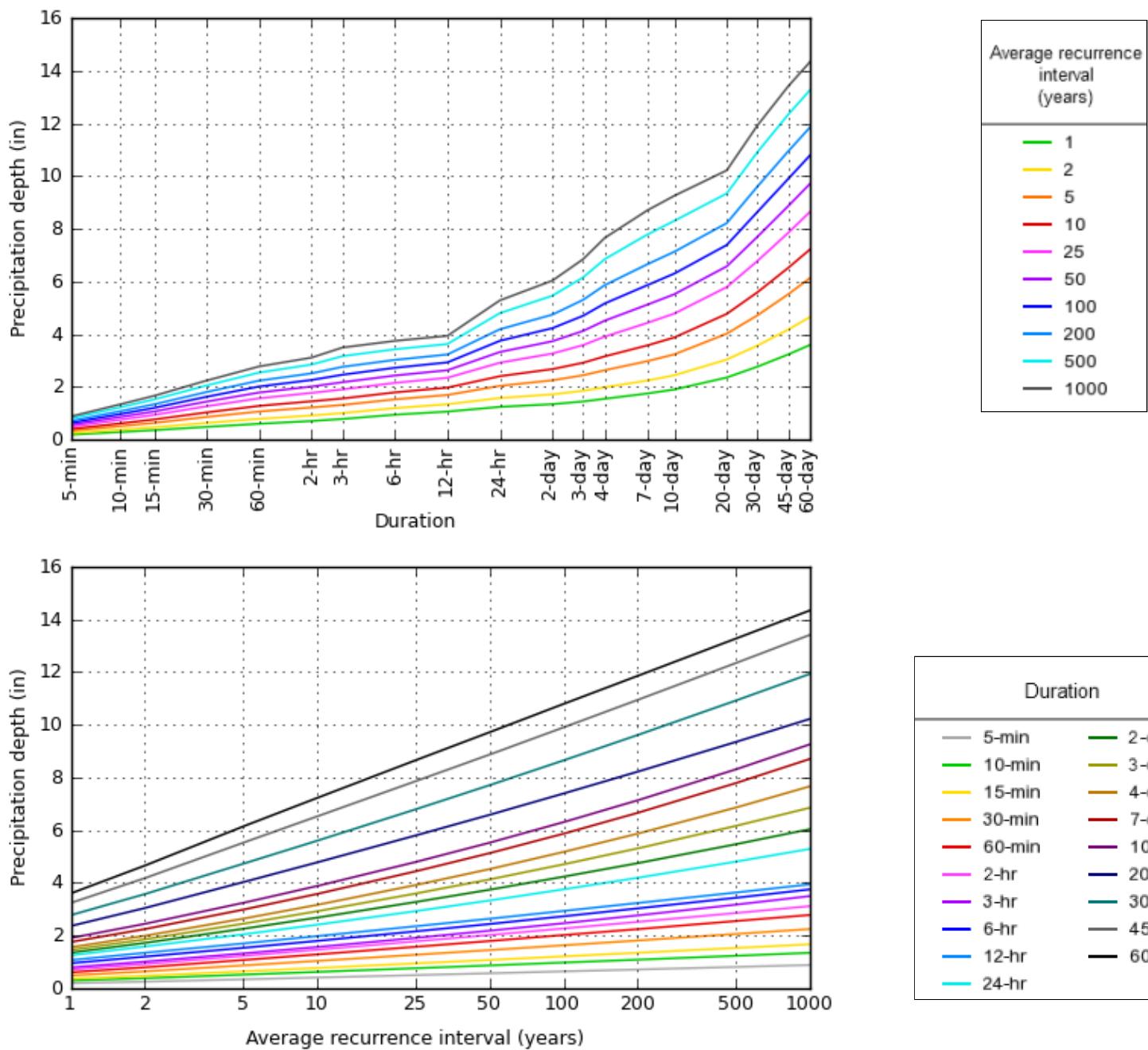
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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#### PF graphical

PDS-based depth-duration-frequency (DDF) curves  
 Latitude: 33.6220°, Longitude: -111.8880°



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## Maps & aerials

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## POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

[PF tabular](#) | [PF graphical](#) | [Maps & aerials](#)

### PF tabular

Duration	Average recurrence interval (years)									
	1	2	5	10	25	50	100	200	500	1000
5-min	<b>2.33</b> (1.93-2.86)	<b>3.04</b> (2.54-3.72)	<b>4.09</b> (3.40-5.00)	<b>4.92</b> (4.06-5.98)	<b>6.01</b> (4.87-7.28)	<b>6.85</b> (5.50-8.23)	<b>7.72</b> (6.07-9.26)	<b>8.57</b> (6.65-10.3)	<b>9.73</b> (7.36-11.7)	<b>10.6</b> (7.86-12.8)
10-min	<b>1.77</b> (1.47-2.17)	<b>2.31</b> (1.93-2.83)	<b>3.12</b> (2.59-3.80)	<b>3.74</b> (3.08-4.55)	<b>4.57</b> (3.71-5.54)	<b>5.21</b> (4.18-6.27)	<b>5.87</b> (4.63-7.05)	<b>6.52</b> (5.05-7.82)	<b>7.41</b> (5.60-8.90)	<b>8.08</b> (5.98-9.72)
15-min	<b>1.46</b> (1.22-1.79)	<b>1.91</b> (1.60-2.34)	<b>2.58</b> (2.13-3.14)	<b>3.09</b> (2.55-3.76)	<b>3.78</b> (3.06-4.58)	<b>4.30</b> (3.45-5.18)	<b>4.85</b> (3.82-5.83)	<b>5.39</b> (4.18-6.46)	<b>6.12</b> (4.62-7.35)	<b>6.68</b> (4.94-8.03)
30-min	<b>0.984</b> (0.818-1.21)	<b>1.29</b> (1.08-1.58)	<b>1.74</b> (1.44-2.12)	<b>2.08</b> (1.72-2.53)	<b>2.54</b> (2.06-3.09)	<b>2.90</b> (2.33-3.49)	<b>3.27</b> (2.57-3.92)	<b>3.63</b> (2.81-4.35)	<b>4.12</b> (3.11-4.95)	<b>4.50</b> (3.33-5.41)
60-min	<b>0.609</b> (0.506-0.746)	<b>0.796</b> (0.665-0.976)	<b>1.07</b> (0.889-1.31)	<b>1.29</b> (1.06-1.57)	<b>1.57</b> (1.28-1.91)	<b>1.79</b> (1.44-2.16)	<b>2.02</b> (1.59-2.43)	<b>2.25</b> (1.74-2.69)	<b>2.55</b> (1.93-3.06)	<b>2.78</b> (2.06-3.35)
2-hr	<b>0.356</b> (0.300-0.426)	<b>0.462</b> (0.390-0.553)	<b>0.614</b> (0.516-0.732)	<b>0.730</b> (0.607-0.870)	<b>0.890</b> (0.733-1.05)	<b>1.01</b> (0.820-1.19)	<b>1.14</b> (0.906-1.34)	<b>1.26</b> (0.990-1.48)	<b>1.43</b> (1.10-1.68)	<b>1.56</b> (1.17-1.84)
3-hr	<b>0.263</b> (0.222-0.323)	<b>0.337</b> (0.285-0.415)	<b>0.440</b> (0.370-0.539)	<b>0.522</b> (0.434-0.635)	<b>0.636</b> (0.521-0.769)	<b>0.728</b> (0.588-0.874)	<b>0.822</b> (0.652-0.987)	<b>0.921</b> (0.718-1.10)	<b>1.06</b> (0.799-1.26)	<b>1.17</b> (0.861-1.40)
6-hr	<b>0.159</b> (0.137-0.189)	<b>0.201</b> (0.172-0.239)	<b>0.256</b> (0.218-0.303)	<b>0.300</b> (0.254-0.354)	<b>0.361</b> (0.301-0.423)	<b>0.407</b> (0.334-0.476)	<b>0.456</b> (0.369-0.532)	<b>0.506</b> (0.402-0.592)	<b>0.573</b> (0.444-0.669)	<b>0.627</b> (0.474-0.733)
12-hr	<b>0.089</b> (0.077-0.105)	<b>0.112</b> (0.096-0.132)	<b>0.141</b> (0.121-0.166)	<b>0.164</b> (0.140-0.192)	<b>0.195</b> (0.164-0.228)	<b>0.219</b> (0.182-0.255)	<b>0.244</b> (0.200-0.283)	<b>0.269</b> (0.217-0.312)	<b>0.302</b> (0.238-0.352)	<b>0.327</b> (0.254-0.385)
24-hr	<b>0.052</b> (0.046-0.060)	<b>0.066</b> (0.058-0.076)	<b>0.085</b> (0.075-0.099)	<b>0.101</b> (0.088-0.116)	<b>0.122</b> (0.106-0.140)	<b>0.139</b> (0.119-0.159)	<b>0.156</b> (0.133-0.180)	<b>0.175</b> (0.147-0.201)	<b>0.200</b> (0.166-0.230)	<b>0.220</b> (0.180-0.254)
2-day	<b>0.028</b> (0.025-0.032)	<b>0.036</b> (0.031-0.041)	<b>0.047</b> (0.041-0.054)	<b>0.056</b> (0.048-0.064)	<b>0.068</b> (0.059-0.078)	<b>0.078</b> (0.066-0.089)	<b>0.088</b> (0.075-0.101)	<b>0.099</b> (0.083-0.114)	<b>0.114</b> (0.094-0.132)	<b>0.126</b> (0.102-0.146)
3-day	<b>0.020</b> (0.018-0.023)	<b>0.026</b> (0.023-0.030)	<b>0.034</b> (0.030-0.039)	<b>0.041</b> (0.035-0.046)	<b>0.050</b> (0.043-0.057)	<b>0.057</b> (0.049-0.065)	<b>0.065</b> (0.056-0.075)	<b>0.074</b> (0.062-0.085)	<b>0.086</b> (0.071-0.098)	<b>0.095</b> (0.078-0.110)
4-day	<b>0.016</b> (0.014-0.019)	<b>0.021</b> (0.018-0.024)	<b>0.028</b> (0.024-0.031)	<b>0.033</b> (0.029-0.037)	<b>0.041</b> (0.036-0.046)	<b>0.047</b> (0.041-0.054)	<b>0.054</b> (0.046-0.061)	<b>0.061</b> (0.052-0.070)	<b>0.071</b> (0.060-0.082)	<b>0.080</b> (0.066-0.092)
7-day	<b>0.010</b> (0.009-0.012)	<b>0.013</b> (0.012-0.015)	<b>0.018</b> (0.016-0.020)	<b>0.021</b> (0.019-0.024)	<b>0.026</b> (0.023-0.030)	<b>0.030</b> (0.026-0.035)	<b>0.035</b> (0.030-0.040)	<b>0.040</b> (0.033-0.045)	<b>0.046</b> (0.039-0.053)	<b>0.052</b> (0.043-0.060)
10-day	<b>0.008</b> (0.007-0.009)	<b>0.010</b> (0.009-0.012)	<b>0.013</b> (0.012-0.015)	<b>0.016</b> (0.014-0.018)	<b>0.020</b> (0.017-0.023)	<b>0.023</b> (0.020-0.026)	<b>0.026</b> (0.022-0.030)	<b>0.030</b> (0.025-0.034)	<b>0.035</b> (0.029-0.040)	<b>0.039</b> (0.032-0.044)
20-day	<b>0.005</b> (0.004-0.006)	<b>0.006</b> (0.006-0.007)	<b>0.008</b> (0.007-0.010)	<b>0.010</b> (0.009-0.011)	<b>0.012</b> (0.011-0.014)	<b>0.014</b> (0.012-0.016)	<b>0.015</b> (0.013-0.018)	<b>0.017</b> (0.015-0.020)	<b>0.019</b> (0.017-0.022)	<b>0.021</b> (0.018-0.024)
30-day	<b>0.004</b> (0.003-0.004)	<b>0.005</b> (0.004-0.006)	<b>0.007</b> (0.006-0.007)	<b>0.008</b> (0.007-0.009)	<b>0.009</b> (0.008-0.011)	<b>0.011</b> (0.009-0.012)	<b>0.012</b> (0.010-0.014)	<b>0.013</b> (0.011-0.015)	<b>0.015</b> (0.013-0.017)	<b>0.017</b> (0.014-0.019)
45-day	<b>0.003</b> (0.003-0.003)	<b>0.004</b> (0.003-0.004)	<b>0.005</b> (0.005-0.006)	<b>0.006</b> (0.005-0.007)	<b>0.007</b> (0.006-0.008)	<b>0.008</b> (0.007-0.009)	<b>0.009</b> (0.008-0.010)	<b>0.010</b> (0.009-0.012)	<b>0.011</b> (0.010-0.013)	<b>0.012</b> (0.011-0.014)
60-day	<b>0.002</b> (0.002-0.003)	<b>0.003</b> (0.003-0.004)	<b>0.004</b> (0.004-0.005)	<b>0.005</b> (0.004-0.006)	<b>0.006</b> (0.005-0.007)	<b>0.007</b> (0.006-0.008)	<b>0.007</b> (0.007-0.008)	<b>0.008</b> (0.007-0.009)	<b>0.009</b> (0.008-0.010)	<b>0.010</b> (0.008-0.011)

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

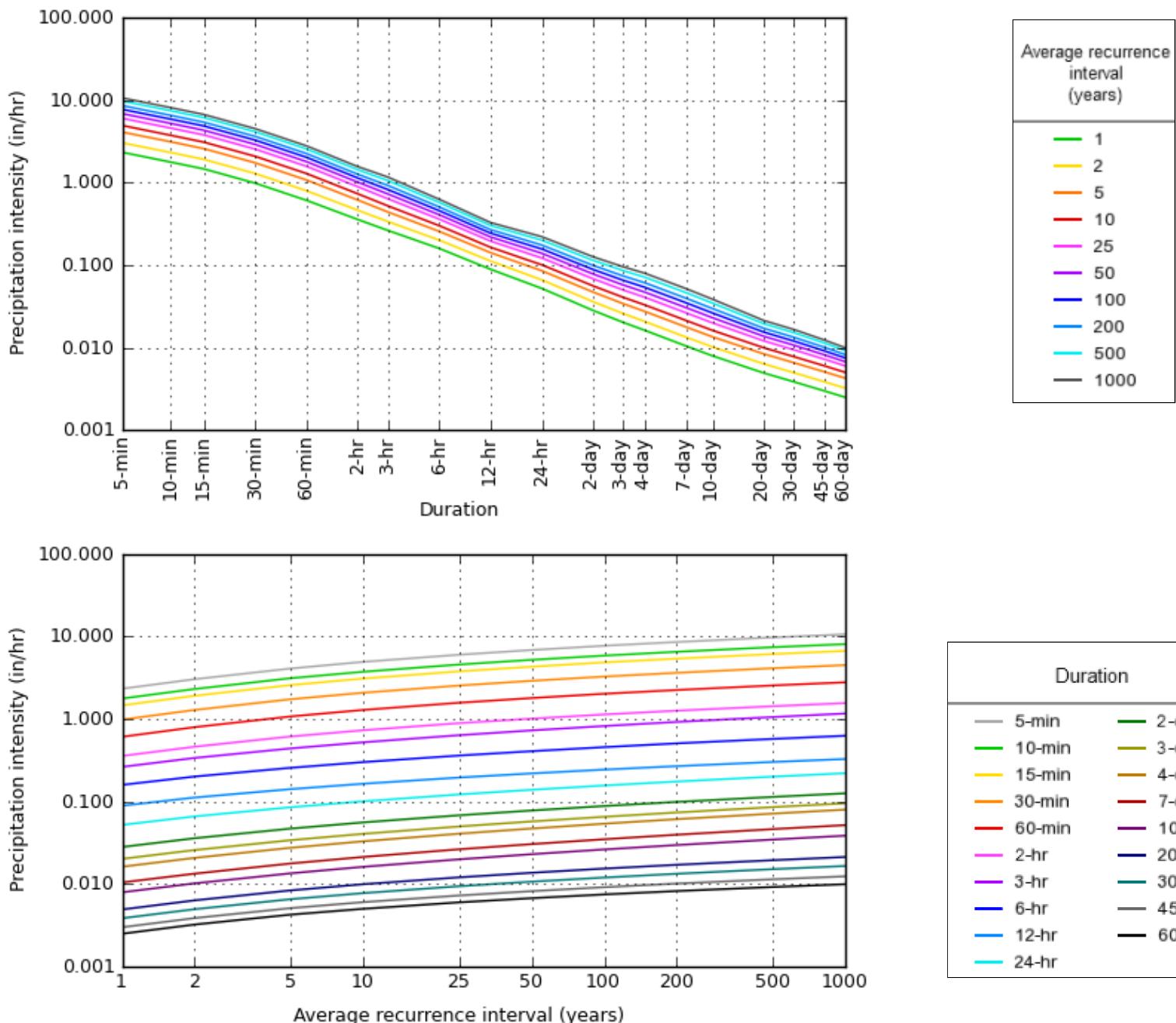
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

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### PF graphical

PDS-based intensity-duration-frequency (IDF) curves  
 Latitude: 33.6220°, Longitude: -111.8880°



NOAA Atlas 14, Volume 1, Version 5

Created (GMT): Mon Aug 17 20:40:19 2020

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## Maps & aerials

[Small scale terrain](#)



**Large scale terrain**



**Large scale map**



**Large scale aerial**

## *APPENDIX II*

### *Calculations*

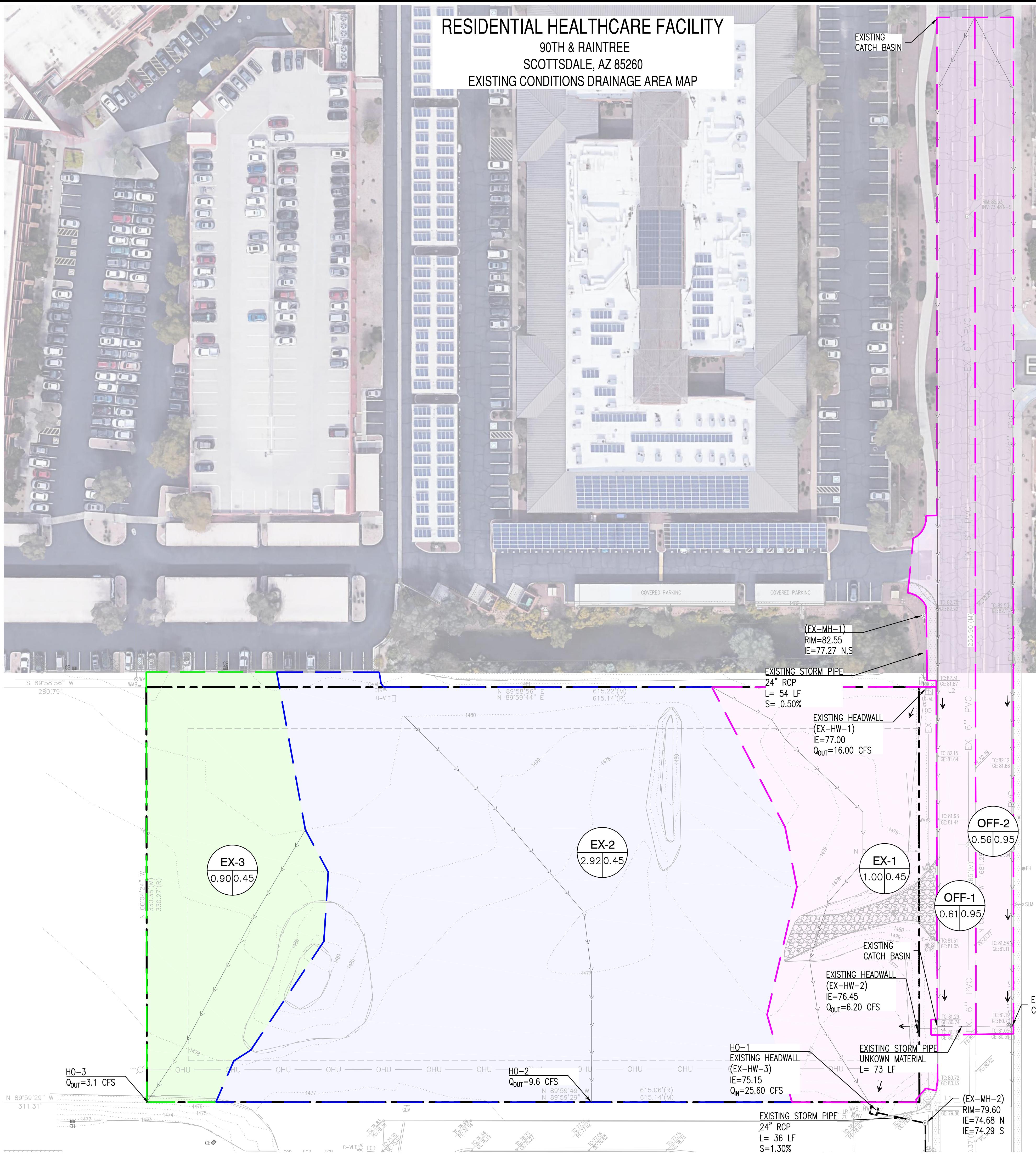
*8280 E. Gelding Dr., Suite 101  
Scottsdale, AZ 85260*

Sustainability Engineering Group

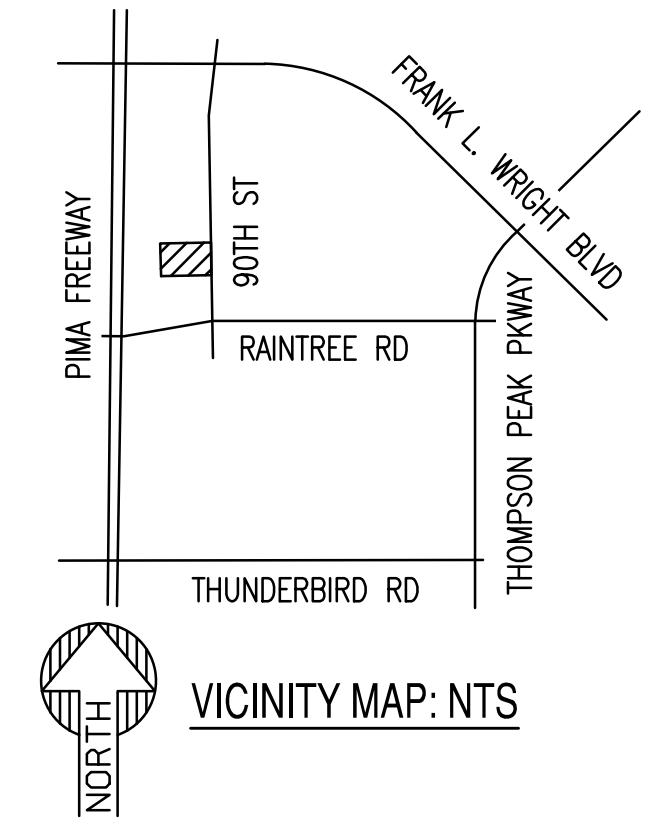
[info@azSEG.com](mailto:info@azSEG.com) 480.588.7226 [www.azSEG.com](http://www.azSEG.com)

APPENDIX

4-DR-2021  
2/8/2021



NOTE: STORM DRAIN MANHOLE RIM AND  
INVERTS OBTAINED FROM C.O.S. QS #34-49  
AND SCOTTSDALE CORPORATE CENTER PHASE II  
GRADING PLAN #36286

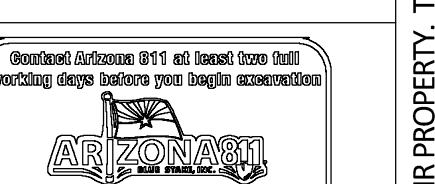


**SUSTAINABILITY ENGINEERING GROUP**



820 E. GELDING DRIVE SUITE 101 SCOTTSDALE, ARIZONA 85260  
WWW.AZSEG.COM TEL: 480.388.7226 FAX: 480.259.3534

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PROJECT		LOCATION	
RESIDENTIAL HEALTH CARE FACILITY		N 90TH ST. & RAINtree CIRCLE DR. SCOTTSDALE, ARIZONA 85260	
DRAWN	RM	01/28/2021	
DESIGNED	RM	01/28/2021	
QC			
QA			
PROJ. MGR.	AF	01/28/2021	
DATE:			
ISSUED FOR:	DRB		
REVISION NO.:			
JOB NO.:	200626		
SHEET TITLE:			
EXISTING CONDITIONS DRAINAGE AREA MAP			
PAGE NO.:			
SHEET NO.:			

ID	Sub Basin Data					Sub Basin Hydrology Summary						
	Area (acres)	Length (ft)	USGE	DSGE	Slope (ft/mi)	Kb	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
<b>Major Basin ID: 01</b>												
OFF-1	0.6	798	0.00	0.00	21.0	0.042	Q (cfs) C	1.0 0.95	1.4 0.95	1.8 0.95	2.3 0.95	2.7 0.95
							CA (ac)	0.53	0.53	0.53	0.53	0.53
							Volume (ac-ft)	0.0285	0.0348	0.0410	0.0478	0.0526
							Tc (min)	16	14	12	11	10
							i (in/hr)	1.86	2.70	3.38	4.32	5.07
OFF-2	0.6	798	0.00	0.00	21.0	0.042	Q (cfs) C	1.0 0.95	1.4 0.95	1.8 0.95	2.3 0.95	2.7 0.95
							CA (ac)	0.53	0.53	0.53	0.53	0.53
							Volume (ac-ft)	0.0285	0.0348	0.0410	0.0478	0.0526
							Tc (min)	16	14	12	11	10
							i (in/hr)	1.86	2.70	3.38	4.32	5.07
EX-1	1.0	334	0.00	0.00	29.2	0.040	Q (cfs) C	1.0 0.37	1.4 0.37	1.7 0.37	2.1 0.37	2.8 0.42
							CA (ac)	0.37	0.37	0.37	0.37	0.45
							Volume (ac-ft)	0.0143	0.0175	0.0197	0.0220	0.0278
							Tc (min)	8	7	6	6	5
							i (in/hr)	2.57	3.68	4.54	5.74	6.67
EX-2	2.9	490	1,480.00	1,477.00	32.3	0.037	Q (cfs) C	2.6 0.37	3.7 0.37	4.6 0.37	5.9 0.37	7.8 0.42
							CA (ac)	1.08	1.08	1.08	1.08	0.45
							Volume (ac-ft)	0.0435	0.0537	0.0617	0.0716	0.0889
							Tc (min)	9	8	7	7	6
							i (in/hr)	2.40	3.46	4.30	5.47	6.38
EX-3	0.9	344	1,481.00	1,478.00	46.0	0.040	Q (cfs) C	0.9 0.37	1.3 0.37	1.6 0.37	2.0 0.37	2.6 0.42
												0.45

\* Non default value

SEG  
 Drainage Design Management System  
**SUB BASINS**  
**Project Reference: GREYSTAR OFFSITE**

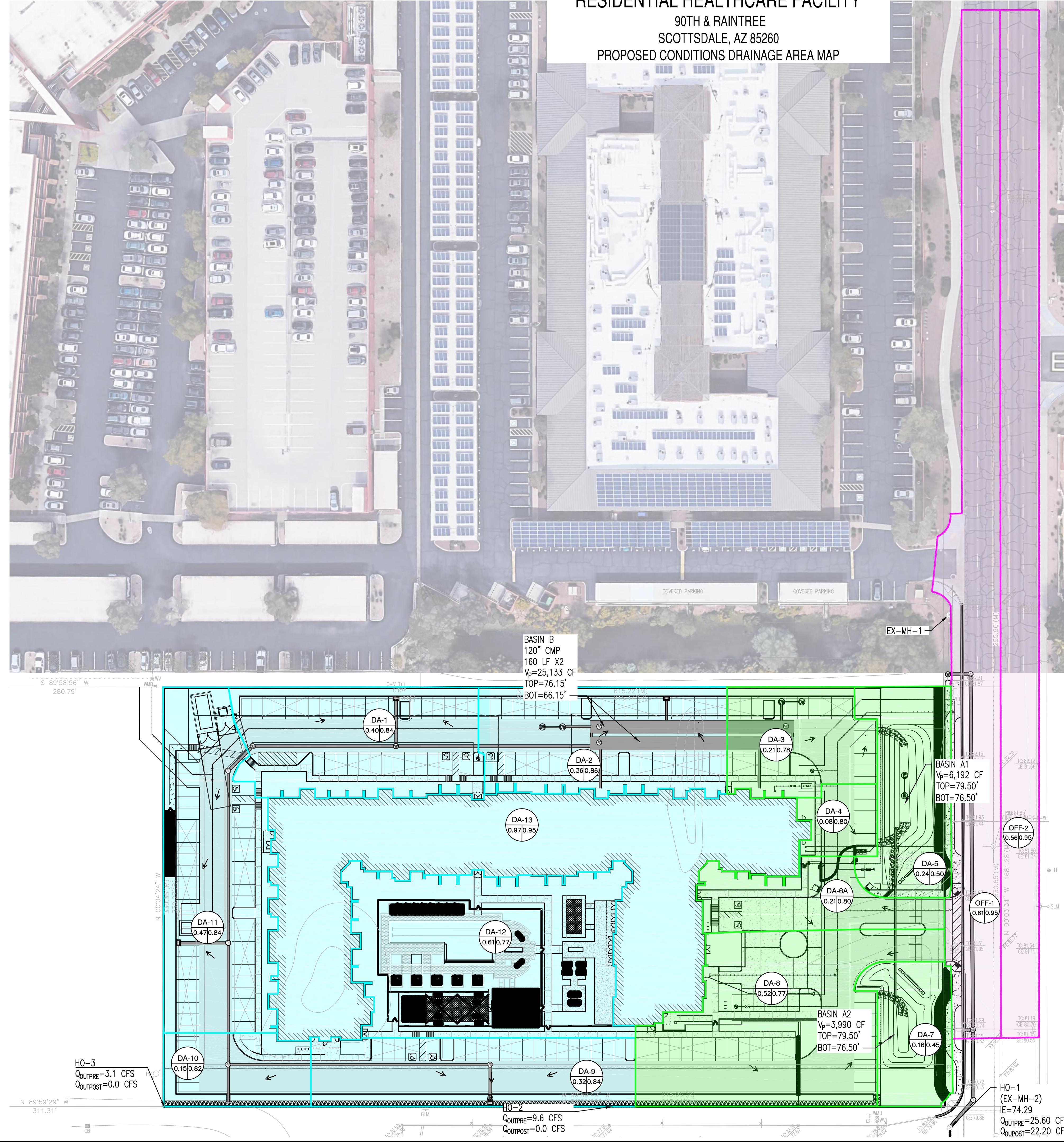
9/23/2020

Page 2

ID	Sub Basin Data				Sub Basin Hydrology Summary							
	Area (acres)	Length (ft)	USGE	DSGE	Slope (ft/mi)	Kb	2 Year	5 Year	10 Year	25 Year	50 Year	100 Year
<b>Major Basin ID: 01</b>												
							CA (ac) 0.0113	0.33 0.0141	0.33 0.0159	0.33 0.0184	0.38 0.0239	0.41 0.0285
							Tc (min) 7	6	5	5	5	5
							i (in/hr) 2.72	3.86	4.77	5.96	6.82	7.68

\* Non default value

(stSubBasRat.rpt)



Weighted Runoff Coefficient-Calculations (Cw)				
EXISTING OVERALL SITE C <sub>w</sub>				
	BUILDING or CONCRETE/ PAVEMENT	DESERT LANDSCAPE	TOTAL AREA	Cwt
C-VALUE	0.95	0.45		
AREA (ac)	0.00	4.82	<b>4.82</b>	<b>0.45</b>
EX-1	0.00	1.00	1.00	0.45
EX-2	0.00	2.92	2.92	0.45
EX-3	0.00	0.90	0.90	0.45
<b>OFFSITE</b>				
	1.17	0.00	<b>1.17</b>	0.95
OFF-1	0.61	0.00	0.61	0.95
OFF-2	0.56	0.00	0.56	0.95

Weighted Runoff Coefficient Calculations (Cw)				
PROPOSED OVERALL SITE C <sub>w</sub>				
	BUILDING or CONCRETE/ PAVEMENT	DESERT LANDSCAPE	TOTAL AREA	Cwt
C-VALUE	0.95	0.45		
AREA (ac)	3.49	1.21	<b>4.70</b>	<b>0.82</b>
DA-1	0.31	0.09	0.40	0.84
DA-2	0.28	0.08	0.36	0.84
DA-3	0.17	0.04	0.21	0.85
DA-4	0.07	0.01	0.08	0.88
DA-5	0.00	0.24	0.24	0.45
DA-6	0.18	0.03	0.21	0.87
DA-7	0.00	0.16	0.16	0.45
DA-8	0.41	0.12	0.52	0.84
DA-9	0.25	0.07	0.32	0.84
DA-10	0.11	0.04	0.15	0.82
DA-11	0.36	0.11	0.47	0.84
DA-12	0.39	0.22	0.61	0.77
DA-13	0.97	0.00	0.97	0.95

<b>OFFSITE</b>				
	1.23	0.00	<b>1.23</b>	0.95
OFF-1	0.67	0.00	0.67	0.95
OFF-2	0.56	0.00	0.56	0.95

### Required Storage Volume Calculations

<b>Rational &amp; Proposed Required Storage Volume Calculations</b>							
							$V_r = 1 * (P/12) * C_w * A$ P=100-yr, 2-hr=2.27 in.
Drainage	Area	C <sub>w</sub>	intensity	Precipitation	Q	Volume Req.	Volume Req.
Area ID	(acres)	(-)	(in/hr)	(in)	(cfs)	(acre-ft)	(CF)
<b>BASIN A1</b>							
DA-3	0.21	0.85	7.72	2.27	1.40	0.03	1494.14
DA-4	0.08	0.88	7.72	2.27	0.51	0.01	549.10
DA-5	0.24	0.45	7.72	2.27	0.84	0.02	899.27
DA-6	0.21	0.87	7.72	2.27	1.41	0.03	1500.87
<b>BASIN A2</b>							
DA-7	0.16	0.45	7.72	2.27	0.54	0.01	581.12
DA-8	0.52	0.84	7.72	2.27	3.38	0.08	3612.92
<b>BASIN B</b>							
DA-1	0.40	0.84	7.72	2.27	2.59	0.06	2768.67
DA-2	0.36	0.84	7.72	2.27	2.31	0.06	2461.45
DA-9	0.32	0.84	7.72	2.27	2.05	0.05	2192.70
DA-10	0.15	0.82	7.72	2.27	0.96	0.02	1020.70
DA-11	0.47	0.84	7.72	2.27	3.04	0.07	3246.11
DA-12	0.61	0.77	7.72	2.27	3.63	0.09	3877.77
DA-13	0.97	0.95	7.72	2.27	7.11	0.17	7592.22
<b>Totals:</b>	<b>4.70</b>	<b>0.82</b>			<b>29.79</b>	<b>0.73</b>	<b>31,797.05</b>

### Provided Storage Calculations

<b>BASIN A1</b>					
ELEV.	AREA	DEPTH	AVG V	SUM V	COMMENT
(FT)	(SF)	(FT)	(CF)	(CF)	
76.5	519			0.00	Bottom
		1.00	970.57		
77.5	1,422			970.57	
		1.00	1,976.22		
78.5	2,530			2,946.79	
		1.00	3,244.89		
79.5	3,959			6,191.68	Top

<b>BASIN A2</b>					
ELEV.	AREA	DEPTH	AVG V	SUM V	COMMENT
(FT)	(SF)	(FT)	(CF)	(CF)	
76.50	251			0.00	Bottom
		1.00	519.50		
77.50	788			519.50	
		1.00	1,232.00		
78.50	1,676			1,751.50	
		1.00	2,238.50		
79.50	2,801			3,990.00	Top

UG Storage ID	Diameter (FT)	Length (FT)	Volume (CF)
B1	10	160	12,566
B2	10	160	12,566

## Existing 24in RGRCP

---

### Project Description

---

Friction Method	Manning Formula
Solve For	Discharge

---

### Input Data

---

Roughness Coefficient	0.013
Channel Slope	0.005 ft/ft
Normal Depth	24.0 in
Diameter	24.0 in

---

### Results

---

Discharge	16.00 cfs
Flow Area	3.1 ft <sup>2</sup>
Wetted Perimeter	6.3 ft
Hydraulic Radius	6.0 in
Top Width	0.00 ft
Critical Depth	17.3 in
Percent Full	100.0 %
Critical Slope	0.007 ft/ft
Velocity	5.09 ft/s
Velocity Head	0.40 ft
Specific Energy	2.40 ft
Froude Number	(N/A)
Maximum Discharge	17.21 cfs
Discharge Full	16.00 cfs
Slope Full	0.005 ft/ft
Flow Type	Supercritical

---

### GVF Input Data

---

Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0

---

### GVF Output Data

---

Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.0 %
Normal Depth Over Rise	50.0 %
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	24.0 in
Critical Depth	17.3 in
Channel Slope	0.005 ft/ft
Critical Slope	0.007 ft/ft

---

100-yr Runoff Calculation Summary								
								P=100-yr, 5-min=7.72 in/hr
Drainage	Area	C <sub>w</sub>	Intensity	Q	Qtotal	Structure	Structure	Capacity
Area ID	(acres)	(-)	(in/hr)	(cfs)	(cfs)	ID	Type	(cfs)
DA-1	0.40	0.84	7.72	2.59	2.59	CB-2	MAG 535	4.95
DA-2	0.36	0.836531	7.72	2.31	2.31	CB-1	MAG 535	4.95
DA-3	0.21	0.85	7.72	1.40	1.40	CO-1	Curb opening	-
DA-4	0.08	0.88	7.72	0.51	0.51	CO-2	Curb opening	-
DA-5	0.24	0.45	7.72	0.84	0.84	CB-6	18" Nyloplast	1.35
DA-6	0.21	0.87	7.72	1.41	1.41	CO-3	Curb opening	-
DA-7	0.16	0.45	7.72	0.54	0.54	N/A	N/A	-
DA-8	0.52	0.84	7.72	3.38	3.38	CO-4	Curb opening	-
DA-9	0.32	0.84	7.72	2.05	5.69	CB-5	2' x 3' Nyloplast Steel Bar	6.75
DA-12	0.61	0.77	7.72	3.63				
DA-10	0.15	0.822887	7.72	0.96	0.96	CB-4	18" Nyloplast	1.35
DA-11	0.47	0.837418	7.72	3.04	3.04	CB-3	MAG 535	4.95
DA-13	0.97	0.95	7.72	7.11	7.11	R-1	Roof drain	-

## 10-yr Runoff Calculation Summary

P=10-yr, 5-min=4.92 in/hr

Drainage	Area	C <sub>w</sub>	Intensity	Q	Qtotal	Structure	Structure
Area ID	(acres)	(-)	(in/hr)	(cfs)	(cfs)	ID	Type
DA-1	0.40	0.84	4.92	1.65	1.65	CB-2	MAG 535
DA-2	0.36	0.836531	4.92	1.47	1.47	CB-1	MAG 535
DA-3	0.21	0.85065	4.92	0.89	0.89	CO-1	Curb opening
DA-4	0.08	0.882224	4.92	0.33	0.33	CO-2	Curb opening
DA-5	0.24	0.45	4.92	0.54	0.54	CB-6	18" Nyloplast
DA-6	0.21	0.871283	4.92	0.90	0.90	CO-3	Curb opening
DA-7	0.16	0.45	4.92	0.35	0.35	N/A	N/A
DA-8	0.52	0.838347	4.92	2.16	2.16	CO-4	Curb opening
DA-9	0.32	0.840123	4.92	1.31	3.62	CB-5	2' x 3' Nyloplast Steel
DA-12	0.61	0.770458	4.92	2.32			
DA-10	0.15	0.822887	4.92	0.61	0.61	CB-4	18" Nyloplast
DA-11	0.47	0.837418	4.92	1.94	1.94	CB-3	MAG 535
DA-13	0.97	0.95	4.92	4.53	4.53	R-1	Roof drain

# Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Jan 28 2021

## CB-1 100 YR

### Grate Inlet

Location	= Sag
Curb Length (ft)	= -0-
Throat Height (in)	= -0-
Grate Area (sqft)	= 3.46
Grate Width (ft)	= 2.50
Grate Length (ft)	= 3.48

### Calculations

Compute by:	Known Q
Q (cfs)	= 2.31

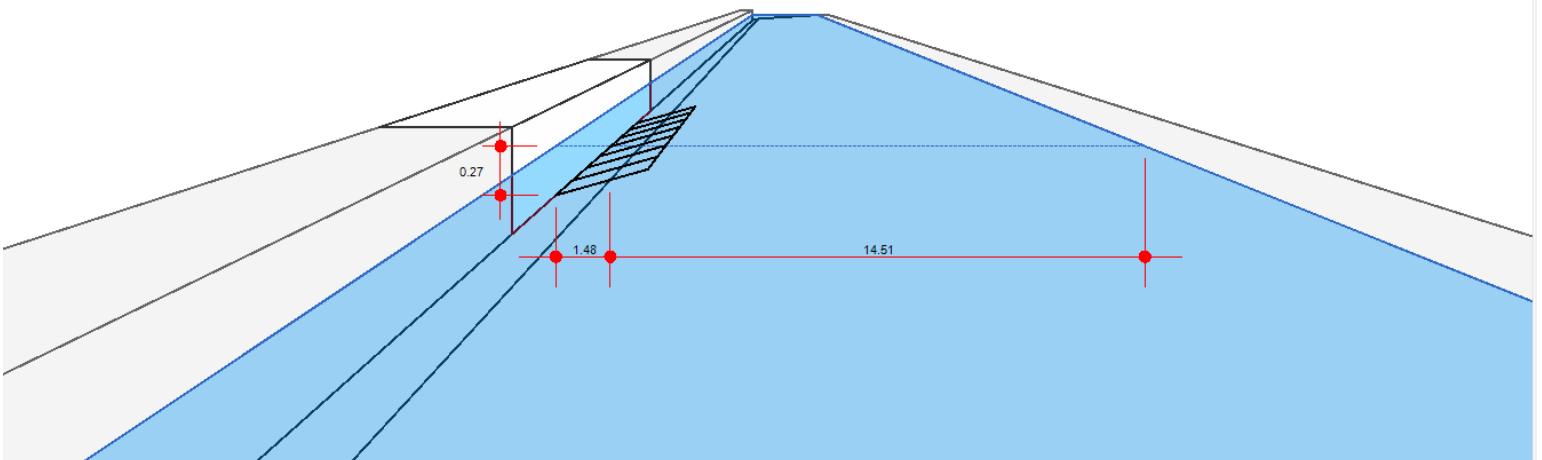
### Highlighted

Q Total (cfs)	= 2.31
Q Capt (cfs)	= 2.31
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 3.29
Efficiency (%)	= 100
Gutter Spread (ft)	= 15.99
Gutter Vel (ft/s)	= -0-
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-

### Gutter

Slope, Sw (ft/ft)	= 0.058
Slope, Sx (ft/ft)	= 0.013
Local Depr (in)	= -0-
Gutter Width (ft)	= 1.48
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

All dimensions in feet



# Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Jan 28 2021

## CB-1A 100 YR

### Grate Inlet

Location	= Sag
Curb Length (ft)	= -0-
Throat Height (in)	= -0-
Grate Area (sqft)	= 3.46
Grate Width (ft)	= 2.50
Grate Length (ft)	= 3.48

### Calculations

Compute by:	Known Q
Q (cfs)	= 2.59

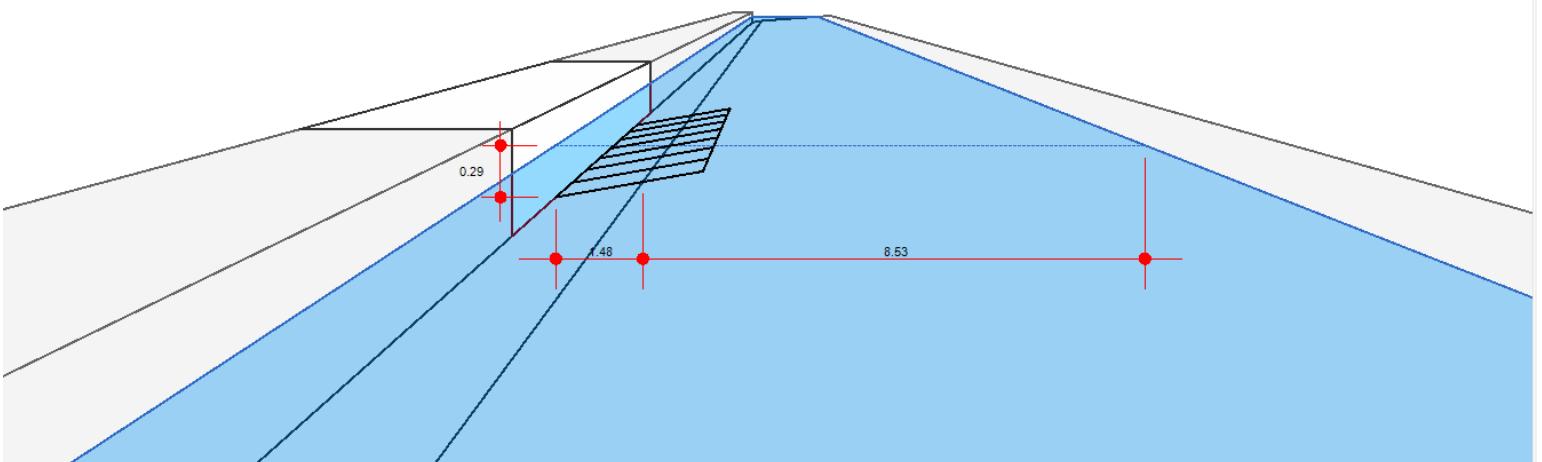
### Highlighted

Q Total (cfs)	= 2.59
Q Capt (cfs)	= 2.59
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 3.49
Efficiency (%)	= 100
Gutter Spread (ft)	= 10.01
Gutter Vel (ft/s)	= -0-
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-

### Gutter

Slope, Sw (ft/ft)	= 0.058
Slope, Sx (ft/ft)	= 0.024
Local Depr (in)	= -0-
Gutter Width (ft)	= 1.48
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

All dimensions in feet



# Inlet Report

Hydraflow Express Extension for Autodesk® Civil 3D® by Autodesk, Inc.

Thursday, Jan 28 2021

## CB-4A Capacity

### Grate Inlet

Location	= Sag
Curb Length (ft)	= -0-
Throat Height (in)	= -0-
Grate Area (sqft)	= 3.46
Grate Width (ft)	= 2.50
Grate Length (ft)	= 3.48

### Calculations

Compute by:	Known Q
Q (cfs)	= 3.04

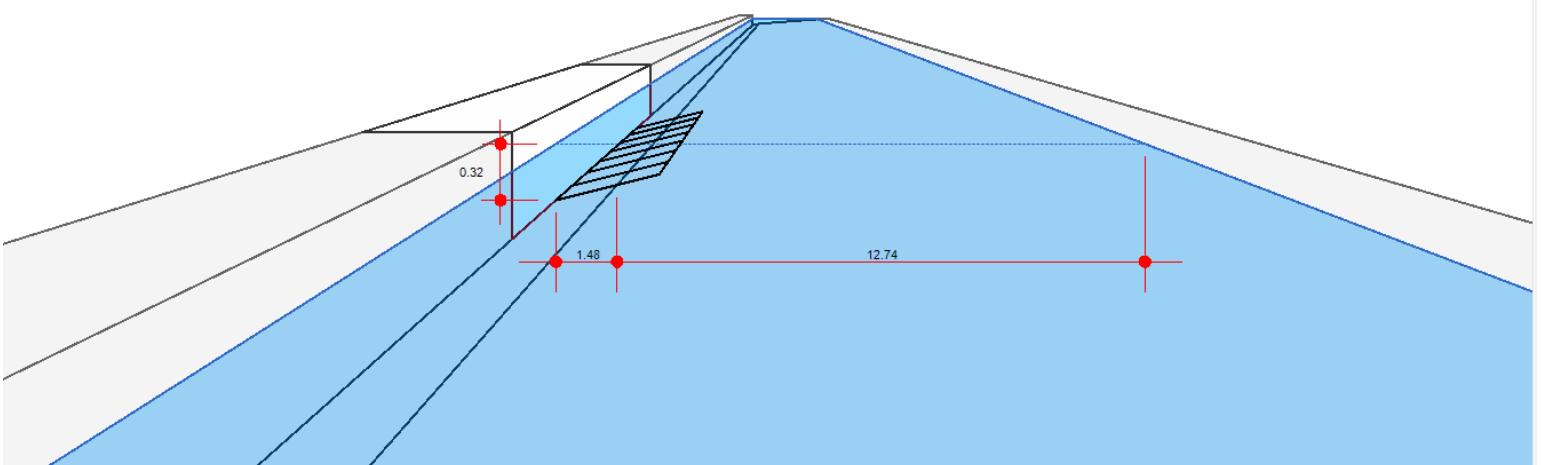
### Highlighted

Q Total (cfs)	= 3.04
Q Capt (cfs)	= 3.04
Q Bypass (cfs)	= -0-
Depth at Inlet (in)	= 3.78
Efficiency (%)	= 100
Gutter Spread (ft)	= 14.22
Gutter Vel (ft/s)	= -0-
Bypass Spread (ft)	= -0-
Bypass Depth (in)	= -0-

### Gutter

Slope, Sw (ft/ft)	= 0.058
Slope, Sx (ft/ft)	= 0.018
Local Depr (in)	= -0-
Gutter Width (ft)	= 1.48
Gutter Slope (%)	= -0-
Gutter n-value	= -0-

All dimensions in feet



## OFF-1 @ 1.80%

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.013
Channel Slope	0.018 ft/ft
Diameter	24.0 in
Discharge	16.00 cfs
Results	
Normal Depth	12.4 in
Flow Area	1.6 ft <sup>2</sup>
Wetted Perimeter	3.2 ft
Hydraulic Radius	6.1 in
Top Width	2.00 ft
Critical Depth	17.3 in
Percent Full	51.6 %
Critical Slope	0.007 ft/ft
Velocity	9.79 ft/s
Velocity Head	1.49 ft
Specific Energy	2.52 ft
Froude Number	1.909
Maximum Discharge	32.65 cfs
Discharge Full	30.35 cfs
Slope Full	0.005 ft/ft
Flow Type	Supercritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.0 %
Normal Depth Over Rise	51.6 %
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	12.4 in
Critical Depth	17.3 in
Channel Slope	0.018 ft/ft
Critical Slope	0.007 ft/ft

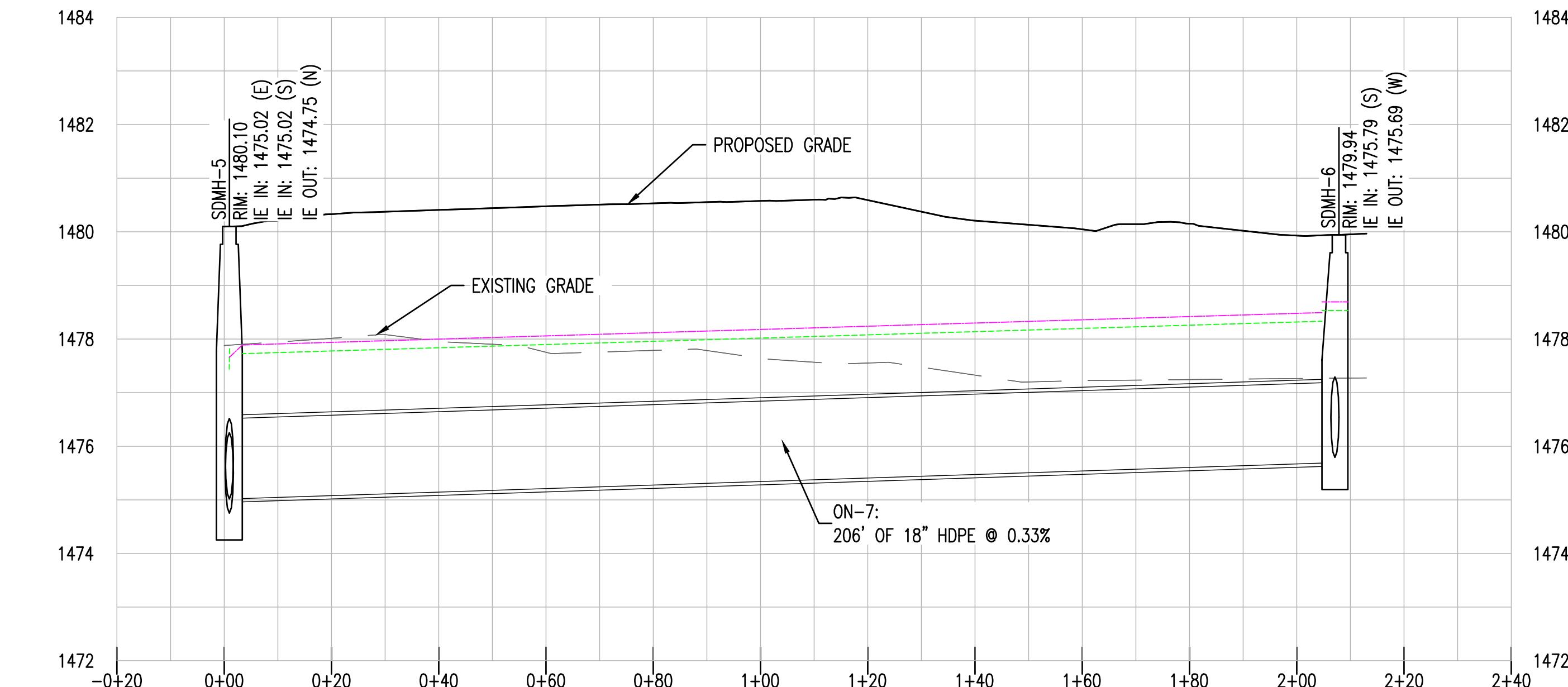
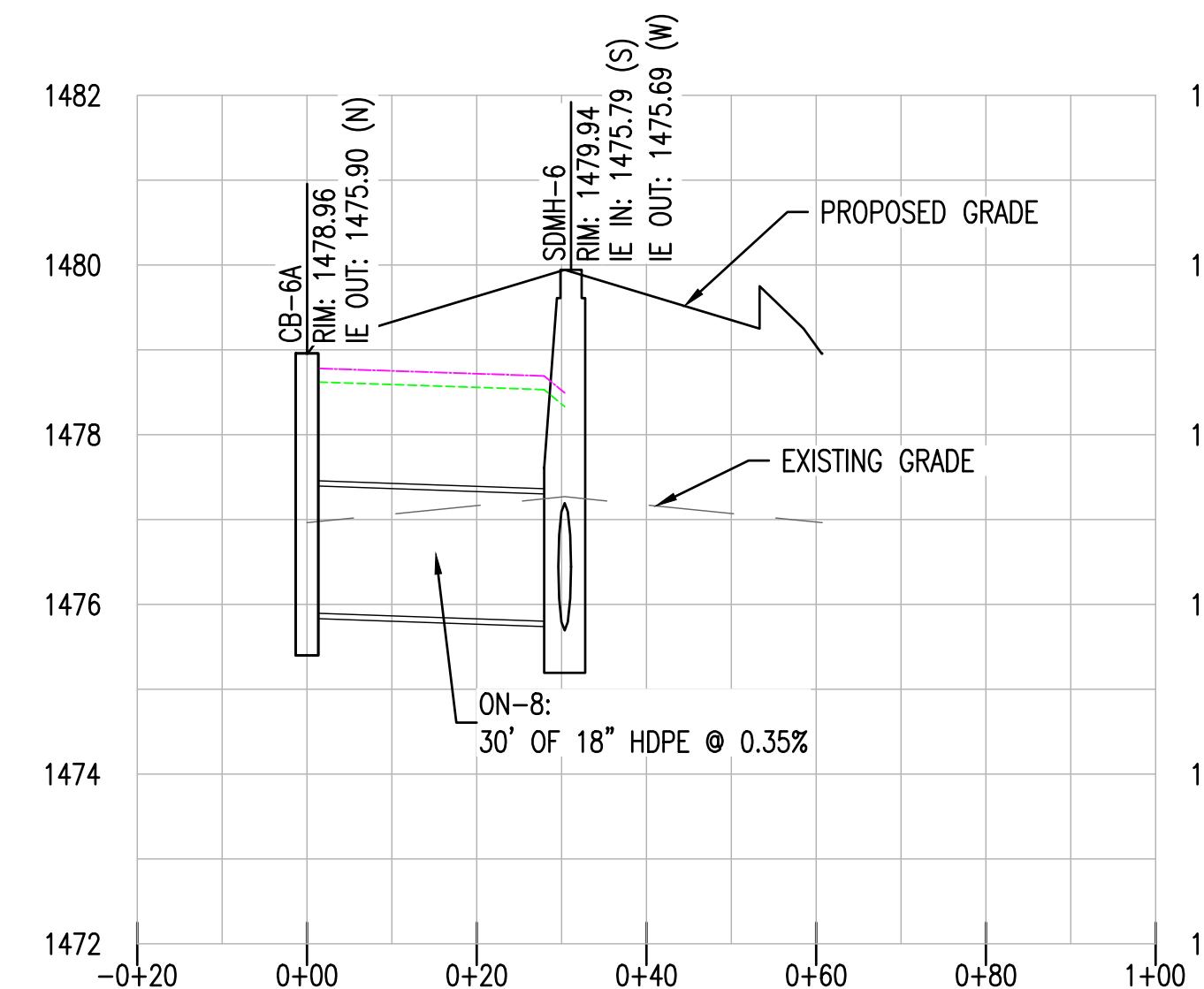
## OFF-2 @ 0.60%

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.013
Channel Slope	0.006 ft/ft
Diameter	24.0 in
Discharge	16.00 cfs
Results	
Normal Depth	18.0 in
Flow Area	2.5 ft <sup>2</sup>
Wetted Perimeter	4.2 ft
Hydraulic Radius	7.2 in
Top Width	1.73 ft
Critical Depth	17.3 in
Percent Full	75.1 %
Critical Slope	0.007 ft/ft
Velocity	6.32 ft/s
Velocity Head	0.62 ft
Specific Energy	2.12 ft
Froude Number	0.922
Maximum Discharge	18.85 cfs
Discharge Full	17.52 cfs
Slope Full	0.005 ft/ft
Flow Type	Subcritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.0 %
Normal Depth Over Rise	51.6 %
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	18.0 in
Critical Depth	17.3 in
Channel Slope	0.006 ft/ft
Critical Slope	0.007 ft/ft

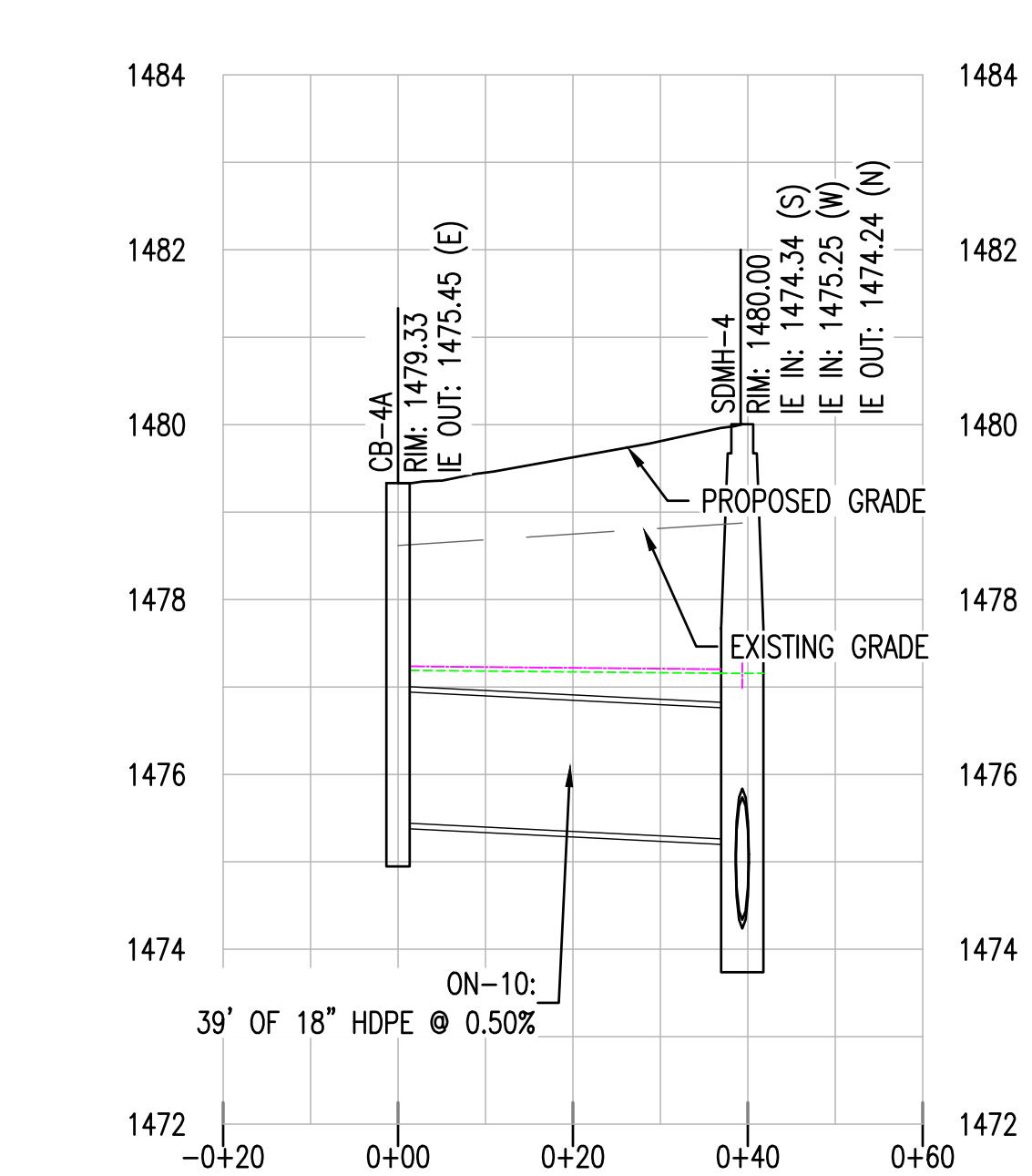
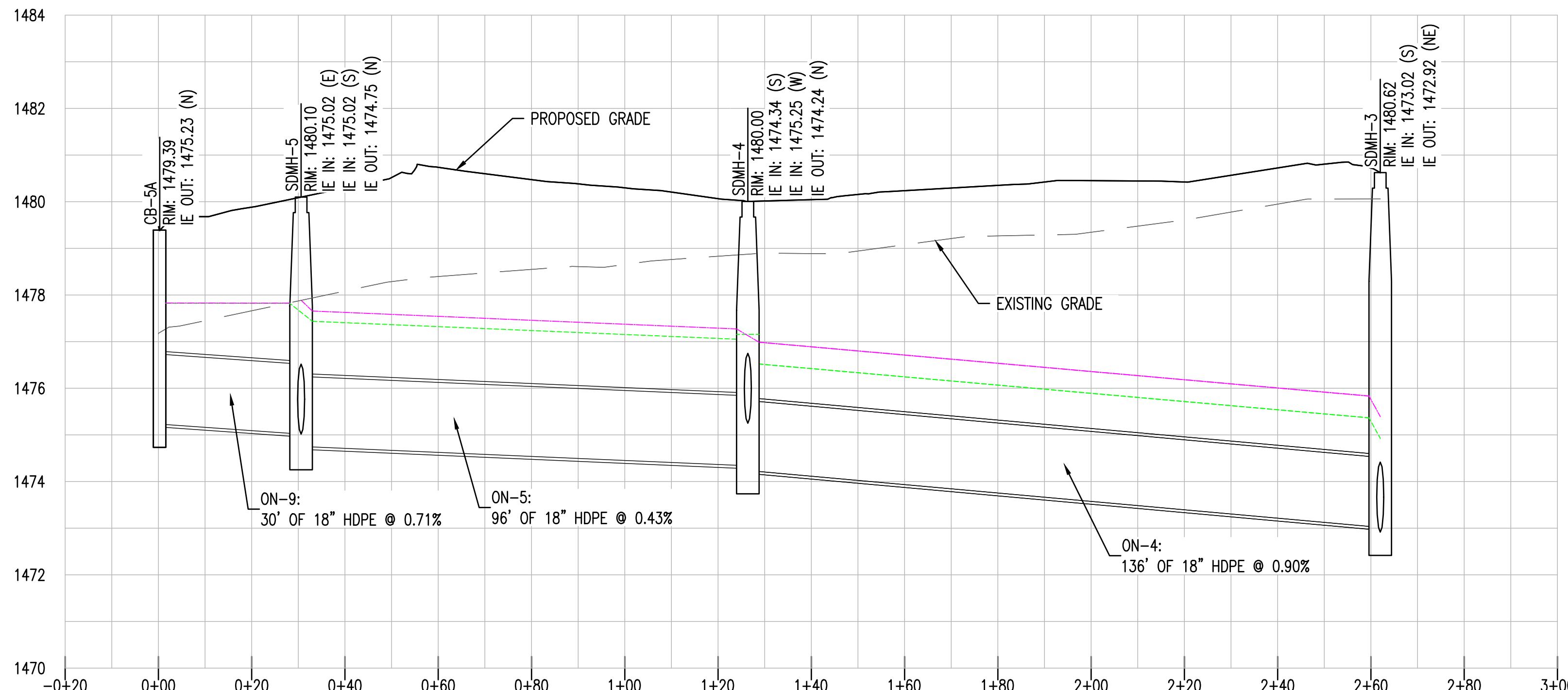
## OFF-3 @ 1.45%

Project Description	
Friction Method	Manning Formula
Solve For	Normal Depth
Input Data	
Roughness Coefficient	0.013
Channel Slope	0.015 ft/ft
Diameter	24.0 in
Discharge	22.22 cfs
Results	
Normal Depth	16.5 in
Flow Area	2.3 ft <sup>2</sup>
Wetted Perimeter	3.9 ft
Hydraulic Radius	7.1 in
Top Width	1.86 ft
Critical Depth	20.2 in
Percent Full	68.6 %
Critical Slope	0.009 ft/ft
Velocity	9.67 ft/s
Velocity Head	1.45 ft
Specific Energy	2.82 ft
Froude Number	1.531
Maximum Discharge	29.30 cfs
Discharge Full	27.24 cfs
Slope Full	0.010 ft/ft
Flow Type	Supercritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.0 %
Normal Depth Over Rise	68.6 %
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	16.5 in
Critical Depth	20.2 in
Channel Slope	0.015 ft/ft
Critical Slope	0.009 ft/ft

# ON-SITE PIPES HYDRAULIC GRADE LINE

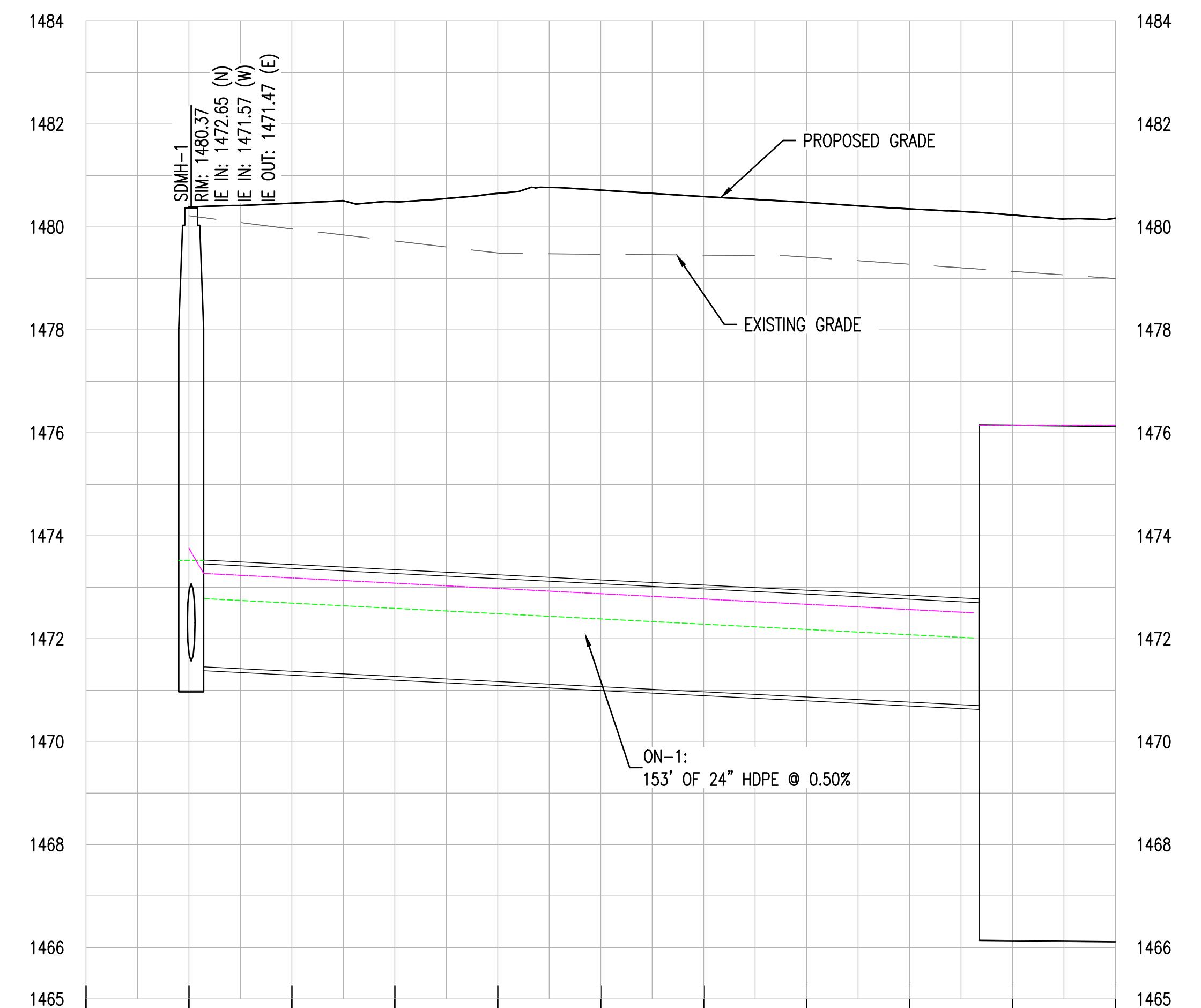
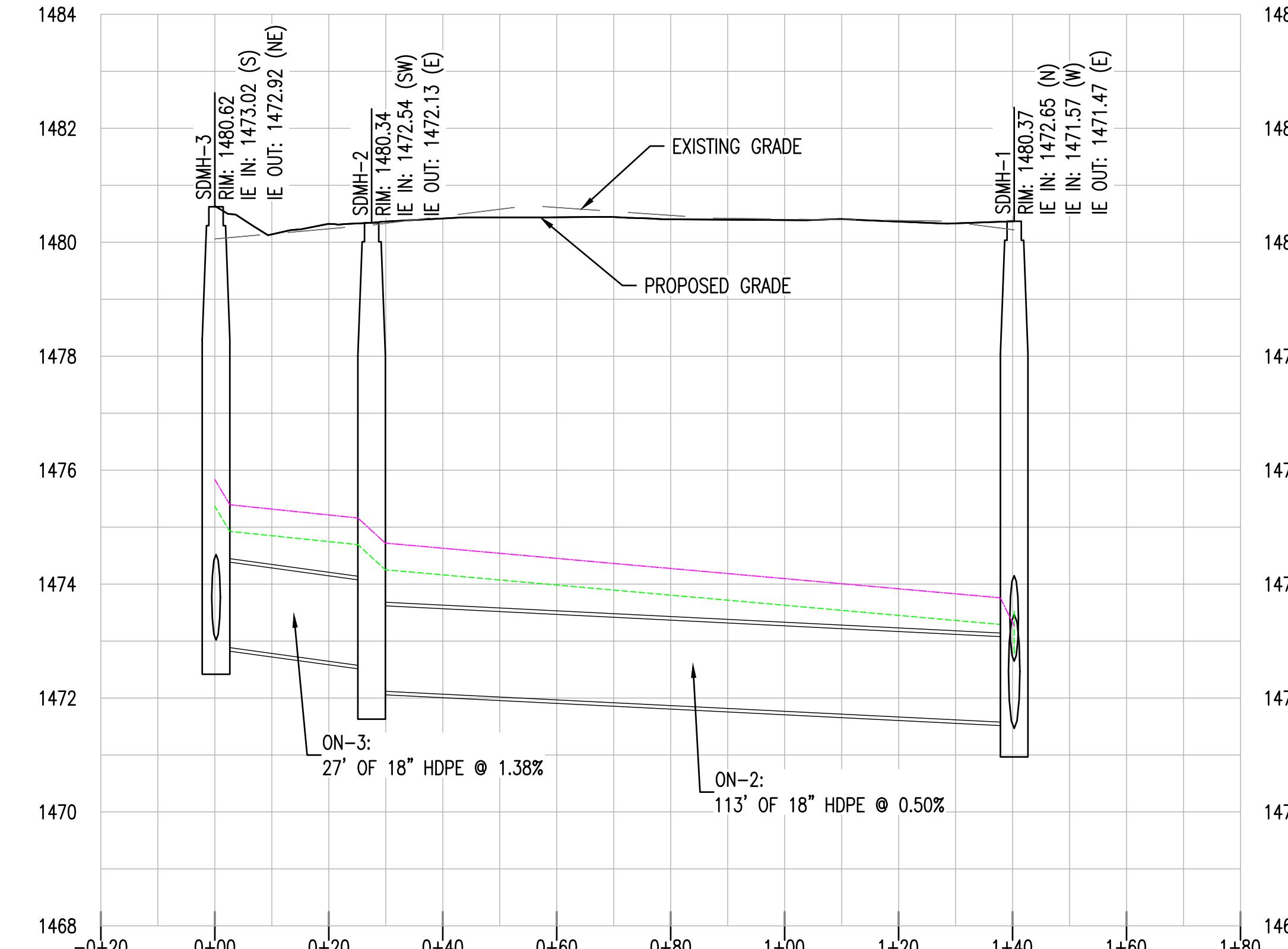


ENERGY GRADE LINE  
HYDRAULIC GRADE LINE

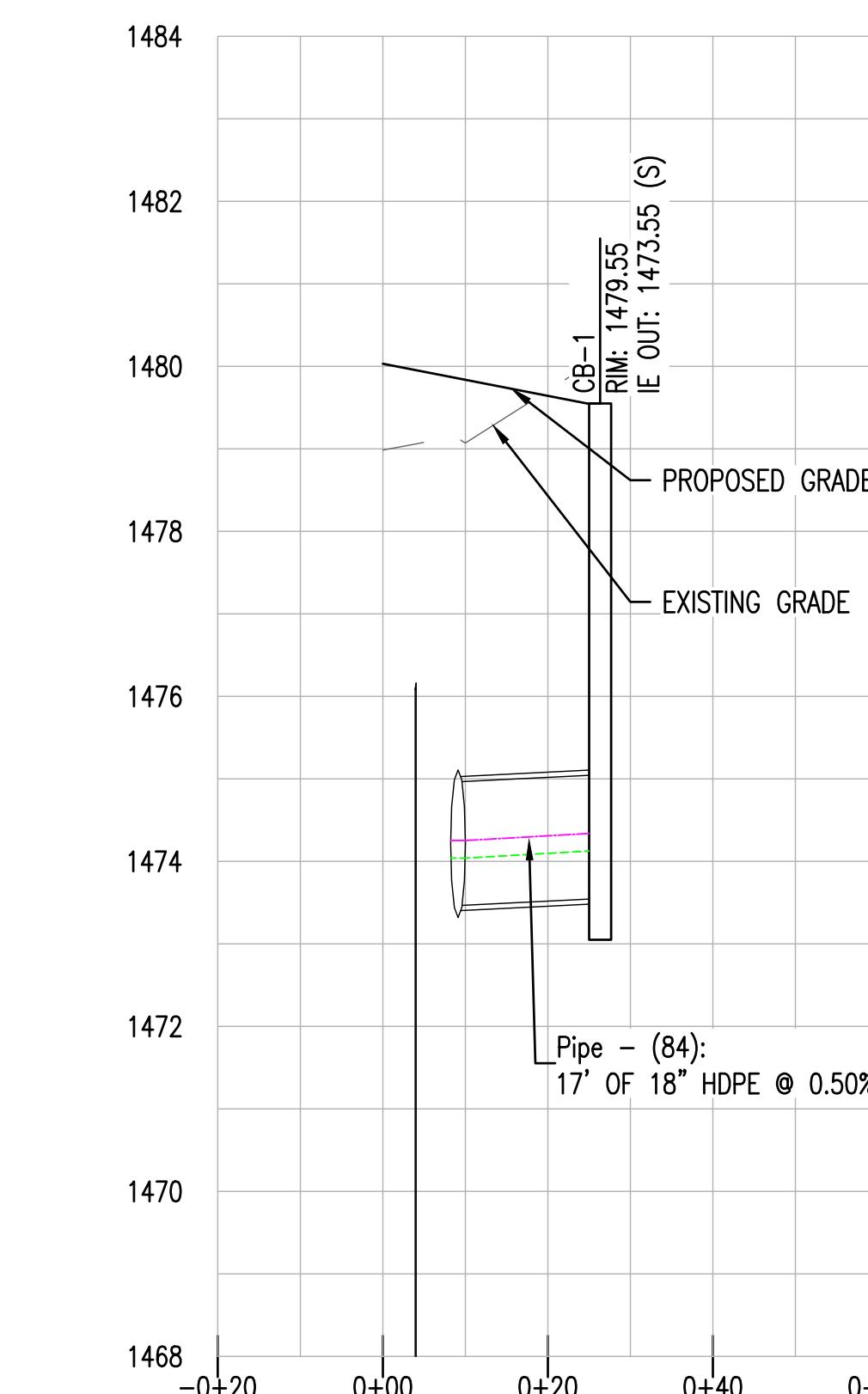
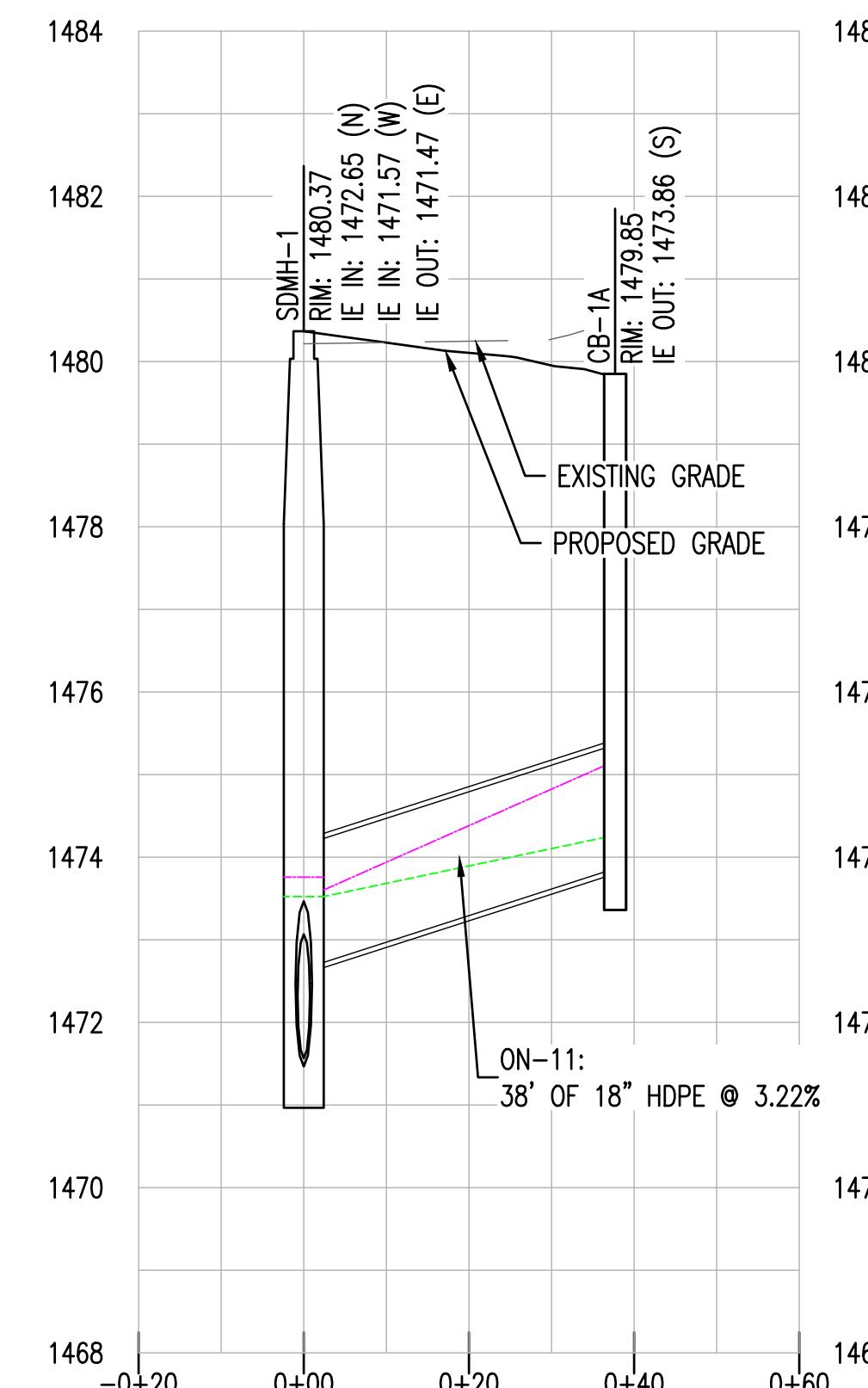


PROFILE VIEW  
HORIZONTAL SCALE: 1" = 20'  
VERTICAL SCALE: 1" = 2'

# ON-SITE PIPES HYDRAULIC GRADE LINE

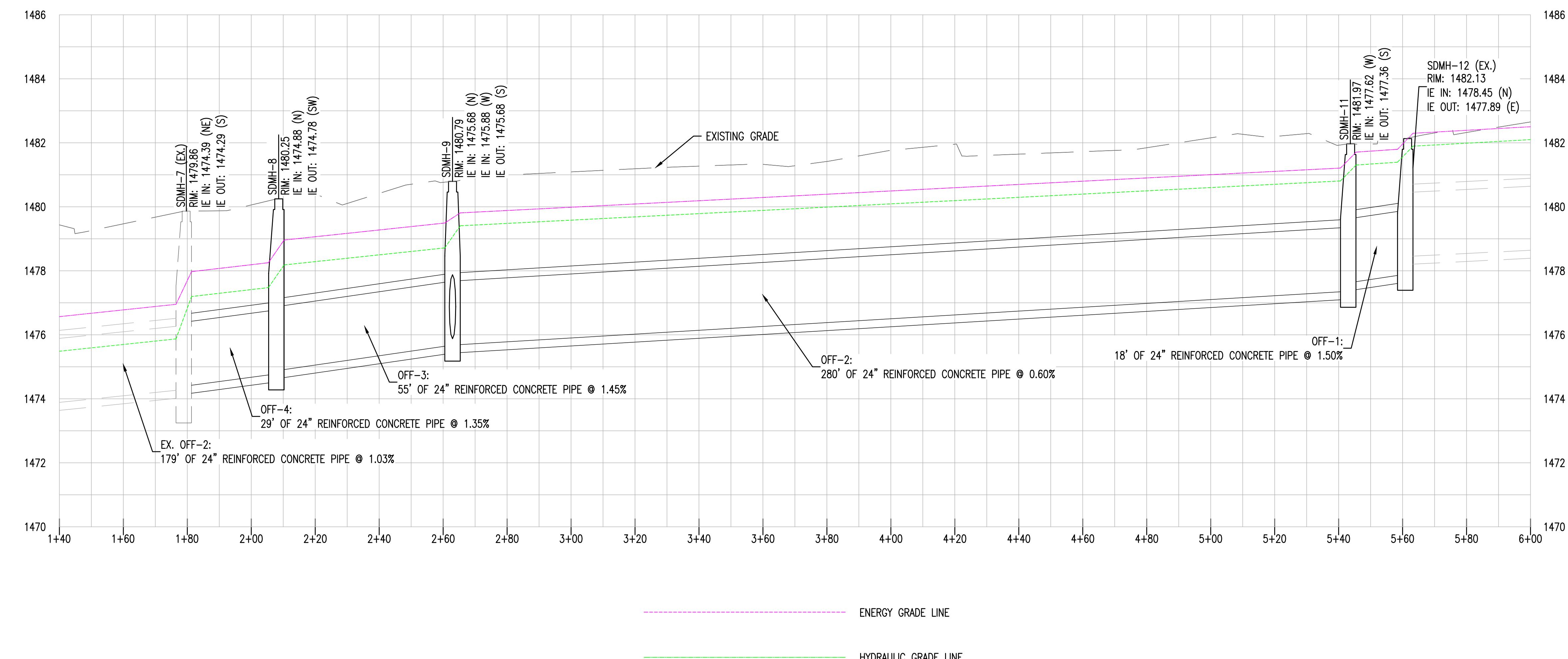


----- ENERGY GRADE LINE  
----- HYDRAULIC GRADE LINE



**PROFILE VIEW**  
HORIZONTAL SCALE: 1" = 20'  
VERTICAL SCALE: 1" = 2'

## OFFSITE PIPES HYDRAULIC GRADE LINE



PROFILE VIEW  
HORIZONTAL SCALE: 1" = 20'  
VERTICAL SCALE: 1" = 2'

### ON SITE-PIPES HYDRAULIC CALCULATIONS

#Line	Pipe	From	To	3D Length - Center to Center	Drainage Area Inc	Drainage Area Total	Runoff Coeff "C"	Area X "C" Inc	Area X "C" Total	Time of Concentration Inlet	Rain "I"	Runoff "Q"	Known Q.	Total Q	Pipe Dia.	Full Q.	Velocity Full	Velocity Design	Sec Time	Invert Elevation U/S	Invert Elevation D/S	Crown Drop	Slope	
				(ft)	(sq. ft)	(sq. ft)		(sq. ft)	(sq. ft)	(min)	(inch/hr)	(cu. ft/sec)	(cu. ft/sec)	(cu. ft/sec)	(ft)	(cu. ft/sec)	(ft/s)	(min)	(ft)	(ft)	(ft)			
1	ON-1	SDMH-1	Structure - (7)	153.129	0	0	0	0	0	0	0	0	0	12.28	2	16.012	5.097	5.614	0.455	1471.466	1470.7	N/A	0.50%	
2	ON-11	CB-1A	SDMH-1	37.718	0	0	0	0	0	0	0	0	0	2.59	2.59	1.5	18.868	10.677	7.481	0.084	1473.862	1472.648	N/A	3.22%
3	ON-2	SDMH-2	SDMH-1	112.766	0	0	0	0	0	0	0	0	0	9.69	1.5	7.435	4.207	5.483	0.343	1472.13	1471.566	N/A	0.50%	
4	ON-3	SDMH-3	SDMH-2	27.303	0	0	0	0	0	0	0	0	0	9.69	1.5	12.339	6.983	7.725	0.059	1472.917	1472.541	N/A	1.38%	
5	ON-4	SDMH-4	SDMH-3	135.625	0	0	0	0	0	0	0	0	0	9.69	1.5	9.975	5.645	6.426	0.352	1474.238	1473.017	N/A	0.90%	
6	ON-5	SDMH-5	SDMH-4	95.803	0	0	0	0	0	0	0	0	0	6.65	1.5	6.92	3.916	4.456	0.358	1474.753	1474.338	N/A	0.43%	
7	ON-7	SDMH-6	SDMH-5	206.152	0	0	0	0	0	0	0	0	0	5.69	1.5	6.021	3.407	3.872	0.887	1475.693	1475.017	N/A	0.33%	
8	ON-8	CB-6A	SDMH-6	30.36	0	0	0	0	0	0	0	0	0	5.69	5.69	1.5	6.22	3.52	3.988	0.127	1475.899	1475.793	N/A	0.35%
9	ON-9	CB-5A	SDMH-5	30.351	0	0	0	0	0	0	0	0	0	0.96	1.5	8.86	5.013	3.28	0.154	1475.232	1475.017	N/A	0.71%	
10	ON-10	CB-4A	SDMH-4	39.365	0	0	0	0	0	0	0	0	0	3.04	3.04	1.5	7.438	4.209	3.994	0.164	1475.447	1475.25	N/A	0.50%

#Line	Struct. ID	D	Q	L	V	d	dc	v^2/2g	EGLo	HGLo	Sf	Total Pipe Loss	EGLi	HGLi	Ea	EGLa	U/S TOC	Surface Elev.	Step4*	Step7*	Step14*
		(ft)	(cu. ft/sec)	(ft)	(ft/s)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)			
0	Structure - (7)								1470.7	1470.7								1472.7	1472.883		
1	SDMH-1	2	12.28	153.129	5.611	1.314	1.26	0.489	1472.504	1472.015	0.005	0.766	1473.27	1472.78	2.106	1473.572	1473.066	1480.367	N/A	Case B	Case B
2	CB-1A	1.5	2.59	37.718	7.471	0.376	0.61	0.868	1473.604	1473.524	0	0	1475.106	1474.238	1.244	1475.106	---	1479.85	N/A	Case F	N/A
3	SDMH-2	1.5	9.69	112.766	5.483	1.5	n/a	0.467	1473.759	1473.291	0.009	0.96	1474.718	1474.251	2.843	1474.973	1474.041	1480.341	Case B	N/A	Case A
4	SDMH-3	1.5	9.69	27.303	5.483	1.5	n/a	0.467	1475.16	1474.693	0.009	0.232	1475.392	1474.925	2.73	1475.647	1474.517	1480.624	Case B	N/A	Case A
5	SDMH-4	1.5	9.69	135.625	5.483	1.5	n/a	0.467	1475.834	1475.366	0.009	1.154	1476.988	1476.52	2.946	1477.184	1475.838	1480.005	Case B	N/A	Case A
6	SDMH-5	1.5	6.65	95.803	3.763	1.5	n/a	0.22	1477.272	1477.052	0.004	0.384	1477.656	1477.436	3.071	1477.824	1476.517	1480.099	Case B	N/A	Case A
7	SDMH-5	1.5	5.69	206.152	3.22	1.5	n/a	0.161	1477.888	1477.727	0.003	0.605	1478.493	1478.332	2.935	1478.628	1477.399	1479.943	Case B	N/A	Case A
8	SDMH-6	1.5	5.69	30.36	3.22	1.5	n/a	0.161	1478.692	1478.531	0.003	0.089	1478.781	1478.62	2.917	1478.817	---	1478.959	Case B	N/A	Case A
9	CB-5A	1.5	0.96	30.351	0.543	1.5	n/a	0.005	1477.825	1477.821	0	0.003	1477.828	1477.823	2.597	1477.83	---	1479.392	Case B	N/A	Case A
10	CB-4A	1.5	3.04	39.365	1.72	1.5	n/a	0.046	1477.203	1477.156	0.001	0.033	1477.235	1477.189	1.81	1477.257	---	1479.331	Case B	N/A	Case A

\*URBAN DRAINAGE DESIGN MANUAL - Hydraulic Engineering Circular No.22 Third Edition

#Line	Struct. ID	Exit Ho	Hf	Hb	Hc	He	Hj	Total	Ei	y+(P/gam ma)	Di	Eai	CB	C-theta	Cp	Ha	Ea
		(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)						(ft)	(ft)	
0	Structure - (7)																
1	SDMH-1	0	0.766	0	0	0	0	0.766	1.804	1.314	0.487	1.977	0	0.742	0	0.129	2.106
2	CB-1A	0.032	0	0	0	0	0	0	1.244	0.376	0.211	0.846	0	0	3.428	0	1.244
3	SDMH-2	0.187	0.96	0	0	0	0	0.96	2.588	2.121	0.789	2.682	0	1.723	0	0.161	2.843
4	SDMH-3	0.187	0.232	0	0	0	0	0.232	2.475	2.008	0.789	2.569	0	1.721	0	0.161	2.73
5	SDMH-4	0.187	1.154	0	0	0	0	1.154	2.75	2.282	0.789	2.843	0	1.099	0	0.103	2.946
6	SDMH-5	0.088	0.384	0	0	0	0	0.384	2.903	2.683	0.542	2.947	0	2.801	0	0.123	3.071
7	SDMH-5	0.064	0.605	0	0	0	0	0.605	2.8	2.639	0.464	2.832	0	3.181	0	0.103	2.935
8	SDMH-6	0.064	0.089	0	0	0	0	0.089	2.882	2.721	0.464	2.914	0	0	0.097	0.003	2.917
9	CB-5A	0.002	0.003	0	0	0	0	0.003	2.595	2.591	0.078	2.596	0	0	1.042	0.001	2.597
10	CB-4A	0.018	0.033	0	0	0	0	0.033	1.788	1.742	0.248	1.798	0	0	1.391	0.013	1.81

## OFFSITE PIPES HYDRAULIC CALCULATIONS

#Line	Pipe	From	To	3D Length - Center to Center	Drainage Area Inc	Drainage Area Total	Runoff Coeff "C"	Area X "C" Inc	Area X "C" Total	Time of Concentration Inlet	Time of Concentration System	Rain "I"	Runoff "Q"	Known Q	Total Q	Pipe Dia.	Full Q	Velocity Full	Velocity Design	Sec Time	Invert Elevation U/S	Invert Elevation D/S	Crown Drop	Slope	
				(ft)	(sq. ft)	(sq. ft)		(sq. ft)	(sq. ft)	(min)	(min)	(inch/hr)	(cu. ft/sec)	(cu. ft/sec)	(cu. ft/sec)	(ft)	(cu. ft/sec)	(ft/s)	(ft/s)	(min)	(ft)	(ft)	(ft)		
1	EX. OFF-2	SDMH-7	structure - (13)	178.897	0	0	0	0	0	0	0	0	0	0	22.22	2	23.028	7.33	8.342	0.357	1474.29	1472.44	N/A	1.03%	
2	OFF-4	SDMH-8	SDMH-7	28.863	0	0	0	0	0	0	0	0	0	0	22.22	2	26.271	8.362	9.372	0.051	1474.778	1474.39	N/A	1.35%	
3	OFF-3	SDMH-9	SDMH-8	55.087	0	0	0	0	0	0	0	0	0	6.22	22.22	2	27.29	8.687	9.673	0.095	1475.678	1474.878	N/A	1.45%	
4	OFF-2	SDMH-11	SDMH-9	280.082	0	0	0	0	0	0	0	0	0	0	16	2	17.542	5.584	6.324	0.738	1477.359	1475.678	N/A	0.60%	
5	OFF-1	SDMH-12	SDMH-11	17.792	0	0	0	0	0	0	0	0	0	0	16	16	2	27.902	8.882	9.178	0.032	1477.986	1477.716	N/A	1.52%

\*URBAN DRAINAGE DESIGN MANUAL - Hydraulic Engineering Circular No.22 Third Edition

#Line	Struct. ID	D	Q	L	V	d	dc	v^2/2g	EGLo	HGlo	Sf	Total Pipe Loss	EGLi	HGLi	Ea	EGLa	U/S TOC	Surface Elev.	Step4*	Step7*	Step14*
		(ft)	(cu. ft/sec)	(ft)	(ft/s)	(ft)	(ft)	(ft)	(ft)	(ft)		(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	(ft)		
0	ucture - (1)								1472.44	1472.44								1474.44	1474.815		
1	SDMH-7	2	22.22	178.897	8.339	1.582	1.683	1.081	1475.103	1474.022	0	0	1476.953	1475.872	3.373	1477.663	1476.39	1479.864	N/A	Case B	N/A
2	SDMH-8	2	22.22	28.863	7.073	2	n/a	0.778	1477.974	1477.196	0.01	0.278	1478.252	1477.475	3.872	1478.65	1476.878	1480.248	Case B	N/A	Case A
3	SDMH-9	2	22.22	55.087	7.073	2	n/a	0.778	1478.961	1478.184	0.01	0.531	1479.493	1478.715	3.97	1479.648	1477.678	1480.795	Case B	N/A	Case A
4	SDMH-11	2	16	280.082	5.093	2	n/a	0.403	1479.81	1479.406	0.005	1.401	1481.211	1480.808	4.188	1481.547	1479.716	1481.967	Case B	N/A	Case A
5	SDMH-12	2	16	17.792	5.093	2	n/a	0.403	1481.708	1481.305	0.005	0.089	1481.797	1481.394	3.892	1481.878	1480.68	1483.529	Case B	N/A	Case A

## ***APPENDIX III***

### ***Preliminary Grading and Drainage Plans***

*8280 E. Gelding Dr., Suite 101  
Scottsdale, AZ 85260*

Sustainability Engineering Group

[info@azSEG.com](mailto:info@azSEG.com) 480.588.7226 [www.azSEG.com](http://www.azSEG.com)

APPENDIX

4-DR-2021  
2/8/2021

# RESIDENTIAL HEALTHCARE FACILITY

## GRADING AND DRAINAGE PLAN KEYMAP

PROJECT ADDRESS  
90TH STREET & RAINTREE DRIVE, SCOTTSDALE, ARIZONA 85260.

PROJECT DESCRIPTION  
NEW 151-UNIT RESIDENTIAL HEALTHCARE FACILITY WITH 3 STORIES AND 4 STORIES COMPONENTS, PARKING, AND COMMON AREA.

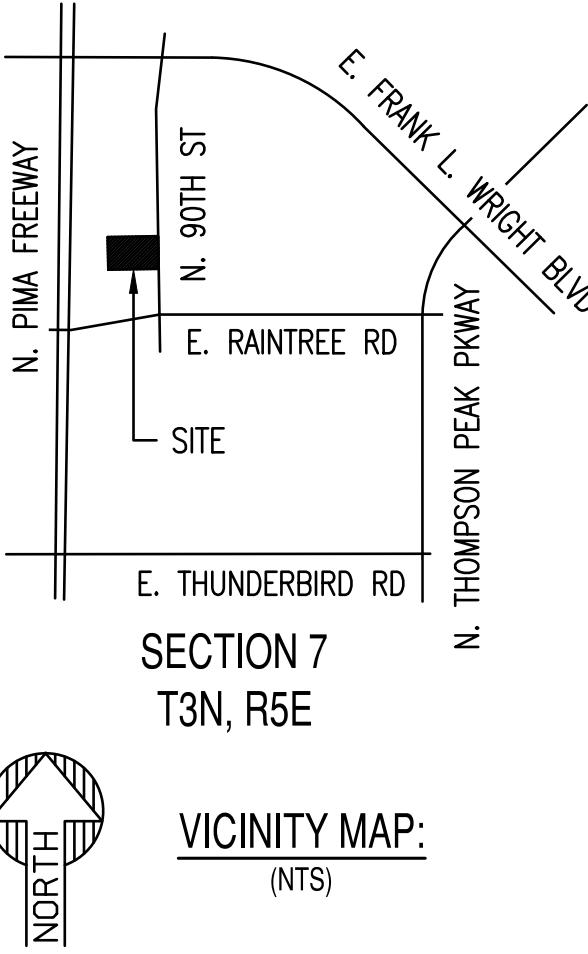
BENCHMARK:  
BENCHMARK IS A BRASS CAP FLUSH, BEING THE SOUTH QUARTER CORNER OF SECTION 7, T3N, R5E.  
ELEVATION: 1447.21' NAVD 88

PARCEL INFORMATION:  
APN: 217-15-033  
ZONING: C-0  
GROSS AREA: 217,800 SF (5.00 AC)  
NET AREA: 202,950 SF (4.66 AC)  
FLOOD ZONE: ZONE X IS DEFINED AS AREAS OF 0.2% ANNUAL FLOOD.

90TH STREET AND RAINTREE  
SCOTTSDALE, AZ 85260

ARCHITECT:  
TODD & ASSOCIATES, INC.  
4019 N.44TH ST.  
PHOENIX, AZ 85018  
PHONE: 602-952-8280  
ATTN: RUSSELL KINDER  
RKINDER@TODDASSOC.COM

CIVIL ENGINEER:  
SUSTAINABILITY ENGINEERING GROUP  
8280 E GELDING DR., SUITE 101  
SCOTTSDALE, AZ 85260  
PHONE: 480-237-2507  
ATTN: ALI FAKIH  
ALIAZSEG.COM



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GROUP

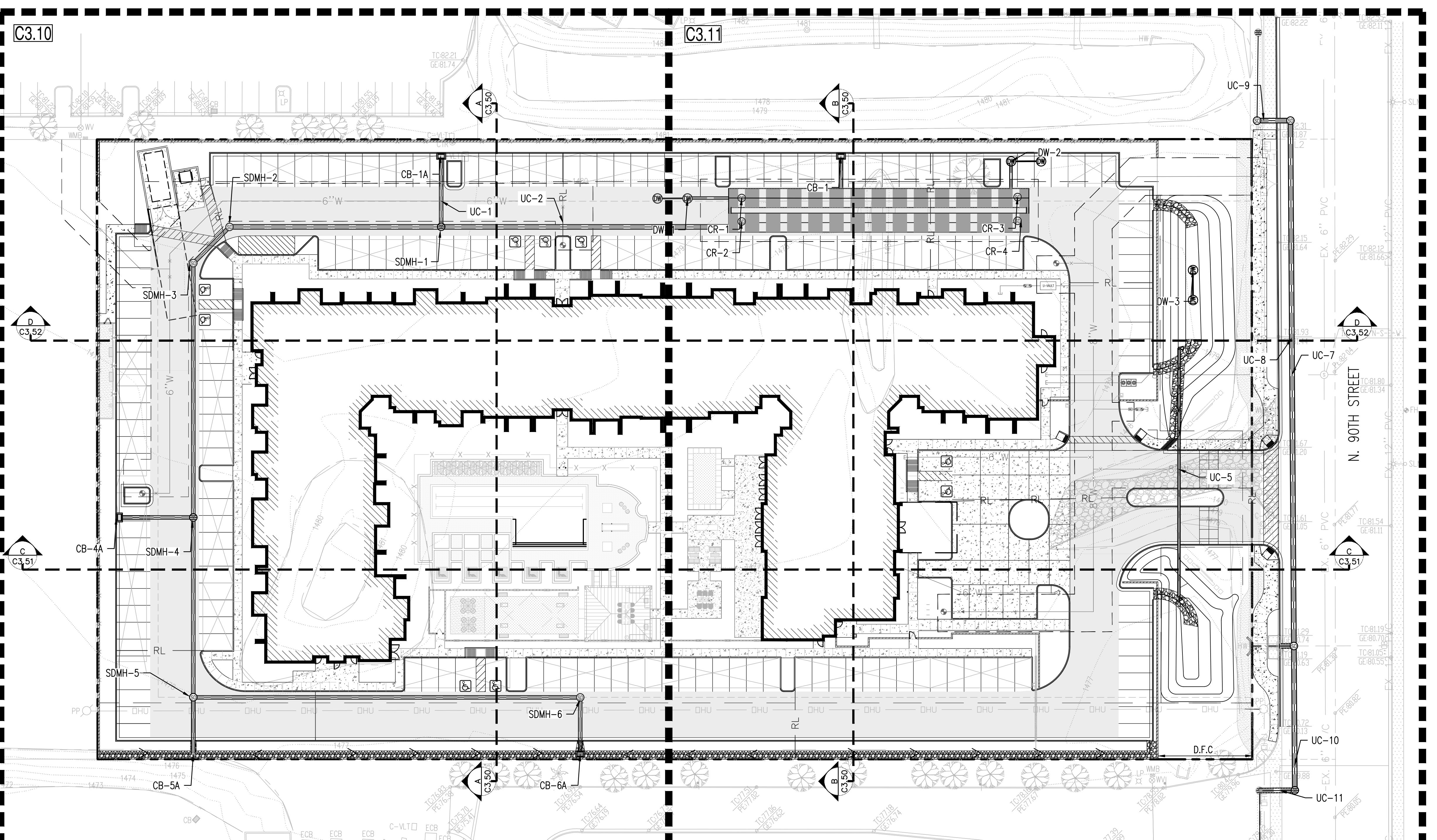
8280 E. GELDING DRIVE SUITE 101, SCOTTSDALE, ARIZONA 85260  
WWW.AZSEG.COM TEL: 480-388-7226 FAX: 480-359-3534

THIS DRAWING IS AN INSTRUMENT OF SERVICE AND THE PROPERTY OF SUSTAINABILITY ENGINEERING GROUP, AND SHALL REMAIN THEIR PROPERTY. THE USE OF THIS DRAWING SHALL BE RESTRICTED TO THE ORIGINAL SITE FOR WHICH IT IS PREPARED AND PUBLICATION THEREOF IS EXPRESSLY LIMITED TO SUCH USE.

4-DR-2021  
2/8/2021

DATE: 2/2/2021

LOCATION: Z:\SHARED\PROJECTS\GREYSTAR\RESIDENTIAL HEALTHCARE-90TH ST & RAINTREE-SCOTTSDALE-200626\11 CAD (SEG)\1.3 CDS\CD200626-C3.00.DWG SAVED BY: LAPTOP06



### LEGAL DESCRIPTION

A PORTION OF THE NORTHWEST QUARTER OF SECTION 7, TOWNSHIP 3 NORTH, RANGE 5 EAST OF THE GILA AND SALT RIVER BASE AND MERIDIAN, MARICOPA COUNTY, ARIZONA.

### STORM WATER STORAGE SUMMARY:

TOTAL VOLUME REQUIRED:  
 $V_R = 33,306 \text{ CF}$

TOTAL 10' CMP PROVIDED: 160+160=320 LF  
 $V_{R1} = 3.14 \times (5')^2 \times 320 = 25,133 \text{ CF}$

TOTAL OPEN RETENTION:  
 $V_{P2} = 6,712 + 3,990 = 10,702 \text{ CF}$

TOTAL BASIN PROVIDED:  
 $V_{P1} = 35,835 \text{ CF}$

### BASIS OF BEARING:

THE BASIS OF BEARING AND ALL MONUMENTATION SHOWN HEREON IS BASED ON THE MONUMENT LINE OF 90TH STREET, USING A BEARING OF SOUTH 00 DEGREES 03 MINUTES 34 SECONDS EAST, AS SHOWN ON RECORD OF SURVEY, RECORDED IN BOOK 896, PAGE 1, MARICOPA COUNTY RECORDS.

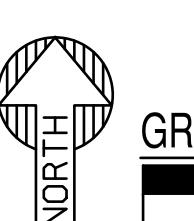
### CUT AND FILL QUANTITIES

(FOR PERMIT FEE ESTIMATION ONLY, CONTRACTOR TO PERFORM ITS OWN CALCULATIONS)

FILL +15,069 CY  
CUT -332 CY  
NET FILL +14,737 CY

UTILITY CROSSINGS			
UC-1	6" WATER BOT 18" STORM TOP	76.65 74.55	NO EXTRA PROTECTION REQUIRED
UC-2	6" WATER BOT 18" STORM TOP	76.65 72.77	NO EXTRA PROTECTION REQUIRED
● UC-5	16" STORM BOT 8" WATER TOP	76.44 74.40	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
UC-7	24" STORM BOT 8" SEWER TOP	76.37 69.20	NO EXTRA PROTECTION REQUIRED
● UC-8	24" STORM BOT 8" WATER TOP	76.41 74.40	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
● UC-9	24" STORM BOT 8" WATER TOP	77.67 75.60	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
● UC-10	24" STORM BOT 12" WATER TOP	74.50 72.50	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
● UC-11	24" STORM BOT 12" WATER TOP	74.24 72.20	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.

● REQUIRES VERTICAL REALIGNMENT PER MAG STD. DET. 370.



GRADING AND DRAINAGE PLAN KEYMAP

SCALE: 1" = 30'

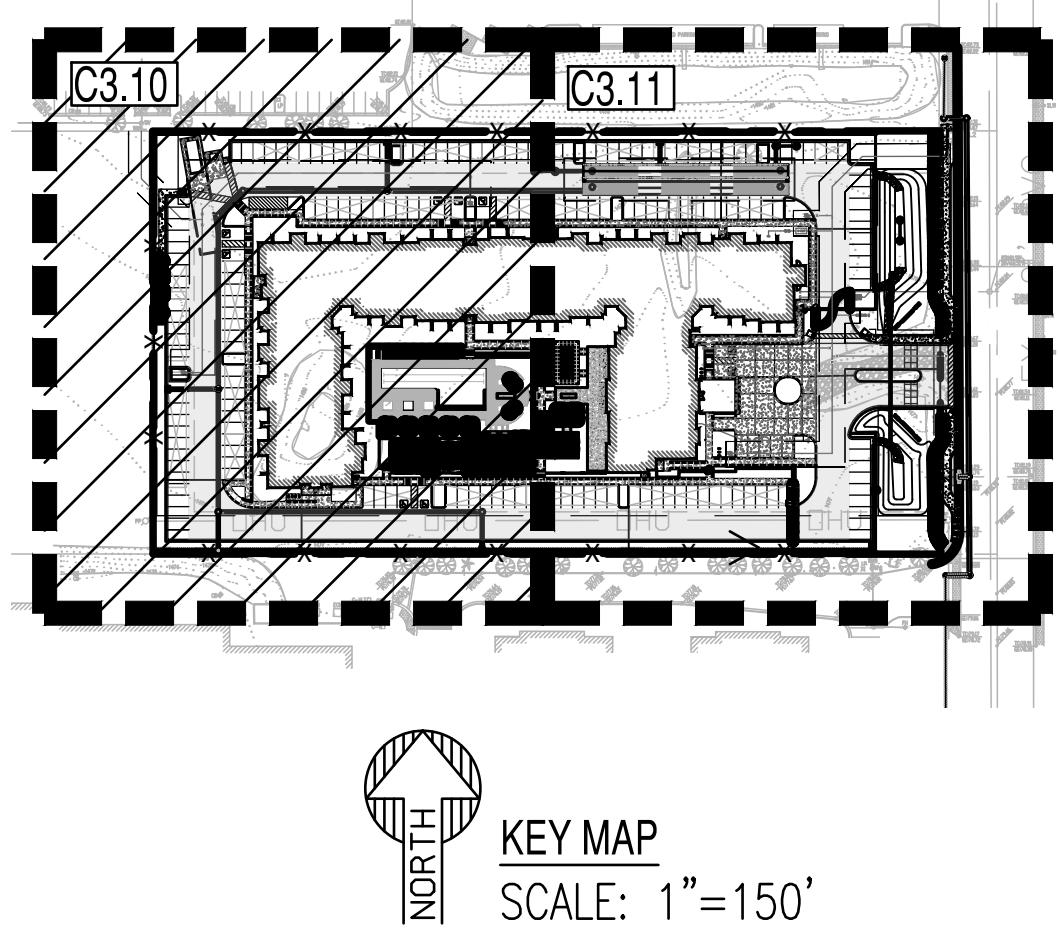
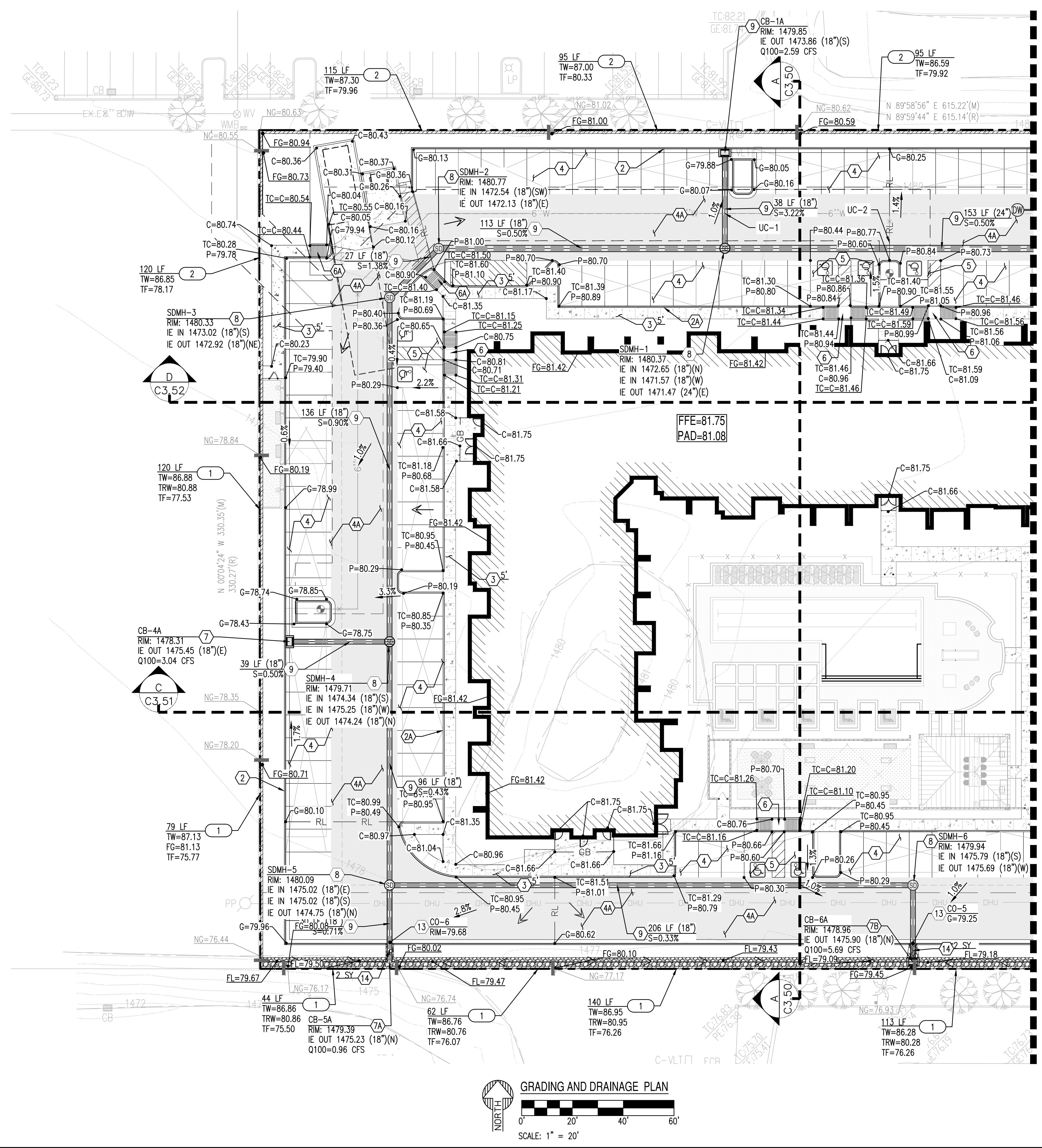
0' 30' 60' 90'

### EXISTING LEGEND:

- - - XXXX - - EX. MAJOR CONTOURS
- - - XXXX - - EX. MINOR CONTOURS
- TC:XX.XX EX. SPOT ELEVATION
- FL:XX.XX EX. PAVEMENT ELEVATION
- EX. EASEMENT LINE AS NOTED
- EX. S SEWER LINE
- CB STORM CATCH BASIN
- (S) SEWER MANHOLE
- (D) STORM MANHOLE
- GAS GAS LINE
- IRRIGATION LINE
- (A) SIGN
- (S) STREET LIGHT

PROJECT	RESIDENTIAL HEALTH CARE FACILITY
LOCATION	N. 90TH ST. & RAINTREE CIRCLE DR. SCOTTSDALE, ARIZONA 85260
DRAWN	RM 02/02/2021
DESIGNED	RM 02/02/2021
QC	SC 01/25/2021
QA	QA
PROJ. MGR.	AF 02/02/2021
DATE:	2/2/2021
ISSUED FOR:	DRB
REVISION NO.:	
DATE:	
REVISION NO.:	
DATE:	
REVISION NO.:	
DATE:	
REVISION NO.:	
DATE:	
REVISION NO.:	
DATE:	
JOB NO.:	200626
SHEET TITLE:	GRADING AND DRAINAGE PLAN KEYMAP
PAGE NO.:	
SHEET NO.:	C3.00

4-DR-2021  
2/8/2021



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CONSTRUCTION

## SUSTAINABILITY ENGINEERING GROUP



820 E. GELDING DRIVE SUITE 101, SCOTTSDALE, ARIZONA 85260  
WWW.AZSEG.COM TEL: 480-388-7226 FAX: 480-259-3534

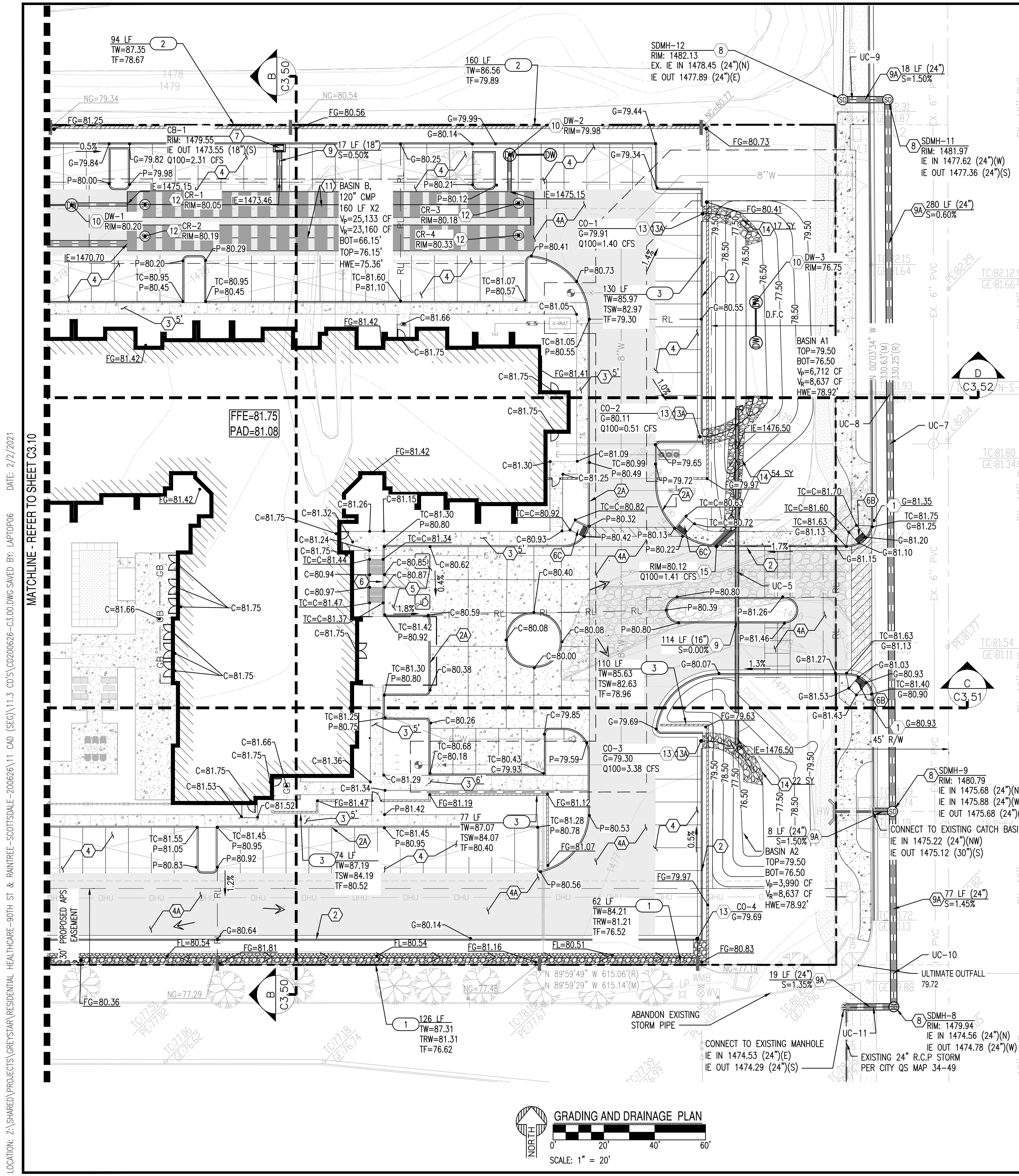


PROJECT	LOCATION
RESIDENTIAL CARE FACILITY	N. 90TH ST. & RAIN TREE CIRCLE DR. SCOTTSDALE, ARIZONA 85260

DRAWN	RM	02/02/2021
DESIGNED	RM	02/02/2021
QC	SC	01/25/2021
QA	QA	
PROJ. MGR.	AF	02/02/2021
DATE:		2/2/2021
ISSUED FOR:		DRB
REVISION NO.:		
DATE:		
JOB NO.:		200626
SHEET TITLE:		

## GRADING AND DRAINAGE PLAN

PAGE NO.: SHEET NO.: C3.10

**PROPOSED LEGEND:**

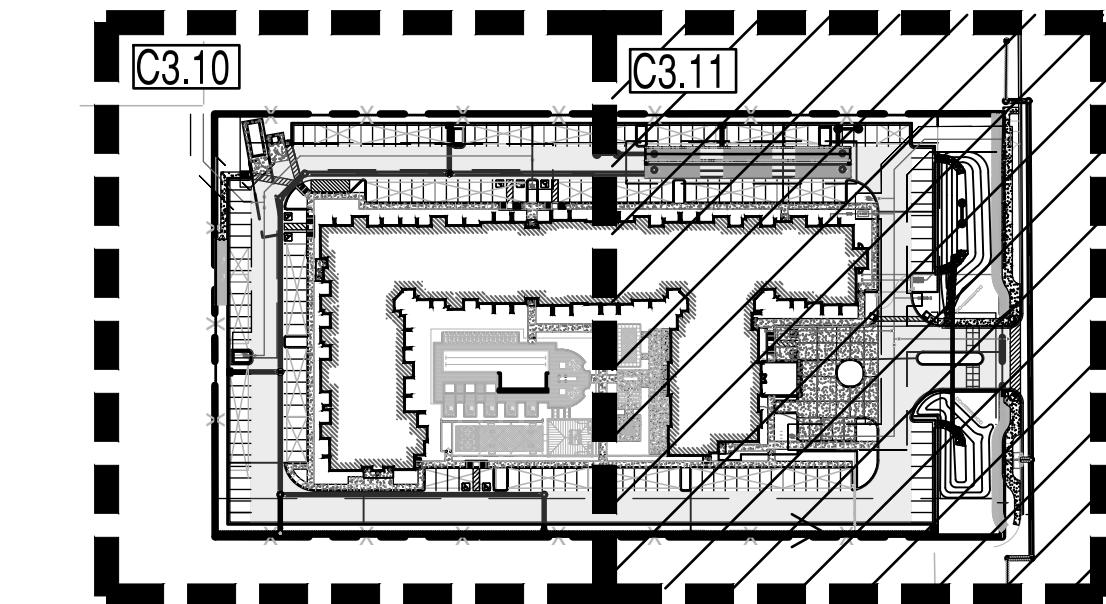
TC	TOP OF CURB
G=XX,XX	GUTTER ELEVATION, TC = G+0.5'
P=XX,XX	PAVEMENT ELEVATION
C=XX,XX	CONCRETE ELEVATION
—	PROPERTY LINE
—	CURB AND GUTTER
—	VERTICAL CURB
—	RIDLIGINE
—	GB — GRADE BREAK
—	LOC — LIMIT OF ON SITE CONSTRUCTION
—	XX — MAJOR CONTOUR
—	XX — MINOR CONTOUR
→	FLOW ARROW
□	CATCH BASIN
○ SD	STORM MANHOLE
—	STORM PIPE
DW DW	DRYWELL
FB	BUBBLER BOX
—	CONCRETE PAVEMENT
—	HEAVY DUTY PAVEMENT
—	LIGHT DUTY PAVEMENT

**RETAINING WALL CONSTRUCTION KEY NOTES**

- (1) CMU RETAINING WALL WITH 3' SCREEN WALL, 8' MAXIMUM RETAINED HEIGHT.
- (2) 6' VIEW FENCE.
- (3) 3' CMU SCREEN WALL WITH 3' VIEW FENCE.

UTILITY CROSSINGS			
● UC-5	16" STORM BOT	76.44	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
	8" WATER TOP	74.40	
● UC-7	24" STORM BOT	76.37	NO EXTRA PROTECTION REQUIRED
	8" SEWER TOP	69.20	
● UC-8	24" STORM BOT	76.41	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
	8" WATER TOP	74.40	
● UC-9	24" STORM BOT	77.67	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
	8" WATER TOP	75.60	
● UC-10	24" STORM BOT	74.50	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
	12" WATER TOP	72.50	
● UC-11	24" STORM BOT	74.24	PROVIDE VERTICAL REALIGNMENT PER MAG STD. DET. 370.
	12" WATER TOP	72.20	

● REQUIRES VERTICAL REALIGNMENT PER MAG STD. DET. 370.

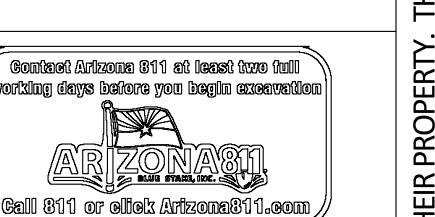


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PROJECT  
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QC	SC	02/02/2021
QA	QA	02/02/2021
PROJ. MGR.	AF	02/02/2021

LOCATION  
N. 90TH ST. & RAINBOW  
CIRCLE DR.  
SCOTTDALE, ARIZONA 85260

DATE:  
2/2/2021

ISSUED FOR:  
DRB

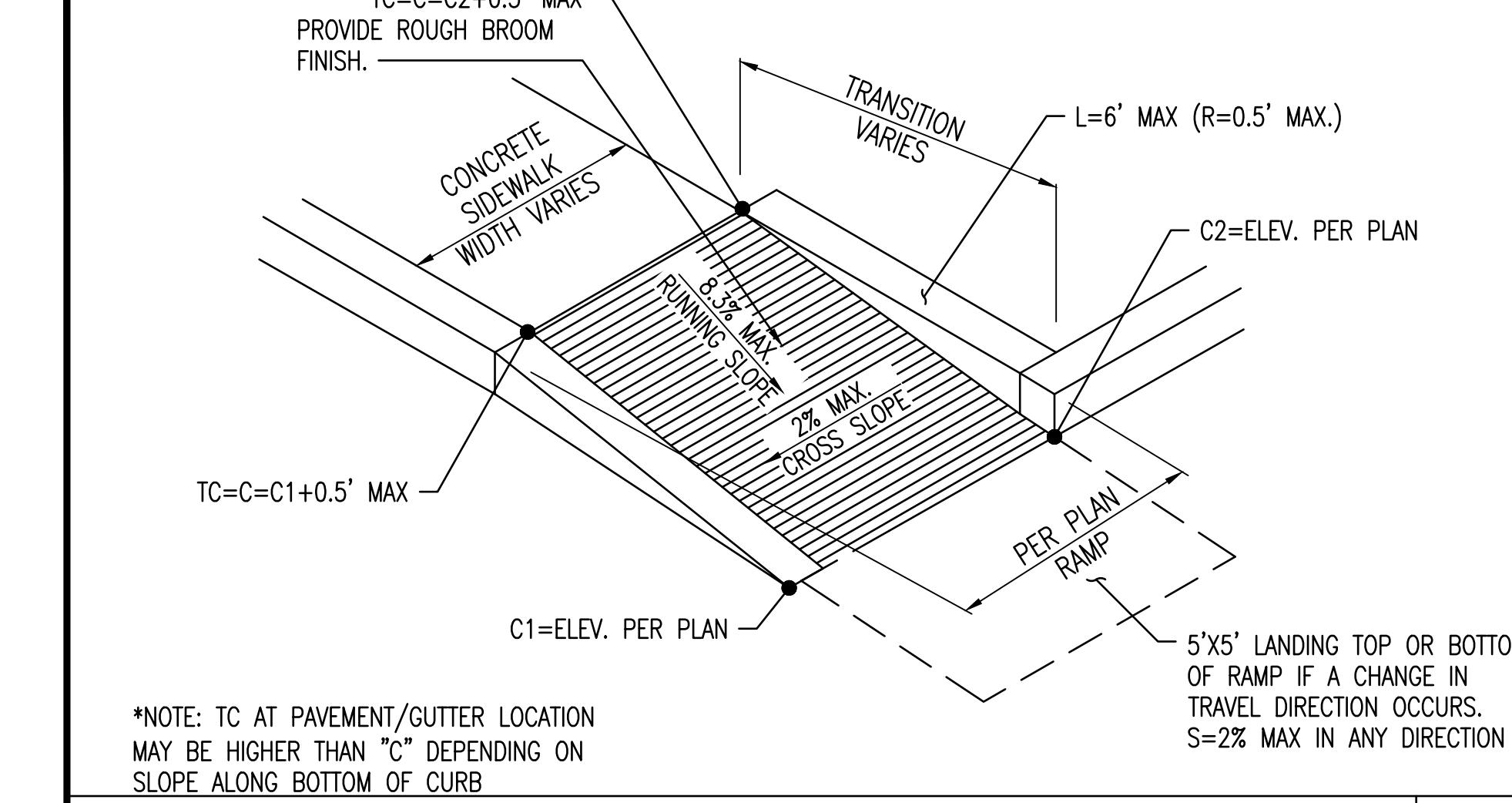
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JOB NO.:  
200626

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GRADING AND DRAINAGE  
PLAN

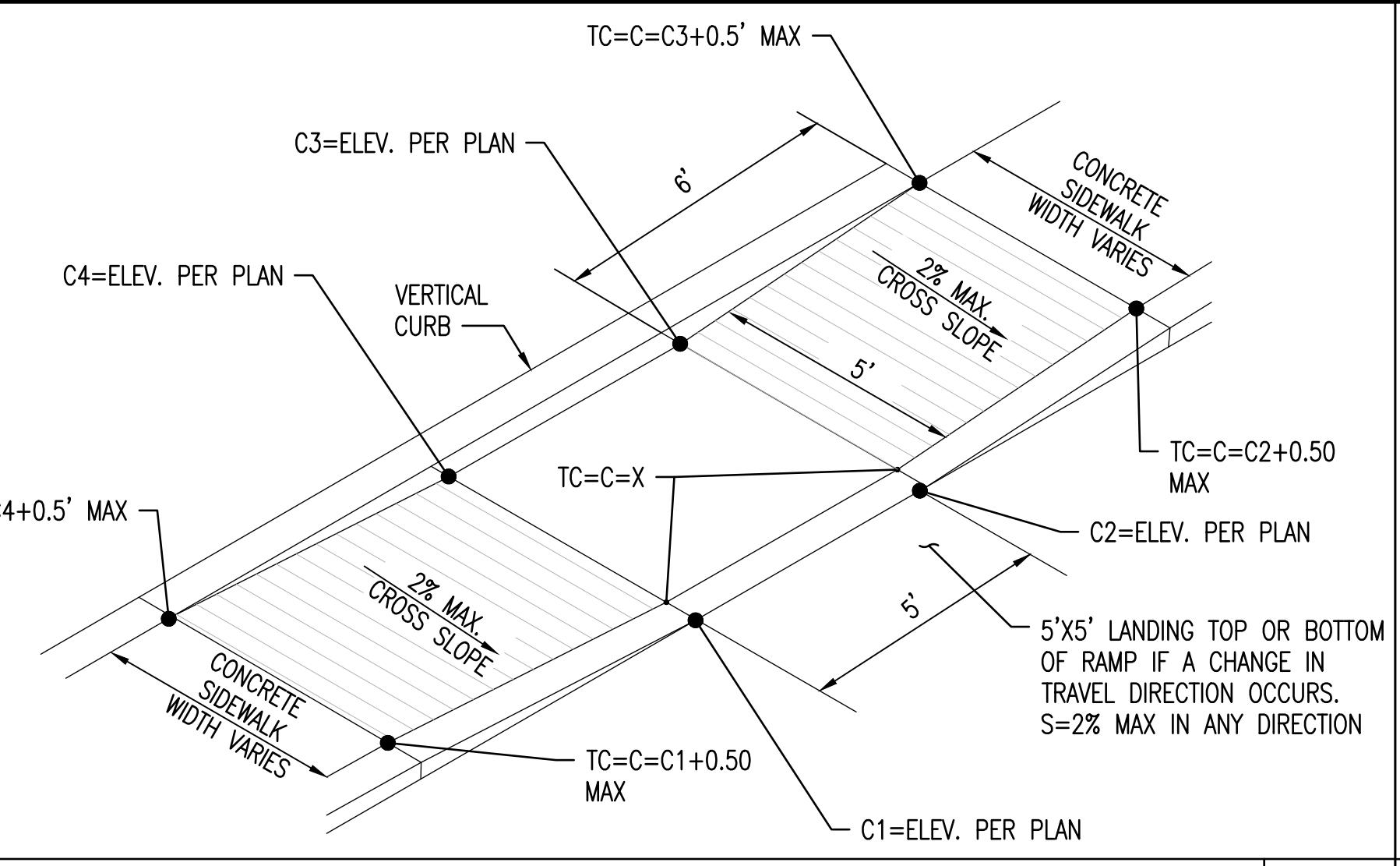
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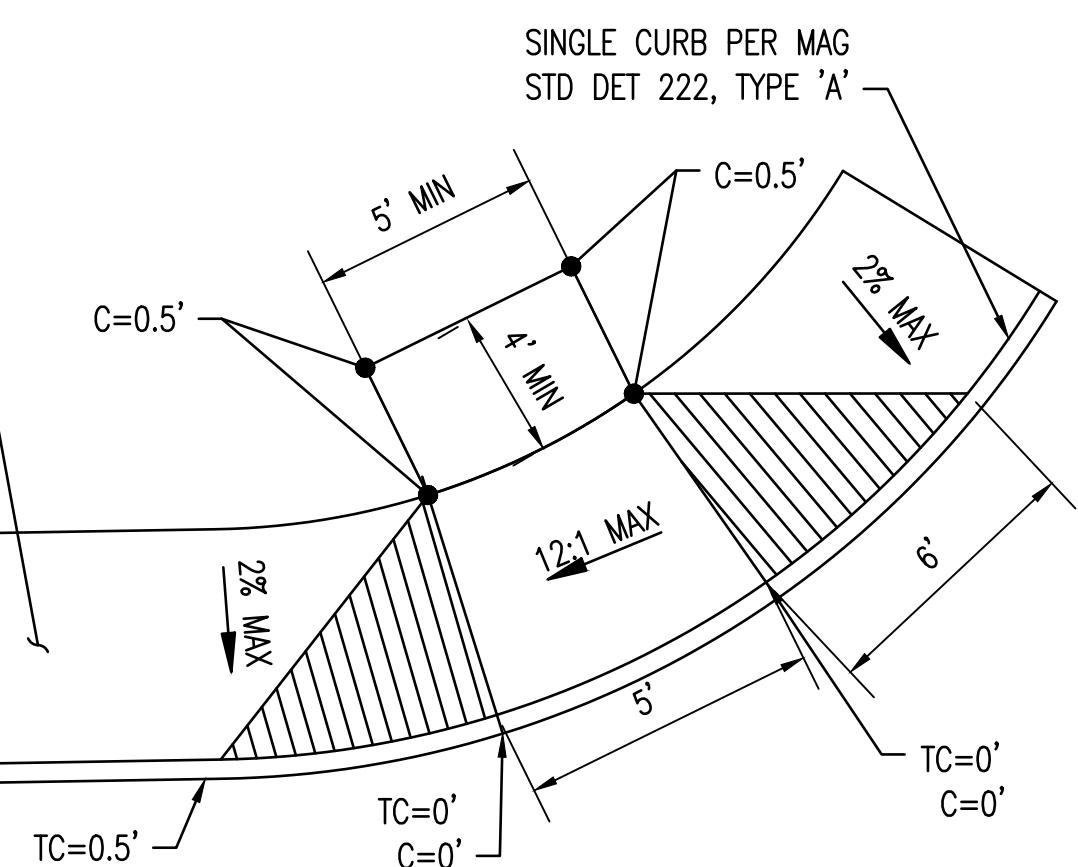
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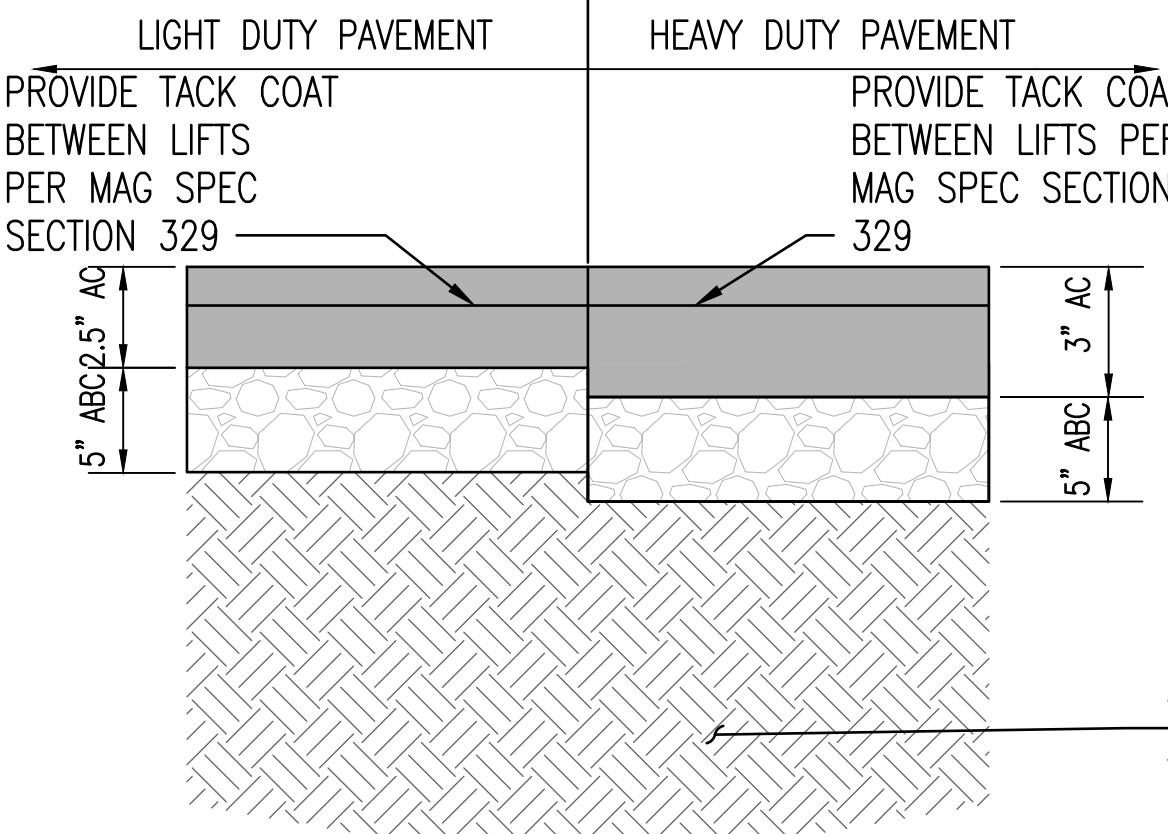
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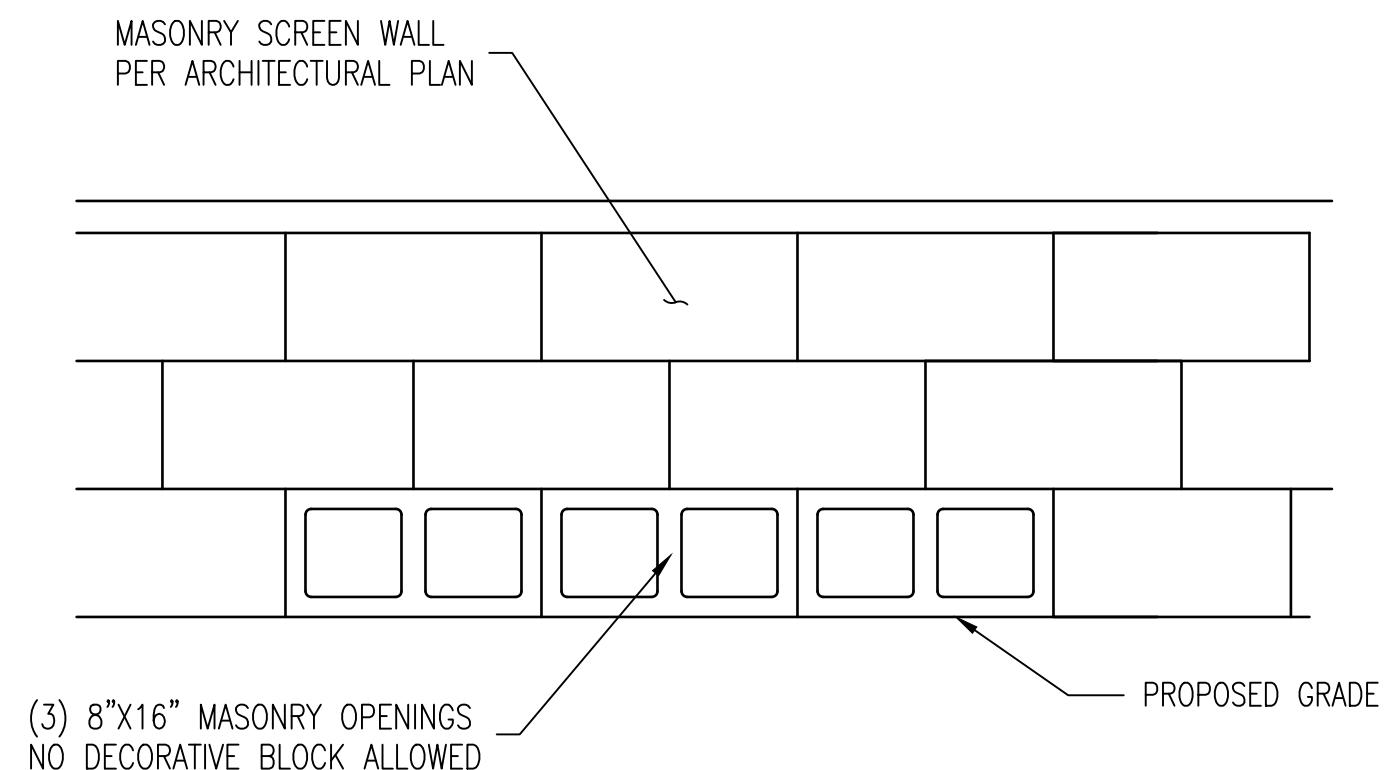
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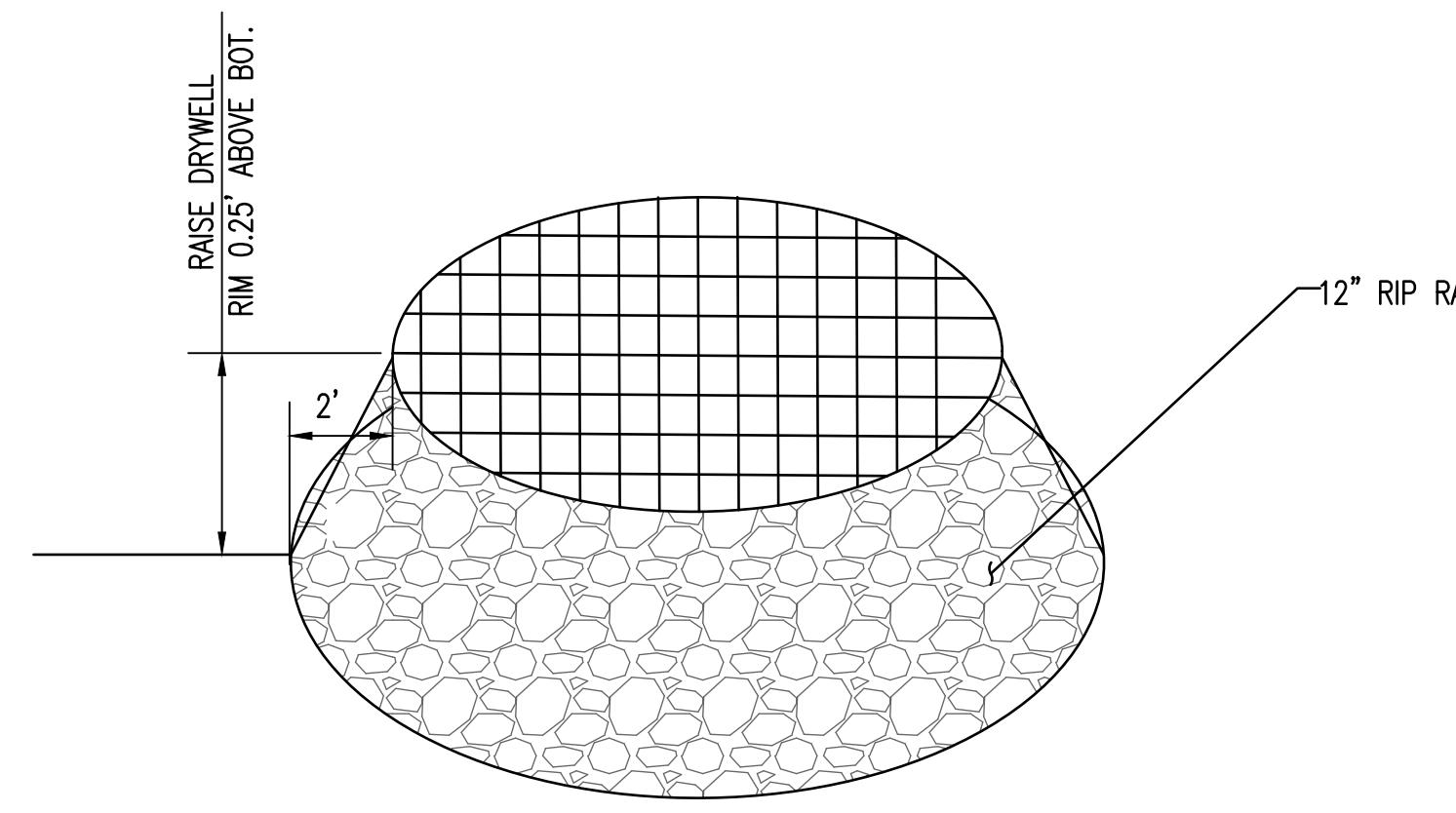
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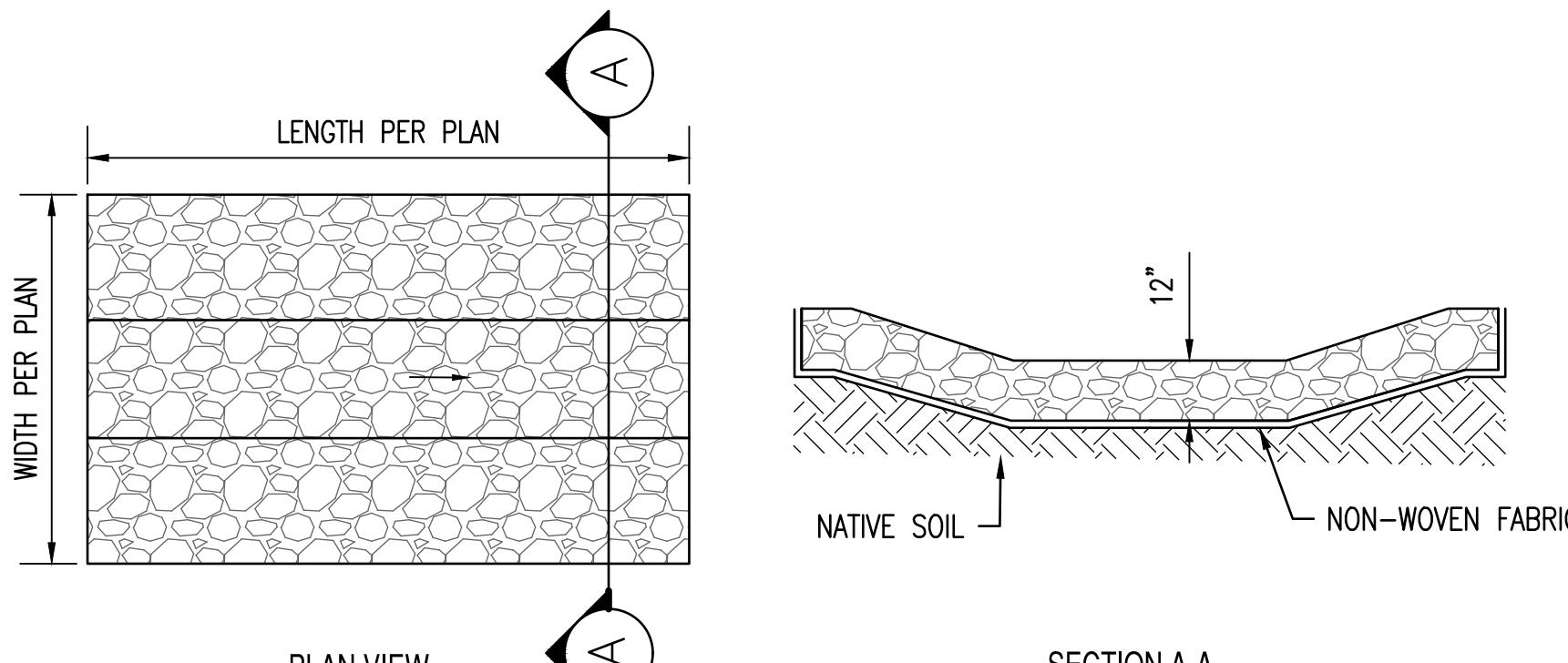
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MASONRY WALL OPENING  
N.T.S.

6

RAISED DRYWELL RIM  
N.T.S.

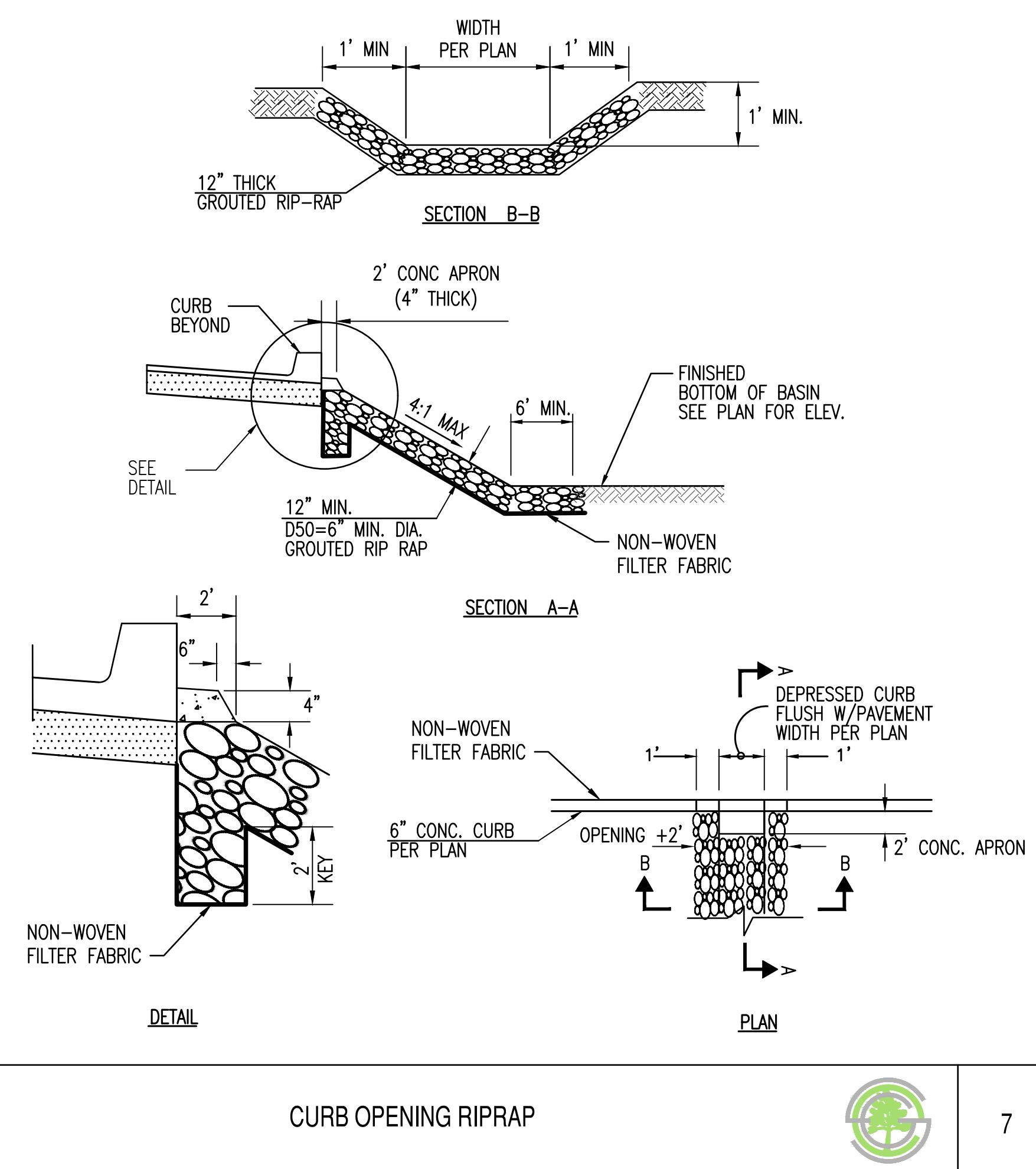
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TYPICAL RIP RAP PAD



5



CURB OPENING RIPRAP



7

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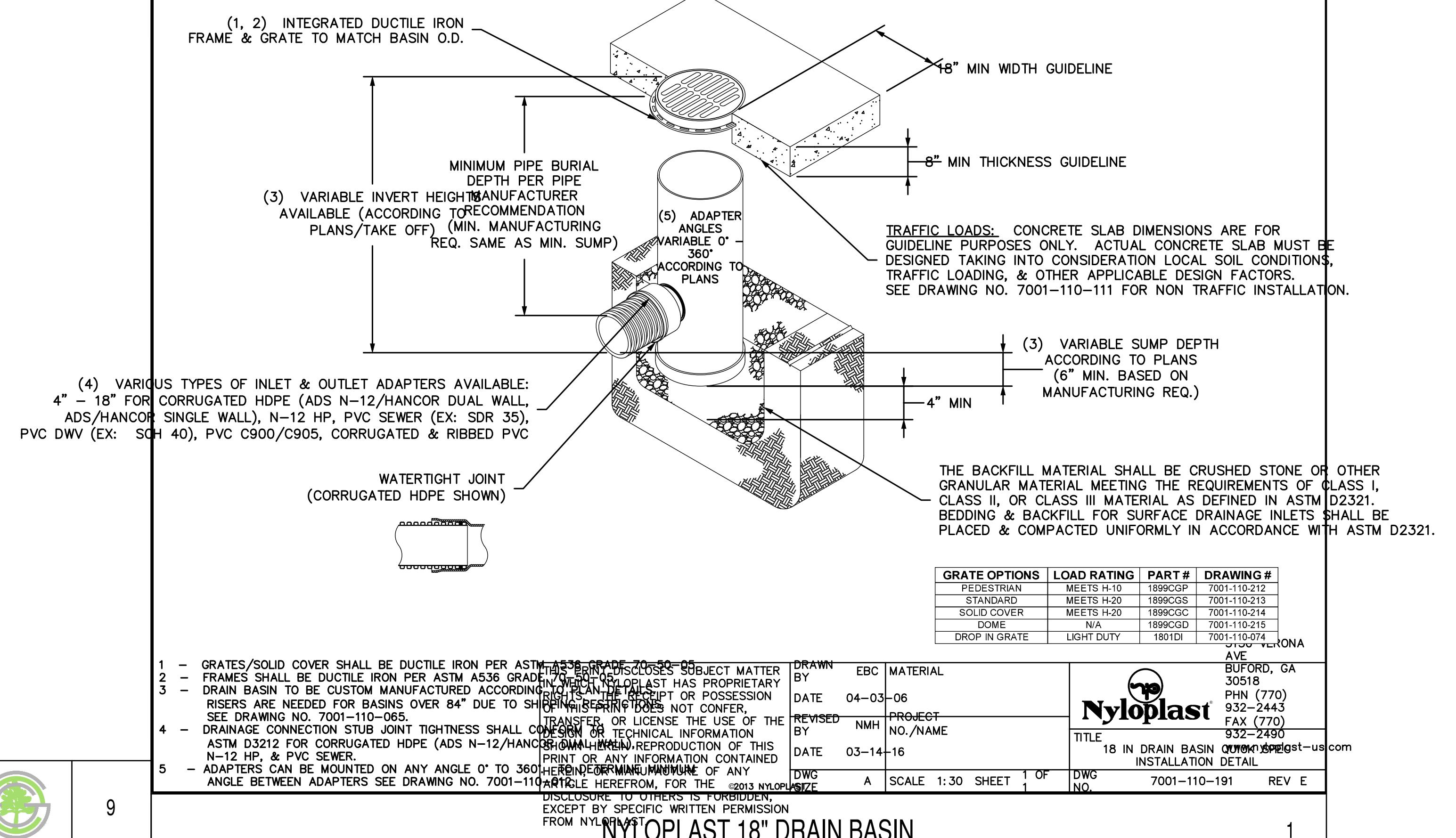
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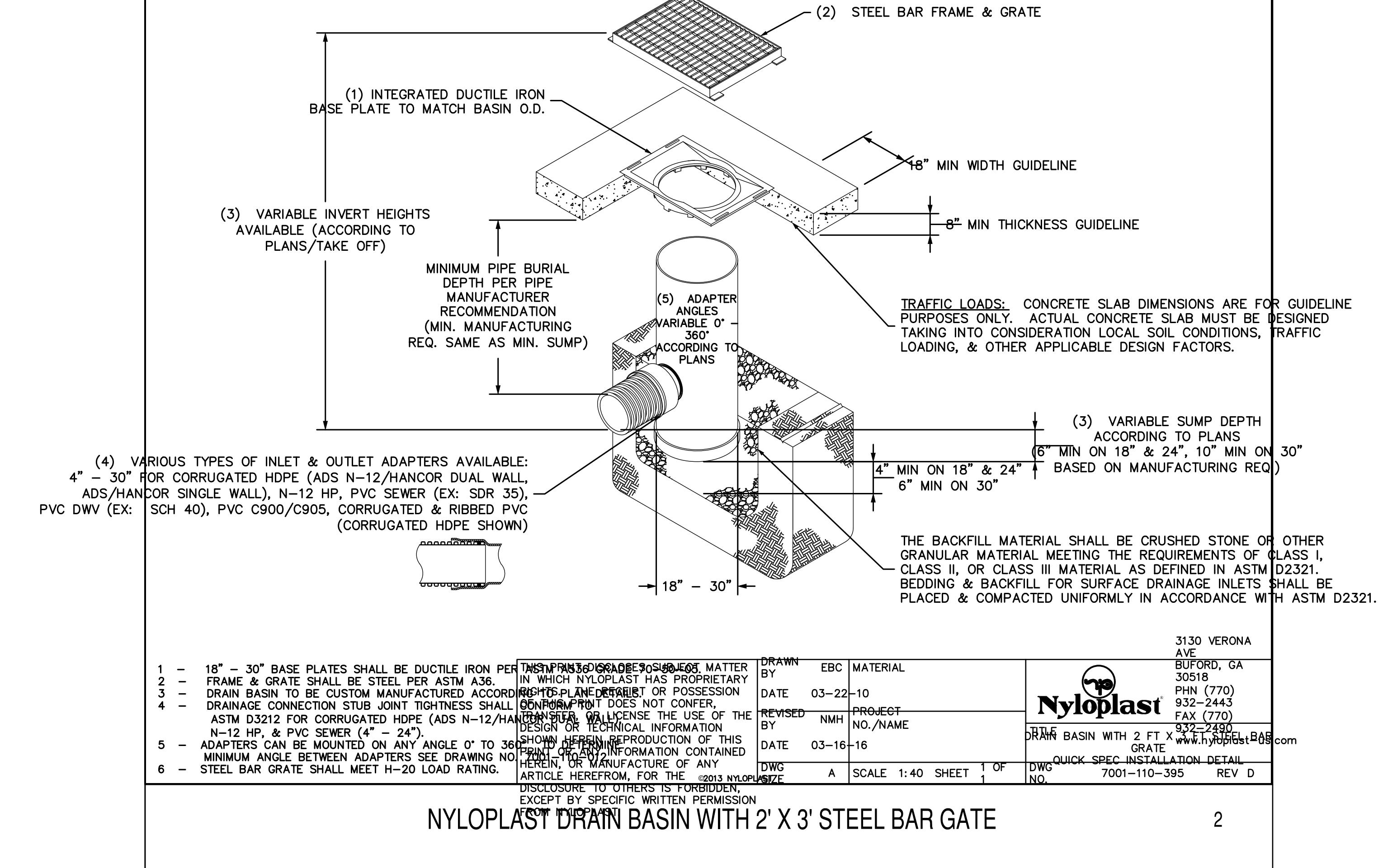
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DRAWN _____ DESIGNED _____ QC _____ QA _____ PROJ. MGR. _____	RM 02/02/2021 SC 01/25/2021 AF 02/02/2021
DATE: 2/2/2021	ISSUED FOR: DRB
REVISION NO.:  △ △ △ △ △	DATE: 2/2/2021
JOB NO.: 200626	SHEET TITLE: GRADING AND DRAINAGE DETAILS
PAGE NO.: C3.20	SHEET NO.: C3.20

## PENDING DRAWING

## NYLOPLAST 18" DRAIN BASIN: 2818AG \_ \_ X



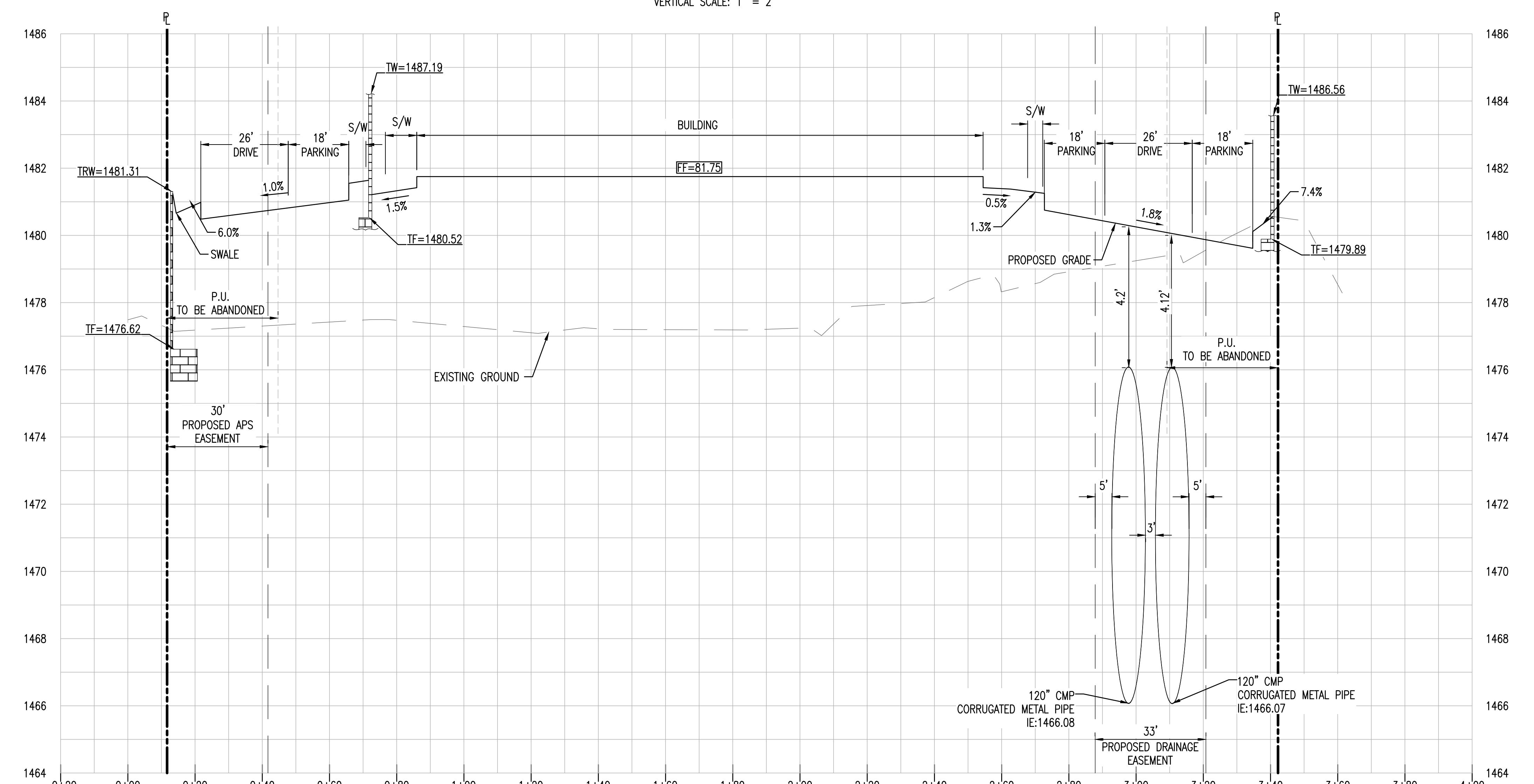
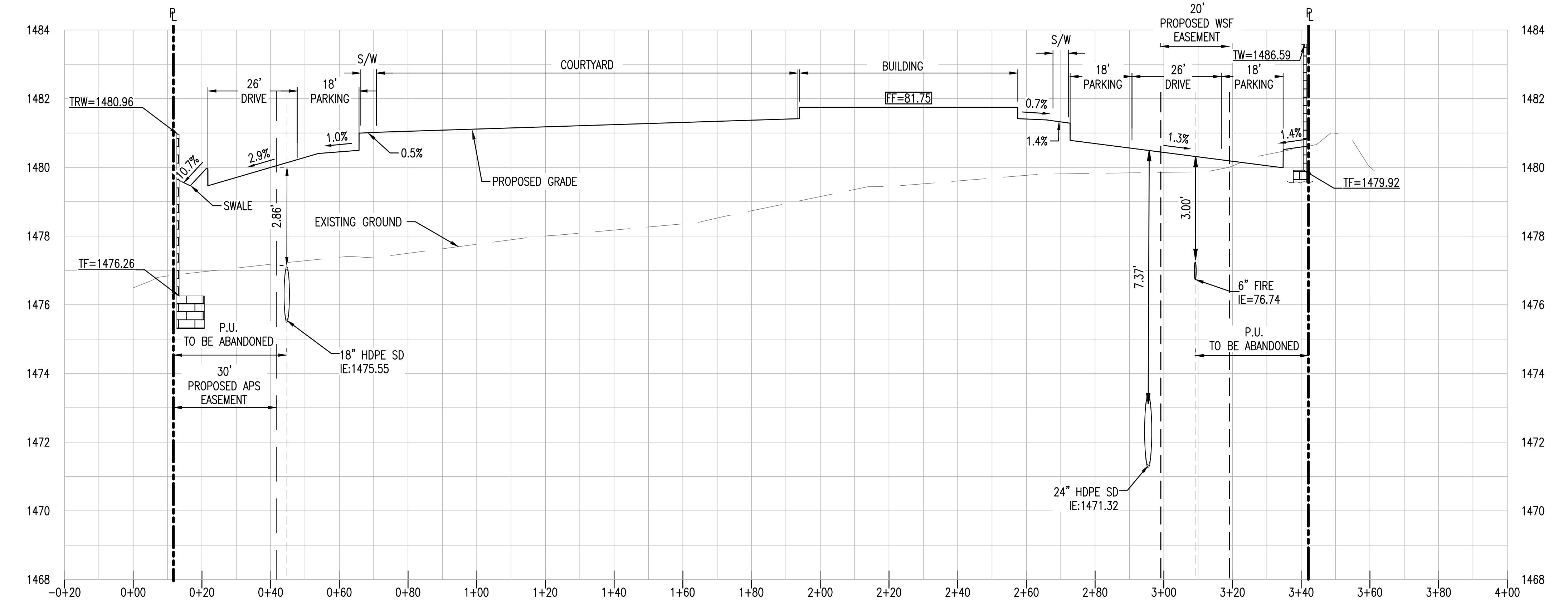
## NYLOPLAST DRAIN BASIN WITH 2 FT X 3 FT STEEL BAR GRATE

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JOB NO.: 200626	
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PAGE NO.:	SHEET NO.:
C3.21	

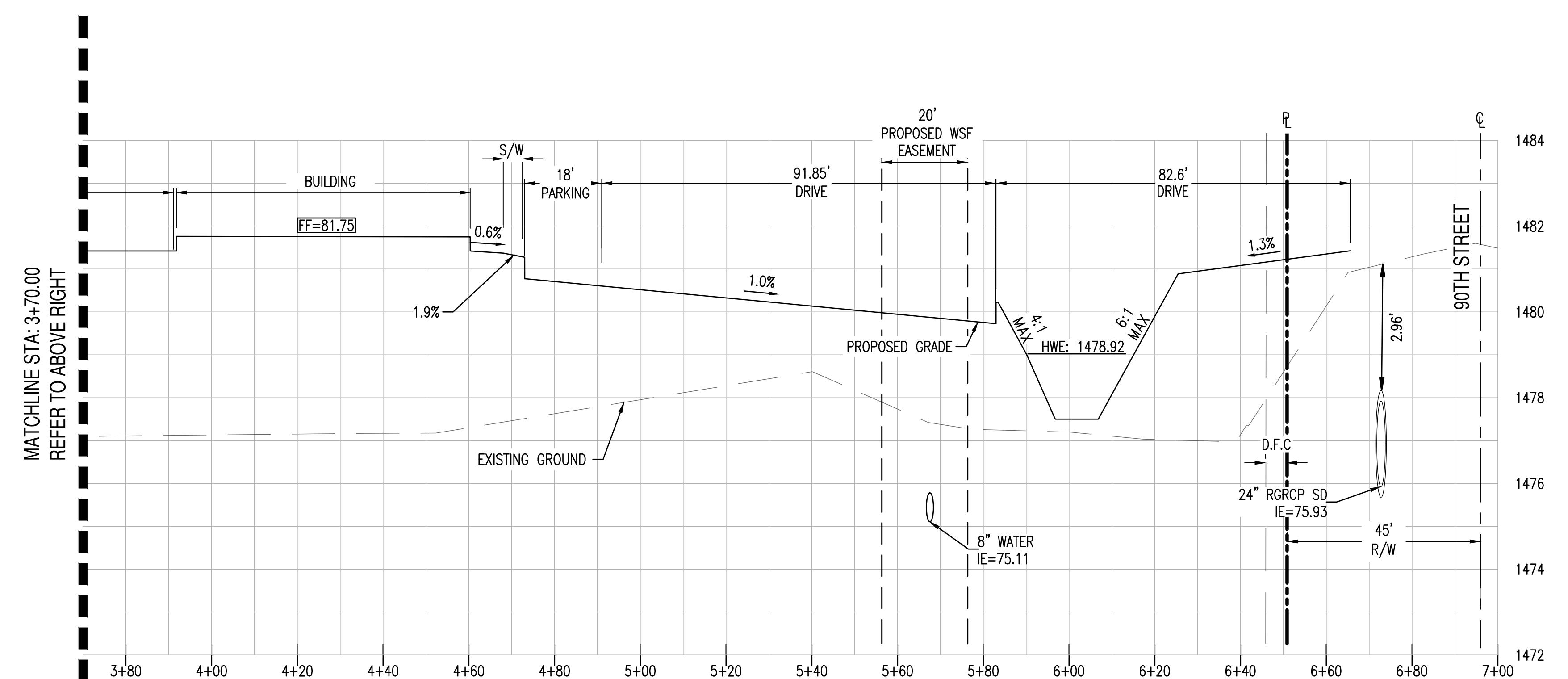
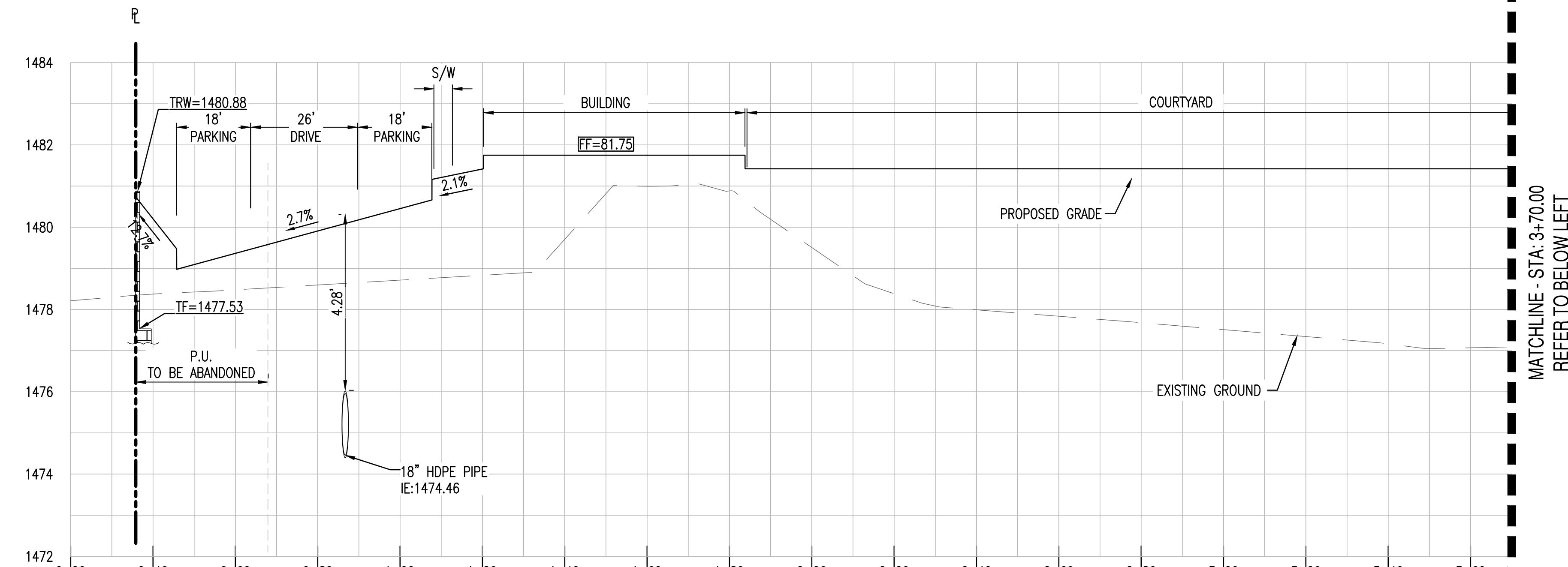
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CROSS-SECTIONS  
C3.50



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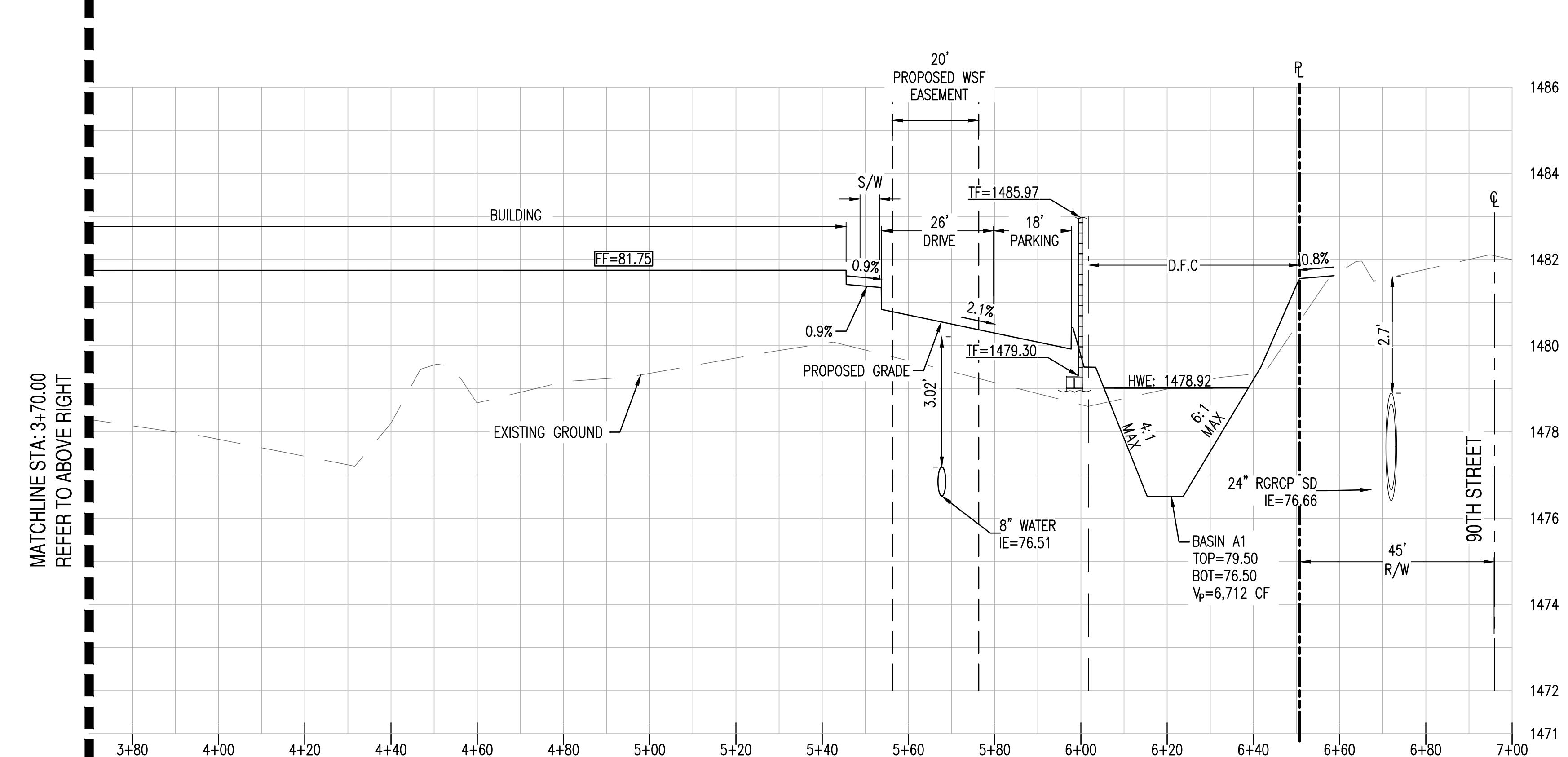
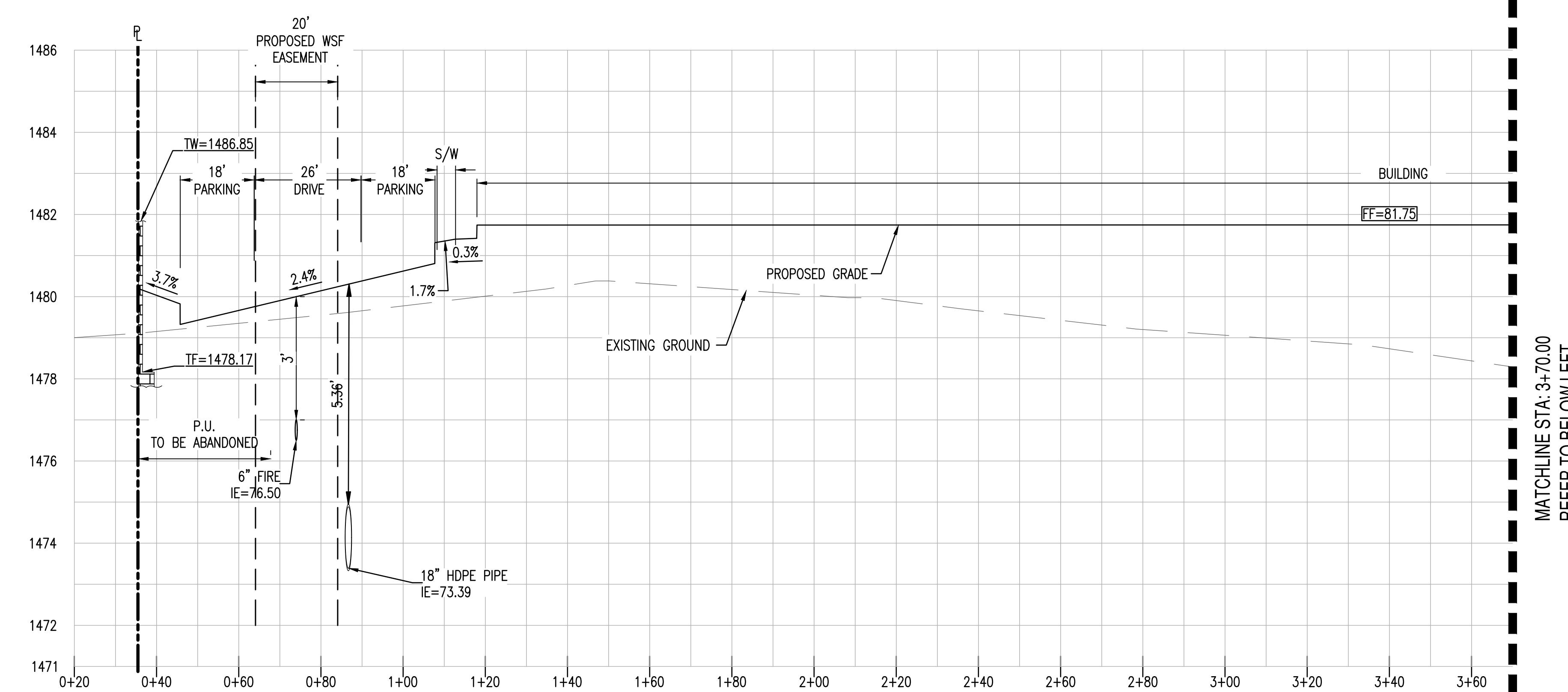


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QA QA	
PROJ. MGR. AF	02/02/2021
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JOB NO.: 200626	
SHEET TITLE: SITE CROSS-SECTIONS	
PAGE NO.: C3.51	SHEET NO.: C3.51



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SITE CROSS-SECTIONS

PAGE NO.: SHEET NO.:  
C3.52