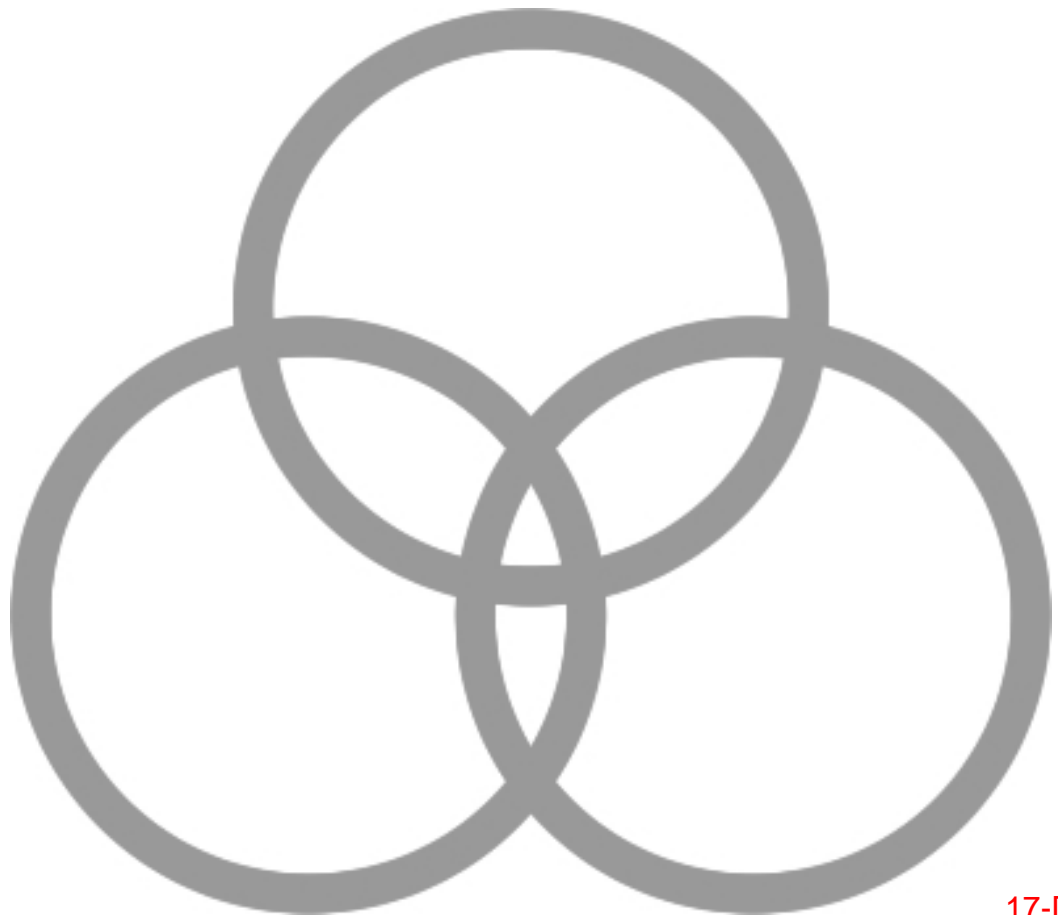


SOUTHDALE

Final Wastewater Basis of Design Report

3 engineering Job #: 1872

April 23, 2021



SOUTHDALE

FINAL WASTEWATER BASIS OF DESIGN REPORT

Prepared for:

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April 23, 2021

Submittal to:

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Job Number 1872

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1. Introduction

The project site, Southdale, is located in the southeast quarter of Section 34, Township 2 North, Range 4 East of the Gila and Salt River Meridian, Maricopa County, Arizona within the City of Scottsdale. The project is located on the northeast corner of 70th Street and McDowell Road. The site is bounded on the north by an apartment complex, on the east by a commercial development, on the south by McDowell Road, and on the west by 70th Street. See Appendix A for a vicinity map.

The existing zoning is C-3. The land is currently used as a commercial development. The General Plan shows the site as a Mixed-Use Neighborhood. The proposed zoning is PUD. The site is a proposed 267-unit apartment complex with office and retail space.

2. Design Documentation

The purpose of this Wastewater Basis of Design Report is to verify that the existing City of Scottsdale sewer system is able to accommodate demands generated by the proposed project, Southdale. FlowMaster V8i by Bentley Systems was used to model and analyze the existing sewer system downstream of the site to verify it has capacity for the existing flow plus the flows generated from the proposed site, Southdale. Modeling was performed in compliance with the City of Scottsdale design requirements.

The existing flow in the system was tested at two manholes in Palm Lane, downstream of the site. The tests were performed by RDH Environmental Services on 1/25/2020 through 2/2/2020. See results in Appendix B.

Demands for the proposed site were calculated using Section 7-1.403A of the City of Scottsdale 2018 Design Standards and Policies Manual. It is our opinion that this report is in accordance with the 2018 City of Scottsdale Design Standards and Policies Manual.

3. Existing Conditions

The existing zoning is C-3. The existing land is a commercial development. See Appendix A for a vicinity map. The site is surrounded by existing multi-family residential development and commercial development. There is an existing 8" V.C.P. sewer line in the apartment complex north of the site that will be utilized by the proposed development. This sewer line flows north to an 8" V.C.P. sewer line in Palm Lane at City of Scottsdale Manhole #31. This manhole has an overflow pipe that is conveyed to Manhole #48, which outlets to a 10" sewer line in Palm Lane. The 8" sewer line in Palm Lane flows to an 8" V.C.P. sewer line in Scottsdale Road, that flows south. The 10" sewer line in Palm lane flows to an 18" V.C.P. sewer line in Scottsdale Road, that flows south. The 8" sewer line running through the apartment north of the site, the 8" and 10" sewer lines in Palm Lane and the 8" sewer line in Scottsdale Road will be analyzed to determine if they have capacity for the additional flow generated from the proposed project. See Figure 1 for existing sewer layout.

4. Proposed Conditions

The project consists of a 267-unit apartment complex with 3,300 s.f. of office space and 2,200 s.f. of retail space on 3.83 acres. It is proposed that this project will tie into the existing 8" V.C.P. sewer line in the apartment complex north of the site. See Preliminary Onsite Utility Plans in Appendix G.

The proposed site includes one pool. The assumed instantaneous backwash rate of the pool is 100 gpm. The pool backwash will be captured by an equalization tank that is to be sized for up to four consecutive backwashes. The tank will have a metered flow of 5 gpm that outlets to the proposed sewer system.

5. Computations

5.1. Proposed Site Demand Calculations

The following demand criteria from the City of Scottsdale 2018 Design Standards and Policies Manual (DSPM) were used in determining the system demands for the proposed site.

1. 267 proposed units
2. 3.83 acre site (70 du/ac)
3. 1.7 persons per unit (Per DSPM, multifamily density exceeding 22 du/ac)
4. 100 gallons per person per day (Per DSPM, residential)
5. Peaking factor = 4 (Per DSPM, residential)
6. 3,300 s.f. proposed Office Space
7. 0.4 gpd/s.f. (Per DSPM, Office)
8. 2,200 s.f. proposed Retail Space
9. 0.5 gpd/s.f. (Per DSPM, Commercial/Retail)
10. Peaking factor = 3 (Per DSPM, Commercial/Retail, Office)
11. 5 gallons per minute per pool for backwash (assume 1 pool)

TABLE 1: ON-SITE SEWER DEMANDS	
Pool Backwash	5 gpm
Avg. daily demand w/ pool backwash	38.20 gpm
Design Flow Rate w/ pool backwash	136.12 gpm

Residential

Average daily demand: $267 \text{ units} \times 1.7 \text{ persons per unit} \times 100 \text{ gpd per person} = 45,390 \text{ gpd}$
 $= 45,390 \text{ gpd} / 1440 \text{ mpd} = 31.52 \text{ gpm}$

Peak flow rate = $4.0 \times 45,390 \text{ gpd} = 181,560 \text{ gpd}$
 $= 181,560 \text{ gpd} / 1440 \text{ mpd} = 126.08 \text{ gpm}$

Office

Average daily demand: $3,300 \text{ s.f.} \times 0.4 \text{ gpd per s.f.} = 1,320 \text{ gpd}$
 $= 1,320 \text{ gpd} / 1440 \text{ mpd} = 0.92 \text{ gpm}$

Peak flow rate = $3.0 \times 1,320 \text{ gpd} = 3,960 \text{ gpd}$
 $= 3,960 \text{ gpd} / 1440 \text{ mpd} = 2.75 \text{ gpm}$

Retail

Average daily demand: $2,200 \text{ s.f.} \times 0.5 \text{ gpd per s.f.} = 1,100 \text{ gpd}$
 $= 1,100 \text{ gpd} / 1440 \text{ mpd} = 0.76 \text{ gpm}$

Peak flow rate = $3.0 \times 1,100 \text{ gpd} = 3,300 \text{ gpd}$
 $= 3,300 \text{ gpd} / 1440 \text{ mpd} = 2.29 \text{ gpm}$

Total

Average daily demand = 33.20 gpm

Peak flow rate = 131.12 gpm

5.2. Existing System Flows

The existing maximum flows for the sewer lines in Palm Lane were determined by the flow test performed 1/25/2020 through 2/2/2020. There is a maximum of 13.172 gpm exiting manhole #48 east to the 10" sewer line in Palm Lane and a maximum of 218.699 gpm exiting manhole #31 east to the 8" sewer line in Palm Lane. The data was logged in 5-minute intervals over 9 days, including two weekends. See Appendix B for flow test data.

Two legs contribute to manhole #31. The leg flowing from the south has 114 single family homes, 101 multi-family units, the Aire Townhome development and ultimately the proposed site. The leg flowing from the west has 349 single family homes, 114 multi-family units, and Tonalea elementary school with 500 students. The flows from the two legs are calculated below per the City of Scottsdale DSPM. See Appendix C for a map of the legs.

South Leg (Orange)

114 Single-family x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 79.16 gpm

Aire townhomes: 80 units x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 55 gpm

Aire townhomes pool backwash: 100 gpm

101 multi-family x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 70.12 gpm

Total Peak flow = 304.28 gpm

West Leg (Green)

349 Single-family x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 242.36 gpm

114 multi-family x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 79.16 gpm

Tonalea elementary: 50 gpd per student x 500 students x 6.0 P.F. / 1440 = 104.17 gpm

Total Peak flow = 425.69 gpm

The total calculated flow for this manhole is 729.97 gpm. The south leg accounts for 41.68% of the total flow and the west leg accounts for 58.32% of the total flow.

The proportion of the total flow for each leg is applied to the tested flow through manhole #31. From the observed test results, the south leg has a proportional flow of 91.15 gpm, and the west leg has a proportional flow of 127.54 gpm. The total flow is 218.69 gpm.

Analysis of the 8" V.C.P. sewer line in Scottsdale Road requires adding the peak flows from four downstream buildings that include: a chiropractor's office, Ace Hardware, Post Office, and Comerica Bank. The flows for the sites are calculated below per the City of Scottsdale DSPM.

Chiropractic: 2,135 sf x 0.4 gpd per sf x 3.0 P.F. / 1440 = 1.78 gpm

Ace Hardware: 20,175 sf x 0.5 gpd per sf x 3.0 P.F. / 1440 = 21.02 gpm

Post Office: 84,225 sf x 0.1 gpd per sf x 3.0 P.F. / 1440 = 17.55 gpm

Bank: 3,950 sf x 0.5 gpd per sf x 3.0 P.F. / 1440 = 4.11 gpm

Total Peak Flow = 44.46 gpm

5.3. Sewer System Analysis

FlowMaster V8i by Bentley Systems was used to model and analyze the existing sewer system for compliance with the C.O.S. design requirements. The sewer lines were modeled with a Manning's n coefficient of 0.013. The sewer rims and inverts were surveyed by 3 engineering on

02/13/20 and 03/16/20. See Figure 1 for an overall system layout. In addition to analyzing the 8" sewer running through the apartment site, the system downstream will be analyzed to address the 8" sewer line in Scottsdale Road which does not have sufficient capacity for the additional flows from the proposed site in the existing configuration. The maximum allowable d/D for all pipes discussed is 0.75.

Existing Sewer Line in Apartment

The existing 8" sewer line running through the apartment complex north of the site was analyzed at the minimum surveyed slope of 0.27%. The existing flow in this segment is the 91.15 gpm from the south leg. The existing d/D is 0.39. See Appendix D for FlowMaster results of this pipe.

Existing Sewer Line in Apartment with Proposed Site

The existing 8" sewer line running through the apartment complex north of the site was analyzed at the minimum surveyed slope of 0.27%. The new flow includes the the 91.15 gpm from the south leg, plus the additional 136.12 gpm of flow from the proposed site for a total of 227.27 gpm. The proposed d/D is 0.68 in the existing line. See Appendix D for FlowMaster results of this pipe.

Existing Sewer System in Palm Lane and Scottsdale Road

In the existing condition, Manhole #31 in Palm lane, receives the 91.15 gpm from the south leg and the 127.54 gpm from the west leg. There is an existing overflow pipe elevated 3" above the downstream pipe in manhole #31 that flows into manhole #48. The overflow pipe was modeled as a weir using the resulting elevation when the total flow of 218.69 gpm enters the 8" pipe in Palm Lane. The overflow pipe conveys a flow of 48.74 gpm to the 10" line in Palm Lane. The results of the existing system analysis are discussed below and FlowMaster Data is included in Appendix E.

- The existing 10" sewer line in Palm Lane was analyzed at a minimum surveyed slope of 0.43%. The existing flow includes the 13.17 gpm from the flow test of manhole #48 plus the 48.74 gpm from the overflow pipe in manhole #31 for a total flow of 61.91 gpm. The existing d/D is 0.21.
- The existing 8" sewer line in Palm Lane was analyzed at a minimum surveyed slope of 0.27%. The existing flow includes the 169.95 gpm that bypasses the overflow pipe in manhole #31. The existing d/D is 0.56.
- The existing 8" sewer line in Scottsdale Road was analyzed at a minimum surveyed slope of 0.19%. The existing flow includes the 169.95 gpm from the 8" line in Palm Lane plus the 44.46 gpm from the buildings along Scottsdale Road for a total flow of 214.41 gpm. The existing d/D is 0.75.

Proposed Sewer System in Palm Lane and Scottsdale Road with Proposed Site

The proposed project, Southdale, generates 136.12 gpm of peak wastewater flow that is conveyed to manhole #31. In the existing configuration, the capacity of the 8" line in Scottsdale Road will be exceeded as the d/D is already 0.75 before the additional flows. The proposed plan is to divert more flow into the 10" line in Palm lane, which has excess capacity.

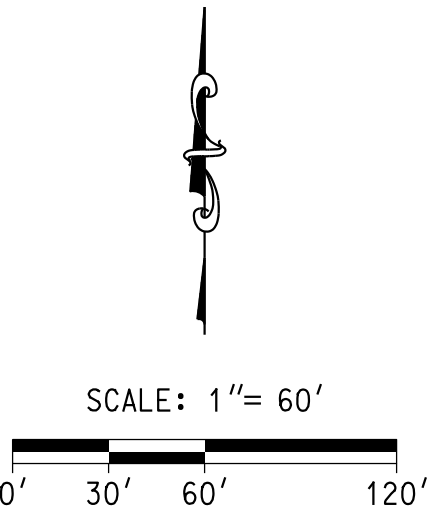
This will be achieved by adding a manhole in the west leg (green) and connecting the leg directly into manhole #48. The 10" line in Palm Lane will then receive the entire 127.54 gpm from the West leg. Manhole #31 in Palm lane will receive the existing 91.15 gpm from the South leg plus the additional 136.12 gpm from the proposed site for a total flow of 227.27 gpm. There is an existing overflow pipe elevated 3" above the downstream pipe in manhole #31 that flows into manhole #48. The overflow pipe will remain unchanged. With this flow, the overflow pipe conveys 54.90 gpm of the 227.27 gpm to manhole #48.

The results are discussed below. FlowMaster Data is included in Appendix F and shown in Figure 1 on the following page.

- The 10" sewer line in Palm Lane was analyzed at a minimum surveyed slope of 0.43%. The proposed flow includes the 127.54 gpm from the west leg plus the 13.17 gpm from the flow test of manhole #48 plus the 54.90 gpm from the overflow pipe in manhole #31 for a total flow of 195.61 gpm. The proposed d/D is 0.38.
- The 8" sewer line in Palm Lane was analyzed at a minimum surveyed slope of 0.27%. The proposed flow includes the 172.37 gpm from the south leg and proposed site that bypasses the overflow pipe. The proposed d/D is 0.57.
- The 8" sewer line in Scottsdale Road was analyzed at a minimum surveyed slope of 0.19%. The proposed flow includes the 172.37 gpm from the 8" line in Palm Lane plus 44.46 gpm from the buildings along Scottsdale Road for a total flow of 216.83 gpm. The proposed d/D is 0.75.

6. Summary

The Peak Flow for the proposed site is 136.12 gpm. The site ties into an existing 8" sewer line, in the apartment complex north of the site, that has an existing flow of 91.15 gpm. The pipe has a proposed d/D of 0.68 with the additional flow from the proposed site. In the existing configuration, the 8" sewer line in Scottsdale Road is at capacity and cannot handle additional flow from the proposed site, Southdale. The proposed improvements address the capacity issue for the 8" sewer line in Scottsdale Road. It is proposed to re-route the west leg of the sewer to the 10" line in Palm Lane via a new manhole and leave the overflow pipe in place. The maximum d/D of 0.75 in the 8" line in Scottsdale Road will remain.



SOUTHDALE
7000 E. MCDOWELL ROAD, SCOTTSDALE, AZ 85257
FIGURE 1 - PROPOSED OVERALL SYSTEM EXHIBIT

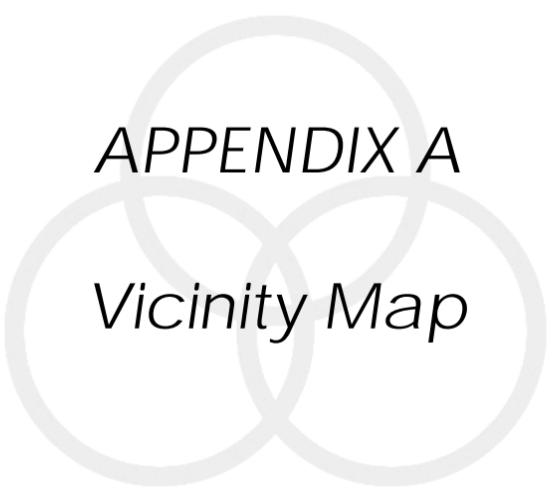
300engineering

3 ENGINEERING, LLC
6370 E. THOMAS ROAD
SUITE # 200
SCOTTSDALE, ARIZONA 85251
PHONE: (602) 334-4387
FAX: (602) 490-3230
WWW.3ENGINEERING.COM

DATE: 06/26/20

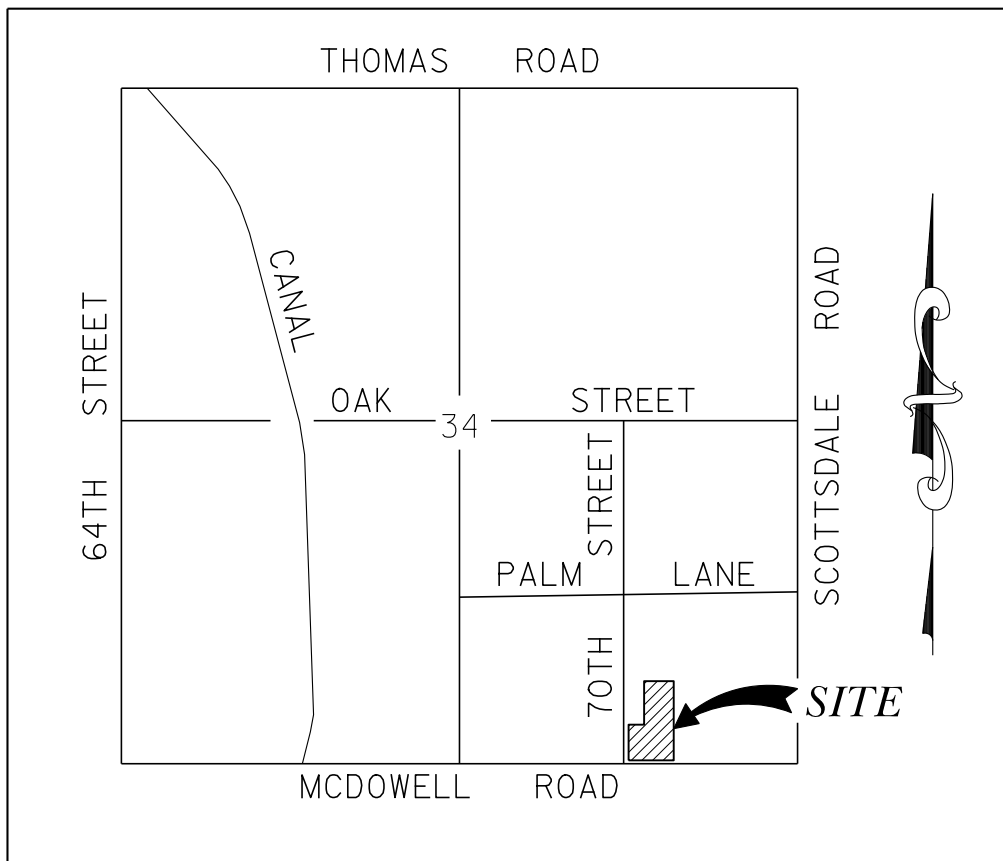
PROJECT NO.
1070

SHEET NO.
1 of 1



APPENDIX A

Vicinity Map



VICINITY MAP

N.T.S.

APPENDIX B

Flow Test Results



Flow Study for 3 Engineering Project: 726-PA-2019 (District at 7000 E. McDowell)

Dan Man

3 Engineering

9379 E. San Salvador Dr. Scottsdale, Arizona • 85258

SL727 RDH Flow Study, 2 sites in Scottsdale, AZ Friday, 1-25-20 to Sunday 2-2-20.

Equipment for Both Sites: Hach 901 Logger with Flo-Dar sensor.

The equipment was installed on 1-24-20 with confined space entry, pipe size confirmed, sensor calibrated and level depth confirmed to the flow level at that time.

Duration of monitoring: 9 days over 2 weekends.

Monitor: Flow (gpm), Level (in), and Velocity (fps)

Data logging: 5 minutes intervals (No averaged intervals)

Site 1: Manhole on Palm Lane just East of 71st Street and West of Scottsdale Rd.

Quarter section: 13-44

Manhole: #31

8" VCP

Flo-Dar sensor installed downstream on the 8" line (due to collecting data from 3 flows)

There was no buildup in the pipe.

All data is good with no sensor interference from debris.

Attached is the excel sheet showing all Level, Velocity and Flow using the Manning equation within the loggers. Below are the data summaries for Site 1:

3 Engineering MH31 Level (in.)				3 Engineering MH31 Velocity (fps)			
Date	Maximum	Minimum	Average	Date	Maximum	Minimum	Average
1/25/2020	4.516	1.670	2.968	1/25/2020	2.048	1.024	1.623
1/26/2020	4.467	1.670	3.077	1/26/2020	2.236	0.969	1.652
1/27/2020	4.101	1.609	2.919	1/27/2020	2.242	0.968	1.663
1/28/2020	4.346	1.664	2.973	1/28/2020	2.225	0.950	1.721
1/29/2020	4.161	1.556	2.942	1/29/2020	2.206	0.991	1.663
1/30/2020	4.448	1.822	3.107	1/30/2020	2.360	1.110	1.713
1/31/2020	4.645	2.279	3.455	1/31/2020	2.466	1.344	1.920
2/1/2020	4.650	2.459	3.585	2/1/2020	2.315	1.181	1.896
2/2/2020	4.860	2.312	3.610	2/2/2020	2.340	1.194	1.869



Flow Study for 3 Engineering Project: 726-PA-2019 (District at 7000 E. McDowell)

3 Engineering MH31 Flow (gpm)			
Date	Maximum	Minimum	Average
1/25/2020	166.794	26.290	90.416
1/26/2020	185.594	23.660	97.869
1/27/2020	181.243	22.000	91.283
1/28/2020	177.327	22.400	96.150
1/29/2020	164.073	22.067	91.924
1/30/2020	186.510	30.502	101.115
1/31/2020	200.695	50.721	126.505
2/1/2020	218.699	52.181	130.384
2/2/2020	206.784	46.251	131.618

Period Summary		
Measures	Value	Unit
Max. Total Flow	314,900	gpd
Min. Total Flow	31,700	gpd
Avg. Total Flow	153,200	gpd
Total Flow	1,378,461.1	gal

RDH Environmental Services

Theresa Hayes

General Manager

gm@rdh-env.com



Flow Study for 3 Engineering Project: 726-PA-2019 (District at 7000 E. McDowell)

Dan Man

3 Engineering

9379 E. San Salvador Dr. Scottsdale, Arizona • 85258

SL727 RDH Flow Study, 2 sites in Scottsdale, AZ Friday, 1-25-20 to Sunday 2-2-20.

Equipment for Both Sites: Hach 901 Logger with Flo-Dar sensor.

The equipment was installed on 1-24-20 with confined space entry, pipe size confirmed, sensor calibrated and level depth confirmed to the flow level at that time.

Duration of monitoring: 9 days over 2 weekends.

Monitor: Flow (gpm), Level (in), and Velocity (fps)

Data logging: 5 minutes intervals (No averaged intervals)

Site 2: Manhole on Palm Lane between 71st Street and Scottsdale Rd.

Quarter section: 13-44

Manhole: #48

10" VCP

Flo-Dar sensor installed upstream on the 10" line

There was no buildup in the pipe.

All data is good with no sensor interference from debris.

Attached is the excel sheet showing all Level, Velocity and Flow using the Manning equation within the loggers. Below are the data summaries for Site 2:

3 Engineering MH48 Level (in.)				3 Engineering MH48 Velocity (fps)			
Date	Maximum	Minimum	Average	Date	Maximum	Minimum	Average
1/25/2020	0.559	0.156	0.317	1/25/2020	1.420	0.765	1.063
1/26/2020	0.583	0.134	0.322	1/26/2020	1.554	0.697	1.058
1/27/2020	0.505	0.199	0.340	1/27/2020	1.521	0.730	1.063
1/28/2020	0.541	0.157	0.330	1/28/2020	1.521	0.659	1.087
1/29/2020	0.524	0.151	0.310	1/29/2020	1.390	0.795	1.070
1/30/2020	0.639	0.178	0.385	1/30/2020	1.506	0.813	1.118
1/31/2020	0.681	0.257	0.392	1/31/2020	1.497	0.835	1.138
2/1/2020	0.759	0.156	0.392	2/1/2020	1.641	0.780	1.169
2/2/2020	0.718	0.168	0.419	2/2/2020	1.556	0.826	1.183



Flow Study for 3 Engineering Project: 726-PA-2019 (District at 7000 E. McDowell)

3 Engineering MH48 Flow (gpm)			
Date	Maximum	Minimum	Average
1/25/2020	6.251	0.759	2.591
1/26/2020	7.116	0.522	2.718
1/27/2020	6.533	0.860	2.831
1/28/2020	6.934	0.706	2.814
1/29/2020	6.403	0.655	2.557
1/30/2020	9.435	0.800	3.708
1/31/2020	10.650	1.475	3.765
2/1/2020	13.172	0.819	4.152
2/2/2020	11.721	0.774	4.619

Period Summary		
Measures	Value	Unit
Max. Total Flow	19,000	gpd
Min. Total Flow	800	gpd
Avg. Total Flow	4,800	gpd
Total Flow	42,833.1	gal

RDH Environmental Services

Theresa Hayes,

General Manager

gm@rdh-env.com



APPENDIX C
System Leg Exhibit



14-43

14-44

West Leg
South Leg

12-43

12-44

17-DR-2021
5/6/2021

APPENDIX D

Apartment Segment FlowMaster Data

Cross Section for Existing Apartment Segment: 8" Sewer min slope

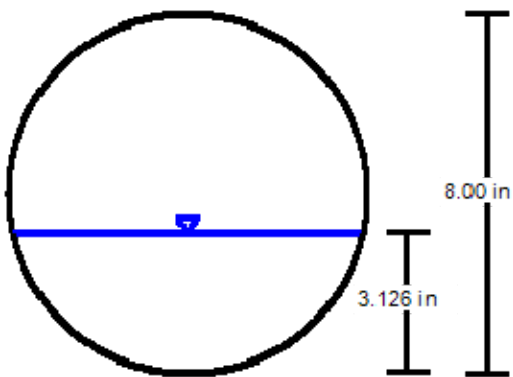
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.27000 %
Normal Depth	3.126 in
Diameter	8.00 in
Discharge	91.15 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Existing Apartment Segment: 8" Sewer min slope

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.27000	%
Diameter	8.00	in
Discharge	91.15	gpm

Results

Normal Depth	3.126	in
Flow Area	18.20	in ²
Wetted Perimeter	0.90	ft
Hydraulic Radius	1.684	in
Top Width	0.65	ft
Critical Depth	0.21	ft
Percent Full	39.1	%
Critical Slope	0.00640	ft/ft
Velocity	1.61	ft/s
Velocity Head	0.04	ft
Specific Energy	0.30	ft
Froude Number	0.64	
Maximum Discharge	0.68	ft ³ /s
Discharge Full	0.63	ft ³ /s
Slope Full	0.00028	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	39.08	%
Downstream Velocity	Infinity	ft/s

Worksheet for Existing Apartment Segment: 8" Sewer min slope

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	3.126	in
Critical Depth	0.21	ft
Channel Slope	0.27000	%
Critical Slope	0.00640	ft/ft

Cross Section for Apartment Segment: 8" Sewer min slope w/ Prop.

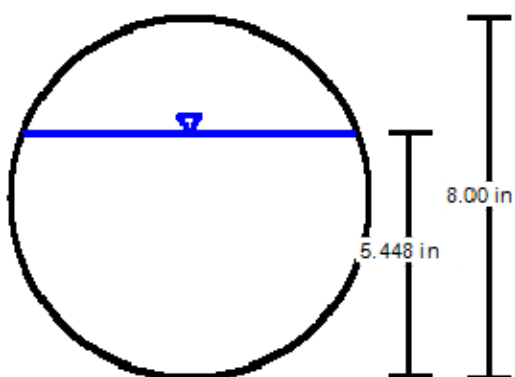
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.27000 %
Normal Depth	5.448 in
Diameter	8.00 in
Discharge	227.27 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Apartment Segment: 8" Sewer min slope w/ Prop. Flow

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.27000	%
Diameter	8.00	in
Discharge	227.27	gpm

Results

Normal Depth	5.448	in
Flow Area	36.46	in ²
Wetted Perimeter	1.29	ft
Hydraulic Radius	2.348	in
Top Width	0.62	ft
Critical Depth	0.33	ft
Percent Full	68.1	%
Critical Slope	0.00702	ft/ft
Velocity	2.00	ft/s
Velocity Head	0.06	ft
Specific Energy	0.52	ft
Froude Number	0.55	
Maximum Discharge	0.68	ft ³ /s
Discharge Full	0.63	ft ³ /s
Slope Full	0.00176	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	68.10	%
Downstream Velocity	Infinity	ft/s

Worksheet for Apartment Segment: 8" Sewer min slope w/ Prop. Flow

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	5.448	in
Critical Depth	0.33	ft
Channel Slope	0.27000	%
Critical Slope	0.00702	ft/ft

APPENDIX E

Existing Sewer FlowMaster Data

Cross Section for Existing: 8" Sewer Palm Lane Overflow to Weir

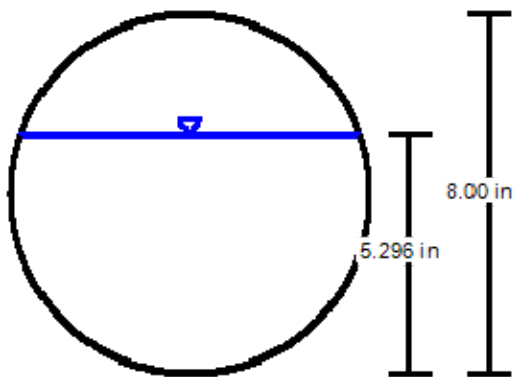
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.27000 %
Normal Depth	5.296 in
Diameter	8.00 in
Discharge	218.69 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Existing: 8" Sewer Palm Lane Overflow to Weir

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.27000	%
Diameter	8.00	in
Discharge	218.69	gpm

Results

Normal Depth	5.296	in
Flow Area	35.32	in ²
Wetted Perimeter	1.27	ft
Hydraulic Radius	2.323	in
Top Width	0.63	ft
Critical Depth	0.33	ft
Percent Full	66.2	%
Critical Slope	0.00697	ft/ft
Velocity	1.99	ft/s
Velocity Head	0.06	ft
Specific Energy	0.50	ft
Froude Number	0.56	
Maximum Discharge	0.68	ft ³ /s
Discharge Full	0.63	ft ³ /s
Slope Full	0.00163	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	66.20	%
Downstream Velocity	Infinity	ft/s

Worksheet for Existing: 8" Sewer Palm Lane Overflow to Weir

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	5.296	in
Critical Depth	0.33	ft
Channel Slope	0.27000	%
Critical Slope	0.00697	ft/ft

Cross Section for Existing: Rectangular Weir Overflow NW

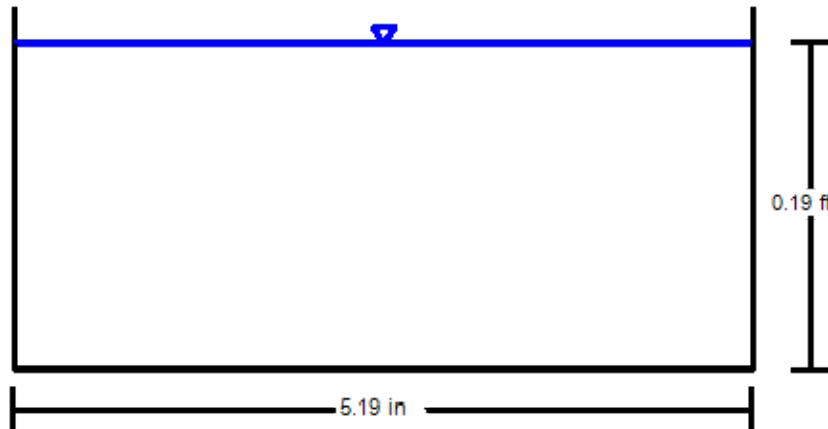
Project Description

Solve For Discharge

Input Data

Discharge	48.74	gpm
Headwater Elevation	2.296	in
Crest Elevation	0.00	in
Tailwater Elevation	0.00	in
Weir Coefficient	3.00	US
Crest Length	5.19	in
Number Of Contractions	0	

Cross Section Image



V: 1
H: 1

Worksheet for Existing: Rectangular Weir Overflow NW

Project Description

Solve For Discharge

Input Data

Headwater Elevation	2.296	in
Crest Elevation	0.00	in
Tailwater Elevation	0.00	in
Weir Coefficient	3.00	US
Crest Length	5.19	in
Number Of Contractions	0	

Results

Discharge	48.74	gpm
Headwater Height Above Crest	0.19	ft
Tailwater Height Above Crest	0.00	ft
Flow Area	11.92	in ²
Velocity	1.31	ft/s
Wetted Perimeter	0.82	ft
Top Width	0.43	ft

Cross Section for Existing: 8" Sewer Palm Lane

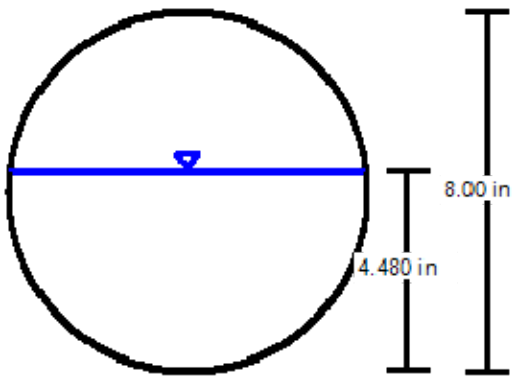
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.27000 %
Normal Depth	4.480 in
Diameter	8.00 in
Discharge	169.95 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Existing: 8" Sewer Palm Lane

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.27000	%
Diameter	8.00	in
Discharge	169.95	gpm

Results

Normal Depth	4.480	in
Flow Area	28.97	in ²
Wetted Perimeter	1.13	ft
Hydraulic Radius	2.141	in
Top Width	0.66	ft
Critical Depth	0.29	ft
Percent Full	56.0	%
Critical Slope	0.00669	ft/ft
Velocity	1.88	ft/s
Velocity Head	0.06	ft
Specific Energy	0.43	ft
Froude Number	0.60	
Maximum Discharge	0.68	ft ³ /s
Discharge Full	0.63	ft ³ /s
Slope Full	0.00098	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	56.01	%
Downstream Velocity	Infinity	ft/s

Worksheet for Existing: 8" Sewer Palm Lane

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	4.480	in
Critical Depth	0.29	ft
Channel Slope	0.27000	%
Critical Slope	0.00669	ft/ft

Cross Section for Existing: 10" Sewer Palm

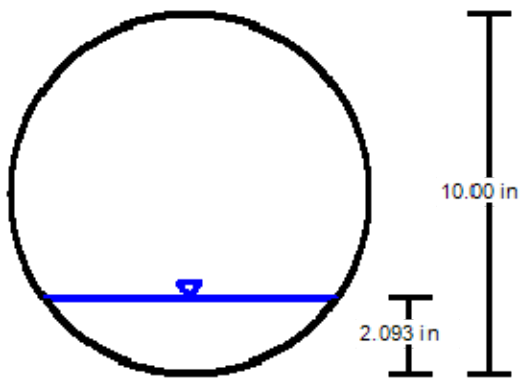
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.43000 %
Normal Depth	2.093 in
Diameter	10.00 in
Discharge	61.91 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Existing: 10" Sewer Palm

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.43000	%
Diameter	10.00	in
Discharge	61.91	gpm

Results

Normal Depth	2.093	in
Flow Area	11.93	in ²
Wetted Perimeter	0.79	ft
Hydraulic Radius	1.256	in
Top Width	0.68	ft
Critical Depth	0.16	ft
Percent Full	20.9	%
Critical Slope	0.00621	ft/ft
Velocity	1.66	ft/s
Velocity Head	0.04	ft
Specific Energy	0.22	ft
Froude Number	0.84	
Maximum Discharge	1.55	ft ³ /s
Discharge Full	1.44	ft ³ /s
Slope Full	0.00004	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	20.93	%
Downstream Velocity	Infinity	ft/s

Worksheet for Existing: 10" Sewer Palm

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	2.093	in
Critical Depth	0.16	ft
Channel Slope	0.43000	%
Critical Slope	0.00621	ft/ft

Cross Section for Existing: 8" Sewer Scottsdale Road

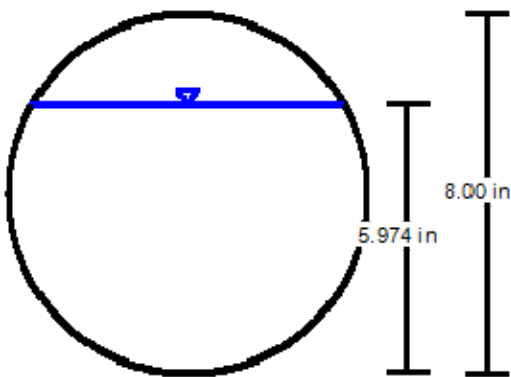
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.19000 %
Normal Depth	5.974 in
Diameter	8.00 in
Discharge	214.41 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Existing: 8" Sewer Scottsdale Road

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.19000	%
Diameter	8.00	in
Discharge	214.41	gpm

Results

Normal Depth	5.974	in
Flow Area	40.26	in ²
Wetted Perimeter	1.39	ft
Hydraulic Radius	2.411	in
Top Width	0.58	ft
Critical Depth	0.32	ft
Percent Full	74.7	%
Critical Slope	0.00694	ft/ft
Velocity	1.71	ft/s
Velocity Head	0.05	ft
Specific Energy	0.54	ft
Froude Number	0.43	
Maximum Discharge	0.57	ft ³ /s
Discharge Full	0.53	ft ³ /s
Slope Full	0.00156	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	74.67	%
Downstream Velocity	Infinity	ft/s

Worksheet for Existing: 8" Sewer Scottsdale Road

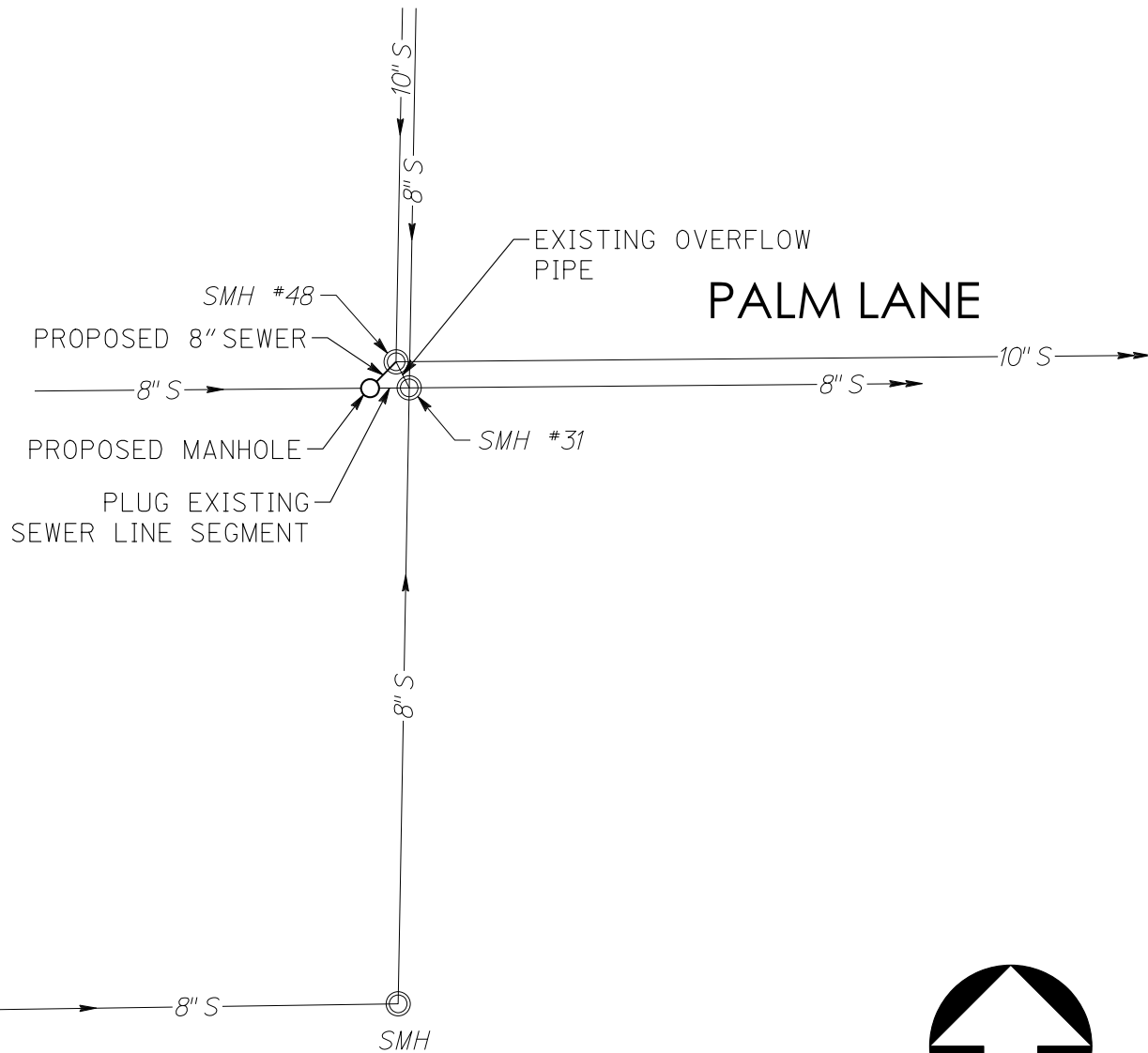
GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	5.974	in
Critical Depth	0.32	ft
Channel Slope	0.19000	%
Critical Slope	0.00694	ft/ft

APPENDIX F

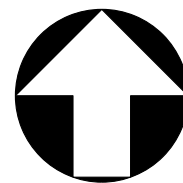
Proposed Sewer FlowMaster Data

71ST STREET

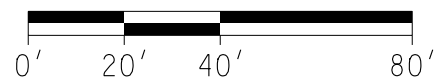


PALM LANE

SCOTTSDALE ROAD



SCALE: 1" = 40'



PROPOSED MANHOLE EXHIBIT

SOUTHDALE

3eengineering
planning civil engineering surveying

3 ENGINEERING, LLC
6370 E. THOMAS ROAD, SUITE # 200 - SCOTTSDALE, ARIZONA 85251
PHONE: (602) 334-4387 - FAX: (602) 490-3230
WWW.3ENGINEERING.COM

DATE:	PROJECT NO.
06/26/20	1872

17-DR-2021

5/6/2021

Cross Section for Proposed: 8" Sewer Palm Lane Overflow to Weir

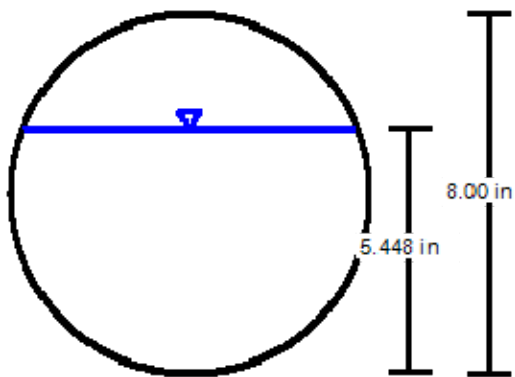
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.27000 %
Normal Depth	5.448 in
Diameter	8.00 in
Discharge	227.27 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Proposed: 8" Sewer Palm Lane Overflow to Weir

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.27000	%
Diameter	8.00	in
Discharge	227.27	gpm

Results

Normal Depth	5.448	in
Flow Area	36.46	in ²
Wetted Perimeter	1.29	ft
Hydraulic Radius	2.348	in
Top Width	0.62	ft
Critical Depth	0.33	ft
Percent Full	68.1	%
Critical Slope	0.00702	ft/ft
Velocity	2.00	ft/s
Velocity Head	0.06	ft
Specific Energy	0.52	ft
Froude Number	0.55	
Maximum Discharge	0.68	ft ³ /s
Discharge Full	0.63	ft ³ /s
Slope Full	0.00176	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	68.10	%
Downstream Velocity	Infinity	ft/s

Worksheet for Proposed: 8" Sewer Palm Lane Overflow to Weir

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	5.448	in
Critical Depth	0.33	ft
Channel Slope	0.27000	%
Critical Slope	0.00702	ft/ft

Cross Section for Proposed: Rectangular Weir Overflow NW

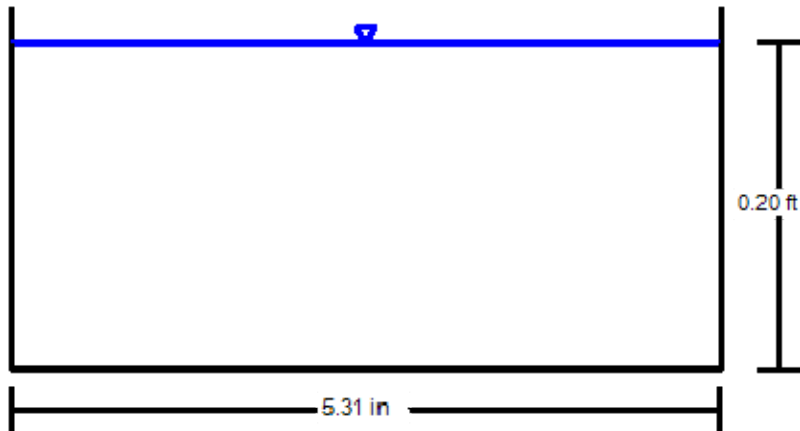
Project Description

Solve For Discharge

Input Data

Discharge	54.90	gpm
Headwater Elevation	2.448	in
Crest Elevation	0.00	in
Tailwater Elevation	0.00	in
Weir Coefficient	3.00	US
Crest Length	5.31	in
Number Of Contractions	0	

Cross Section Image



V: 1
H: 1

Worksheet for Proposed: Rectangular Weir Overflow NW

Project Description

Solve For Discharge

Input Data

Headwater Elevation	2.448	in
Crest Elevation	0.00	in
Tailwater Elevation	0.00	in
Weir Coefficient	3.00	US
Crest Length	5.31	in
Number Of Contractions	0	

Results

Discharge	54.90	gpm
Headwater Height Above Crest	0.20	ft
Tailwater Height Above Crest	0.00	ft
Flow Area	13.00	in ²
Velocity	1.35	ft/s
Wetted Perimeter	0.85	ft
Top Width	0.44	ft

Cross Section for Proposed: 8" Sewer Palm Lane

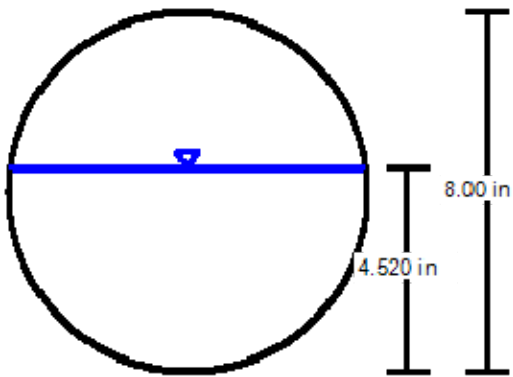
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.27000 %
Normal Depth	4.520 in
Diameter	8.00 in
Discharge	172.37 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Proposed: 8" Sewer Palm Lane

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.27000	%
Diameter	8.00	in
Discharge	172.37	gpm

Results

Normal Depth	4.520	in
Flow Area	29.28	in ²
Wetted Perimeter	1.13	ft
Hydraulic Radius	2.152	in
Top Width	0.66	ft
Critical Depth	0.29	ft
Percent Full	56.5	%
Critical Slope	0.00670	ft/ft
Velocity	1.89	ft/s
Velocity Head	0.06	ft
Specific Energy	0.43	ft
Froude Number	0.60	
Maximum Discharge	0.68	ft ³ /s
Discharge Full	0.63	ft ³ /s
Slope Full	0.00101	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	56.50	%
Downstream Velocity	Infinity	ft/s

Worksheet for Proposed: 8" Sewer Palm Lane

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	4.520	in
Critical Depth	0.29	ft
Channel Slope	0.27000	%
Critical Slope	0.00670	ft/ft

Cross Section for Proposed: 10" Sewer Palm

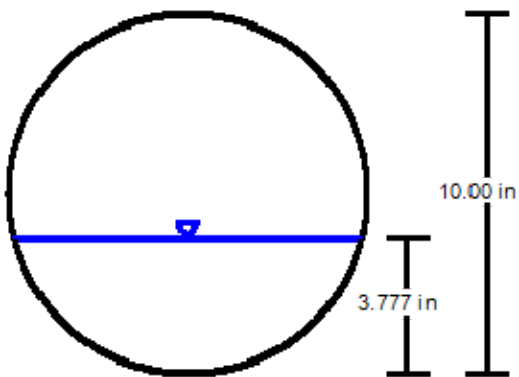
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.43000 %
Normal Depth	3.777 in
Diameter	10.00 in
Discharge	195.61 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Proposed: 10" Sewer Palm

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.43000	%
Diameter	10.00	in
Discharge	195.61	gpm

Results

Normal Depth	3.777	in
Flow Area	27.17	in ²
Wetted Perimeter	1.10	ft
Hydraulic Radius	2.052	in
Top Width	0.81	ft
Critical Depth	0.29	ft
Percent Full	37.8	%
Critical Slope	0.00600	ft/ft
Velocity	2.31	ft/s
Velocity Head	0.08	ft
Specific Energy	0.40	ft
Froude Number	0.84	
Maximum Discharge	1.55	ft ³ /s
Discharge Full	1.44	ft ³ /s
Slope Full	0.00040	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	37.77	%
Downstream Velocity	Infinity	ft/s

Worksheet for Proposed: 10" Sewer Palm

GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	3.777	in
Critical Depth	0.29	ft
Channel Slope	0.43000	%
Critical Slope	0.00600	ft/ft

Cross Section for Proposed: 8" Sewer Scottsdale Road

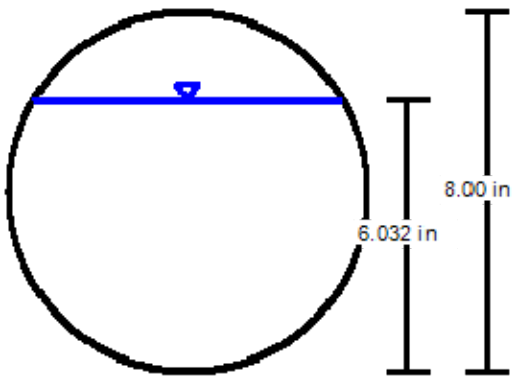
Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013
Channel Slope	0.19000 %
Normal Depth	6.032 in
Diameter	8.00 in
Discharge	216.83 gpm

Cross Section Image



V: 1
H: 1

Worksheet for Proposed: 8" Sewer Scottsdale Road

Project Description

Friction Method	Manning Formula
Solve For	Normal Depth

Input Data

Roughness Coefficient	0.013	
Channel Slope	0.19000	%
Diameter	8.00	in
Discharge	216.83	gpm

Results

Normal Depth	6.032	in
Flow Area	40.66	in ²
Wetted Perimeter	1.40	ft
Hydraulic Radius	2.416	in
Top Width	0.57	ft
Critical Depth	0.33	ft
Percent Full	75.4	%
Critical Slope	0.00696	ft/ft
Velocity	1.71	ft/s
Velocity Head	0.05	ft
Specific Energy	0.55	ft
Froude Number	0.43	
Maximum Discharge	0.57	ft ³ /s
Discharge Full	0.53	ft ³ /s
Slope Full	0.00160	ft/ft
Flow Type	SubCritical	

GVF Input Data

Downstream Depth	0.000	in
Length	0.00	ft
Number Of Steps	0	

GVF Output Data

Upstream Depth	0.000	in
Profile Description		
Profile Headloss	0.00	ft
Average End Depth Over Rise	0.00	%
Normal Depth Over Rise	75.40	%
Downstream Velocity	Infinity	ft/s

Worksheet for Proposed: 8" Sewer Scottsdale Road

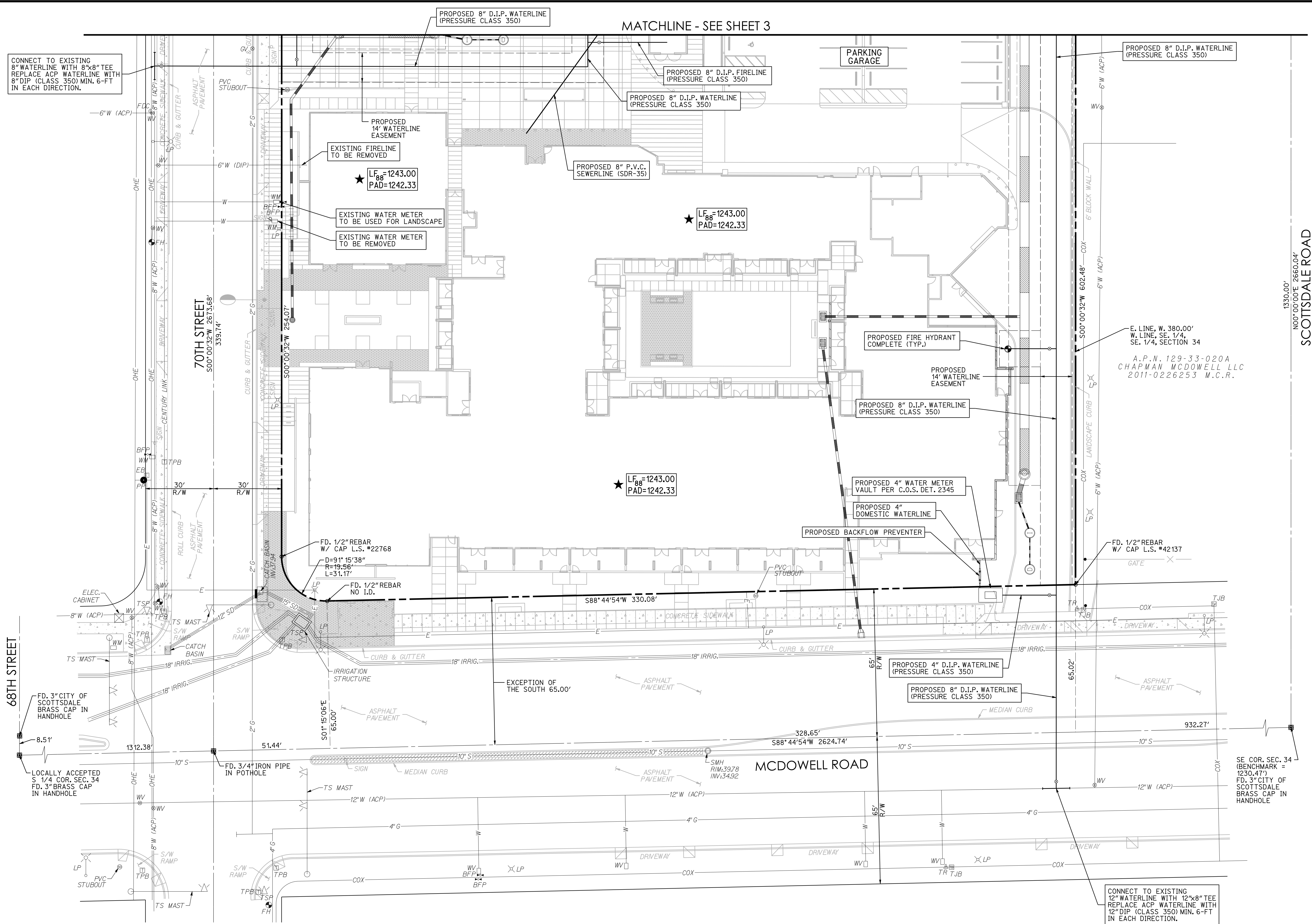
GVF Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	6.032	in
Critical Depth	0.33	ft
Channel Slope	0.19000	%
Critical Slope	0.00696	ft/ft

APPENDIX G

Preliminary Onsite Utility Plans

C:\WV\SecurSync\Projects\1872_70th_SJ_McDowell_Apartments\1872p0102.dgn



Contact Arizona 811 at least two full working days before you begin excavation.
Arizona 811
Call 811 or click Arizona811.com

SOUTHDALE
7000 E. MCDOWELL ROAD, SCOTTSDALE, AZ 85257
PRELIMINARY UTILITY PLAN



3eengineering
civil engineering
planning
surveying
DESIGNED: D. MANN
CHECKED: D. MANN
DATE: 04/26/21
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DATE: 04/26/21
PROJECT NO.
1872
SHEET NO.
PUTL202
2 of 3

Q.S.# 13-44

5/6/2021

