



SOUTHDALE

Final Wastewater Basis of Design Report

3 engineering Job #: 1872

April 23, 2021



# **SOUTHDALE**

# FINAL WASTEWATER BASIS OF DESIGN REPORT

#### Prepared for:

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April 23, 2021

#### Submittal to:

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Job Number 1872



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#### 1. Introduction

The project site, Southdale, is located in the southeast quarter of Section 34, Township 2 North, Range 4 East of the Gila and Salt River Meridian, Maricopa County, Arizona within the City of Scottsdale. The project is located on the northeast corner of 70<sup>th</sup> Street and McDowell Road. The site is bounded on the north by an apartment complex, on the east by a commercial development, on the south by McDowell Road, and on the west by 70<sup>th</sup> Street. See Appendix A for a vicinity map.

The existing zoning is C-3. The land is currently used as a commercial development. The General Plan shows the site as a Mixed-Use Neighborhood. The proposed zoning is PUD. The site is a proposed 267-unit apartment complex with office and retail space.

#### 2. Design Documentation

The purpose of this Wastewater Basis of Design Report is to verify that the existing City of Scottsdale sewer system is able to accommodate demands generated by the proposed project, Southdale. FlowMaster V8i by Bentley Systems was used to model and analyze the existing sewer system downstream of the site to verify it has capacity for the existing flow plus the flows generated from the proposed site, Southdale. Modeling was performed in compliance with the City of Scottsdale design requirements.

The existing flow in the system was tested at two manholes in Palm Lane, downstream of the site. The tests were performed by RDH Environmental Services on 1/25/2020 through 2/2/2020. See results in Appendix B.

Demands for the proposed site were calculated using Section 7-1.403A of the City of Scottsdale 2018 Design Standards and Policies Manual. It is our opinion that this report is in accordance with the 2018 City of Scottsdale Design Standards and Policies Manual.

#### 3. Existing Conditions

The existing zoning is C-3. The existing land is a commercial development. See Appendix A for a vicinity map. The site is surrounded by existing multi-family residential development and commercial development. There is an existing 8" V.C.P. sewer line in the apartment complex north of the site that will be utilized by the proposed development. This sewer line flows north to an 8" V.C.P. sewer line in Palm Lane at City of Scottsdale Manhole #31. This manhole has an overflow pipe that is conveyed to Manhole #48, which outlets to a 10" sewer line in Palm Lane. The 8" sewer line in Palm Lane flows to an 8" V.C.P. sewer line in Scottsdale Road, that flows south. The 10" sewer line in Palm lane flows to an 18" V.C.P. sewer line in Scottsdale Road, that flows south. The 8" sewer line running through the apartment north of the site, the 8" and 10" sewer lines in Palm Lane and the 8" sewer line in Scottsdale Road will be analyzed to determine if they have capacity for the additional flow generated from the proposed project. See Figure 1 for existing sewer layout.

#### 4. Proposed Conditions

The project consists of a 267-unit apartment complex with 3,300 s.f. of office space and 2,200 s.f. of retail space on 3.83 acres. It is proposed that this project will tie into the existing 8" V.C.P. sewer line in the apartment complex north of the site. See Preliminary Onsite Utility Plans in Appendix G.



The proposed site includes one pool. The assumed instantaneous backwash rate of the pool is 100 gpm. The pool backwash will be captured by an equalization tank that is to be sized for up to four consecutive backwashes. The tank will have a metered flow of 5 gpm that outlets to the proposed sewer system.

#### 5. Computations

#### 5.1. Proposed Site Demand Calculations

The following demand criteria from the City of Scottsdale 2018 Design Standards and Policies Manual (DSPM) were used in determining the system demands for the proposed site.

- 1. 267 proposed units
- 2. 3.83 acre site (70 du/ac)
- 3. 1.7 persons per unit (Per DSPM, multifamily density exceeding 22 du/ac)
- 4. 100 gallons per person per day (Per DSPM, residential)
- 5. Peaking factor = 4 (Per DSPM, residential)
- 6. 3,300 s.f. proposed Office Space
- 7. 0.4 gpd/s.f. (Per DPSM, Office)
- 8. 2,200 s.f. proposed Retail Space
- 9. 0.5 gpd/s.f. (Per DSPM, Commercial/Retail)
- 10. Peaking factor = 3 (Per DSPM, Commercial/Retail, Office)
- 11. 5 gallons per minute per pool for backwash (assume 1 pool)

TABLE 1: ON-SITE SEWER DEMANDS			
Pool Backwash	5 gpm		
Avg. daily demand w/ pool backwash	38.20 gpm		
Design Flow Rate w/ pool backwash	136.12 gpm		

#### Residentail

Average daily demand: 267 units x 1.7 persons per unit x 100 gpd per person = 45,390 gpd = 45,390 gpd/1440 mpd = 31.52 gpm

Peak flow rate =  $4.0 \times 45,390 \text{ gpd} = 181,560 \text{ gpd}$ = 181,560 gpd/1440 mpd = 126.08 gpm

#### Office

Average daily demand: 3,300 s.f. x 0.4 gpd per s.f. = 1,320 gpd = 1,320 gpd/1440 mpd = 0.92 gpm

Peak flow rate =  $3.0 \times 1,320 \text{ gpd} = 3,960 \text{ gpd}$ = 3,960 gpd/1440 mpd = 2.75 gpm

#### Retail

Average daily demand: 2,200 s.f. x 0.5 gpd per s.f. = 1,100 gpd = 1,100 gpd/1440 mpd = 0.76 gpm

Peak flow rate =  $3.0 \times 1,100 \text{ gpd} = 3,300 \text{ gpd}$ = 3,300 gpd/1440 mpd = 2.29 gpm



#### Total

Average daily demand = 33.20 gpm Peak flow rate = 131.12 gpm

#### 5.2. Existing System Flows

The existing maximum flows for the sewer lines in Palm Lane were determined by the flow test performed 1/25/2020 through 2/2/2020. There is a maximum of 13.172 gpm exiting manhole #48 east to the 10" sewer line in Palm Lane and a maximum of 218.699 gpm exiting manhole #31 east to the 8" sewer line in Palm Lane. The data was logged in 5-minute intervals over 9 days, including two weekends. See Appendix B for flow test data.

Two legs contribute to manhole #31. The leg flowing from the south has 114 single family homes, 101 multi-family units, the Aire Townhome development and ultimately the proposed site. The leg flowing from the west has 349 single family homes, 114 multi-family units, and Tonalea elementary school with 500 students. The flows from the two legs are calculated below per the City of Scottsdale DSPM. See Appendix C for a map of the legs.

#### South Leg (Orange)

114 Single-family x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 79.16 gpm Aire townhomes: 80 units x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 55 gpm Aire townhomes pool backwash: 100 gpm 101 multi-family x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 70.12 gpm

Total Peak flow = 304.28 gpm

#### West Leg (Green)

349 Single-family x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 242.36 gpm 114 multi-family x 2.5 persons per unit x 100 gpd per person x 4.0 P.F. / 1440 = 79.16 gpm Tonalea elementary: 50 gpd per student x 500 students x 6.0 P.F. / 1440 = 104.17 gpm Total Peak flow = 425.69 gpm

The total calculated flow for this manhole is 729.97 gpm. The south leg accounts for 41.68% of the total flow and the west leg accounts for 58.32% of the total flow.

The proportion of the total flow for each leg is applied to the tested flow through manhole #31. From the observed test results, the south leg has a proportional flow of 91.15 gpm, and the west leg has a proportional flow of 127.54 gpm. The total flow is 218.69 gpm.

Analysis of the 8" V.C.P. sewer line in Scottsdale Road requires adding the peak flows from four downstream buildings that include: a chiropractor's office, Ace Hardware, Post Office, and Comerica Bank. The flows for the sites are calculated below per the City of Scottsdale DSPM.

Chiropractic: 2,135 sf x 0.4 gpd per sf x 3.0 P.F. / 1440 = 1.78 gpm Ace Hardware: 20,175 sf x 0.5 gpd per sf x 3.0 P.F. / 1440 = 21.02 gpm Post Office: 84,225 sf x 0.1 gpd per sf x 3.0 P.F. / 1440 = 17.55 gpm

Bank: 3,950 sf x 0.5 gpd per sf x 3.0 P.F. / 1440 = 4.11 gpm

Total Peak Flow = 44.46 gpm

#### 5.3. Sewer System Analysis

FlowMaster V8i by Bentley Systems was used to model and analyze the existing sewer system for compliance with the C.O.S. design requirements. The sewer lines were modeled with a Manning's n coefficient of 0.013. The sewer rims and inverts were surveyed by 3 engineering on

02/13/20 and 03/16/20. See Figure 1 for an overall system layout. In addition to analyzing the 8" sewer running through the apartment site, the system downstream will be analyzed to address the 8" sewer line in Scottsdale Road which does not have sufficient capacity for the additional flows from the proposed site in the existing configuration. The maximum allowable d/D for all pipes discussed is 0.75.

#### **Existing Sewer Line in Apartment**

The existing 8" sewer line running through the apartment complex north of the site was analyzed at the minimum surveyed slope of 0.27%. The existing flow in this segment is the 91.15 gpm from the south leg. The existing d/D is 0.39. See Appendix D for FlowMaster results of this pipe.

#### Existing Sewer Line in Apartment with Proposed Site

The existing 8" sewer line running through the apartment complex north of the site was analyzed at the minimum surveyed slope of 0.27%. The new flow includes the the 91.15 gpm from the south leg, plus the additional 136.12 gpm of flow from the proposed site for a total of 227.27 gpm. The proposed d/D is 0.68 in the existing line. See Appendix D for FlowMaster results of this pipe.

#### Existing Sewer System in Palm Lane and Scottsdale Road

In the existing condition, Manhole #31 in Palm lane, receives the 91.15 gpm from the south leg and the 127.54 gpm from the west leg. There is an existing overflow pipe elevated 3" above the downstream pipe in manhole #31 that flows into manhole #48. The overflow pipe was modeled as a weir using the resulting elevation when the total flow of 218.69 gpm enters the 8" pipe in Palm Lane. The overflow pipe conveys a flow of 48.74 gpm to the 10" line in Palm Lane. The results of the existing system analysis are discussed below and FlowMaster Data is included in Appendix E.

- The existing 10" sewer line in Palm Lane was analyzed at a minimum surveyed slope of 0.43%. The existing flow includes the 13.17 gpm from the flow test of manhole #48 plus the 48.74 gpm from the overflow pipe in manhole #31 for a total flow of 61.91 gpm. The existing d/D is 0.21.
- The existing 8" sewer line in Palm Lane was analyzed at a minimum surveyed slope of 0.27%. The existing flow includes the 169.95 gpm that bypasses the overflow pipe in manhole #31. The existing d/D is 0.56.
- The existing 8" sewer line in Scottsdale Road was analyzed at a minimum surveyed slope of 0.19%. The existing flow includes the 169.95 gpm from the 8" line in Palm Lane plus the 44.46 gpm from the buildings along Scottsdale Road for a total flow of 214.41 gpm. The existing d/D is 0.75.

<u>Proposed Sewer System in Palm Lane and Scottsdale Road with Proposed Site</u>
The proposed project, Southdale, generates 136.12 gpm of peak wastewater flow that is conveyed to manhole #31. In the existing configuration, the capacity of the 8" line in Scottsdale Road will be exceeded as the d/D is already 0.75 before the additional flows. The proposed plan is to divert more flow into the 10" line in Palm lane, which has excess capacity.

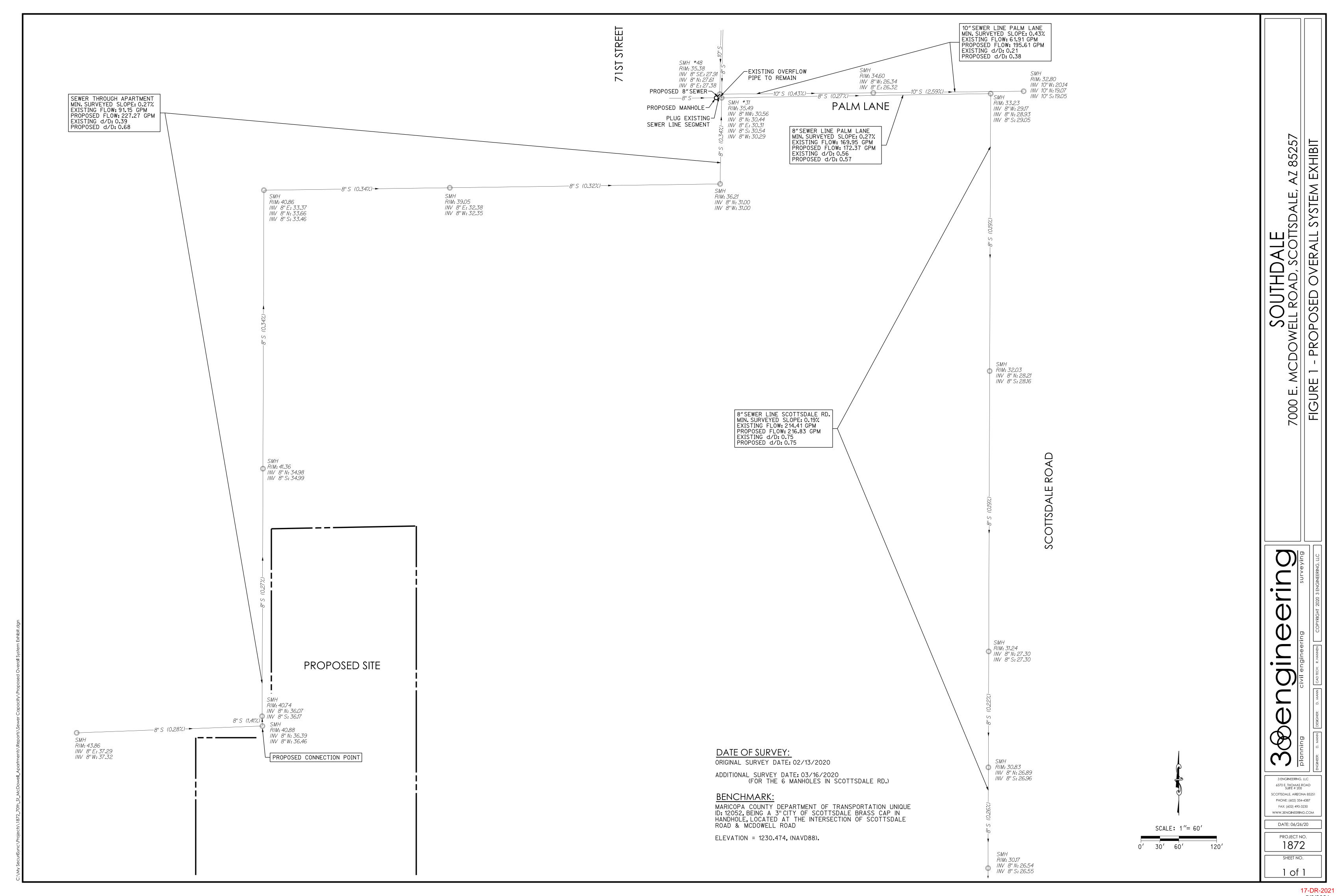
This will be achieved by adding a manhole in the west leg (green) and connecting the leg directly into manhole #48. The 10" line in Palm Lane will then receive the entire 127.54 gpm from the West leg. Manhole #31 in Palm lane will receive the existing 91.15 gpm from the South leg plus the additional 136.12 gpm from the proposed site for a total flow of 227.27 gpm. There is an existing overflow pipe elevated 3" above the downstream pipe in manhole #31 that flows into manhole #48. The overflow pipe will remain unchanged. With this flow, the overflow pipe conveys 54.90 gpm of the 227.27 gpm to manhole #48.

The results are discussed below. FlowMaster Data is included in Appendix F and shown in Figure 1 on the following page.

- The 10" sewer line in Palm Lane was analyzed at a minimum surveyed slope of 0.43%. The proposed flow includes the 127.54 gpm from the west leg plus the 13.17 gpm from the flow test of manhole #48 plus the 54.90 gpm from the overflow pipe in manhole #31 for a total flow of 195.61 gpm. The proposed d/D is 0.38.
- The 8" sewer line in Palm Lane was analyzed at a minimum surveyed slope of 0.27%. The proposed flow includes the 172.37 gpm from the south leg and proposed site that bypasses the overflow pipe. The proposed d/D is 0.57.
- The 8" sewer line in Scottsdale Road was analyzed at a minimum surveyed slope of 0.19%. The proposed flow includes the 172.37 gpm from the 8" line in Palm Lane plus 44.46 gpm from the buildings along Scottsdale Road for a total flow of 216.83 gpm. The proposed d/D is 0.75.

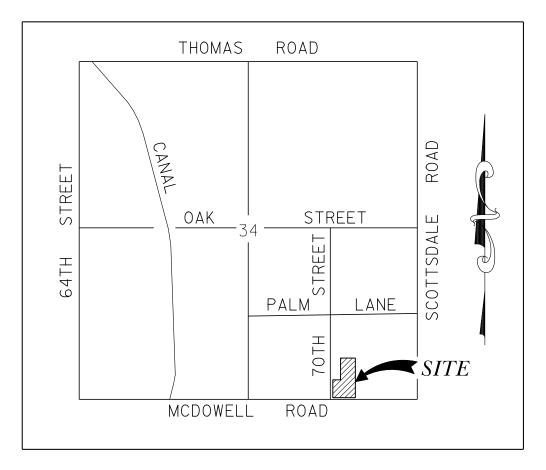
#### 6. Summary

The Peak Flow for the proposed site is 136.12 gpm. The site ties into an existing 8" sewer line, in the apartment complex north of the site, that has an existing flow of 91.15 gpm. The pipe has a proposed d/D of 0.68 with the additional flow from the proposed site. In the existing configuration, the 8" sewer line in Scottsdale Road is at capacity and cannot handle additional flow from the proposed site, Southdale. The proposed improvements address the capacity issue for the 8" sewer line in Scottsdale Road. It is proposed to re-route the west leg of the sewer to the 10" line in Palm Lane via a new manhole and leave the overflow pipe in place. The maximum d/D of 0.75 in the 8" line in Scottsdale Road will remain.





APPENDIX A
Vicinity Map



VICINITY MAP

N.T.S.



# APPENDIX B

Flow Test Results

5/6/2021



# Dan Man 3 Engineering

9379 E. San Salvador Dr. Scottsdale, Arizona • 85258

## SL727 RDH Flow Study, 2 sites in Scottsdale, AZ Friday, 1-25-20 to Sunday 2-2-20.

**Equipment for Both Sites:** Hach 901 Logger with Flo-Dar sensor.

The equipment was installed on 1-24-20 with confined space entry, pipe size confirmed, sensor calibrated and level depth confirmed to the flow level at that time.

Duration of monitoring: 9 days over 2 weekends. Monitor: Flow (gpm), Level (in), and Velocity (fps)

Data logging: 5 minutes intervals (No averaged intervals)

## Site 1: Manhole on Palm Lane just East of 71st Street and West of Scottsdale Rd.

Quarter section: 13-44

Manhole: #31 8" VCP

Flo-Dar sensor installed downstream on the 8" line (due to collecting data from 3 flows)

There was no buildup in the pipe.

All data is good with no sensor interference from debris.

Attached is the excel sheet showing all Level, Velocity and Flow using the Manning equation within the loggers. Below are the data summaries for Site 1:

3 Engineering MH31 Level (in.)					
Date	Maximum	Minimum	Average		
1/25/2020	4.516	1.670	2.968		
1/26/2020	4.467	1.670	3.077		
1/27/2020	4.101	1.609	2.919		
1/28/2020	4.346	1.664	2.973		
1/29/2020	4.161	1.556	2.942		
1/30/2020	4.448	1.822	3.107		
1/31/2020	4.645	2.279	3.455		
2/1/2020	4.650	2.459	3.585		
2/2/2020	4.860	2.312	3.610		

3 Engineering MH31 Velocity (fps)				
Date	Maximum	Minimum	Average	
1/25/2020	2.048	1.024	1.623	
1/26/2020	2.236	0.969	1.652	
1/27/2020	2.242	0.968	1.663	
1/28/2020	2.225	0.950	1.721	
1/29/2020	2.206	0.991	1.663	
1/30/2020	2.360	1.110	1.713	
1/31/2020	2.466	1.344	1.920	
2/1/2020	2.315	1.181	1.896	
2/2/2020	2.340	1.194	1.869	



3 Engineering MH31 Flow (gpm)				
Date	Maximum	Minimum	Average	
1/25/2020	166.794	26.290	90.416	
1/26/2020	185.594	23.660	97.869	
1/27/2020	181.243	22.000	91.283	
1/28/2020	177.327	22.400	96.150	
1/29/2020	164.073	22.067	91.924	
1/30/2020	186.510	30.502	101.115	
1/31/2020	200.695	50.721	126.505	
2/1/2020	218.699	52.181	130.384	
2/2/2020	206.784	46.251	131.618	

Period Summary				
Measures	Value	Unit		
Max. Total Flow	314,900	gpd		
Min. Total Flow	31,700	gpd		
Avg. Total Flow	153,200	gpd		
Total Flow	1,378,461.1	gal		

RDH Environmental Services Theresa Hayes General Manager gm@rdh-env.com



# Dan Man 3 Engineering

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## SL727 RDH Flow Study, 2 sites in Scottsdale, AZ Friday, 1-25-20 to Sunday 2-2-20.

Equipment for Both Sites: Hach 901 Logger with Flo-Dar sensor.

The equipment was installed on 1-24-20 with confined space entry, pipe size confirmed, sensor calibrated and level depth confirmed to the flow level at that time.

Duration of monitoring: 9 days over 2 weekends.

Monitor: Flow (gpm), Level (in), and Velocity (fps)

Data logging: 5 minutes intervals (No averaged intervals)

#### Site 2: Manhole on Palm Lane between 71st Street and Scottsdale Rd.

Quarter section: 13-44

Manhole: #48 10" VCP

Flo-Dar sensor installed upstream on the 10" line

There was no buildup in the pipe.

All data is good with no sensor interference from debris.

Attached is the excel sheet showing all Level, Velocity and Flow using the Manning equation within the loggers. Below are the data summaries for Site 2:

3 Engineering MH48 Level (in.)					
Date	Maximum	Minimum	Average		
1/25/2020	0.559	0.156	0.317		
1/26/2020	0.583	0.134	0.322		
1/27/2020	0.505	0.199	0.340		
1/28/2020	0.541	0.157	0.330		
1/29/2020	0.524	0.151	0.310		
1/30/2020	0.639	0.178	0.385		
1/31/2020	0.681	0.257	0.392		
2/1/2020	0.759	0.156	0.392		
2/2/2020	0.718	0.168	0.419		

3 Engineering MH48 Velocity (fps)				
Date	Maximum Minimum Ave		Average	
1/25/2020	1.420	0.765	1.063	
1/26/2020	1.554	0.697	1.058	
1/27/2020	1.521	0.730	1.063	
1/28/2020	1.521	0.659	1.087	
1/29/2020	1.390	0.795	1.070	
1/30/2020	1.506	0.813	1.118	
1/31/2020	1.497	0.835	1.138	
2/1/2020	1.641	0.780	1.169	
2/2/2020	1.556	0.826	1.183	



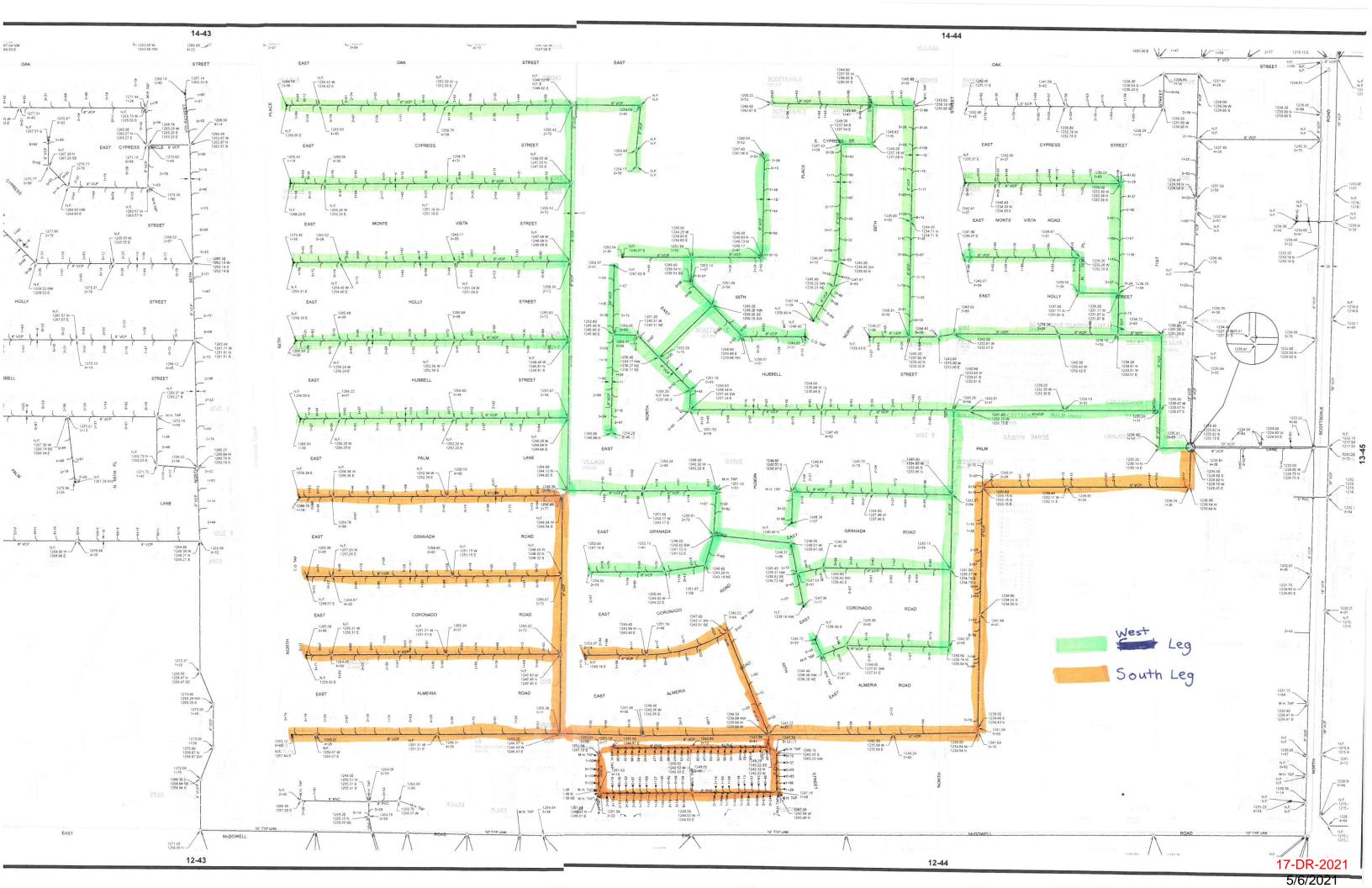
3 Engineering MH48 Flow (gpm)					
Date	Maximum	Minimum	Average		
1/25/2020	6.251	0.759	2.591		
1/26/2020	7.116	0.522	2.718		
1/27/2020	6.533	0.860	2.831		
1/28/2020	6.934	0.706	2.814		
1/29/2020	6.403	0.655	2.557		
1/30/2020	9.435	0.800	3.708		
1/31/2020	10.650	1.475	3.765		
2/1/2020	13.172	0.819	4.152		
2/2/2020	11.721	0.774	4.619		

Period Summary				
Measures	Value	Unit		
Max. Total Flow	19,000	gpd		
Min. Total Flow	800	gpd		
Avg. Total Flow	4,800	gpd		
Total Flow	42,833.1	gal		

RDH Environmental Services Theresa Hayes, General Manager gm@rdh-env.com



# APPENDIX C System Leg Exhibit





# APPENDIX D

Apartment Segment FlowMaster Data

# **Cross Section for Existing Apartment Segment: 8" Sewer min slope**

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

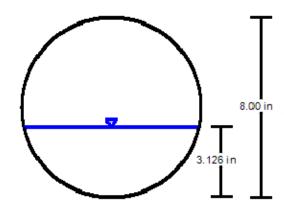
 Channel Slope
 0.27000
 %

 Normal Depth
 3.126
 in

 Diameter
 8.00
 in

 Discharge
 91.15
 gpm

#### Cross Section Image



V: 1 📐

# **Worksheet for Existing Apartment Segment: 8" Sewer min slope**

WOLKSHEET IOLE	- Alstilly Apai	inient Jegi	Hent. 6	Jewei	min stope	<u>-</u>
Project Description						
Friction Method	Manning Formula					
Solve For	Normal Depth					
	'					
Input Data						
Roughness Coefficient		0.013				
Channel Slope		0.27000	%			
Diameter		8.00	in			
Discharge		91.15	gpm			
Results						
Normal Depth		3.126	in			
Flow Area		18.20	in²			
Wetted Perimeter		0.90	ft			
Hydraulic Radius		1.684	in			
Top Width		0.65	ft			
Critical Depth		0.03	ft			
Percent Full		39.1	%			
Critical Slope		0.00640	ft/ft			
Velocity		1.61	ft/s			
Velocity Head		0.04	ft			
Specific Energy		0.30	ft			
Froude Number		0.64				
Maximum Discharge		0.68	ft³/s			
Discharge Full		0.63	ft³/s			
Slope Full		0.00028	ft/ft			
Flow Type	SubCritical					
GVF Input Data						
		0.000	in			
Downstream Depth Length			in ft			
Number Of Steps		0.00	IL			
GVF Output Data						
Upstream Depth		0.000	in			
Profile Description						
Profile Headloss		0.00	ft			
Average End Depth Over Rise		0.00	%			
Normal Depth Over Rise		39.08	%			
Downstream Velocity		Infinity	ft/s			

# Worksheet for Existing Apartment Segment: 8" Sewer min slope

## **GVF** Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 3.126
 in

 Critical Depth
 0.21
 ft

 Channel Slope
 0.27000
 %

 Critical Slope
 0.00640
 ft/ft

# Cross Section for Apartment Segment: 8" Sewer min slope w/ Prop.

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

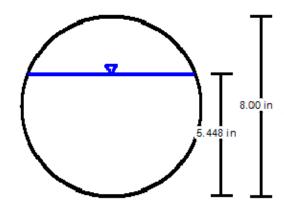
 Channel Slope
 0.27000
 %

 Normal Depth
 5.448
 in

 Diameter
 8.00
 in

 Discharge
 227.27
 gpm

#### **Cross Section Image**



V: 1 \( \bigcap\_{\text{H: 1}} \)

# Worksheet for Apartment Segment: 8" Sewer min slope w/ Prop. Flow

			<u> </u>
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.27000	%
Diameter		8.00	in
Discharge		227.27	gpm
Results			
Normal Depth		5.448	in
Flow Area		36.46	in²
Wetted Perimeter		1.29	ft
Hydraulic Radius		2.348	in
Top Width		0.62	ft
Critical Depth		0.33	ft
Percent Full		68.1	%
Critical Slope		0.00702	ft/ft
Velocity		2.00	ft/s
Velocity Head		0.06	ft
Specific Energy		0.52	ft
Froude Number		0.55	
Maximum Discharge		0.68	ft³/s
Discharge Full		0.63	ft³/s
Slope Full		0.00176	ft/ft
Flow Type	SubCritical		
GVF Input Data			
Downstream Depth		0.000	in
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.000	in
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%
Normal Depth Over Rise		68.10	%
Downstream Velocity		Infinity	ft/s

# Worksheet for Apartment Segment: 8" Sewer min slope w/ Prop. Flow

# **GVF** Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	5.448	in
Critical Depth	0.33	ft
Channel Slope	0.27000	%
Critical Slope	0.00702	ft/ft



# APPENDIX E

Existing Sewer FlowMaster Data

# Cross Section for Existing: 8" Sewer Palm Lane Overflow to Weir

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

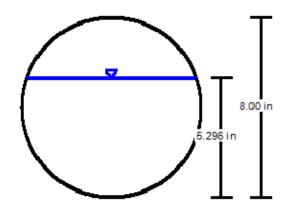
 Channel Slope
 0.27000
 %

 Normal Depth
 5.296
 in

 Diameter
 8.00
 in

 Discharge
 218.69
 gpm

#### **Cross Section Image**



V: 1 📐

# Worksheet for Existing: 8" Sewer Palm Lane Overflow to Weir

worksneet for	Existing. 0	JCWCI I all	n Lane Overnow	to wen
Project Description				
Friction Method	Manning Formula			
Solve For	Normal Depth			
Innut Data	·			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.27000	%	
Diameter		8.00	in	
Discharge		218.69	gpm	
Results				
Normal Depth		5.296	in	
Flow Area		35.32	in²	
Wetted Perimeter		1.27	ft	
Hydraulic Radius		2.323	in	
Top Width		0.63	ft	
Critical Depth		0.33	ft	
Percent Full		66.2	%	
Critical Slope		0.00697	ft/ft	
Velocity		1.99	ft/s	
Velocity Head		0.06	ft	
Specific Energy		0.50	ft	
Froude Number		0.56		
Maximum Discharge		0.68	ft³/s	
Discharge Full		0.63	ft³/s	
Slope Full		0.00163	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.000	in	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.000	in	
Profile Description		2.300		
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		66.20	%	
Downstream Velocity		Infinity	ft/s	
23iodiodiii volooity				

# Worksheet for Existing: 8" Sewer Palm Lane Overflow to Weir

## **GVF** Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 5.296
 in

 Critical Depth
 0.33
 ft

 Channel Slope
 0.27000
 %

 Critical Slope
 0.00697
 ft/ft

# **Cross Section for Existing: Rectangular Weir Overflow NW**

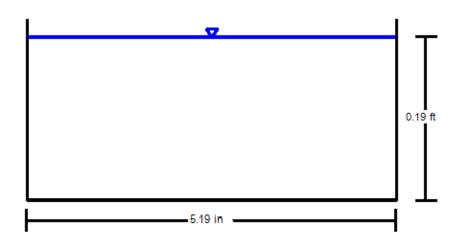
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Solve For Discharge

#### Input Data

Discharge		48.74	gpm
Headwater Elevation		2.296	in
Crest Elevation		0.00	in
Tailwater Elevation		0.00	in
Weir Coefficient		3.00	US
Crest Length		5.19	in
Number Of Contractions	0		

#### Cross Section Image



1 L

# Worksheet for Existing: Rectangular Weir Overflow NW

	ioi Exiotiiig.		
Project Description			
Solve For	Discharge		
Input Data			
Headwater Elevation		2.296	in
Crest Elevation		0.00	in
Tailwater Elevation		0.00	in
Weir Coefficient		3.00	US
Crest Length		5.19	in
Number Of Contractions	0		
Results			
Discharge		48.74	gpm
Headwater Height Above Crest		0.19	ft
Tailwater Height Above Crest		0.00	ft
Flow Area		11.92	in²
Velocity		1.31	ft/s
Wetted Perimeter		0.82	ft
Top Width		0.43	ft

# **Cross Section for Existing: 8" Sewer Palm Lane**

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

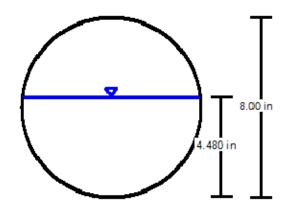
 Channel Slope
 0.27000
 %

 Normal Depth
 4.480
 in

 Diameter
 8.00
 in

 Discharge
 169.95
 gpm

#### Cross Section Image



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## Worksheet for Existing: 8" Sewer Palm Lane

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

 Channel Slope
 0.27000
 %

 Diameter
 8.00
 in

 Discharge
 169.95
 gpm

#### Results

Normal Depth 4.480 in Flow Area 28.97 in² Wetted Perimeter ft 1.13 Hydraulic Radius 2.141 in Top Width 0.66 ft Critical Depth 0.29 ft Percent Full 56.0 % Critical Slope 0.00669 ft/ft Velocity 1.88 ft/s 0.06 Velocity Head ft Specific Energy 0.43 ft Froude Number 0.60 Maximum Discharge 0.68 ft³/s Discharge Full 0.63 ft³/s Slope Full 0.00098 ft/ft SubCritical Flow Type

#### **GVF Input Data**

#### **GVF Output Data**

Upstream Depth

Profile Description

Profile Headloss 0.00 ft

Average End Depth Over Rise 0.00 %

Normal Depth Over Rise 56.01 %

Downstream Velocity Infinity ft/s

0.000

# Worksheet for Existing: 8" Sewer Palm Lane

#### **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 4.480
 in

 Critical Depth
 0.29
 ft

 Channel Slope
 0.27000
 %

 Critical Slope
 0.00669
 ft/ft

# **Cross Section for Existing: 10" Sewer Palm**

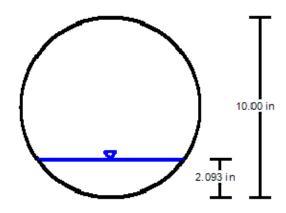
## **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.43000	%
Normal Depth	2.093	in
Diameter	10.00	in
Discharge	61.91	gpm

#### **Cross Section Image**



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## Worksheet for Existing: 10" Sewer Palm

Project	Description
---------	-------------

Friction Method Manning Formula Solve For Normal Depth

#### Input Data

0.013 Roughness Coefficient 0.43000 Channel Slope 10.00 Diameter in 61.91 Discharge gpm

#### Results

Normal Depth 2.093 in Flow Area 11.93 in² Wetted Perimeter ft 0.79 Hydraulic Radius 1.256 in Top Width 0.68 ft Critical Depth 0.16 ft Percent Full 20.9 % Critical Slope 0.00621 ft/ft Velocity 1.66 ft/s 0.04 Velocity Head ft Specific Energy 0.22 ft Froude Number 0.84 Maximum Discharge 1.55 ft³/s Discharge Full ft³/s 1.44 ft/ft Slope Full 0.00004 SubCritical Flow Type

#### **GVF Input Data**

Downstream Depth 0.000 in 0.00 Length ft 0 Number Of Steps

#### **GVF Output Data**

Upstream Depth Profile Description Profile Headloss 0.00 ft 0.00 Average End Depth Over Rise % Normal Depth Over Rise 20.93 % Infinity Downstream Velocity ft/s

> Bentley Systems, Inc. Haestad Methods Sollatidle CFitterMaster V8i (SELECTseries 1) [08.11.01.03] 27 Siemons Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2

0.000

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## **Worksheet for Existing: 10" Sewer Palm**

#### **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 2.093
 in

 Critical Depth
 0.16
 ft

 Channel Slope
 0.43000
 %

 Critical Slope
 0.00621
 ft/ft

## **Cross Section for Existing: 8" Sewer Scottsdale Road**

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

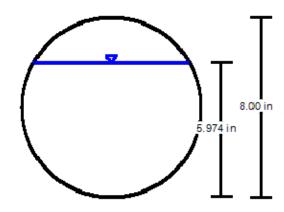
 Channel Slope
 0.19000
 %

 Normal Depth
 5.974
 in

 Diameter
 8.00
 in

 Discharge
 214.41
 gpm

#### **Cross Section Image**



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Friction Method Solve For Normal Depth    Input Data	Wo	orksheet for Existing: 8" Sewer Scottsdale Road
Normal Depth   Normal Depth   Normal Depth   Normal Depth   Normal Depth   Normal Depth   Normal Discharge   Normal Depth   Normal Depth	Project Description	
Input Data   Roughness Coefficient   0.013   Channel Slope   0.19000   %   Diameter   8.00   in   Discharge   214.41   gpm   Results	Friction Method	Manning Formula
Roughness Coefficient   0.013   Channel Slope   0.19000   %   Diameter   8.00   in   Discharge   214.41   gpm	Solve For	
Channel Slope         0.19000         %           Diameter         8.00         in           Discharge         214.41         gpm           Results           Normal Depth         5.974         in           Flow Area         40.26         in²           Wetted Perimeter         1.39         ft           Hydraulic Radius         2.411         in           Top Width         0.58         ft           Critical Depth         0.32         ft           Percent Full         74.7         %           Critical Slope         0.00694         ft/ft           Velocity         1.71         ft/s           Velocity Head         0.05         ft           Specific Energy         0.54         ft           Froude Number         0.43         Maximum Discharge           Discharge Full         0.53         ft/s           Slope Full         0.00156         ft/ft           Flow Type         SubCritical         SubCritical           GVF Input Data           Downstream Depth         0.00         ft           Length         0.00         ft           Norman Ar	Input Data	
Diameter   S.00   in   Discharge   214.41   gpm	Roughness Coefficient	0.013
Discharge   214.41 gpm	Channel Slope	0.19000 %
Normal Depth   5.974   in	Diameter	8.00 in
Normal Depth   5.974   in	Discharge	214.41 gpm
Flow Area	Results	
Wetted Perimeter       1.39 ft         Hydraulic Radius       2.411 in         Top Width       0.58 ft         Critical Depth       0.32 ft         Percent Full       74.7 %         Critical Slope       0.00694 ft/ft         Velocity       1.71 ft/s         Velocity Head       0.05 ft         Specific Energy       0.54 ft         Froude Number       0.43         Maximum Discharge       0.57 ft²/s         Discharge Full       0.53 ft²/s         Slope Full       0.00156 ft/ft         Flow Type       SubCritical         GVF Input Data       0.000 ft         Downstream Depth       0.000 ft         Length       0.00 ft         Number Of Steps       0	Normal Depth	5.974 in
Hydraulic Radius	Flow Area	40.26 in <sup>2</sup>
Top Width 0.58 ft Critical Depth 0.32 ft Percent Full 74.7 % Critical Slope 0.00694 ft/ft Velocity 1.71 ft/s Velocity Head 0.05 ft Specific Energy 0.54 ft Froude Number 0.43 Maximum Discharge 0.57 ft³/s Discharge Full 0.53 ft³/s Slope Full 0.00156 ft/ft Flow Type SubCritical  GVF Input Data  Downstream Depth 0.000 in Length 0.00 ft Number Of Steps 0	Wetted Perimeter	1.39 ft
Critical Depth       0.32       ft         Percent Full       74.7       %         Critical Slope       0.00694       ft/ft         Velocity       1.71       ft/s         Velocity Head       0.05       ft         Specific Energy       0.54       ft         Froude Number       0.43       ft*/s         Maximum Discharge       0.57       ft*/s         Discharge Full       0.53       ft*/s         Slope Full       0.00156       ft/ft         Flow Type       SubCritical         GVF Input Data         Downstream Depth       0.000       in         Length       0.00       ft         Number Of Steps       0	Hydraulic Radius	2.411 in
Percent Full 74.7 %  Critical Slope 0.00694 ft/ft  Velocity 1.71 ft/s  Velocity Head 0.05 ft  Specific Energy 0.54 ft  Froude Number 0.43  Maximum Discharge 0.57 ft*/s  Discharge Full 0.53 ft*/s  Slope Full 0.00156 ft/ft  Flow Type SubCritical  GVF Input Data  Downstream Depth 0.000 in  Length 0.000 ft  Number Of Steps 0	Top Width	0.58 ft
Critical Slope         0.00694         ft/ft           Velocity         1.71         ft/s           Velocity Head         0.05         ft           Specific Energy         0.54         ft           Froude Number         0.43         Maximum Discharge           Maximum Discharge         0.57         ft³/s           Discharge Full         0.53         ft³/s           Slope Full         0.00156         ft/ft           Flow Type         SubCritical         SubCritical           GVF Input Data         0.000         in           Length         0.000         ft           Number Of Steps         0         0	Critical Depth	0.32 ft
Velocity       1.71       ft/s         Velocity Head       0.05       ft         Specific Energy       0.54       ft         Froude Number       0.43       tt         Maximum Discharge       0.57       ft³/s         Discharge Full       0.53       ft³/s         Slope Full       0.00156       ft/ft         Flow Type       SubCritical         GVF Input Data         Downstream Depth       0.000       in         Length       0.00       ft         Number Of Steps       0	Percent Full	74.7 %
Velocity Head         0.05 ft           Specific Energy         0.54 ft           Froude Number         0.43           Maximum Discharge         0.57 ft³/s           Discharge Full         0.53 ft³/s           Slope Full         0.00156 ft/ft           Flow Type         SubCritical           GVF Input Data         0.000 in           Length         0.00 ft           Number Of Steps         0	Critical Slope	0.00694 ft/ft
Specific Energy         0.54         ft           Froude Number         0.43           Maximum Discharge         0.57         ft³/s           Discharge Full         0.53         ft³/s           Slope Full         0.00156         ft/ft           Flow Type         SubCritical           GVF Input Data         0.000         in           Length         0.00         ft           Number Of Steps         0         0	Velocity	1.71 ft/s
Froude Number	Velocity Head	0.05 ft
Maximum Discharge         0.57 ft³/s           Discharge Full         0.53 ft³/s           Slope Full         0.00156 ft/ft           Flow Type         SubCritical           GVF Input Data           Downstream Depth         0.000 in           Length         0.00 ft           Number Of Steps         0	Specific Energy	0.54 ft
Discharge Full 0.53 ft³/s  Slope Full 0.00156 ft/ft  Flow Type SubCritical   GVF Input Data  Downstream Depth 0.000 in  Length 0.00 ft  Number Of Steps 0	Froude Number	0.43
Slope Full 0.00156 ft/ft Flow Type SubCritical  GVF Input Data  Downstream Depth 0.000 in  Length 0.00 ft  Number Of Steps 0	Maximum Discharge	0.57 ft³/s
Flow Type SubCritical  GVF Input Data  Downstream Depth 0.000 in  Length 0.00 ft  Number Of Steps 0	Discharge Full	0.53 ft³/s
GVF Input Data  Downstream Depth  Length  Number Of Steps  0.000 in  0.00 ft  0	Slope Full	0.00156 ft/ft
Downstream Depth 0.000 in  Length 0.00 ft  Number Of Steps 0	Flow Type	SubCritical
Length 0.00 ft Number Of Steps 0	GVF Input Data	
Number Of Steps 0	Downstream Depth	0.000 in
<u> </u>	Length	0.00 ft
GVF Output Data	Number Of Steps	0
	GVF Output Data	
Upstream Depth 0.000 in	Upstream Depth	0.000 in
	Profile Description	
	Profile Headloss	0.00 ft

Bentley Systems, Inc. Haestad Methods So**Ratitle©Firter**Master V8i (SELECTseries 1) [08.11.01.03] 27 Siemons Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2

0.00 %

74.67 %

Infinity ft/s

Downstream Velocity

Average End Depth Over Rise

Normal Depth Over Rise

## **Worksheet for Existing: 8" Sewer Scottsdale Road**

### **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 5.974
 in

 Critical Depth
 0.32
 ft

 Channel Slope
 0.19000
 %

 Critical Slope
 0.00694
 ft/ft



## APPENDIX F

Proposed Sewer FlowMaster Data



SOUTHDALE

3 Engineering, LLC 6370 E. Thomas Road, Suite # 200 - Scottsdale, Arizona 85251 Phone: (602) 334-4387 - Fax: (602) 490-3230 www.3engineering.com

## Cross Section for Proposed: 8" Sewer Palm Lane Overflow to Weir

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

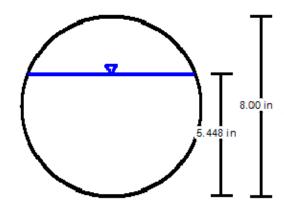
 Channel Slope
 0.27000
 %

 Normal Depth
 5.448
 in

 Diameter
 8.00
 in

 Discharge
 227.27
 gpm

#### **Cross Section Image**



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## Worksheet for Proposed: 8" Sewer Palm Lane Overflow to Weir

worksneet for	Proposed. 6	Sewei Pai	in Lane Overnow to well	
Project Description				
Friction Method	Manning Formula			
Solve For	Normal Depth			
	·			
Input Data				
Roughness Coefficient		0.013		
Channel Slope		0.27000	%	
Diameter		8.00	in	
Discharge		227.27	gpm	
Results				
Normal Depth		5.448	in	
Flow Area		36.46	in²	
Wetted Perimeter		1.29	ft	
Hydraulic Radius		2.348	in	
Top Width		0.62	ft	
Critical Depth		0.33	ft	
Percent Full		68.1	%	
Critical Slope		0.00702	ft/ft	
Velocity		2.00	ft/s	
Velocity Head		0.06	ft	
Specific Energy		0.52	ft	
Froude Number		0.55		
Maximum Discharge		0.68	ft³/s	
Discharge Full		0.63	ft³/s	
Slope Full		0.00176	ft/ft	
Flow Type	SubCritical			
GVF Input Data				
Downstream Depth		0.000	in	
Length		0.00	ft	
Number Of Steps		0		
GVF Output Data				
Upstream Depth		0.000	in	
Profile Description				
Profile Headloss		0.00	ft	
Average End Depth Over Rise		0.00	%	
Normal Depth Over Rise		68.10	%	
Downstream Velocity		Infinity	ft/s	

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## Worksheet for Proposed: 8" Sewer Palm Lane Overflow to Weir

## **GVF** Output Data

Upstream Velocity	Infinity	ft/s
Normal Depth	5.448	in
Critical Depth	0.33	ft
Channel Slope	0.27000	%
Critical Slope	0.00702	ft/ft

## **Cross Section for Proposed: Rectangular Weir Overflow NW**

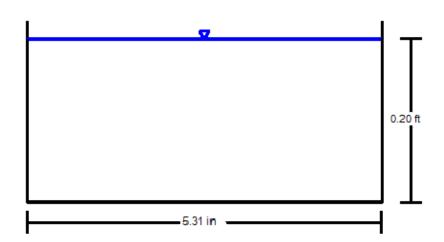
#### **Project Description**

Solve For Discharge

#### Input Data

Discharge		54.90	gpm
Headwater Elevation			in
Crest Elevation		0.00	in
Tailwater Elevation		0.00	in
Weir Coefficient			US
Crest Length		5.31	in
Number Of Contractions	0		

#### Cross Section Image



## **Worksheet for Proposed: Rectangular Weir Overflow NW**

Project Description			
Solve For	Discharge		
Input Data			
Headwater Elevation		2.448	in
Crest Elevation		0.00	in
Tailwater Elevation		0.00	in
Weir Coefficient		3.00	US
Crest Length		5.31	in
Number Of Contractions	0		
Results			
Discharge		54.90	gpm
Headwater Height Above Crest		0.20	ft
Tailwater Height Above Crest		0.00	ft
Flow Area		13.00	in²
Velocity		1.35	ft/s
Wetted Perimeter		0.85	ft
Top Width		0.44	ft

## **Cross Section for Proposed: 8" Sewer Palm Lane**

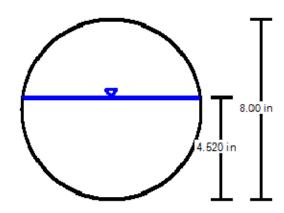
## **Project Description**

Friction Method Manning Formula Solve For Normal Depth

#### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.27000	%
Normal Depth	4.520	in
Diameter	8.00	in
Discharge	172.37	gpm

#### **Cross Section Image**



## Worksheet for Proposed: 8" Sewer Palm Lane

<b>Project</b>	Description
----------------	-------------

Friction Method Manning Formula Solve For Normal Depth

#### Input Data

0.013 Roughness Coefficient 0.27000 Channel Slope 8.00 Diameter in Discharge 172.37 gpm

#### Results

Normal Depth 4.520 in Flow Area 29.28 in² Wetted Perimeter ft 1.13 Hydraulic Radius 2.152 in Top Width 0.66 ft Critical Depth 0.29 ft Percent Full 56.5 % Critical Slope 0.00670 ft/ft Velocity 1.89 ft/s 0.06 Velocity Head ft Specific Energy 0.43 ft Froude Number 0.60 Maximum Discharge 0.68 ft³/s Discharge Full 0.63 ft³/s Slope Full 0.00101 ft/ft SubCritical Flow Type

#### **GVF Input Data**

Downstream Depth 0.000 in 0.00 Length ft 0 Number Of Steps

#### **GVF Output Data**

Upstream Depth Profile Description Profile Headloss 0.00 ft 0.00 Average End Depth Over Rise % Normal Depth Over Rise 56.50 % Infinity Downstream Velocity ft/s

0.000

## **Worksheet for Proposed: 8" Sewer Palm Lane**

### **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 4.520
 in

 Critical Depth
 0.29
 ft

 Channel Slope
 0.27000
 %

 Critical Slope
 0.00670
 ft/ft

## **Cross Section for Proposed: 10" Sewer Palm**

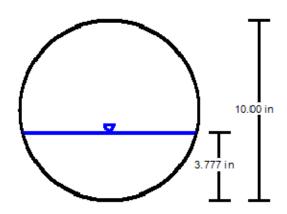
## **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

Roughness Coefficient	0.013	
Channel Slope	0.43000	%
Normal Depth	3.777	in
Diameter	10.00	in
Discharge	195.61	gpm

#### **Cross Section Image**



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## Worksheet for Proposed: 10" Sewer Palm

Project Description						

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

 Channel Slope
 0.43000
 %

 Diameter
 10.00
 in

 Discharge
 195.61
 gpm

#### Results

Normal Depth 3.777 in Flow Area 27.17 in² Wetted Perimeter ft 1.10 Hydraulic Radius 2.052 in Top Width 0.81 ft Critical Depth 0.29 ft Percent Full 37.8 % Critical Slope 0.00600 ft/ft Velocity 2.31 ft/s 0.08 Velocity Head ft Specific Energy 0.40 ft Froude Number 0.84 Maximum Discharge 1.55 ft³/s Discharge Full ft³/s 1.44 ft/ft Slope Full 0.00040 SubCritical Flow Type

#### **GVF Input Data**

#### **GVF Output Data**

Upstream Depth

Profile Description

Profile Headloss 0.00 ft

Average End Depth Over Rise 0.00 %

Normal Depth Over Rise 37.77 %

Downstream Velocity Infinity ft/s

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0.000

## **Worksheet for Proposed: 10" Sewer Palm**

## **GVF** Output Data

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 3.777
 in

 Critical Depth
 0.29
 ft

 Channel Slope
 0.43000
 %

 Critical Slope
 0.00600
 ft/ft

## **Cross Section for Prposed: 8" Sewer Scottsdale Road**

#### **Project Description**

Friction Method Manning Formula
Solve For Normal Depth

#### Input Data

 Roughness Coefficient
 0.013

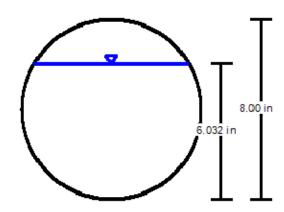
 Channel Slope
 0.19000
 %

 Normal Depth
 6.032
 in

 Diameter
 8.00
 in

 Discharge
 216.83
 gpm

#### **Cross Section Image**



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Workshe	et for Prposed:	8" Sewe	er Scottsdale Road
Project Description			
Friction Method	Manning Formula		
Solve For	Normal Depth		
Input Data			
Roughness Coefficient		0.013	
Channel Slope		0.19000	%
Diameter		8.00	in
Discharge		216.83	gpm
Results			
Normal Depth		6.032	in
Flow Area		40.66	in²
Wetted Perimeter		1.40	ft
Hydraulic Radius		2.416	in
Top Width		0.57	ft
Critical Depth		0.33	ft
Percent Full		75.4	%
Critical Slope		0.00696	ft/ft
Velocity		1.71	ft/s
Velocity Head		0.05	ft
Specific Energy		0.55	ft
Froude Number		0.43	
Maximum Discharge		0.57	ft³/s
Discharge Full		0.53	ft³/s
Slope Full		0.00160	ft/ft
Flow Type	SubCritical		
GVF Input Data			
Downstream Depth		0.000	in
Length		0.00	ft
Number Of Steps		0	
GVF Output Data			
Upstream Depth		0.000	in
Profile Description			
Profile Headloss		0.00	ft
Average End Depth Over Rise		0.00	%

Normal Depth Over Rise

Downstream Velocity

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Bentley Systems, Inc. Haestad Methods SoBdittle CFItterMaster V8i (SELECTseries 1) [08.11.01.03] 27 Siemons Company Drive Suite 200 W Watertown, CT 06795 USA +1-203-755-1666 Page 1 of 2

75.40 %

Infinity ft/s

## **Worksheet for Prposed: 8" Sewer Scottsdale Road**

#### **GVF Output Data**

 Upstream Velocity
 Infinity
 ft/s

 Normal Depth
 6.032
 in

 Critical Depth
 0.33
 ft

 Channel Slope
 0.19000
 %

 Critical Slope
 0.00696
 ft/ft



## APPENDIX G

Preliminary Onsite Utility Plans

PALM LANE

A.P.N. 129-33-019B CAPITAL REAL ESTATE-DWELL LLC

**OAK STREET** 

A.P.N.129-33-019A CHAPMAN

## LEGAL DESCRIPTION:

THAT PORTION OF THE SOUTHEAST QUARTER OF THE SOUTHEAST QUARTER OF SECTION 34. TOWNSHIP 2 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER BASE AND MERIDIAN, MARICOPA COUNTY, ARIZONA, MORE PARTICULARLY DESCRIBED AS FOLLOWS:

BEGINNING AT A POINT ON THE NORTH LINE OF THE SOUTH HALF OF SAID SOUTHEAST QUARTER OF THE SOUTHEAST QUARTER, A DISTANCE OF 380.00 FEET EAST OF THE WEST LINE OF SAID SOUTHEAST QUARTER OF THE SOUTHEAST QUARTER:

THENCE WEST ALONG SAID NORTH LINE TO A POINT ON THE EAST LINE OF A NORTH-SOUTH ALLEY AS SHOWN ON THE PLAT OF WONDERLAND, ACCORDING TO BOOK 100 OF MAPS, PAGE 19, RECORDS OF MARICOPA COUNTY, ARIZONA:

THENCE SOUTH ALONG THE EAST LINE OF AFORESAID ALLEY TO AN ANGLE POINT THEREON;

THENCE WEST ALONG THE SOUTH LINE OF AN EAST-WEST ALLEY AS SHOWN ON AFORESAID PLAT OF WONDERLAND, TO A POINT ON THE EAST LINE OF 70TH STREET AS SHOWN ON ÁFORESAID PLAT:

THENCE SOUTH ALONG SAID EAST LINE, A DISTANCE OF 253.88 FEET TO THE BEGINNING OF A CURVE TO THE LEFT HAVING A CENTRAL ANGLE OF 91 DEGREES 14 MINUTES 49 SECONDS AND A TANGENT OF 20.00 FEET;

THENCE SOUTHEASTERLY ALONG SAID CURVE TO THE LEFT, AN ARC DISTANCE OF 31.17 FEET;

THENCE SOUTH PARALLEL WITH THE WEST LINE OF THE SOUTHEAST QUARTER OF THE SOUTHEAST QUARTER OF SAID SECTION 34, A DISTANCE OF 65.00 FEET TO A POINT ON THE SOUTH LINE OF THE SOUTHEAST QUARTER OF THE SOUTHEAST QUARTER OF SAID SECTION 34, FROM WHICH THE SOUTHWEST CORNER THEREOF BEARS WEST, A

DISTANCE OF 52.42 FEET;
THENCE EAST ALONG THE SOUTH LINE OF THE SOUTHEAST QUARTER OF
THE SOUTHEAST QUARTER OF SAID SECTION 34, TO A POINT 380.00
FEET EAST OF THE SOUTHWEST CORNER OF SAID SOUTHEAST QUARTER SOUTHEAST QUARTER:

THENCE NORTH ALONG A LINE PARALLEL TO AND 380.00 FEET EAST OF THE WEST LINE OF SAID SOUTHEAST QUARTER OF THE SOUTHEAST QUARTER TO THE POINT OF BEGINNING:

EXCEPT THE SOUTH 65.00 FEET THEREOF.

## GENERAL NOTES FOR PUBLIC WORKS CONSTRUCTION:

- 1. ALL CONSTRUCTION IN THE PUBLIC RIGHTS-OF-WAY OR IN EASEMENTS GRANTED FOR PUBLIC USE MUST CONFORM TO THE LATEST MARICOPA ASSOCIATION OF GOVERNMENTS (MAG) UNIFORM STANDARD SPECIFICATIONS AND UNIFORM STANDARD DETAILS FOR PUBLIC WORKS CONSTRUCTION AS AMENDED BY THE LATEST VERSION OF THE CITY OF SCOTTSDALE STANDARD SPECIFICATIONS AND SUPPLEMENTAL STANDARD DETAILS. IF THERE IS A CONFLICT, THE CITY'S SUPPLEMENTAL STANDARD DETAILS WILL
- 2. THE CITY ONLY APPROVES THE SCOPE, NOT THE DETAIL OF ENGINEERING DESIGNS: THEREFORE IF CONSTRUCTION QUANTITIES ARE SHOWN ON THESE PLANS, THEY ARE NOT VERIFIED BY THE CITY.
- 3. THE APPROVAL OF PLANS IS VALID FOR SIX (6) MONTHS. IF ASSOCIATED PERMIT HAS NOT BEEN ISSUED WITHIN THIS TIME FRAME, THE PLANS MUST BE RESUBMITTED TO THE CITY FOR RE-APPROVAL.
- SCOTTSDALE. NOTIFY INSPECTION SERVICES 72 HOURS BEFORE BEGINNING

4. A CITY INSPECTOR WILL INSPECT ALL WORKS WITHIN THE CITY OF

- 5. WHENEVER EXCAVATION IS NECESSARY, CALL THE BLUE STAKE CENTER, 811, TWO WORKING DAYS BEFORE EXCAVATION BEGINS.
- 6. PERMISSION TO WORK IN THE RIGHT-OF-WAY (PWR) PERMITS ARE REQUIRED FOR ALL WORKS WITHIN THE RIGHTS-OF-WAY AND EASEMENTS GRANTED FOR PUBLIC PURPOSES. COPIES OF ALL PERMITS MUST BE RETAINED ON-SITE AND BE AVAILABLE FOR INSPECTION AT ALL TIMES. FAILURE TO PRODUCE THE REQUIRED PERMITS WILL RESULT IN IMMEDIATE SUSPENSION OF ALL WORK UNTIL THE PROPER PERMIT DOCUMENTATION IS OBTAINED.

UTILITY	UTILITY COMPANY	NAME OF COMPANY REPRESENTATIVE	TELEPHONE NUMBER	DATE SIGNED
ELECTRIC	APS			
TELEPHONE	CENTURY LINK			
NATURAL GAS	SOUTHWEST GAS			
CABLE TV	COX COMMUNICATIONS			
OTHER	A.T.&T.			
OTHER				

ENGINEER'S CERTIFICATION

DANIEL G. MANN, AS THE ENGINEER OF RECORD FOR THIS DEVELOPMENT, HEREBY CERTIFY THAT LL UTILITY COMPANIES LISTED ABOVE HAVE BEEN PROVIDED FINAL IMPROVEMENT PLANS FOR REVIEW. AND THAT ALL CONFLICTS IDENTIFIED BY THE UTILITIES HAVE BEEN RESOLVED. IN ADDITION "NO CONFLICT" FORMS HAVE BEEN OBTAINED FROM EACH UTILITY COMPANY AND ARE INCLUDED IN THIS SUBMITTAL.

DATE SIGNATURE

SHEET PUTL10: 020 ELL M.C.

SHEET PUTL102

MCDOWELL ROAD

SITE MAP

INDEX OF SHEETS

PRELIMINARY UTILITY PLAN

PRELIMINARY UTILITY PLAN

FLOOD INSURANCE RATE MAP (FIRM) INFORMATION:

SUFFIX

THE LOWEST FINISH FLOOR ELEVATION(S) AND/OR FLOOD PROOFING ELEVATION(S) ON THIS PLAN ARE SUFFICIENTLY HIGH

TO PROVIDE PROTECTION FROM FLOODING CAUSED BY A 100-YEAR STORM, AND ARE IN ACCORDANCE WITH SCOTTSDALE

COVER SHEET - PRELIMINARY UTILITY PLAN

FIRM DATE

OCTOBER 16, 2013

FIRM ZONE

DESCRIPTION

BASE FLOOD ELEVATION

N/A

1 WONDERLAND 00, PG. 19, M.C.R. .N. 129-33-018B EAL ESTATE-DWEL -0940342 M.C.R.

SHEET NO.

PUTL 101

PUTL 102

PUTL 103

PANEL NUMBER

ENGINEER'S CERTIFICATION:

PANEL DATE

OCTOBER 16, 2013

REVISED CODE, CHAPTER 37 - FLOODPLAIN AND STORMWATER REGULATION.

STR

COMMUNITY

NUMBER

1560 — INDICATES EXISTING CONTOUR ELEVATION 58— INDICATES PROPOSED CONTOUR ELEVATION INDICATES EXISTING TOP OF CURB ELEVATION INDICATES EXISTING GUTTER ELEVATION INDICATES EXISTING GROUND ELEVATION INDICATES EXISTING PAVEMENT ELEVATION + C: 56.69 INDICATES EXISTING CONCRETE ELEVATION INDICATES PROPOSED GROUND ELEVATION INDICATES DIRECTION OF FLOW & SLOPE INDICATES GRADE BREAK INDICATES PROPOSED PAVEMENT ELEVATION INDICATES PROPOSED TOP OF CONC. ELEVATION INDICATES PROPOSED GUTTER ELEVATION INDICATES LOWEST FINISH FLOOR ELEVATION

LEGEND

Ш

----- INDICATES PROPERTY / BOUNDARY LINE

INDICATES PROPOSED SEWERLINE

INDICATES PROPOSED WATERLINE

INDICATES PROPOSED METER INDICATES PROPOSED SEWER CLEANOUT INDICATES PROPOSED CATCH BASIN INDICATES PROPOSED STORM DRAIN PIPE INDICATES PROPOSED STORM DRAIN MANHOLE INDICATES PROPOSED FIRE HYDRANT FH 😱 INDICATES EXISTING FIRE HYDRANT INDICATES EXISTING STORM DRAIN PIPE

----24" SD----INDICATES EXISTING SEWER LINE & SIZE

BWV∞

INDICATES EXISTING WATER LINE, VALVE & SIZE INDICATES EXISTING BURIED ELECTRIC CONDUIT INDICATES EXISTING GAS LINE INDICATES EXISTING OVERHEAD ELECTRIC INDICATES EXISTING POWER POLE

INDICATES EXISTING LIGHT POLE  $ET \boxtimes$ INDICATES EXISTING ELECTRIC TRANSFORMER INDICATES EXISTING ELECTRIC BOX EB 🛮  $WM \square$ INDICATES EXISTING WATER METER

INDICATES EXISTING BACKFLOW PREVENTER VALVE

THOMAS ROAD PALM LANE MCDOWELL

Call 811 or click Arizona811.co

*KENIZION2* 

 $\mathcal{L}$ 

RELIMIN

46857

DANIEL G.

# VICINITY MAP

**ENGINEER:** 

3 ENGINEERING

PROJECT SCOPE:

THE SCOPE OF THIS PROJECT IS A NEW RESIDENTIAL APARTMENT COMPLEX WITH 267 UNITS ALSO WITH PARKING GARAGE, UTILITY IMPROVEMENTS AND LANDSCAPE.

CLIENT:

HAWKINS COMPANIES LLC 4700 S. MCCLINTOCK DR. #160 TEMPE, ARIZONA 85282

CONTACT: MARK MITCHELL

PHONE: (480) 223-8239

6370 E. THOMAS ROAD. SUITE #200 SCOTTSDALE, ARIZONA 85251

CONTACT: DANIEL G. MANN. P.E. PHONE: (602) 334-4387 EMAIL: DAN@3ENGINEERING.COM

N.T.S.

PARCEL ADDRESS:

EMAIL: MMITCHELL@HCOLLC.COM

7000 E. MCDOWELL ROAD, SCOTTSDALE, ARIZONA 85257

ASSESSORS PARCEL NUMBER:

129-33-001S

LOT AREA:

GROSS AREA: 4.690 ACRES 3.932 ACRES NET AREA:

DISTURBED AREA: 3.932 ACRES

BENCHMARK:

MARICOPA COUNTY DEPARTMENT OF TRANSPORTATION UNIQUE ID: 12052, BEING A 3" CITY OF SCOTTSDALE BRASS CAP IN HANDHOLE, LOCATED AT THE INTERSECTION OF SCOTTSDALE

ELEVATION = 1230.474 (NAVD'88)CITY OF SCOTTSDALE DATUM

IHEREBY CERTIFY THAT ALL ELEVATIONS REPRESENTED ON THIS PLAN ARE BASED ON THE ELEVATION DATUM FOR THE CITY OF SCOTTSDALE BENCHMARK PROVIDED ABOVE.

**ENGINEER** 

4/26/2021 DATE

BASIS OF BEARING

THE BASIS OF BEARING IS THE MONUMENT LINE OF SCOTTSDALE ROAD, ALSO BEING THE WEST LINE OF THE SOUTHEAST CORNER, SECTION 34, USING A BEARING OF NORTH OO DEGREES OO MINUTES OO SECONDS EAST, AS PER THE RECORD OF SURVEY IN BOOK 1250 OF MAPS, PAGE 15, RECORDS OF MARICOPA COUNTY, ARIZONA.

**ENGINEER'S STATEMENT:** 

THE ENGINEER OF RECORD ON THESE PLANS HAS RECEIVED A COPY OF THE APPROVED STIPULATIONS FOR THIS PROJECT AND HAS DESIGNED THESE PLANS IN CONFORMANCE WITH THE APPROVED STIPULATIONS

AS-BUILT CERTIFICATION:

HEREBY CERTIFY THAT THE RECORD DRAWING MEASUREMENTS AS SHOWN HEREON WERE MADE UNDER MY SUPERVISION OR AS NOTED AND ARE CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

REGISTERED ENGINEER/LAND SURVEYOR

ENGINEERING COORDINATION MGR. (OR DESIGNEE)

DATE

REGISTRATION NUMBER

	CIVIL AF	PROVAL				
EVIEW & REC	EVIEW & RECOMMENDED APRROVAL BY:					
AVING		TRAFFIC				
& D		PLANNING				
& S		FIRE				
ET.WALLS						
				ĺ		

PROJECT NO. PUTL201 1 of 3

3 ENGINEERING, LLC

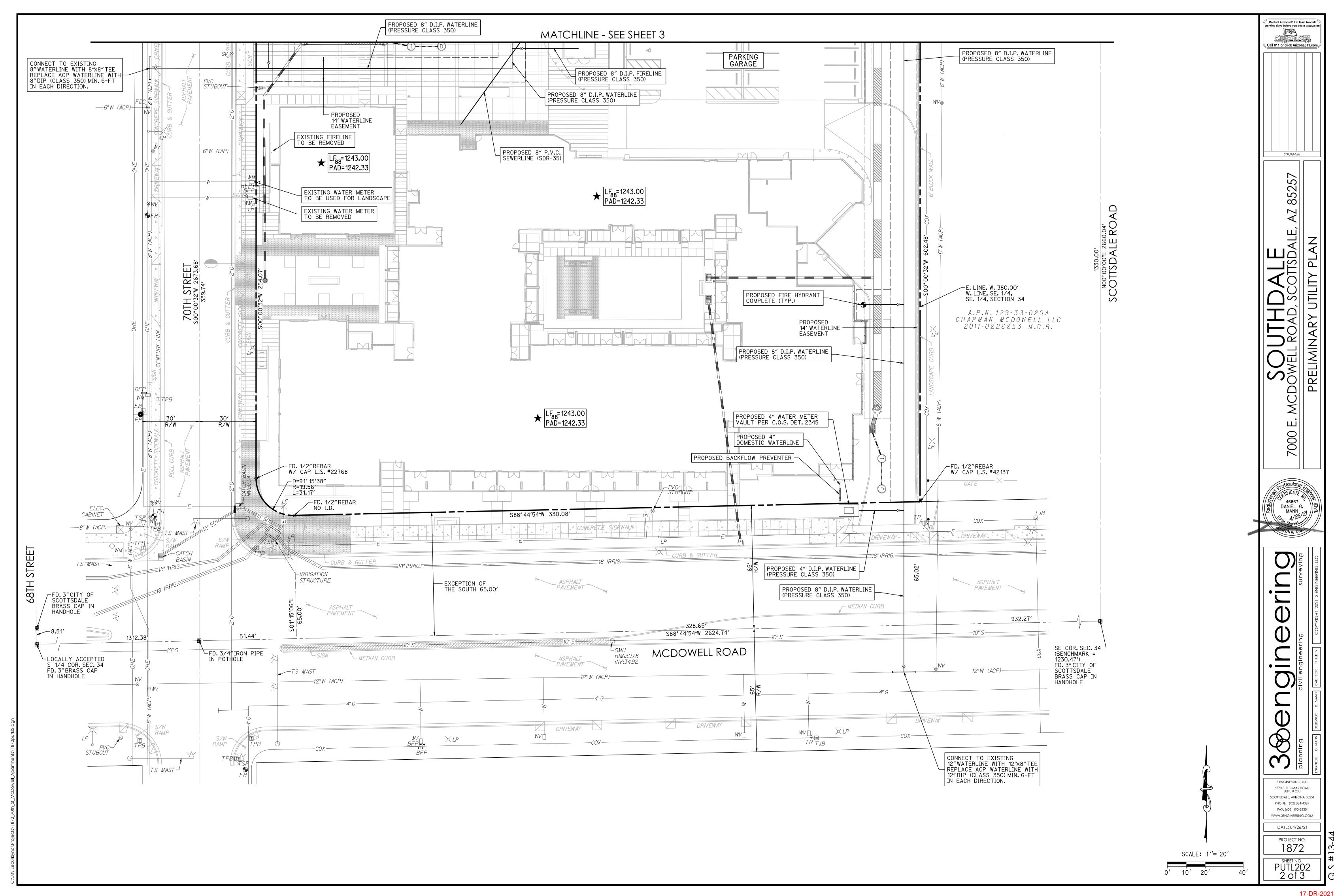
6370 E. THOMAS ROAD SUITE # 200

SCOTTSDALE, AR<mark>I</mark>ZONA 8525 PHONE: (602) 334-4387

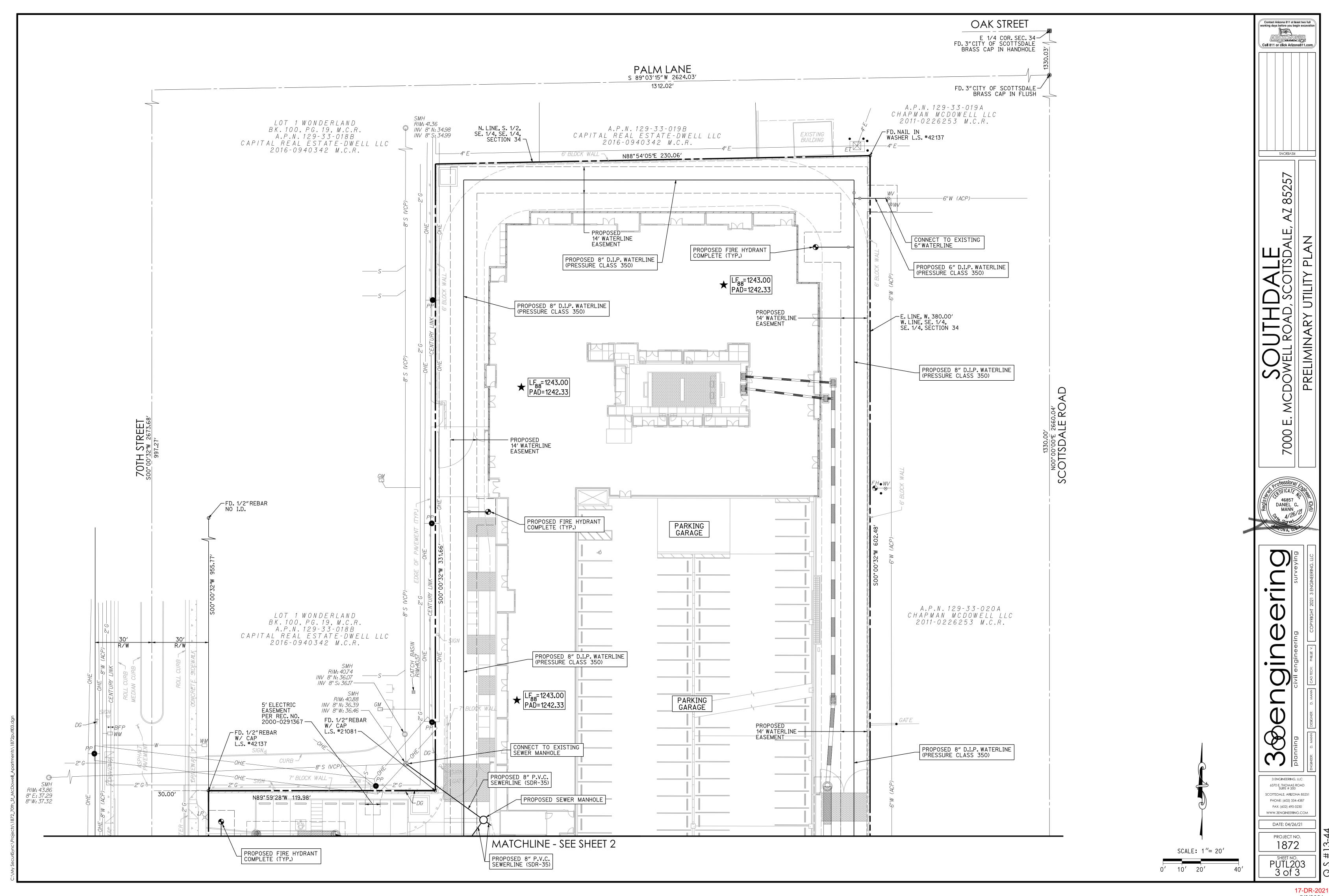
FAX: (602) 490-3230

WWW.3ENGINEERING.CO

5/6/2021



17-DR-2021 5/6/2021



17-DR-2021 5/6/2021