

# ***PRELIMINARY DRAINAGE REPORT***

## **Optima McDowell Mountain Village Scottsdale Road and Mayo Boulevard Scottsdale, Arizona**

### **Prepared For:**

*DCH Development, Inc.  
7157 E. Rancho Vista Drive  
Scottsdale, Arizona 85251*



### **Prepared By:**

*Kimley-Horn and Associates, Inc.  
7740 N. 16<sup>th</sup> Avenue, Suite 300  
Phoenix, Arizona 85020*

*Michael L. Delmarter*  
EXP: 12/31/2023

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<b><u>Section</u></b>	<b><u>Page No.</u></b>
<b>1.0 Introduction</b>	<b>3</b>
1.1 Project Description	3
1.2 Site Location	3
1.3 Purpose	3
1.4 Objectives	3
<b>2.0 Description of Existing Drainage Conditions and Characteristics</b>	<b>4</b>
2.1 Existing On-Site Drainage Conditions	4
2.2 Existing Off-Site Drainage Conditions	4
2.3 Context Relative to Adjacent Projects and Improvements	8
2.4 FEMA Flood Hazard Areas	8
<b>3.0 Proposed Drainage Plan</b>	<b>9</b>
3.1 General Description	9
3.2 Proposed Site Conditions	9
3.3 Proposed Off-Site Conditions	10
3.4 Future Conditions	10
3.5 Storage Requirements	10
3.6 Proposed Drainage Structures or Special Drainage Facilities	10
3.7 ADEQ AZPDES requirements	11
3.8 Project Phasing	11
<b>4.0 Special Conditions</b>	<b>11</b>
4.1 404 Discussion	11
4.2 Preservation of existing channel	11
<b>5.0 Data Analysis Methods</b>	<b>12</b>
5.1 Hydrologic Procedures, Parameter Selection, and Assumptions	12
5.2 Hydraulic Procedures, Methods, Parameter Selection, and Assumptions	12
5.3 Storm Water Storage Calculation Methods and Assumptions	13
<b>6.0 Conclusion</b>	<b>13</b>
<b>7.0 References</b>	<b>14</b>

**List of Appendices**

- A Site Location Map and Legal Description
- B FEMA Federal Insurance Rate Map (FIRM) and Natural Grade Exhibit
- C Crossroads East Planning Unit IV Drainage Report
- D Hydrologic/Hydraulic Calculations
- E Context Aerial plan
- F Existing Conditions Topographic Map
- G Preliminary Grading and Drainage Plan
- H Scottsdale Road Improvements Phase 2 Drainage Report
- I Wood Patel Interim Drainage Channel Drainage Report
- J Site Basin Delineation
- K As-Builts for Lund Channel
- L As-Builts for One Scottsdale South Drainage Basin Improvement Plans
- M As Builts for Scottsdale Road Interim Drainage Channel.
- N Interim Drainage Channel Report
- O Interim Regional Channel Design Report

## **1.0 Introduction**

### **1.1 Project Description**

The applicant is proposing to construct a multi-family development on a 15.637+/- net acre parcel located at the northeast corner of Scottsdale Road and Mayo Boulevard. The project, Optima McDowell Mountain Village, is anticipated to consist of apartment and condominium buildings and amenities constructed over an underground parking garage which will have access to both Scottsdale Road and Mayo Boulevard.

### **1.2 Site Location**

The proposed development encompasses approximately 15.637± net acres in a portion of the Southwest Quarter of Section 26, Township 4 North, Range 4 East of the Gila and Salt River Base and Meridian in Maricopa County, Arizona. More specifically, the parcel is bounded by the Loop 101 Freeway to the north, vacant State Land to the east, a car dealership to the south, and Scottsdale Road to the west. See **Appendix A** for the site location map and legal description. See **Appendix E** for a Context Aerial Map.

### **1.3 Purpose**

This Preliminary Drainage Report is intended to satisfy City of Scottsdale requirements and demonstrate conformance to the regional drainage planning solutions implemented by other projects immediately south of the project. This report provides a description of the current storm water drainage patterns and systems and a description of the required and proposed drainage improvements.

### **1.4 Objectives**

This report provides a drainage plan for the site that is intended to meet the drainage standards and guidelines of the City of Scottsdale and the Flood Control District of Maricopa County (FCDMC). In particular, this report will demonstrate the following:

1. Off-site flows are diverted around the site via the ADOT Freeway improvements, and the downstream City of Scottsdale box culverts and channel system located along the eastern side of the property.
2. The site drainage patterns will remain consistent with the existing hydrology patterns.
3. Permanent drainage facilities will have a positive outfall for flows exceeding storage capacity and any detained storm water will be disposed of within 36 hours via drywells and or bleed pipes.
4. Drainage facilities will be designed to retain pre vs post development flows. All runoff in excess of the retained storage capacity will be discharged into an adjacent channel which is already sized to handle existing conditions in the area.



## 2.0 Description of Existing Drainage Conditions and Characteristics

### 2.1 Existing On-Site Drainage Conditions

The site currently consists of vacant, undeveloped land with sparse desert vegetation throughout the site. The site is bounded by the Loop 101 Freeway to the north, vacant State Land to the east, a car dealership to the south, and Scottsdale Road to the west.

The site generally slopes from the north to the south at approximately 1.5%. The Crossroads East planning area lies immediately east of the site on the eastern side of the regional drainage channel that passes offsite flows around the eastern side of the site.

**Appendix I**, includes the Scottsdale Road Drainage Report which discusses the Crossroads East planning and shows how the storm water from the site ultimately outfalls to Reach 11 (Dike 2) in the City of Phoenix.

In 2003, as part of a City of Scottsdale improvement project, 2 sets of double 6'x4' box culverts were installed in a 30' wide parcel of City owned land along the northern property line to intercept offsite flows from under the Loop 101 freeway. These box culverts discharge into a drainage channel that runs along the eastern property line which turns westerly near the southern property line before entering a triple 8'x3' box culvert that flows under Mayo Boulevard and enters the Bell Lexus site. **Appendix K** contains the as-built drawings for the Lund Channel design through the property.

The remainder of the existing site currently discharges as sheet flow onto Mayo Boulevard where flows are picked up in existing catch basins and conveyed to the aforementioned box culvert in Mayo Boulevard.

Refer to **Appendix F** for the Existing Conditions Topography Exhibit.

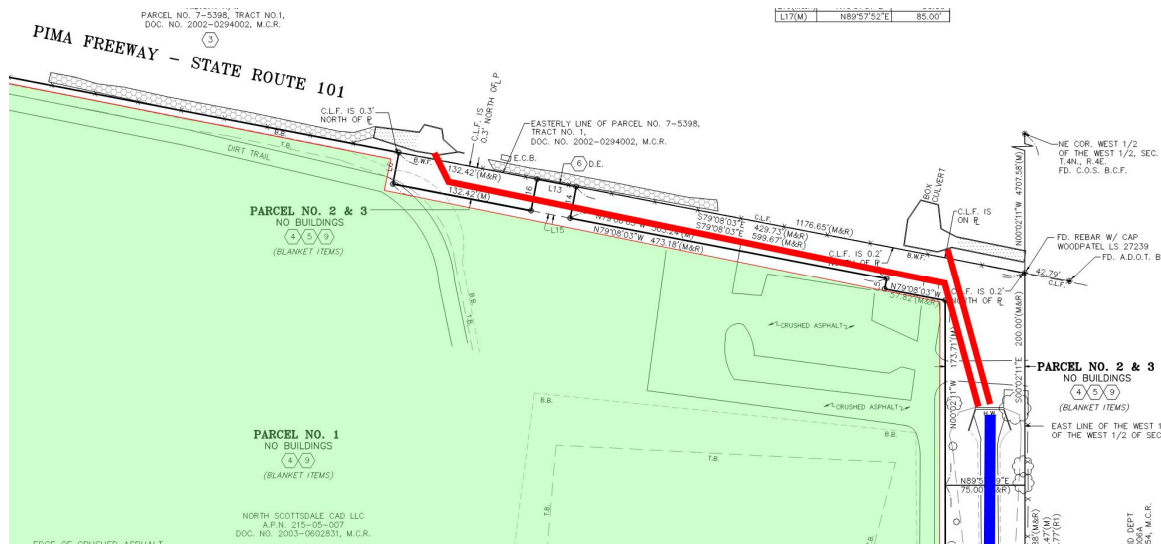
### 2.2 Existing Off-Site Drainage Conditions

Upstream improvements, north of the freeway, were installed in 2007 as part of the One Scottsdale project. This project installed culverts and retention basins which reduced flows tributary to the original ADOT box culverts. See **Appendix L** One Scottsdale South Drainage Basin Improvement Plans for details.

An interim drainage channel was constructed immediately downstream of the project in 2009 that conveyed flows leaving the southern end of the Lund Channel Box Culvert under Mayo Boulevard to a double 8'x3' box culvert located just north of Princess Boulevard. See **Appendix M** Scottsdale Road Interim Drainage Channel.

The double 8'x3' box culvert under Scottsdale Road was also designed in 2009 as part of Segment 2 of Scottsdale Road improvements by the City of Scottsdale. Note: the Scottsdale Road improvements immediately adjacent to the site were constructed as Segment 1 construction. This double box culvert ultimately discharges west of Scottsdale Road and south of Princess Drive into Reach 11.

Subsequent extensions of the Lund Channel system were made across the “Bell Lexus” site immediately downstream of Mayo Boulevard and across the other downstream projects ultimately connecting to the existing 2 – 8’x3’ box culverts under Scottsdale Road that discharge to Reach 11.



Existing drainage from Scottsdale Road is collected via catch basins which tie into the 36” diameter storm drain in Scottsdale Road that also eventually discharges to Reach 11. Mayo Boulevard drainage is also collected in catch basins that tie back into the existing “Lund Channel” box culverts under Mayo Boulevard which also discharge to Reach 11.

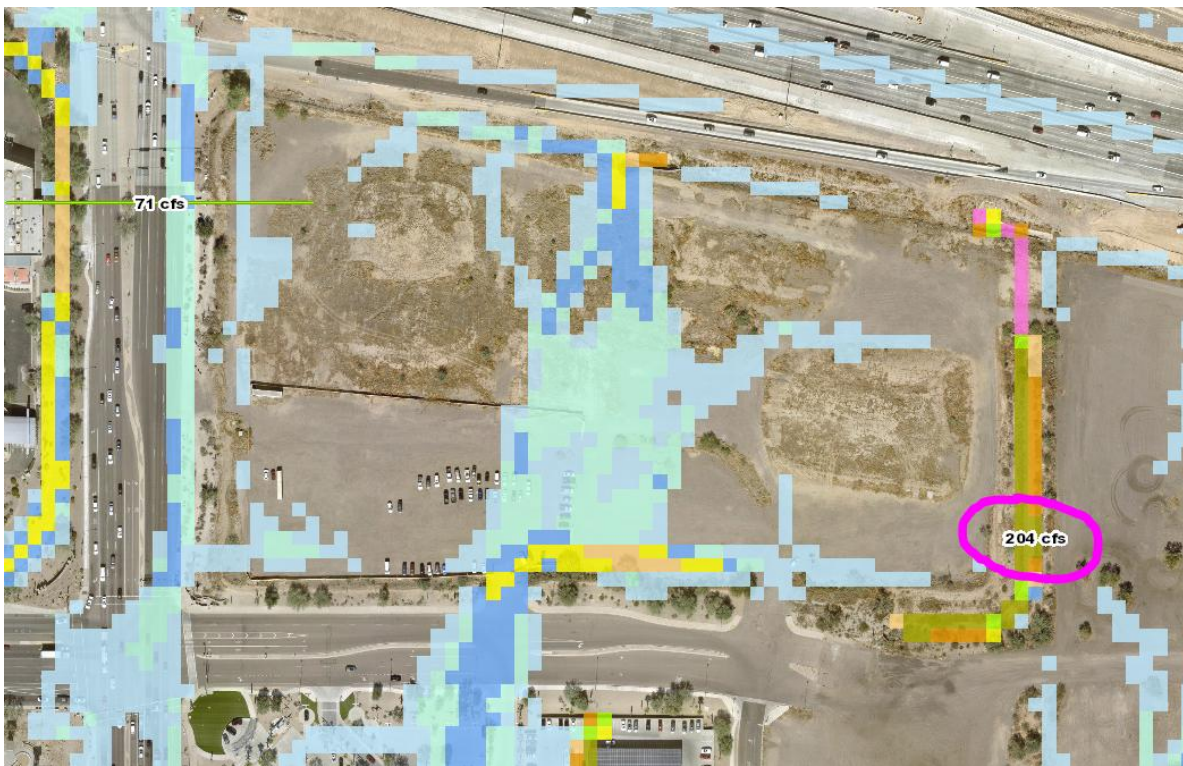
The original design for the ADOT Box culverts anticipated that a total of 600 cfs would be conveyed through the boxes and the “Lund Channel” adjacent to the subject property.

Updated Offsite Hydrology was included in the Final Drainage Report for the Interim Regional Drainage Channel prepared by Wood Patel in October 2008 (see **Appendix O**) and was utilized to design the downstream improvements based on flows that are significantly less than the original ADOT design flow rates. This hydrology is described in the report as follows:

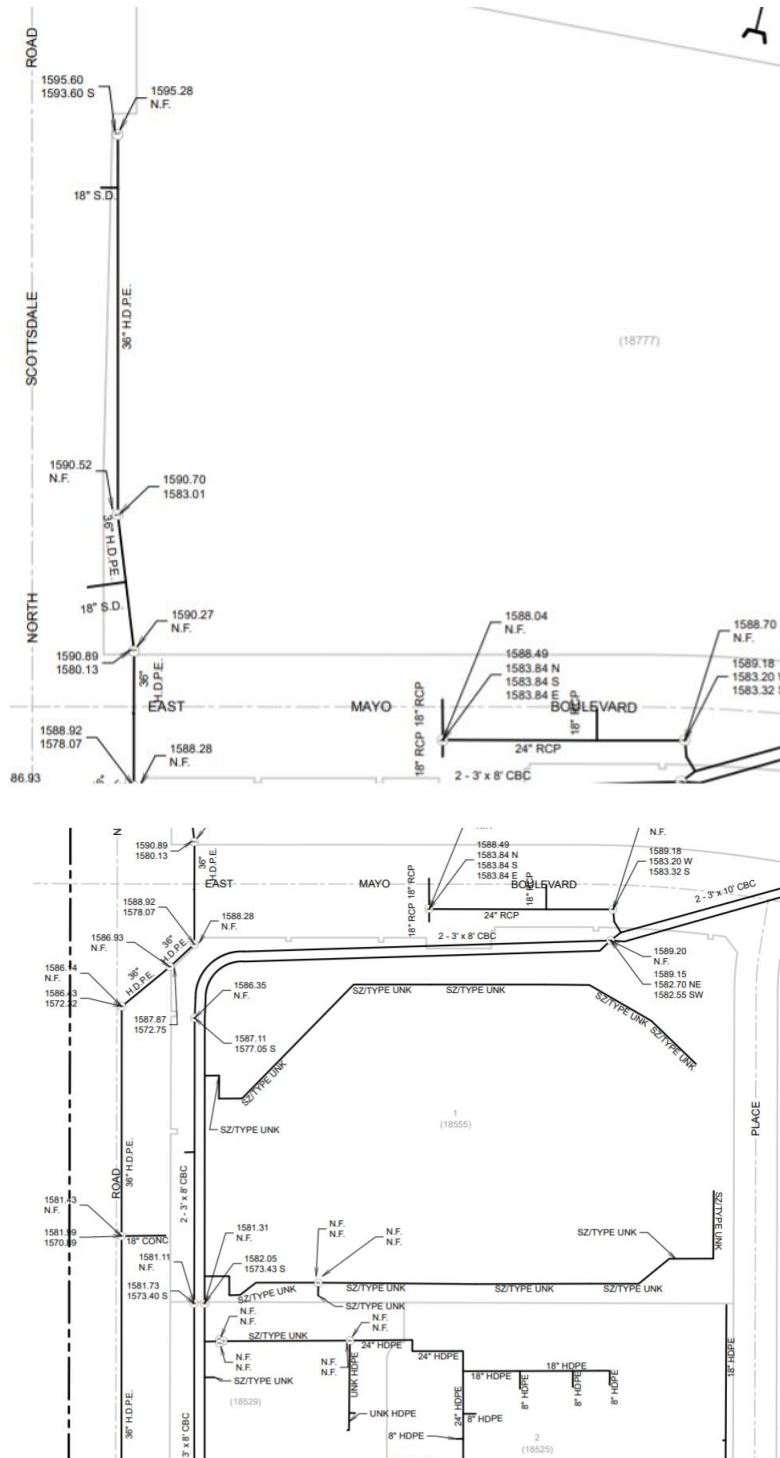
*“The 100 year design flow for the Interim Regional Drainage Channel is 300 cfs. This is based on a 100 year 6 hour design storm utilizing HEC-1. Results of this model are included in Appendix A (of the WP Report)... The included HEC-1 model is an expansion of the hydrology model completed for the One Scottsdale Master Drainage Plan by Wood Patel and Associates. The One Scottsdale development lies upstream of the project site to the north of the Loop 101 Freeway. The model was revised to expand to the south to include the proposed improvements. Flow from the Loop 101 Freeway culverts is now routed through the Interim Regional Drainage Channel (R33E.1). Runoff from the Adjacent State Land Parcel (ASLD) joins at the outfall culvert under Scottsdale Road*

*near Princess (CPPRIN). This downstream flow was used as the design flow from the entire channel.”* The conclusions from the WP report determined that the “Lund Channel” conveys 256 cfs and after inclusion of the other downstream tributary State Land area, the culverts under Scottsdale Road are subject to 300 cfs.

FLO-2D modeling has recently been prepared by the Maricopa County Flood Control District as part of the Pinnacle Peak West – Lower Rawhide analysis and indicate that the 100-year flows in the “Lund Channel” are 204 cfs with another 64 cfs reaching the site from the western ADOT culverts. These flows will actually combine for approximately 268 cfs as the model does not recognize that the 2 box culverts under the freeway combine. While FLO-2D is utilized as a planning tool, these results are consistent with the hydrology presented in the Wood Patel Report. This methodology and analysis have been accepted by the City of Scottsdale and will be used for the purposes of future site design considerations. The following figure is a snip of the FLO 2D results.



The below images are clipped from the City of Scottsdale Quarter Section maps showing storm drain infrastructure in the adjacent streets and also downstream through the Bell Lexus site.



A copy of the Crossroads East Planning Unit IV Drainage Report that provides more detail about the downstream box culverts and proposed developments is included in **Appendix C**.

Refer to **Appendix F** for the Existing Conditions Exhibit.

### **2.3 Context Relative to Adjacent Projects and Improvements**

The site is located between the Loop 101 and Mayo Boulevard on the east side of Scottsdale Road. The Bell Lexus development lies immediately south. See **Appendix E** for Context Aerial of the site.

### **2.4 FEMA Flood Hazard Areas**

The site is located in Flood Zone “AO” according to the Flood Insurance Rate Map 04013C1320L, dated October 16, 2013. Zone “AO” is designated by FEMA as “areas of flood depths of 1 foot (usually sheet flow on sloping terrain) average depths determined for areas of alluvial fan flooding, velocities also determined.” Refer to Appendix B for the FEMA FIRMette map for the site. Efforts are currently underway to change the Flood Zone designation to Zone X similar to LOMR’s recently approved immediately upstream of the Loop 101 freeway. This process will take up to 12 months, but planning and preliminary engineering is premised on the assumption that this effort will be completed by the end of 2022. Refer to **Appendix B** for current FEMA Flood Map.

The LOMR application has been approved by the City and was submitted to FEMA on June 29, 2022. FEMA comments are anticipated within 90 days.



### 3.0 Proposed Drainage Plan

#### 3.1 General Description

In the analysis of the proposed drainage conditions the following items are considered:

- Area Types (concrete pavement, building, and desert landscaping)
- Magnitude of areas
- Slopes
- Storm Drain
- Detention Basins

#### 3.2 Proposed Site Conditions

As previously discussed, the existing eastern channel and downstream conveyance system was originally designed for the 100-year discharge of 600 cfs while the current Maricopa County Flood Control FLO 2D study and the 2009 Wood Patel report indicates that the revised flows in the eastern channel are actually 256-268 cfs. The interim regional drainage channel downstream of the property was conservatively designed for 300 cfs including the predeveloped conditions from the subject property. It is therefore proposed that this site be designed for the greater of pre vs post or first flush flows as it has been shown that runoff can be safely delivered to the Reach 11.

Site-generated storm water in excess of existing conditions storage requirement is proposed to be discharged to the regional drainage channel from the underground detention basin.

Most of the 15.637 +/- net acre property will be covered by an underground parking garage with the surface level of the garage set at elevation 1596.0. The fire loop road around the northern and eastern sides of the property is also at 1596.0. This elevation is above the top of bank elevation of the northern end of the existing channel on the east side of the property and 3.5 feet above the top of bank (1592.5) at the southern end of the channel.

With the proposed discharge point located at the southeast corner of the project, the onsite collection system will also serve to provide pre vs post storage and convey excess flows to the outfall location. This storage and conveyance tank is proposed to be a standalone tank located along the southern edge of the garage with the outlet pipe inverts to be located 3.5 feet below the finished floor elevation at 1592.5. Based on a single point of discharge, the overflow pipes will be designed for the 100-year flow which is calculated to be 37.6 cfs with 3 – 24” pipes extending to the bottom of the channel. Supporting calculations are located in **Appendix D** and **Appendix H**.

A new fire access road crossing of the channel is proposed to occur at the southern end of the channel. This crossing will require the installation of a triple 4'x8' box culvert that will be sized to match the existing culverts under Mayo Boulevard immediately downstream of the site. Note: The existing culverts were designed to convey the original 600 cfs assumed by ADOT. These box culverts may be reduced in size with final engineering design to match the capacity of the downstream conveyance system based on the 2009 hydrology discussed above.

### 3.3 Proposed Off-Site Conditions

Regional off-site storm water runoff from north of the Loop 101 onto Planning Unit IV is proposed to be handled in accordance with the Crossroads East Planning Unit IV Master Drainage Report located in **Appendix I**. Off-site storm water impacts beyond those discussed above are not anticipated due to the built-out condition of the upstream areas adjacent to the site.

### 3.4 Future Conditions

No future drainage impacts are anticipated for the site due to the previous development of areas upstream of the subject parcel. It is anticipated that undeveloped areas adjacent to the site will be developed in accordance with the Planning Unit IV Master Drainage Report and City of Scottsdale standards.

### 3.5 Storage Requirements

As previously noted, the site is submitting the documentation for a Stormwater Storage Waiver. Pre vs Post Detention will be provided based on the difference in C-values for the onsite tributary area. A C coefficient of 0.9 is assumed for the post developed conditions and 0.45 is utilized for the existing cleared desert conditions.

**Table 1: Pre- vs. Post Detention Volume Requirement**

Basin	Land Use	Delta Runoff Coefficient	Drainage Area (ft <sup>2</sup> )	Rainfall	Required Volume (ft <sup>3</sup> )
Basin A	Garage Footprint	0.9-0.45 =0.45	681,146	2.3"	58,749

**Volume Provided = 59,400 cf**

### 3.6 Proposed Drainage Structures or Special Drainage Facilities

An underground retention vault will be constructed in the southeast corner of the site adjacent to the garage footprint to store the pre- vs post development volume. Based on preliminary calcs, it is assumed that the vault will extend to the bottom floor of the garage which is 16.5 feet below the outlet elevation. The cast in place vault is anticipated to be approximately 15' wide by 240 feet long resulted in a storage volume of 59,400 cf which exceeds the required 58,749 cf volume indicated in Table 1 above. While the basin is designed to scalp the flow from the 100-year storm, the overflow outlet will be

designed based on a ration method calculation based on the delta C values. Therefore, the overflow 100-year storm will discharge 37.6 cfs into the adjacent Lund Channel.

The invert of the outlet pipes to the basin will be set at 3.5 feet below the first-floor elevation of 1592.5, and is located above the top of bank of the adjacent regional drainage channel. The pipes will extend to bottom of the channel and outlet immediately upstream of the box culvert under Mayo Boulevard. All pipes will be equipped with a grate.

Dry Wells are designed to drain the tank in less than 36 hours at an initial rate of 0.1 cfs. Based on this rate, each drywell can drain  $0.1 \text{ cf/sec} \times 36 \text{ hrs} \times 60 \text{ min/hr} \times 60 \text{ sec/minute} = 12,960 \text{ cf}$  per drywell. A total of 5 dry wells are required to drain the tanks. These drywells will be installed in the bottom of the tanks at 50 foot intervals with one drywell located outside of the tank. As the dry wells are constructed, each dry well will be tested to determine actual infiltration rate and the number of required drywells may be reduced accordingly.

### **3.7 ADEQ AZPDES requirements**

Prior to construction an executed Notice of Intent (NOI) shall be submitted to Arizona Department of Environmental Quality (ADEQ) in conformance with the Arizona Pollution Discharge Elimination System Permit (AZPDES) permit. The NOI and associated storm water management best management practices will remain active on the site until construction is complete and a Notice of Termination is filed with ADEQ in conformance with AZPDES permit.

### **3.8 Project Phasing**

This project will be constructed in multiple phases. The retention vault will be constructed with Phase 1 but sized for the entire site.

## **4.0 Special Conditions**

### **4.1 404 Discussion**

No existing U.S. Army Corp of Engineers 404 jurisdictional washes are present on site that would be impacted by the proposed improvements.

### **4.2 Preservation of existing channel**

No proposed disturbance to the “Lund Channel” located on the eastern edge of the property is proposed except for the proposed overflow pipe connection and the installation of the triple box culvert discussed in Section 3.2 above. Per City of Scottsdale requirements, contributing off-site upstream flows must be maintained in the post-development condition.



## 5.0 Data Analysis Methods

### 5.1 Hydrologic Procedures, Parameter Selection, and Assumptions

All roof drains from the proposed residential buildings and area drains from the landscaped areas located on top of the garage footprint will be sized by the MEP per building code requirements and will tie directly to the concrete detention vault which will be located within the underground garage. Courtyard inlets are designed to be placed on 30 feet placed grid lines. Refer to **Appendix G**, for the Preliminary Grading and Drainage Plans.

Hydrologic calculations for the site were performed using the rational equation in the FCDMC Drainage Design Manual Volume I, which is limited to drainage areas of up to 160 acres. A weighted runoff coefficient was used for the site based upon the large amount of landscaping located adjacent to perimeters of the site. The completed calculations for the Rational Method are included in **Appendix D**.

### 5.2 Hydraulic Procedures, Methods, Parameter Selection, and Assumptions

All flows for proposed conditions will be determined using the rational method as outlined by the Drainage Design Manual by Maricopa County Flood Control District. Since all pipe inlets and roof drains will be discharging to the cast in place vault described above, a minimum time of concentration of 10 minutes has been used. All drainage basins will assume a runoff coefficient of 0.95 to account for the current land description. The delineated water shed used in calculation can be found in **Appendix J**.

The following criteria will be used to size the proposed pipes for on-site storm water conveyance:

- A maximum allowable 100-year ponding depth of six inches above the catch basin grate.
- A minimum of 12 inches of freeboard between the 100-year ponding depth and the building finish floor elevation.
- The tailwater condition for the 100-year event will be assumed to be the hydraulic grade line at the pipe connection location.
- The 10-year tailwater condition will be assumed to be free outfall.

StormCAD analysis for the 10-year and 100-year events will be provided with the final drainage report.

### 5.3 Storm Water Storage Calculation Methods and Assumptions

As stated above, the difference in pre vs post development runoff volumes will be stored in the retention tank. The standard formula for determining the required first flush storage volumes is as follows:

$$V_R = CPA/12$$

Where:  $V_R$  = storage volume required (cubic feet)

$C$  = weighted runoff coefficient = 1.0

$P$  = precipitation depth for First Flush = 0.50 inches

$A$  = contributing drainage area to basin (square feet)

## 6.0 Conclusion

Based on the results of this final drainage report, the following can be concluded:

- An underground storage retention vault will be constructed adjacent to the garage footprint to store pre vs post development retention volume.
- Discharge from the underground vault will be via 3- 24" pipes into the Lund Channel
- Onsite Storm drainage systems consisting of area drain and roof drains will tie directly into the detention basin located adjacent to the garage footprint.
- The building finish floor elevations have been designed to be at least fourteen inches above the ultimate site outfall elevation.
- Off-site storm water from areas upstream of the site are currently and will remain routed around the site, in the existing Lund Channel and discharged at their historical flow path.
- A new box culvert will be installed at the southeast corner of the site across the Lund Channel to provide Fire Department access to the east side of the site.
- A separate LOMR effort is currently being submitted to FEMA by Kimley-Horn to remove the property from FEMA Zone "AO". All design is being performed assuming the site is reclassified as Zone X.
- All runoff generated in Scottsdale Road and Mayo Blvd are collected in existing catch basins and are not stored on-site and do not impact the site.

This drainage report is intended to provide a level of assurance that the site will adhere to all appropriate reviewing agency guidelines with respect to drainage and flood protection.

## **7.0 References**

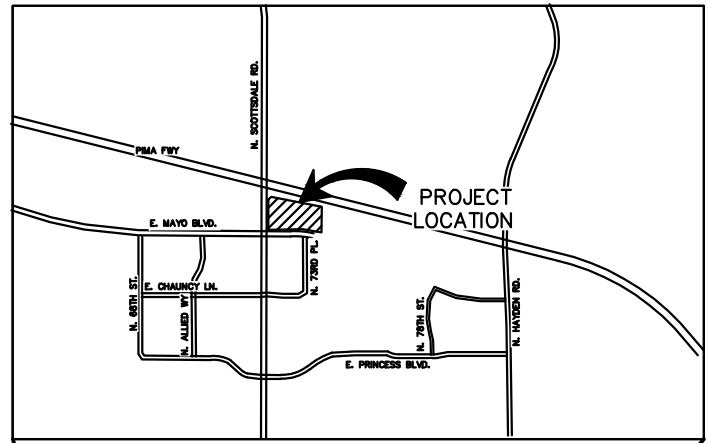
1. City of Scottsdale, *Design Standards and Policies Manual, Chapter 4: Grading and Drainage*, January 2010.
2. Federal Emergency Management Agency (FEMA), *Flood Insurance Rate Map (FIRM) of Maricopa County, Arizona and Incorporated Areas, Panel 1320 of 4425, Map Number 0413C1320L*, October 16, 2013.
3. Flood Control District of Maricopa County (FCDMC), *Drainage Design Manual for Maricopa County, Hydrology Volume*, February 2008.
4. Flood Control District of Maricopa County (FCDMC), *Drainage Design Manual for Maricopa County, Hydraulics Volume*, January 1996.
5. Kimley-Horn and Associates, Inc., *Final Drainage Report for Improvement Plans for Scottsdale Road and Chauncey Lane, Crossroads East Planning Unit IV*, August 2012.
6. City of Phoenix, *Storm Water Policies and Standards*, December 2013.
7. Kimley-Horn and Associates, Inc., *Final Drainage Report for Bell Lexus of North Scottsdale*, Scottsdale, Arizona, 2012.
8. Wood Patel and Associates, *Final Drainage Report for the Interim Regional Drainage Channel* October 2008

***Appendix A***

Site Location Map and Legal Descriptions

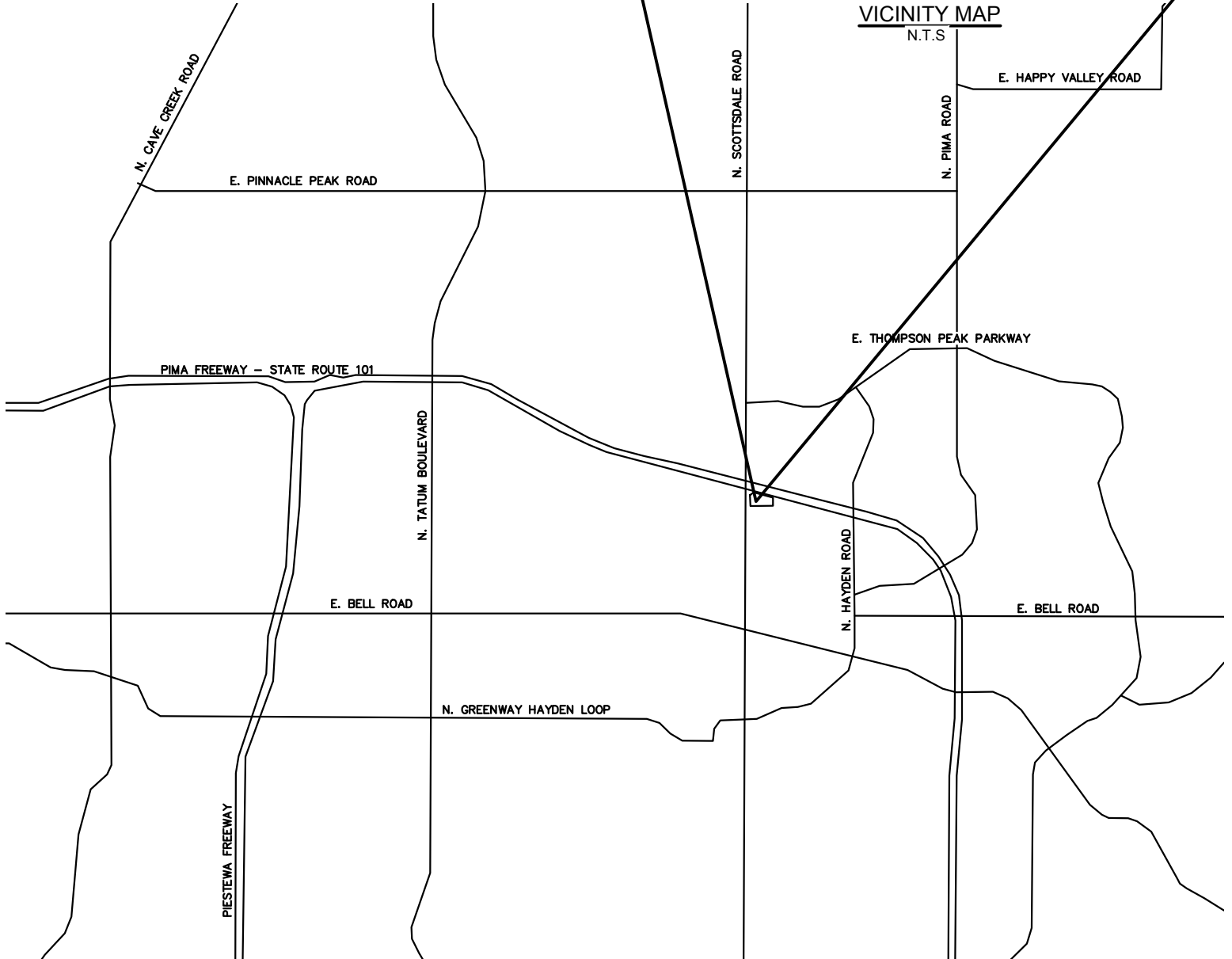
## PROJECT INFORMATION

SITE ADDRESS: 18777 N. SCOTTSDALE  
ROAD SCOTTSDALE, ARIZONA 85255



### VICINITY MAP

N.T.S



***Appendix B***

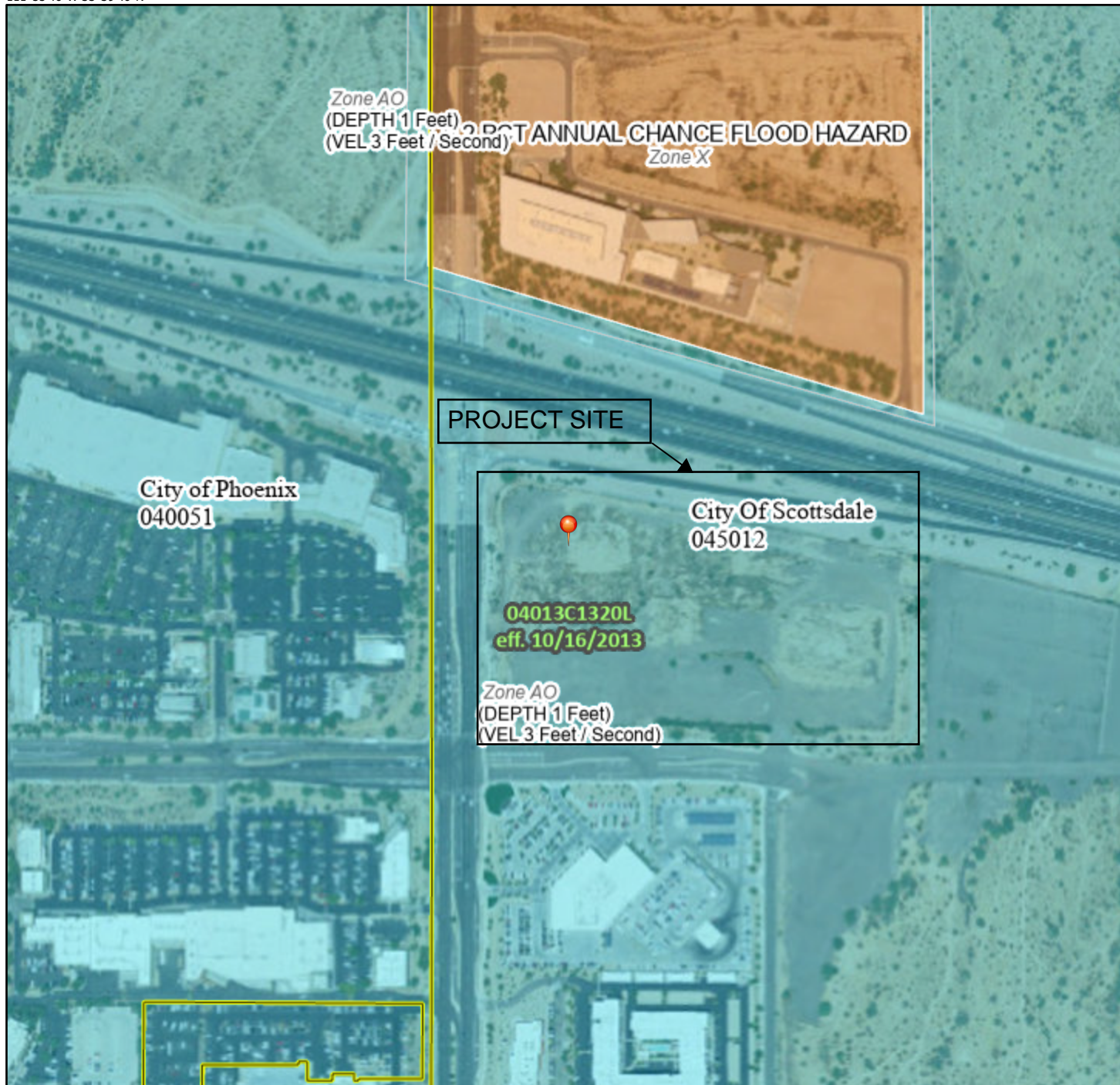
**FEMA Flood Insurance Rate Map (FIRM)**



# National Flood Hazard Layer FIRMette



111°55'46"W 33°39'40"N



0 250 500 1,000 1,500 2,000 Feet 1:6,000

Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

## Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
		Regulatory Floodway
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
OTHER AREAS		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
GENERAL STRUCTURES		Area of Undetermined Flood Hazard Zone D
		Channel, Culvert, or Storm Sewer
OTHER FEATURES		Levee, Dike, or Floodwall
		Cross Sections with 1% Annual Chance Water Surface Elevation
OTHER FEATURES		Coastal Transect
		Base Flood Elevation Line (BFE)
OTHER FEATURES		Limit of Study
		Jurisdiction Boundary
OTHER FEATURES		Coastal Transect Baseline
		Profile Baseline
OTHER FEATURES		Hydrographic Feature
		Digital Data Available
MAP PANELS		No Digital Data Available
		Unmapped



The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on **11/22/2021 at 1:30 PM** and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

*Appendix C*

Crossroads East Final Drainage Report





## ***FINAL DRAINAGE REPORT***

**Improvement plans for Scottsdale  
Road and Chauncey Lane; and**

**Crossroads East Planning Unit IV**

**Scottsdale, Arizona**

**Plan check # 2519-2, 1442-12**

Plan #	1442-12
Case #	
Q-S #	
<input checked="" type="checkbox"/> Accepted	
<input type="checkbox"/> Corrections	
M. Rahmann	8-14-12
Reviewed By	Date

**Prepared For:**

***Diversified Partners, LLC***

191235025  
August 2012  
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Kimley-Horn  
and Associates, Inc.

# ***FINAL DRAINAGE REPORT***

## **Improvement plans for Scottsdale Road and Chauncey Lane; and**

## **Crossroads East Planning Unit IV**

**Scottsdale, Arizona  
Plan check # 2519-2, 1442-12**

### **Prepared For:**

*Diversified Partners, LLC  
7500 E. McDonald Drive  
Suite 100A  
Scottsdale, Arizona 85250*

### **Prepared By:**

*Kimley-Horn and Associates, Inc.  
7740 North 16<sup>th</sup> Street  
Suite 300  
Phoenix, Arizona 85020*



191235025  
August 2012  
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<b><u>Section</u></b>	<b><u>Page No.</u></b>
<b>1.0 Introduction</b>	<b>3</b>
1.1 Project Description	3
1.2 Site Location	3
1.3 Purpose	3
1.4 Objectives	3
<b>2.0 Description of Existing Drainage Conditions and Characteristics</b>	<b>5</b>
2.1 General Description	5
2.2 Existing Sale Parcel Drainage Conditions	5
2.3 Existing Remainder of Planning Unit IV Drainage Conditions	7
2.4 Existing Off-site Drainage Conditions	7
2.5 Context Relative to Adjacent Projects and Improvements	7
2.6 FEMA Flood Hazard Areas	7
<b>3.0 Proposed Drainage Plan</b>	<b>9</b>
3.1 General Description	9
3.2 Proposed Sale Parcel Conditions	9
3.3 Proposed Remainder of Planning Unit IV Conditions	11
3.4 Proposed Off-site Conditions	11
3.5 Future Conditions	12
3.6 Storm Water Storage Requirements	12
3.7 Pre- and Post-Development Runoff Characteristics at Concentration Points	14
3.8 Proposed Drainage Structures or Special Drainage Facilities	15
3.9 Project Phasing	15
<b>4.0 Special Conditions</b>	<b>16</b>
4.1 404 Discussion	16
<b>5.0 Data Analysis Methods</b>	<b>17</b>
5.1 Hydrologic Procedures, Parameter Selection, and Assumptions	17
5.2 Hydraulic Procedures, Methods, Parameter Selection, and Assumptions	18
5.3 Storm Water Storage Calculation Methods and Assumptions	19
<b>6.0 Conclusion</b>	<b>20</b>
6.1 Overall Project	20
<b>7.0 References</b>	<b>22</b>

**List of Tables**

Table 1: On-site Detention Volume	14
-----------------------------------	----

**List of Figures in Appendix (Exhibits)**

Figure 1: Context Aerial plan
Figure 2: Grading and Drainage Plan
Figure 3: Hydrologic Delineation Map
Figure 4: Existing Conditions Topographic Map
Figure 5: Site Basin Delineation
Figure 6: HEC-RAS Sections Exhibit
Figure 7: Enlarged Sub Basin Delineation

**List of Appendices**

A	Site Location Map and Legal Description
B	FEMA Federal Insurance Rate Map (FIRM)
C	Hydrologic Calculations
D	Hydraulic Calculations
E	Exhibits
F	Dibble Drainage Report
G	Wood-Patel Drainage Report
H	Corp of Engineers Correspondence
I	Warning and Disclaimer Form

## **1.0 Introduction**

### **1.1 Project Description**

Diversified Partners, LLC is proposing development of a portion of Crossroads East Planning Unit IV (Planning Unit IV) at the southeast corner of Scottsdale Road and Mayo Boulevard for commercial use. The project is anticipated to consist of perimeter roadway and utility infrastructure for future multiple buildings with associated parking improvements.

### **1.2 Site Location**

Proposed development, hereinafter referred to as the “sale parcel”, encompasses approximately 29.4± gross acres in a portion of the Northwest Quarter of Section 33, Township 4 North, Range 4 East of the Gila and Salt River Base and Meridian in Maricopa County, Arizona. The sale parcel is a portion of Crossroads East Planning Unit IV (138± acres), and is zoned PCD. More specifically, the sale parcel is bounded by Mayo Boulevard and vacant undeveloped desert zoned PCD(C-4) to the north, vacant undeveloped desert zoned PCD to the east, vacant undeveloped desert and the Princess Resort zoned PCD to the south, and Scottsdale Road to the west. See *Appendix A* for the site location map and legal description; and, Figure 1 and 2 in Appendix E for a Context Aerial map and Grading and Drainage Plan.

### **1.3 Purpose**

This Final Drainage Report for the Planning Unit IV is intended to satisfy the storm drainage master planning stipulation number 2.5 for Zoning Case 19-ZN-2002 with regards to Planning Unit IV, as well as more specific guidelines for the aforementioned commercial development infrastructure (sale parcel) in accordance with the City of Scottsdale drainage guidelines and standards. This report provides a description of the current storm water drainage patterns and systems, a description of required and proposed drainage off-site improvements, and outlines anticipated phasing for Planning Unit IV and the sale parcel.

### **1.4 Objectives**

This final report provides a drainage plan for Planning Unit IV and the sale parcel that is intended to meet the drainage standards and guidelines of the City of Scottsdale and the Flood Control District of Maricopa County (FCDMC). In particular, the report will demonstrate the following:

1. Off-site storm water from the north being routed around the sale parcel development and discharging to the box culvert under Scottsdale Road at Princess Drive; consistent with current drainage patterns.
2. A delineation of land east and west of the natural drainage divide (hydrologic divide) that bisects Planning Unit IV; and, how drainage will be handled on each side.



3. Sale parcel development designating on and off-site drainage facilities, including temporary and permanent detention basins, for the 100-year, 2-hour storm event.
4. Temporary and permanent drainage facilities having positive outfall; and, any detained storm water being disposed of within 36 hours.
5. Drainage facilities being designed such that the 100-year, 2-hour post-development flow is collected and conveyed in such a manner as to not cause damage to buildings and property.
6. Future drainage requirements for the remainder of Planning Unit IV.

## 2.0 Description of Existing Drainage Conditions and Characteristics

### 2.1 General Description

Planning Unit IV's existing drainage conditions and characteristics have been classified into two areas, the sale parcel and the remainder of Planning Unit IV (or simply "remainder"), per the following descriptions:

#### Sale Parcel

This area consists of 29.4 gross acres of commercial development from the Chauncey Lane alignment to Mayo Boulevard, and from Scottsdale Road to the 73<sup>rd</sup> Place alignment.

#### Remainder of Planning Unit IV

This area consists of the remainder of acreage of Planning Unit IV from the sale parcel limits to Loop 101 and the Miller Road alignment, south to Princess Road and east to Scottsdale Road.

### 2.2 Existing Sale Parcel Drainage Conditions

The sale parcel currently consists of vacant desert and a seasonal use facility with an asphalt and gravel parking area. The sale parcel is bounded on the west by Scottsdale Road, on the north by Mayo Boulevard, on the east by the proposed east right-of-way of 73<sup>rd</sup> Place, and on the south by the proposed south right-of-way of Chauncey Lane.

The general topography of the sale parcel area is mildly sloping terrain at approximately 2%. A hydrologic divide bisects the sale parcel directing drainage to two separate facilities – Reach 11 (Dike 2) in the City of Phoenix and the TPC (Dike 3) in the City of Scottsdale (see Figure 3 of *Appendix E*). Storm water from land west of the hydrologic divide flows southwest toward the intersection of Scottsdale Road and Chauncey Lane, it then proceeds south along the east side Scottsdale Road in a swale to a box culvert under Scottsdale Road at Princess Boulevard where it is conveyed to Reach 11. An existing double-barrel 10'x3' arch culvert discharges off-site storm water onto the sale parcel at its northeast corner, west of the hydrologic divide (See photos 1 and 2 below). Storm water from this culvert proceeds south to a temporary detention basin at the center of the sale parcel, where it connects to "West Wash" identified on Figure 4 in *Appendix E*. "West Wash" flows southwest toward the intersection of Scottsdale Road and Chauncey Lane to the previously noted roadside swale that connects to the existing box culvert under Scottsdale Road at Princess Boulevard.



Photo 1: Downstream outlet from 10'x3' arch culvert.



Photo 2: Upstream Inlet from 10'x3' arch culvert.

Storm water from land east of the hydrologic divide flows south/southeast toward “East Wash” identified on Figure 4 in *Appendix E*. “East Wash” flows south and intersects with



an existing channel along the north side of Princess Boulevard, continuing on to the TPC via a box culvert under Princess Boulevard.

### **2.3 Existing Remainder of Planning Unit IV Drainage Conditions**

The remainder of Planning Unit IV currently consists of vacant desert and a gravel parking area along the Loop 101. The remainder is bounded on the west by Scottsdale Road and the sale parcel, on the north by Loop 101, on the east by the proposed Miller Road alignment, and the south by Princess Boulevard.

The general topography of the remainder is mildly sloping terrain at approximately 2%. A hydrologic divide bisects a portion of the remainder directing drainage to two separate facilities – Reach 11 (Dike 2) in the City of Phoenix and the TPC (Dike 3) in the City of Scottsdale (see Figure 3 of *Appendix E*). Storm water from land west of the hydrologic divide flows southwest toward a box culvert under Scottsdale Road at Princess Boulevard where it is conveyed to Reach 11.

Storm water from land east of the hydrologic divide flows south/southeast toward “East Wash” identified on Figure 4 in *Appendix E*. “East Wash” flows south and intersects with an existing channel along the north side of Princess Boulevard, continuing on to the TPC via a box culvert under Princess Boulevard. Two existing culverts under Loop 101 discharge off-site storm water onto the remainder along its north boundary, east of the hydrologic divide. Storm water from these culverts proceeds south in “East Wash” identified on Figure 4 in *Appendix E*. “East Wash” flows south toward Princess Boulevard to the previously noted roadside channel that connects to the existing box culvert under Princess Boulevard.

### **2.4 Existing Off-site Drainage Conditions**

Four box culverts under the Loop 101 exist north of Planning Unit IV. The two western most box culverts (See Figure 4) discharge to arch culverts that combine to an open channel that is routed around property that is not part of Planning Unit IV; bringing flow south under Mayo Boulevard onto the sale parcel. The two eastern most box culverts (See Figure 4) discharge directly onto the gravel parking area on the remainder of Planning Unit IV. Off-site flows proceed through Planning Unit IV as described in Sections 2.2 and 2.3.

### **2.5 Context Relative to Adjacent Projects and Improvements**

The proposed sale parcel is located south of Mayo Boulevard, east of Scottsdale Road, North of the proposed alignment of Chauncey Lane, and west of the proposed 73<sup>rd</sup> Street alignment. See Figure 1 in *Appendix E* for Context Aerial of the site.

### **2.6 FEMA Flood Hazard Areas**

The sale parcel site is located in Flood Zone “A” according to the Flood Insurance Rate Map 04013C1245H, dated September 30, 2005. Zone “AO” is designated by FEMA as “areas of flood depths of 1 foot (usually sheet flow on sloping terrain) average depths



determined for areas of alluvial fan flooding, velocities also determined.” Refer to Appendix B for the FEMA FIRMette map for the site. An elevation certificate will be required for any building to be constructed in this flood hazard designation.



### **3.0 Proposed Drainage Plan**

#### **3.1 General Description**

Planning Unit IV's proposed drainage conditions and characteristics remain classified into two areas, the sale parcel area and the remainder of Planning Unit IV (or simply "remainder"), per the following descriptions:

##### Sale Parcel

This area consists of 29.4 gross acres of commercial development from the Chauncey Lane alignment to Mayo Boulevard and from Scottsdale Road to the 73<sup>rd</sup> Place alignment.

##### Remainder of Planning Unit IV

This area consists of the remainder of acreage of Planning Unit IV from the sale parcel limits to Loop 101 and the Miller Road alignment, south to Princess Road and west to Scottsdale Road.

In the analysis of the proposed drainage conditions the following items were considered:

- Area Types (asphaltic pavement, building, and desert landscaping)
- Magnitude of areas
- Slopes
- Storm Drain
- Detention Basins

#### **3.2 Proposed Sale Parcel Conditions**

The sale parcel proposes a combination of in-kind contribution and detention for the 100-year, 2-hour storm event. In-kind contribution, in the form of a regional drainage channel, will be used to convey off-site flows around the sale parcel and for direct drainage of land west of the hydrologic divide. Detention will be used for land east of the hydrologic divide. To accommodate the off-site roadway drainage design of 73<sup>rd</sup> Place, the hydrologic divide was modified along the western boundary of 73<sup>rd</sup> place with an equivalent land area exchange between the land east and west of the hydrologic divide to maintain respective drainage areas and flows. See Figure 5 (Site Basin Delineation) for adjusted hydrologic divide location in relation to the Sale Parcel and Planning Unit IV.

### *West of Hydrologic Divide*

Sale Parcel land west of the hydrologic divide is proposed to be captured in a channel/box culvert along Scottsdale Road. No permanent site surface or underground retention is required for this area due to the in-kind contribution and construction of a regional drainage channel/culvert along Scottsdale Road. The regional drainage channel's construction is planned to coincide with development of the sale parcel. It is the sale parcel developer's preference to utilize a box culvert to convey storm water around the site from Mayo Boulevard to Chauncey versus an open channel. South of Chauncey, the box culvert discharges to an open channel. If the development preferences for the sale parcel change from a box to an open channel, an amended drainage study will be provided to reflect that change.

Interim stormwater run-off from the site, prior to full development, will be captured in two temporary basins that will drain via catch basins connected to the proposed box culvert with 30" RCP. The temporary basins will collect the 100-year 2-hour storm water runoff from the sale parcel and bleed off the storm water through the aforementioned storm drain connections. Upon full development of the sale parcel, the temporary basins will be removed, the existing storm drain connections can be extended through the site. Additional storm drain connections to the box culvert may be added to accommodate the fully-developed 100 year peak flow. Locations and sizes of additional storm drain connections will be determined based upon the individual site development drainage plans.

Sale Parcel land west of the hydrologic divide is identified as basin ASLD1 in Figure 5 (*Appendix E*) with a concentration point of ASLDCT. Based upon the previously prepared Wood Patel HEC-1 model, with modifications outlined in section 5.1, the associated flows from the ASLD1 basin and the combined 100yr peak flow (on-site and off-site) at this concentration point are calculated to be 114 and 317 cfs, respectively. See Figure 5 (*Appendix E*) for the Site Basin Delineation Map Exhibit.

### *East of Hydrologic Divide*

Drainage from the 100-year, 2-hour storm for land east of the hydrologic divide will be detained in a multiple surface detention basins located on the west side of the proposed 73<sup>rd</sup> Place alignment. These detention basins will drain to one another via storm drain pipes with orifice plates to restrict disposal rates ultimately out-falling to the southeast to the "East Wash", consistent with the current drainage pattern. The east side of 73<sup>rd</sup> Place and the south side of Chauncey Lane will drain to a roadside swale, discharging to the "East Wash" as an interim condition. The combined peak flow of the interim roadside swale and the bleed off basins is less than the undeveloped peak flow for the area discharging to the "East Wash," see Appendix D for calculations. Flows will continue on their current path to the box culvert that crosses south under Princess Boulevard and outfalls into the TPC golf course. See Figure 5 (*Appendix E*) for Site Basin Delineation Map Exhibit.

Future development along the east side of 73<sup>rd</sup> Place and south side of Chauncey Lane will be responsible for detaining the 100-year 2-hour storm for their adjacent half streets, unless a master drainage solution for the east of the hydrologic divide has been developed

### **3.3 Proposed Remainder of Planning Unit IV Conditions**

The remainder of Planning Unit IV proposes a combination of in-kind contribution and future detention for the 100-year, 2-hour storm event. In-kind contribution, in the form of a regional drainage channel, will be used for drainage from land west of the hydrologic divide. Drainage from land east of the hydrologic divide will continue to on its historic path until future development occurs.

#### *West of Hydrologic Divide*

Remainder land west of the hydrologic divide is proposed to be captured in a channel along the east side of Scottsdale Road. No permanent site surface or underground retention will be provided for this area due to the in-kind contribution and construction of a regional drainage channel/culvert along Scottsdale Road. The regional drainage channels construction is planned to coincide with development of the sale parcel. Interim storm water runoff from the remainder parcel shall sheet flow into the open channel along Scottsdale Road. Future development of the remainder parcel may add storm drain connections to the drainage channel to accommodate proposed site development.

Remainder land west of the hydrologic divide is identified as basin ASLD2 in Figure 5 (*Appendix E*) with a concentration point of CPPRIN. Based upon the previously prepared Wood-Patel HEC-1 model, with modifications outlined in section 5.1, the associated flows from the ASLD2 basin and the combined 100 yr peak flow (on-site and off-site) at this concentration point are calculated to be 84 and 351 cfs, respectively. See Figure 5 (*Appendix E*) for Site Basin Delineation Exhibit.

#### *East of Hydrologic Divide*

The future development of this area will detain the 100-year, 2-hour storm in multiple surface detention basins as warranted by proposed improvements. The detention basins should be designed to discharge to an existing wash or drainage conveyance channel that ultimately connects to the existing drainage channel along the north side of Princess Boulevard, consistent with the current drainage patterns.

### **3.4 Proposed Off-site Conditions**

Off-site storm water runoff from north of the 101 onto Planning Unit IV is proposed to be handled in the following manner.

#### *Western two box culverts – Sale Parcel*

The western two box culverts that convey storm water from north of the Loop 101 onto Planning Unit IV currently discharge onto the proposed sale parcel, west of the



hydrologic divide. With the development of the sale parcel, per the preference of the sale parcel owner, off-site storm water will be routed to the east side of Scottsdale Road and then south to Chauncey Lane via two 8'x3' box culverts (see *Appendix D* for calculations). South of Chauncey Lane, along the east side of Scottsdale Road, off-site storm water will be conveyed in an interim trapezoidal open channel with grade control structures to the existing box culvert under Scottsdale Road that connects to the Reach 11 (Dike 2). The flows in the box culvert and the interim open channel have been sized to accommodate the future fully-developed portions of ASLD1 and ALS2 drainage basins. See Figure 5 (*Appendix E*) for site basin delineation map.

#### *Eastern two box culverts - Remainder*

Future development of this area will dictate how off-site flows are managed and routed to the existing channel on the north side of Princess Boulevard, consistent with the current drainage patterns.

It should be noted that discussions with the City of Scottsdale have revealed the channel north of Princess Boulevard is currently experiencing notable erosion and sediment transport. Drainage studies in conjunction with future development should explore channel armoring options.

### **3.5 Future Conditions**

No future drainage impacts are anticipated for the sale parcel due to the proposed installation of the regional drainage channel/box culvert along the east side of Scottsdale Road from Mayo Boulevard to Princess Drive. The channel/box culvert adjacent to the sale parcel from Mayo Boulevard to Chauncey Lane will be constructed in its final configuration in accordance with the City of Scottsdale scenic corridor guidelines. The channel south of Chauncey Lane to the culvert under Scottsdale Road at Princess Boulevard will be an interim channel that may be modified for the needs of the adjacent future development. Individual future parcels of remainder Planning Unit IV will be responsible for their respective 100-year 2-hour detention depending upon their location in relation to the hydrologic divide.

### **3.6 Storm Water Storage Requirements**

Sale Parcel surface detention basins have been designed to detain the on-site runoff volume associated with the 100-year, 2-hour storm for land east of the hydrologic divide. No permanent storm water storage will be provided for land west of the hydrologic divide due to the approved in-kind contribution to build a regional drainage channel along the east side of Scottsdale Road. Two interim storm water detention basins are proposed along Scottsdale Road next to the box culvert to allow for capturing of site generated storm water into the box culvert prior to full development.

Detention volume will be provided by multiple surface retention basins along the proposed 73<sup>rd</sup> Place and Chauncey Road alignments. The side slopes for the retention basin are a maximum of 4:1 with a maximum depth of 3 feet.

Future development within the remainder of Planning Unit IV will be required to provide at least one foot of freeboard from the basin overflow elevation to the finished floor elevation of any proposed buildings, in accordance with the City of Scottsdale design standards and policy manual.

The following Table summarizes proposed detention to be constructed as part of the sale parcel development by basin name, type, total contributing area to the basin, runoff coefficient for the contributing area, and the required and provided detention volume for the sale parcel and impacted areas of remainder land.

**Table 1: On-site Detention Volume**

Basin	Land Use	Runoff Coefficient	Drainage Area (ft <sup>2</sup> )	Required Volume (ft <sup>3</sup> )	Provided Volume (ft <sup>3</sup> )	Surplus (ft <sup>3</sup> )
A	Landscaping	0.45	3,703	350		
	Pavement	0.95	11,890	2,371		
			15,593	2,721	3,142	421

Basin	Land Use	Runoff Coefficient	Drainage Area (ft <sup>2</sup> )	Required Volume (ft <sup>3</sup> )	Provided Volume (ft <sup>3</sup> )	Surplus (ft <sup>3</sup> )
B	Landscaping	0.45	5,220	493		
	Pavement	0.95	32,641	6,509		
			37,861	7,002	7,588	586

Basin	Land Use	Runoff Coefficient	Drainage Area (ft <sup>2</sup> )	Required Volume (ft <sup>3</sup> )	Provided Volume (ft <sup>3</sup> )	Surplus (ft <sup>3</sup> )
C	Landscaping	0.45	13,164	1,244		
	Pavement	0.95	66,572	13,276		
			79,736	14,519	17,843	3,323

Basin	Land Use	Runoff Coefficient	Drainage Area (ft <sup>2</sup> )	Required Volume (ft <sup>3</sup> )	Provided Volume (ft <sup>3</sup> )	Surplus (ft <sup>3</sup> )
D (Temp Basin)	Landscaping	0.45	449,197	42,432		
	Pavement	0.95	0	0		
			449,197	42,432	44,212	1,780

Basin	Land Use	Runoff Coefficient	Drainage Area (ft <sup>2</sup> )	Required Volume (ft <sup>3</sup> )	Provided Volume (ft <sup>3</sup> )	Surplus (ft <sup>3</sup> )
E (Temp Basin)	Landscaping	0.45	396,700	37,473		
	Pavement	0.95	0	0		
			396,700	37,473	39,762	2,289

The detention basins are designed such that the 100-year, 2-hour runoff volume is disposed of via pipe flow and overland flow, See Figure 5 in *Appendix E* for Basin Delineation.

### 3.7 Pre- and Post-Development Runoff Characteristics at Concentration Points

The existing site consists primarily of vacant undeveloped desert. Current topography shows the site draining from northeast to southwest. Upon site development, Sale Parcel storm water west of the hydrologic divide will sheet flow to catch basins and then be conveyed through underground storm drain to the regional channel/box culvert along the east side Scottsdale Road. Sale Parcel storm water east of the hydrologic divide will sheet flow to curb openings/scuppers and then be conveyed through underground storm



drain to a series of connected detention basins that will allow the water to sheet flow south to the existing channel along the north side of Princess Boulevard, consistent with the current drainage patterns.

### **3.8 Proposed Drainage Structures or Special Drainage Facilities**

Aesthetics and site access needs dictate that a portion of the regional drainage channel be proposed as a double-barrel box culvert. This box culvert is anticipated to connect to the existing culvert under Mayo Boulevard and extend around the perimeter of the Sale Parcel to the south side of the proposed Chauncey Lane alignment. The box culvert has been designed to accommodate the 100-year storm peak flow as a dry box. The final design will include a drainage easement, dedicated to the City of Scottsdale.

### **3.9 Project Phasing**

This project will be constructed in a multiple phases as follows:

1. Regional Drainage Channel, 73<sup>rd</sup> Place, Chauncey Lane, and rough grading the remaining Sale Parcel area for site development.
2. Sale Parcel on-site development/improvement. Site development may occur in multiple sub-phases (A, B, C, etc) as market conditions warrant.
3. Remainder portions of Planning Unit IV. Development may occur in multiple sub-phases (A, B, C, etc) as market conditions warrant.

## 4.0 Special Conditions

### 4.1 404 Discussion

Per correspondence with the U.S. Army Corp of Engineers 404 jurisdictional washes are impacted by the proposed Regional Channel improvements, roadway improvements, and temporary drainage basins. A Nationwide permit with the Corp of Engineers has been obtained for the disturbance of the existing 404 jurisdictional wash on-site. See Appendix H for Corp of Engineers Certificate of Compliance with Department of the Army Nationwide Permit.

## 5.0 Data Analysis Methods

### 5.1 Hydrologic Procedures, Parameter Selection, and Assumptions

#### *West of Hydrologic Divide*

Hydrologic calculations for land west of the hydrologic divide were performed using the computer program HEC-1 as outlined for FCDMC Drainage Design Manual Volume I. The previously prepared IIEC-1 model for *Interim Regional Drainage Channel* prepared by Wood-Patel and Associates, Inc., was modified to maintain the previous NOAA 2 rainfall data with a change to the sale parcel hydrologic characteristics to reflect the fully developed condition of Planning Unit IV west of the hydrologic divide. In addition the HEC-1 model was modified to reflect the routing of off-site storm water through a box culvert, instead of an open channel to Chauncey Lane (per sale parcel owner's preference for box culvert versus channel), and the subdivision of the previous study's ASLD basin into a north basin, ASLD1, and a south basin, ASLD2.

The NOAA 2 rainfall data used in the previous study was unchanged from the previous approved HEC-1 model. The fully developed condition for land west of the hydrologic divide was achieved by increasing the impervious value of the of sub basin ASLD1 and ASLD2 to 95%. The results of the revised HEC-1 model are located in *Appendix C*. Figure 5, which identifies the drainage sub-basins and concentration points associated with the HEC-1 model, is located in *Appendix E*.

To accommodate the roadway alignment and grading of 73<sup>rd</sup> Place through the northern end of the hydrologic divide, a land swap between the east and west was utilized. The portion of land located east of the western right of way line of 73<sup>rd</sup> Place to the hydrologic divide line was exchanged for the equal land area located along the southern portion of the sale parcel See Figure 5, Site Basin Delineation, for the land swap area locations. Since the land area exchange is the same, the flow quantity and magnitudes east and west of the hydrologic divide should remain unchanged.

#### *East of Hydrologic Divide*

Hydrologic calculations for land east of the hydrologic divide were performed using the rational equation in the FCDMC Drainage Design Manual Volume I, which is limited to drainage areas of up to 160 acres using NOAA 14 rainfall data. A weighted runoff coefficient was used for the site for the large amount of desert landscaping located adjacent to 73<sup>rd</sup> Place and Chauncey Lane in the required landscape setbacks. All other drainage sub basins were modeled using a fully developed pavement runoff coefficient to account for future developments.

For analysis of the sale parcel east of the hydrologic divide, the site was sub-divided into sixteen sub-basins (ten sub-basins for the sale parcel, west half street of 73<sup>rd</sup> Place, and north half street of Chauncey Lane; six sub-basins for the remaining half streets) consisting of the pavement, landscaping, and future commercial. For each sub-basin, the

rational equation was used to calculate the peak flow at each concentration point for each basin. The results of the rational method are located in Appendix C. Figure 7, which identifies the drainage sub-basins, is located in *Appendix E*.

## 5.2 Hydraulic Procedures, Methods, Parameter Selection, and Assumptions

### *West of Hydrologic Divide*

The regional drainage channel along the east side of Scottsdale Road was evaluated using the computer programs StormCAD, by Bentley, for the box culvert routing, and HEC-RAS for the open channel routing and backwater analysis.

Using StormCAD the proposed box culvert from north of Mayo Boulevard to south of Chauncey Lane was analyzed for the 100-year peak flow of 317 cfs at the outlet (peak flow calculated at culvert outfall from modified HEC-1) with a total of 8 cfs being captured between inlets CB-50 and CB-55 and 309 cfs entering the upstream culvert entrance (conservative model due to future connections and flows at each connection). Headlosses at the bends/junctions of the box culverts were individually calculated and included in the analysis as a user defined values.

Using HEC-RAS, the interim channel south of Chauncey Lane to the existing box culvert that crosses Scottsdale Road at Princess Boulevard was analyzed for the peak flow of 351 cfs (peak flow calculated at Box culvert under Scottsdale Road from modified HEC-1 model). Cross sections were taken at the upstream and downstream of each grade control structure (See Figure 6: HEC-RAS Cross Section Locations). The upstream boundary condition was set to match the water surface elevation calculated at the outfall of the double 8'x3' box culvert. The downstream boundary condition was set at the water elevation that would match the calculated head for the dry crossing at the culvert entrance per the *Scottsdale Road Drainage Report* prepared by Dibble and Associates, Inc., in March 2009. Rip rap and grade control structures are proposed to maintain velocities below 6 feet per second in the main channel areas. Manning's n values for the channel were selected from the *Maricopa County Flood Control District Hydraulics Manual*.

### *East of Hydrologic Divide*

The sale parcel site east of the hydrologic divide is divided into sixteen sub-basins that drain into an on-site detention basin. As described in Section 5.1, ten of the sub-basins include the sale parcel land and adjacent half street right-of-ways, and the other six include the remaining half street right-of-ways and the impacted remainder land. See Figure 7 in Appendix F for enlarged sub-basin boundaries.

All flows for proposed conditions were determined using the rational method as outlined by the *Drainage Design Manual by Maricopa County Flood Control District*. Due to the small nature of the watersheds for the individual sub-basins, a minimum time of concentration of five minutes was assumed. All of the drainage basins assume a runoff coefficients of 0.95 (100-year) and 0.85 (10-year) with the exception of the landscape

sub-basins. Due to the relatively large amount of landscaping in these areas, a weighted runoff coefficient was used for future landscape areas only (all other basins used a fully developed runoff coefficient). Per the *City of Scottsdale Design Standards and Policy Manual* (January 2010), the runoff coefficient for desert landscaping (no impervious weed barrier) is 0.45 for Hydrologic Soil Group B. The peak flows at the sub-basin concentration points were calculated using the rational method using NOAA 14 rainfall data (see *Appendix C* for hydrologic results).

The following criteria were used to size the proposed pipes and drainage inlets for on-site storm water conveyance and disposal:

- A maximum allowable 100-year ponding depth of 8 inches above the drainage inlet for roadway and contained within the road right-of-way.
- One dry lane in each direction for the 10-year spread in Chauncey Lane (Collector street classification).
- Stormwater contained within the curbs for the 10-year spread in 73<sup>rd</sup> Place (Local street classification).
- A maximum allowable 10-year ponding depth of 6 inches to contain all storm water runoff within the roadway. (6" depth max).
- Only negligible amount of flow is allowed to bypass the scuppers located at the hydrologic divide (less than 0.30 cfs)

Storm drain calculations and inlet calculations are included in Appendix D.

### 5.3 Storm Water Storage Calculation Methods and Assumptions

Storm water storage requirements were calculated per City of Scottsdale and Flood Control District of Maricopa County design standards. The standard formula for determining the required storage volumes for the 100-year, 2-hour storm is as follows:

Equation 2: Standard Formula for On-Site Storage Requirement

$$V_R = CPA/12$$

Where:

- $V_R$  = storage volume required (acre-feet)
- $C$  = weighted runoff coefficient
- $P$  = precipitation depth for 100-year, 2-hour event = 2.29 inches
- $A$  = contributing drainage area to basin (acres)

## 6.0 Conclusion

### 6.1 Overall Project

Based on the results of this final drainage report, the following can be concluded:

- Off-site storm water west of the hydrologic divide will be channelized (Regional Drainage Channel) and directed around the sale parcel.
- Off-site storm water east of the hydrologic divide will continue on its historic path.
- Sale Parcel drainage west of the hydrologic divide will be directed to the Regional Drainage Channel as part of the in-kind contribution.
- Storm drainage systems consisting of catch basins and storm drain pipe will be provided to collect and convey drainage to the Regional Drainage Channel.
- Surface detention will be provided to detain the post-development 100-year, 2-hour storm water for sale parcel land east of the hydrologic divide. Permanent basins for sale parcel site development and site development half-streets (west half of 73<sup>rd</sup> Place and north half of Chauncey Lane) will be provided on-site. Storm water for the east half of 73<sup>rd</sup> Place and the south half of Chauncey Lane will discharge into roadway swales with outfall to a natural wash.
- Surface detention basins east of the hydrologic divide will outfall/drain via pipe and overland flow toward the channel along Princess Boulevard.
- Storm drainage systems consisting of curb cuts, storm drain pipe, headwalls, and orifice plates will be provided to collect and convey drainage to the detention basins.
- Remainder site generated storm drainage will continue to flow in its current drainage pattern.
- Future building finish floor elevations will be designed at least fourteen inches above the ultimate site outfall elevation and at least 2 foot above the highest adjacent natural grade to provide one foot of clearance/freeboard from the depth of sheet flow.
- Based on the current Flood Insurance Rate Map (FRIM), the sale parcel is located in the Zone "AO". Any buildings in this Flood Zone will be designed above the depth of flow as indicated on the FIRM map with one foot of clearance/freeboard.
- Drainage easements are provided for the permanent and temporary surface detention basins and final Regional Drainage Channel/Culvert.

This final drainage report is intended to provide a level of assurance that the sale parcel and remainder of Planning Unit IV will adhere to all appropriate reviewing agency guidelines with respect to drainage and flood protection.

## 7.0 References

1. City of Scottsdale, *Design Standards and Policies Manual, Chapter 4: Grading and Drainage*, January 2010.
2. Dibble Engineering, Inc, *Drainage Report for Scottsdale Road Frank Lloyd Wright Blvd to Thompson Peak Parkway Segment 2*, March 2009.
3. Federal Emergency Management Agency (FEMA), *Flood Insurance Rate Map (FIRM) of Maricopa County, Arizona and Incorporated Areas, Panel 2160 of 4350, Map Number 04013C2160F*, September 30, 2005.
4. Flood Control District of Maricopa County (FCDMC), *Drainage Design Manual for Maricopa County, Hydrology Volume*, February, 2008.
5. Flood Control District of Maricopa County (FCDMC), *Drainage Design Manual for Maricopa County, Hydraulics Volume*, January, 1996.
6. Wood Patel and Associates, Inc, *Final Drainage Report for Interim Regional Drainage Channel*, October 2008.



## *Appendix A*

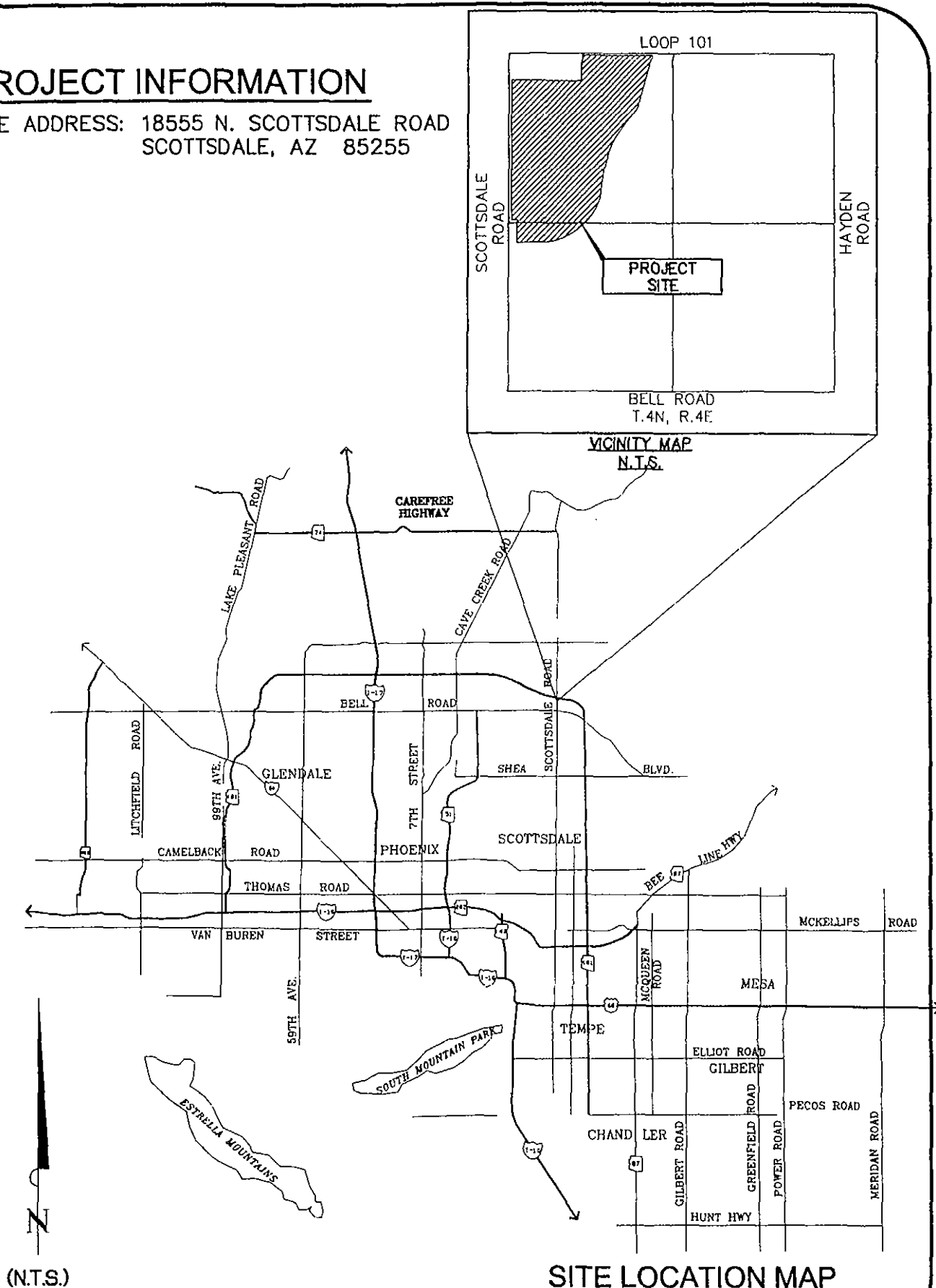
### Site Location Map and Legal Descriptions

LEGAL DESCRIPTION:

TRACT 3A, STATE PLAT NO. 16, SOUTH CORE, ACCORDING TO BOOK 324 OF MAPS,  
PAGE 50, RECORDS OF MARICOPA COUNTY, ARIZONA.

SITE ADDRESS: 18555 N. SCOTTSDALE ROAD  
SCOTTSDALE, AZ 85255

SITE ADDRESS: 18555 N. SCOTTSDALE ROAD  
SCOTTSDALE, AZ 85255



(N.T.S.)

## SITE LOCATION MAP



**Kimley-Horn  
and Associates, Inc.**



## ***Appendix B***

### FEMA Flood Insurance Rate Map (FIRM)



## *Appendix C*

### Hydrologic Calculations

*HEC-1 Calculations*

```

1.....
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1)
*   JUN 1998
*   VERSION 4.1
*
* RUN DATE 08AUG12 TIME 16:57:57
*
*.....

```

```

*.....
*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104
*
*.....

```

```

X   X XXXXXXX XXXXX      X
X   X X      X   X      XX
X   X X      X   X      X
XXXXXXX XXXX X   XXXXX X
X   X X      X   X      X
X   X X      X   X      X
X   X XXXXXXX XXXXX      XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION  
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,  
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION  
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1         ID      ONE SCOTTSDALE (STACKED 40S) POST DEVELOPMENT CONDITION 100-YR 6-HR STORM
2         ID      OFFSITE HYDROLOGY & ONSITE HYDROLOGY FOR AREA GOVERNED BY PRE-POST CRITERIA
3         ID      OPTION A - ASLD CHANNEL
4         ID      FILE: 100YR-N2.DAT
5         ID      OPTION B - 34.1 ACRES OF ASLD PARCEL
6         ID
7         ID      BASED ON MODELS PREPARED BY: ROBERT L. WARD, P.E., CONSULTING ENGINEER
8         ID
9         ID      PR5W-100.6I
10        ID      C1.6I (CENTER DRIVE PROJECT)
11        ID      S40EX100.6I (STACKED 40S EXISTING CONDITION)
12        ID
13        ID      ALL CURVE NUMBERS ADJUSTED TO 6-HOUR VALUES ON AUGUST 13, 2002
14        ID      100-YEAR, 6-HOUR HYPOTHETICAL STORM
15        ID
16        ID      AREAL RAINFALL REDUCTION IS BASED ON A 14 SQUARE MILE STORM.
17        ID
18        ID      *DIAGRAM
19        ID      IT      5
20        ID      IO      5
21        ID
22        ID      *
23        ID      * BEGIN GRAYHAWK - VILLAGE 1 DRAINAGE PLAN
24        ID      * PREPARED BY: GILBERTSON ASSOCIATES, INC., HEC-1 FILE: UDPLAN.DAT.
25        ID      * THIS GILBERTSON MODEL USES SCS UNIT HYDROGRAPH METHODOLOGY.
26        ID      * THE ORIGINAL MODEL WAS BASED ON A 1-MINUTE COMPUTATION INTERVAL.
27        ID      *
28        KK      1A1
29        KM      EXCESS RUNOFF FROM SUBAREA 1A1
30        KM      RAINFALL REGION 3
31        BA      .0188
32        PH      14      0.76      1.50      2.54      2.81      2.99      3.33
33        LS      77      36
34        UD      0.08
35        KK      DET1A1
36        KM      DETENTION BASIN FOR SUBAREA 1A1
37        RS      1      STOR      0
38        SV      0      1.76
39        SQ      0      20
40        SE      0      3.0
41        ST      3.0      15      2.8      1.5
42        KK      RA1-C4
43        KM      ROUTE OUTFLOW FROM DET1A1 TO CP1C4
44        KM      TRIANGULAR CHANNEL PER PLANS (1182-E-94 AND 190-E-95)
45        KM      SIDE SLOPE = 3:1 (H:V)
46        KM      MAX DEPTH = 1.35 FT.
47        RS      1      FLOW      -1
48        RC      0.025      0.025      0.025      670      0.0179
49        RX      0      0.5      1.0      5.04      5.05      9.1      9.5      10
50        RY      1.37      1.36      1.35      0      1.35      1.36      1.37

```

1

HEC-1 INPUT

PAGE 2

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
43        KK      1C4
44        KM      EXCESS RUNOFF FROM SUBAREA 1C4
45        BA      .005
46        LS      77      5
47        UD      .08

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48      KK      CP1C4
49      KM      COMBINE HYDROGRAPHS FROM RA1 C4 AND 1C4
50      HC      2

51      KK      RC4-C3
52      KM      ROUTE OUTFLOW FROM CP1C4 TO CP1C3I
53      KM      TRIANGULAR CHANNEL PER PLANS (1182-E-94 AND 190-E-95)
54      KM      SIDE SLOPE = 3:1 (H:V)
55      KM      MAX DEPTH = 1.5 FT.
56      RS      1      FLOW      -1
57      RC      0.025  0.025  0.025  400  0.020
58      RX      0      0.5      1.0  4.49  4.5      9      9.5      10
59      RY      1.52  1.51  1.5      0      0      1.5  1.51  1.52

60      KK      1Da3
61      KM      EXCESS RUNOFF FROM SUBAREA 1Da3
62      BA      .0148
63      LS      77      34
64      UD      .06

65      KK      DE1Da3
66      KM      DETENTION FOR SUBAREA 1Da3
67      KM      OUTLET IS A 18" RGRCP WITH AN 8" ORIFICE PLATE PER PLANS (905-E-95)
68      RS      1      STOR      0
69      SV      0      1.27
70      SQ      0      4
71      SE      0      3.0
72      ST      3.0  15      2.8  1.5

73      KK      1Da4
74      KM      EXCESS RUNOFF FROM SUBAREA 1Da4
75      BA      .01
76      LS      77      38
77      UD      .05

78      KK      CP1Da4
79      KM      COMBINE HYDROGRAPHS FROM 1Da4 AND DE1Da3
80      HC      2

81      KK      DE1Da4
82      KM      DETENTION FOR SUBAREA 1Da4
83      KM      OUTLET IS A 18" PVC WITH AN 8" ORIFICE PLATE PER PLANS (905-E-95)
84      RS      1      STOR      0
85      SV      0      0.76
86      SQ      0      4
87      SE      0      3.0
88      ST      3.0  15      2.8  1.5

```

HEC-1 INPUT

PAGE 3

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

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89      KK      1Da5
90      KM      EXCESS RUNOFF FROM SUBAREA 1Da5
91      BA      .004
92      LS      77      5
93      UD      .08

94      KK      CP1C3I
95      KM      COMBINE HYDROGRAHS FROM RC4-C3, 1Da5 AND DE1Da4
96      HC      3

97      KK      RC3-C3
98      KM      ROUTE OUTFLOW FROM CP1C3I TO DET1C3
99      KM      TRIANGULAR CHANNEL PER PLANS (1182-E-94 AND 190-E-95)
100     KM      SIDE SLOPE = 3:1 (H:V)
101     KM      MAX DEPTH = 2.35 FT.
102     RS      1      FLOW      -1
103     RC      0.025  0.025  0.025  850  0.005
104     RX      0      0.5      1.0  8.04  8.05  15.1  15.5  16
105     RY      2.37  2.36  2.35  0      0      2.35  2.36  2.37
*
* *START AT OFF-SITE BASIN ON THE NORTHEAST CORNER OF VILLAGE 1*
*

106     KK      Off-1A
107     KM      OFF-SITE CONTRIBUTING AREA LOCATED ON CITY'S LAND
108     BA      .012
109     LS      77
110     UD      .06

111     KK      1A2
112     KM      EXCESS RUNOFF FROM SUBAREA 1A2
113     BA      .004
114     LS      77      44
115     UD      .06

116     KK      1A3
117     KM      EXCESS RUNOFF FROM SUBAREA 1A3
118     BA      .006
119     LS      77      40
120     UD      .05

121     KK      CPA3
122     KM      COMBINE HYDROGRAPHS FROM 1A1, Off-1A AND 1A3
123     HC      3

124     KK      DET1A3
125     KM      DETENTION BASIN FOR SUBAREA 1A3
126     RS      1      STOR      0
127     SV      0      0.38

```

128 SQ 0 22  
 129 SE 0 2.5  
 130 ST 2.5 15 2.8 1.5  
 HEC-1 INPUT

PAGE 4

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

131 KK RA3-A6  
 132 KM ROUTE OUTFLOW HYDROGRAPH FROM DET1A3 TO DET1A6  
 133 KM TRAPEZOIDAL CHANNEL (ASSUMED)  
 134 KM SIDE SLOPE = 5:1 (H:V)  
 135 KM MAX DEPTH = 1.0 FT.  
 136 KM BOT.WIDTH = 19.0 FT.  
 137 RS 1 FLOW -1  
 138 RC 0.025 0.025 0.025 550 0.0145  
 139 RX 0 0.5 1.0 6 16 21 21.5 22.0  
 140 RY 1.02 1.01 1.0 0 0 1.0 1.01 1.02

141 KK 1A6  
 142 KM EXCESS RUNOFF FROM SUBAREA 1A6  
 143 BA .004  
 144 LS 77 44  
 145 UD .05

146 KK CPlA6  
 147 KM COMBINE HYDROGRAPHS FROM RA3-A6 AND 1A6  
 148 HC 2

149 KK DET1A6  
 150 KM DETENTION BASIN FOR SUBAREA 1A6  
 151 RS 1 STOR 0  
 152 SV 0 0.28  
 153 SQ 0 22  
 154 SE 0 2.5  
 155 ST 2.5 15 2.8 1.5

156 KK 1A5  
 157 KM EXCESS RUNOFF FROM SUBAREA 1A5  
 158 BA .016  
 159 LS 77 46  
 160 UD .07

161 KK CPlA5  
 162 KM COMBINE HYDROGRAPHS FROM DET1A6 AND 1A5  
 163 HC 2

164 KK DET1A5  
 165 KM DETENTION BASIN FOR SUBAREA 1A5  
 166 RS 1 STOR 0  
 167 SV 0 0.65  
 168 SQ 0 34  
 169 SE 0 2.5  
 170 ST 2.5 15 2.8 1.5

171 KK 1A4  
 172 KM EXCESS RUNOFF FROM SUBAREA 1A4  
 173 BA .010  
 174 LS 77 48  
 175 UD .07

HEC-1 INPUT

PAGE 5

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

176 KK RA4-A7  
 177 KM ROUTE OUTFLOW FROM DET1A4 TO DET1A7  
 178 KM TRAPEZOIDAL CHANNEL (ASSUMED)  
 179 KM SIDE SLOPE = 10:1 (H:V)  
 180 KM MAX DEPTH = 1.0 FT.  
 181 KM BOT.WIDTH = 10.0 FT.  
 182 RS 1 FLOW -1  
 183 RC 0.030 0.030 0.030 800 0.0175  
 184 RX 0 0.5 1.0 11 21 31 31.5 32.0  
 185 RY 1.02 1.01 1.0 0 0 1.0 1.01 1.02

186 KK DET1A4  
 187 KM DETENTION BASIN FOR SUBAREA 1A4  
 188 RS 1 STOR 0  
 189 SV 0 0.27  
 190 SQ 0 11  
 191 SE 0 2.5  
 192 ST 2.5 15 2.8 1.5

193 KK 1A7  
 194 KM EXCESS RUNOFF FROM SUBAREA 1A7  
 195 BA .008  
 196 LS 77 27  
 197 UD .05

198 KK CPlA7  
 199 KM COMBINE HYDROGRAPHS FROM DET1A5, DET1A4, AND 1A7  
 200 HC 3

201 KK DET1A7  
 202 KM DETENTION BASIN FOR SUBAREA 1A7  
 203 RS 1 STOR 0  
 204 SV 0 0.93  
 205 SQ 0 11  
 206 SE 0 2.5  
 207 ST 2.5 15 2.8 1.5

208 KK 1C1  
 209 KM EXCESS RUNOFF FROM SUBAREA 1C1  
 210 BA .024  
 211 LS 77 38  
 212 UD .09  
  
 213 KK CP1C1  
 214 KM COMBINE HYDROGRAPHS FROM DET1A7, AND 1C1  
 215 HC 2  
  
 216 KK DET1C1  
 217 KM DETENTION BASIN FOR SUBAREA 1C1  
 218 KM STORAGE VOLUME PER PLANS (405-E-95)  
 219 KM OUTLET IS A 18" RGRCP PER PLANS (405-E-95)  
 220 RS 1 STOR 0  
 221 SV 0 1.5  
 222 SQ 0 14

HEC-1 INPUT

PAGE 6

1  
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
  
 223 SE 0 3.6  
 224 ST 3.6 15 2.8 1.5  
  
 225 KK 1C2  
 226 KM EXCESS RUNOFF FROM SUBAREA 1C2  
 227 BA .024  
 228 LS 77 32  
 229 UD .08  
  
 230 KK CP1C2  
 231 KM COMBINE HYDROGRAPHS FROM DET1C1 AND 1C2  
 232 HC 2  
  
 233 KK DE1C2A  
 234 KM DETENTION BASIN FOR SUBAREA 1C2  
 235 KM STORAGE VOLUME PER PLANS (405-E-95)  
 236 KM OUTLET IS A 18" RGRCP PER PLANS (405-E-95)  
 237 RS 1 STOR 0  
 238 SV 0 0.39  
 239 SQ 0 14  
 240 SE 0 3.6  
 241 ST 3.6 15 2.8 1.5  
  
 242 KK DE1C2B  
 243 KM DETENTION BASIN FOR SUBAREAS 1C2  
 244 KM STORAGE VOLUME PER PLANS (405-E-95)  
 245 KM OUTLET IS A 18" RGRCP PER PLANS (405-E-95)  
 246 RS 1 STOR 0  
 247 SV 0 0.92  
 248 SQ 0 14  
 249 SE 0 3.6  
 250 ST 3.6 15 2.8 1.5  
  
 251 KK DE1C2C  
 252 KM DETENTION BASIN FOR SUBAREAS 1C2  
 253 KM STORAGE VOLUME PER PLANS (405-E-95)  
 254 KM OUTLET IS A 18" RGRCP PER PLANS (405-E-95)  
 255 RS 1 STOR 0  
 256 SV 0 0.54  
 257 SQ 0 14  
 258 SE 0 3.6  
 259 ST 3.6 15 2.8 1.5  
  
 260 KK 1C3  
 261 KM EXCESS RUNOFF FROM SUBAREA 1C3  
 262 BA .026  
 263 LS 77 35  
 264 UD .06  
  
 265 KK CP1C3  
 266 KM COMBINE HYDROGRAPHS FROM RC2-C3, DET1C2C, AND 1C3  
 267 HC 3

HEC-1 INPUT

PAGE 7

1  
 LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10  
  
 268 KK DET1C3  
 269 KM DETENTION BASIN FOR SUBAREAS 1C3  
 270 KM STORAGE VOLUME PER PLANS (405-E-95)  
 271 KM OUTLET IS A 6'W x 3'H CBC PER PLANS (1132-E-94 AND 190-E-95)  
 272 RS 1 STOR 0  
 273 SV 0 1.4  
 274 SQ 0 150  
 275 SE 0 3.5  
 276 ST 3.5 15 2.8 1.5  
  
 277 KK RC3COM  
 278 KM ROUTE OUTFLOW FROM DET1C3 TO WHERE DETCOM OUTFLOWS  
 279 RS 1 FLOW -3  
 280 RC 0.030 0.030 0.030 1000 0.016  
 281 RX 0 5 10 20 30 40 45 50  
 282 RY 12.0 13.75 11.5 10.0 10.0 11.5 11.75 12.0  
  
 283 KK COMM  
 284 KM EXCESS RUNOFF FROM SUBAREA COMMERCIAL  
 285 BA .03  
 286 LS 77 90  
 287 UD .07

```

288      KK  DETCOM
289      KM      DETENTION FOR SUBAREA COMMERCIAL
290      RS      1      STOR      0
291      SV      0      4.1
292      SQ      0      13
293      SE      0      3
294      ST      3      15      2.8      1.5

295      KK  CPCOM
296      KM      COMBINE HYDROGRAPHS FROM R3COM AND COMM
297      HC      2

298      KK  COMOF1
299      KM      ROUTE CPCOM TO CPOFF1
300      RS      1      FLOW      -1
301      RC      0.030  0.030  0.030  900  0.0155
302      RX      0      5      10      20      30      40      45      50
303      RY      12.0  11.75  11.5  10.0  10.0  11.5  11.75  12.0

304      KK  OFF1
305      KM      EXCESS RUNOFF FROM SUBAREA OFF1
306      BA      .02
307      LS      77      90
308      UD      .05

309      KK  DEOFF1
310      KM      DETENTION FOR SUBAREA OFF1
311      RS      1      STOR      0
312      SV      0      2.4
313      SQ      0      13
314      SE      0      3

```

HEC-1 INPUT

PAGE 8

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

315      ST      3      15      2.8      1.5

316      KK  CPOFF1
317      KM      COMBINE HYDROGRAPHS FROM COMOFF AND DEOFF1
318      HC      2

319      KK  OF1OF3
320      KM      ROUTE CPOFF1 TO CPOFF3
321      RS      1      FLOW      -1
322      RC      0.030  0.030  0.030  600  0.013
323      RX      0      5      10      20      30      40      45      50
324      RY      12.0  11.75  11.5  10.0  10.0  11.5  11.75  12.0

325      KK  OFF3
326      KM      EXCESS RUNOFF FROM SUBAREA OFF3
327      BA      .016
328      LS      77      90
329      UD      .07

330      KK  DEOFF3
331      KM      DETENTION FOR SUBAREA OFF3
332      RS      1      STOR      0
333      SV      0      2.24
334      SQ      0      13
335      SE      0      3
336      ST      3      15      2.8      1.5

337      KK  CPOFF3
338      KM      COMBINE HYDROGRAPHS FROM DEOFF3 AND OF1OF3
339      HC      2
*
*      START WEST SIDE OF STACKED 40 DESIGN CONCEPT CROSSING SCOTTSDALE RD
*

340      KK  33A1      CP
341      KM      ROUTE CPOFF3 THROUGH SUB 33A
342      RK      1960  .0161  .045      TRAP      20      3
*

343      KK  33A      SUB
344      KM      RUNOFF FROM SUB 33A, INCLUDES WEST SIDE OF CENTER DRIVE
345      BA      .054
346      LS      77      85
347      UK      300  0.020  .05      100
348      RK      2325  .012  .015      TRAP      20      3
*

349      KK  33A3      CP
350      KO      1
351      KM      COMBINE SUB 33A, CP 33A1
352      HC      2
*
*      END WEST SIDE OF STACKED 40 DESIGN CONCEPT CROSSING SCOTTSDALE RD
*
*
*      BEGIN GILBERTSON MODEL FOR GRAYHAWK - VILLAGE 1
*      START AT NORTHEAST CORNER OF PARCEL 1DB AND GO SOUTHWEST THROUGH
*      PROPOSED PARK SITE.
*

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HEC-1 INPUT

PAGE 9

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

353      KK  1DB

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```

354      KM      EXCESS RUNOFF FROM SUBAREA 1Db
355      BA      .04
356      LS      77      35
357      UD      .06

358      KK      DE1Db
359      KM      DETENTION FOR SUBAREA 1Db
360      RS      1      STOR      0
361      SV      0      2.7
362      SQ      0      13
363      SE      0      3.0
364      ST      3.0      15      2.8      1.5

365      KK      1Da1
366      KM      EXCESS RUNOFF FROM SUBAREA 1Da1
367      BA      .0099
368      LS      77      35
369      UD      .05

370      KK      DE1Da1
371      KM      DETENTION FOR SUBAREA 1Da1
372      KM      OUTLET IS A 18" PVC WITH AN 8" ORIFICE PLATE PER PLANS (905-E-95)
373      RS      1      STOR      0
374      SV      0      0.548
375      SQ      0      4
376      SE      0      3.0
377      ST      3.0      15      2.8      1.5

378      KK      1Da2
379      KM      EXCESS RUNOFF FROM SUBAREA 1Da2
380      BA      .003
381      LS      77
382      UD      .08

383      KK      CP1Dab
384      KM      COMBINE HYDROGRAPHS FROM 1Da2, DE1Db AND DE1Da1
385      HC      3

386      KK      RDabE2
387      KM      ROUTE OUTFLOW FROM CP1Dab TO CP1Ea2
388      KM      TRAPEZOIDAL CHANNEL PER PLANS (1182-E-94 AND 190-E-95)
389      KM      SIDE SLOPE = 4:1 (H:V)
390      KM      MAX DEPTH = 1.0 FT.
391      KM      BOT.WIDTH = 3.0 FT.
392      RS      1      FLOW      -1
393      RC      0.030      0.030      0.030      1400      0.0171
394      RX      0      0.5      1.0      5      8      12      12.5      13
395      RY      1.2      1.1      1.0      0      0      1.0      1.1      1.2

```

HEC-1 INPUT

PAGE 10

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

```

396      KK      1Ea1
397      KM      EXCESS RUNOFF FROM SUBAREA 1Ea1
398      BA      .019
399      LS      77      37
400      UD      .08

401      KK      DE1Ea1
402      KM      DETENTION FOR SUBAREA 1Ea1
403      KM      OUTLET IS A 8" PVC CONNECTED TO AN 18" RGRCP (407-E-95)
404      RS      1      STOR      0
405      SV      0      1.54
406      SQ      0      4
407      SE      0      3
408      ST      3      15      2.8      1.5

409      KK      1Ea2
410      KM      EXCESS RUNOFF FROM SUBAREA 1Ea2
411      BA      .024
412      LS      77      39
413      UD      .06

414      KK      CP1Ea2
415      KM      COMBINE HYDROGRAPHS FROM DE1Ea1 AND 1Ea2
416      HC      2

417      KK      DE1Ea2
418      KM      DETENTION FOR SUBAREA 1Ea2
419      RS      1      STOR      0
420      SV      0      1.5
421      SQ      0      10
422      SE      0      3
423      ST      3      15      2.8      1.5

424      KK      CP1Ea2
425      KM      COMBINE HYDROGRAPHS FROM DE1Ea2 AND RDabE2
426      HC      2

427      KK      PARK
428      KM      EXCESS RUNOFF FROM PROPOSED CITY'S PARK SITE
429      BA      .021
430      LS      77
431      UD      .06

432      KK      SCHOOL
433      KM      EXCESS RUNOFF FROM PROPOSED SCHOOL SITE
434      BA      .015
435      LS      77      80
436      UD      .05

```

LINE	ID	1	2	3	4	5	6	7	8	9	10	
437	KK	DETSCH										
438	KM	DETENTION FOR SUBAREA SCHOOL										
439	RS	1	STOR	0								
440	SV	0	1.3									
441	SQ	0	13									
442	SE	0	3									
443	ST	3	15	2.8	1.5							
444	KK	SCH12										
445	KM	ROUTE OUTFLOW FROM DETSCH TO CP1Ec										
446	RS	1	FLOW	-1								
447	RC	0.030	0.030	0.030	500	0.009						
448	RX	0	2.5	5	10	20	25	27.5	30			
449	RY	12.0	11.75	11.5	10.0	10.0	11.5	11.75	12.0			
450	KK	1Ec										
451	KM	EXCESS RUNOFF FROM SUBAREA 1Ec										
452	BA	.0089										
453	LS		77	80								
454	UD	.06										
455	KK	DE1Ec										
456	KM	DETENTION FOR SUBAREA 1Ec										
457	RS	1	STOR	0								
458	SV	0	0.8									
459	SQ	0	11									
460	SE	0	3									
461	ST	3	15	2.8	1.5							
462	KK	CP1Ec										
463	KM	COMBINE HYDROGRAPHS FROM SCH12 AND DE1Ec										
464	HC	2										
465	KK	1EcEa2										
466	KM	ROUTE OUTFLOW FROM CP1Ec TO CP1Ea2										
467	RS	1	FLOW	-1								
468	RC	0.030	0.030	0.030	500	0.009						
469	RX	0	2.5	5	10	20	25	27.5	30			
470	RY	12.0	11.75	11.5	10.0	10.0	11.5	11.75	12.0			
471	KK	CP1Ea										
472	KM	COMBINE HYDROGRAPHS FROM CP1Ea2, 1EcEa2 AND PARK										
473	HC	3										
474	KK	REaTPP										
475	KM	ROUTE CP1Ea TO THOMPSON PEAK PARKWAY										
476	RS	1	FLOW	-1								
477	RC	0.030	0.030	0.030	750	0.0186						
478	RX	0	2.5	5	10	20	25	27.5	30			
479	RY	12.0	11.75	11.5	10.0	10.0	11.5	11.75	12.0			

HEC-1 INPUT

PAGE 12

LINE	ID	1	2	3	4	5	6	7	8	9	10	
480	KK	1Eb										
481	KM	EXCESS RUNOFF FROM SUBAREA 1Eb										
482	BA	.0576										
483	LS		77	52								
484	UD	.08										
485	KK	DET1Eb										
486	KM	DETENTION FOR PARCEL 1Eb										
487	RS	1	STOR	0								
488	SV	0	4.9									
489	SQ	0	52									
490	SE	0	3									
491	ST	3	15	2.8	1.5							
492	KK	OFF2										
493	KM	EXCESS RUNOFF FROM SUBAREA OFF2. PUMPED HOSPITAL FLOWS.										
494	BA	.033										
495	LS		77	90								
496	UD	.07										
497	KK	DEOFF2										
498	KM	DETENTION FOR SUBAREA OFF2. PUMPED HOSPITAL FLOWS.										
499	RS	1	STOR	0								
500	SV	0	4.5									
501	SQ	0	13									
502	SE	0	3									
503	ST	3	15	2.8	1.5							
504	KK	CPOFF2										
505	KM	COMBINE HYDROGRAPHS REaTPP, DET1Eb AND DEOFF2										
506	HC	3										
507	KK	1Kf.1 ROUTE										
508	KM	ROUTE CPOFF2 THROUGH SUB 1Kf										

END GILBERTSON MODEL FOR GRAYHAWK - VILLAGE 1

START EAST SIDE OF STACKED 40 DESIGN

509 RK 840 .0135 .045 TRAP 10 2  
 \*  
 510 KK 1Kr SUB  
 511 KM R/O FROM SUB 1Kr  
 512 KM DA HAS BEEN REVISED TO REFLECT DEVELOPED SHAPE OF PARCEL 1K  
 513 BA .0515  
 514 LS 77 55  
 515 UD 0.15

HEC-1 INPUT

PAGE 13

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

516 KK DET1K  
 517 KM DETENTION FOR SUBAREA 1Kr  
 518 RS 1 STOR 0  
 519 SV 0 4.6  
 520 SQ 0 20  
 521 SE 0 3  
 522 ST 3 15 2.8 1.5  
 \*  
 523 KK 1Kr.2 COMBINE  
 524 KM COMBINE DET1K & 1Kr.1  
 525 HC 2  
 \*  
 526 KK 1Mr.1 ROUTE  
 527 KM ROUTE 1Kr.2 THROUGH SUB 1Mr  
 528 RK 1200 .0149 .045 TRAP 10 2  
 \*  
 529 KK 1Mr SUB  
 530 KM R/O FROM SUB 1Mr  
 531 KM DA HAS BEEN REVISED TO REFLECT DEVELOPED SHAPE OF PARCEL 1M  
 532 BA .0537  
 533 LS 77 64  
 534 UD .08  
 \*  
 535 KK DET1M DAM  
 536 KM ROUTE SUB 1M THROUGH DETENTION BASIN  
 537 RS 1 STOR 0  
 538 SV 0 3.3  
 539 SQ 0 20  
 540 SE 0 3  
 541 ST 3 15 2.8 1.5  
 \*  
 542 KK 1Mr.2 COMBINE  
 543 KM COMBINE DET1M & 1Mr.1  
 544 HC 2  
 \*  
 \* STACKED 40 BASIN 33E.1 NORTH OF CENTER DR  
 \*  
 \*  
 545 KK 33E SUB  
 546 KM R/O FROM SUB 33E  
 547 BA .0395  
 548 LS 77 84  
 549 UK 100 0.02 0.050 100  
 550 RK 2130 0.015 0.035 TRAP 20 3  
 \*  
 \*

HEC-1 INPUT

PAGE 14

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

551 KK 33BE SUB  
 552 KM RUNOFF FROM SUB 33BE. EAST SIDE OF CENTER DRIVE.  
 553 BA .0011  
 554 LS 77 78  
 555 UK 300 0.020 .035 100  
 556 RK 2325 .012 .015 TRAP 20 3  
 \*  
 557 KK 33E.2 COMBINE  
 558 KM COMBINE 1Mr.2 & 33E & 33BE. FLOW INTO CULVERT AND SD SYSTEM  
 559 KM UNDER CENTER DRIVE.  
 560 HC 3  
 \*  
 561 KK R33E.2 ROUTE  
 562 KM ROUTE 33E.2 ALONG EAST SIDE OF STACK 40 PARCEL TO FRONTAGE ROAD  
 563 KM 2-54" PIPES. DIAMETER PROVIDED IN ROUTING IS EQUIVALENT DIA OF  
 564 KM BOTH PIPES.  
 565 RK 2250 .0147 .015 CIRC 6.3  
 \*  
 \* INSERT EXISTING CONDITION SUBBASIN 33D  
 \*  
 566 KK 33D SUB  
 567 KM RUNOFF FROM SUB 33D  
 568 KO 5  
 569 BA .0403  
 570 LS 77  
 571 UK 89 .0213 .10 100  
 572 RK 2250 .0140 .045 TRAP 20 3

```

*
573 KK S40ET SUB
574 KM SUB SOUTH OF CENTER DRIVE, EASTERN SIDE OF PROPERTY, FLOWS TO
575 KM EASTERN DIVERSION STRUCTURE.
576 BA .0183
577 LS 77 86
578 UK 175 .0075 .05 100
579 RK 2000 .008 .015 CIRC 5
*
*
580 KK CT13.0 COMBINE
581 KO 1
582 KM COMBINE R33E.2, SUB 33D, S40ET, & S40CN. FLOWS INTO JUNCTION STRUCTURE
583 HC 3
*
*
584 KK D_ADOT
585 KM DIVERT FLOW FROM BASIN DIRECTLY TO ADOT CULVERT 6
586 KM FLOW TO ADOT CULVERT 6 OF 223 CFS
587 DT P_ADOT
588 DI 0 2.7 10.4 22.6 38.7 58.4 80.8 105.4 143.3 191.9
589 DI 246.9 306.5 361.9 419.9
HEC-1 INPUT

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PAGE 15

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

590 DQ 0 2.7 10.4 22.6 38.7 58.4 80.8 105.4 131.6 158.6
591 DQ 185.7 212.3 230.2 246.9
*
*
592 KK 33C SUB
593 KM SUBBASIN 33C SOUTH OF CENTER DRIVE WEST SIDE OF PROPERTY
594 KM MODIFIED AREA TO ACCOUNT FOR NEW SITE PLAN AND SUBS 04-27-06 - ADDED SOUTHWEST
595 BA 0.0296
596 LS 77 87
597 UK 200 .0068 .05 100
598 RK 1750 .017 .015 CIRC 5
*
*
599 KK S40CN SUB
600 KM SUB SOUTH OF CENTER DRIVE, CENTRAL BASIN FLOWING DIRECTLY INTO DET/RET
601 KM INCLUDES DETENTION BASIN
602 BA .0448
603 LS 77 87
604 UK 250 .0075 .05 100
605 RK 1500 .009 .015 CIRC 4.5
*
*
606 KK CT13.1 COMBINE
607 KM COMBINE CT13.0, 33C FLOWS (Total Flow at the BASIN)
608 HC 3
*
*
609 KK D_BAS
610 KM BY-PASS FLOW THROUGH d=2' PIPE (MAX q = 20 CFS) BASIN OUTLETS PROVIDE
611 KM EQUIVALENT AMOUNT OF DISCHARGE
612 DT P-PIPE
613 DI 0 1.0 10.0 30.0 30 100.0 300.0 500.0 800.0
614 DQ 0 1.0 10.0 30.0 30 30 30 30 30
*
*
615 KK D_BAS1
616 KM DIVERT THE FIRST 1 AC-FT INTO THE SURFACE STORAGE
617 DT D-BAS2 1.0
618 DI 0 1.0 10.0 40.0 70.0 100.0 300.0 500.0 800.0
619 DQ 0 1.0 10.0 40.0 70.0 100.0 300.0 500.0 800.0
*
*
620 KK D_SURF
621 KM DIVERT FLOW INTO SUB_SURFACE STORAGE
622 KM (1110', 10' DIAMETER PIPE, VOL = 2.0 Ac-Ft)
623 KO 1
624 DT D-SURF 2
625 DI 0 1.0 10.0 40.0 70.0 100.0 300.0 500.0 800.0
626 DQ 0 1.0 10.0 40.0 70.0 100.0 300.0 500.0 800.0
*
*

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HEC-1 INPUT

PAGE 16

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

627 KK B_PIPE
628 KM RETRIEVE DIVERTED PIPE FLOW
629 DR P-PIPE
*
*
630 KK B_SURF
631 KM RETRIEVE DIVERTED SURFACE FLOW
632 DR D-BAS2
*
*
633 KK CS40B COMBINE
634 KO 1
635 KM COMBINE PIPE FLOW, DIVERTED SURFACE FLOW AND REMAINING SURFACE FLOW
636 HC 3
*

```



637 KK S40BAS  
638 KO 1  
639 KM ROUTE DIVERTED FLOW THROUGH OFFLINE BASIN CONCEPT MAX H =5.9  
640 KM ASSUMED 1000'X 80' BASIN WITH 5:1 SIDE SLOPES & 36" OUTLET  
641 KM 24" BLEED-OFF PIPE PLUS 20' WIDE SPILLWAY AT 3.8'  
642 RS 1 STOR -1  
643 SV 0 .001 .14 .87 1.84 3.04 4.49 5.16 5.49 5.82  
644 SV 6.15  
645 SE 0 .8 1 2 3 4 5 5.4 5.6 5.8  
646 SE 6  
647 SL 1 3.14 0.62 0.5  
648 SS 3.8 20 2.8 1.5  
\*

649 KK P33E.1  
650 KO 1  
651 KM DIVIDE THE FLOW INTO TWO ADOT CULVERTS  
652 DT D33C.2  
653 DI 0 100 200 400 600  
654 DQ 0 68 136 272 408  
\*

655 KK R ADOT  
656 KM RETRIEVE DIVERTED ADOT CULVERT FLOW  
657 DR P\_ADOT  
\*

658 KK 33E.1 COMBINE  
659 KO 1 21  
660 KM COMBINED DISCHARGE AT ADOT CULVERT 5 AND 6  
661 HC 2  
\*

# HEC-1 INPUT

PAGE 17

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

662 KK R33E.1 ROUTE  
663 KO 1 21  
664 KM ROUTE ADOT CULVERT 5 AND 6 FLOWS THROUGH ASLD LAND TO  
665 KM UNION HILLS DRIVE (MAYO) AND 73RD PLACE.  
666 KM ROUTE L=1600', TRAP SECTION BW=19' Z=5, TWmax=39'  
667 KM ASSUME GRASS LINED CHANNEL N=.030 UP=1592.5 DWN=1582.66  
668 RK 1600 0.0088 0.03 TRAP 19 5  
\*

669 KK ASLDR1 ROUTE  
670 KO 1 21  
671 KM ROUTE FLOWS FROM CHANNEL THROUGH BOX CULVERT ALONG UNION  
672 KM HILLS DRIVE (MAYO) TO SCOTTSDALE ROAD, SOUTH TO CHAUNCEY.  
673 KM ROUTE L=1830', BOX SECTION W=8' H=3'  
674 KM ASSUME CONCRTE LINED CHANNEL N=.013 UP=1582.55 DWN=1566.32  
675 RK 1830 0.0089 .013 TRAP 16 0  
\*

676 KK ASLD1 SUB  
677 KO 1 21  
678 KM ASLD NORTH PARCEL EAST OF SCOTTSDALE ROAD AND NORTH OF CHAUNCEY LANE  
679 BA 0.0315  
680 LS 77 83  
681 UK 345 0.001 0.015 100  
682 RK 1400 .0131 .015 TRAP 17 4  
\*

683 KK ASLDCT COMBINE  
684 KO 1 21  
685 KM COMBINED DISCHARGE AT ASLDR1 AND ASLD1 SUB BASIN  
686 HC 2  
\*

687 KK ASLDR2 ROUTE  
688 KO 1 21  
689 KM ROUTE ASLDR1 AND ASLD1 SUB TO SCOTTSDALE ROAD  
690 KM AND PRINCESS DRIVE  
691 KM ROUTE L=1000', TRAP SECTION BW=17' Z=4, TWmax=41'  
692 KM ASSUME GRASS LINED CHANNEL N=.030 UP=1570.15 DWN=1548.60  
693 RK 1000 0.0075 0.03 TRAP 17 4  
\*

694 KK ASLD2 SUB  
695 KO 1 21  
696 KM ASLD SOUTH PARCEL EAST OF SCOTTSDALE ROAD AND NORTH OF CHAUNCEY LANE  
697 BA 0.0193  
698 LS 77 78  
699 UK 269 .0022 0.015 100  
700 RK 600 .0139 .015 TRAP 17 4  
\*

# HEC-1 INPUT

PAGE 18

LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10

701 KK CPPERIN COMBINE  
702 KO 1 21  
703 KM COMBINE ROUTED ROUTED ASLDCHNI WITH ASLD2  
704 HC 2  
\*

705 KK R33C.2

```

706      KO      1
707      KM      RETRIEVE DIVERTED PIPE FLOW
708      DR      D33C.2
      *
709      KK      S40WT      SUB
710      KO      1
711      KM      SUB EAST OF SCOTTSDALE RD. FLOWING DIRECTLY INTO SCOTTSDALE RD
712      KM      CULVERT, TAKES SCOTTS RD HALF ST AND SCENIC CORRIDOR
713      BA      0.0053
714      LS
715      UK      50      .01      .05      100
716      RK      600      .01      .015      CIRC      4.5
      *
      *
717      KK      33C.2 COMBINE
718      KO      1
719      KM      COMBINED DISCHARGE AT SCOTTSDALE ROAD CULVERT
720      HC      2
      *
      *
721      ZZ

```

1

# SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT
LINE      (V) ROUTING      (--->) DIVERSION OR PUMP FLOW
NO.      (.) CONNECTOR      (<---) RETURN OF DIVERTED OR PUMPED FLOW

20      1A1
      V
      V
27      DET1A1
      V
      V
44      RA1-C4
      .
      .
43      .      1C4
      .
      .
48      CP1C4.....
      V
      V
51      RC4-C3
      .
      .
50      .      1Da3
      .      V
      .      V
55      .      DE1Da3
      .
      .
73      .      .      1Da4
      .
      .
78      .      CP1Da4.....
      .      V
      .      V
81      .      DE1Da4
      .
      .
89      .      .      1Da5
      .
      .
94      CP1C3I.....
      V
      V
97      RC3-C3
      .
      .
106     .      Off-1A
      .
      .
111     .      .      1A2
      .
      .
116     .      .      .      1A3
      .
      .
121     .      CPA3.....
      .      V
      .      V
124     .      DET1A3
      .      V
      .      V
131     .      RA3-A6
      .
      .
141     .      .      1A6
      .
      .
146     .      CP1A6.....
      .      V
      .      V
149     .      DET1A6
      .
      .
156     .      .      1A5
      .
      .

```

161	.	CP1A5.....	.
	.	V	.
	.	V	.
164	.	DET1A5	.
	.	.	.
171	.	.	1A4
	.	.	V
	.	.	V
176	.	.	RA4-A7
	.	.	V
	.	.	V
186	.	DET1A4	.
	.	.	.
193	.	.	1A7
	.	.	.
198	.	CP1A7.....	.
	.	V	.
	.	V	.
201	.	DET1A7	.
	.	.	.
208	.	.	1C1
	.	.	.
213	.	CP1C1.....	.
	.	V	.
	.	V	.
216	.	DET1C1	.
	.	.	.
225	.	.	1C2
	.	.	.
230	.	CP1C2.....	.
	.	V	.
	.	V	.
233	.	DE1C2A	.
	.	V	.
	.	V	.
242	.	DE1C2B	.
	.	V	.
	.	V	.
251	.	DE1C2C	.
	.	.	.
260	.	.	1C3
	.	.	.
265	.	CP1C3.....	.
	.	V	.
	.	V	.
268	.	DET1C3	.
	.	V	.
	.	V	.
277	.	RC3COM	.
	.	.	.
283	.	COMM	.
	.	V	.
	.	V	.
288	.	DETCOM	.
	.	.	.
295	.	CPCOM.....	.
	.	V	.
	.	V	.
298	.	COMOF1	.
	.	.	.
304	.	OFF1	.
	.	V	.
	.	V	.
309	.	DEOFF1	.
	.	.	.
316	.	CPOFF1.....	.
	.	V	.
	.	V	.
319	.	OF1OF3	.
	.	.	.
325	.	OFF3	.
	.	V	.
	.	V	.
330	.	DEOFF3	.
	.	.	.
337	.	CPOFF3.....	.
	.	V	.
	.	V	.
340	.	33A1	.
	.	.	.
343	.	33A	.
	.	.	.
349	.	33A3.....	.

353	.	1Db	.
	.	V	.
	.	V	.
358	.	DE1Db	.
	.	.	.
365	.	1Da1	.
	.	V	.
	.	V	.
370	.	DE1Da1	.
	.	.	.
378	.	.	1Da2
	.	.	.
	.	.	.
383	.	CP1Da1	.....
	.	V	.
	.	V	.
386	.	RDabE2	.
	.	.	.
396	.	1Ea1	.
	.	V	.
	.	V	.
401	.	DE1Ea1	.
	.	.	.
409	.	.	1Ea2
	.	.	.
	.	.	.
414	.	CP1Ea2	.....
	.	V	.
	.	V	.
417	.	DE1Ea2	.
	.	.	.
	.	.	.
424	.	CP1Ea2	.....
	.	.	.
427	.	PARK	.
	.	.	.
432	.	.	SCHOOL
	.	.	V
	.	.	V
437	.	.	DETSCH
	.	.	V
	.	.	V
444	.	.	SCH12
	.	.	.
450	.	.	1Ec
	.	.	V
	.	.	V
455	.	.	DE1Ec
	.	.	.
	.	.	.
462	.	.	CP1Ec
	.	.	V
	.	.	V
465	.	.	1EcEa2
	.	.	.
	.	.	.
471	.	CP1Ea	.....
	.	V	.
	.	V	.
474	.	REaTPP	.
	.	.	.
480	.	1Eb	.
	.	V	.
	.	V	.
485	.	DET1Eb	.
	.	.	.
492	.	.	OFF2
	.	.	V
	.	.	V
497	.	.	DEOFF2
	.	.	.
	.	.	.
504	.	CPOFF2	.....
	.	V	.
	.	V	.
507	.	1Kr.1	.
	.	.	.
510	.	1Kr	.
	.	V	.
	.	V	.
516	.	DET1K	.
	.	.	.
	.	.	.
523	.	1Kr.2	.....
	.	V	.
	.	V	.
526	.	1Kr.1	.
	.	.	.
	.	.	.

```

529 . . . 1Mr
. . . V
. . . V
535 . . . DET1M
. . .
542 . 1Mr.2.....
. . .
545 . . . 33E
. . .
551 . . . 33BE
. . .
557 . 33E.2.....
. . . V
. . . V
561 . R33E.2
. . .
566 . . . 33D
. . .
573 . . . S40ET
. . .
580 . CT13.0.....
. . .
587 . -----> P_ADOT
584 . D_ADOT
. . .
592 . . . 33C
. . .
599 . . . S40CN
. . .
606 . CT13.1.....
. . .
612 . -----> P-PIPE
609 . D_BAS
. . .
617 . -----> D-BAS2
615 . D_BAS1
. . .
624 . -----> D-SURF
620 . D_SURF
. . .
629 . . . .----- P-PIPE
627 . B_PIPE
. . .
632 . . . .----- D-BAS2
630 . B_SURF
. . .
633 . CS40B.....
. . . V
. . . V
637 . S40BAS
. . .
652 . -----> D33C.2
649 . P33E.1
. . .
657 . . . .----- P_ADOT
655 . P_ADOT
. . .
658 . 33E.1.....
. . . V
. . . V
662 . R33E.1
. . . V
. . . V
669 . ASLDR1
. . .
576 . . . ASLD
. . .
683 . ASLDC.....
. . . V
. . . V
687 . ASLDR2
. . .
694 . . . ASLD
. . .
701 . CFPIN.....
. . .

```

708 . . . . . D33C.2  
 705 . . . . . R33C.2  
 . . . . .  
 709 . . . . . S40WT  
 . . . . .  
 717 . . . . . 33C.2.....

(\*\*\*) RUNOFF ALSO COMPUTED AT THIS LOCATION

\* FLOOD HYDROGRAPH PACKAGE (HEC-1) \*  
 \* JUN 1998 \*  
 \* VERSION 4.1 \*  
 \* RUN DATE: 09AUG12 TIME 16:57:57 \*

\* U.S. ARMY CORPS OF ENGINEERS \*  
 \* HYDROLOGIC ENGINEERING CENTER \*  
 \* 609 SECOND STREET \*  
 \* DAVIS, CALIFORNIA 95616 \*  
 \* (916) 756-1104 \*

ONE SCOTTSDALE (STACKED 40S) POST DEVELOPMENT CONDITION 100-YR 6-HR STORM  
 OFFSITE HYDROLOGY & ONSITE HYDROLOGY FOR AREA GOVERNED BY PRE-POST CRITERIA  
 OPTION A - ASLD CHANNEL  
 FILE: 100YR-N2.DAT  
 OPTION B - 34.1 ACRES OF ASLD PARCEL

BASED ON MODELS PREPARED BY: ROBERT L. WARD, P.E., CONSULTING ENGINEER

PR5W-100.6I  
 CL.6I (CENTER DRIVE PROJECT)  
 S40EX100.6I (STACKED 40S EXISTING CONDITON)

ALL CURVE NUMBERS ADJUSTED TO 6-HOUR VALUES ON AUGUST 13, 2002  
 100-YEAR, 6-HOUR HYPOTHETICAL STORM

AREAL RAINFALL REDUCTION IS BASED ON A 14 SQUARE MILE STORM.

19 IO OUTPUT CONTROL VARIABLES  
 IPRNT 5 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IT HYDROGRAPH TIME DATA  
 NMIN 5 MINUTES IN COMPUTATION INTERVAL  
 IDATE 1 0 STARTING DATE  
 ITIME 0000 STARTING TIME  
 HQ 300 NUMBER OF HYDROGRAPH ORDINATES  
 NDDATE 2 0 ENDING DATE  
 NDTIME 0055 ENDING TIME  
 ICENT 19 CENTURY MARK  
 COMPUTATION INTERVAL .08 HOURS  
 TOTAL TIME BASE 24.92 HOURS

ENGLISH UNITS  
 DRAINAGE AREA SQUARE MILES  
 PRECIPITATION DEPTH INCHES  
 LENGTH, ELEVATION FEET  
 FLOW CUBIC FEET PER SECOND  
 STORAGE VOLUME ACRE-FEET  
 SURFACE AREA ACRES  
 TEMPERATURE DEGREES FAHRENHEIT

349 KK 33A3 CP

350 KO OUTPUT CONTROL VARIABLES  
 IPRNT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 COMBINE SUB 33A, CP 33A1

352 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION 33A3  
 SUM OF 2 HYDROGRAPHS

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	1	0.	1	0615	76	41.	1	1230	151	5.	1	1945	226	1				
1	0005	2	0.	1	0620	77	40.	1	1235	152	4.	1	1950	227	1.				

1	0010	3	0.	*	1	0625	73	39.	*	1	1240	153	4.	*	1	1855	228	1.
1	0015	4	0.	*	1	0630	79	37.	*	1	1245	154	4.	*	1	1900	229	1.
1	0020	5	0.	*	1	0635	80	36.	*	1	1250	155	4.	*	1	1905	230	1.
1	0025	6	0.	*	1	0640	81	35.	*	1	1255	156	4.	*	1	1910	231	1.
1	0030	7	1.	*	1	0645	82	34.	*	1	1300	157	4.	*	1	1915	232	1.
1	0035	8	1.	*	1	0650	83	33.	*	1	1305	158	4.	*	1	1920	233	1.
1	0040	9	2.	*	1	0655	84	32.	*	1	1310	159	4.	*	1	1925	234	1.
1	0045	10	3.	*	1	0700	85	31.	*	1	1315	160	3.	*	1	1930	235	1.
1	0050	11	3.	*	1	0705	86	31.	*	1	1320	161	3.	*	1	1935	236	1.
1	0055	12	4.	*	1	0710	87	30.	*	1	1325	162	3.	*	1	1940	237	1.
1	0100	13	4.	*	1	0715	88	30.	*	1	1330	163	3.	*	1	1945	238	0.
1	0105	14	4.	*	1	0720	89	29.	*	1	1335	164	3.	*	1	1950	239	0.
1	0110	15	5.	*	1	0725	90	28.	*	1	1340	165	3.	*	1	1955	240	0.
1	0115	16	5.	*	1	0730	91	28.	*	1	1345	166	3.	*	1	2000	241	0.
1	0120	17	5.	*	1	0735	92	27.	*	1	1350	167	3.	*	1	2005	242	0.
1	0125	18	6.	*	1	0740	93	26.	*	1	1355	168	3.	*	1	2010	243	0.
1	0130	19	6.	*	1	0745	94	26.	*	1	1400	169	3.	*	1	2015	244	0.
1	0135	20	7.	*	1	0750	95	25.	*	1	1405	170	3.	*	1	2020	245	0.
1	0140	21	7.	*	1	0755	96	24.	*	1	1410	171	3.	*	1	2025	246	0.
1	0145	22	8.	*	1	0800	97	24.	*	1	1415	172	2.	*	1	2030	247	0.
1	0150	23	8.	*	1	0805	98	23.	*	1	1420	173	2.	*	1	2035	248	0.
1	0155	24	9.	*	1	0810	99	22.	*	1	1425	174	2.	*	1	2040	249	0.
1	0200	25	9.	*	1	0815	100	22.	*	1	1430	175	2.	*	1	2045	250	0.
1	0205	26	10.	*	1	0820	101	21.	*	1	1435	176	2.	*	1	2050	251	0.
1	0210	27	11.	*	1	0825	102	21.	*	1	1440	177	2.	*	1	2055	252	0.
1	0215	28	11.	*	1	0830	103	20.	*	1	1445	178	2.	*	1	2100	253	0.
1	0220	29	12.	*	1	0835	104	19.	*	1	1450	179	2.	*	1	2105	254	0.
1	0225	30	13.	*	1	0840	105	19.	*	1	1455	180	2.	*	1	2110	255	0.
1	0230	31	15.	*	1	0845	106	18.	*	1	1500	181	2.	*	1	2115	256	0.
1	0235	32	18.	*	1	0850	107	18.	*	1	1505	182	2.	*	1	2120	257	0.
1	0240	33	25.	*	1	0855	108	17.	*	1	1510	183	2.	*	1	2125	258	0.
1	0245	34	34.	*	1	0900	109	17.	*	1	1515	184	2.	*	1	2130	259	0.
1	0250	35	45.	*	1	0905	110	16.	*	1	1520	185	2.	*	1	2135	260	0.
1	0255	36	60.	*	1	0910	111	16.	*	1	1525	186	2.	*	1	2140	261	0.
1	0300	37	109.	*	1	0915	112	15.	*	1	1530	187	2.	*	1	2145	262	0.
1	0305	38	232.	*	1	0920	113	15.	*	1	1535	188	2.	*	1	2150	263	0.
1	0310	39	198.	*	1	0925	114	15.	*	1	1540	189	2.	*	1	2155	264	0.
1	0315	40	150.	*	1	0930	115	14.	*	1	1545	190	2.	*	1	2200	265	0.
1	0320	41	143.	*	1	0935	116	14.	*	1	1550	191	1.	*	1	2205	266	0.
1	0325	42	141.	*	1	0940	117	13.	*	1	1555	192	1.	*	1	2210	267	0.
1	0330	43	135.	*	1	0945	118	13.	*	1	1600	193	1.	*	1	2215	268	0.
1	0335	44	132.	*	1	0950	119	12.	*	1	1605	194	1.	*	1	2220	269	0.
1	0340	45	138.	*	1	0955	120	12.	*	1	1610	195	1.	*	1	2225	270	0.
1	0345	46	149.	*	1	1000	121	12.	*	1	1615	196	1.	*	1	2230	271	0.
1	0350	47	151.	*	1	1005	122	11.	*	1	1620	197	1.	*	1	2235	272	0.
1	0355	48	144.	*	1	1010	123	11.	*	1	1625	198	1.	*	1	2240	273	0.
1	0400	49	133.	*	1	1015	124	11.	*	1	1630	199	1.	*	1	2245	274	0.
1	0405	50	123.	*	1	1020	125	10.	*	1	1635	200	1.	*	1	2250	275	0.
1	0410	51	114.	*	1	1025	126	10.	*	1	1640	201	1.	*	1	2255	276	0.
1	0415	52	107.	*	1	1030	127	10.	*	1	1645	202	1.	*	1	2300	277	0.
1	0420	53	99.	*	1	1035	128	9.	*	1	1650	203	1.	*	1	2305	278	0.
1	0425	54	93.	*	1	1040	129	9.	*	1	1655	204	1.	*	1	2310	279	0.
1	0430	55	88.	*	1	1045	130	9.	*	1	1700	205	1.	*	1	2315	280	0.
1	0435	56	83.	*	1	1050	131	9.	*	1	1705	206	1.	*	1	2320	281	0.
1	0440	57	78.	*	1	1055	132	8.	*	1	1710	207	1.	*	1	2325	282	0.
1	0445	58	74.	*	1	1100	133	8.	*	1	1715	208	1.	*	1	2330	283	0.
1	0450	59	70.	*	1	1105	134	8.	*	1	1720	209	1.	*	1	2335	284	0.
1	0455	60	67.	*	1	1110	135	8.	*	1	1725	210	1.	*	1	2340	285	0.
1	0500	61	64.	*	1	1115	136	7.	*	1	1730	211	1.	*	1	2345	286	0.
1	0505	62	61.	*	1	1120	137	7.	*	1	1735	212	1.	*	1	2350	287	0.
1	0510	63	59.	*	1	1125	138	7.	*	1	1740	213	1.	*	1	2355	288	0.
1	0515	64	56.	*	1	1130	139	7.	*	1	1745	214	1.	*	2	0000	289	0.
1	0520	65	54.	*	1	1135	140	6.	*	1	1750	215	1.	*	2	0005	290	0.
1	0525	66	53.	*	1	1140	141	6.	*	1	1755	216	1.	*	2	0010	291	0.
1	0530	67	51.	*	1	1145	142	6.	*	1	1800	217	1.	*	2	0015	292	0.
1	0535	68	50.	*	1	1150	143	6.	*	1	1805	218	1.	*	2	0020	293	0.
1	0540	69	49.	*	1	1155	144	6.	*	1	1810	219	1.	*	2	0025	294	0.
1	0545	70	48.	*	1	1200	145	5.	*	1	1815	220	1.	*	2	0030	295	0.
1	0550	71	47.	*	1	1205	146	5.	*	1	1820	221	1.	*	2	0035	296	0.
1	0555	72	46.	*	1	1210	147	5.	*	1	1825	222	1.	*	2	0040	297	0.
1	0600	73	45.	*	1	1215	148	5.	*	1	1830	223	1.	*	2	0045	298	0.
1	0605	74	44.	*	1	1220	149	5.	*	1	1835	224	1.	*	2	0050	299	0.
1	0610	75	42.	*	1	1225	150	5.	*	1	1840	225	1.	*	2	0055	300	0.

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24.92-HR
232.	3.08	65.	19.	19.	19.
(INCHES)		1.984	2.334	2.334	2.334
(AC-FT)		32.	38.	38.	38.

CUMULATIVE AREA = .31 SQ MI

568 KO OUTPUT CONTROL VARIABLES

IPRNT	5	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

580 KK CT13.0 COMBINE

541 KO

## OUTPUT CONTROL VARIABLES

TPRNT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 COMBINE R33E.2, SUB 33D, S40ET, & S40CN. FLOWS INTO JUNCTION STRUCTURE

583 HC

## HYDROGRAPH COMBINATION

ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CT13.0  
 SUM OF 3 HYDROGRAPHS

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	1	0.	*	1	0615	76	58.	*	1	1230	151	5.	*	1	1845	226	1.	
1	0005	2	0.	*	1	0620	77	55.	*	1	1235	152	5.	*	1	1850	227	1.	
1	0010	3	0.	*	1	0625	78	53.	*	1	1240	153	5.	*	1	1855	228	1.	
1	0015	4	0.	*	1	0630	79	50.	*	1	1245	154	5.	*	1	1900	229	1.	
1	0020	5	0.	*	1	0635	80	48.	*	1	1250	155	5.	*	1	1905	230	1.	
1	0025	6	1.	*	1	0640	81	46.	*	1	1255	156	5.	*	1	1910	231	1.	
1	0030	7	1.	*	1	0645	82	44.	*	1	1300	157	5.	*	1	1915	232	1.	
1	0035	8	2.	*	1	0650	83	42.	*	1	1305	158	5.	*	1	1920	233	1.	
1	0040	9	3.	*	1	0655	84	41.	*	1	1310	159	4.	*	1	1925	234	1.	
1	0045	10	4.	*	1	0700	85	39.	*	1	1315	160	4.	*	1	1930	235	1.	
1	0050	11	5.	*	1	0705	86	38.	*	1	1320	161	4.	*	1	1935	236	1.	
1	0055	12	6.	*	1	0710	87	36.	*	1	1325	162	4.	*	1	1940	237	1.	
1	0100	13	6.	*	1	0715	88	35.	*	1	1330	163	4.	*	1	1945	238	1.	
1	0105	14	7.	*	1	0720	89	34.	*	1	1335	164	4.	*	1	1950	239	1.	
1	0110	15	7.	*	1	0725	90	32.	*	1	1340	165	4.	*	1	1955	240	1.	
1	0115	16	8.	*	1	0730	91	31.	*	1	1345	166	4.	*	1	2000	241	1.	
1	0120	17	9.	*	1	0735	92	30.	*	1	1350	167	4.	*	1	2005	242	1.	
1	0125	18	9.	*	1	0740	93	29.	*	1	1355	168	4.	*	1	2010	243	1.	
1	0130	19	10.	*	1	0745	94	28.	*	1	1400	169	3.	*	1	2015	244	1.	
1	0135	20	10.	*	1	0750	95	27.	*	1	1405	170	3.	*	1	2020	245	1.	
1	0140	21	11.	*	1	0755	96	26.	*	1	1410	171	3.	*	1	2025	246	1.	
1	0145	22	12.	*	1	0800	97	25.	*	1	1415	172	3.	*	1	2030	247	1.	
1	0150	23	12.	*	1	0805	98	25.	*	1	1420	173	3.	*	1	2035	248	1.	
1	0155	24	13.	*	1	0810	99	24.	*	1	1425	174	3.	*	1	2040	249	1.	
1	0200	25	14.	*	1	0815	100	23.	*	1	1430	175	3.	*	1	2045	250	1.	
1	0205	26	15.	*	1	0820	101	22.	*	1	1435	176	3.	*	1	2050	251	1.	
1	0210	27	16.	*	1	0825	102	22.	*	1	1440	177	3.	*	1	2055	252	1.	
1	0215	28	17.	*	1	0830	103	21.	*	1	1445	178	3.	*	1	2100	253	1.	
1	0220	29	18.	*	1	0835	104	20.	*	1	1450	179	3.	*	1	2105	254	1.	
1	0225	30	20.	*	1	0840	105	20.	*	1	1455	180	3.	*	1	2110	255	1.	
1	0230	31	21.	*	1	0845	106	19.	*	1	1500	181	3.	*	1	2115	256	1.	
1	0235	32	25.	*	1	0850	107	18.	*	1	1505	182	3.	*	1	2120	257	1.	
1	0240	33	33.	*	1	0855	108	18.	*	1	1510	183	2.	*	1	2125	258	0.	
1	0245	34	44.	*	1	0900	109	17.	*	1	1515	184	2.	*	1	2130	259	0.	
1	0250	35	58.	*	1	0905	110	17.	*	1	1520	185	2.	*	1	2135	260	0.	
1	0255	36	77.	*	1	0910	111	16.	*	1	1525	186	2.	*	1	2140	261	0.	
1	0300	37	134.	*	1	0915	112	16.	*	1	1530	187	2.	*	1	2145	262	0.	
1	0305	38	295.	*	1	0920	113	15.	*	1	1535	188	2.	*	1	2150	263	0.	
1	0310	39	340.	*	1	0925	114	15.	*	1	1540	189	2.	*	1	2155	264	0.	
1	0315	40	303.	*	1	0930	115	14.	*	1	1545	190	2.	*	1	2200	265	0.	
1	0320	41	275.	*	1	0935	116	14.	*	1	1550	191	2.	*	1	2205	266	0.	
1	0325	42	257.	*	1	0940	117	14.	*	1	1555	192	2.	*	1	2210	267	0.	
1	0330	43	243.	*	1	0945	118	13.	*	1	1600	193	2.	*	1	2215	268	0.	
1	0335	44	226.	*	1	0950	119	13.	*	1	1605	194	2.	*	1	2220	269	0.	
1	0340	45	204.	*	1	0955	120	12.	*	1	1610	195	2.	*	1	2225	270	0.	
1	0345	46	184.	*	1	1000	121	12.	*	1	1615	196	2.	*	1	2230	271	0.	
1	0350	47	168.	*	1	1005	122	12.	*	1	1620	197	2.	*	1	2235	272	0.	
1	0355	48	156.	*	1	1010	123	11.	*	1	1625	198	2.	*	1	2240	273	0.	
1	0400	49	147.	*	1	1015	124	11.	*	1	1630	199	2.	*	1	2245	274	0.	
1	0405	50	140.	*	1	1020	125	11.	*	1	1635	200	2.	*	1	2250	275	0.	
1	0410	51	134.	*	1	1025	126	10.	*	1	1640	201	2.	*	1	2255	276	0.	
1	0415	52	129.	*	1	1030	127	10.	*	1	1645	202	2.	*	1	2300	277	0.	
1	0420	53	125.	*	1	1035	128	10.	*	1	1650	203	2.	*	1	2305	278	0.	
1	0425	54	120.	*	1	1040	129	10.	*	1	1655	204	2.	*	1	2310	279	0.	
1	0430	55	116.	*	1	1045	130	9.	*	1	1700	205	2.	*	1	2315	280	0.	
1	0435	56	112.	*	1	1050	131	9.	*	1	1705	206	1.	*	1	2320	281	0.	
1	0440	57	108.	*	1	1055	132	9.	*	1	1710	207	1.	*	1	2325	282	0.	
1	0445	58	105.	*	1	1100	133	9.	*	1	1715	208	1.	*	1	2330	283	0.	
1	0450	59	101.	*	1	1105	134	8.	*	1	1720	209	1.	*	1	2335	284	0.	
1	0455	60	98.	*	1	1110	135	8.	*	1	1725	210	1.	*	1	2340	285	0.	
1	0500	61	95.	*	1	1115	136	8.	*	1	1730	211	1.	*	1	2345	286	0.	
1	0505	62	92.	*	1	1120	137	8.	*	1	1735	212	1.	*	1	2350	287	0.	
1	0510	63	89.	*	1	1125	138	8.	*	1	1740	213	1.	*	1	2355	288	0.	
1	0515	64	86.	*	1	1130	139	7.	*	1	1745	214	1.	*	2	0000	289	0.	
1	0520	65	83.	*	1	1135	140	7.	*	1	1750	215	1.	*	2	0005	290	0.	
1	0525	66	81.	*	1	1140	141	7.	*	1	1755	216	1.	*	2	0010	291	0.	
1	0530	67	78.	*	1	1145	142	7.	*	1	1800	217	1.	*	2	0015	292	0.	
1	0535	68	76.	*	1	1150	143	7.	*	1	1805	218	1.	*	2	0020	293	0.	
1	0540	69	74.	*	1	1155	144	6.	*	1	1810	219	1.	*	2	0025	294	0.	
1	0545	70	72.	*	2	1200	145	6.	*	1	1815	220	1.	*	2	0030	295	0.	
1	0550	71	70.	*	1	1205	146	6.	*	1	1820	221	1.	*	2	0035	296	0.	
1	0555	72	68.	*	1	1210	147	6.	*	1	1825	222	1.	*	2	0040	297	0.	
1	0600	73	66.	*	1	1215	148	6.	*	1	1830	223	1.	*	2	0045	298	0.	
1	0605	74	64.	*	1	1220	149	6.	*	1	1835	224	1.	*	2	0050	299	0.	
1	0610	75	61.	*	1	1225	150	6.	*	1	1840	225	1.	*	2	0055	300	0.	

PEAK FLOW

TIME

MAXIMUM AVERAGE FLOW



[illegible]

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*
*      D_SURF
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### OUTPUT CONTROL VARIABLES

IPRNT	1	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE

## DIVERSION

ISTAD	D-SUBF	DIVERSION HYDROGRAPH IDENTIFICATION
DSTRMX	2.00	MAXIMUM VOLUME TO BE DIVERTED

INFLOW

.00	1.00	10.00	40.00	70.00	100.00	300.00	500.00	800.00
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## DIVERTED FLOW

00	1 00	10 00	40 00	70 00	100 00	300 00	500 00	800 00
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DIVERSION HYDROGRAPH D-SUBF

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DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	
1	0000	1	0.	*	1	0615	76	0.	*	1	1230	151	0.	*	1	1845	226	0.	*	1	0000	1	0.	*
1	0005	2	0.	*	1	0620	77	0.	*	1	1235	152	0.	*	1	1850	227	0.	*	1	0005	2	0.	*
1	0010	3	0.	*	1	0625	78	0.	*	1	1240	153	0.	*	1	1855	228	0.	*	1	0010	3	0.	*
1	0015	4	0.	*	1	0630	79	0.	*	1	1245	154	0.	*	1	1900	229	0.	*	1	0015	4	0.	*
1	0020	5	0.	*	1	0635	80	0.	*	1	1250	155	0.	*	1	1905	230	0.	*	1	0020	5	0.	*
1	0025	6	0.	*	1	0640	81	0.	*	1	1255	156	0.	*	1	1910	231	0.	*	1	0025	6	0.	*
1	0030	7	0.	*	1	0645	82	0.	*	1	1300	157	0.	*	1	1915	232	0.	*	1	0030	7	0.	*
1	0035	8	0.	*	1	0650	83	0.	*	1	1305	158	0.	*	1	1920	233	0.	*	1	0035	8	0.	*
1	0040	9	0.	*	1	0655	84	0.	*	1	1310	159	0.	*	1	1925	234	0.	*	1	0040	9	0.	*
1	0045	10	0.	*	1	0700	85	0.	*	1	1315	160	0.	*	1	1930	235	0.	*	1	0045	10	0.	*
1	0050	11	0.	*	1	0705	86	0.	*	1	1320	161	0.	*	1	1935	236	0.	*	1	0050	11	0.	*
1	0055	12	0.	*	1	0710	87	0.	*	1	1325	162	0.	*	1	1940	237	0.	*	1	0055	12	0.	*
1	0100	13	0.	*	1	0715	88	0.	*	1	1330	163	0.	*	1	1945	238	0.	*	1	0100	13	0.	*
1	0105	14	0.	*	1	0720	89	0.	*	1	1335	164	0.	*	1	1950	239	0.	*	1	0105	14	0.	*
1	0110	15	0.	*	1	0725	90	0.	*	1	1340	165	0.	*	1	1955	240	0.	*	1	0110	15	0.	*
1	0115	16	0.	*	1	0730	91	0.	*	1	1345	166	0.	*	1	2000	241	0.	*	1	0115	16	0.	*
1	0120	17	0.	*	1	0735	92	0.	*	1	1350	167	0.	*	1	2005	242	0.	*	1	0120	17	0.	*
1	0125	18	0.	*	1	0740	93	0.	*	1	1355	168	0.	*	1	2010	243	0.	*	1	0125	18	0.	*
1	0130	19	0.	*	1	0745	94	0.	*	1	1400	169	0.	*	1	2015	244	0.	*	1	0130	19	0.	*
1	0135	20	0.	*	1	0750	95	0.	*	1	1405	170	0.	*	1	2020	245	0.	*	1	0135	20	0.	*
1	0140	21	0.	*	1	0755	96	0.	*	1	1410	171	0.	*	1	2025	246	0.	*	1	0140	21	0.	*
1	0145	22	0.	*	1	0800	97	0.	*	1	1415	172	0.	*	1	2030	247	0.	*	1	0145	22	0.	*
1	0150	23	0.	*	1	0805	98	0.	*	1	1420	173	0.	*	1	2035	248	0.	*	1	0150	23	0.	*
1	0155	24	0.	*	1	0810	99	0.	*	1	1425	174	0.	*	1	2040	249	0.	*	1	0155	2		

1	0445	56	0.	*	1	1109	133	0.	*	1	1715	208	0.	*	1	2330	283	0.
1	0450	59	0.	*	1	1105	134	0.	*	1	1720	209	0.	*	1	2335	284	0.
1	0455	60	0.	*	1	1110	135	0.	*	1	1725	210	0.	*	1	2340	285	0.
1	0500	61	0.	*	1	1115	136	0.	*	1	1730	211	0.	*	1	2345	286	0.
1	0505	62	0.	*	1	1120	137	0.	*	1	1735	212	0.	*	1	2350	287	0.
1	0510	63	0.	*	1	1125	138	0.	*	1	1740	213	0.	*	1	2355	288	0.
1	0515	64	0.	*	1	1130	139	0.	*	1	1745	214	0.	*	2	0000	229	0.
1	0520	65	0.	*	1	1135	140	0.	*	1	1750	215	0.	*	2	0005	290	0.
1	0525	66	0.	*	1	1140	141	0.	*	1	1755	216	0.	*	2	0010	291	0.
1	0530	67	0.	*	1	1145	142	0.	*	1	1800	217	0.	*	2	0015	292	0.
1	0535	68	0.	*	1	1150	143	0.	*	1	1805	218	0.	*	2	0020	293	0.
1	0540	69	0.	*	1	1155	144	0.	*	1	1810	219	0.	*	2	0025	294	0.
1	0545	70	0.	*	1	1200	145	0.	*	1	1815	220	0.	*	2	0030	295	0.
1	0550	71	0.	*	1	1205	146	0.	*	1	1820	221	0.	*	2	0035	296	0.
1	0555	72	0.	*	1	1210	147	0.	*	1	1825	222	0.	*	2	0040	297	0.
1	0600	73	0.	*	1	1215	148	0.	*	1	1830	223	0.	*	2	0045	298	0.
1	0605	74	0.	*	1	1220	149	0.	*	1	1835	224	0.	*	2	0050	299	0.
1	0610	75	0.	*	1	1225	150	0.	*	1	1840	225	0.	*	2	0055	300	0.

PEAK FLOW      TIME  
 +    (CFS)      (HR)  
 +    237.      3.08  
                  (CFS)  
                  (INCHES)  
                  (AC-FT)  
 CUMULATIVE AREA -      .51 SQ MI

# HYDROGRAPH AT STATION D\_SURF

DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*
1	0000	1	0.	*	1	0615	76	0.	*	1	1230	151	0.	*	1	1845	226	0.					
1	0005	2	0.	*	1	0620	77	0.	*	1	1235	152	0.	*	1	1850	227	0.					
1	0010	3	0.	*	1	0625	78	0.	*	1	1240	153	0.	*	1	1855	228	0.					
1	0015	4	0.	*	1	0630	79	0.	*	1	1245	154	0.	*	1	1900	229	0.					
1	0020	5	0.	*	1	0635	80	0.	*	1	1250	155	0.	*	1	1905	230	0.					
1	0025	6	0.	*	1	0640	81	0.	*	1	1255	156	0.	*	1	1910	231	0.					
1	0030	7	0.	*	1	0645	82	0.	*	1	1300	157	0.	*	1	1915	232	0.					
1	0035	8	0.	*	1	0650	83	0.	*	1	1305	158	0.	*	1	1920	233	0.					
1	0040	9	0.	*	1	0655	84	0.	*	1	1310	159	0.	*	1	1925	234	0.					
1	0045	10	0.	*	1	0700	85	0.	*	1	1315	160	0.	*	1	1930	235	0.					
1	0050	11	0.	*	1	0705	86	0.	*	1	1320	161	0.	*	1	1935	236	0.					
1	0055	12	0.	*	1	0710	87	0.	*	1	1325	162	0.	*	1	1940	237	0.					
1	0100	13	0.	*	1	0715	88	0.	*	1	1330	163	0.	*	1	1945	238	0.					
1	0105	14	0.	*	1	0720	89	0.	*	1	1335	164	0.	*	1	1950	239	0.					
1	0110	15	0.	*	1	0725	90	0.	*	1	1340	165	0.	*	1	1955	240	0.					
1	0115	16	0.	*	1	0730	91	0.	*	1	1345	166	0.	*	1	2000	241	0.					
1	0120	17	0.	*	1	0735	92	0.	*	1	1350	167	0.	*	1	2005	242	0.					
1	0125	18	0.	*	1	0740	93	0.	*	1	1355	168	0.	*	1	2010	243	0.					
1	0130	19	0.	*	1	0745	94	0.	*	1	1400	169	0.	*	1	2015	244	0.					
1	0135	20	0.	*	1	0750	95	0.	*	1	1405	170	0.	*	1	2020	245	0.					
1	0140	21	0.	*	1	0755	96	0.	*	1	1410	171	0.	*	1	2025	246	0.					
1	0145	22	0.	*	1	0800	97	0.	*	1	1415	172	0.	*	1	2030	247	0.					
1	0150	23	0.	*	1	0805	98	0.	*	1	1420	173	0.	*	1	2035	248	0.					
1	0155	24	0.	*	1	0810	99	0.	*	1	1425	174	0.	*	1	2040	249	0.					
1	0200	25	0.	*	1	0815	100	0.	*	1	1430	175	0.	*	1	2045	250	0.					
1	0205	26	0.	*	1	0820	101	0.	*	1	1435	176	0.	*	1	2050	251	0.					
1	0210	27	0.	*	1	0825	102	0.	*	1	1440	177	0.	*	1	2055	252	0.					
1	0215	28	0.	*	1	0830	103	0.	*	1	1445	178	0.	*	1	2100	253	0.					
1	0220	29	0.	*	1	0835	104	0.	*	1	1450	179	0.	*	1	2105	254	0.					
1	0225	30	0.	*	1	0840	105	0.	*	1	1455	180	0.	*	1	2110	255	0.					
1	0230	31	0.	*	1	0845	106	0.	*	1	1500	181	0.	*	1	2115	256	0.					
1	0235	32	0.	*	1	0850	107	0.	*	1	1505	182	0.	*	1	2120	257	0.					
1	0240	33	0.	*	1	0855	108	0.	*	1	1510	183	0.	*	1	2125	258	0.					
1	0245	34	0.	*	1	0900	109	0.	*	1	1515	184	0.	*	1	2130	259	0.					
1	0250	35	0.	*	1	0905	110	0.	*	1	1520	185	0.	*	1	2135	260	0.					
1	0255	36	0.	*	1	0910	111	0.	*	1	1525	186	0.	*	1	2140	261	0.					
1	0300	37	0.	*	1	0915	112	0.	*	1	1530	187	0.	*	1	2145	262	0.					
1	0305	38	126.	*	1	0920	113	0.	*	1	1535	188	0.	*	1	2150	263	0.					
1	0310	39	309.	*	1	0925	114	0.	*	1	1540	189	0.	*	1	2155	264	0.					
1	0315	40	189.	*	1	0930	115	0.	*	1	1545	190	0.	*	1	2200	265	0.					
1	0320	41	131.	*	1	0935	116	0.	*	1	1550	191	0.	*	1	2205	266	0.					
1	0325	42	101.	*	1	0940	117	0.	*	1	1555	192	0.	*	1	2210	267	0.					
1	0330	43	82.	*	1	0945	118	0.	*	1	1600	193	0.	*	1	2215	268	0.					
1	0335	44	60.	*	1	0950	119	0.	*	1	1605	194	0.	*	1	2220	269	0.					
1	0340	45	38.	*	1	0955	120	0.	*	1	1610	195	0.	*	1	2225	270	0.					
1	0345	46	21.	*	1	1000	121	0.	*	1	1615	196	0.	*	1	2230	271	0.					
1	0350	47	10.	*	1	1005	122	0.	*	1	1620	197	0.	*	1	2235	272	0.					
1	0355	48	3.	*	1	1010	123	0.	*	1	1625	198	0.	*	1	2240	273	0.					
1	0400	49	0.	*	1	1015	124	0.	*	1	1630	199	0.	*	1	2245	274	0.					
1	0405	50	0.	*	1	1020	125	0.	*	1	1635	200	0.	*	1	2250	275	0.					
1	0410	51	0.	*	1	1025	126	0.	*	1	1640	201	0.	*	1	2255	276	0.					
1	0415	52	0.	*	1	1030	127	0.	*	1	1645	202	0.	*	1	2300	277	0.					
1	0420	53	0.	*	1	1035	128	0.	*	1	1650	203	0.	*	1	2305	278	0.					
1	0425	54	0.	*	1	1040	129	0.	*	1	1655	204	0.	*	1	2310	279	0.					
1	0430	55	0.	*	1	1045	130	0.	*	1	1700	205	0.	*	1	2315	280	0.					
1	0435	56	0.	*	1	1050	131	0.	*	1	1705	206	0.	*	1	2320	281	0.					
1	0440	57	0.	*	1	1055	132	0.	*	1	1710	207	0.	*	1	2325	282	0.					
1	0445	58	0.	*	1	1100	133	0.	*	1	1715	208	0.	*	1	2330	283	0.					
1	0450	59	0.	*	1	1105	134	0.	*	1	1720	209	0.	*	1	2335	284	0.					
1	0455	60	0.	*	1	1110	135	0.	*	1	1725	210	0.	*	1	2340	285	0.					
1	0500	61	0.	*	1	1115	136	0.	*	1	1730	211	0.	*	1	2345	286	0.					

1	0505	62	0.	*	1	1120	137	0.	*	1	1735	212	0.	*	1	2350	287	0.
1	0510	63	0.	*	1	1125	138	0.	*	1	1740	213	0.	*	1	2355	288	0.
1	0515	64	0.	*	1	1130	139	0.	*	1	1745	214	0.	*	2	0000	289	0.
1	0520	65	0.	*	1	1135	140	0.	*	1	1750	215	0.	*	2	0005	290	0.
1	0525	66	0.	*	1	1140	141	0.	*	1	1755	216	0.	*	2	0010	291	0.
1	0530	67	0.	*	1	1145	142	0.	*	1	1800	217	0.	*	2	0015	292	0.
1	0535	68	0.	*	1	1150	143	0.	*	1	1805	218	0.	*	2	0020	293	0.
1	0540	69	0.	*	1	1155	144	0.	*	1	1810	219	0.	*	2	0025	294	0.
1	0545	70	0.	*	1	1200	145	0.	*	1	1815	220	0.	*	2	0030	295	0.
1	0550	71	0.	*	1	1205	146	0.	*	1	1820	221	0.	*	2	0035	296	0.
1	0555	72	0.	*	1	1210	147	0.	*	1	1825	222	0.	*	2	0040	297	0.
1	0600	73	0.	*	1	1215	148	0.	*	1	1830	223	0.	*	2	0045	298	0.
1	0605	74	0.	*	1	1220	149	0.	*	1	1835	224	0.	*	2	0050	299	0.
1	0610	75	0.	*	1	1225	150	0.	*	1	1840	225	0.	*	2	0055	300	0.

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 + (CFS) (HR) 6-HR 24-HR 72-HR 24.92-HR  
 + 309. 3.17 15. 4. 4. 4.  
 (INCHES) .271 .271 .271 .271  
 (AC-FT) 7. 7. 7. 7.  
 CUMULATIVE AREA = .51 SQ MI

633 KK

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 \* CS40B \*  
 \* \*  
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COMBINE

634 KO

OUTPUT CONTROL VARIABLES

IPRNT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 COMBINE PIPE FLOW, DIVERGED SURFACE FLOW AND REMAINING SURFACE FLOW

636 HC

HYDROGRAPH COMBINATION

ICOMP 3 NUMBER OF HYDROGRAPHS TO COMBINE

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# HYDROGRAPH AT STATION CS40B SUM OF 3 HYDROGRAPHS

DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*
1	0000	1	0.	*	1	0615	76	3.	*	1	1230	151	0.	*	1	1845	226	0.	*				
1	0005	2	0.	*	1	0620	77	2.	*	1	1235	152	0.	*	1	1850	227	0.	*				
1	0010	3	0.	*	1	0625	78	2.	*	1	1240	153	0.	*	1	1855	228	0.	*				
1	0015	4	0.	*	1	0630	79	1.	*	1	1245	154	0.	*	1	1900	229	0.	*				
1	0020	5	1.	*	1	0635	80	1.	*	1	1250	155	0.	*	1	1905	230	0.	*				
1	0025	6	1.	*	1	0640	81	1.	*	1	1255	156	0.	*	1	1910	231	0.	*				
1	0030	7	2.	*	1	0645	82	1.	*	1	1300	157	0.	*	1	1915	232	0.	*				
1	0035	8	2.	*	1	0650	83	1.	*	1	1305	158	0.	*	1	1920	233	0.	*				
1	0040	9	3.	*	1	0655	84	1.	*	1	1310	159	0.	*	1	1925	234	0.	*				
1	0045	10	4.	*	1	0700	85	0.	*	1	1315	160	0.	*	1	1930	235	0.	*				
1	0050	11	4.	*	1	0705	86	0.	*	1	1320	161	0.	*	1	1935	236	0.	*				
1	0055	12	4.	*	1	0710	87	0.	*	1	1325	162	0.	*	1	1940	237	0.	*				
1	0100	13	5.	*	1	0715	88	0.	*	1	1330	163	0.	*	1	1945	238	0.	*				
1	0105	14	5.	*	1	0720	89	0.	*	1	1335	164	0.	*	1	1950	239	0.	*				
1	0110	15	5.	*	1	0725	90	0.	*	1	1340	165	0.	*	1	1955	240	0.	*				
1	0115	16	5.	*	1	0730	91	0.	*	1	1345	166	0.	*	1	2000	241	0.	*				
1	0120	17	5.	*	1	0735	92	0.	*	1	1350	167	0.	*	1	2005	242	0.	*				
1	0125	18	6.	*	1	0740	93	0.	*	1	1355	168	0.	*	1	2010	243	0.	*				
1	0130	19	6.	*	1	0745	94	0.	*	1	1400	169	0.	*	1	2015	244	0.	*				
1	0135	20	6.	*	1	0750	95	0.	*	1	1405	170	0.	*	1	2020	245	0.	*				
1	0140	21	6.	*	1	0755	96	0.	*	1	1410	171	0.	*	1	2025	246	0.	*				
1	0145	22	7.	*	1	0800	97	0.	*	1	1415	172	0.	*	1	2030	247	0.	*				
1	0150	23	7.	*	1	0805	98	0.	*	1	1420	173	0.	*	1	2035	248	0.	*				
1	0155	24	7.	*	1	0810	99	0.	*	1	1425	174	0.	*	1	2040	249	0.	*				
1	0200	25	8.	*	1	0815	100	0.	*	1	1430	175	0.	*	1	2045	250	0.	*				
1	0205	26	8.	*	1	0820	101	0.	*	1	1435	176	0.	*	1	2050	251	0.	*				
1	0210	27	9.	*	1	0825	102	0.	*	1	1440	177	0.	*	1	2055	252	0.	*				
1	0215	28	10.	*	1	0830	103	0.	*	1	1445	178	0.	*	1	2100	253	0.	*				
1	0220	29	10.	*	1	0835	104	0.	*	1	1450	179	0.	*	1	2105	254	0.	*				
1	0225	30	11.	*	1	0840	105	0.	*	1	1455	180	0.	*	1	2110	255	0.	*				
1	0230	31	11.	*	1	0845	106	0.	*	1	1500	181	0.	*	1	2115	256	0.	*				
1	0235	32	19.	*	1	0850	107	0.	*	1	1505	182	0.	*	1	2120	257	0.	*				
1	0240	33	28.	*	1	0855	108	0.	*	1	1510	183	0.	*	1	2125	258	0.	*				
1	0245	34	39.	*	1	0900	109	0.	*	1	1515	184	0.	*	1	2130	259	0.	*				
1	0250	35	53.	*	1	0905	110	0.	*	1	1520	185	0.	*	1	2135	260	0.	*				
1	0255	36	74.	*	1	0910	111	0.	*	1	1525	186	0.	*	1	2140	261	0.	*				
1	0300	37	98.	*	1	0915	112	0.	*	1	1530	187	0.	*	1	2145	262	0.	*				
1	0305	38	156.	*	1	0920	113	0.	*	1	1535	188	0.	*	1	2150	263	0.	*				
1	0310	39	339.	*	1	0925	114	0.	*	1	1540	189	0.	*	1	2155	264	0.	*				
1	0315	40	219.	*	1	0930	115	0.	*	1	1545	190	0.	*	1	2200	265	0.	*				
1	0320	41	161.	*	1	0935	116	0.	*	1	1550	191	0.	*	1	2205	266	0.	*				
1	0325	42	131.	*	1	0940	117	0.	*	1	1555	192	0.	*	1	2210	267	0.	*				

1	0330	43	112.	*	1	0945	118	0.	*	1	1600	193	0.	*	1	2215	268	0.
1	0335	44	90.	*	1	0950	119	0.	*	1	1605	194	0.	*	1	2220	269	0.
1	0340	45	68.	*	1	0955	120	0.	*	1	1610	195	0.	*	1	2225	270	0.
1	0345	46	51.	*	1	1000	121	0.	*	1	1615	196	0.	*	1	2230	271	0.
1	0350	47	40.	*	1	1005	122	0.	*	1	1620	197	0.	*	1	2235	272	0.
1	0355	48	33.	*	1	1010	123	0.	*	1	1625	198	0.	*	1	2240	273	0.
1	0400	49	27.	*	1	1015	124	0.	*	1	1630	199	0.	*	1	2245	274	0.
1	0405	50	23.	*	1	1020	125	0.	*	1	1635	200	0.	*	1	2250	275	0.
1	0410	51	20.	*	1	1025	126	0.	*	1	1640	201	0.	*	1	2255	276	0.
1	0415	52	18.	*	1	1030	127	0.	*	1	1645	202	0.	*	1	2300	277	0.
1	0420	53	16.	*	1	1035	128	0.	*	1	1650	203	0.	*	1	2305	278	0.
1	0425	54	14.	*	1	1040	129	0.	*	1	1655	204	0.	*	1	2310	279	0.
1	0430	55	12.	*	1	1045	130	0.	*	1	1700	205	0.	*	1	2315	280	0.
1	0435	56	11.	*	1	1050	131	0.	*	1	1705	206	0.	*	1	2320	281	0.
1	0440	57	9.	*	1	1055	132	0.	*	1	1710	207	0.	*	1	2325	282	0.
1	0445	58	8.	*	1	1100	133	0.	*	1	1715	208	0.	*	1	2330	283	0.
1	0450	59	7.	*	1	1105	134	0.	*	1	1720	209	0.	*	1	2335	284	0.
1	0455	60	7.	*	1	1110	135	0.	*	1	1725	210	0.	*	1	2340	285	0.
1	0500	61	7.	*	1	1115	136	0.	*	1	1730	211	0.	*	1	2345	286	0.
1	0505	62	7.	*	1	1120	137	0.	*	1	1735	212	0.	*	1	2350	287	0.
1	0510	63	6.	*	1	1125	138	0.	*	1	1740	213	0.	*	1	2355	288	0.
1	0515	64	6.	*	1	1130	139	0.	*	1	1745	214	0.	*	2	0000	289	0.
1	0520	65	6.	*	1	1135	140	0.	*	1	1750	215	0.	*	2	0005	290	0.
1	0525	66	6.	*	1	1140	141	0.	*	1	1755	216	0.	*	2	0010	291	0.
1	0530	67	5.	*	1	1145	142	0.	*	1	1800	217	0.	*	2	0015	292	0.
1	0535	68	5.	*	1	1150	143	0.	*	1	1805	218	0.	*	2	0020	293	0.
1	0540	69	5.	*	1	1155	144	0.	*	1	1810	219	0.	*	2	0025	294	0.
1	0545	70	5.	*	1	1200	145	0.	*	1	1815	220	0.	*	2	0030	295	0.
1	0550	71	5.	*	1	1205	146	0.	*	1	1820	221	0.	*	2	0035	296	0.
1	0555	72	5.	*	1	1210	147	0.	*	1	1825	222	0.	*	2	0040	297	0.
1	0600	73	5.	*	1	1215	148	0.	*	1	1830	223	0.	*	2	0045	298	0.
1	0605	74	4.	*	1	1220	149	0.	*	1	1835	224	0.	*	2	0050	299	0.
1	0610	75	3.	*	1	1225	150	0.	*	1	1840	225	0.	*	2	0055	300	0.

```

PEAK FLOW      TIME
+ (CFS)        (HR)
+ 339.         3.17
(CFS)
(INCHES)      .540
(AC-FT)       15.

```

CUMULATIVE AREA = .51 SQ MI

637 KK

```

*****
* S40BAS *
*****

```

638 KO

#### OUTPUT CONTROL VARIABLES

```

IPRNT      1  PRINT CONTROL
IPLOT      0  PLOT CONTROL
QSCAL      0.  HYDROGRAPH PLOT SCALE
ROUTE DIVERTED FLOW THROUGH OFFLINE BASIN CONCEPT MAX H =5.9
ASSUMED 1000'X 80' BASIN WITH 5:1 SIDE SLOPES & 36" OUTLET
24" BLEED-OFF PIPE PLUS 20' WIDE SPILLWAY AT 3.8'

```

#### HYDROGRAPH ROUTING DATA

642 RS

#### STORAGE ROUTING

```

NSTPS      1  NUMBER OF SUBREACHES
LTYP       STOR TYPE OF INITIAL CONDITION
RSVRIC     -1.00 INITIAL CONDITION
X          .00 WORKING R AND D COEFFICIENT

```

643 SV

#### STORAGE

```

.0          .0          .1          .9          1.8          3.0          4.5          5.2          5.5          5.8
6.2

```

645 SE

#### ELEVATION

```

.00         .80         1.00         2.00         3.00         4.00         5.00         5.40         5.60         5.80
6.00

```

647 SL

#### LOW-LEVEL OUTLET

```

ELEV      1.00  ELEVATION AT CENTER OF OUTLET
CAREA     3.14  CROSS-SECTIONAL AREA
COQL      .62   COEFFICIENT
EXPL      .50   EXPONENT OF HEAD

```

648 SS

#### SPILLWAY

```

CREL      3.80  SPILLWAY CREST ELEVATION
SPWID     20.00 SPILLWAY WIDTH
COQW      2.80  WEIR COEFFICIENT
EXPW      1.50  EXPONENT OF HEAD

```

\*\*\*

#### COMPUTED OUTFLOW-ELEVATION DATA

```

OUTFLOW     .00      .00      15.21      16.18      17.27      18.53      19.98      21.68      23.70      26.13
ELEVATION    .00      1.00      1.95      2.07      2.22      2.41      2.64      2.93      3.30      3.80

OUTFLOW     26.75     28.89     33.54     41.63     54.26     72.26     96.63    128.34    168.36    217.65
ELEVATION    3.34     3.92     4.03     4.19     4.39     4.63     4.91     5.23     5.60     6.00

```

## COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

STORAGE	.00	.00	.14	.83	.87	.94	1.09	1.27	1.49	1.77
OUTFLOW	.00	.00	.00	15.21	15.61	16.18	17.27	19.53	19.98	21.68
ELEVATION	.00	.80	1.00	1.95	2.00	2.07	2.22	2.41	2.64	2.93
STORAGE	1.84	2.20	2.80	2.85	2.94	3.04	3.09	3.32	3.61	3.96
OUTFLOW	22.08	23.70	26.13	26.75	28.89	32.05	33.54	41.58	54.26	72.26
ELEVATION	3.00	3.30	3.80	3.94	3.92	4.00	4.03	4.19	4.39	4.63
STORAGE	4.36	4.49	4.88	5.16	5.48	5.82	6.15			
OUTFLOW	96.63	104.84	128.34	146.09	168.36	192.60	217.65			
ELEVATION	4.91	5.00	5.23	5.40	5.60	5.80	6.00			

## HYDROGRAPH AT STATION S40BAS

DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE	*	DA	MON	HRMN	ORD	OUTFLOW	STORAGE	STAGE
1		0000	1	0.	.0	.8	*	1		0820	101	1.	.2	1.0	*	1		1640	201	0.	.1	1.0
1		0005	2	0.	.0	.8	*	1		0825	102	0.	.2	1.0	*	1		1645	202	0.	.1	1.0
1		0010	3	0.	.0	.8	*	1		0830	103	0.	.2	1.0	*	1		1650	203	0.	.1	1.0
1		0015	4	0.	.0	.8	*	1		0835	104	0.	.2	1.0	*	1		1655	204	0.	.1	1.0
1		0020	5	0.	.0	.8	*	1		0840	105	0.	.2	1.0	*	1		1700	205	0.	.1	1.0
1		0025	6	0.	.0	.8	*	1		0845	106	0.	.2	1.0	*	1		1705	206	0.	.1	1.0
1		0030	7	0.	.0	.8	*	1		0850	107	0.	.2	1.0	*	1		1710	207	0.	.1	1.0
1		0035	8	0.	.0	.9	*	1		0855	108	0.	.2	1.0	*	1		1715	208	0.	.1	1.0
1		0040	9	0.	.1	.9	*	1		0900	109	0.	.1	1.0	*	1		1720	209	0.	.1	1.0
J		0045	10	0.	.1	.9	*	1		0905	110	0.	.1	1.0	*	1		1725	210	0.	.1	1.0
1		0050	11	0.	.1	.9	*	1		0910	111	0.	.1	1.0	*	1		1730	211	0.	.1	1.0
1		0055	12	0.	.1	1.0	*	1		0915	112	0.	.1	1.0	*	1		1735	212	0.	.1	1.0
1		0100	13	0.	.2	1.0	*	1		0920	113	0.	.1	1.0	*	1		1740	213	0.	.1	1.0
1		0105	14	1.	.2	1.1	*	1		0925	114	0.	.1	1.0	*	1		1745	214	0.	.1	1.0
1		0110	15	2.	.2	1.1	*	1		0930	115	0.	.1	1.0	*	1		1750	215	0.	.1	1.0
1		0115	16	2.	.2	1.1	*	1		0935	116	0.	.1	1.0	*	1		1755	216	0.	.1	1.0
1		0120	17	3.	.3	1.2	*	1		0940	117	0.	.1	1.0	*	1		1800	217	0.	.1	1.0
1		0125	18	3.	.3	1.2	*	1		0945	118	0.	.1	1.0	*	1		1805	218	0.	.1	1.0
1		0130	19	3.	.3	1.2	*	1		0950	119	0.	.1	1.0	*	1		1810	219	0.	.1	1.0
1		0135	20	4.	.3	1.2	*	1		0955	120	0.	.1	1.0	*	1		1815	220	0.	.1	1.0
1		0140	21	4.	.3	1.3	*	1		1000	121	0.	.1	1.0	*	1		1820	221	0.	.1	1.0
1		0145	22	4.	.3	1.3	*	1		1005	122	0.	.1	1.0	*	1		1825	222	0.	.1	1.0
1		0150	23	5.	.4	1.3	*	1		1010	123	0.	.1	1.0	*	1		1830	223	0.	.1	1.0
1		0155	24	5.	.4	1.3	*	1		1015	124	0.	.1	1.0	*	1		1835	224	0.	.1	1.0
1		0200	25	5.	.4	1.3	*	1		1020	125	0.	.1	1.0	*	1		1840	225	0.	.1	1.0
1		0205	26	6.	.4	1.4	*	1		1025	126	0.	.1	1.0	*	1		1845	226	0.	.1	1.0
1		0210	27	6.	.4	1.4	*	1		1030	127	0.	.1	1.0	*	1		1850	227	0.	.1	1.0
1		0215	28	7.	.4	1.4	*	1		1035	128	0.	.1	1.0	*	1		1855	228	0.	.1	1.0
1		0220	29	7.	.5	1.4	*	1		1040	129	0.	.1	1.0	*	1		1900	229	0.	.1	1.0
1		0225	30	8.	.5	1.5	*	1		1045	130	0.	.1	1.0	*	1		1905	230	0.	.1	1.0
1		0230	31	8.	.5	1.5	*	1		1050	131	0.	.1	1.0	*	1		1910	231	0.	.1	1.0
1		0235	32	9.	.6	1.6	*	1		1055	132	0.	.1	1.0	*	1		1915	232	0.	.1	1.0
1		0240	33	11.	.7	1.7	*	1		1100	133	0.	.1	1.0	*	1		1920	233	0.	.1	1.0
1		0245	34	14.	.8	1.9	*	1		1105	134	0.	.1	1.0	*	1		1925	234	0.	.1	1.0
1		0250	35	17.	1.0	2.1	*	1		1110	135	0.	.1	1.0	*	1		1930	235	0.	.1	1.0
1		0255	36	19.	1.3	2.5	*	1		1115	136	0.	.1	1.0	*	1		1935	236	0.	.1	1.0
2		0300	37	22.	1.8	2.9	*	2		1120	137	0.	.2	1.0	*	2		1940	237	0.	.1	1.0
1		0305	38	25.	2.5	3.5	*	1		1125	138	0.	.1	1.0	*	1		1945	238	0.	.1	1.0
1		0310	39	68.	3.9	4.6	*	1		1130	139	0.	.1	1.0	*	1		1950	239	0.	.1	1.0
1		0315	40	141.	5.1	5.4	*	1		1135	140	0.	.1	1.0	*	1		1955	240	0.	.1	1.0
1		0320	41	159.	5.4	5.5	*	1		1140	141	0.	.1	1.0	*	1		2000	241	0.	.1	1.0
1		0325	42	154.	5.3	5.5	*	1		1145	142	0.	.1	1.0	*	1		2005	242	0.	.1	1.0
1		0330	43	142.	5.1	5.4	*	1		1150	143	0.	.1	1.0	*	1		2010	243	0.	.1	1.0
1		0335	44	127.	4.9	5.2	*	1		1155	144	0.	.1	1.0	*	1		2015	244	0.	.1	1.0
1		0340	45	111.	4.6	5.1	*	1		1200	145	0.	.1	1.0	*	1		2020	245	0.	.1	1.0
1		0345	46	93.	4.3	4.9	*	1		1205	146	0.	.1	1.0	*	1		2025	246	0.	.1	1.0
1		0350	47	77.	4.0	4.7	*	1		1210	147	0.	.1	1.0	*	1		2030	247	0.	.1	1.0
2		0355	48	64.	3.8	4.5	*	2		1215	148	0.	.2	1.0	*	2		2035	248	0.	.1	1.0
1		0400	49	54.	3.6	4.4	*	1		1220	149	0.	.1	1.0	*	1		2040	249	0.	.1	1.0
1		0405	50	46.	3.4	4.3	*	1		1225	150	0.	.1	1.0	*	1		2045	250	0.	.1	1.0
1		0410	51	40.	3.3	4.2	*	1		1230	151	0.	.1	1.0	*	1		2050	251	0.	.1	1.0
1		0415	52	36.	3.1	4.1	*	1		1235	152	0.	.1	1.0	*	1		2055	252	0.	.1	1.0
1		0420	53	32.	3.0	4.0	*	1		1240	153	0.	.1	1.0	*	1		2100	253	0.	.1	1.0
1		0425	54	29.	2.9	3.9	*	1		1245	154	0.	.1	1.0	*	1		2105	254	0.	.1	1.0
1		0430	55	27.	2.8	3.8	*	1		1250	155	0.	.1	1.0	*	1		2110	255	0.	.1	1.0
1		0435	56	26.	2.7	3.7	*	1		1255	156	0.	.1	1.0	*	1		2115	256	0.	.1	1.0
1		0440	57	25.	2.6	3.7	*	1		1300	157	0.	.1	1.0	*	1		2120	257	0.	.1	1.0
1		0445	58	25.	2.5	3.6	*	1		1305	158	0.	.1	1.0	*	1		2125	258	0.	.1	1.0
1		0450	59	24.	2.4	3.5	*	1		1310	159	0.	.1	1.0	*	1		2130	259	0.	.1	1.0
1		0455	60	24.	2.3	3.4	*	1		1315	160	0.	.1	1.0	*	1		2135	260	0.	.1	1.0
1		0500	61	23.	2.2	3.3	*	1		1320	161	0.	.1	1.0	*	1		2140	261	0.	.1	1.0
1		0505	62	23.	2.0	3.2	*	1		1325	162	0.	.1	1.0	*	1		2145	262	0.	.1	1.0
1		0510	63	22.	1.9	3.1	*	1		1330	163	0.	.1	1.0	*	1		2150	263	0.	.1	1.0
1		0515	64	22.	1.8	3.0	*	1		1335	164	0.	.1	1.0	*	1		2155	264	0.	.1	1.0
1		0520	65	21.	1.7	2.9	*	1		1340	165	0.	.1	1.0	*	1		2200	265	0.	.1	1.0
1		0525	66	21.	1.6	2.8	*	1		1345	166	0.	.1	1.0	*	1		2205	266	0.	.1	1.0
1		0530	67	20.	1.5	2.7	*	1		1350	167	0.	.1	1.0	*	1		2210	267	0.	.1	1.0
1		0535	68	19.	1.4	2.6	*	1		1355	168	0.	.1	1.0	*	1		2215	268	0.	.1	1.0
1		0540	69	19.	1.3	2.5	*	1		1400	169	0.	.2	1.0	*	1		2220	269	0.	.1	1.0
1		0545	70	18.	1.2	2.4	*	1		1405	170	0.	.1	1.0	*	1		2225	270	0.	.1	1.0
1		0550	71	18.	1.1	2.3	*	1		1410	171	0.	.1	1.0	*	1		2230	271	0.	.1	1.0
1		0555	72																			

1	0625	78	10.	.6	1.6 *	1	1445	178	0.	.1	1.0 *	1	2305	278	0.	.1	1.0
1	0630	72	9.	.5	1.6 *	1	1450	179	0.	.1	1.0 *	1	2310	279	0.	.1	1.0
1	0635	80	8.	.5	1.5 *	1	1455	180	0.	.1	1.0 *	1	2315	280	0.	.1	1.0
1	0640	81	7.	.5	1.4 *	1	1500	181	0.	.1	1.0 *	1	2320	281	0.	.1	1.0
1	0645	82	6.	.4	1.4 *	1	1505	182	0.	.1	1.0 *	1	2325	282	0.	.1	1.0
1	0650	83	5.	.4	1.3 *	1	1510	183	0.	.1	1.0 *	1	2330	283	0.	.1	1.0
1	0655	84	5.	.4	1.3 *	1	1515	184	0.	.1	1.0 *	1	2335	284	0.	.1	1.0
1	0700	85	4.	.3	1.3 *	1	1520	185	0.	.1	1.0 *	1	2340	285	0.	.1	1.0
1	0705	86	4.	.3	1.2 *	1	1525	186	0.	.1	1.0 *	1	2345	286	0.	.1	1.0
1	0710	87	3.	.3	1.2 *	1	1530	187	0.	.1	1.0 *	1	2350	287	0.	.1	1.0
1	0715	88	3.	.3	1.2 *	1	1535	188	0.	.1	1.0 *	1	2355	288	0.	.1	1.0
1	0720	89	2.	.2	1.1 *	1	1540	189	0.	.1	1.0 *	2	0000	289	0.	.1	1.0
1	0725	90	2.	.2	1.1 *	1	1545	190	0.	.1	1.0 *	2	0005	290	0.	.1	1.0
1	0730	91	2.	.2	1.1 *	1	1550	191	0.	.1	1.0 *	2	0010	291	0.	.1	1.0
1	0735	92	2.	.2	1.1 *	1	1555	192	0.	.1	1.0 *	2	0015	292	0.	.1	1.0
1	0740	93	1.	.2	1.1 *	1	1600	193	0.	.1	1.0 *	2	0020	293	0.	.1	1.0
1	0745	94	1.	.2	1.1 *	1	1605	194	0.	.1	1.0 *	2	0025	294	0.	.1	1.0
1	0750	95	1.	.2	1.1 *	1	1610	195	0.	.1	1.0 *	2	0030	295	0.	.1	1.0
1	0755	96	1.	.2	1.1 *	1	1615	196	0.	.1	1.0 *	2	0035	296	0.	.1	1.0
1	0800	97	1.	.2	1.1 *	1	1620	197	0.	.1	1.0 *	2	0040	297	0.	.1	1.0
1	0805	98	1.	.2	1.0 *	1	1625	198	0.	.1	1.0 *	2	0045	298	0.	.1	1.0
1	0810	99	1.	.2	1.0 *	1	1630	199	0.	.1	1.0 *	2	0050	299	0.	.1	1.0
1	0815	100	1.	.2	1.0 *	1	1635	200	0.	.1	1.0 *	2	0055	300	0.	.1	1.0

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
(CFS)	(HR)				
159.	3.33	29.	7.	7.	7.
(INCHES)		.532	.539	.539	.539
(AC-FT)		14.	15.	15.	15.

PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
(AC-FT)	(HR)				
5.	3.33	2.	1.	1.	1.

PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
(FEET)	(HR)				
5.52	3.33	2.64	1.42	1.40	1.40

CUMULATIVE AREA = .51 SQ MI

649 KK

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* P33E.1 *
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650 KG

OUTPUT CONTROL VARIABLES

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IPRNT      1  PRINT CONTROL
IPLLOT      0  PLOT CONTROL
QSCAL       0.  HYDROGRAPH PLOT SCALE
DIVIDE THE FLOW INTO TWO ADOT CULVERTS

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DT	DIVERSION	ISTAD	D33C.2	DIVERSION HYDROGRAPH IDENTIFICATION				
DI	INFLOW	.00	100.00	200.00	400.00	600.00		
DQ	DIVERTED FLOW	.00	68.00	136.00	272.00	408.00		

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DIVERSION HYDROGRAPH D33C.2

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	1	0.	*	1	0615	76	9.	*	1	1230	151	0.	*	1	1845	226	0.	
1	0005	2	0.	*	1	0620	77	8.	*	1	1235	152	0.	*	1	1850	227	0.	
1	0010	3	0.	*	1	0625	78	7.	*	1	1240	153	0.	*	1	1855	228	0.	
1	0015	4	0.	*	1	0630	79	6.	*	1	1245	154	0.	*	1	1900	229	0.	
1	0020	5	0.	*	1	0635	80	5.	*	1	1250	155	0.	*	1	1905	230	0.	
1	0025	6	0.	*	1	0640	81	5.	*	1	1255	156	0.	*	1	1910	231	0.	
1	0030	7	0.	*	1	0645	82	4.	*	1	1300	157	0.	*	1	1915	232	0.	
1	0035	8	0.	*	1	0650	83	4.	*	1	1305	158	0.	*	1	1920	233	0.	
1	0040	9	0.	*	1	0655	84	3.	*	1	1310	159	0.	*	1	1925	234	0.	
1	0045	10	0.	*	1	0700	85	3.	*	1	1315	160	0.	*	1	1930	235	0.	
1	0050	11	0.	*	1	0705	86	2.	*	1	1320	161	0.	*	1	1935	236	0.	
1	0055	12	0.	*	1	0710	87	2.	*	1	1325	162	0.	*	1	1940	237	0.	
1	0100	13	0.	*	1	0715	88	2.	*	1	1330	163	0.	*	1	1945	238	0.	
1	0105	14	1.	*	1	0720	89	2.	*	1	1335	164	0.	*	1	1950	239	0.	
1	0110	15	1.	*	1	0725	90	1.	*	1	1340	165	0.	*	1	1955	240	0.	
1	0115	16	1.	*	1	0730	91	1.	*	1	1345	166	0.	*	1	2000	241	0.	
1	0120	17	2.	*	1	0735	92	1.	*	1	1350	167	0.	*	1	2005	242	0.	
1	0125	18	2.	*	1	0740	93	1.	*	1	1355	168	0.	*	1	2010	243	0.	
1	0130	19	2.	*	1	0745	94	1.	*	1	1400	169	0.	*	1	2015	244	0.	
1	0135	20	3.	*	1	0750	95	1.	*	1	1405	170	0.	*	1	2020	245	0.	

1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127 128 129 130 131 132 133 134 135 136 137 138 139 140 141 142 143 144 145 146 147 148 149 150 151 152 153 154 155 156 157 158 159 160 161 162 163 164 165 166 167 168 169 170 171 172 173 174 175 176 177 178 179 180 181 182 183 184 185 186 187 188 189 190 191 192 193 194 195 196 197 198 199 200 201 202 203 204 205 206 207 208 209 210 211 212 213 214 215 216 217 218 219 220 221 222 223 224 225 226 227 228 229 230 231 232 233 234 235 236 237 238 239 240 241 242 243 244 245 246 247 248 249 250 251 252 253 254 255 256 257 258 259 260 261 262 263 264 265 266 267 268 269 270 271 272 273 274 275 276 277 278 279 280 281 282 283 284 285 286 287 288 289 290 291 292 293 294 295 296 297 298 299 300 301 302 303 304 305 306 307 308 309 310 311 312 313 314 315 316 317 318 319 320 321 322 323 324 325 326 327 328 329 330 331 332 333 334 335 336 337 338 339 340 341 342 343 344 345 346 347 348 349 350 351 352 353 354 355 356 357 358 359 360 361 362 363 364 365 366 367 368 369 370 371 372 373 374 375 376 377 378 379 380 381 382 383 384 385 386 387 388 389 390 391 392 393 394 395 396 397 398 399 400 401 402 403 404 405 406 407 408 409 410 411 412 413 414 415 416 417 418 419 420 421 422 423 424 425 426 427 428 429 430 431 432 433 434 435 436 437 438 439 440 441 442 443 444 445 446 447 448 449 450 451 452 453 454 455 456 457 458 459 460 461 462 463 464 465 466 467 468 469 470 471 472 473 474 475 476 477 478 479 480 481 482 483 484 485 486 487 488 489 490 491 492 493 494 495 496 497 498 499 500 501 502 503 504 505 506 507 508 509 510 511 512 513 514 515 516 517 518 519 520 521 522 523 524 525 526 527 528 529 530 531 532 533 534 535 536 537 538 539 540 541 542 543 544 545 546 547 548 549 550 551 552 553 554 555 556 557 558 559 560 561 562 563 564 565 566 567 568 569 570 571 572 573 574 575 576 577 578 579 580 581 582 583 584 585 586 587 588 589 590 591 592 593 594 595 596 597 598 599 600 601 602 603 604 605 606 607 608 609 610 611 612 613 614 615 616 617 618 619 620 621 622 623 624 625 626 627 628 629 630 631 632 633 634 635 636 637 638 639 640 641 642 643 644 645 646 647 648 649 650 651 652 653 654 655 656 657 658 659 660 661 662 663 664 665 666 667 668 669 670 671 672 673 674 675 676 677 678 679 680 681 682 683 684 685 686 687 688 689 690 691 692 693 694 695 696 697 698 699 700 701 702 703 704 705 706 707 708 709 710 711 712 713 714 715 716 717 718 719 720 721 722 723 724 725 726 727 728 729 730 731 732 733 734 735 736 737 738 739 740 741 742 743 744 745 746 747 748 749 750 751 752 753 754 755 756 757 758 759 760 761 762 763 764 765 766 767 768 769 770 771 772 773 774 775 776 777 778 779 780 781 782 783 784 785 786 787 788 789 790 791 792 793 794 795 796 797 798 799 800 801 802 803 804 805 806 807 808 809 810 811 812 813 814 815 816 817 818 819 820 821 822 823 824 825 826 827 828 829 830 831 832 833 834 835 836 837 838 839 840 841 842 843 844 845 846 847 848 849 850 851 852 853 854 855 856 857 858 859 860 861 862 863 864 865 866 867 868 869 870 871 872 873 874 875 876 877 878 879 880 881 882 883 884 885 886 887 888 889 890 891 892 893 894 895 896 897 898 899 900 901 902 903 904 905 906 907 908 909 910 911 912 913 914 915 916 917 918 919 920 921 922 923 924 925 926 927 928 929 930 931 932 933 934 935 936 937 938 939 940 941 942 943 944 945 946 947 948 949 950 951 952 953 954 955 956 957 958 959 960 961 962 963 964 965 966 967 968 969 970 971 972 973 974 975 976 977 978 979 980 981 982 983 984 985 986 987 988 989 990 991 992 993 994 995 996 997 998 999 1000 1001 1002 1003 1004 1005 1006 1007 1008 1009 1010 1011 1012 1013 1014 1015 1016 1017 1018 1019 1020 1021 1022 1023 1024 1025 1026 1027 1028 1029 1030 1031 1032 1033 1034 1035 1036 1037 1038 1039 104

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[illegible]

1	0200	25	2.	*	1	0815	100	0.	*	1	1430	175	0.	*	1	2045	250	0.
1	0205	26	2.	*	1	0820	101	0.	*	1	1435	176	0.	*	1	2050	251	0.
1	0210	27	2.	*	1	0825	102	0.	*	1	1440	177	0.	*	1	2055	252	0.
1	0215	28	2.	*	1	0830	103	0.	*	1	1445	178	0.	*	1	2100	253	0.
1	0220	29	2.	*	1	0835	104	0.	*	1	1450	179	0.	*	1	2105	254	0.
1	0225	30	2.	*	1	0840	105	0.	*	1	1455	180	0.	*	1	2110	255	0.
1	0230	31	3.	*	1	0845	106	0.	*	1	1500	181	0.	*	1	2115	256	0.
1	0235	32	3.	*	1	0850	107	0.	*	1	1505	182	0.	*	1	2120	257	0.
1	0240	33	4.	*	1	0855	108	0.	*	1	1510	183	0.	*	1	2125	258	0.
1	0245	34	5.	*	1	0900	109	0.	*	1	1515	184	0.	*	1	2130	259	0.
1	0250	35	5.	*	1	0905	110	0.	*	1	1520	185	0.	*	1	2135	260	0.
1	0255	36	6.	*	1	0910	111	0.	*	1	1525	186	0.	*	1	2140	261	0.
1	0300	37	7.	*	1	0915	112	0.	*	1	1530	187	0.	*	1	2145	262	0.
1	0305	38	8.	*	1	0920	113	0.	*	1	1535	188	0.	*	1	2150	263	0.
1	0310	39	22.	*	1	0925	114	0.	*	1	1540	189	0.	*	1	2155	264	0.
1	0315	40	45.	*	1	0930	115	0.	*	1	1545	190	0.	*	1	2200	265	0.
1	0320	41	51.	*	1	0935	116	0.	*	1	1550	191	0.	*	1	2205	266	0.
1	0325	42	49.	*	1	0940	117	0.	*	1	1555	192	0.	*	1	2210	267	0.
1	0330	43	45.	*	1	0945	118	0.	*	1	1600	193	0.	*	1	2215	268	0.
1	0335	44	41.	*	1	0950	119	0.	*	1	1605	194	0.	*	1	2220	269	0.
1	0340	45	35.	*	1	0955	120	0.	*	1	1610	195	0.	*	1	2225	270	0.
1	0345	46	30.	*	1	1000	121	0.	*	1	1615	196	0.	*	1	2230	271	0.
1	0350	47	25.	*	1	1005	122	0.	*	1	1620	197	0.	*	1	2235	272	0.
1	0355	48	20.	*	1	1010	123	0.	*	1	1625	198	0.	*	1	2240	273	0.
1	0400	49	17.	*	1	1015	124	0.	*	1	1630	199	0.	*	1	2245	274	0.
1	0405	50	15.	*	1	1020	125	0.	*	1	1635	200	0.	*	1	2250	275	0.
1	0410	51	13.	*	1	1025	126	0.	*	1	1640	201	0.	*	1	2255	276	0.
1	0415	52	11.	*	1	1030	127	0.	*	1	1645	202	0.	*	1	2300	277	0.
1	0420	53	10.	*	1	1035	128	0.	*	1	1650	203	0.	*	1	2305	278	0.
1	0425	54	9.	*	1	1040	129	0.	*	1	1655	204	0.	*	1	2310	279	0.
1	0430	55	8.	*	1	1045	130	0.	*	1	1700	205	0.	*	1	2315	280	0.
1	0435	56	8.	*	1	1050	131	0.	*	1	1705	206	0.	*	1	2320	281	0.
1	0440	57	8.	*	1	1055	132	0.	*	1	1710	207	0.	*	1	2325	282	0.
1	0445	58	8.	*	1	1100	133	0.	*	1	1715	208	0.	*	1	2330	283	0.
1	0450	59	8.	*	1	1105	134	0.	*	1	1720	209	0.	*	1	2335	284	0.
1	0455	60	8.	*	1	1110	135	0.	*	1	1725	210	0.	*	1	2340	285	0.
1	0500	61	8.	*	1	1115	136	0.	*	1	1730	211	0.	*	1	2345	286	0.
1	0505	62	7.	*	1	1120	137	0.	*	1	1735	212	0.	*	1	2350	287	0.
1	0510	63	7.	*	1	1125	138	0.	*	1	1740	213	0.	*	1	2355	288	0.
1	0515	64	7.	*	1	1130	139	0.	*	1	1745	214	0.	*	2	0000	289	0.
1	0520	65	7.	*	1	1135	140	0.	*	1	1750	215	0.	*	2	0005	290	0.
1	0525	66	7.	*	2	1140	141	0.	*	2	1755	216	0.	*	2	0010	291	0.
1	0530	67	6.	*	1	1145	142	0.	*	1	1800	217	0.	*	2	0015	292	0.
1	0535	68	6.	*	1	1150	143	0.	*	1	1805	218	0.	*	2	0020	293	0.
1	0540	69	6.	*	1	1155	144	0.	*	1	1810	219	0.	*	2	0025	294	0.
1	0545	70	6.	*	1	1200	145	0.	*	1	1815	220	0.	*	2	0030	295	0.
1	0550	71	6.	*	1	1205	146	0.	*	1	1820	221	0.	*	2	0035	296	0.
1	0555	72	5.	*	1	1210	147	0.	*	1	1825	222	0.	*	2	0040	297	0.
1	0600	73	5.	*	1	1215	148	0.	*	1	1830	223	0.	*	2	0045	298	0.
1	0605	74	5.	*	1	1220	149	0.	*	1	1835	224	0.	*	2	0050	299	0.
1	0610	75	5.	*	1	1225	150	0.	*	1	1840	225	0.	*	2	0055	300	0.

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24.92-HR
51.	3.33	9.	2.	2.	2.
		(INCHES)	.170	.172	.172
		(AC-FT)	5.	5.	5.

CUMULATIVE AREA = .51 SQ MI

658 KK 33E.1 COMBINE

659 KO OUTPUT CONTROL VARIABLES

IPRNT	1	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

COMBINED DISCHARGE AT ADOT CULVERT 5 AND 6

661 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION 33E.1  
SUM OF 2 HYDROGRAPHS

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
----	-----	------	-----	------	----	-----	------	-----	------	----	-----	------	-----	------



1	0000	1	0.	*	1	0615	76	62	*	1	1730	151	5.	*	1	1845	226	1.
1	0005	2	0.	*	1	0620	77	59.	*	1	1735	152	5.	*	1	1850	227	1.
1	0010	3	0.	*	1	0625	78	56.	*	1	1740	153	5.	*	1	1855	228	1.
1	0015	4	0.	*	1	0630	79	53.	*	1	1745	154	5.	*	1	1900	229	1.
1	0020	5	0.	*	1	0635	80	51.	*	1	1750	155	5.	*	1	1905	230	1.
1	0025	6	1.	*	1	0640	81	48.	*	1	1755	156	5.	*	1	1910	231	1.
1	0030	7	1.	*	1	0645	82	46.	*	1	1800	157	5.	*	1	1915	232	1.
1	0035	8	2.	*	1	0650	83	44.	*	1	1805	158	5.	*	1	1920	233	1.
1	0040	9	3.	*	1	0655	84	42.	*	1	1810	159	4.	*	1	1925	234	1.
1	0045	10	4.	*	1	0700	85	40.	*	1	1815	160	4.	*	1	1930	235	1.
1	0050	11	5.	*	1	0705	86	39.	*	1	1820	161	4.	*	1	1935	236	1.
1	0055	12	6.	*	1	0710	87	37.	*	1	1825	162	4.	*	1	1940	237	1.
1	0100	13	7.	*	1	0715	88	36.	*	1	1830	163	4.	*	1	1945	238	1.
1	0105	14	7.	*	1	0720	89	34.	*	1	1835	164	4.	*	1	1950	239	1.
1	0110	15	8.	*	1	0725	90	33.	*	1	1840	165	4.	*	1	1955	240	1.
1	0115	16	9.	*	1	0730	91	32.	*	1	1845	166	4.	*	1	2000	241	1.
1	0120	17	9.	*	1	0735	92	31.	*	1	1850	167	4.	*	1	2005	242	1.
1	0125	18	10.	*	1	0740	93	30.	*	1	1855	168	4.	*	1	2010	243	1.
1	0130	19	11.	*	1	0745	94	29.	*	1	1900	169	3.	*	1	2015	244	1.
1	0135	20	12.	*	1	0750	95	28.	*	1	1905	170	3.	*	1	2020	245	1.
1	0140	21	12.	*	1	0755	96	27.	*	1	1910	171	3.	*	1	2025	246	1.
1	0145	22	13.	*	1	0800	97	26.	*	1	1915	172	3.	*	1	2030	247	1.
1	0150	23	14.	*	1	0805	98	25.	*	1	1920	173	3.	*	1	2035	248	1.
1	0155	24	15.	*	1	0810	99	24.	*	1	1925	174	3.	*	1	2040	249	1.
1	0200	25	16.	*	1	0815	100	23.	*	1	1930	175	3.	*	1	2045	250	1.
1	0205	26	17.	*	1	0820	101	22.	*	1	1935	176	3.	*	1	2050	251	1.
1	0210	27	18.	*	1	0825	102	22.	*	1	1940	177	3.	*	1	2055	252	1.
1	0215	28	19.	*	1	0830	103	21.	*	1	1945	178	3.	*	1	2100	253	1.
1	0220	29	21.	*	1	0835	104	20.	*	1	1950	179	3.	*	1	2105	254	1.
1	0225	30	22.	*	1	0840	105	20.	*	1	1955	180	3.	*	1	2110	255	1.
1	0230	31	24.	*	1	0845	106	19.	*	1	1959	181	3.	*	1	2115	256	1.
1	0235	32	28.	*	1	0850	107	18.	*	1	1955	182	3.	*	1	2120	257	1.
1	0240	33	37.	*	1	0855	108	18.	*	1	1950	183	2.	*	1	2125	258	0.
1	0245	34	49.	*	1	0900	109	17.	*	1	1955	184	2.	*	1	2130	259	0.
1	0250	35	63.	*	1	0905	110	17.	*	1	1950	185	2.	*	1	2135	260	0.
1	0255	36	83.	*	1	0910	111	16.	*	1	1955	186	2.	*	1	2140	261	0.
1	0300	37	132.	*	1	0915	112	16.	*	1	1950	187	2.	*	1	2145	262	0.
1	0305	38	215.	*	1	0920	113	15.	*	1	1955	188	2.	*	1	2150	263	0.
1	0310	39	245.	*	1	0925	114	15.	*	1	1950	189	2.	*	1	2155	264	0.
1	0315	40	256.	*	1	0930	115	14.	*	1	1955	190	2.	*	1	2200	265	0.
1	0320	41	249.	*	1	0935	116	14.	*	1	1950	191	2.	*	1	2205	266	0.
1	0325	42	240.	*	1	0940	117	14.	*	1	1955	192	2.	*	1	2210	267	0.
1	0330	43	229.	*	1	0945	118	13.	*	1	1950	193	2.	*	1	2215	268	0.
1	0335	44	236.	*	1	0950	119	13.	*	1	1955	194	2.	*	1	2220	269	0.
1	0340	45	200.	*	1	0955	120	12.	*	1	1950	195	2.	*	1	2225	270	0.
1	0345	46	184.	*	1	1000	121	12.	*	1	1955	196	2.	*	1	2230	271	0.
1	0350	47	170.	*	1	1005	122	12.	*	1	1950	197	2.	*	1	2235	272	0.
1	0355	48	159.	*	1	1010	123	11.	*	1	1955	198	2.	*	1	2240	273	0.
1	0400	49	151.	*	1	1015	124	11.	*	1	1950	199	2.	*	1	2245	274	0.
1	0405	50	144.	*	1	1020	125	11.	*	1	1955	200	2.	*	1	2250	275	0.
1	0410	51	138.	*	1	1025	126	10.	*	1	1950	201	2.	*	1	2255	276	0.
1	0415	52	133.	*	1	1030	127	10.	*	1	1955	202	2.	*	1	2300	277	0.
1	0420	53	129.	*	1	1035	128	10.	*	1	1950	203	2.	*	1	2305	278	0.
1	0425	54	125.	*	1	1040	129	10.	*	1	1955	204	2.	*	1	2310	279	0.
1	0430	55	121.	*	1	1045	130	9.	*	1	1950	205	2.	*	1	2315	280	0.
1	0435	56	118.	*	1	1050	131	9.	*	1	1955	206	1.	*	1	2320	281	0.
1	0440	57	116.	*	1	1055	132	9.	*	1	1950	207	1.	*	1	2325	282	0.
1	0445	58	113.	*	1	1100	133	9.	*	1	1955	208	1.	*	1	2330	283	0.
1	0450	59	109.	*	1	1105	134	8.	*	1	1950	209	1.	*	1	2335	284	0.
1	0455	60	106.	*	1	1110	135	8.	*	1	1955	210	1.	*	1	2340	285	0.
1	0500	61	102.	*	1	1115	136	8.	*	1	1950	211	1.	*	1	2345	286	0.
1	0505	62	99.	*	1	1120	137	8.	*	1	1955	212	1.	*	1	2350	287	0.
1	0510	63	96.	*	1	1125	138	8.	*	1	1950	213	1.	*	1	2355	288	0.
1	0515	64	93.	*	1	1130	139	7.	*	1	1955	214	1.	*	2	0000	289	0.
1	0520	65	90.	*	1	1135	140	7.	*	1	1950	215	1.	*	2	0005	290	0.
1	0525	66	87.	*	1	1140	141	7.	*	1	1955	216	1.	*	2	0010	291	0.
1	0530	67	85.	*	1	1145	142	7.	*	1	1950	217	1.	*	2	0015	292	0.
1	0535	68	82.	*	1	1150	143	7.	*	1	1955	218	1.	*	2	0020	293	0.
1	0540	69	80.	*	1	1155	144	6.	*	1	1950	219	1.	*	2	0025	294	0.
1	0545	70	78.	*	1	1200	145	6.	*	1	1955	220	1.	*	2	0030	295	0.
1	0550	71	75.	*	1	1205	146	6.	*	1	1950	221	1.	*	2	0035	296	0.
1	0555	72	73.	*	1	1210	147	6.	*	1	1955	222	1.	*	2	0040	297	0.
1	0600	73	71.	*	1	1215	148	6.	*	1	1950	223	1.	*	2	0045	298	0.
1	0605	74	69.	*	1	1220	149	6.	*	1	1955	224	1.	*	2	0050	299	0.
1	0610	75	66.	*	1	1225	150	6.	*	1	1950	225	1.	*	2	0055	300	0.

PEAK FLOW      TIME  
 +      (CFS)      (HR)  
 4      256.      3.25  
                                  (CFS)  
                                  (INCHES)  
                                  (AC-FT)  
                                  CUMULATIVE AREA = .51 SQ MI

662 KK

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R33E.1

ROUTE

663 RD

## OUTPUT CONTROL VARIABLES

IPRNT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 9. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT .093 TIME INTERVAL IN HOURS

ROUTE ADOT CULVERT 5 AND 6 FLOWS THROUGH ASLD LAND TO  
 UNION HILLS DRIVE (MAYO) AND 73RD PLACE.  
 ROUTE L=1600', TRAP SECTION BW=19' Z=5, T<sub>Wmax</sub>=39'  
 ASSUME GRASS LINED CHANNEL N=.030 UP=1592.5 DWN=1582.66

## HYDROGRAPH ROUTING DATA

669 RK

## KINEMATIC WAVE STREAM ROUTING

L 1600. CHANNEL LENGTH  
 S .0088 SLOPE  
 N .030 CHANNEL, ROUGHNESS COEFFICIENT  
 CA .00 CONTRIBUTING AREA  
 SHAPE TRAP CHANNEL SHAPE  
 WD 19.00 BOTTOM WIDTH OR DIAMETER  
 Z 5.00 SIDE SLOPE  
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS

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COMPUTED KINEMATIC PARAMETERS  
 VARIABLE TIME STEP  
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.98	1.43	1.31	522.33	255.46	197.67	1.92	7.46

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5208E+02 EXCESS= .0000E+00 OUTFLOW= .5208E+02 BASIN STORAGE= .7950E-02 PERCENT ERROR= .0

## INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
MAIN	.98	1.43	5.00		252.31	200.00	1.92	

## HYDROGRAPH AT STATION R33E.1

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	1	0.	1	0615	76	65.	1	1230	151	6.	1	1845	226	1.				
1	0005	2	0.	1	0620	77	62.	1	1235	152	5.	1	1850	227	1.				
1	0010	3	0.	1	0625	78	58.	1	1240	153	5.	1	1855	228	1.				
1	0015	4	0.	1	0630	79	55.	1	1245	154	5.	1	1900	229	1.				
1	0020	5	0.	1	0635	80	53.	1	1250	155	5.	1	1905	230	1.				
1	0025	6	0.	1	0640	81	50.	1	1255	156	5.	1	1910	231	1.				
1	0030	7	0.	1	0645	82	48.	1	1300	157	5.	1	1915	232	1.				
1	0035	8	0.	1	0650	83	46.	1	1305	158	5.	1	1920	233	1.				
1	0040	9	1.	1	0655	84	44.	1	1310	159	5.	1	1925	234	1.				
1	0045	10	2.	1	0700	85	42.	1	1315	160	4.	1	1930	235	1.				
1	0050	11	3.	1	0705	86	40.	1	1320	161	4.	1	1935	236	1.				
1	0055	12	5.	1	0710	87	39.	1	1325	162	4.	1	1940	237	1.				
1	0100	13	6.	1	0715	88	37.	1	1330	163	4.	1	1945	238	1.				
1	0105	14	6.	1	0720	89	36.	1	1335	164	4.	1	1950	239	1.				
1	0110	15	7.	1	0725	90	34.	1	1340	165	4.	1	1955	240	1.				
1	0115	16	8.	1	0730	91	33.	1	1345	166	4.	1	2000	241	1.				
1	0120	17	8.	1	0735	92	32.	1	1350	167	4.	1	2005	242	1.				
1	0125	18	9.	1	0740	93	31.	1	1355	168	4.	1	2010	243	1.				
1	0130	19	10.	1	0745	94	30.	1	1400	169	4.	1	2015	244	1.				
1	0135	20	11.	1	0750	95	29.	1	1405	170	4.	1	2020	245	1.				
1	0140	21	11.	1	0755	96	28.	1	1410	171	3.	1	2025	246	1.				
1	0145	22	12.	1	0800	97	27.	1	1415	172	3.	1	2030	247	1.				
1	0150	23	13.	1	0805	98	26.	1	1420	173	3.	1	2035	248	1.				
1	0155	24	14.	1	0810	99	25.	1	1425	174	3.	1	2040	249	1.				
1	0200	25	15.	1	0815	100	24.	1	1430	175	3.	1	2045	250	1.				
1	0205	26	16.	1	0820	101	23.	1	1435	176	3.	1	2050	251	1.				
1	0210	27	17.	1	0825	102	22.	1	1440	177	3.	1	2055	252	1.				
1	0215	28	18.	1	0830	103	22.	1	1445	178	3.	1	2100	253	1.				
1	0220	29	19.	1	0835	104	21.	1	1450	179	3.	1	2105	254	1.				
1	0225	30	21.	1	0840	105	20.	1	1455	180	3.	1	2110	255	1.				
1	0230	31	22.	1	0845	106	20.	1	1500	181	3.	1	2115	256	1.				
1	0235	32	24.	1	0850	107	19.	1	1505	182	3.	1	2120	257	1.				
1	0240	33	25.	1	0855	108	18.	1	1510	183	3.	1	2125	258	1.				
1	0245	34	30.	1	0900	109	18.	1	1515	184	3.	1	2130	259	1.				
1	0250	35	52.	1	0905	110	17.	1	1520	185	2.	1	2135	260	1.				
1	0255	36	69.	1	0910	111	17.	1	1525	186	2.	1	2140	261	0.				
1	0300	37	101.	1	0915	112	16.	1	1530	187	2.	1	2145	262	0.				
1	0305	38	170.	1	0920	113	16.	1	1535	188	2.	1	2150	263	0.				
1	0310	39	230.	1	0925	114	15.	1	1540	189	2.	1	2155	264	0.				
1	0315	40	251.	1	0930	115	15.	1	1545	190	2.	1	2200	265	0.				
1	0320	41	252.	1	0935	116	14.	1	1550	191	2.	1	2205	266	0.				
1	0325	42	244.	1	0940	117	14.	1	1555	192	2.	1	2210	267	0.				
1	0330	43	234.	1	0945	118	14.	1	1600	193	2.	1	2215	268	0.				
1	0335	44	223.	1	0950	119	13.	1	1605	194	2.	1	2220	269	0.				
1	0340	45	208.	1	0955	120	13.	1	1610	195	2.	1	2225	270	0.				
1	0345	46	192.	1	1000	121	13.	1	1615	196	2.	1	2230	271	0.				

1	0350	47	177.	*	1	1005	123	12.	*	1	1620	197	2.	*	1	2235	272	0.
1	0355	48	165.	*	1	1010	123	12.	*	1	1625	198	2.	*	1	2240	273	0.
1	0400	49	155.	*	1	1015	124	11.	*	1	1630	199	2.	*	1	2245	274	0.
1	0405	50	148.	*	1	1020	125	11.	*	1	1635	200	2.	*	1	2250	275	0.
1	0410	51	141.	*	1	1025	126	11.	*	1	1640	201	2.	*	1	2255	276	0.
1	0415	52	136.	*	1	1030	127	11.	*	1	1645	202	2.	*	1	2300	277	0.
1	0420	53	132.	*	1	1035	128	10.	*	1	1650	203	2.	*	1	2305	278	0.
1	0425	54	127.	*	1	1040	129	10.	*	1	1655	204	2.	*	1	2310	279	0.
1	0430	55	123.	*	1	1045	130	10.	*	1	1700	205	2.	*	1	2315	280	0.
1	0435	56	120.	*	1	1050	131	9.	*	1	1705	206	2.	*	1	2320	281	0.
1	0440	57	117.	*	1	1055	132	9.	*	1	1710	207	2.	*	1	2325	282	0.
1	0445	58	114.	*	1	1100	133	9.	*	1	1715	208	1.	*	1	2330	283	0.
1	0450	59	111.	*	1	1105	134	9.	*	1	1720	209	1.	*	1	2335	284	0.
1	0455	60	108.	*	1	1110	135	8.	*	1	1725	210	1.	*	1	2340	285	0.
1	0500	61	104.	*	1	1115	136	8.	*	1	1730	211	1.	*	1	2345	286	0.
1	0505	62	101.	*	1	1120	137	8.	*	1	1735	212	1.	*	1	2350	287	0.
1	0510	63	98.	*	1	1125	138	8.	*	1	1740	213	1.	*	1	2355	288	0.
1	0515	64	95.	*	1	1130	139	8.	*	1	1745	214	1.	*	2	0000	289	0.
1	0520	65	92.	*	1	1135	140	7.	*	1	1750	215	1.	*	2	0005	290	0.
1	0525	66	89.	*	1	1140	141	7.	*	1	1755	216	1.	*	2	0010	291	0.
1	0530	67	87.	*	1	1145	142	7.	*	1	1800	217	1.	*	2	0015	292	0.
1	0535	68	84.	*	1	1150	143	7.	*	1	1805	218	1.	*	2	0020	293	0.
1	0540	69	82.	*	1	1155	144	7.	*	1	1810	219	1.	*	2	0025	294	0.
1	0545	70	79.	*	1	1200	145	7.	*	1	1815	220	1.	*	2	0030	295	0.
1	0550	71	77.	*	1	1205	146	6.	*	1	1820	221	1.	*	2	0035	296	0.
1	0555	72	75.	*	1	1210	147	6.	*	1	1825	222	1.	*	2	0040	297	0.
1	0600	73	73.	*	1	1215	148	6.	*	1	1830	223	1.	*	2	0045	298	0.
1	0605	74	70.	*	1	1220	149	6.	*	1	1835	224	1.	*	2	0050	299	0.
1	0610	75	68.	*	1	1225	150	6.	*	1	1840	225	1.	*	2	0055	300	0.

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24.92-HR
252.	3.33	91.	26.	25.	25.
		(INCHES)	1.655	1.917	1.917
		(AC-FT)	45.	52.	52.
CUMULATIVE AREA =		.51 SQ MI			

669 KK \*\*\*\*\*  
 ASLDR1 ROUTE  
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670 KQ OUTPUT CONTROL VARIABLES

IPRNT	1	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMEINT	.083	TIME INTERVAL IN HOURS

ROUTE FLOWS FROM CHANNEL THROUGH BOX CULVERT ALONG UNION  
 HILLS DRIVE (MAYO) TO SCOTTSDALE ROAD, SOUTH TO CHAUNCEY.  
 ROUTE L=1830', BOX SECTION W=8' H=3'  
 ASSUME CONCRTE LINED CHANNEL N=.013 UP=1582.55 DWN=1566.32

# HYDROGRAPH ROUTING DATA

675 RK KINEMATIC WAVE STREAM ROUTING

L	1830.	CHANNEL LENGTH
S	.0089	SLOPE
N	.013	CHANNEL ROUGHNESS COEFFICIENT
CA	.00	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	16.00	BOTTOM WIDTH OR DIAMETER
Z	.00	SIDE SLOPE
NDXMIN	2	MINIMUM NUMBER OF DX INTERVALS

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 COMPUTED KINEMATIC PARAMETERS  
 VARIABLE TIME STEP  
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
MAIN	1.70	1.67	.56	610.00	252.12	200.80	1.92	20.96

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5206E+02 EXCESS= .0000E+00 OUTFLOW= .5205E+02 BASIN STORAGE= .8142E-02 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	1.70	1.67	5.00	251.98	200.00	1.92
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HYDROGRAPH AT STATION ASLDR1

DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*
1	0000	1	0.	*	1	0615	76	66.	*	1	1230	151	6.	*	1	1845	226	1.					
1	0005	2	0.	*	1	0620	77	63.	*	1	1235	152	6.	*	1	1850	227	1.					
1	0010	3	0.	*	1	0625	78	59.	*	1	1240	153	5.	*	1	1855	228	1.					
1	0015	4	0.	*	1	0630	79	56.	*	1	1245	154	5.	*	1	1900	229	1.					
1	0020	5	0.	*	1	0635	80	54.	*	1	1250	155	5.	*	1	1905	230	2.					
1	0025	6	0.	*	1	0640	81	51.	*	1	1255	156	5.	*	1	1910	231	1.					
1	0030	7	0.	*	1	0645	82	49.	*	1	1300	157	5.	*	1	1915	232	1.					
1	0035	8	0.	*	1	0650	83	47.	*	1	1305	158	5.	*	1	1920	233	1.					
1	0040	9	0.	*	1	0655	84	45.	*	1	1310	159	5.	*	1	1925	234	1.					
1	0045	10	0.	*	1	0700	85	43.	*	1	1315	160	5.	*	1	1930	235	1.					
1	0050	11	1.	*	1	0705	86	41.	*	1	1320	161	4.	*	1	1935	236	1.					
1	0055	12	3.	*	1	0710	87	39.	*	1	1325	162	4.	*	1	1940	237	1.					
1	0100	13	5.	*	1	0715	88	38.	*	1	1330	163	4.	*	1	1945	238	1.					
1	0105	14	6.	*	1	0720	89	36.	*	1	1335	164	4.	*	1	1950	239	1.					
1	0110	15	6.	*	1	0725	90	35.	*	1	1340	165	4.	*	1	1955	240	1.					
1	0115	16	7.	*	1	0730	91	34.	*	1	1345	166	4.	*	1	2000	241	1.					
1	0120	17	8.	*	1	0735	92	32.	*	1	1350	167	4.	*	1	2005	242	1.					
1	0125	18	9.	*	1	0740	93	31.	*	1	1355	168	4.	*	1	2010	243	1.					
1	0130	19	9.	*	1	0745	94	30.	*	1	1400	169	4.	*	1	2015	244	1.					
1	0135	20	10.	*	1	0750	95	29.	*	1	1405	170	4.	*	1	2020	245	1.					
1	0140	21	11.	*	1	0755	96	28.	*	1	1410	171	4.	*	1	2025	246	1.					
1	0145	22	12.	*	1	0800	97	27.	*	1	1415	172	3.	*	1	2030	247	1.					
1	0150	23	12.	*	1	0805	98	26.	*	1	1420	173	3.	*	1	2035	248	1.					
1	0155	24	13.	*	1	0810	99	25.	*	1	1425	174	3.	*	1	2040	249	1.					
1	0200	25	14.	*	1	0815	100	24.	*	1	1430	175	3.	*	1	2045	250	1.					
1	0205	26	15.	*	1	0820	101	24.	*	1	1435	176	3.	*	1	2050	251	1.					
1	0210	27	16.	*	1	0825	102	23.	*	1	1440	177	3.	*	1	2055	252	1.					
1	0215	28	17.	*	1	0830	103	22.	*	1	1445	178	3.	*	1	2100	253	1.					
1	0220	29	19.	*	1	0835	104	21.	*	1	1450	179	3.	*	1	2105	254	1.					
1	0225	30	20.	*	1	0840	105	21.	*	1	1455	180	3.	*	1	2110	255	1.					
1	0230	31	21.	*	1	0845	106	20.	*	1	1500	181	3.	*	1	2115	256	1.					
1	0235	32	23.	*	1	0850	107	19.	*	1	1505	182	3.	*	1	2120	257	1.					
1	0240	33	27.	*	1	0855	108	19.	*	1	1510	183	3.	*	1	2125	258	1.					
1	0245	34	35.	*	1	0900	109	18.	*	1	1515	184	3.	*	1	2130	259	1.					
1	0250	35	47.	*	1	0905	110	18.	*	1	1520	185	3.	*	1	2135	260	1.					
1	0255	36	63.	*	1	0910	111	17.	*	1	1525	186	3.	*	1	2140	261	1.					
1	0300	37	92.	*	1	0915	112	17.	*	1	1530	187	2.	*	1	2145	262	1.					
1	0305	38	154.	*	1	0920	113	16.	*	1	1535	188	2.	*	1	2150	263	0.					
1	0310	39	210.	*	1	0925	114	16.	*	1	1540	189	2.	*	1	2155	264	0.					
1	0315	40	247.	*	1	0930	115	15.	*	1	1545	190	2.	*	1	2200	265	0.					
1	0320	41	252.	*	1	0935	116	15.	*	1	1550	191	2.	*	1	2205	266	0.					
1	0325	42	246.	*	1	0940	117	14.	*	1	1555	192	2.	*	1	2210	267	0.					
1	0330	43	236.	*	1	0945	118	14.	*	1	1600	193	2.	*	1	2215	268	0.					
1	0335	44	225.	*	1	0950	119	14.	*	1	1605	194	2.	*	1	2220	269	0.					
1	0340	45	211.	*	1	0955	120	13.	*	1	1610	195	2.	*	1	2225	270	0.					
1	0345	46	196.	*	1	1000	121	13.	*	1	1615	196	2.	*	1	2230	271	0.					
1	0350	47	180.	*	1	1005	122	12.	*	1	1620	197	2.	*	1	2235	272	0.					
1	0355	48	168.	*	1	1010	123	12.	*	1	1625	198	2.	*	1	2240	273	0.					
1	0400	49	150.	*	1	1015	124	12.	*	1	1630	199	2.	*	1	2245	274	0.					
1	0405	50	150.	*	1	1020	125	11.	*	1	1635	200	2.	*	1	2250	275	0.					
1	0410	51	143.	*	1	1025	126	11.	*	1	1640	201	2.	*	1	2255	276	0.					
1	0415	52	137.	*	1	1030	127	11.	*	1	1645	202	2.	*	1	2300	277	0.					
1	0420	53	133.	*	1	1035	128	10.	*	1	1650	203	2.	*	1	2305	278	0.					
1	0425	54	128.	*	1	1040	129	10.	*	1	1655	204	2.	*	1	2310	279	0.					
1	0430	55	124.	*	1	1045	130	10.	*	1	1700	205	2.	*	1	2315	280	0.					
1	0435	56	121.	*	1	1050	131	10.	*	1	1705	206	2.	*	1	2320	281	0.					
1	0440	57	118.	*	1	1055	132	9.	*	1	1710	207	2.	*	1	2325	282	0.					
1	0445	58	115.	*	1	1100	133	9.	*	1	1715	208	2.	*	1	2330	283	0.					
1	0450	59	112.	*	1	1105	134	9.	*	1	1720	209	2.	*	1	2335	284	0.					
1	0455	60	109.	*	1	1110	135	9.	*	1	1725	210	1.	*	1	2340	285	0.					
1	0500	61	105.	*	1	1115	136	8.	*	1	1730	211	1.	*	1	2345	286	0.					
1	0505	62	102.	*	1	1120	137	8.	*	1	1735	212	1.	*	1	2350	287	0.					
1	0510	63	99.	*	1	1125	138	8.	*	1	1740	213	1.	*	1	2355	288	0.					
1	0515	64	96.	*	1	1130	139	8.	*	1	1745	214	1.	*	2	0000	289	0.					
1	0520	65	93.	*	1	1135	140	8.	*	1	1750	215	1.	*	2	0005	290	0.					
1	0525	66	90.	*	1	1140	141	7.	*	1	1755	216	1.	*	2	0010	291	0.					
1	0530	67	87.	*	1	1145	142	7.	*	1	1800	217	1.	*	2	0015	292	0.					
1	0535	68	85.	*	1	1150	143	7.	*	1	1805	218	1.	*	2	0020	293	0.					
1	0540	69	82.	*	1	1155	144	7.	*	1	1810	219	1.	*	2	0025	294	0.					
1	0545	70	80.	*	1	1200	145	7.	*	1	1815	220	1.	*	2	0030	295	0.					
1	0550	71	78.	*	1	1205	146	6.	*	1	1820	221	1.	*	2	0035	296	0.					
1	0555	72	75.	*	1	1210	147	6.	*	1	1825	222	1.	*	2	0040	297	0.					
1	0600	73	73.	*	1	1215	148	6.	*	1	1830	223	1.	*	2	0045	298	0.					
1	0605	74	71.	*	1	1220	149	6.	*	1	1835	224	1.	*	2	0050	299	0.					
1	0610	75	69.	*	1	1225	150	6.	*	1	1840	225	1.	*	2	0055	300	0.					

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24-92-HR
(CFS)	(HR)						
252.	3.33	(CFS)	91.	26.	25.	25.	
		(INCHES)	1.056	1.917	1.917	1.917	
		(AC-FT)	45.	52.	52.	52.	

CUMULATIVE AREA = .51 SQ MI

\*\*\*\*\*  
 676 KK \* ASLD \* 1 SUR  
 \*\*\*\*\*

677 KO OUTPUT CONTROL VARIABLES  
 IPRNT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 IPNCH 0 PUNCH COMPUTED HYDROGRAPH  
 IOUT 21 SAVE HYDROGRAPH ON THIS UNIT  
 ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT .093 TIME INTERVAL IN HOURS

ASLD NORTH PARCEL EAST OF SCOTTSDALE ROAD AND NORTH OF CHAUNCEY LANE

SUBBASIN RUNOFF DATA

679 BA SUBBASIN CHARACTERISTICS  
 TAREA .03 SUBBASIN AREA

PRECIPITATION DATA

24 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM  
 ..... HYDRO-35 ..... TP-40 .....  
 5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 2-DAY 4-DAY 7-DAY 10-DAY  
 .76 1.50 2.54 2.81 2.99 3.33 .00 .00 .00 .00 .00 .00

STORM AREA = 14.00

680 LS SCS LOSS RATE  
 SRTTL .60 INITIAL ABSTRACTION  
 CRVNR 77.00 CURVE NUMBER  
 RTIMP 83.00 PERCENT IMPERVIOUS AREA

KINEMATIC WAVE  
 691 UK OVERLAND-FLOW ELEMENT NO. 1  
 L 345. OVERLAND FLOW LENGTH  
 S .0010 SLOPE  
 N .015 ROUGHNESS COEFFICIENT  
 PA 100.0 PERCENT OF SUBBASIN  
 DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

KINEMATIC WAVE  
 682 RK MAIN CHANNEL  
 L 1400. CHANNEL LENGTH  
 S .0131 SLOPE  
 N .015 CHANNEL ROUGHNESS COEFFICIENT  
 CA .03 CONTRIBUTING AREA  
 SHAPE TRAP CHANNEL SHAPE  
 WD 17.00 BOTTOM WIDTH OR DIAMETER  
 Z 4.00 SIDE SLOPE  
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS  
 RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

\*\*\*  
 COMPUTED KINEMATIC PARAMETERS  
 VARIABLE TIME STEP  
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FES)
PLANE1	3.14	1.67	1.19	69.00	128.15	185.47	2.88	1.06
MAIN	2.48	1.44	.64	466.67	123.54	186.54	2.89	12.81

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4844E+01 OUTFLOW= .4845E+01 BASIN STORAGE= .3741E-03 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
MAIN	2.48	1.44	5.00		114.18	185.00	2.89	

HYDROGRAPH AT STATION ASLD

DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	.00	.00	.00	0.	*	1	1230	151	.00	.00	.00	0.	
1	0005	2	.01	.00	.01	0.	*	1	1235	152	.00	.00	.00	0.	
1	0010	3	.01	.00	.01	0.	*	1	1240	153	.00	.00	.00	0.	
1	0015	4	.01	.00	.01	0.	*	1	1245	154	.00	.00	.00	0.	
1	0020	5	.01	.00	.01	0.	*	1	1250	155	.00	.00	.00	0.	
1	0025	6	.01	.00	.01	0.	*	1	1255	156	.00	.00	.00	0.	
1	0030	7	.01	.00	.01	0.	*	1	1300	157	.00	.00	.00	0.	
1	0035	8	.01	.00	.01	1.	*	1	1305	158	.00	.00	.00	0.	
1	0040	9	.01	.00	.01	1.	*	1	1310	159	.00	.00	.00	0.	
1	0045	10	.01	.00	.01	1.	*	1	1315	160	.00	.00	.00	0.	
1	0050	11	.01	.00	.01	1.	*	1	1320	161	.00	.00	.00	0.	
1	0055	12	.01	.00	.01	2.	*	1	1325	162	.00	.00	.00	0.	
1	0100	13	.01	.00	.01	2.	*	1	1330	163	.00	.00	.00	0.	
1	0105	14	.01	.00	.01	2.	*	1	1335	164	.00	.00	.00	0.	

1	0110	15	.01	.00	.01	2.	*	1	1340	165	.00	.00	.00	0.
1	0115	16	.01	.00	.01	2.	*	1	1345	166	.00	.00	.00	0.
1	0120	17	.01	.00	.01	2.	*	1	1350	167	.00	.00	.00	0.
1	0125	18	.01	.00	.01	2.	*	1	1355	168	.00	.00	.00	0.
1	0130	19	.01	.00	.01	2.	*	1	1400	169	.00	.00	.00	0.
1	0135	20	.01	.00	.01	2.	*	1	1405	170	.00	.00	.00	0.
1	0140	21	.01	.00	.01	2.	*	1	1410	171	.00	.00	.00	0.
1	0145	22	.02	.00	.01	3.	*	1	1415	172	.00	.00	.00	0.
1	0150	23	.02	.00	.01	3.	*	1	1420	173	.00	.00	.00	0.
1	0155	24	.02	.00	.01	3.	*	1	1425	174	.00	.00	.00	0.
1	0200	25	.02	.00	.02	3.	*	1	1430	175	.00	.00	.00	0.
1	0205	26	.02	.00	.02	3.	*	1	1435	176	.00	.00	.00	0.
1	0210	27	.02	.00	.02	3.	*	1	1440	177	.00	.00	.00	0.
1	0215	28	.02	.00	.02	4.	*	1	1445	178	.00	.00	.00	0.
1	0220	29	.02	.00	.02	4.	*	1	1450	179	.00	.00	.00	0.
1	0225	30	.03	.00	.02	4.	*	1	1455	180	.00	.00	.00	0.
1	0230	31	.03	.01	.03	5.	*	1	1500	181	.00	.00	.00	0.
1	0235	32	.08	.01	.06	6.	*	1	1505	182	.00	.00	.00	0.
1	0240	33	.09	.01	.07	10.	*	1	1510	183	.00	.00	.00	0.
1	0245	34	.10	.02	.08	14.	*	1	1515	184	.00	.00	.00	0.
1	0250	35	.14	.02	.11	19.	*	1	1520	185	.00	.00	.00	0.
1	0255	36	.18	.02	.15	27.	*	1	1525	186	.00	.00	.00	0.
1	0300	37	.40	.05	.35	52.	*	1	1530	187	.00	.00	.00	0.
1	0305	38	.69	.06	.63	114.	*	1	1535	188	.00	.00	.00	0.
1	0310	39	.28	.02	.26	99.	*	1	1540	189	.00	.00	.00	0.
1	0315	40	.15	.01	.14	59.	*	1	1545	190	.00	.00	.00	0.
1	0320	41	.11	.01	.10	39.	*	1	1550	191	.00	.00	.00	0.
1	0325	42	.09	.01	.09	29.	*	1	1555	192	.00	.00	.00	0.
1	0330	43	.08	.00	.08	23.	*	1	1600	193	.00	.00	.00	0.
1	0335	44	.03	.00	.03	16.	*	1	1605	194	.00	.00	.00	0.
1	0340	45	.03	.00	.03	13.	*	1	1610	195	.00	.00	.00	0.
1	0345	46	.03	.00	.02	10.	*	1	1615	196	.00	.00	.00	0.
1	0350	47	.02	.00	.02	8.	*	1	1620	197	.00	.00	.00	0.
1	0355	48	.02	.00	.02	7.	*	1	1625	198	.00	.00	.00	0.
1	0400	49	.02	.00	.02	6.	*	1	1630	199	.00	.00	.00	0.
1	0405	50	.02	.00	.02	6.	*	1	1635	200	.00	.00	.00	0.
1	0410	51	.02	.00	.02	5.	*	1	1640	201	.00	.00	.00	0.
1	0415	52	.02	.00	.02	5.	*	1	1645	202	.00	.00	.00	0.
1	0420	53	.02	.00	.01	4.	*	1	1650	203	.00	.00	.00	0.
1	0425	54	.02	.00	.01	4.	*	1	1655	204	.00	.00	.00	0.
1	0430	55	.01	.00	.01	4.	*	1	1700	205	.00	.00	.00	0.
1	0435	56	.01	.00	.01	4.	*	1	1705	206	.00	.00	.00	0.
1	0440	57	.01	.00	.01	4.	*	1	1710	207	.00	.00	.00	0.
1	0445	58	.01	.00	.01	3.	*	1	1715	208	.00	.00	.00	0.
1	0450	59	.01	.00	.01	3.	*	1	1720	209	.00	.00	.00	0.
1	0455	60	.01	.00	.01	3.	*	1	1725	210	.00	.00	.00	0.
1	0500	61	.01	.00	.01	2.	*	1	1730	211	.00	.00	.00	0.
1	0505	62	.01	.00	.01	3.	*	1	1735	212	.00	.00	.00	0.
1	0510	63	.01	.00	.01	3.	*	1	1740	213	.00	.00	.00	0.
1	0515	64	.01	.00	.01	3.	*	1	1745	214	.00	.00	.00	0.
1	0520	65	.01	.00	.01	3.	*	1	1750	215	.00	.00	.00	0.
1	0525	66	.01	.00	.01	2.	*	1	1755	216	.00	.00	.00	0.
1	0530	67	.01	.00	.01	2.	*	1	1800	217	.00	.00	.00	0.
1	0535	68	.01	.00	.01	2.	*	1	1805	218	.00	.00	.00	0.
1	0540	69	.01	.00	.01	2.	*	1	1810	219	.00	.00	.00	0.
1	0545	70	.01	.00	.01	2.	*	1	1815	220	.00	.00	.00	0.
1	0550	71	.01	.00	.01	2.	*	1	1820	221	.00	.00	.00	0.
1	0555	72	.01	.00	.01	2.	*	1	1825	222	.00	.00	.00	0.
1	0600	73	.01	.00	.01	2.	*	1	1830	223	.00	.00	.00	0.
1	0605	74	.00	.00	.00	2.	*	1	1835	224	.00	.00	.00	0.
1	0610	75	.00	.00	.00	2.	*	1	1840	225	.00	.00	.00	0.
1	0615	76	.00	.00	.00	1.	*	1	1845	226	.00	.00	.00	0.
1	0620	77	.00	.00	.00	1.	*	1	1850	227	.00	.00	.00	0.
1	0625	78	.00	.00	.00	1.	*	1	1855	228	.00	.00	.00	0.
1	0630	79	.00	.00	.00	1.	*	1	1900	229	.00	.00	.00	0.
1	0635	80	.00	.00	.00	1.	*	1	1905	230	.00	.00	.00	0.
1	0640	81	.00	.00	.00	1.	*	1	1910	231	.00	.00	.00	0.
1	0645	82	.00	.00	.00	0.	*	1	1915	232	.00	.00	.00	0.
1	0650	83	.00	.00	.00	0.	*	1	1920	233	.00	.00	.00	0.
1	0655	84	.00	.00	.00	0.	*	1	1925	234	.00	.00	.00	0.
1	0700	85	.00	.00	.00	0.	*	1	1930	235	.00	.00	.00	0.
1	0705	86	.00	.00	.00	0.	*	1	1935	236	.00	.00	.00	0.
1	0710	87	.00	.00	.00	0.	*	1	1940	237	.00	.00	.00	0.
1	0715	88	.00	.00	.00	0.	*	1	1945	238	.00	.00	.00	0.
1	0720	89	.00	.00	.00	0.	*	1	1950	239	.00	.00	.00	0.
1	0725	90	.00	.00	.00	0.	*	1	1955	240	.00	.00	.00	0.
1	0730	91	.00	.00	.00	0.	*	1	2000	241	.00	.00	.00	0.
1	0735	92	.00	.00	.00	0.	*	1	2005	242	.00	.00	.00	0.
1	0740	93	.00	.00	.00	0.	*	1	2010	243	.00	.00	.00	0.
1	0745	94	.00	.00	.00	0.	*	1	2015	244	.00	.00	.00	0.
1	0750	95	.00	.00	.00	0.	*	1	2020	245	.00	.00	.00	0.
1	0755	96	.00	.00	.00	0.	*	1	2025	246	.00	.00	.00	0.
1	0800	97	.00	.00	.00	0.	*	1	2030	247	.00	.00	.00	0.
1	0805	98	.00	.00	.00	0.	*	1	2035	248	.00	.00	.00	0.
1	0810	99	.00	.00	.00	0.	*	1	2040	249	.00	.00	.00	0.
1	0815	100	.00	.00	.00	0.	*	1	2045	250	.00	.00	.00	0.
1	0820	101	.00	.00	.00	0.	*	1	2050	251	.00	.00	.00	0.
1	0825	102	.00	.00	.00	0.	*	1	2055	252	.00	.00	.00	0.
1	0830	103	.00	.00	.00	0.	*	1	2100	253	.00	.00	.00	0.
1	0835	104	.00	.00	.00	0.	*	1	2105	254	.00	.00	.00	0.
1	0840	105	.00	.00	.00	0.	*	1	2110	255	.00	.00	.00	0.
1	0845	106	.00	.00	.00	0.	*	1	2115	256	.00	.00	.00	0.
1	0850	107	.00	.00	.00	0.	*	1	2120	257	.00	.00	.00	0.
1	0855	108	.00	.00	.00	0.	*	1	2125	258	.00	.00	.00	0.
1	0900	109	.00	.00	.00	0.	*	1	2130	259	.00	.00	.00	0.
1	0905	110	.00	.00	.00	0.	*	1	2135	260	.00	.00	.00	0.
1	0910	111	.00	.00	.00	0.	*	1	2140	261	.00	.00	.00	0.
1	0915	112	.00	.00	.00	0.	*	1	2145	262	.00	.00	.00	0.
1	0920	113	.00	.00	.00	0.	*	1	2150	263	.00	.00	.00	0.
1	0925	114	.00	.00	.00	0.	*	1	2155	264	.00	.00	.00	0.
1	0930	115	.00	.00	.00	0.	*	1	2200	265	.00	.00	.00	0.

1	0935	116	.00	.00	.00	0.	*	1	2205	266	.00	.00	.00	0.
1	0940	117	.00	.00	.00	0.	*	1	2210	267	.00	.00	.00	0.
1	0945	118	.00	.00	.00	0.	*	1	2215	268	.00	.00	.00	0.
1	0950	119	.00	.00	.00	0.	*	1	2220	269	.00	.00	.00	0.
1	0955	120	.00	.00	.00	0.	*	1	2225	270	.00	.00	.00	0.
1	1000	121	.00	.00	.00	0.	*	1	2230	271	.00	.00	.00	0.
1	1005	122	.00	.00	.00	0.	*	1	2235	272	.00	.00	.00	0.
1	1010	123	.00	.00	.00	0.	*	1	2240	273	.00	.00	.00	0.
1	1015	124	.00	.00	.00	0.	*	1	2245	274	.00	.00	.00	0.
1	1020	125	.00	.00	.00	0.	*	1	2250	275	.00	.00	.00	0.
1	1025	126	.00	.00	.00	0.	*	1	2255	276	.00	.00	.00	0.
1	1030	127	.00	.00	.00	0.	*	1	2300	277	.00	.00	.00	0.
1	1035	128	.00	.00	.00	0.	*	1	2305	278	.00	.00	.00	0.
1	1040	129	.00	.00	.00	0.	*	1	2310	279	.00	.00	.00	0.
1	1045	130	.00	.00	.00	0.	*	1	2315	280	.00	.00	.00	0.
1	1050	131	.00	.00	.00	0.	*	1	2320	281	.00	.00	.00	0.
1	1055	132	.00	.00	.00	0.	*	1	2325	282	.00	.00	.00	0.
1	1100	133	.00	.00	.00	0.	*	1	2330	283	.00	.00	.00	0.
1	1105	134	.00	.00	.00	0.	*	1	2335	284	.00	.00	.00	0.
1	1110	135	.00	.00	.00	0.	*	1	2340	285	.00	.00	.00	0.
1	1115	136	.00	.00	.00	0.	*	1	2345	286	.00	.00	.00	0.
1	1120	137	.00	.00	.00	0.	*	1	2350	287	.00	.00	.00	0.
1	1125	138	.00	.00	.00	0.	*	1	2355	288	.00	.00	.00	0.
1	1130	139	.00	.00	.00	0.	*	2	0000	289	.00	.00	.00	0.
1	1135	140	.00	.00	.00	0.	*	2	0005	290	.00	.00	.00	0.
1	1140	141	.00	.00	.00	0.	*	2	0010	291	.00	.00	.00	0.
1	1145	142	.00	.00	.00	0.	*	2	0015	292	.00	.00	.00	0.
1	1150	143	.00	.00	.00	0.	*	2	0020	293	.00	.00	.00	0.
1	1155	144	.00	.00	.00	0.	*	2	0025	294	.00	.00	.00	0.
1	1200	145	.00	.00	.00	0.	*	2	0030	295	.00	.00	.00	0.
1	1205	146	.00	.00	.00	0.	*	2	0035	296	.00	.00	.00	0.
1	1210	147	.00	.00	.00	0.	*	2	0040	297	.00	.00	.00	0.
1	1215	148	.00	.00	.00	0.	*	2	0045	298	.00	.00	.00	0.
1	1220	149	.00	.00	.00	0.	*	2	0050	299	.00	.00	.00	0.
1	1225	150	.00	.00	.00	0.	*	2	0055	300	.00	.00	.00	0.

TOTAL RAINFALL = 3.22, TOTAL LOSS = .34, TOTAL EXCESS = 2.88

PEAK FLOW	TIME		6-HR	MAXIMUM AVERAGE FLOW	24-HR	72-HR	24.92-HR
(CFS)	(HR)	(CFS)					
114.	3.08		10.	2.	2.	2.	
		(INCHES)	2.860	2.888	2.888	2.888	
		(AC-FT)	5.	5.	5.	5.	

CUMULATIVE AREA = .03 SQ MI

683 KK ASLDC T COMBINE

684 KO OUTPUT CONTROL VARIABLES

IPRNT	1	PRINT CONTROL
IPLST	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	300	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

COMBINED DISCHARGE AT ASLDR1 AND ASLD1 SUB BASIN

686 HC HYDROGRAPH COMBINATION

ICOMP	2	NUMBER OF HYDROGRAPHS TO COMBINE
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HYDROGRAPH AT STATION ASLDC  
SUM OF 2 HYDROGRAPHS

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	1	0.	*	1	0615	76	67.	*	1	1230	151	6.	*	1	1845	226	1.	
1	0005	2	0.	*	1	0620	77	64.	*	1	1235	152	6.	*	1	1850	227	1.	
1	0010	3	0.	*	1	0625	78	60.	*	1	1240	153	5.	*	1	1855	228	1.	
1	0015	4	0.	*	1	0630	79	57.	*	1	1245	154	5.	*	1	1900	229	1.	
1	0020	5	0.	*	1	0635	80	54.	*	1	1250	155	5.	*	1	1905	230	1.	
1	0025	6	0.	*	1	0640	81	52.	*	1	1255	156	5.	*	1	1910	231	1.	
1	0030	7	0.	*	1	0645	82	49.	*	1	1300	157	5.	*	1	1915	232	1.	
1	0035	8	1.	*	1	0650	83	47.	*	1	1305	158	5.	*	1	1920	233	1.	
1	0040	9	1.	*	1	0655	84	45.	*	1	1310	159	5.	*	1	1925	234	1.	
1	0045	10	1.	*	1	0700	85	43.	*	1	1315	160	5.	*	1	1930	235	1.	
1	0050	11	2.	*	1	0705	86	41.	*	1	1320	161	4.	*	1	1935	236	1.	
1	0055	12	5.	*	1	0710	87	39.	*	1	1325	162	4.	*	1	1940	237	1.	
1	0100	13	6.	*	1	0715	88	38.	*	1	1330	163	4.	*	1	1945	238	1.	

1	0105	14	7.	*	1	0720	89	36.	*	1	1335	164	4.	*	1	1950	239	1.
1	0110	15	8.	*	1	0725	90	35.	*	1	1340	165	4.	*	1	1955	240	1.
1	0115	16	9.	*	1	0730	91	34.	*	1	1345	166	4.	*	1	2000	241	1.
1	0120	17	10.	*	1	0735	92	32.	*	1	1350	167	4.	*	1	2005	242	1.
1	0125	18	11.	*	1	0740	93	31.	*	1	1355	168	4.	*	1	2010	243	1.
1	0130	19	12.	*	1	0745	94	30.	*	1	1400	169	4.	*	1	2015	244	1.
1	0135	20	13.	*	1	0750	95	29.	*	1	1405	170	4.	*	1	2020	245	1.
1	0140	21	13.	*	1	0755	96	28.	*	1	1410	171	4.	*	1	2025	246	1.
1	0145	22	14.	*	1	0800	97	27.	*	1	1415	172	3.	*	1	2030	247	1.
1	0150	23	15.	*	1	0805	98	26.	*	1	1420	173	3.	*	1	2035	248	1.
1	0155	24	16.	*	1	0810	99	25.	*	1	1425	174	3.	*	1	2040	249	1.
1	0200	25	17.	*	1	0815	100	24.	*	1	1430	175	3.	*	1	2045	250	1.
1	0205	26	18.	*	1	0820	101	24.	*	1	1435	176	3.	*	1	2050	251	1.
1	0210	27	20.	*	1	0825	102	23.	*	1	1440	177	3.	*	1	2055	252	1.
1	0215	28	21.	*	1	0830	103	22.	*	1	1445	178	3.	*	1	2100	253	1.
1	0220	29	23.	*	1	0835	104	21.	*	1	1450	179	3.	*	1	2105	254	1.
1	0225	30	24.	*	1	0840	105	21.	*	1	1455	180	3.	*	1	2110	255	1.
1	0230	31	26.	*	1	0845	106	20.	*	1	1500	181	3.	*	1	2115	256	1.
1	0235	32	30.	*	1	0850	107	19.	*	1	1505	182	3.	*	1	2120	257	1.
1	0240	33	37.	*	1	0855	108	19.	*	1	1510	183	3.	*	1	2125	258	1.
1	0245	34	49.	*	1	0900	109	18.	*	1	1515	184	3.	*	1	2130	259	1.
1	0250	35	67.	*	1	0905	110	18.	*	1	1520	185	3.	*	1	2135	260	1.
1	0255	36	91.	*	1	0910	111	17.	*	1	1525	186	3.	*	1	2140	261	1.
1	0300	37	144.	*	1	0915	112	17.	*	1	1530	187	2.	*	1	2145	262	1.
1	0305	38	268.	*	1	0920	113	16.	*	1	1535	188	2.	*	1	2150	263	0.
1	0310	39	317.	*	1	0925	114	16.	*	1	1540	189	2.	*	1	2155	264	0.
1	0315	40	305.	*	1	0930	115	15.	*	1	1545	190	2.	*	1	2200	265	0.
1	0320	41	291.	*	1	0935	116	15.	*	1	1550	191	2.	*	1	2205	266	0.
1	0325	42	275.	*	1	0940	117	14.	*	1	1555	192	2.	*	1	2210	267	0.
1	0330	43	260.	*	1	0945	118	14.	*	1	1600	193	2.	*	1	2215	268	0.
1	0335	44	243.	*	1	0950	119	14.	*	1	1605	194	2.	*	1	2220	269	0.
1	0340	45	225.	*	1	0955	120	13.	*	1	1610	195	2.	*	1	2225	270	0.
1	0345	46	206.	*	1	1000	121	13.	*	1	1615	196	2.	*	1	2230	271	0.
1	0350	47	189.	*	1	1005	122	12.	*	1	1620	197	2.	*	1	2235	272	0.
1	0355	48	175.	*	1	1010	123	12.	*	1	1625	198	2.	*	1	2240	273	0.
1	0400	49	164.	*	1	1015	124	12.	*	1	1630	199	2.	*	1	2245	274	0.
1	0405	50	155.	*	1	1020	125	11.	*	1	1635	200	2.	*	1	2250	275	0.
1	0410	51	148.	*	1	1025	126	11.	*	1	1640	201	2.	*	1	2255	276	0.
1	0415	52	142.	*	1	1030	127	11.	*	1	1645	202	2.	*	1	2300	277	0.
1	0420	53	137.	*	1	1035	128	10.	*	1	1650	203	2.	*	1	2305	278	0.
1	0425	54	133.	*	1	1040	129	10.	*	1	1655	204	2.	*	1	2310	279	0.
1	0430	55	128.	*	1	1045	130	10.	*	1	1700	205	2.	*	1	2315	280	0.
1	0435	56	125.	*	1	1050	131	10.	*	1	1705	206	2.	*	1	2320	281	0.
1	0440	57	122.	*	1	1055	132	9.	*	1	1710	207	2.	*	1	2325	282	0.
1	0445	58	119.	*	1	1100	133	9.	*	1	1715	208	2.	*	1	2330	283	0.
1	0450	59	115.	*	1	1105	134	9.	*	1	1720	209	2.	*	1	2335	284	0.
1	0455	60	112.	*	1	1110	135	9.	*	1	1725	210	1.	*	1	2340	285	0.
1	0500	61	108.	*	1	1115	136	8.	*	1	1730	211	1.	*	1	2345	286	0.
1	0505	62	105.	*	1	1120	137	8.	*	1	1735	212	1.	*	1	2350	287	0.
1	0510	63	102.	*	1	1125	138	8.	*	1	1740	213	1.	*	1	2355	288	0.
1	0515	64	98.	*	1	1130	139	8.	*	1	1745	214	1.	*	2	0000	289	0.
1	0520	65	95.	*	1	1135	140	8.	*	1	1750	215	1.	*	2	0005	290	0.
1	0525	66	93.	*	1	1140	141	7.	*	1	1755	216	1.	*	2	0010	291	0.
1	0530	67	90.	*	1	1145	142	7.	*	1	1800	217	1.	*	2	0015	292	0.
1	0535	68	87.	*	1	1150	143	7.	*	1	1805	218	1.	*	2	0020	293	0.
1	0540	69	85.	*	1	1155	144	7.	*	1	1810	219	1.	*	2	0025	294	0.
1	0545	70	82.	*	1	1200	145	7.	*	1	1815	220	1.	*	2	0030	295	0.
1	0550	71	80.	*	1	1205	146	6.	*	1	1820	221	1.	*	2	0035	296	0.
1	0555	72	77.	*	1	1210	147	6.	*	1	1825	222	1.	*	2	0040	297	0.
1	0600	73	75.	*	1	1215	148	6.	*	1	1830	223	1.	*	2	0045	298	0.
1	0605	74	73.	*	1	1220	149	6.	*	1	1835	224	1.	*	2	0050	299	0.
1	0610	75	70.	*	1	1225	150	6.	*	1	1840	225	1.	*	2	0055	300	0.

PEAK FLOW      TIME  
 (CFS)          (HR)  
 317.          3.17  
 (INCHES)      1.714  
 (AC-FT)        49.

MAXIMUM AVERAGE FLOW  
 6-HR      24-HR      72-HR      24.92-HR  
 100.      29.      28.      29.  
 1.973      1.974      1.974  
 49.      57.      57.      57.

CUMULATIVE AREA = .54 SQ MI

687 KK      \*\*\*\*\*  
              \* ASLDR2 \*      ROUTE  
              \*               \*  
              \*\*\*\*\*

688 KO      OUTPUT CONTROL VARIABLES  
              IPRINT      1      PRINT CONTROL  
              IPLOT      0      PLOT CONTROL  
              QSCAL      0.      HYDROGRAPH PLOT SCALE  
              IPUNCH      0      PUNCH COMPUTED HYDROGRAPH  
              IGOUT      21      SAVE HYDROGRAPH ON THIS UNIT  
              ISAV1      1      FIRST ORDINATE PUNCHED OR SAVED  
              ISAV2      300      LAST ORDINATE PUNCHED OR SAVED  
              TIMINT      .083      TIME INTERVAL IN HOURS

ROUTE ASLDR1 AND ASLDR2 SUB TO SCOTTSDALE ROAD  
 AND PRINCESS DRIVE  
 ROUTE 1-1000', TRAP SECTION BW=17' Z=4, TWmax=41'  
 ASSUME GRASS LINED CHANNEL N=.030 UP=1570.15 DWN=1540.60



## HYDROGRAPH ROUTING DATA

693 RE KINEMATIC WAVE STREAM ROUTING  
 L 1000. CHANNEL LENGTH  
 S .0075 SLOPE  
 N .030 CHANNEL ROUGHNESS COEFFICIENT  
 CA .00 CONTRIBUTING AREA  
 SHAPE TRAP CHANNEL SHAPE  
 WD 17.00 BOTTOM WIDTH OR DIAMETER  
 Z 4.00 SIDE SLOPE  
 NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS

\*\*\*  
 COMPUTED KINEMATIC PARAMETERS  
 VARIABLE TIME STEP  
 (DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELEBRITY (FPS)
MAIN	.94	1.44	.72	333.33	316.25	191.53	1.97	7.98

CONTINUITY SUMMARY (AC-FT) - INFLOW= .5692E+02 EXCESS= .0000E+00 OUTFLOW= .5692E+02 RASIN STORAGE= .5511E-02 PERCENT ERROR= .0

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELEBRITY
MAIN	.94	1.44	5.00		308.60	195.00	1.97	

## HYDROGRAPH AT STATION ASLDR2

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	1	0.	*	1	0615	76	69.	*	1	1230	151	6.	*	1	1845	226	1.	
1	0005	2	0.	*	1	0620	77	65.	*	1	1235	152	6.	*	1	1850	227	1.	
1	0010	3	0.	*	1	0625	78	62.	*	1	1240	153	6.	*	1	1855	228	1.	
1	0015	4	0.	*	1	0630	79	59.	*	1	1245	154	5.	*	1	1900	229	1.	
1	0020	5	0.	*	1	0635	80	56.	*	1	1250	155	5.	*	1	1905	230	1.	
1	0025	6	0.	*	1	0640	81	53.	*	1	1255	156	5.	*	1	1910	231	1.	
1	0030	7	0.	*	1	0645	82	50.	*	1	1300	157	5.	*	1	1915	232	1.	
1	0035	8	0.	*	1	0650	83	48.	*	1	1305	158	5.	*	1	1920	233	1.	
1	0040	9	0.	*	1	0655	84	46.	*	1	1310	159	5.	*	1	1925	234	1.	
1	0045	10	1.	*	1	0700	85	44.	*	1	1315	160	5.	*	1	1930	235	1.	
1	0050	11	1.	*	1	0705	86	42.	*	1	1320	161	5.	*	1	1935	236	1.	
1	0055	12	2.	*	1	0710	87	40.	*	1	1325	162	4.	*	1	1940	237	1.	
1	0100	13	4.	*	1	0715	88	39.	*	1	1330	163	4.	*	1	1945	238	1.	
1	0105	14	6.	*	1	0720	89	37.	*	1	1335	164	4.	*	1	1950	239	1.	
1	0110	15	8.	*	1	0725	90	36.	*	1	1340	165	4.	*	1	1955	240	1.	
1	0115	16	9.	*	1	0730	91	34.	*	1	1345	166	4.	*	1	2000	241	1.	
1	0120	17	9.	*	1	0735	92	33.	*	1	1350	167	4.	*	1	2005	242	1.	
1	0125	18	10.	*	1	0740	93	32.	*	1	1355	168	4.	*	1	2010	243	1.	
1	0130	19	11.	*	1	0745	94	31.	*	1	1400	169	4.	*	1	2015	244	1.	
1	0135	20	12.	*	1	0750	95	30.	*	1	1405	170	4.	*	1	2020	245	1.	
1	0140	21	13.	*	1	0755	96	29.	*	1	1410	171	4.	*	1	2025	246	1.	
1	0145	22	14.	*	1	0800	97	28.	*	1	1415	172	4.	*	1	2030	247	1.	
1	0150	23	15.	*	1	0805	98	27.	*	1	1420	173	3.	*	1	2035	248	1.	
1	0155	24	16.	*	1	0810	99	26.	*	1	1425	174	3.	*	1	2040	249	1.	
1	0200	25	17.	*	1	0815	100	25.	*	1	1430	175	3.	*	1	2045	250	1.	
1	0205	26	18.	*	1	0820	101	24.	*	1	1435	176	3.	*	1	2050	251	1.	
1	0210	27	19.	*	1	0825	102	23.	*	1	1440	177	3.	*	1	2055	252	1.	
1	0215	28	20.	*	1	0830	103	23.	*	1	1445	178	3.	*	1	2100	253	1.	
1	0220	29	22.	*	1	0835	104	22.	*	1	1450	179	3.	*	1	2105	254	1.	
1	0225	30	23.	*	1	0840	105	21.	*	1	1455	180	3.	*	1	2110	255	1.	
1	0230	31	25.	*	1	0845	106	21.	*	1	1500	181	3.	*	1	2115	256	1.	
1	0235	32	28.	*	1	0850	107	20.	*	1	1505	182	3.	*	1	2120	257	1.	
1	0240	33	33.	*	1	0855	108	19.	*	1	1510	183	3.	*	1	2125	258	1.	
1	0245	34	43.	*	1	0900	109	19.	*	1	1515	184	3.	*	1	2130	259	1.	
1	0250	35	58.	*	1	0905	110	18.	*	1	1520	185	3.	*	1	2135	260	1.	
1	0255	36	81.	*	1	0910	111	18.	*	1	1525	186	3.	*	1	2140	261	1.	
1	0300	37	124.	*	1	0915	112	17.	*	1	1530	187	3.	*	1	2145	262	1.	
1	0305	38	230.	*	1	0920	113	16.	*	1	1535	188	2.	*	1	2150	263	1.	
1	0310	39	303.	*	1	0925	114	16.	*	1	1540	189	2.	*	1	2155	264	1.	
1	0315	40	309.	*	1	0930	115	16.	*	1	1545	190	2.	*	1	2200	265	0.	
1	0320	41	295.	*	1	0935	116	15.	*	1	1550	191	2.	*	1	2205	266	0.	
1	0325	42	279.	*	1	0940	117	15.	*	1	1555	192	2.	*	1	2210	267	0.	
1	0330	43	264.	*	1	0945	118	14.	*	1	1600	193	2.	*	1	2215	268	0.	
1	0335	44	248.	*	1	0950	119	14.	*	1	1605	194	2.	*	1	2220	269	0.	
1	0340	45	230.	*	1	0955	120	13.	*	1	1610	195	2.	*	1	2225	270	0.	
1	0345	46	212.	*	1	1000	121	13.	*	1	1615	196	2.	*	1	2230	271	0.	
1	0350	47	194.	*	1	1005	122	13.	*	1	1620	197	2.	*	1	2235	272	0.	
1	0355	48	175.	*	1	1010	123	12.	*	1	1625	198	2.	*	1	2240	273	0.	
1	0400	49	167.	*	1	1015	124	12.	*	1	1630	199	2.	*	1	2245	274	0.	
1	0405	50	158.	*	1	1020	125	12.	*	1	1635	200	2.	*	1	2250	275	0.	
1	0410	51	151.	*	1	1025	126	11.	*	1	1640	201	2.	*	1	2255	276	0.	
1	0415	52	144.	*	1	1030	127	11.	*	1	1645	202	2.	*	1	2300	277	0.	
1	0420	53	139.	*	1	1035	128	11.	*	1	1650	203	2.	*	1	2305	278	0.	
1	0425	54	134.	*	1	1040	129	10.	*	1	1655	204	2.	*	1	2310	279	0.	
1	0430	55	130.	*	1	1045	130	10.	*	1	1700	205	2.	*	1	2315	280	0.	
1	0435	56	126.	*	1	1050	131	10.	*	1	1705	206	2.	*	1	2320	281	0.	
1	0440	57	123.	*	1	1055	132	10.	*	1	1710	207	2.	*	1	2325	282	0.	
1	0445	58	120.	*	1	1100	133	9.	*	1	1715	208	2.	*	1	2330	283	0.	
1	0450	59	117.	*	1	1105	134	9.	*	1	1720	209	2.	*	1	2335	284	0.	
1	0455	60	113.	*	1	1110	135	9.	*	1	1725	210	2.	*	1	2340	285	0.	

1	0500	61	110.	*	1	1115	136	9.	*	1	1730	211	1.	*	1	2345	286	0.
1	0505	62	106.	*	1	1120	137	8.	*	1	1735	212	1.	*	1	2350	287	0.
1	0510	63	103.	*	1	1125	138	8.	*	1	1740	213	1.	*	1	2355	288	0.
1	0515	64	100.	*	1	1130	139	8.	*	1	1745	214	1.	*	2	0000	289	0.
1	0520	65	97.	*	1	1135	140	8.	*	1	1750	215	1.	*	2	0005	290	0.
1	0525	66	94.	*	1	1140	141	8.	*	1	1755	216	1.	*	2	0010	291	0.
1	0530	67	91.	*	1	1145	142	7.	*	1	1800	217	1.	*	2	0015	292	0.
1	0535	68	88.	*	1	1150	143	7.	*	1	1805	218	1.	*	2	0020	293	0.
1	0540	69	86.	*	1	1155	144	7.	*	1	1810	219	1.	*	2	0025	294	0.
1	0545	70	83.	*	1	1200	145	7.	*	1	1815	220	1.	*	2	0030	295	0.
1	0550	71	81.	*	1	1205	146	7.	*	1	1820	221	1.	*	2	0035	296	0.
1	0555	72	78.	*	1	1210	147	6.	*	1	1825	222	1.	*	2	0040	297	0.
1	0600	73	76.	*	1	1215	148	6.	*	1	1830	223	1.	*	2	0045	298	0.
1	0605	74	74.	*	1	1220	149	6.	*	1	1835	224	1.	*	2	0050	299	0.
1	0610	75	71.	*	1	1225	150	6.	*	1	1840	225	1.	*	2	0055	300	0.

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24.92-HR
309.	3.25	100.	29.	28.	28.
		(INCHES)	1.715	1.974	1.974
		(AC-FT)	49.	57.	57.
CUMULATIVE AREA =		.54 SQ MI			

694 KK ASLD 2 SUB

695 KO OUTPUT CONTROL VARIABLES

IPRNT	1	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	360	LAST ORDINATE PUNCHED OR SAVED
TIMINT	.083	TIME INTERVAL IN HOURS

ASLD SOUTH PARCEL EAST OF SCOTTSDALE ROAD AND NORTH OF CHAUNCEY LANE

#### SUBBASIN RUNOFF DATA

697 BA SUBBASIN CHARACTERISTICS

TAREA	.02	SUBBASIN AREA
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#### PRECIPITATION DATA

74 PH DEPTHS FOR 0-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40			TP-49					
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.76	1.50	2.54	2.81	2.99	3.33	.00	.00	.00	.00	.00	.00

STORM AREA = 14.00

698 LS SCS LOSS RATE

STRTL	.60	INITIAL ABSTRACTION
CRVNR	77.00	CURVE NUMBER
RTIMP	78.00	PERCENT IMPERVIOUS AREA

699 UK KINEMATIC WAVE OVERLAND-FLOW ELEMENT NO. 1

L	269.	OVERLAND FLOW LENGTH
S	.0022	SLOPE
N	.015	ROUGHNESS COEFFICIENT
PA	100.0	PERCENT OF SUBBASIN
DXMIN	5	MINIMUM NUMBER OF DX INTERVALS

700 RK KINEMATIC WAVE MAIN CHANNEL

L	600.	CHANNEL LENGTH
S	.0139	SLOPE
N	.015	CHANNEL ROUGHNESS COEFFICIENT
CA	.02	CONTRIBUTING AREA
SHAPE	TRAP	CHANNEL SHAPE
WD	17.00	BOTTOM WIDTH OR DIAMETER
Z	4.00	SIDE SLOPE
NDXMIN	2	MINIMUM NUMBER OF DX INTERVALS
RUPSTQ	NO	ROUTE UPSTREAM HYDROGRAPH

\*\*\*  
COMPUTED KINEMATIC PARAMETERS  
VARIABLE TIME STEP  
(DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(IN)	(FPS)
PLANE1	4.66	1.67	.70	53.80	87.24	185.04	2.78	1.27

MAIN 2.56 1.44 .36 200.00 84.72 185.20 2.78 11.87

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2955E+01 OUTFLOW= .2863E+01 BASIN STORAGE= .7801E-04 PERCENT ERROR= .1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 2.56 1.44 5.00 84.18 185.00 2.80

HYDROGRAPH AT STATION ASLD

DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q		DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	.00	.00	.00	0.	*	1	1230	151	.00	.00	.00	.00	0.	
1	0005	2	.01	.00	.01	0.	*	1	1235	152	.00	.00	.00	.00	0.	
1	0010	3	.01	.00	.01	0.	*	1	1240	153	.00	.00	.00	.00	0.	
1	0015	4	.01	.00	.01	0.	*	1	1245	154	.00	.00	.00	.00	0.	
1	0020	5	.01	.00	.01	0.	*	1	1250	155	.00	.00	.00	.00	0.	
1	0025	6	.01	.00	.01	0.	*	1	1255	156	.00	.00	.00	.00	0.	
1	0030	7	.01	.00	.01	1.	*	1	1300	157	.00	.00	.00	.00	0.	
1	0035	8	.01	.00	.01	1.	*	1	1305	158	.00	.00	.00	.00	0.	
1	0040	9	.01	.00	.01	1.	*	1	1310	159	.00	.00	.00	.00	0.	
1	0045	10	.01	.00	.01	1.	*	1	1315	160	.00	.00	.00	.00	0.	
1	0050	11	.01	.00	.01	1.	*	1	1320	161	.00	.00	.00	.00	0.	
1	0055	12	.01	.00	.01	1.	*	1	1325	162	.00	.00	.00	.00	0.	
1	0100	13	.01	.00	.01	1.	*	1	1330	163	.00	.00	.00	.00	0.	
1	0105	14	.01	.00	.01	1.	*	1	1335	164	.00	.00	.00	.00	0.	
1	0110	15	.01	.00	.01	1.	*	1	1340	165	.00	.00	.00	.00	0.	
1	0115	16	.01	.00	.01	1.	*	1	1345	166	.00	.00	.00	.00	0.	
1	0120	17	.01	.00	.01	1.	*	1	1350	167	.00	.00	.00	.00	0.	
1	0125	18	.01	.00	.01	1.	*	1	1355	168	.00	.00	.00	.00	0.	
1	0130	19	.01	.00	.01	1.	*	1	1400	169	.00	.00	.00	.00	0.	
1	0135	20	.02	.00	.01	1.	*	1	1405	170	.00	.00	.00	.00	0.	
1	0140	21	.01	.00	.01	2.	*	1	1410	171	.00	.00	.00	.00	0.	
1	0145	22	.02	.00	.01	2.	*	1	1415	172	.00	.00	.00	.00	0.	
1	0150	23	.02	.00	.01	2.	*	1	1420	173	.00	.00	.00	.00	0.	
1	0155	24	.02	.00	.01	2.	*	1	1425	174	.00	.00	.00	.00	0.	
1	0200	25	.02	.00	.01	2.	*	1	1430	175	.00	.00	.00	.00	0.	
1	0205	26	.02	.00	.02	2.	*	1	1435	176	.00	.00	.00	.00	0.	
1	0210	27	.02	.00	.02	2.	*	1	1440	177	.00	.00	.00	.00	0.	
1	0215	28	.02	.00	.02	2.	*	1	1445	178	.00	.00	.00	.00	0.	
1	0220	29	.02	.01	.02	3.	*	1	1450	179	.00	.00	.00	.00	0.	
1	0225	30	.03	.01	.02	3.	*	1	1455	180	.00	.00	.00	.00	0.	
1	0230	31	.03	.01	.02	3.	*	1	1500	181	.00	.00	.00	.00	0.	
1	0235	32	.08	.02	.06	5.	*	1	1505	182	.00	.00	.00	.00	0.	
1	0240	33	.09	.02	.07	8.	*	1	1510	183	.00	.00	.00	.00	0.	
1	0245	34	.10	.02	.08	10.	*	1	1515	184	.00	.00	.00	.00	0.	
1	0250	35	.14	.03	.11	13.	*	1	1520	185	.00	.00	.00	.00	0.	
1	0255	36	.18	.03	.14	19.	*	1	1525	186	.00	.00	.00	.00	0.	
1	0300	37	.40	.06	.34	40.	*	1	1530	187	.00	.00	.00	.00	0.	
1	0305	38	.69	.08	.61	84.	*	1	1535	188	.00	.00	.00	.00	0.	
1	0310	39	.28	.03	.25	48.	*	1	1540	189	.00	.00	.00	.00	0.	
1	0315	40	.15	.01	.14	27.	*	1	1545	190	.00	.00	.00	.00	0.	
1	0320	41	.11	.01	.10	19.	*	1	1550	191	.00	.00	.00	.00	0.	
1	0325	42	.09	.01	.09	15.	*	1	1555	192	.00	.00	.00	.00	0.	
1	0330	43	.08	.01	.07	12.	*	1	1600	193	.00	.00	.00	.00	0.	
1	0335	44	.03	.00	.03	9.	*	1	1605	194	.00	.00	.00	.00	0.	
1	0340	45	.03	.00	.03	6.	*	1	1610	195	.00	.00	.00	.00	0.	
1	0345	46	.03	.00	.02	5.	*	1	1615	196	.00	.00	.00	.00	0.	
1	0350	47	.02	.00	.02	4.	*	1	1620	197	.00	.00	.00	.00	0.	
1	0355	48	.02	.00	.02	4.	*	1	1625	198	.00	.00	.00	.00	0.	
1	0400	49	.02	.00	.02	3.	*	1	1630	199	.00	.00	.00	.00	0.	
1	0405	50	.02	.00	.02	3.	*	1	1635	200	.00	.00	.00	.00	0.	
1	0410	51	.02	.00	.02	3.	*	1	1640	201	.00	.00	.00	.00	0.	
1	0415	52	.02	.00	.02	3.	*	1	1645	202	.00	.00	.00	.00	0.	
1	0420	53	.02	.00	.01	2.	*	1	1650	203	.00	.00	.00	.00	0.	
1	0425	54	.02	.00	.01	2.	*	1	1655	204	.00	.00	.00	.00	0.	
1	0430	55	.01	.00	.01	2.	*	1	1700	205	.00	.00	.00	.00	0.	
1	0435	56	.01	.00	.01	2.	*	1	1705	206	.00	.00	.00	.00	0.	
1	0440	57	.01	.00	.01	2.	*	1	1710	207	.00	.00	.00	.00	0.	
1	0445	58	.01	.00	.01	2.	*	1	1715	208	.00	.00	.00	.00	0.	
1	0450	59	.01	.00	.01	2.	*	1	1720	209	.00	.00	.00	.00	0.	
1	0455	60	.01	.00	.01	2.	*	1	1725	210	.00	.00	.00	.00	0.	
1	0500	61	.01	.00	.01	2.	*	1	1730	211	.00	.00	.00	.00	0.	
1	0505	62	.01	.00	.01	2.	*	1	1735	212	.00	.00	.00	.00	0.	
1	0510	63	.01	.00	.01	2.	*	1	1740	213	.00	.00	.00	.00	0.	
1	0515	64	.01	.00	.01	1.	*	1	1745	214	.00	.00	.00	.00	0.	
1	0520	65	.01	.00	.01	1.	*	1	1750	215	.00	.00	.00	.00	0.	
1	0525	66	.01	.00	.01	1.	*	1	1755	216	.00	.00	.00	.00	0.	
1	0530	67	.01	.00	.01	1.	*	1	1800	217	.00	.00	.00	.00	0.	
1	0535	68	.01	.00	.01	1.	*	1	1805	218	.00	.00	.00	.00	0.	
1	0540	69	.01	.00	.01	1.	*	1	1810	219	.00	.00	.00	.00	0.	
1	0545	70	.01	.00	.01	1.	*	1	1815	220	.00	.00	.00	.00	0.	
1	0550	71	.01	.00	.01	1.	*	1	1820	221	.00	.00	.00	.00	0.	
1	0555	72	.01	.00	.01	1.	*	1	1825	222	.00	.00	.00	.00	0.	
1	0600	73	.01	.00	.01	1.	*	1	1830	223	.00	.00	.00	.00	0.	
1	0605	74	.00	.00	.00	1.	*	1	1835	224	.00	.00	.00	.00	0.	
1	0610	75	.00	.00	.00	1.	*	1	1840	225	.00	.00	.00	.00	0.	
1	0615	76	.00	.00	.00	1.	*	1	1845	226	.00	.00	.00	.00	0.	
1	0620	77	.00	.00	.00	0.	*	1	1850	227	.00	.00	.00	.00	0.	
1	0625	78	.00	.00	.00	0.	*	1	1855	228	.00	.00	.00	.00	0.	
1	0630	79	.00	.00	.00	0.	*	1	1900	229	.00	.00	.00	.00	0.	
1	0635	80	.00	.00	.00	0.	*	1	1905	230	.00	.00	.00	.00	0.	
1	0640	81	.00	.00	.00	0.	*	1	1910	231	.00	.00	.00	.00	0.	
1	0645	82	.00	.00	.00	0.	*	1	1915	232	.00	.00	.00	.00	0.	

1	0650	83	.00	.00	.00	0.	*	1	1920	233	.00	.00	.00	0.
1	0655	84	.00	.00	.00	0.	*	1	1925	234	.00	.00	.00	0.
1	0700	85	.00	.00	.00	0.	*	1	1930	235	.00	.00	.00	0.
1	0705	86	.00	.00	.00	0.	*	1	1935	236	.00	.00	.00	0.
1	0710	87	.00	.00	.00	0.	*	1	1940	237	.00	.00	.00	0.
1	0715	88	.00	.00	.00	0.	*	1	1945	238	.00	.00	.00	0.
1	0720	89	.00	.00	.00	0.	*	1	1950	239	.00	.00	.00	0.
1	0725	90	.00	.00	.00	0.	*	1	1955	240	.00	.00	.00	0.
1	0730	91	.00	.00	.00	0.	*	1	2000	241	.00	.00	.00	0.
1	0735	92	.00	.00	.00	0.	*	1	2005	242	.00	.00	.00	0.
1	0740	93	.00	.00	.00	0.	*	1	2010	243	.00	.00	.00	0.
1	0745	94	.00	.00	.00	0.	*	1	2015	244	.00	.00	.00	0.
1	0750	95	.00	.00	.00	0.	*	1	2020	245	.00	.00	.00	0.
1	0755	96	.00	.00	.00	0.	*	1	2025	246	.00	.00	.00	0.
1	0800	97	.00	.00	.00	0.	*	1	2030	247	.00	.00	.00	0.
1	0805	98	.00	.00	.00	0.	*	1	2035	248	.00	.00	.00	0.
1	0810	99	.00	.00	.00	0.	*	1	2040	249	.00	.00	.00	0.
1	0815	100	.00	.00	.00	0.	*	1	2045	250	.00	.00	.00	0.
1	0820	101	.00	.00	.00	0.	*	1	2050	251	.00	.00	.00	0.
1	0825	102	.00	.00	.00	0.	*	1	2055	252	.00	.00	.00	0.
1	0830	103	.00	.00	.00	0.	*	1	2100	253	.00	.00	.00	0.
1	0835	104	.00	.00	.00	0.	*	1	2105	254	.00	.00	.00	0.
1	0840	105	.00	.00	.00	0.	*	1	2110	255	.00	.00	.00	0.
1	0845	106	.00	.00	.00	0.	*	1	2115	256	.00	.00	.00	0.
1	0850	107	.00	.00	.00	0.	*	1	2120	257	.00	.00	.00	0.
1	0855	108	.00	.00	.00	0.	*	1	2125	258	.00	.00	.00	0.
1	0900	109	.00	.00	.00	0.	*	1	2130	259	.00	.00	.00	0.
1	0905	110	.00	.00	.00	0.	*	1	2135	260	.00	.00	.00	0.
1	0910	111	.00	.00	.00	0.	*	1	2140	261	.00	.00	.00	0.
1	0915	112	.00	.00	.00	0.	*	1	2145	262	.00	.00	.00	0.
1	0920	113	.00	.00	.00	0.	*	1	2150	263	.00	.00	.00	0.
1	0925	114	.00	.00	.00	0.	*	1	2155	264	.00	.00	.00	0.
1	0930	115	.00	.00	.00	0.	*	1	2200	265	.00	.00	.00	0.
1	0935	116	.00	.00	.00	0.	*	1	2205	266	.00	.00	.00	0.
1	0940	117	.00	.00	.00	0.	*	1	2210	267	.00	.00	.00	0.
1	0945	118	.00	.00	.00	0.	*	1	2215	268	.00	.00	.00	0.
1	0950	119	.00	.00	.00	0.	*	1	2220	269	.00	.00	.00	0.
1	0955	120	.00	.00	.00	0.	*	1	2225	270	.00	.00	.00	0.
1	1000	121	.00	.00	.00	0.	*	1	2230	271	.00	.00	.00	0.
1	1005	122	.00	.00	.00	0.	*	1	2235	272	.00	.00	.00	0.
1	1010	123	.00	.00	.00	0.	*	1	2240	273	.00	.00	.00	0.
1	1015	124	.00	.00	.00	0.	*	1	2245	274	.00	.00	.00	0.
1	1020	125	.00	.00	.00	0.	*	1	2250	275	.00	.00	.00	0.
1	1025	126	.00	.00	.00	0.	*	1	2255	276	.00	.00	.00	0.
1	1030	127	.00	.00	.00	0.	*	1	2300	277	.00	.00	.00	0.
1	1035	128	.00	.00	.00	0.	*	1	2305	278	.00	.00	.00	0.
1	1040	129	.00	.00	.00	0.	*	1	2310	279	.00	.00	.00	0.
1	1045	130	.00	.00	.00	0.	*	1	2315	280	.00	.00	.00	0.
1	1050	131	.00	.00	.00	0.	*	1	2320	281	.00	.00	.00	0.
1	1055	132	.00	.00	.00	0.	*	1	2325	282	.00	.00	.00	0.
1	1100	133	.00	.00	.00	0.	*	1	2330	283	.00	.00	.00	0.
1	1105	134	.00	.00	.00	0.	*	1	2335	284	.00	.00	.00	0.
1	1110	135	.00	.00	.00	0.	*	1	2340	285	.00	.00	.00	0.
1	1115	136	.00	.00	.00	0.	*	1	2345	286	.00	.00	.00	0.
1	1120	137	.00	.00	.00	0.	*	1	2350	287	.00	.00	.00	0.
1	1125	138	.00	.00	.00	0.	*	1	2355	288	.00	.00	.00	0.
1	1130	139	.00	.00	.00	0.	*	2	0000	289	.00	.00	.00	0.
1	1135	140	.00	.00	.00	0.	*	2	0005	290	.00	.00	.00	0.
1	1140	141	.00	.00	.00	0.	*	2	0010	291	.00	.00	.00	0.
1	1145	142	.00	.00	.00	0.	*	2	0015	292	.00	.00	.00	0.
1	1150	143	.00	.00	.00	0.	*	2	0020	293	.00	.00	.00	0.
1	1155	144	.00	.00	.00	0.	*	2	0025	294	.00	.00	.00	0.
1	1200	145	.00	.00	.00	0.	*	2	0030	295	.00	.00	.00	0.
1	1205	146	.00	.00	.00	0.	*	2	0035	296	.00	.00	.00	0.
1	1210	147	.00	.00	.00	0.	*	2	0040	297	.00	.00	.00	0.
1	1215	148	.00	.00	.00	0.	*	2	0045	298	.00	.00	.00	0.
1	1220	149	.00	.00	.00	0.	*	2	0050	299	.00	.00	.00	0.
1	1225	150	.00	.00	.00	0.	*	2	0055	300	.00	.00	.00	0.

TOTAL RAINFALL = 3.22, TOTAL LOSS = .44, TOTAL EXCESS = 2.78

PEAK FLOW	TIME		6-HR	24-HR	72-HR	24.92-HR
(CFS)	(HR)	(CFS)				
84.	3.08		6.	1.	1.	1.
		(INCHES)	2.777	2.795	2.795	2.795
		(AC-FT)	3.	3.	3.	3.

CUMULATIVE AREA = .02 SQ MI

701 KK

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\* CPBRIN \*  
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COMBINE

702 KO

OUTPUT CONTROL VARIABLES

IPRNT	1	PRINT CONTROL
IPLOT	0	PLOT CONTROL
QSCAL	0.	HYDROGRAPH PLOT SCALE
IPNCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT

ISAV1 1 FIRST ORDINATE PUNCHED OR SAVED  
 ISAV2 300 LAST ORDINATE PUNCHED OR SAVED  
 TIMINT .083 TIME INTERVAL IN HOURS

COMBINE ROUTED ROUTED ASL1CHNL WITH ASL12

704 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION CPBRIN  
 SUM OF 2 HYDROGRAPHS

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1		0000	1	0.	1		0615	76	69.	1		1230	151	6.	1		1845	226	1.
1		0005	2	0.	1		0620	77	66.	1		1235	152	6.	1		1850	227	1.
1		0010	3	0.	1		0625	78	62.	1		1240	153	6.	1		1855	228	1.
1		0015	4	0.	1		0630	79	59.	1		1245	154	5.	1		1900	229	1.
1		0020	5	0.	1		0635	80	56.	1		1250	155	5.	1		1905	230	1.
1		0025	6	0.	1		0640	81	53.	1		1255	156	5.	1		1910	231	1.
1		0030	7	1.	1		0645	82	51.	1		1300	157	5.	1		1915	232	1.
1		0035	8	1.	1		0650	83	48.	1		1305	158	5.	1		1920	233	1.
1		0040	9	1.	1		0655	84	46.	1		1310	159	5.	1		1925	234	1.
1		0045	10	2.	1		0700	85	44.	1		1315	160	5.	1		1930	235	1.
1		0050	11	2.	1		0705	86	42.	1		1320	161	5.	1		1935	236	1.
1		0055	12	3.	1		0710	87	40.	1		1325	162	4.	1		1940	237	1.
1		0100	13	5.	1		0715	88	39.	1		1330	163	4.	1		1945	238	1.
1		0105	14	8.	1		0720	89	37.	1		1335	164	4.	1		1950	239	1.
1		0110	15	9.	1		0725	90	36.	1		1340	165	4.	1		1955	240	1.
1		0115	16	10.	1		0730	91	34.	1		1345	166	4.	1		2000	241	1.
1		0120	17	11.	1		0735	92	33.	1		1350	167	4.	1		2005	242	1.
1		0125	18	12.	1		0740	93	32.	1		1355	168	4.	1		2010	243	1.
1		0130	19	12.	1		0745	94	31.	1		1400	169	4.	1		2015	244	1.
1		0135	20	13.	1		0750	95	30.	1		1405	170	4.	1		2020	245	1.
1		0140	21	14.	1		0755	96	29.	1		1410	171	4.	1		2025	246	1.
1		0145	22	15.	1		0800	97	28.	1		1415	172	4.	1		2030	247	1.
1		0150	23	16.	1		0805	98	27.	1		1420	173	3.	1		2035	248	1.
1		0155	24	17.	1		0810	99	26.	1		1425	174	3.	1		2040	249	1.
1		0200	25	19.	1		0815	100	25.	1		1430	175	3.	1		2045	250	1.
1		0205	26	20.	1		0820	101	24.	1		1435	176	3.	1		2050	251	1.
1		0210	27	21.	1		0825	102	23.	1		1440	177	3.	1		2055	252	1.
1		0215	28	23.	1		0830	103	23.	1		1445	178	3.	1		2100	253	1.
1		0220	29	24.	1		0835	104	22.	1		1450	179	3.	1		2105	254	1.
1		0225	30	26.	1		0840	105	21.	1		1455	180	3.	1		2110	255	1.
1		0230	31	28.	1		0845	106	21.	1		1500	181	3.	1		2115	256	1.
1		0235	32	32.	1		0850	107	20.	1		1505	182	3.	1		2120	257	1.
1		0240	33	40.	1		0855	108	19.	1		1510	183	3.	1		2125	258	1.
1		0245	34	53.	1		0900	109	19.	1		1515	184	3.	1		2130	259	1.
1		0250	35	72.	1		0905	110	18.	1		1520	185	3.	1		2135	260	1.
1		0255	36	100.	1		0910	111	18.	1		1525	186	3.	1		2140	261	1.
1		0300	37	164.	1		0915	112	17.	1		1530	187	3.	1		2145	262	1.
1		0305	38	314.	1		0920	113	17.	1		1535	188	2.	1		2150	263	1.
1		0310	39	357.	1		0925	114	16.	1		1540	189	2.	1		2155	264	1.
1		0315	40	336.	1		0930	115	16.	1		1545	190	2.	1		2200	265	0.
1		0320	41	314.	1		0935	116	15.	1		1550	191	2.	1		2205	266	0.
1		0325	42	294.	1		0940	117	15.	1		1555	192	2.	1		2210	267	0.
1		0330	43	277.	1		0945	118	14.	1		1600	193	2.	1		2215	268	0.
1		0335	44	257.	1		0950	119	14.	1		1605	194	2.	1		2220	269	0.
1		0340	45	236.	1		0955	120	13.	1		1610	195	2.	1		2225	270	0.
1		0345	46	217.	1		1000	121	13.	1		1615	196	2.	1		2230	271	0.
1		0350	47	198.	1		1005	122	13.	1		1620	197	2.	1		2235	272	0.
1		0355	48	183.	1		1010	123	12.	1		1625	198	2.	1		2240	273	0.
1		0400	49	171.	1		1015	124	12.	1		1630	199	2.	1		2245	274	0.
1		0405	50	161.	1		1020	125	12.	1		1635	200	2.	1		2250	275	0.
1		0410	51	153.	1		1025	126	11.	1		1640	201	2.	1		2255	276	0.
1		0415	52	147.	1		1030	127	11.	1		1645	202	2.	1		2300	277	0.
1		0420	53	141.	1		1035	128	11.	1		1650	203	2.	1		2305	278	0.
1		0425	54	137.	1		1040	129	10.	1		1655	204	2.	1		2310	279	0.
1		0430	55	132.	1		1045	130	10.	1		1700	205	2.	1		2315	280	0.
1		0435	56	128.	1		1050	131	10.	1		1705	206	2.	1		2320	281	0.
1		0440	57	125.	1		1055	132	10.	1		1710	207	2.	1		2325	282	0.
1		0445	58	122.	1		1100	133	9.	1		1715	208	2.	1		2330	283	0.
1		0450	59	118.	1		1105	134	9.	1		1720	209	2.	1		2335	284	0.
1		0455	60	115.	1		1110	135	9.	1		1725	210	2.	1		2340	285	0.
1		0500	61	111.	1		1115	136	9.	1		1730	211	1.	1		2345	286	0.
1		0505	62	108.	1		1120	137	8.	1		1735	212	1.	1		2350	287	0.
1		0510	63	104.	1		1125	138	8.	1		1740	213	1.	1		2355	288	0.
1		0515	64	101.	1		1130	139	8.	1		1745	214	1.	1		0000	289	0.
1		0520	65	98.	1		1135	140	8.	1		1750	215	1.	1		0005	290	0.
1		0525	66	95.	1		1140	141	8.	1		1755	216	1.	1		0010	291	0.
1		0530	67	92.	1		1145	142	7.	1		1800	217	1.	1		0015	292	0.
1		0535	68	90.	1		1150	143	7.	1		1805	218	1.	1		0020	293	0.
1		0540	69	87.	1		1155	144	7.	1		1810	219	1.	1		0025	294	0.
1		0545	70	84.	1		1200	145	7.	1		1815	220	1.	1		0030	295	0.
1		0550	71	82.	1		1205	146	7.	1		1820	221	1.	1		0035	296	0.
1		0555	72	80.	1		1210	147	6.	1		1825	222	1.	1		0040	297	0.
1		0600	73	77.	1		1215	148	6.	1		1830	223	1.	1		0045	298	0.
1		0605	74	75.	1		1220	149	6.	1		1835	224	1.	1		0050	299	0.
1		0610	75	72.	1		1225	150	6.	1		1840	225	1.	1		0055	300	0.

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
 6-HR 24-HR 72-HR 24.92-HR  
 (CFS) (HR)

+ 351. 3.17 (CFS) 105. 30. 29. 29.  
 (INCHES) 1.744 2.002 2.003 2.003  
 (AC-FT) 52. 60. 60. 60.  
 CUMULATIVE AREA = .56 SQ MI

705 KK

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 \* R33C.2 \*  
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706 KO

OUTPUT CONTROL VARIABLES  
 IPRNT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 RETRIEVE DIVERTED PIPE FLOW

708 DR

RETRIEVE DIVERSION HYDROGRAPH  
 ISTAT D33C.2 DIVERSION HYDROGRAPH IDENTIFICATION

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# HYDROGRAPH AT STATION R33C.2

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	1	0.	*	1	0615	76	9.	*	1	1230	151	0.	*	1	1845	226	0.	
1	0005	2	0.	*	1	0620	77	8.	*	1	1235	152	0.	*	1	1850	227	0.	
1	0010	3	0.	*	1	0625	78	7.	*	1	1240	153	0.	*	1	1855	228	0.	
1	0015	4	0.	*	1	0630	79	6.	*	1	1245	154	0.	*	1	1900	229	0.	
1	0020	5	0.	*	1	0635	80	5.	*	1	1250	155	0.	*	1	1905	230	0.	
1	0025	6	0.	*	1	0640	81	5.	*	1	1255	156	0.	*	1	1910	231	0.	
1	0030	7	0.	*	1	0645	82	4.	*	1	1300	157	0.	*	1	1915	232	0.	
1	0035	8	0.	*	1	0650	83	4.	*	1	1305	158	0.	*	1	1920	233	0.	
1	0040	9	0.	*	1	0655	84	3.	*	1	1310	159	0.	*	1	1925	234	0.	
1	0045	10	0.	*	1	0700	85	3.	*	1	1315	160	0.	*	1	1930	235	0.	
1	0050	11	0.	*	1	0705	86	2.	*	1	1320	161	0.	*	1	1935	236	0.	
1	0055	12	0.	*	1	0710	87	2.	*	1	1325	162	0.	*	1	1940	237	0.	
1	0100	13	0.	*	1	0715	88	2.	*	1	1330	163	0.	*	1	1945	238	0.	
1	0105	14	1.	*	1	0720	89	2.	*	1	1335	164	0.	*	1	1950	239	0.	
1	0110	15	1.	*	1	0725	90	1.	*	1	1340	165	0.	*	1	1955	240	0.	
1	0115	16	1.	*	1	0730	91	1.	*	1	1345	166	0.	*	1	2000	241	0.	
1	0120	17	2.	*	1	0735	92	1.	*	1	1350	167	0.	*	1	2005	242	0.	
1	0125	18	2.	*	1	0740	93	1.	*	1	1355	168	0.	*	1	2010	243	0.	
1	0130	19	2.	*	1	0745	94	1.	*	1	1400	169	0.	*	1	2015	244	0.	
1	0135	20	3.	*	1	0750	95	1.	*	1	1405	170	0.	*	1	2020	245	0.	
1	0140	21	3.	*	1	0755	96	1.	*	1	1410	171	0.	*	1	2025	246	0.	
1	0145	22	3.	*	1	0800	97	1.	*	1	1415	172	0.	*	1	2030	247	0.	
1	0150	23	3.	*	1	0805	98	1.	*	1	1420	173	0.	*	1	2035	248	0.	
1	0155	24	3.	*	1	0810	99	0.	*	1	1425	174	0.	*	1	2040	249	0.	
2	0200	25	4.	*	1	0815	100	0.	*	1	1430	175	0.	*	1	2045	250	0.	
1	0205	26	4.	*	1	0820	101	0.	*	1	1435	176	0.	*	1	2050	251	0.	
1	0210	27	4.	*	1	0825	102	0.	*	1	1440	177	0.	*	1	2055	252	0.	
1	0215	28	5.	*	1	0830	103	0.	*	1	1445	178	0.	*	1	2100	253	0.	
1	0220	29	5.	*	1	0835	104	0.	*	1	1450	179	0.	*	1	2105	254	0.	
1	0225	30	5.	*	1	0840	105	0.	*	1	1455	180	0.	*	1	2110	255	0.	
1	0230	31	6.	*	1	0845	106	0.	*	1	1500	181	0.	*	1	2115	256	0.	
1	0235	32	6.	*	1	0850	107	0.	*	1	1505	182	0.	*	1	2120	257	0.	
1	0240	33	8.	*	1	0855	108	0.	*	1	1510	183	0.	*	1	2125	258	0.	
1	0245	34	10.	*	1	0900	109	0.	*	1	1515	184	0.	*	1	2130	259	0.	
1	0250	35	11.	*	1	0905	110	0.	*	1	1520	185	0.	*	1	2135	260	0.	
1	0255	36	13.	*	1	0910	111	0.	*	1	1525	186	0.	*	1	2140	261	0.	
1	0300	37	15.	*	1	0915	112	0.	*	1	1530	187	0.	*	1	2145	262	0.	
1	0305	38	17.	*	1	0920	113	0.	*	1	1535	188	0.	*	1	2150	263	0.	
1	0310	39	46.	*	1	0925	114	0.	*	1	1540	189	0.	*	1	2155	264	0.	
1	0315	40	96.	*	1	0930	115	0.	*	1	1545	190	0.	*	1	2200	265	0.	
1	0320	41	108.	*	1	0935	116	0.	*	1	1550	191	0.	*	1	2205	266	0.	
1	0325	42	105.	*	1	0940	117	0.	*	1	1555	192	0.	*	1	2210	267	0.	
1	0330	43	96.	*	1	0945	118	0.	*	1	1600	193	0.	*	1	2215	268	0.	
1	0335	44	86.	*	1	0950	119	0.	*	1	1605	194	0.	*	1	2220	269	0.	
1	0340	45	75.	*	1	0955	120	0.	*	1	1610	195	0.	*	1	2225	270	0.	
1	0345	46	63.	*	1	1000	121	0.	*	1	1615	196	0.	*	1	2230	271	0.	
1	0350	47	52.	*	1	1005	122	0.	*	1	1620	197	0.	*	1	2235	272	0.	
1	0355	48	44.	*	1	1010	123	0.	*	1	1625	198	0.	*	1	2240	273	0.	
1	0400	49	37.	*	2	1015	124	0.	*	1	1630	199	0.	*	1	2245	274	0.	
1	0405	50	31.	*	1	1020	125	0.	*	1	1635	200	0.	*	1	2250	275	0.	
1	0410	51	27.	*	1	1025	126	0.	*	1	1640	201	0.	*	1	2255	276	0.	
1	0415	52	24.	*	1	1030	127	0.	*	1	1645	202	0.	*	1	2300	277	0.	
1	0420	53	22.	*	1	1035	128	0.	*	1	1650	203	0.	*	1	2305	278	0.	
2	0425	54	19.	*	2	1040	129	0.	*	1	1655	204	0.	*	1	2310	279	0.	
1	0430	55	18.	*	1	1045	130	0.	*	1	1700	205	0.	*	1	2315	280	0.	
1	0435	56	18.	*	1	1050	131	0.	*	1	1705	206	0.	*	1	2320	281	0.	
1	0440	57	17.	*	1	1055	132	0.	*	1	1710	207	0.	*	1	2325	282	0.	
1	0445	58	17.	*	1	1100	133	0.	*	1	1715	208	0.	*	1	2330	283	0.	
1	0450	59	17.	*	1	1105	134	0.	*	1	1720	209	0.	*	1	2335	284	0.	
1	0455	60	16.	*	1	1110	135	0.	*	1	1725	210	0.	*	1	2340	285	0.	
1	0500	61	16.	*	1	1115	136	0.	*	1	1730	211	0.	*	1	2345	286	0.	
1	0505	62	16.	*	1	1120	137	0.	*	1	1735	212	0.	*	1	2350	287	0.	
1	0510	63	15.	*	1	1125	138	0.	*	1	1740	213	0.	*	1	2355	288	0.	

1	0515	64	15.	*	1	1130	139	0.	*	1	1745	214	0.	*	2	0000	289	0.
1	0520	65	14.	*	1	1135	140	0.	*	1	1750	215	0.	*	2	0005	290	0.
1	0525	66	14.	*	1	1140	141	0.	*	1	1755	216	0.	*	2	0010	291	0.
1	0530	67	14.	*	1	1145	142	0.	*	1	1800	217	0.	*	2	0015	292	0.
1	0535	68	13.	*	1	1150	143	0.	*	1	1805	218	0.	*	2	0020	293	0.
1	0540	69	13.	*	1	1155	144	0.	*	1	1810	219	0.	*	2	0025	294	0.
1	0545	70	12.	*	1	1200	145	0.	*	1	1815	220	0.	*	2	0030	295	0.
1	0550	71	12.	*	1	1205	146	0.	*	1	1820	221	0.	*	2	0035	296	0.
1	0555	72	12.	*	1	1210	147	0.	*	1	1825	222	0.	*	2	0040	297	0.
1	0600	73	11.	*	1	1215	148	0.	*	1	1830	223	0.	*	2	0045	298	0.
1	0605	74	11.	*	1	1220	149	0.	*	1	1835	224	0.	*	2	0050	299	0.
1	0610	75	10.	*	1	1225	150	0.	*	1	1840	225	0.	*	2	0055	300	0.

\*\*\*\*\*

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24.92-HR
106.	3.33	20.	5.	5.	5.
		(INCHES)	.329	.333	.333
		(AC-FT)	10.	10.	10.

CUMULATIVE AREA = .00 SQ MI

709 KK

\*\*\*\*\*  
S40WT  
\*\*\*\*\*

SUB

710 KO

OUTPUT CONTROL VARIABLES

IPRNT 1 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCAL 0. HYDROGRAPH PLOT SCALE  
SUB EAST OF SCOTTSDALE RD, FLOWING DIRECTLY INTO SCOTTSDALE RD  
CULVERT. TAKES SCOTTS RD HALF ST AND SCENIC CORRIDOR

SUBBASIN RUNOFF DATA

713 BA

SUBBASIN CHARACTERISTICS

TAREA .01 SUBBASIN AREA

PRECIPITATION DATA

24 PH

DEPTHS FOR 6-PERCENT HYPOTHETICAL STORM

HYDRO-35			TP-40					TP-49			
5-MIN	15-MIN	60-MIN	2-HR	3-HR	6-HR	12-HR	24-HR	2-DAY	4-DAY	7-DAY	10-DAY
.76	1.50	2.54	2.81	2.95	3.33	.00	.00	.00	.00	.00	.00

STORM AREA = 14.00

714 LS

SCS LOSS RATE

STRTL .60 INITIAL ABSTRACTION  
CRVNR 77.00 CURVE NUMBER  
RTIMP 39.00 PERCENT IMPERVIOUS AREA

715 UK

KINEMATIC WAVE

OVERLAND-FLOW ELEMENT NO. 1  
L 50. OVERLAND FLOW LENGTH  
S .0100 SLOPE  
N .050 ROUGHNESS COEFFICIENT  
PA 100.0 PERCENT OF SUBBASIN  
DXMIN 5 MINIMUM NUMBER OF DX INTERVALS

716 RK

KINEMATIC WAVE

MAIN CHANNEL  
L 600. CHANNEL LENGTH  
S .0100 SLOPE  
N .015 CHANNEL ROUGHNESS COEFFICIENT  
CA .01 CONTRIBUTING AREA  
SHAPE CIRC CHANNEL SHAPE  
WD 4.50 BOTTOM WIDTH OR DIAMETER  
Z .00 SIDE SLOPE  
NDXMIN 2 MINIMUM NUMBER OF DX INTERVALS  
RUPSTQ NO ROUTE UPSTREAM HYDROGRAPH

\*\*\*

COMPUTED KINEMATIC PARAMETERS  
VARIABLE TIME STEP  
(DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
PLANET	2.98	1.67	.43	10.00	41.73	184.64	3.00	.54
MAIN	5.89	1.25	.33	200.00	11.72	184.75	3.00	12.50

CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1009E+01 OUTFLOW= .1008E+01 BASIN STORAGE= .4454E-05 PERCENT ERROR= .1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 6.89 1.25 5 00 31.47 185.00 3.01

HYDROGRAPH AT STATION 540WT

DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q		DA	MON	HRMN	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	.00	.00	.00	0.	*		1	1230	151	.00	.00	.00	0.	
1	0005	2	.01	.00	.01	0.	*		1	1235	152	.00	.00	.00	0.	
1	0010	3	.01	.00	.01	0.	*		1	1240	153	.00	.00	.00	0.	
1	0015	4	.01	.00	.01	0.	*		1	1245	154	.00	.00	.00	0.	
1	0020	5	.01	.00	.01	0.	*		1	1250	155	.00	.00	.00	0.	
1	0025	6	.01	.00	.01	0.	*		1	1255	156	.00	.00	.00	0.	
1	0030	7	.01	.00	.01	0.	*		1	1300	157	.00	.00	.00	0.	
1	0035	8	.01	.00	.01	0.	*		1	1305	158	.00	.00	.00	0.	
1	0040	9	.01	.00	.01	0.	*		1	1310	159	.00	.00	.00	0.	
1	0045	10	.01	.00	.01	0.	*		1	1315	160	.00	.00	.00	0.	
1	0050	11	.01	.00	.01	0.	*		1	1320	161	.00	.00	.00	0.	
1	0055	12	.01	.00	.01	0.	*		1	1325	162	.00	.00	.00	0.	
1	0100	13	.01	.00	.01	0.	*		1	1330	163	.00	.00	.00	0.	
1	0105	14	.01	.00	.01	0.	*		1	1335	164	.00	.00	.00	0.	
1	0110	15	.01	.00	.01	0.	*		1	1340	165	.00	.00	.00	0.	
1	0115	16	.01	.00	.01	0.	*		1	1345	166	.00	.00	.00	0.	
1	0120	17	.01	.00	.01	1.	*		1	1350	167	.00	.00	.00	0.	
1	0125	18	.01	.00	.01	1.	*		1	1355	168	.00	.00	.00	0.	
1	0130	19	.01	.00	.01	1.	*		1	1400	169	.00	.00	.00	0.	
1	0135	20	.01	.00	.01	1.	*		1	1405	170	.00	.00	.00	0.	
1	0140	21	.01	.00	.01	1.	*		1	1410	171	.00	.00	.00	0.	
1	0145	22	.02	.00	.01	1.	*		1	1415	172	.00	.00	.00	0.	
1	0150	23	.02	.00	.01	1.	*		1	1420	173	.00	.00	.00	0.	
1	0155	24	.02	.00	.02	1.	*		1	1425	174	.00	.00	.00	0.	
1	0200	25	.02	.00	.02	1.	*		1	1430	175	.00	.00	.00	0.	
1	0205	26	.02	.00	.02	1.	*		1	1435	176	.00	.00	.00	0.	
1	0210	27	.02	.00	.02	1.	*		1	1440	177	.00	.00	.00	0.	
1	0215	28	.02	.00	.02	1.	*		1	1445	178	.00	.00	.00	0.	
1	0220	29	.02	.00	.02	1.	*		1	1450	179	.00	.00	.00	0.	
1	0225	30	.03	.00	.02	1.	*		1	1455	180	.00	.00	.00	0.	
1	0230	31	.03	.00	.03	1.	*		1	1500	181	.00	.00	.00	0.	
1	0235	32	.08	.01	.07	3.	*		1	1505	182	.00	.00	.00	0.	
1	0240	33	.09	.01	.08	4.	*		1	1510	183	.00	.00	.00	0.	
1	0245	34	.10	.01	.09	4.	*		1	1515	184	.00	.00	.00	0.	
1	0250	35	.14	.01	.12	6.	*		1	1520	185	.00	.00	.00	0.	
1	0255	36	.19	.02	.16	8.	*		1	1525	186	.00	.00	.00	0.	
1	0300	37	.40	.03	.37	18.	*		1	1530	187	.00	.00	.00	0.	
1	0305	38	.69	.04	.65	31.	*		1	1535	188	.00	.00	.00	0.	
1	0310	39	.28	.01	.26	13.	*		1	1540	189	.00	.00	.00	0.	
1	0315	40	.15	.01	.15	7.	*		1	1545	190	.00	.00	.00	0.	
1	0320	41	.11	.00	.10	5.	*		1	1550	191	.00	.00	.00	0.	
1	0325	42	.09	.00	.09	4.	*		1	1555	192	.00	.00	.00	0.	
1	0330	43	.08	.00	.08	4.	*		1	1600	193	.00	.00	.00	0.	
1	0335	44	.03	.00	.03	2.	*		1	1605	194	.00	.00	.00	0.	
1	0340	45	.03	.00	.03	1.	*		1	1610	195	.00	.00	.00	0.	
1	0345	46	.03	.00	.03	1.	*		1	1615	196	.00	.00	.00	0.	
1	0350	47	.02	.00	.02	1.	*		1	1620	197	.00	.00	.00	0.	
1	0355	48	.02	.00	.02	1.	*		1	1625	198	.00	.00	.00	0.	
1	0400	49	.02	.00	.02	1.	*		1	1630	199	.00	.00	.00	0.	
1	0405	50	.02	.00	.02	1.	*		1	1635	200	.00	.00	.00	0.	
1	0410	51	.02	.00	.02	1.	*		1	1640	201	.00	.00	.00	0.	
1	0415	52	.02	.00	.02	1.	*		1	1645	202	.00	.00	.00	0.	
1	0420	53	.02	.00	.02	1.	*		1	1650	203	.00	.00	.00	0.	
1	0425	54	.02	.00	.01	1.	*		1	1655	204	.00	.00	.00	0.	
1	0430	55	.01	.00	.01	1.	*		1	1700	205	.00	.00	.00	0.	
1	0435	56	.01	.00	.01	1.	*		1	1705	206	.00	.00	.00	0.	
1	0440	57	.01	.00	.01	1.	*		1	1710	207	.00	.00	.00	0.	
1	0445	58	.01	.00	.01	1.	*		1	1715	208	.00	.00	.00	0.	
1	0450	59	.01	.00	.01	1.	*		1	1720	209	.00	.00	.00	0.	
1	0455	60	.01	.00	.01	1.	*		1	1725	210	.00	.00	.00	0.	
1	0500	61	.01	.00	.01	1.	*		1	1730	211	.00	.00	.00	0.	
1	0505	62	.01	.00	.01	1.	*		1	1735	212	.00	.00	.00	0.	
1	0510	63	.01	.00	.01	0.	*		1	1740	213	.00	.00	.00	0.	
1	0515	64	.01	.00	.01	0.	*		1	1745	214	.00	.00	.00	0.	
1	0520	65	.01	.00	.01	0.	*		1	1750	215	.00	.00	.00	0.	
1	0525	66	.01	.00	.01	0.	*		1	1755	216	.00	.00	.00	0.	
1	0530	67	.01	.00	.01	0.	*		1	1800	217	.00	.00	.00	0.	
1	0535	68	.01	.00	.01	0.	*		1	1805	218	.00	.00	.00	0.	
1	0540	69	.01	.00	.01	0.	*		1	1810	219	.00	.00	.00	0.	
1	0545	70	.01	.00	.01	0.	*		1	1815	220	.00	.00	.00	0.	
1	0550	71	.01	.00	.01	0.	*		1	1820	221	.00	.00	.00	0.	
1	0555	72	.01	.00	.01	0.	*		1	1825	222	.00	.00	.00	0.	
1	0600	73	.01	.00	.01	0.	*		1	1830	223	.00	.00	.00	0.	
1	0605	74	.00	.00	.00	0.	*		1	1835	224	.00	.00	.00	0.	
1	0610	75	.00	.00	.00	0.	*		1	1840	225	.00	.00	.00	0.	
1	0615	76	.00	.00	.00	0.	*		1	1845	226	.00	.00	.00	0.	
1	0620	77	.00	.00	.00	0.	*		1	1850	227	.00	.00	.00	0.	
1	0625	78	.00	.00	.00	0.	*		1	1855	228	.00	.00	.00	0.	
1	0630	79	.00	.00	.00	0.	*		1	1900	229	.00	.00	.00	0.	
1	0635	80	.00	.00	.00	0.	*		1	1905	230	.00	.00	.00	0.	
1	0640	81	.00	.00	.00	0.	*		1	1910	231	.00	.00	.00	0.	
1	0645	82	.00	.00	.00	0.	*		1	1915	232	.00	.00	.00	0.	
1	0650	83	.00	.00	.00	0.	*		1	1920	233	.00	.00	.00	0.	
1	0655	84	.00	.00	.00	0.	*		1	1925	234	.00	.00	.00	0.	
1	0700	85	.00	.00	.00	0.	*		1	1930	235	.00	.00	.00	0.	
1	0705	86	.00	.00	.00	0.	*		1	1935	236	.00	.00	.00	0.	
1	0710	87	.00	.00	.00	0.	*		1	1940	237	.00	.00	.00	0.	
1	0715	88	.00	.00	.00	0.	*		1	1945	238	.00	.00	.00	0.	
1	0720	89	.00	.00	.00	0.	*		1	1950	239	.00	.00	.00	0.	
1	0725	90	.00	.00	.00	0.	*		1	1955	240	.00	.00	.00	0.	



1	0730	91	.00	.00	.00	0.	*	1	2000	241	.00	.00	.00	0.
1	0735	92	.00	.00	.00	0.	*	1	2005	242	.00	.00	.00	0.
1	0740	93	.00	.00	.00	0.	*	1	2010	243	.00	.00	.00	0.
1	0745	94	.00	.00	.00	0.	*	1	2015	244	.00	.00	.00	0.
1	0750	95	.00	.00	.00	0.	*	1	2020	245	.00	.00	.00	0.
1	0755	96	.00	.00	.00	0.	*	1	2025	246	.00	.00	.00	0.
1	0800	97	.00	.00	.00	0.	*	1	2030	247	.00	.00	.00	0.
1	0805	98	.00	.00	.00	0.	*	1	2035	248	.00	.00	.00	0.
1	0810	99	.00	.00	.00	0.	*	1	2040	249	.00	.00	.00	0.
1	0815	100	.00	.00	.00	0.	*	1	2045	250	.00	.00	.00	0.
1	0820	101	.00	.00	.00	0.	*	1	2050	251	.00	.00	.00	0.
1	0825	102	.00	.00	.00	0.	*	1	2055	252	.00	.00	.00	0.
1	0830	103	.00	.00	.00	0.	*	1	2100	253	.00	.00	.00	0.
1	0835	104	.00	.00	.00	0.	*	1	2105	254	.00	.00	.00	0.
1	0840	105	.00	.00	.00	0.	*	1	2110	255	.00	.00	.00	0.
1	0845	106	.00	.00	.00	0.	*	1	2115	256	.00	.00	.00	0.
1	0850	107	.00	.00	.00	0.	*	1	2120	257	.00	.00	.00	0.
1	0855	108	.00	.00	.00	0.	*	1	2125	258	.00	.00	.00	0.
1	0900	109	.00	.00	.00	0.	*	1	2130	259	.00	.00	.00	0.
1	0905	110	.00	.00	.00	0.	*	1	2135	260	.00	.00	.00	0.
1	0910	111	.00	.00	.00	0.	*	1	2140	261	.00	.00	.00	0.
1	0915	112	.00	.00	.00	0.	*	1	2145	262	.00	.00	.00	0.
1	0920	113	.00	.00	.00	0.	*	1	2150	263	.00	.00	.00	0.
1	0925	114	.00	.00	.00	0.	*	1	2155	264	.00	.00	.00	0.
1	0930	115	.00	.00	.00	0.	*	1	2200	265	.00	.00	.00	0.
1	0935	116	.00	.00	.00	0.	*	1	2205	266	.00	.00	.00	0.
1	0940	117	.00	.00	.00	0.	*	1	2210	267	.00	.00	.00	0.
1	0945	118	.00	.00	.00	0.	*	1	2215	268	.00	.00	.00	0.
1	0950	119	.00	.00	.00	0.	*	1	2220	269	.00	.00	.00	0.
1	0955	120	.00	.00	.00	0.	*	1	2225	270	.00	.00	.00	0.
1	1000	121	.00	.00	.00	0.	*	1	2230	271	.00	.00	.00	0.
1	1005	122	.00	.00	.00	0.	*	1	2235	272	.00	.00	.00	0.
1	1010	123	.00	.00	.00	0.	*	1	2240	273	.00	.00	.00	0.
1	1015	124	.00	.00	.00	0.	*	1	2245	274	.00	.00	.00	0.
1	1020	125	.00	.00	.00	0.	*	1	2250	275	.00	.00	.00	0.
1	1025	126	.00	.00	.00	0.	*	1	2255	276	.00	.00	.00	0.
1	1030	127	.00	.00	.00	0.	*	1	2300	277	.00	.00	.00	0.
1	1035	128	.00	.00	.00	0.	*	1	2305	278	.00	.00	.00	0.
1	1040	129	.00	.00	.00	0.	*	1	2310	279	.00	.00	.00	0.
1	1045	130	.00	.00	.00	0.	*	1	2315	280	.00	.00	.00	0.
1	1050	131	.00	.00	.00	0.	*	1	2320	281	.00	.00	.00	0.
1	1055	132	.00	.00	.00	0.	*	1	2325	282	.00	.00	.00	0.
1	1100	133	.00	.00	.00	0.	*	1	2330	283	.00	.00	.00	0.
1	1105	134	.00	.00	.00	0.	*	1	2335	284	.00	.00	.00	0.
1	1110	135	.00	.00	.00	0.	*	1	2340	285	.00	.00	.00	0.
1	1115	136	.00	.00	.00	0.	*	1	2345	286	.00	.00	.00	0.
1	1120	137	.00	.00	.00	0.	*	1	2350	287	.00	.00	.00	0.
1	1125	138	.00	.00	.00	0.	*	1	2355	288	.00	.00	.00	0.
1	1130	139	.00	.00	.00	0.	*	2	0000	289	.00	.00	.00	0.
1	1135	140	.00	.00	.00	0.	*	2	0005	290	.00	.00	.00	0.
1	1140	141	.00	.00	.00	0.	*	2	0010	291	.00	.00	.00	0.
1	1145	142	.00	.00	.00	0.	*	2	0015	292	.00	.00	.00	0.
1	1150	143	.00	.00	.00	0.	*	2	0020	293	.00	.00	.00	0.
1	1155	144	.00	.00	.00	0.	*	2	0025	294	.00	.00	.00	0.
1	1200	145	.00	.00	.00	0.	*	2	0030	295	.00	.00	.00	0.
1	1205	146	.00	.00	.00	0.	*	2	0035	296	.00	.00	.00	0.
1	1210	147	.00	.00	.00	0.	*	2	0040	297	.00	.00	.00	0.
1	1215	148	.00	.00	.00	0.	*	2	0045	298	.00	.00	.00	0.
1	1220	149	.00	.00	.00	0.	*	2	0050	299	.00	.00	.00	0.
1	1225	150	.00	.00	.00	0.	*	2	0055	300	.00	.00	.00	0.

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TOTAL RAINFALL = 3.22, TOTAL LOSS = .22, TOTAL EXCESS = 3.00

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24.92-HR
31.	3.08	2.	1.	0.	0.
		(INCHES)	3.004	3.013	3.013
		(AC-FT)	1.	1.	1.

CUMULATIVE AREA = .91 SQ MI

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717 KK      \*\*\*\*\*  
 \*      33C.2      \*      COMBINE  
 \*      \*      \*  
 \*\*\*\*\*

718 KO      OUTPUT CONTROL VARIABLES  
 IPRINT      1      PRINT CONTROL  
 IPLOT      0      PLOT CONTROL  
 QSCAL      0      HYDROGRAPH PLOT SCALE  
 COMBINED DISCHARGE AT SCOTTSDALE ROAD CULVERT

720 HC      HYDROGRAPH COMBINATION  
 ICOMP      2      NUMBER OF HYDROGRAPHS TO COMBINE

.....

HYDROGRAPH AT STATION      33C.2

SUM OF 2 HYDROGRAPHS

DA	MON	HRMN	GRD	FLOW	*	DA	MON	HRMN	GRD	FLOW	*	DA	MON	HRMN	GRD	FLOW	*	DA	MON	HRMN	GRD	FLOW	*
1		0000	1	0.	*	1		0615	76	9.	*	1		1230	151	0.	*	1		1845	226	0.	*
1		0005	2	0.	*	1		0620	77	8.	*	1		1235	152	0.	*	1		1850	227	0.	*
1		0010	3	0.	*	1		0625	78	7.	*	1		1240	153	0.	*	1		1855	228	0.	*
1		0015	4	0.	*	1		0630	79	6.	*	1		1245	154	0.	*	1		1900	229	0.	*
1		0020	5	0.	*	1		0635	80	5.	*	1		1250	155	0.	*	1		1905	230	0.	*
1		0025	6	0.	*	1		0640	81	5.	*	1		1255	156	0.	*	1		1910	231	0.	*
1		0030	7	0.	*	1		0645	82	4.	*	1		1300	157	0.	*	1		1915	232	0.	*
1		0035	8	0.	*	1		0650	83	4.	*	1		1305	158	0.	*	1		1920	233	0.	*
1		0040	9	0.	*	1		0655	84	3.	*	1		1310	159	0.	*	1		1925	234	0.	*
1		0045	10	0.	*	1		0700	85	2.	*	1		1315	160	0.	*	1		1930	235	0.	*
1		0050	11	0.	*	1		0705	86	2.	*	1		1320	161	0.	*	1		1935	236	0.	*
1		0055	12	0.	*	1		0710	87	2.	*	1		1325	162	0.	*	1		1940	237	0.	*
1		0100	13	1.	*	1		0715	88	2.	*	1		1330	163	0.	*	1		1945	238	0.	*
1		0105	14	1.	*	1		0720	89	2.	*	1		1335	164	0.	*	1		1950	239	0.	*
1		0110	15	2.	*	1		0725	90	1.	*	1		1340	165	0.	*	1		1955	240	0.	*
1		0115	16	2.	*	1		0730	91	1.	*	1		1345	166	0.	*	1		2000	241	0.	*
1		0120	17	2.	*	1		0735	92	1.	*	1		1350	167	0.	*	1		2005	242	0.	*
1		0125	18	3.	*	1		0740	93	1.	*	1		1355	168	0.	*	1		2010	243	0.	*
1		0130	19	3.	*	1		0745	94	1.	*	1		1400	169	0.	*	1		2015	244	0.	*
1		0135	20	3.	*	1		0750	95	1.	*	1		1405	170	0.	*	1		2020	245	0.	*
1		0140	21	3.	*	1		0755	96	1.	*	1		1410	171	0.	*	1		2025	246	0.	*
1		0145	22	4.	*	1		0800	97	1.	*	1		1415	172	0.	*	1		2030	247	0.	*
1		0150	23	4.	*	1		0805	98	1.	*	1		1420	173	0.	*	1		2035	248	0.	*
1		0155	24	4.	*	1		0810	99	0.	*	1		1425	174	0.	*	1		2040	249	0.	*
1		0200	25	5.	*	1		0815	100	0.	*	1		1430	175	0.	*	1		2045	250	0.	*
1		0205	26	5.	*	1		0820	101	0.	*	1		1435	176	0.	*	1		2050	251	0.	*
1		0210	27	5.	*	1		0825	102	0.	*	1		1440	177	0.	*	1		2055	252	0.	*
1		0215	28	6.	*	1		0830	103	0.	*	1		1445	178	0.	*	1		2100	253	0.	*
1		0220	29	6.	*	1		0835	104	0.	*	1		1450	179	0.	*	1		2105	254	0.	*
1		0225	30	6.	*	1		0840	105	0.	*	1		1455	180	0.	*	1		2110	255	0.	*
1		0230	31	7.	*	1		0845	106	0.	*	1		1500	181	0.	*	1		2115	256	0.	*
1		0235	32	9.	*	1		0850	107	0.	*	1		1505	182	0.	*	1		2120	257	0.	*
1		0240	33	11.	*	1		0855	108	0.	*	1		1510	183	0.	*	1		2125	258	0.	*
1		0245	34	14.	*	1		0900	109	0.	*	1		1515	184	0.	*	1		2130	259	0.	*
1		0250	35	17.	*	1		0905	110	0.	*	1		1520	185	0.	*	1		2135	260	0.	*
1		0255	36	21.	*	1		0910	111	0.	*	1		1525	186	0.	*	1		2140	261	0.	*
1		0300	37	33.	*	1		0915	112	0.	*	1		1530	187	0.	*	1		2145	262	0.	*
1		0305	38	48.	*	1		0920	113	0.	*	1		1535	188	0.	*	1		2150	263	0.	*
1		0310	39	59.	*	1		0925	114	0.	*	1		1540	189	0.	*	1		2155	264	0.	*
1		0315	40	103.	*	1		0930	115	0.	*	1		1545	190	0.	*	1		2200	265	0.	*
1		0320	41	114.	*	1		0935	116	0.	*	1		1550	191	0.	*	1		2205	266	0.	*
1		0325	42	109.	*	1		0940	117	0.	*	1		1555	192	0.	*	1		2210	267	0.	*
1		0330	43	100.	*	1		0945	118	0.	*	1		1600	193	0.	*	1		2215	268	0.	*
1		0335	44	89.	*	1		0950	119	0.	*	1		1605	194	0.	*	1		2220	269	0.	*
1		0340	45	77.	*	1		0955	120	0.	*	1		1610	195	0.	*	1		2225	270	0.	*
1		0345	46	64.	*	1		1000	121	0.	*	1		1615	196	0.	*	1		2230	271	0.	*
1		0350	47	52.	*	1		1005	122	0.	*	1		1620	197	0.	*	1		2235	272	0.	*
1		0355	48	45.	*	1		1010	123	0.	*	1		1625	198	0.	*	1		2240	273	0.	*
1		0400	49	38.	*	1		1015	124	0.	*	1		1630	199	0.	*	1		2245	274	0.	*
1		0405	50	32.	*	1		1020	125	0.	*	1		1635	200	0.	*	1		2250	275	0.	*
1		0410	51	28.	*	1		1025	126	0.	*	1		1640	201	0.	*	1		2255	276	0.	*
1		0415	52	25.	*	1		1030	127	0.	*	1		1645	202	0.	*	1		2300	277	0.	*
1		0420	53	22.	*	1		1035	128	0.	*	1		1650	203	0.	*	1		2305	278	0.	*
1		0425	54	20.	*	1		1040	129	0.	*	1		1655	204	0.	*	1		2310	279	0.	*
1		0430	55	19.	*	1		1045	130	0.	*	1		1700	205	0.	*	1		2315	280	0.	*
1		0435	56	18.	*	1		1050	131	0.	*	1		1705	206	0.	*	1		2320	281	0.	*
1		0440	57	18.	*	1		1055	132	0.	*	1		1710	207	0.	*	1		2325	282	0.	*
1		0445	58	18.	*	1		1100	133	0.	*	1		1715	208	0.	*	1		2330	283	0.	*
1		0450	59	17.	*	1		1105	134	0.	*	1		1720	209	0.	*	1		2335	284	0.	*
1		0455	60	17.	*	1		1110	135	0.	*	1		1725	210	0.	*	1		2340	285	0.	*
1		0500	61	16.	*	1		1115	136	0.	*	1		1730	211	0.	*	1		2345	286	0.	*
1		0505	62	16.	*	1		1120	137	0.	*	1		1735	212	0.	*	1		2350	287	0.	*
1		0510	63	16.	*	1		1125	138	0.	*	1		1740	213	0.	*	1		2355	288	0.	*
1		0515	64	15.	*	1		1130	139	0.	*	1		1745	214	0.	*	2		0000	289	0.	*
1		0520	65	15.	*	1		1135	140	0.	*	1		1750	215	0.	*	2		0005	290	0.	*
1		0525	66	15.	*	1		1140	141	0.	*	1		1755	216	0.	*	2		0010	291	0.	*
1		0530	67	14.	*	1		1145	142	0.	*	1		1800	217	0.	*	2		0015	292	0.	*
1		0535	68	14.	*	1		1150	143	0.	*	1		1805	218	0.	*	2		0020	293	0.	*
1		0540	69	13.	*	1		1155	144	0.	*	1		1810	219	0.	*	2		0025	294	0.	*
1		0545	70	13.	*	1		1200	145	0.	*	1		1815	220	0.	*	2		0030	295	0.	*
1		0550	71	12.	*	1		1205	146	0.	*	1		1820	221	0.	*	2		0035	296	0.	*
1		0555	72	12.	*	1		1210	147	0.	*	1		1825	222	0.	*	2		0040	297	0.	*
1		0600	73	11.	*	1		1215	148	0.	*	1		1830	223	0.	*	2		0045	298	0.	*
1		0605	74	11.	*	1		1220	149	0.	*	1		1835	224	0.	*	2		0050	299	0.	*
1		0610	75	10.	*	1		1225	150	0.	*	1		1840	225	0.	*	2		0055	300	0.	*

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
+	(CFS)	(HR)	6-HR	24-HR	72-HR	24-92-HR
+	114.	3.33	22.	6.	5.	5.
			32.144	32.619	32.619	32.619
			11.	11.	11.	11.
			(INCHES)			
			(AC-FT)			
			CUMULATIVE AREA	.01	SQ MI	

1

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS, AREA IN SQUARE MILES

OPERATION	STATION	PEAK FLOW	TIME OF PEAK	AVERAGE FLOW FOR MAXIMUM PERIOD	Basin Area	MAXIMUM STAGE	TIME OF MAX STAGE
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					6-HOUR	24-HOUR	72-HOUR		
+	HYDROGRAPH AT								
+		1A1	44.	3.17	4.	1.	1.	.02	
+	ROUTED TO								
+		DET1A1	12.	3.50	4.	1.	1.	.02	1.73 3.50
+	ROUTED TO								
+		RA1-C4	11.	3.50	4.	1.	1.	.02	.91 3.50
+	HYDROGRAPH AT								
+		1C4	9.	3.17	1.	0.	0.	.00	
+	2 COMBINED AT								
+		CP1C4	15.	3.17	4.	1.	1.	.02	
+	ROUTED TO								
+		RC4-C3	15.	3.25	4.	1.	1.	.02	1.05 3.25
+	HYDROGRAPH AT								
+		1Da3	38.	3.08	3.	1.	1.	.01	
+	ROUTED TO								
+		DE1Da3	3.	3.67	2.	1.	1.	.01	2.51 3.67
+	HYDROGRAPH AT								
+		1Da4	29.	3.08	2.	1.	1.	.01	
+	2 COMBINED AT								
+		CP1Da4	30.	3.08	4.	1.	1.	.02	
+	ROUTED TO								
+		DE1Da4	6.	3.58	4.	1.	1.	.02	3.14 3.58
+	HYDROGRAPH AT								
+		1Da5	7.	3.17	1.	0.	0.	.00	
+	3 COMBINED AT								
+		CP1C3I	25.	3.17	9.	3.	3.	.05	
+	ROUTED TO								
+		RC3-C3	24.	3.25	9.	3.	3.	.05	1.52 3.25
+	HYDROGRAPH AT								
+		Off-1A	21.	3.08	2.	0.	0.	.01	
+	HYDROGRAPH AT								
+		1A2	11.	3.08	1.	0.	0.	.00	
+	HYDROGRAPH AT								
+		1A3	18.	3.08	1.	0.	0.	.01	
+	3 COMBINED AT								
+		CPA3	50.	3.08	4.	1.	1.	.02	
+	ROUTED TO								
+		DET1A3	33.	3.17	4.	1.	1.	.02	2.84 3.17
+	ROUTED TO								
+		RA3-A6	35.	3.25	4.	1.	1.	.02	.60 3.25
+	HYDROGRAPH AT								
+		1A6	12.	3.08	1.	0.	0.	.00	
+	2 COMBINED AT								
+		CP1A6	40.	3.25	5.	1.	1.	.03	
+	ROUTED TO								
+		DET1A6	35.	3.33	5.	1.	1.	.03	2.67 3.33
+	HYDROGRAPH AT								
+		1A5	42.	3.08	4.	1.	1.	.02	
+	2 COMBINED AT								
+		CP1A5	59.	3.25	8.	2.	2.	.04	
+	ROUTED TO								
+		DET1A5	53.	3.33	8.	2.	2.	.04	2.96 3.33
+	HYDROGRAPH AT								
+		1A4	27.	3.08	2.	1.	1.	.01	
+	ROUTED TO								
+		RA4-A7	25.	3.17	2.	1.	1.	.01	.50 3.17
+	ROUTED TO								
+		DET1A4	14.	3.33	2.	1.	1.	.01	2.65 3.33

+	HYDROGRAPH AT	1A7	21.	3.08	2.	0.	0.	.01		
+	3 COMBINED AT	CP1A7	74.	3.34	12.	3.	3.	.06		
+	ROUTED TO	DET1A7	66.	3.42	12.	3.	3.	.06	3.62	3.42
+	HYDROGRAPH AT	1C1	57.	3.17	5.	1.	1.	.02		
+	2 COMBINED AT	CP1C1	85.	3.33	17.	4.	4.	.08		
+	ROUTED TO	DET1C1	78.	3.50	16.	4.	4.	.08	4.86	3.50
+	HYDROGRAPH AT	1C2	54.	3.17	5.	1.	1.	.02		
+	2 COMBINED AT	CP1C2	92.	3.50	21.	6.	5.	.11		
+	ROUTED TO	DE1C2A	93.	3.50	21.	6.	5.	.11	5.05	3.50
+	ROUTED TO	DE1C2B	90.	2.50	21.	6.	5.	.11	5.02	3.50
+	ROUTED TO	DE1C2C	92.	3.50	21.	6.	5.	.11	5.04	2.50
+	HYDROGRAPH AT	1C3	68.	3.08	5.	1.	1.	.03		
+	3 COMBINED AT	CP1C3	128.	3.50	33.	10.	9.	.19		
+	ROUTED TO	DET1C3	109.	3.67	33.	10.	9.	.19	2.55	3.67
+	ROUTED TO	RC3COM	108.	3.67	33.	10.	9.	.19	11.14	3.67
+	HYDROGRAPH AT	COMM	110.	3.08	10.	2.	2.	.03		
+	ROUTED TO	DETCOM	11.	3.67	7.	2.	2.	.03	2.55	3.67
+	2 COMBINED AT	CPCOM	119.	3.67	41.	12.	12.	.22		
+	ROUTED TO	COMOF1	119.	3.75	41.	12.	12.	.22	11.20	3.75
+	HYDROGRAPH AT	CPE1	84.	3.08	6.	2.	2.	.02		
+	ROUTED TO	DEOFF1	11.	3.50	6.	2.	2.	.02	2.61	3.50
+	2 COMBINED AT	CPOFF1	130.	3.75	46.	14.	13.	.24		
+	ROUTED TO	OF1OF3	129.	3.75	46.	14.	13.	.24	11.31	3.75
+	HYDROGRAPH AT	OFF3	58.	3.08	5.	1.	1.	.02		
+	ROUTED TO	DEOFF3	10.	3.50	5.	1.	1.	.02	2.20	3.50
+	2 COMBINED AT	CPOFF3	138.	3.75	51.	15.	14.	.25		
+	ROUTED TO	33A1	137.	3.83	51.	15.	14.	.25		
+	HYDROGRAPH AT	33A	213.	3.08	17.	4.	4.	.05		
+	2 COMBINED AT	33A3	232.	3.08	65.	19.	19.	.41		
+	HYDROGRAPH AT	1DB	104.	3.08	8.	2.	2.	.04		

[illegible]

+		DET1K	18.	3.75	11.	7.	3.	.05		
+									2.77	3.75
+	2 COMBINED AT	1K1.2	132.	3.50	57.	17.	16.	.28		
+	ROUTED TO	1M1.1	132.	3.50	57.	17.	16.	.28		
+	HYDROGRAPH AT	1M1	152.	3.17	14.	4.	3.	.05		
+	ROUTED TO	DET1M	49.	3.42	13.	4.	3.	.05		
+									3.70	3.42
+	2 COMBINED AT	1M1.2	178.	3.50	70.	20.	20.	.34		
+	HYDROGRAPH AT	33E	160.	3.08	12.	3.	3.	.04		
+	HYDROGRAPH AT	335E	3.	3.17	0.	0.	0.	.00		
+	3 COMBINED AT	33E.2	225.	3.17	81.	24.	23.	.38		
+	ROUTED TO	R33E.2	224.	3.17	81.	24.	23.	.38		
+	HYDROGRAPH AT	33D	61.	3.17	5.	1.	1.	.04		
+	HYDROGRAPH AT	S40ET	76.	3.08	6.	1.	1.	.02		
+	3 COMBINED AT	CT13.0	340.	3.17	92.	26.	25.	.43		
+	DIVERSION TO	P_ADOT	223.	3.17	82.	24.	23.	.43		
+	HYDROGRAPH AT	D_ADOT	117.	3.17	10.	3.	2.	.43		
+	HYDROGRAPH AT	33C	126.	3.08	9.	2.	2.	.03		
+	HYDROGRAPH AT	S40CN	180.	3.08	14.	4.	3.	.04		
+	3 COMBINED AT	CT13.1	353.	3.08	34.	8.	8.	.51		
+	DIVERSION TO	P-PIPE	30.	3.09	13.	3.	3.	.51		
+	HYDROGRAPH AT	D_BAS	363.	3.08	21.	5.	5.	.51		
+	DIVERSION TO	D-BAS2	69.	3.08	2.	1.	0.	.51		
+	HYDROGRAPH AT	D_BAS1	363.	3.09	19.	5.	5.	.51		
+	DIVERSION TO	D-SUBF	237.	3.17	4.	1.	1.	.51		
+	HYDROGRAPH AT	D_SURF	309.	3.17	15.	4.	4.	.51		
+	HYDROGRAPH AT	B_PIPE	30.	2.75	13.	3.	3.	.00		
+	HYDROGRAPH AT	B_SURF	69.	3.00	2.	1.	0.	.00		
+	3 COMBINED AT	CS40B	339.	3.17	30.	7.	7.	.51		
+	ROUTED TO	S40BAS	159.	3.33	29.	7.	7.	.51		
+									5.52	3.33
+	DIVERSION TO	D33C.2	108.	3.33	20.	5.	5.	.51		
+	HYDROGRAPH AT	P33E.1	51.	3.33	9.	2.	2.	.51		
+	HYDROGRAPH AT	R_ADOT	223.	3.17	82.	24.	23.	.00		
+	2 COMBINED AT	33E.1	256.	3.25	91.	26.	25.	.51		
+	ROUTED TO	R33E.1	222.	3.33	91.	26.	25.	.51		

ROUTED TO	ASJDR1	252.	3.33	91.	26.	25.	.51
HYDROGRAPH AT	ASLD	114.	3.08	10.	2	2.	.03
2 COMBINED AT	ASLDC	317.	3.17	100.	29.	28.	.54
ROUTED TO	ASLDR2	309.	3.25	100.	29.	28.	.54
HYDROGRAPH AT	ASLD	84.	3.08	6.	1.	1.	.02
2 COMBINED AT	CPPRIN	351.	3.17	105.	30.	29.	.56
HYDROGRAPH AT	R33C.2	106.	3.33	20.	5.	5.	.00
HYDROGRAPH AT	S40WT	31.	3.08	2.	1.	0.	.01
2 COMBINED AT	33C.2	114.	3.33	22.	6.	5.	.01

SUMMARY OF KINEMATIC WAVE - MUSKINGUM-CUNGE ROUTING  
(FLOW IS DIRECT RUNOFF WITHOUT BASE FLOW)

1STAQ	ELEMENT	DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	INTERPOLATED TO COMPUTATION INTERVAL			
						DT (MIN)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)
33A1	MANE	1.88	138.05	228.99	2.21	5.00	137.32	230.00	2.21
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2975E+02 EXCESS= .0000E+00 OUTFLOW= .2974E+02 BASIN STORAGE= .7425E-02 PERCENT ERROR= .0									
33A	MANE	.94	229.59	186.25	2.93	5.00	213.27	185.00	2.93
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .8419E+01 OUTFLOW= .8424E+01 BASIN STORAGE= .3781E-03 PERCENT ERROR= -.1									
1KE.1	MANE	.88	115.21	210.94	2.20	5.00	115.14	210.00	2.20
CONTINUITY SUMMARY (AC-FT) - INFLOW= .2702E+02 EXCESS= .0000E+00 OUTFLOW= .2702E+02 BASIN STORAGE= .3402E-02 PERCENT ERROR= .0									
1ME.1	MANE	1.04	132.38	212.01	2.22	5.00	131.65	210.00	2.22
CONTINUITY SUMMARY (AC-FT) - INFLOW= .3341E+02 EXCESS= .0000E+00 OUTFLOW= .3341E+02 BASIN STORAGE= .5096E-02 PERCENT ERROR= .0									
33E	MANE	1.58	168.66	186.51	2.90	5.00	159.64	185.00	2.91
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .6117E+01 OUTFLOW= .6111E+01 BASIN STORAGE= .8650E-04 PERCENT ERROR= .1									
33BE	MANE	3.45	3.22	190.32	2.78	5.00	3.18	190.00	2.78
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1633E+00 OUTFLOW= .1630E+00 BASIN STORAGE= .1193E-04 PERCENT ERROR= .2									
R33E.2	MANE	.67	224.58	190.57	2.34	5.00	224.36	190.00	2.34
CONTINUITY SUMMARY (AC-FT) - INFLOW= .4687E+02 EXCESS= .0000E+00 OUTFLOW= .4687E+02 BASIN STORAGE= .1478E-02 PERCENT ERROR= .0									
33D	MANE	2.02	64.29	192.41	1.22	5.00	61.02	190.00	1.22
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2639E+01 OUTFLOW= .2627E+01 BASIN STORAGE= .1983E-03 PERCENT ERROR= .5									
S40ET	MANE	.85	79.65	186.49	2.94	5.00	76.00	185.00	2.95
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2673E+01 OUTFLOW= .2671E+01 BASIN STORAGE= .1120E-03 PERCENT ERROR= .0									
33C	MANE	.51	129.46	185.80	2.96	5.00	125.66	185.00	2.97
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4678E+01 OUTFLOW= .4675E+01 BASIN STORAGE= .1952E-03 PERCENT ERROR= .1									
S40CN	MANE	.57	187.23	186.05	2.96	5.00	179.92	185.00	2.97
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .7080E+01 OUTFLOW= .7077E+01 BASIN STORAGE= .4086E-03 PERCENT ERROR= .0									

R33E.1	MANE	1.31	255.16	197.67	1.92	5.00	252.31	200.00	1.92
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5206E+02 EXCESS= .0000E+00 OUTFLOW= .5208E+02 BASIN STORAGE= .7950E-02 PERCENT ERROR= .0									
ASLDR1	MANE	.56	252.12	200.80	1.92	5.00	251.99	200.00	1.92
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5206E+02 EXCESS= .0000E+00 OUTFLOW= .5205E+02 BASIN STORAGE= .6142E-02 PERCENT ERROR= .0									
ASLD	MANE	.64	123.54	186.54	2.38	5.00	114.18	185.00	2.39
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .4844E+01 OUTFLOW= .4845E+01 BASIN STORAGE= .3741E-03 PERCENT ERROR= .0									
ASLDR2	MANE	.72	316.25	191.53	1.97	5.00	308.60	195.00	1.97
CONTINUITY SUMMARY (AC-FT) - INFLOW= .5692E+02 EXCESS= .0000E+00 OUTFLOW= .5692E+02 BASIN STORAGE= .5511E-02 PERCENT ERROR= .0									
ASLD	MANE	.36	84.72	185.20	2.78	5.00	84.18	185.00	2.80
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .2365E+01 OUTFLOW= .2863E+01 BASIN STORAGE= 7801E-04 PERCENT ERROR= .1									
S40WT	MANE	.33	31.72	184.75	3.00	5.00	31.47	185.00	3.01
CONTINUITY SUMMARY (AC-FT) - INFLOW= .0000E+00 EXCESS= .1909E+01 OUTFLOW= .1008E+01 BASIN STORAGE= .4454E-05 PERCENT ERROR= .1									

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1A1  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1	INITIAL VALUE			SPILLWAY CREST		TOP OF DAM		
		ELEVATION							
		STORAGE	0.		3.00		3.00		
		OUTFLOW	0.		2.		2.		
			0.		20.		20.		
		RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	1.73	.00	1.	12.	.00	3.50	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELDa3 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									

PLAN	1	INITIAL VALUE			SPILLWAY CREST		TOP OF DAM		
		ELEVATION							
		STORAGE	0.		3.00		3.00		
		OUTFLOW	0.		1.		1.		
			0.		4.		4.		
		RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.51	.00	1.	3.	.00	3.67	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELDa4 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									

PLAN	1	INITIAL VALUE			SPILLWAY CREST		TOP OF DAM		
		ELEVATION							
		STORAGE	0.		3.00		3.00		
		OUTFLOW	0.		1.		1.		
			0.		4.		4.		
		RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	3.14	.14	1.	6.	1.42	3.58	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1A3 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									

PLAN	1	INITIAL VALUE			SPILLWAY CREST		TOP OF DAM		
		ELEVATION							
		STORAGE	0		2.50		2.50		
		OUTFLOW	0.		0.		0.		
			0.		22.		22.		
		RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.84	.34	0.	33.	.25	3.17	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1A6 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									



PLAN	1	INITIAL VALUE		SPILLWAY CREST		TOP OF DAM			
		ELEVATION	.00	2.50	2.50				
		STORAGE	0.	0.	0.				
		OUTFLOW	0.	22.	22.				
		RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.87	.37	0.	35.	.43	3.33	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1A5 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									
PLAN	1	INITIAL VALUE		SPILLWAY CREST		TOP OF DAM			
		ELEVATION	.00	2.50	2.50				
		STORAGE	0.	1.	1.				
		OUTFLOW	0.	34.	34.				
		RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.96	.46	1.	53.	.33	3.33	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1A4 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									
PLAN	1	INITIAL VALUE		SPILLWAY CREST		TOP OF DAM			
		ELEVATION	.00	2.50	2.50				
		STORAGE	0.	0.	0.				
		OUTFLOW	0.	11.	11.				
		RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.65	.15	0.	14.	.17	3.33	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1A7 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									
PLAN	1	INITIAL VALUE		SPILLWAY CREST		TOP OF DAM			
		ELEVATION	.00	2.50	2.50				
		STORAGE	0.	1.	1.				
		OUTFLOW	0.	11.	11.				
		RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	3.62	1.12	1.	66.	1.50	3.42	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1C1 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									
PLAN	1	INITIAL VALUE		SPILLWAY CREST		TOP OF DAM			
		ELEVATION	.00	3.60	3.60				
		STORAGE	0.	2.	2.				
		OUTFLOW	0.	14.	14.				
		RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	4.86	1.26	2.	78.	1.83	3.50	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1C2A (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									
PLAN	1	INITIAL VALUE		SPILLWAY CREST		TOP OF DAM			
		ELEVATION	.00	3.60	3.60				
		STORAGE	0.	0.	0.				
		OUTFLOW	0.	14.	14.				
		RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	5.05	1.45	1.	93.	2.75	3.50	.00	
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1C2B (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)									
PLAN	1	INITIAL VALUE		SPILLWAY CREST		TOP OF DAM			
		ELEVATION	.00	3.60	3.60				
		STORAGE	0.	1.	1.				
		OUTFLOW	0.	14.	14.				
		RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	5.02	1.42	1.	90.	2.92	3.50	.00	

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELC2C  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	ELEVATION	.00	3.60	3.60
	STORAGE	0.	1.	1.
	OUTFLOW	0.	14.	14.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	5.04	1.44	1.	92.	3.00	3.50	.00

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1C3  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	ELEVATION	.00	3.50	3.50
	STORAGE	0.	1.	1.
	OUTFLOW	0.	150.	150.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	2.55	.00	1.	109.	.00	3.67	.00

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETCOM  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	ELEVATION	.00	3.00	3.00
	STORAGE	0.	4.	4.
	OUTFLOW	0.	13.	13.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	2.55	.00	3.	11.	.00	3.67	.00

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEOFF1  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	ELEVATION	.00	3.00	3.00
	STORAGE	0.	2.	2.
	OUTFLOW	0.	13.	13.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	2.61	.00	2.	11.	.00	3.50	.00

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEOFF3  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	ELEVATION	.00	3.00	3.00
	STORAGE	0.	2.	2.
	OUTFLOW	0.	13.	13.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	2.20	.00	2.	10.	.00	3.50	.00

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELDB  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	ELEVATION	.00	3.00	3.00
	STORAGE	0.	3.	3.
	OUTFLOW	0.	13.	13.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	2.99	.00	3.	13.	.00	3.53	.00

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELDd1  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 .....		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	ELEVATION	.00	3.00	3.00
	STORAGE	0.	1.	1.
	OUTFLOW	0.	4.	4.

RATIO	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM	DURATION	TIME OF	TIME OF
-------	---------	---------	---------	---------	----------	---------	---------

	OF PMF	RESERVOIR W.S.ELEV	DEPTH OVER DAM	STORAGE AC-FT	OUTFLOW CFS	OVER TOP HOURS	MAX OUTFLOW HOURS	FAILURE HOURS
1	1.00	2.95	.00	1.	4.	.00	3.50	.00
	SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DE1Ea1 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)							
PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	.00	3.00	3.00			
		STORAGE	0.	2.	2.			
		OUTFLOW	0.	4.	4.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.81	.00	1.	4.	.00	3.75	.00
	SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DE1Ea2 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)							
PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	.00	3.00	3.00			
		STORAGE	0.	2.	2.			
		OUTFLOW	0.	10.	10.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	3.25	.25	2.	16.	.67	3.50	.00
	SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETSCH (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)							
PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	.00	3.00	3.00			
		STORAGE	0.	1.	1.			
		OUTFLOW	0.	13.	13.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.84	.00	1.	12.	.00	3.42	.00
	SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DE1E3 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)							
PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	.00	3.00	3.00			
		STORAGE	0.	1.	1.			
		OUTFLOW	0.	11.	11.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.47	.00	1.	9.	.00	3.33	.00
	SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1E5 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)							
PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	.00	3.00	3.00			
		STORAGE	0.	5.	5.			
		OUTFLOW	0.	52.	52.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.26	.00	4.	39.	.00	3.50	.00
	SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEOFF2 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)							
PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	.00	3.00	3.00			
		STORAGE	0.	5.	5.			
		OUTFLOW	0.	13.	13.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1	1.00	2.59	.00	4.	11.	.00	3.67	.00
	SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1K (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)							
PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
		ELEVATION	.00	3.00	3.00			
		STORAGE	0.	5.	5.			

	OUTFLOW	0.	20.	20.			
RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	2.77	.00	4.	18.	.00	3.75	.00
SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETIM							
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)							

PLAN 1 .....		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	ELEVATION	.00	3.00	3.00			
	STORAGE	0.	3.	3.			
	OUTFLOW	0.	20.	20.			

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1.00	3.70	.70	4.	49.	.83	3.42	.00

\*\*\* NORMAL END OF HEC-1 \*\*\*

***Appendix D***

**Hydraulic/Hydrology Calculations**

CP	Sub-basins	A	Cw	L	HP	LP	S	Kb-cls	m	b	Kb	Init Tc	Cw1	Tc,clc1	Tc,tot1	i1	Q1	Cw2	Tc,clc2	Tc,tot2	i2	Q2
Hide/Unhide as applicable ----->												<----- Hide/Unhide as applic ----->										

## Peak Flow Calculations Using The Rational Method

Project: Optima McDowell Mountain Village  
 Proj #:   
 Date: 2/23/22  
 Prep by: DJH  
 Check by: MLD

Base Sheet Prepared By GA, Version 2

Source of Rainfall Data --->NOAA Atlas 14

Rainfall Depth-Duration-Frequency (D-D-F), (inch)					
Storm Frequency	Time				
	5 min	10 min	15 min	30 min	60 min
10-Yr	0.42	0.63	0.78	1.05	1.30
100-Yr	0.65	0.99	1.23	1.66	2.05
Derived Rainfall Intensity-Duration-Frequency (I-D-F), (in/hr)					
10-Yr	4.98	3.79	3.13	2.10	1.30
100-Yr	7.81	5.95	4.92	3.32	2.05

AF for Cw per Cw <sub>10-Yr</sub>		
Freq.	Typical	Applic.
2-Yr	1.00	1.00
5-Yr	1.00	1.00
10-Yr	1.00	1.00
25-Yr	1.10	1.00
50-Yr	1.20	1.00
100-Yr	1.25	1.00

AF=Frequency Adjustment Factor

Attach source and supporting data for rainfall depths

Drainage Area ID: -----							Tc,calc method: 1=Papadakis and Kazan, 2=Avg Veloc.					10-Yr				100-Yr						
							1	Tc,calc=11.4*L^0.5*Kb^0.52*S^0.31*i^-0.38				Cw for each frequency is adjusted as a function of the 100-year value per the table above										
Concent. Point #	Contributing Sub-basins	Total Area (ac)	Base Cw (2-10 yr)	Flow Path, L (ft)	Approx High pt (ft)	Approx Low pt (ft)	Average Slope ft/ft	K <sub>b</sub> Class A-->D	m	b	K <sub>b</sub>	Initial/lot Tc (min)	Minim allowed Tc,tot = 10.0				Q 10-Yr (cfs)	Minim allowed Tc,tot = 10.0				Q 100-Yr (cfs)
													Cw AF=1.00	Tc,calc (min)	Tc,tot (min)	i (in/hr)		Cw AF=1.00	Tc,calc (min)	Tc,tot (min)	i (in/hr)	
Pre v Post	1	15.64	0.50	1306.2	1600.00	1593.0	0.0150	A	-0.00625	0.04	0.0325	10	0.50	8.5	18.5	2.92	22.9	0.50	6.9	16.9	4.81	37.6
100-Yr 2-Hr	1	15.64	0.95	1306	1600	1593	0.0150	A	-0.00625	0.04	0.0325	10	0.95	8.5	18.5	2.92	43.4	0.95	6.9	16.9	4.81	71.5
								A	-0.00625	0.04	#NUM!	0		#####	#NUM!	#NUM!	#####		#####	#####	#NUM!	#####
								A	-0.00625	0.04	#NUM!	0		#####	#NUM!	#NUM!	#####		#####	#####	#NUM!	#####
								A	-0.00625	0.04	#NUM!	0		#####	#NUM!	#NUM!	#####		#####	#####	#NUM!	#####
								A	-0.00625	0.04	#NUM!	0		#####	#NUM!	#NUM!	#####		#####	#####	#NUM!	#####

Point precipitation frequency estimates (inches)

NOAA Atlas 14 Volume 1 Version 5

Data type: Precipitation depth

Time series type: Partial duration

Project area: Southwest

Location n: Arizona USA

Station Name: -

Latitude: 33.6562°

Longitude: -111.9232°

Elevation (USGS): 1594.27 ft

PRECIPITATION FREQUENCY ESTIMATES

by duration:	1	2	5	10	25	50	100	200	500
5-min:	0.196	0.256	0.346	0.415	0.507	0.578	0.651	0.724	0.822
10-min:	0.299	0.39	0.526	0.631	0.772	0.88	0.991	1.1	1.25
15-min:	0.37	0.483	0.652	0.782	0.957	1.09	1.23	1.37	1.55
30-min:	0.498	0.651	0.878	1.05	1.29	1.47	1.66	1.84	2.09
60-min:	0.617	0.805	1.09	1.3	1.6	1.82	2.05	2.28	2.59
2-hr:	0.72	0.931	1.24	1.48	1.8	2.04	2.3	2.55	2.89
3-hr:	0.794	1.02	1.33	1.58	1.92	2.2	2.48	2.78	3.19
6-hr:	0.956	1.21	1.54	1.81	2.17	2.45	2.74	3.04	3.45
12-hr:	1.08	1.36	1.72	1.99	2.37	2.66	2.96	3.26	3.66
24-hr:	1.26	1.6	2.07	2.44	2.96	3.37	3.8	4.25	4.88
2-day:	1.37	1.74	2.28	2.71	3.31	3.78	4.29	4.81	5.54
4-day:	1.57	2	2.66	3.18	3.94	4.55	5.21	5.92	6.92
7-day:	1.77	2.27	3.01	3.61	4.48	5.18	5.93	6.74	7.88
10-day:	1.92	2.46	3.26	3.91	4.83	5.57	6.37	7.21	8.41
20-day:	2.39	3.07	4.06	4.82	5.85	6.65	7.48	8.32	9.47
30-day:	2.8	3.61	4.77	5.66	6.86	7.78	8.74	9.72	11
45-day:	3.27	4.22	5.58	6.59	7.95	8.97	10	11.1	12.5
60-day:	3.63	4.7	6.19	7.29	8.73	9.81	10.9	12	13.4

Date/time (GMT): Wed Feb 23 23:39:34 2022

pyRunTime: 0.0254480838776

***Appendix E***

**Contextual Aerial Plan**

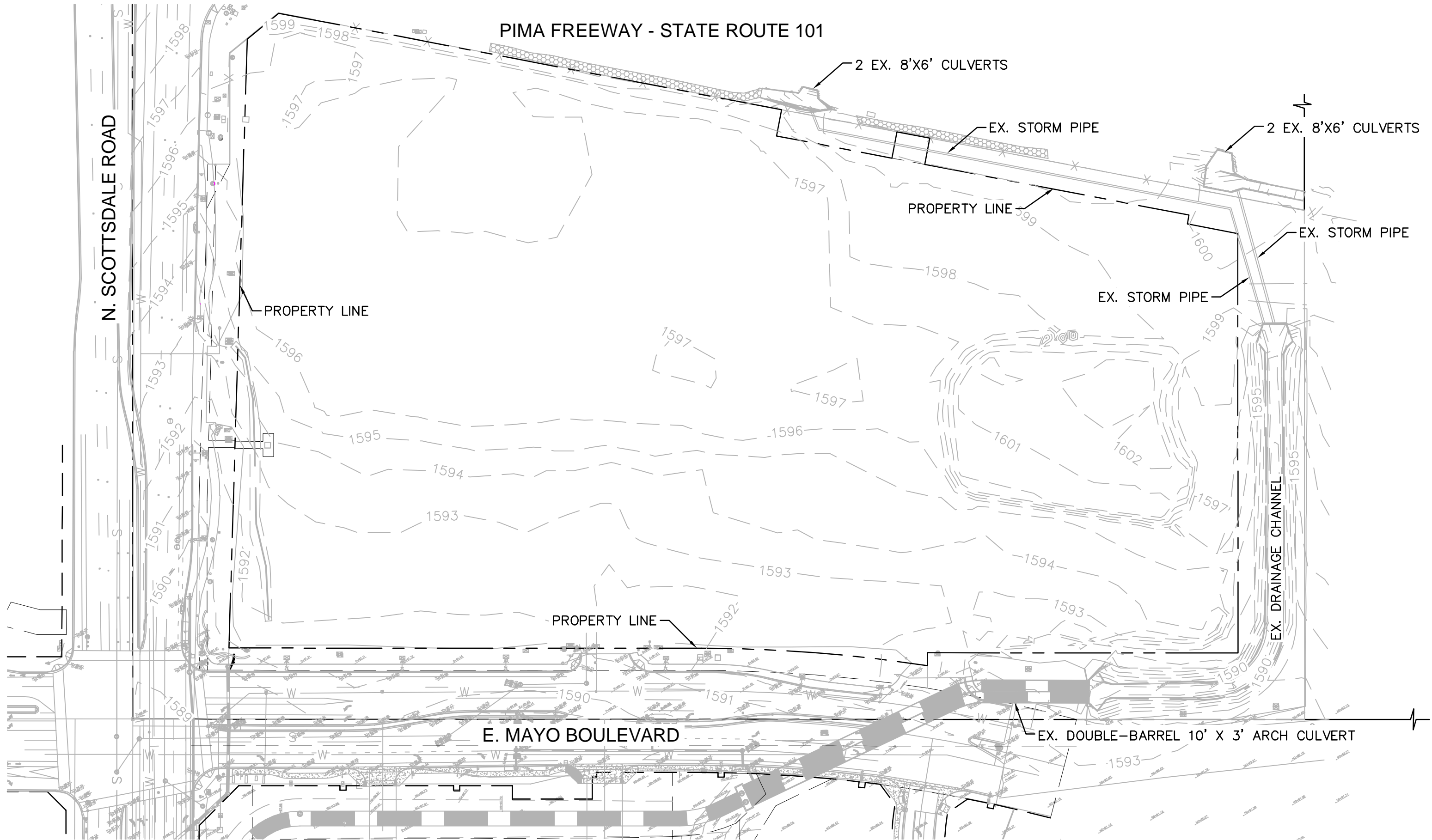




***Appendix F***

Existing Conditions Topographic Map





***Appendix G***

**Preliminary Grading and Drainage Plan**



**CIVIL ENGINEER**  
KIMLEY-HORN AND ASSOCIATES, INC.  
7740 N. 16TH STREET, SUITE 300  
PHOENIX, AZ 85020  
PH: (602) 944-5500  
CONTACT: MIKE DELMARTER, PE

**ARCHITECT**  
OPTIMA  
7157 E. RANCHO VISTA DRIVE #109  
SCOTTSDALE, AZ 85251  
PH: (480) 874-9900  
CONTACT: TJ LENICK

**LAND SURVEYOR**  
ATWELL  
4700 E. SOUTHERN AVE.  
MESA, AZ 85206  
PH: (480) 218-8831  
CONTACT: J. RICHARDSON

**GENERAL NOTES**

1. ADD 0.5 TO PAVEMENT ELEVATIONS FOR TOP OF CURB ELEVATION, UNLESS OTHERWISE NOTED.
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6. CONTRACTOR TO COORDINATE LIGHTING CONDUIT LOCATIONS, TYPE, ETC. WITH LANDSCAPE ARCHITECT/ELECTRICIAN PRIOR TO SITE GRADING AND PAVEMENT/CONCRETE CONSTRUCTION.

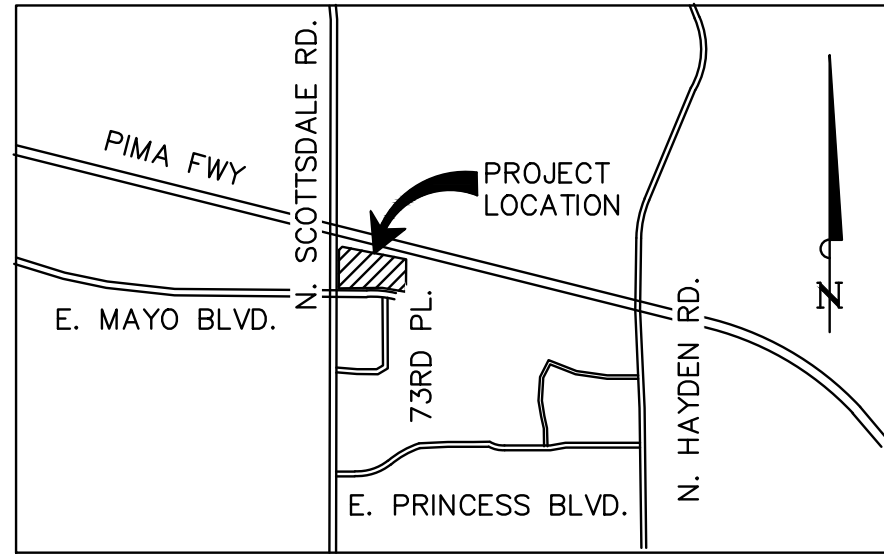
**PRELIMINARY GRADING AND DRAINAGE NOTES**

- ① PROPOSED AREA DRAIN, CONNECT TO GARAGE SYSTEM BELOW.
- ② PROPOSED CATCH BASIN.

Optima McDowell Mountain Village - Pre vs Post								
Drainage Area	Land Use	Area [A]		Runoff Coefficient [C]	Precipitation Depth [P]	Required Storage (V <sub>REQ</sub> = CPA/12)		Retention Basin
		sf	ac			cf	ac-ft	
Building Footprint	Building	681,146	15.637	0.45	2.30	58,749	1.349	1
<b>TOTAL</b>	-	<b>681,146</b>	<b>15.637</b>	-	-	<b>58,749</b>	<b>1.349</b>	-

Underground Retention Summary			
Scenario	Required Volume	Provided Storage	As-Built Volume
	cf	cf	cf
Pre vs Post	58,749	59,400	

Drywell Summary				
Scenario	Volume	Percolation Rate	Drywells Required	Drain Time
	cf	cfs	ea	hr
Pre vs Post	58,749	0.10	5	33



VICINITY MAP  
N.T.S.

**LEGEND**

- PROPERTY LINE
- RIGHT OF WAY LINE
- STREET CENTERLINE
- EASEMENT LINE
- S --- EXISTING SEWER MAIN
- W --- EXISTING PUBLIC WATER MAIN
- W --- PROPOSED WATER MAIN
- S --- PROPOSED SEWER MAIN
- EXISTING STORM DRAIN
- 12 --- PROPOSED CONTOUR
- 2 --- EXISTING CONTOURS
- 50.00 --- PROPOSED PAVEMENT SPOT ELEVATION
- IC=49.88 --- EXISTING SPOT ELEVATION
- G=49.55 --- EXISTING SANITARY SEWER MANHOLE
- HP --- EXISTING FIRE HYDRANT
- HP --- PROPOSED CATCH BASIN
- HP --- SURFACE FLOW DIRECTION
- HP --- EXISTING STORM DRAIN MANHOLE
- HP --- PROPOSED CONCRETE BIKE PATH
- HP --- PROPOSED PAVER WALKWAY
- HP --- PROPOSED GRID LINE

**FLOOD INFORMATION**

ACCORDING TO THE FLOOD INSURANCE RATE MAP #04013C1320 L, DATED OCTOBER 16, 2013, THIS PROPERTY IS LOCATED IN FLOOD ZONE "AO". AREAS SUBJECT TO INUNDATION BY 1-PERCENT-ANNUAL-CHANCE SHALLOW FLOODING (USUALLY SHEET FLOOD ON SLOPING TERRAIN) WHERE AVERAGE DEPTHS ARE BETWEEN ONE AND THREE FEET. AVERAGE FLOOD DEPTHS DERIVED FROM DETAILED HYDRAULIC ANALYSES ARE SHOWN IN THIS ZONE. MANDATORY FLOOD INSURANCE PURCHASE REQUIREMENTS AND FLOODPLAIN MANAGEMENT STANDARDS APPLY.

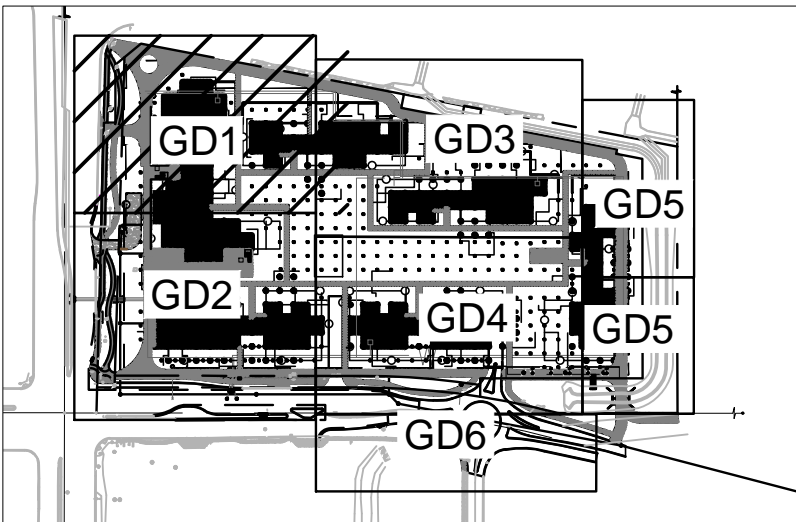
SOME ZONE "AO" HAVE BEEN DESIGNATED IN AREAS WITH HIGH FLOOD VELOCITIES SUCH AS ALLUVIAL FANS AND WASHES. COMMUNITIES ARE ENCOURAGED TO ADOPT MORE RESTRICTIVE REQUIREMENTS FOR THESE AREAS.

**DRAINAGE STATEMENT**

THE EXISTING SITE CONSISTS OF DESERT VEGETATION THAT GENERALLY FLOWS FROM NORTH TO SOUTH. THE PROJECT LOT IS VACANT AND OCCASIONALLY USED FOR EXTENDED PARKING.

THE PROPOSED DESIGN CAPTURES STORM WATER GENERATED ON SITE WITH STORM DRAINS AT THE SURFACE LEVEL OF THE BUILDING AND DROPS THE DRAINAGE DIRECTLY DOWN TO THE GARAGE LEVEL WHERE IT IS CONVEYED TO THE PROPOSED RETENTION TANK AT THE SOUTHEAST CORNER OF THE GARAGE LOWER LEVEL. PRE VS POST RETENTION IS PROVIDED IN THE TANK WHICH THEN OUTLETS AT AN ELEVATION OF 1592.51' AT THE SOUTHEAST CORNER OF THE GARAGE INTO THE EXISTING DRAINAGE CHANNEL. THE ULTIMATE SITE OUTFALL IS LOCATED AT THE SOUTH EAST EDGE OF THE SITE AT AN ELEVATION OF 1586.03'.

THIS SITE IS CURRENTLY LOCATED IN FLOOD ZONE 'AO' BUT IS CURRENTLY GOING THROUGH AN APPROVAL WITH FEMA TO BE REMOVED FROM THE FLOODPLAIN COMPLETELY. 600 CFS OF OFF-SITE FLOWS PASS THROUGH THE SITE ON THE EASTERN BOUNDARY IN AN EXISTING DRAINAGE CHANNEL. THE ULTIMATE SITE OUTFALL IS LOCATED AT THE SOUTH EAST EDGE OF THE SITE AT AN ELEVATION OF 1586.03'.



KEY MAP  
N.T.S.

Q.S.#: 39-45

**Kimley»Horn**

OPTIMA MCDOWELL MOUNTAIN VILLAGE  
PRELIMINARY GRADING AND DRAINAGE PLAN

FOR REVIEW ONLY  
NOT FOR CONSTRUCTION PURPOSES  
**Kimley»Horn**  
ENGINEER MIKE DELMARTER  
PE NO. 30886 DATE 09/23/22

PROJECT NO.  
191007011  
DRAWING NAME  
GD1



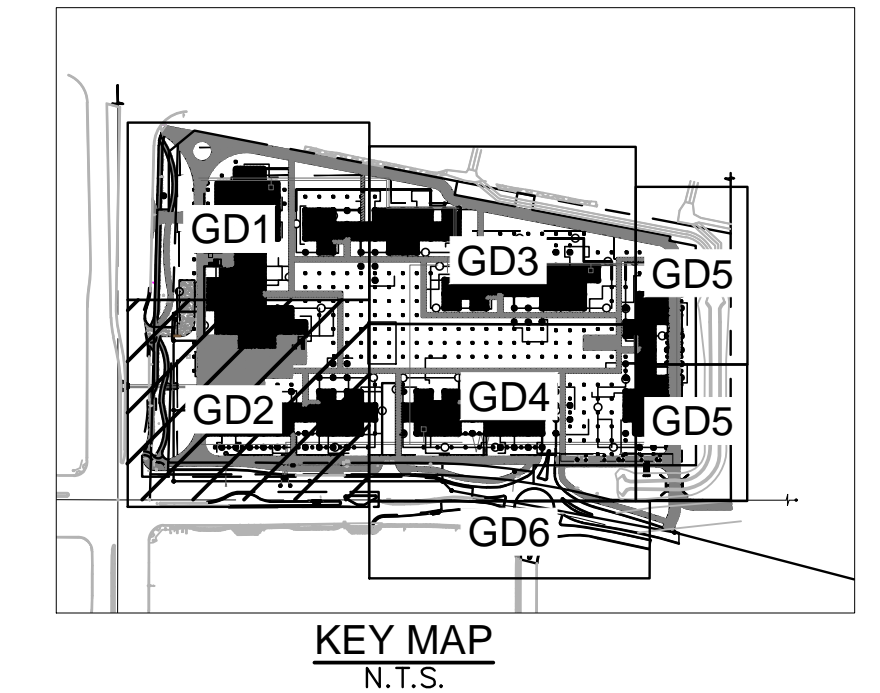
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**LEGEND**

- PROPERTY LINE
- RIGHT OF WAY LINE
- STREET CENTERLINE
- EASEMENT LINE
- EXISTING SEWER MAIN
- EXISTING PUBLIC WATER MAIN
- PROPOSED WATER MAIN
- PROPOSED SEWER MAIN
- EXISTING STORM DRAIN
- PROPOSED CONTOUR
- EXISTING CONTOURS
- PROPOSED PAVEMENT SPOT ELEVATION
- EXISTING SPOT ELEVATION
- EXISTING SANITARY SEWER MANHOLE
- EXISTING FIRE HYDRANT
- PROPOSED CATCH BASIN
- SURFACE FLOW DIRECTION
- EXISTING STORM DRAIN MANHOLE
- PROPOSED CONCRETE BIKE PATH
- PROPOSED PAVER WALKWAY
- PROPOSED GRID LINE

- GENERAL NOTES**
- ADD 0.5 TO PAVEMENT ELEVATIONS FOR TOP OF CURB ELEVATION, UNLESS OTHERWISE NOTED.
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- PRELIMINARY GRADING AND DRAINAGE NOTES**
- PROPOSED AREA DRAIN, CONNECT TO GARAGE SYSTEM BELOW.
  - PROPOSED CATCH BASIN.



**GRAPHIC SCALE IN FEET**  
0 10 20 40

**ARIZONA811**  
Contact Arizona 811 at least two full working days before you begin excavation  
Call 811 or click Arizona811.com

**Kimley»Horn**  
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7740 North 16th Street, Suite 300  
Phoenix, Arizona 85020 (602) 944-5500

**OPTIMA MCDOWELL MOUNTAIN VILLAGE**  
**PRELIMINARY GRADING AND DRAINAGE PLAN**  
**SCOTTSDALE, ARIZONA 85255**

**PRELIMINARY**  
NOT FOR CONSTRUCTION PURPOSES  
**Kimley»Horn**  
DRAWN BY: DJH  
CHECKED BY: MLD  
DATE: SEP 2022  
PROJECT NO. 191007011  
DRAWING NAME GD2  
2 OF 7

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DWG: 191007011.dwg  
DATE: 09/02/22  
BY: DJH  
CHECKED BY: MLD  
DATE: 09/02/22



\_\_\_\_\_

3 OF 7

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Phoenix, Arizona 85020 (602) 944-5500

REVISION	BY	DATE	APPR.
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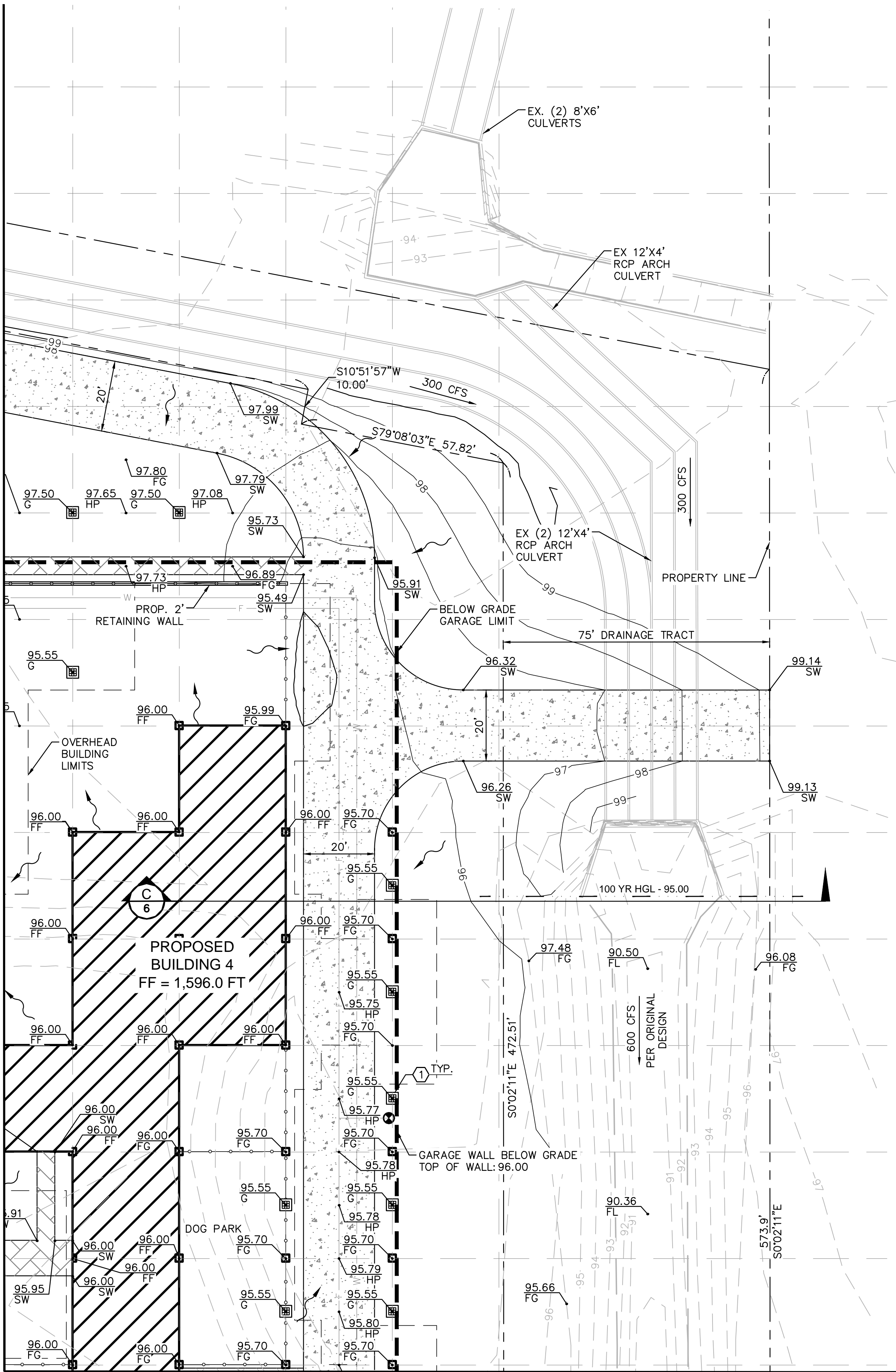






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MATCH LINE: SEE SHEET GD3



MATCH LINE: SEE SHEET GD5

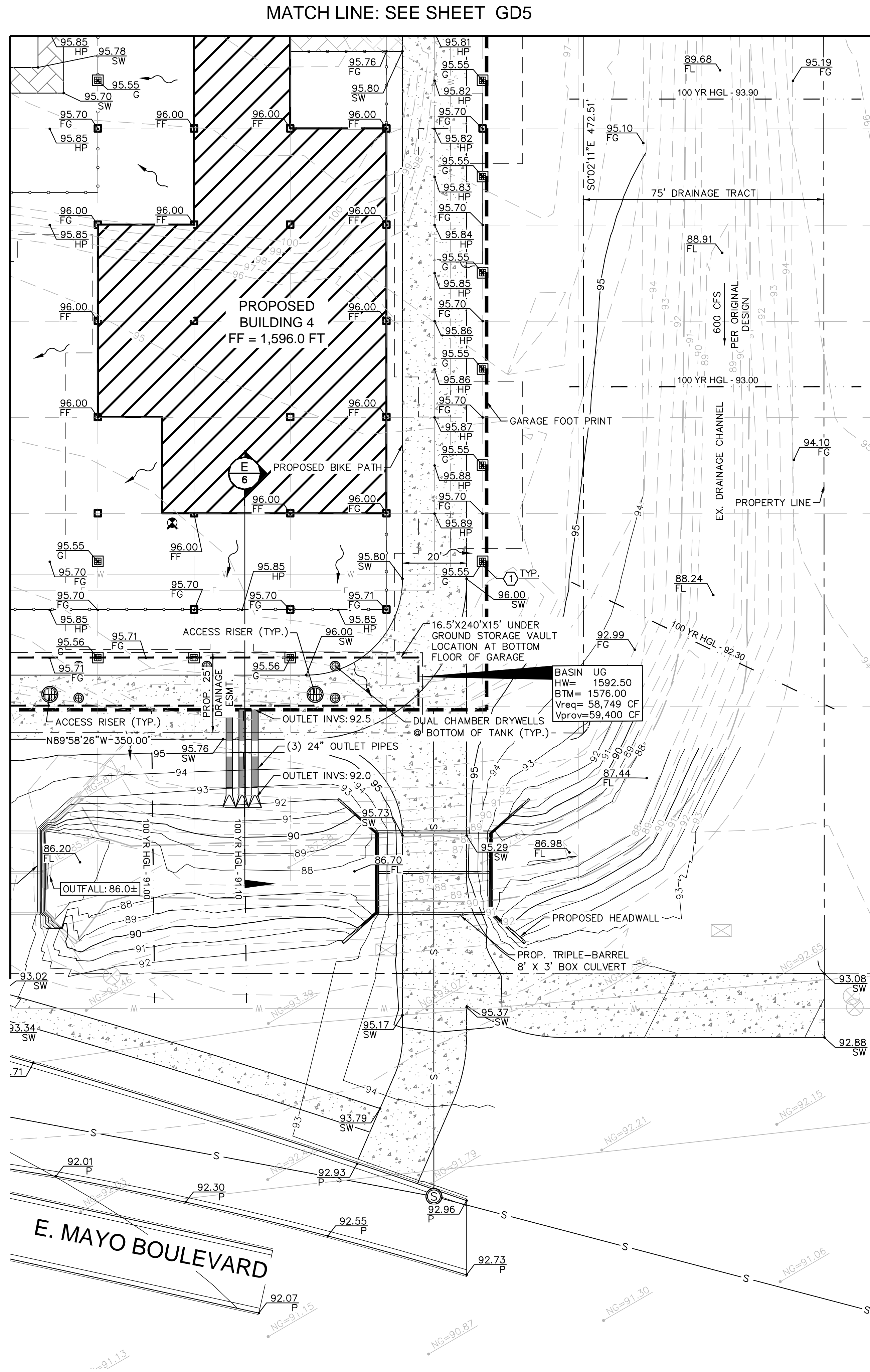
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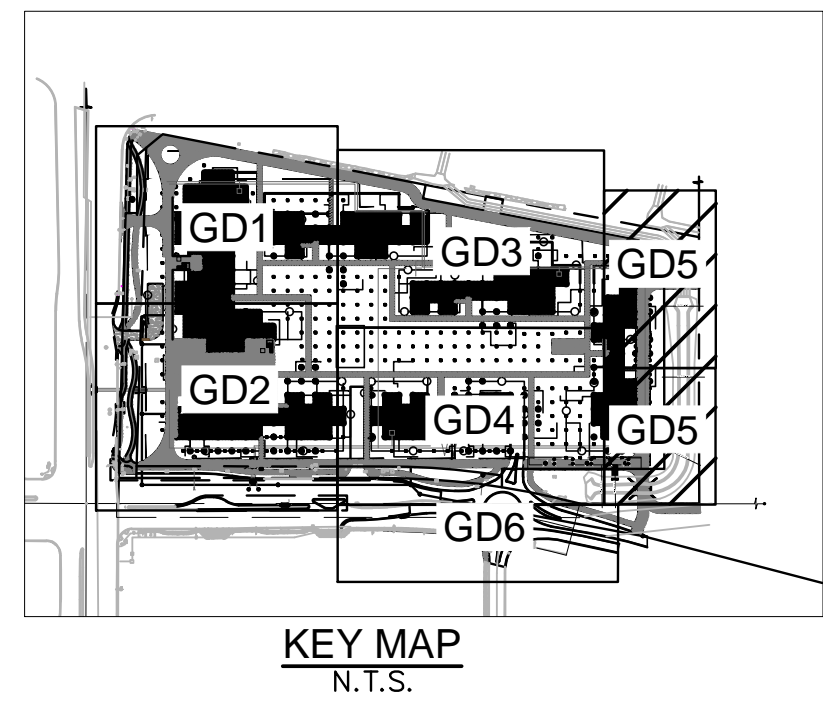
#### PRELIMINARY GRADING AND DRAINAGE NOTES

1. PROPOSED AREA DRAIN, CONNECT TO GARAGE SYSTEM BELOW.

MATCH LINE: SEE SHEET GD4

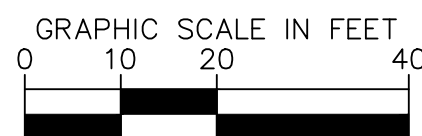
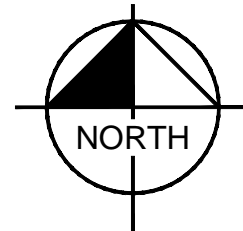


MATCH LINE: SEE SHEET GD5



#### LEGEND

- PROPERTY LINE
- RIGHT OF WAY LINE
- STREET CENTERLINE
- EASEMENT LINE
- EXISTING SEWER MAIN
- EXISTING WATER MAIN
- PROPOSED WATER MAIN
- PROPOSED SEWER MAIN
- EXISTING STORM DRAIN
- PROPOSED CONTOUR
- EXISTING CONTOURS
- PROPOSED PAVEMENT
- SPOT ELEVATION
- EXISTING SPOT ELEVATION
- EXISTING SANITARY SEWER MANHOLE
- EXISTING FIRE HYDRANT
- PROPOSED CATCH BASIN
- SURFACE FLOW DIRECTION
- EXISTING STORM DRAIN MANHOLE
- PROPOSED CONCRETE BIKE PATH
- PROPOSED PAVER WALKWAY
- PROPOSED GRID LINE



Q.S. #: 39-45

**Kimley»Horn**

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7740 North 16th Street, Suite 300  
Phoenix, Arizona 85020 (602) 944-5500

OPTIMA MCDOWELL MOUNTAIN VILLAGE  
PRELIMINARY GRADING AND DRAINAGE PLAN

PRELIMINARY  
FOR REVIEW ONLY  
NOT FOR CONSTRUCTION PURPOSES  
**Kimley»Horn**  
ENGINEER: MARK DELAMATER  
PE NO. 30886 DATE 09/22/22

PROJECT NO.  
191007011

DRAWING NAME  
GD5

5 OF 7



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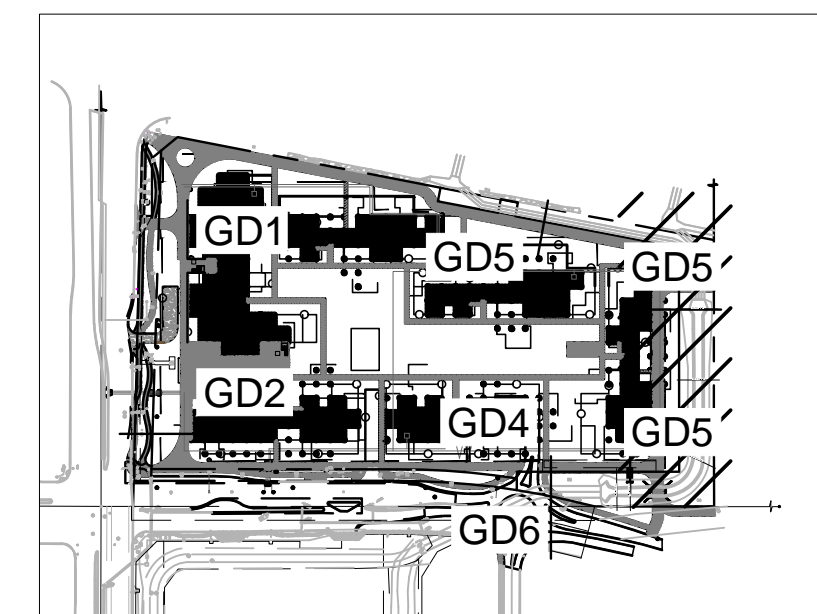
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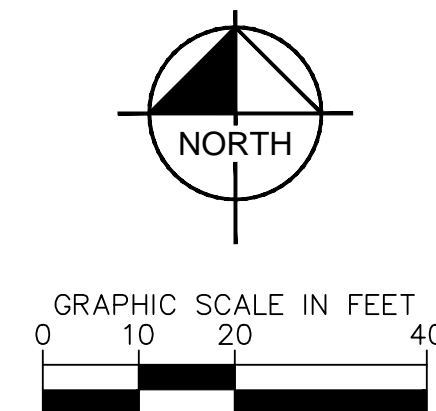
- ① PROPOSED AREA DRAIN, CONNECT TO GARAGE SYSTEM BELOW.
- ② PROPOSED CATCH BASIN.

#### LEGEND

	PROPERTY LINE		PROPOSED CATCH BASIN
	RIGHT OF WAY LINE		SURFACE FLOW DIRECTION
	STREET CENTERLINE		EXISTING STORM DRAIN MANHOLE
	EASEMENT LINE		PROPOSED CONCRETE BIKE PATH
	EXISTING SEWER MAIN		PROPOSED PAVER WALKWAY
	EXISTING PUBLIC WATER MAIN		PROPOSED GRID LINE
	PROPOSED WATER MAIN		
	PROPOSED SEWER MAIN		
	EXISTING STORM DRAIN		
	PROPOSED CONTOUR		
	EXISTING CONTOURS		
	PROPOSED PAVEMENT SPOT ELEVATION		
	EXISTING SPOT ELEVATION		
	EXISTING SANITARY SEWER MANHOLE		
	EXISTING FIRE HYDRANT		



KEY MAP  
N.T.S.



Q.S.#: 39-45



OPTIMA MCDOWELL MOUNTAIN VILLAGE  
PRELIMINARY GRADING AND DRAINAGE PLAN  
SCOTTSDALE, ARIZONA 85255

PRELIMINARY  
FOR REVIEW ONLY  
NOT FOR CONSTRUCTION PURPOSES  
Kimley»Horn  
OWNER: MCDOWELL MOUNTAIN VILLAGE  
DATE: 09/02/22

PROJECT NO.  
191007011  
DRAWING NAME  
GD6

6 OF 7

Kimley»Horn  
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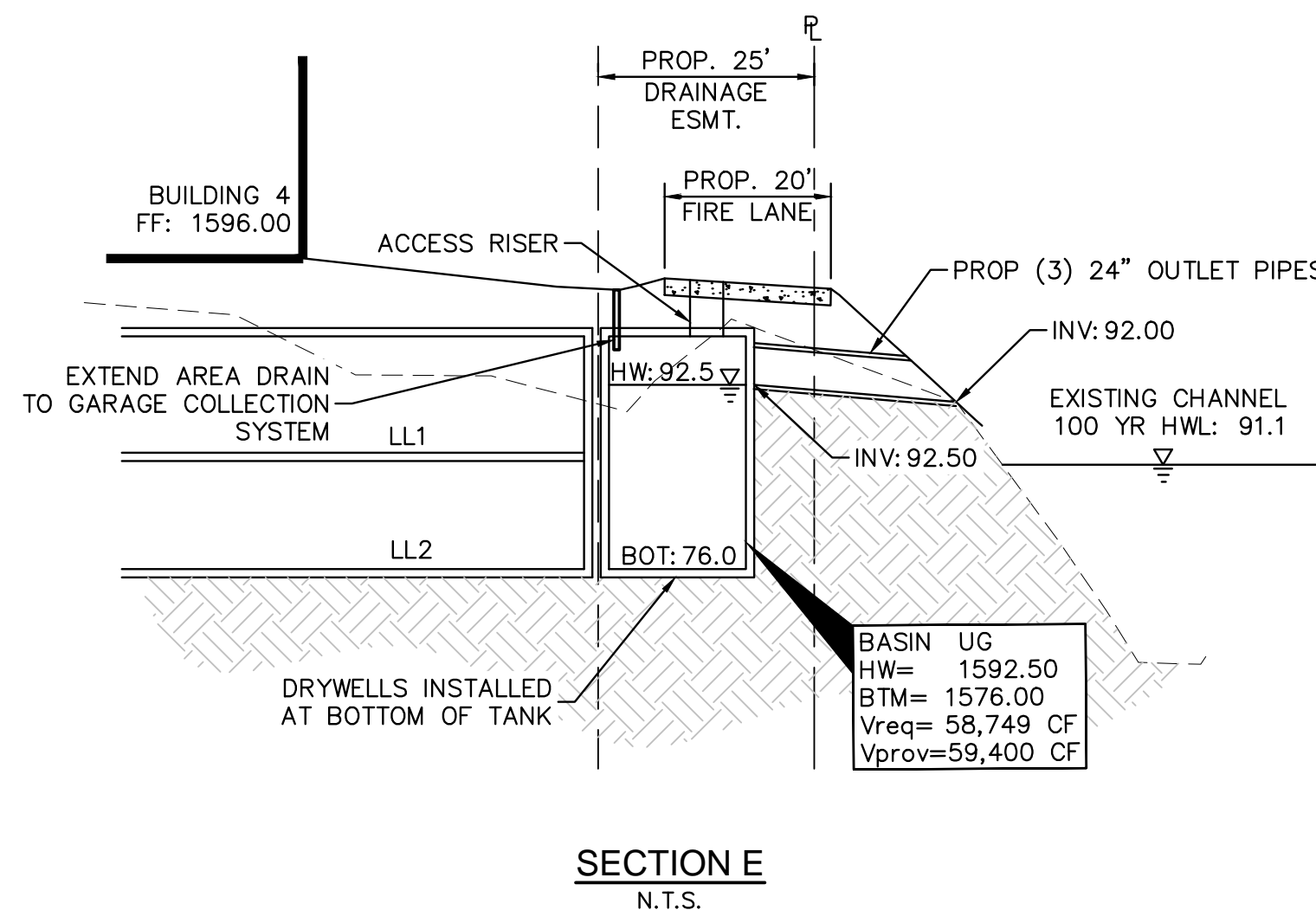
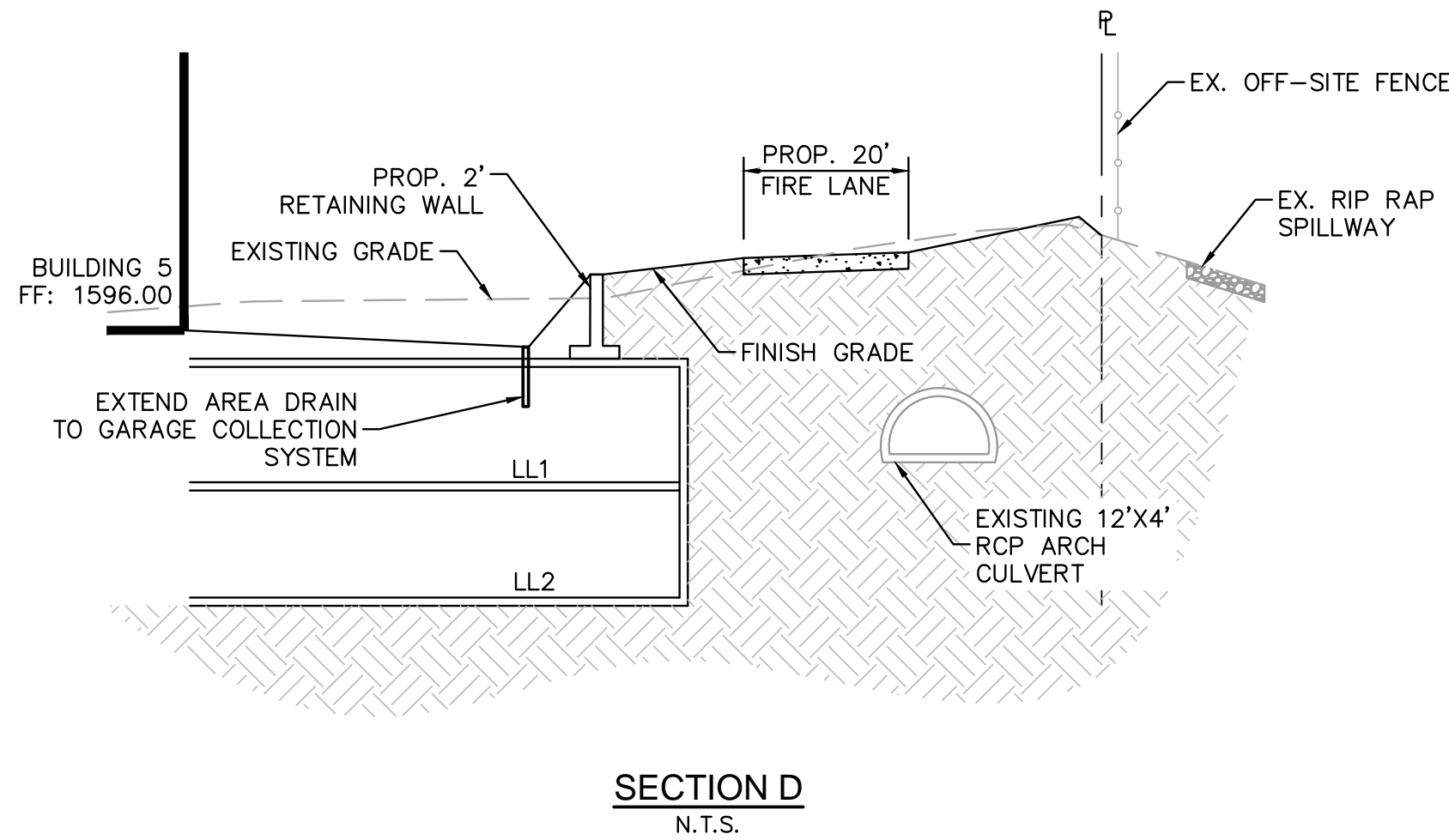
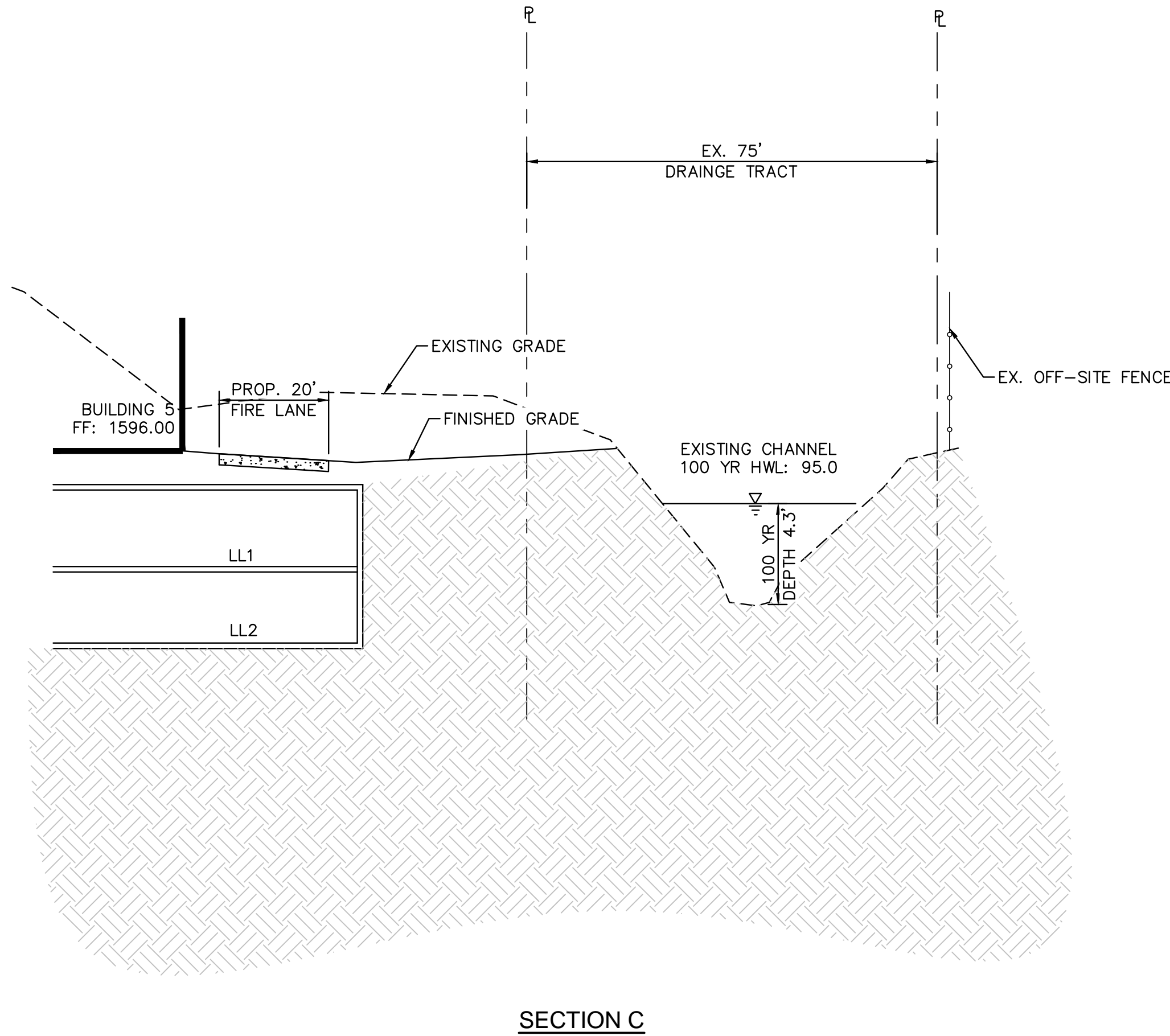
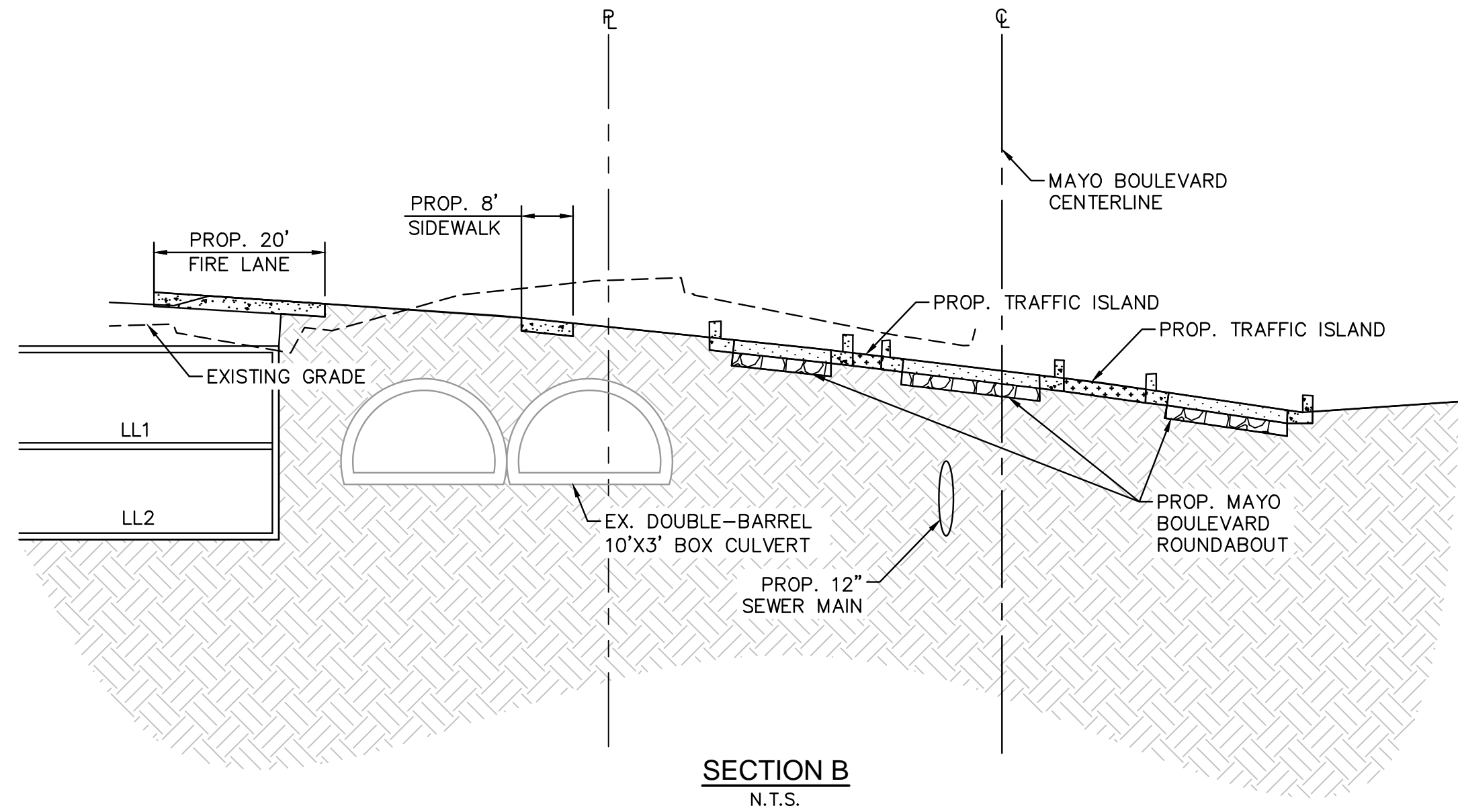
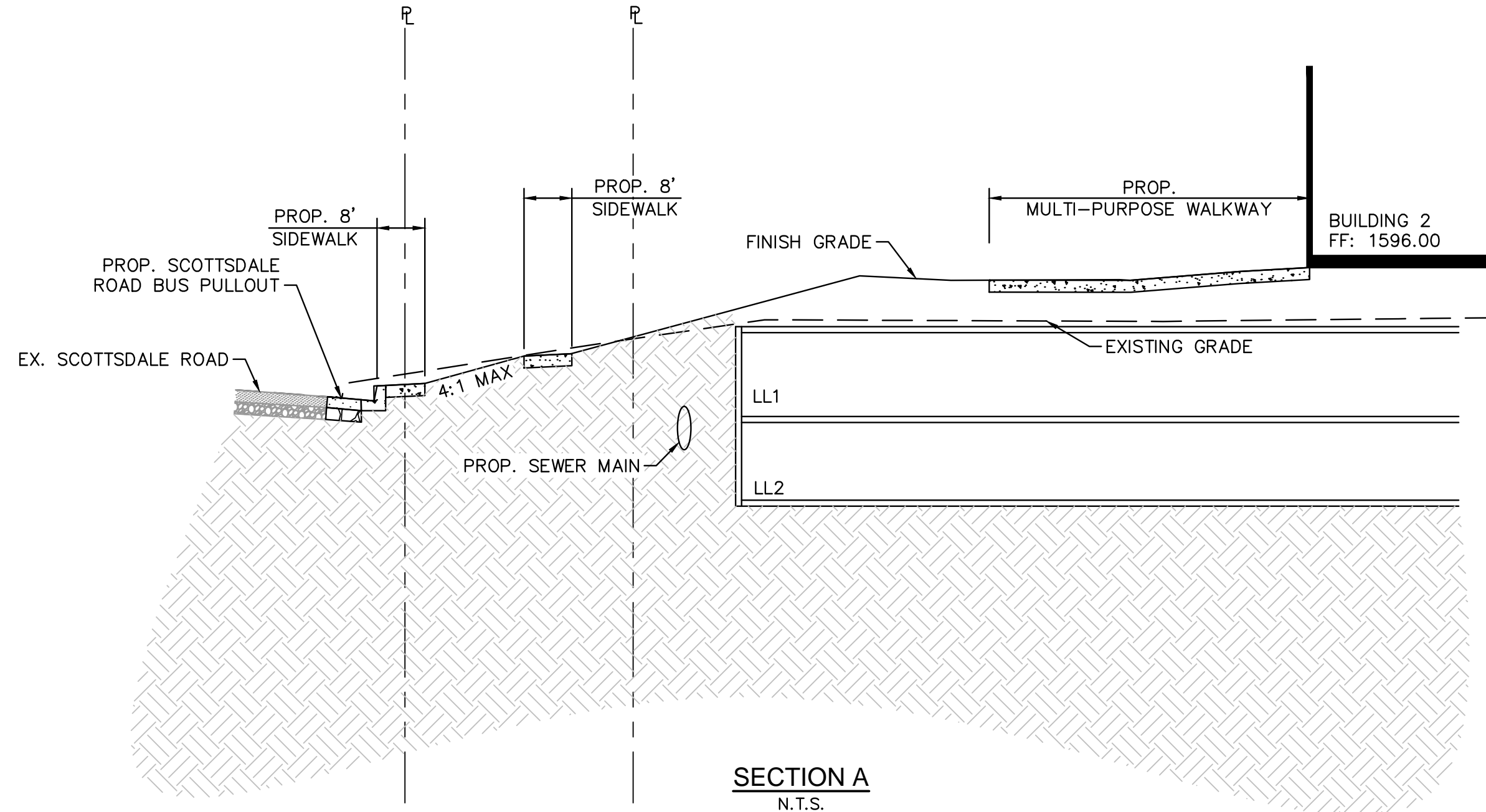
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DRAWN BY: DJH  
CHECKED BY: MLD  
DATE: SEP 2022

NO.	REVISION	BY	DATE	APPR.

MATCH LINE: SEE SHEET GD4



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Phoenix, Arizona 85020 (602) 944-5500

SCALE (H): 1"=20'  
SCALE (V): NONE  
DESIGNED BY: DJH  
DRAWN BY: DJH  
CHECKED BY: MLD  
DATE: SEP 2022

OPTIMA MCDOWELL MOUNTAIN VILLAGE  
SECTIONS  
SCOTTSDALE, ARIZONA 85255

PRELIMINARY  
FOR REVIEW ONLY  
NOT FOR CONSTRUCTION PURPOSES  
**Kimley»Horn**  
OWNER: MCDOWELL  
PROJECT NO.: 191007011  
DATE: 09/20/2022

PROJECT NO.  
191007011  
DRAWING NAME  
GD7

7 OF 7

REVISION

NO.

BY DATE APPR.

***Appendix H***

**Basin Outlet Calculations**

## 24" Outlet Pipe

Project Description	
Friction Method	Manning
Solve For	Formula Discharge
Input Data	
Roughness Coefficient	0.013
Channel Slope	0.020 ft/ft
Normal Depth	24.0 in
Diameter	24.0 in
Results	
Discharge	31.99 cfs
Flow Area	3.1 ft <sup>2</sup>
Wetted Perimeter	6.3 ft
Hydraulic Radius	6.0 in
Top Width	0.00 ft
Critical Depth	22.7 in
Percent Full	100.0 %
Critical Slope	0.017 ft/ft
Velocity	10.18 ft/s
Velocity Head	1.61 ft
Specific Energy	3.61 ft
Froude Number	(N/A)
Maximum Discharge	34.41 cfs
Discharge Full	31.99 cfs
Slope Full	0.020 ft/ft
Flow Type	Supercritical
GVF Input Data	
Downstream Depth	0.0 in
Length	0.0 ft
Number Of Steps	0
GVF Output Data	
Upstream Depth	0.0 in
Profile Description	N/A
Profile Headloss	0.00 ft
Average End Depth Over Rise	0.0 %
Normal Depth Over Rise	100.0 %
Downstream Velocity	Infinity ft/s
Upstream Velocity	Infinity ft/s
Normal Depth	24.0 in
Critical Depth	22.7 in
Channel Slope	0.020 ft/ft
Critical Slope	0.017 ft/ft

***Appendix I***

Scottsdale Road Drainage Report

# DRAINAGE REPORT

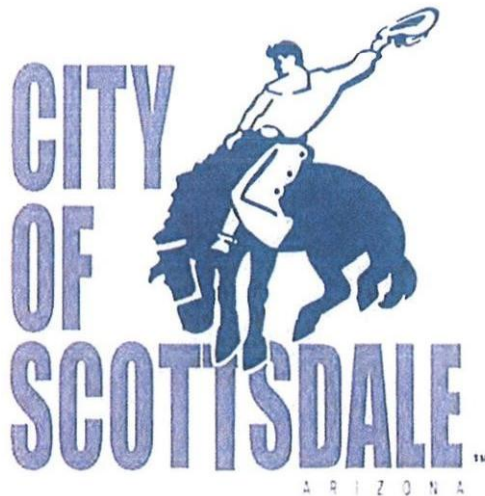
## SCOTTSDALE ROAD

FRANK LLOYD WRIGHT BLVD to  
THOMPSON PEAK PARKWAY

### SEGMENT 2

March 2009

Prepared For:



City of Scottsdale  
Capital Project Management  
Transportation Capital Improvement  
Program - Major Streets

By:

**Dibble**  
**Engineering**

7500 North Dreamy Draw Drive, Suite 200  
Phoenix, Arizona 85020



DRAINAGE REPORT  
PROJ. #S7005  
SCOTTSDALE ROAD – FRANK LLOYD WRIGHT BLVD TO THOMPSON PEAK PKWY  
SEGMENT 2

I. INTRODUCTION .....	1
A. General.....	1
B. Study Area.....	2
C. Existing Drainage Studies .....	4
D. Corps of Engineers 404 Permit .....	5
II. DESIGN CRITERIA.....	6
A. Rainfall .....	6
B. Roadway Inundation .....	8
C. Catch Basins & Scuppers .....	8
D. Storm Drains .....	9
E. Open Channels .....	9
F. Off-site Runoff Cross-Road Drainage .....	10
III. HYDROLOGY .....	11
A. Introduction .....	11
B. Offsite Methodology .....	11
B.1 Final Drainage Report, Pima Freeway 9A, Part II.....	11
B.2 Interim Regional Drainage Channel .....	11
B.3 Hydrology Analysis, Paradise Ridge .....	12
B.4 Master Drainage Report for North Scottsdale Gateway .....	12
B.6 Powerline Corridor Channel .....	13
C. Onsite Methodology .....	13
D. Design Assumptions .....	14
IV. HYDRAULICS .....	15
A. Roadway Drainage .....	15
A.1 Methodology.....	15
A.2 Assumptions .....	15
B. Channels.....	15
B.1 Methodology .....	15
B.2 Channel Lining .....	16
B.3 Channel Cross Section .....	16
C. Culverts .....	16
V. RESULTS & RECOMMENDATIONS .....	17
A. Pavement Drainage Design.....	17
B. Offsite Hydrology .....	18
C. Offsite Drainage Design .....	18
D. North Scottsdale Gateway Retention and Outfall Design .....	21
REFERENCES .....	26



## LIST OF FIGURES

Figure-1 Project Limits .....	2
Figure-2 Contributing Existing Drainage Studies Map .....	7
Figure-3 Offsite Drainage Concept .....	19
Figure-4 North Scottsdale Gateway 100 Year Watershed Area Map .....	24

## LIST OF TABLES

Table-1 Offsite Design Flow Summary .....	18
Table-2 North Scottsdale Gateway Retention Summary .....	23

## LIST OF APPENDICES

Precipitation Data .....	Appendix A
Roadway Drainage Calculations .....	Appendix B
Offsite Drainage Calculations .....	Appendix C
North Scottsdale Gateway Retention Calculations .....	Appendix D
404 Permit .....	Appendix E
Hydrology Memo .....	Appendix F



FINAL DRAINAGE REPORT  
PROJ. #S7005  
*SCOTTSDALE ROAD – FRANK LLOYD WRIGHT BLVD TO THOMPSON PEAK PKWY*  
*SEGMENT 2*

**I. INTRODUCTION**

**A. General**

This drainage report is prepared for the City of Scottsdale as part of the Segment 2 roadway improvements design of Scottsdale Road from Frank Lloyd Wright Boulevard to Thompson Peak Parkway in Scottsdale, Arizona. The drainage portions of the project include on-site roadway drainage design, as well as design to accommodate off-site runoff crossing the project corridor. This report presents the project background, drainage analysis, and results for the project. The project location is shown on **Figure 1** on the following page.

---

The improvements to Scottsdale Road are being constructed in two separate segments. **Segment 1** extends from Scottsdale Road centerline station 148+00, just south of Union Hills Boulevard, to the Loop 101, Pima Freeway. Also included in this segment are (1) improvements to Union Hills Boulevard extending from Scottsdale Road, Union Hills centerline station 10+00, to Union Hills centerline station 19+82.37 (EOP) and (2) the offsite flow conveyance system for the Lund Cadillac development at the intersection of Union Hills Boulevard and Scottsdale Road. **Segment 2** extends from Frank Lloyd Wright Boulevard to Scottsdale Road centerline station 148+00, just south of Union Hills Boulevard, and from the Loop 101 , Pima Freeway to Thompson Peak Parkway. This report documents the design of Segment 2. At the time of the writing of this report, construction of Segment 1 is complete. For documentation of Segment 1 of this project refer to *Drainage Report, Frank Lloyd Wright Blvd to Thompson Peak Parkway – Segment 1 100%*, by Dibble Engineering.

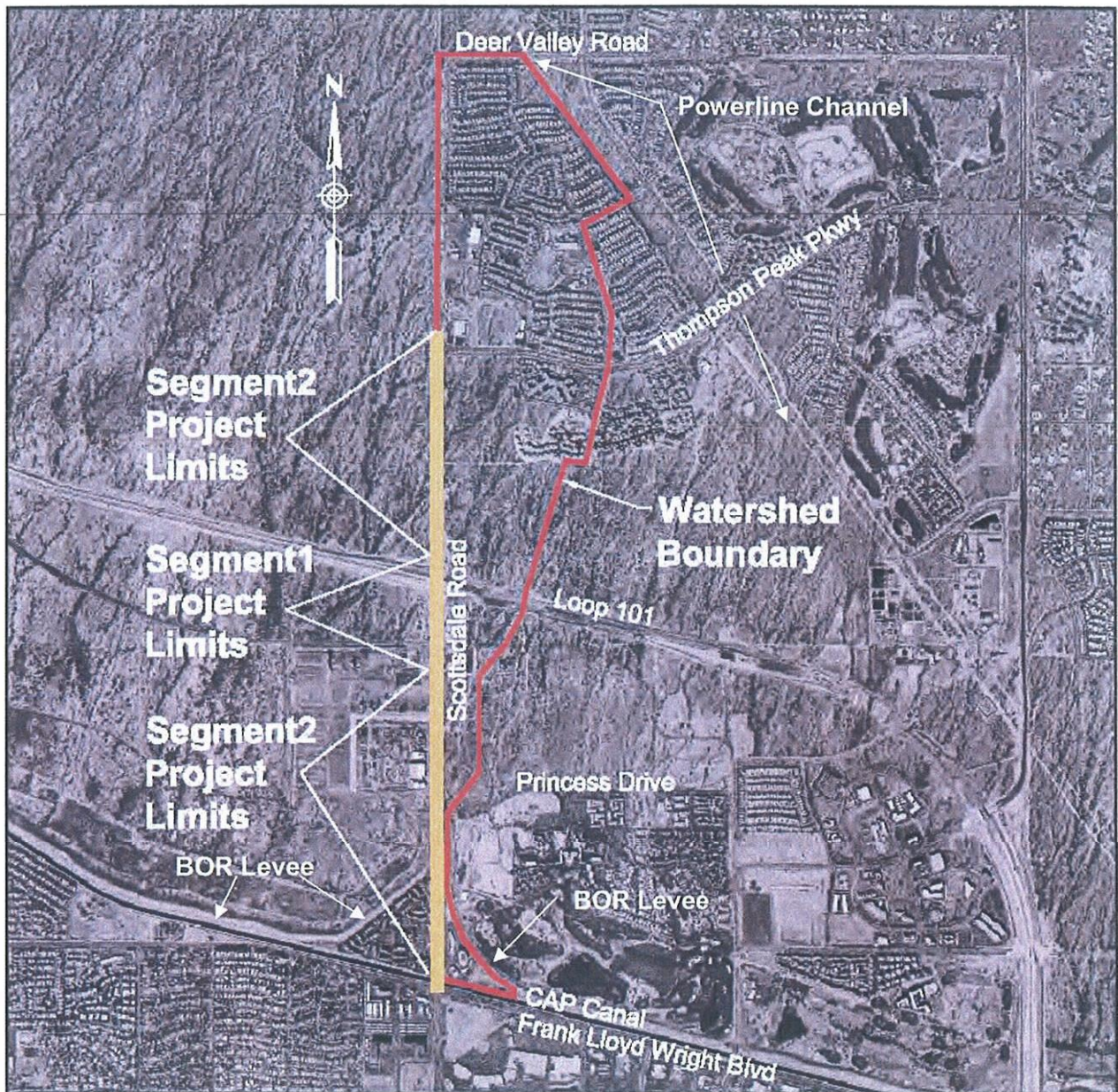
The improvements proposed for Scottsdale Road consist of widening the roadway to provide three 12-foot driving lanes in each direction, with a 4-foot bike lane and a 24-foot median, and the addition of concrete curb, gutter, and sidewalk. Where it is necessary, culverts will be



added underneath the roadway to allow off-site flow to pass through the corridor unobstructed and at their historic locations.

### **B. Study Area**

Existing drainage patterns along the project alignment are generally from the northeast to the southwest. The U.S. Bureau of Reclamation (BOR) has constructed large storm water storage embankments along the upstream (north) side of the CAP Canal that impound all runoff generated north of the canal. The Powerline Channel bisects the contributing



**Figure 1 – Project Limits**

watershed area and diverts runoff away from the project reducing the peak discharges reaching the roadway. The resulting watershed contributing to drainage across the project corridor has been delineated and is shown on **Figure 1**. The project is located within FEMA flood zone AO consisting of shallow sheet flow flooding conditions on sloping terrain. Within the project limits, the FEMA maps indicate average flooding depths of 1 foot with velocities in the range of 3 to 4 feet-per-second. The sheet flow flooding conditions are being modified as development takes place within the watershed. The developments are providing on-site retention and providing channelization to control the flow and fix its location. Development is rapidly occurring adjacent to the existing roadway resulting in a mix of fully improved roadway sections with full curb and gutter and older roadway sections with no curb and gutter and dip crossings at existing washes. The existing roadway drainage is described by reach as follows:

---

**Frank Lloyd Wright Blvd. to Princess Drive**

The BOR embankments wrap to the north on both sides of Scottsdale Road to contain runoff and allow the roadway profile to drop down to the CAP Canal bridge elevation. The embankments extend northerly to near Princess Drive. Due to the lower elevation, runoff generated south of the embankment terminus cannot be drained by gravity into the impoundment area. Off-site runoff generated within this area is currently contained in retention areas constructed with the developments on both sides of the road. The retention areas currently have no outfall to drain the basins. Pavement runoff generated in this area either drains into the retention basins or drains to the CAP canal service road. The CAP does not accept offsite runoff into the canal right-of-way, so this project will need to identify an alternate means of disposing of the runoff.

**Princess Drive to Mayo Boulevard**

There is a dip crossing at Chauncey Lane that conveys the runoff from a natural wash on the east side of the road into an improved, landscaped channel constructed as part of the Automotive Group Realty automall. The improved channel drains southerly along the west side of Scottsdale Road to the south side of the automall development where it ends. Runoff reaching the southerly limit of the channel fills the channel and spills out into the roadway shoulder area and continues south to a point where it drains into a

small natural wash that drains into culverts under Princess Drive and into the BOR impoundment area. A second dip section just north of Princess Drive directs runoff accumulating along the east side of Scottsdale Road into the small natural wash into an existing culvert beneath Princess Drive and into the impoundment area.

#### **Loop 101 to Thompson Peak Parkway**

The land adjacent to Scottsdale Road is currently unimproved between Loop 101 and Thompson Peak Parkway. Runoff currently crosses the roadway in dip sections at three locations. The crossings are at approximate stations 183+00, 189+00, and 200+00.

There is an existing dip crossing about 400 feet north of Thompson Peak parkway near station 211+00. The Discount Tire corporate offices have been constructed on the northeast corner of Scottsdale Road and Thompson Peak Parkway. This development diverts offsite flow from the north and northeast across Scottsdale Road prior to Thompson Peak Parkway. On-site retention and landscaping has been completed outside the City ROW. The on-site retention basins drain through 3-36 inch pipes under Thompson Peak Parkway into an existing wash that continues to the south. The 3-36 inch pipes also convey Thompson Peak Parkway roadway drainage.

#### ***C. Existing Drainage Studies***

All areas of the Scottsdale Road project corridor are planned for development in the coming years. A number of drainage reports exist for these developments, and are being investigated for use in the design of the current improvements. The following projects are currently planned or are completed for the Scottsdale Road project corridor.

- ❑ Final Drainage Report, Pima Freeway 9A, Part II, reference #10
- ❑ Drainage Study, Core North/Core South, reference #15
- ❑ Interim Regional Drainage Channel, reference #18
- ❑ Master Drainage Report for North Scottsdale Gateway, reference #4
- ❑ Palisene-Paradise Ridge Conceptual Drainage Plan Report, reference #6



**D. Corps of Engineers 404 Permit**

The U.S. Army Corps of Engineers (COE) has determined that the One Scottsdale (formerly the Stacked 40's) development north of Union Hills Boulevard does not contain jurisdictional washes. Existing jurisdictional washes upstream of the One Scottsdale have been rerouted due to upstream development, cutting off natural wash flow to the area. As there are no significant crossings of Scottsdale Road that do not originate on the One Scottsdale property, there are no jurisdictional waters in the project area and a 404 permit is not required. The delineation determination letter from the COE is contained in **Appendix E**. The Arizona State Land Department (ASLD) has obtained a 404 permit for the entire Paradise Ridge development. The special conditions from that permit will apply to any property obtained from the ASLD within the permitted area.

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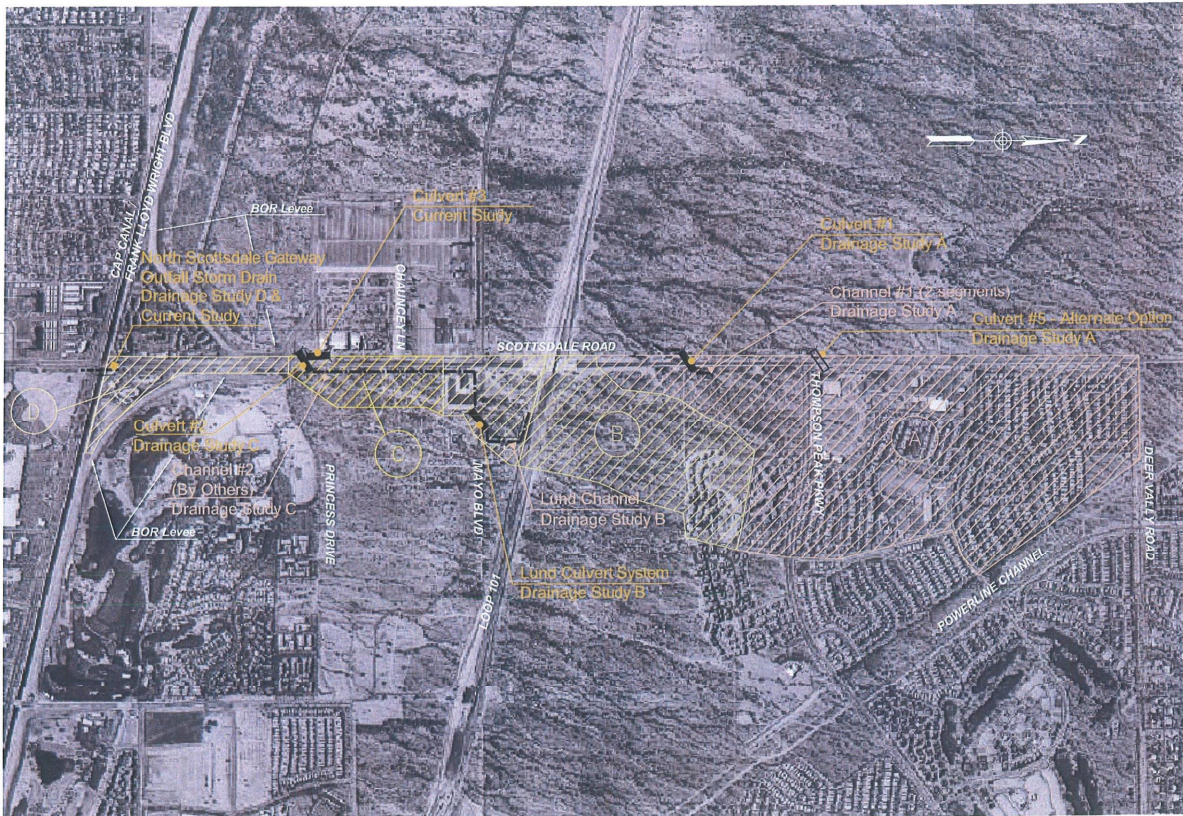
## **II. DESIGN CRITERIA**

The City of Scottsdale's drainage requirements as stated in the *City of Scottsdale, Arizona Design Standards and Policies Manual* (DSPM), August 2007, Chapter 4, as well as the *Drainage Design Manual for Maricopa County, Arizona, Volume I, Hydrology*, January 1, 1995, (Hydrology Manual), and *Drainage Design Manual for Maricopa County, Arizona, Volume II, Hydraulics*, January 28, 1996, (Hydraulics Manual), will be used as the basis for design. Discussions of specific design criteria are in the sections that follow.

### **A. Rainfall**

As mentioned in *Section I.C.*, a number of drainage studies have already been prepared along the Scottsdale Road corridor to support the design of various developments and the Loop 101, Pima Freeway. A significant portion of the offsite flow design of this project will be based on the rainfall runoff results provided within these previous studies. These projects are listed in *section I.C.* **Figure 2** displays the portions of the project watershed studied within these existing drainage studies, along with proposed offsite drainage features. It can be seen in **Figure 2** that the entire project watershed has been studied within the previous studies, and drainage features will be designed based on the results of the corresponding study.

For pavement runoff, and where previous studies of off-site flows require supplementation, rainfall values are obtained from the DSPM isopluvials (for volume calculations) and city-wide IDF curves presented as DSPM *Figure 4.1-3* (maximum discharge calculations).



**Figure 2 - Contributing Existing Drainage Studies Map**

Exhibit of the areas of the project watershed analyzed by previous drainage studies.

**Existing Drainage Studies**

- (A) Paradise Ridge (Reference #6)
- (B) Pima Freeway 9A, Part II (Reference #10)
- (C) Interim Regional Drainage Channel (Reference #18)
- (D) North Scottsdale Gateway (Reference #4)



### **B. Roadway Inundation**

Runoff is allowed to collect in the two right-most driving lanes and bicycle lane for a maximum allowable spread of 29.5 feet from the face of vertical curb. Pavement drainage is collected in curb opening catch basins and MAG scuppers. The following criteria apply to the on-site drainage:

- ❖ A Manning's n value of 0.015 (normal asphalt) will be used for street flow.
- ❖ Streets will be designed to carry runoff from a 10-year peak storm. Arterial streets and major collectors will be designed to maintain a single 12-foot dry driving lane in each direction. The peak flows from a 100-year storm will be carried within the cross-section between the right-of-way lines, will be below finished floor of adjacent buildings, and will not produce a depth above the street greater than 8 inches.
- ❖ In cases where the peak flows from the design storm exceed the street capacity, underground pipes of sufficient size to carry the excess will be installed.
- ❖ Roadside ditches are to be sized to prevent the 10-year storm runoff from saturating the pavement sub-grade.

In addition to the above City of Scottsdale requirements, the following criteria from the Hydraulics Manual have also been adopted for roadway drainage.

- ❖ Trapezoidal channel bottoms are a minimum of 4 feet wide for maintenance purposes.
- ❖ V-shaped channels are allowed in lieu of a 4-foot trapezoidal channel.

### **C. Catch Basins & Scuppers**

Catch basins are placed as necessary to meet the roadway inundation criteria and at intersections to prevent cross street flow. Curb opening catch basins will be City of Phoenix Standard P1569-1. Area inlet catch basins will be MAG Standard 537, type 'G'. Scuppers will be MAG Standard 206. The interception capacity of catch basins and scuppers is reduced to account for plugging by debris. Grated catch basin capacity is reduced by 50% in sump conditions and by 40% in continuous grade conditions. Curb opening catch basin and scupper capacity is reduced by 20% in both continuous grade and sump conditions.

#### **D. Storm Drains**

If a storm drain system is deemed necessary, it will be sized for 10-year inlet flows and will limit the hydraulic grade line to a minimum of 6 inches below the inlet structures using a Manning's n value of 0.013 for precast concrete pipe and 0.011 for smooth walled HDPE pipe.

- ❖ The minimum pipe size is 24 inch for mainline storm drains in the pavement and 15 inch for catch basin connector pipes.
- ❖ Pipes will be deep enough to not project into the pavement structural section.
- ❖ Maximum spacing of manholes is 300 ft for pipes up to 30 in diameter, 400 ft for pipes larger than 30 in and smaller than 48 in, and 500 ft for pipes 48 in and larger.

Pipes will be designed to accommodate inlets with 100% capture efficiency. Minimum flowing full velocities of 3 ft/s and maximum flowing full velocity of 10 ft/s will be maintained unless restricted by minimum pipe size requirements. The design will, if possible, avoid the interception of an off-site natural wash with the intent of collecting it and putting it into a pipe or underground storm sewer system. If there is no alternative to the routing of an open channel into a piped system, water will be first routed into a sediment or debris basin. The capacity of the conduit should be 100 percent of the design discharge plus 30 percent to accommodate any sediment and debris.

#### **E. Open Channels**

- ❖ Regional channels will be designed to convey the 100-year planned-to-date conditions peak discharge within the channel banks.
- ❖ The design channel depth is the normal flow depth plus freeboard. Required freeboard is 0.25 times the sum of flow depth plus velocity head with a minimum of 1 foot.
- ❖ Froude numbers for channel design are to be less than or equal to 0.86 for sub-critical flow. Super-critical flow will be avoided whenever possible.
- ❖ If possible, the minimum channel bend radius will be 3-times the channel top width at the depth of flow.
- ❖ Longitudinal channel slopes may be set as steeply as possible within the limitations of the channel material design allowable tractive shear and the limitation on Froude number.
- ❖ Surface runoff entering the channel from the side will be directed to enter the channel at planned locations with side spillways. This will limit the possibility of rill erosion for earth channels. Where the top of channel projects above the adjacent existing ground (fill situations), a parallel channel or swale will be used to convey

runoff to a planned channel inflow point. Additional right-of-way may be required in these areas. The parallel auxiliary drainage channel should generally be a v-shaped swale.

#### ***F. Off-site Runoff Cross-Road Drainage***

It will be necessary to construct a number of culverts beneath Scottsdale Road. The location of these culverts and offsite conveyance channels can be seen in **Figure 2**. As stated in the DSPM, cross road culverts for major collector and arterial streets will be designed to convey the 50-year storm underneath the roadway, with no overtopping; and 100-year storm flows over and above the 50 year values will be conveyed over the roadway with a depth not to exceed 6 inches. However, the proposed profile for Scottsdale Road along the project corridor consists of a nearly continuous grade from north to south, with dip sections at natural wash locations removed. If runoff generated by the 100-year storm were to overtop the curb and gutter, it would be directed down the street, not directly over it. Therefore, culverts will be designed to convey the 100- year storm with no roadway overtopping.

- ❖ Box Culverts will have a minimum height of 4 feet for maintenance purposes, unless physical constraints make a 3 foot box necessary.
- ❖ Culverts constructed with channels will be designed to the same 100-year design discharge as used for the channel.

### **III. HYDROLOGY**

#### **A. Introduction**

The vast majority of the hydrology for the area has been developed as part of a number of drainage studies for new developments fronting Scottsdale Road and the Loop 101 – Pima Freeway. These studies are listed here and are described in more detail in *Section B. Offsite Methodology*.

- ❑ Final Drainage Report, Pima Freeway 9A, Part II, reference #10
- ❑ Interim Regional Drainage Channel, reference #18
- ❑ Hydrology Analysis, Paradise Ridge, reference #6
- ❑ Master Drainage Report for North Scottsdale Gateway, reference #4

In areas where existing studies require supplementation, and in the design of the pavement drainage, the Rational Method has been employed.

#### **B. Offsite Methodology**

**Figure 2** displays the portions of the project watershed studied within previous drainage studies, along with proposed offsite drainage features.

##### *B.1 Final Drainage Report, Pima Freeway 9A, Part II*

This hydrology study was performed by HDR Engineering Inc. for ADOT to aid in the design of SR101 from Scottsdale Road to Pima Road, resulting in a total watershed area of 15.71 square miles. The study is a combination of portions of several different models that have been prepared for the area by various consultants since 1992. Hydrologic analysis was performed using the U.S. Army Corps of Engineers HEC-1 Flood Hydrograph Package, Version 4.0.3E. The results of this study were used to size pass-through culverts beneath the freeway. In Segment 1 of this project, the results are used to design the Lund Cadillac culvert and channel system. A conservative measure, given that the study has since been revised, and flow rates reduced, within the *Core North/Core South* study.

##### *B.2 Interim Regional Drainage Channel*

In 2008 the City contracted with Wood, Patel & Associates to design an interim drainage channel to connect the Lund Channel System to a proposed box culvert approximately 150' north of Princess Drive. Hydrology was done for this channel that incorporated changes made

to the watershed due to the **One Scottsdale** development area north of the Loop 101, i.e. the series of parcels fronting Scottsdale Road on the east side from Loop 101 to Thompson Peak Parkway. One Scottsdale was formerly known as the Stacked 40's. The resulting 100-year peak runoff for the channel is 300 cfs.

### *B.3 Hydrology Analysis, Paradise Ridge*

This hydrology study was performed by Bob Ward, P.E., as a subconsultant to Entranco Biological Resource Group. Paradise Ridge is a proposed subdivision development on the western edge of Scottsdale Road, extending from Mayo Boulevard to Deer Valley Road. The purpose of the study was to assist in the development of jurisdictional "404" washes and to prepare a Master Drainage Plan for Paradise Ridge. The study pieces together a number of previous studies to establish off-site flow patterns impacting the Paradise Ridge property. Minor modifications were made to these models to provide connections to jurisdictional wash inflow points along the east boundary of Paradise Ridge. As part of the development of a Master Drainage Plan a post development runoff model was developed, with anticipated regional drainage features in place on the Paradise Ridge property. Hydrologic analysis was performed using the U.S. Army Corps of Engineers HEC-1 Flood Hydrograph Package, Version 4.0.3E. In the current project, the results of the Paradise Ridge study are used to design Scottsdale Road offsite drainage elements north of Loop 101 and south of Deer Valley Road. The study does not incorporate proposed improvements to **One Scottsdale**. As One Scottsdale is developed they will need to incorporate any improvements made to Scottsdale Road in the current project based on the results of the Paradise Ridge study.

### *B.4 Master Drainage Report for North Scottsdale Gateway*

This hydrology study was performed by Development Coordination Group, Ltd for Byxbee Development Partners, LLC. North Scottsdale Gateway (NSG) is a triangular shaped site located on the east side of Scottsdale Road, adjacent to and north of the Central Arizona Project Canal (CAP). The site is roughly 18 total acres in size. The site is of particular interest because it is the downstream boundary of flow along Scottsdale Road, before reaching the CAP canal. The site is almost completely protected from offsite flows by the Bureau of Reclamation Levee and

basin system, the only exception being runoff from Scottsdale road and right-of-way south of Princess Drive, and the levee bank itself. The site receives runoff from the entire roadway right-of-way section, except at the downstream end, where roadway runoff is allowed to drain directly onto the CAP canal service road and canal. Hydrologic analysis for the study was performed using the Rational Method. In the current project, the city has been instructed that the CAP canal is not an allowable depository of storm runoff, and runoff presently reaching the service road and the canal must be diverted to an alternative outfall. Also, the NSG property has no acceptable outfall to drain their basins except by evaporation and percolation. A prior commitment was made by the city to connect to the NSG basin system and provide a bleed-off outfall as part of this Scottsdale Road improvement project. The results of the North Scottsdale Gateway study are modified to account for the improved roadway. These results are used to improve North Scottsdale Gateway retention basins for the increased Scottsdale Road runoff and to design a site outfall for the North Scottsdale Gateway Property.

#### *B.6 Powerline Corridor Channel*

The Powerline Corridor Channel currently ends about 1,500-feet southeast of Thompson Peak Parkway, capturing and diverting regional flows to the southeast. The *Core North/Core South* hydrology model is structured to include this channel at its current level of construction. Plans are underway to extend the Powerline Corridor Channel southeast to the COS Water Campus. This construction will not impact the portion of the existing studies used for the current project, design flows would remain unchanged with the new channel in place.

### **C. Onsite Methodology**

The rational method is used for runoff calculations for roadway drainage design using a site specific Intensity-Duration-Frequency relationship, checked against the curves presented as *Figure 4.1-3* in the DSPM to ensure the higher intensity is used. This I-D-F relation is also shown in **Appendix A**. The Papadakis and Kazan time of concentration equation from the Hydrology Manual is used to calculate the inlet time (overland flow time) for each inlet. The overland flow time for all inlets is 5 minutes. This value is input into *Hydraflow*. Tc for the system is

calculated by *Hydraflow*: travel time in the storm drain pipe is computed based on the pipe flowing full velocity and added to the surface runoff times of concentration to obtain the totaled time of concentration for storm drain design.

#### ***D. Design Assumptions***

The hydrology for this project models the 100-year event (10-year for roadway runoff design) for watershed and land-use conditions as planned by the above referenced developments.

#### **IV. HYDRAULICS**

##### **A. Roadway Drainage**

###### **A.1 Methodology**

The current project represents the full build out of the roadway with complete curb and gutter. Pavement and inlet hydraulic calculations are based on procedures contained in the Federal Highway Administration Hydraulic Engineering Circular No. 12 *Drainage of Highway Pavements*, 1996 and are performed within *Hydraflow v.10.0.0.6* design software.

Storm drain hydraulic grade line calculations are performed by *Hydraflow*, and are made using an iterative procedure that applies Bernoulli's energy equation between downstream and upstream ends of each line in the system. Manning's equation is used to determine head losses due to pipe friction. *Hydraflow* estimates junction losses by using the City of Los Angeles Thompson equation. Manhole losses are computed as K times the velocity head. The values of K are input manually into *Hydraflow* based on criteria adapted from FHWA Hydraulic Engineering Circular No. 12.

###### **A.2 Assumptions**

The following assumptions are made in performing the pavement drainage analysis:

1. A minimum time of concentration of five minutes is used.
2. The 10-year design discharge used for inlet sizing is based on the runoff generated within the proposed right-of-way.
3. The C factor for runoff generated within the right-of-way is 0.95..
4. The gutter flow reduction factor for parked vehicles is 1.0, since parking will not be allowed along Scottsdale Road.

##### **B. Channels**

###### **B.1 Methodology**

Channels are sized using Manning's equation for developed conditions 100-year peak discharges with freeboard using velocity and tractive shear as the primary design parameter. To minimize the overall channel width, the channel cross-section and slope in each channel reach is set to meet an acceptable design velocity.



### B.2 Channel Lining

Due to the natural steepness of the ground slope of the area, some channels have a tractive shear value requiring a rip-rap lining to eliminate scour and head cutting. The Manning roughness coefficient,  $n$ , is a measure of the flow resistance or relative roughness of a channel. The flow resistance is affected by many factors including bed material, cross section irregularities, depth of flow, vegetation, channel alignment, channel shape, obstructions, suspended material and bed-load. The Arizona Department of Water Resources *Manual for Engineering Analysis of Fluvial Systems* provides an equation for calculating an  $n$ -value based on the size of bed material. The base Manning's  $n$ -value for 6" dumped rip-rap material is calculated from the following equation;

$$n_b = 0.0395 \times D_{50}^{(1/6)}$$

Where  $D_{50}$  = Diameter, in feet, in which 50% of the particles (by weight) are smaller.

This equation yields a base Manning's  $n$ -value of 0.034 for the 6" dumped rip-rap.

### B.3 Channel Cross Section

Channels are a trapezoidal section with 3 to 1 to 4 to 1 sideslopes. Where a riprap lining is used, a 3 to 1 sideslope is allowable. In an effort to keep velocities low, roadside channels are generally wide and shallow—less than 3 feet in depth.

### C. Culverts

New culverts are sized using standard culvert design methodology considering inlet or outlet control as presented in Federal Highway Administration, Hydraulic Design Series No. 5, *Hydraulic Design of Highway Culverts*, September 1985. The calculations check for inlet control, pipe barrel (friction), or tail water control. The condition resulting in the highest computed headwater elevation governs.

## **V. RESULTS & RECOMMENDATIONS**

### **A. Pavement Drainage Design**

The roadway pavement drainage design uses a combination of scuppers with roadside drainage ditches and storm drain. This portion of Scottsdale Road contains few sumps in the roadway profile. Therefore, management of inlet flow-by of gutter flow at intersections governed the selection of spacing and sizing for scuppers and curb inlets along Scottsdale Road. Gutter spread is kept within the design criteria at the design spacing. Gutter depths do not exceed six inches. Hydraflow surface drainage calculations and drainage area calculations can be found in **Appendix B**; Hydraflow surface drainage models provided are described below:

<i>File Name</i>	<i>Description</i>
<i>SurfaceCalcs_West.stm</i>	Surface runoff model for the west halfstreet of Scottsdale Road between Frank Lloyd Wright Blvd and Thompson Peak Pkwy.
<i>SurfaceCalcs_Seg1_East.stm</i>	Surface runoff model for the east halfstreet of Scottsdale Road between Stations 141+93 & 168+04.
<i>SurfaceCalcs_East_N_101.stm</i>	Surface runoff model for east halfstreet of Scottsdale Road between the Loop 101 and Thompson Peak Parkway.
<i>SurfaceCalcs_East_S_Chauncey.stm</i>	Surface runoff model for east halfstreet of Scottsdale Road between Frank Lloyd Wright and Chauncey Lane.

Scuppers are MAG Standard 206, modified to remove the concrete spillway and sidewalk; in order to accommodate the future construction of detached concrete sidewalks along the roadway corridor riprap spillways will be used. Inlet lengths vary from 12 feet to 16 feet. Catch basins are COP Standard P1569-1 M1 or M2.

Two underground storm drain systems exist on the project. The first is located at the northwest corner of Scottsdale Road and Princess Drive. This short 10-year system conveys Scottsdale Road and Princess Drive runoff to an existing culvert beneath Princess Drive. This model is provided in **Appendix B**, filename *Princess\_Stormdrain.stm*. A second underground

storm drain is designed to provide an outfall for retention basins fronting the North Scottsdale Gateway property. This system is described in more detail in **Section V.D.**

### ***B. Offsite Hydrology***

Offsite hydrology results are summarized in the following table and **Figure 3.**

**Table 1 – Offsite Design Flow Summary**

<b>Hydraulic Structure</b>	<b>Location</b>	<b>Source Drainage Report</b>	<b>100-year Flow</b>
<b>Culvert #1</b>	0.37 mi. South of Thompson Peak Parkway	Paradise Ridge, Bob Ward	224 cfs
<b>Culvert #2</b>	150 ft North of Princess Drive	Interim Regional Drainage Channel, Wood Patel	300 cfs
<b>Culvert #3</b>	2-36" Pipes Automall Frontage (Connects to Culvert #2)	Current Study	76 cfs
<b>Channel #1</b>	0.37 mi. South of Thompson Peak Parkway	Paradise Ridge, Bob Ward	224 cfs
<b>Channel #2</b>	Chauncey to Culvert #2	Interim Regional Drainage Channel, Wood Patel	300 cfs

### ***C. Offsite Drainage Design***

There are three offsite drainage features being constructed as part of the Scottsdale Road Segment 2 improvements. Flow rates for each drainage element are presented in **Table 1** and **Figure 3.**

*Channel#1/Culvert#1* is located 0.37 miles south of Thompson Peak Parkway, approximate Scottsdale Road centerline station 188+25. Culvert #1 is a single barrel 10'x3' concrete box culvert (CBC). It crosses the intersection of Scottsdale Road and Center Street from Northeast to Southwest at a 48 degree angle. Channel #1 is designed to accept runoff from existing washes and concentrate runoff at the culvert inlet. It is a shallow trapezoidal channel, with a 10 ft. bottom width, 3:1 sideslopes, and a depth of 3 feet. The relatively short channel is riprap lined due to a steep design slope, chosen to match existing grades. Also, an additional segment of Channel #1 has been designed downstream of Culvert #1 to return the runoff to its historic location. Culvert and channel calculations can be found in **Appendix C.**





**One Scottsdale** (formerly known as the Stack 40's) are a series of parcels planned for commercial development in the coming years. They front Scottsdale Road on the eastern side from Union Hills Drive to Thompson Peak Parkway, and they are being designed concurrently with this project. As part of **One Scottsdale**, the Scottsdale Road scenic easement where *Culvert #1* is being constructed will be redesigned. It will be necessary for the scenic easement to be designed to incorporate the culverts and drainage concept described in this report.

*Culvert#2* is located 150 feet north of Princess Drive, approximate Scottsdale Road centerline station 125+00. Culvert #2 is a double barrel 8'x 3' CBC until it leaves the roadway corridor, at which point it becomes a double barrel 8'x4' CBC. This then ties into the existing box culvert beneath Princess Drive. Calculations for this culvert are done using XPStorm software and are provided in **Appendix C**. *Channel #2* is being designed by Wood, Patel & Associates and is documented in Reference #18.

#### *Culvert #3*

Culvert #2 also receives runoff from the frontage of the Automotive Group Realty automall by way of 2-36" storm drain pipes. The existing channel fronting the automall has been designed to accommodate additional offsite flow. However, at the southern end of the automall property there is no outfall for the channel, it simply ends. Culvert #3 begins here and ties into the box culvert (Culvert #2) crossing Scottsdale Road. As part of this drainage plan the existing low flow crossing at Chauncey Lane is removed and offsite flow is directed south in a channel (Channel #2) designed by Wood, Patel, & Associates. This greatly reduces the runoff reaching the automall frontage. The 100-year peak flow used for the design of Culvert #3 is 76 cfs. The peak flow was calculated using the Rational Method. The time of concentration was calculated based on pipe travel time for the Scottsdale Road storm drain outfalling to the automall frontage (36") plus the travel time in the frontage channel itself. The drainage area includes the drainage area contributing to the Scottsdale Road storm drain, the area of the automall frontage, and the west half-street pavement area between Union Hills Drive and the scupper at station 131+60. Calculations are provided in **Appendix C**.

#### ***D. North Scottsdale Gateway Retention and Outfall Design***

As stated in section III.B.4, North Scottsdale Gateway (NSG) is a triangular shaped site located on the east side of Scottsdale Road, adjacent to and north of the Central Arizona Project Canal (CAP). The property was originally designed to retain both the onsite and offsite 100-year 2hr storm runoff, for which there existed no outfall and which ponded on the site prior to development. The total area of offsite runoff is bounded by the western limit of the Scottsdale Road right-of-way to the west, Princess Drive to the north, the BOR flood control berm to the east, and the CAP canal to south. See **Figure 2** on page 7.

With the widening of Scottsdale Road, the area of paved surface has increased beyond that which the previous drainage design anticipated. Also, the widened roadway extends into the area of the scenic corridor that is currently used for retention. The goal of the current project is to maximize the remaining area within the scenic corridor for retention and provide a system outfall to drain the basins and reduce the likelihood of stormwater runoff entering the CAP canal.

In calculating runoff volume, the relevant watershed area was divided into onsite and offsite areas. Onsite areas refer to the NSG property, the scenic easement, and the roadway half-street fronting the NSG. Offsite areas correspond to the western half street and the area upstream of the NSG property up to Princess Drive. Runoff generated north of Princess Drive drains to conveyances that outfall to the BOR storage impoundment areas. **Figure 4** shows the drainage area boundaries for each proposed retention basin.

Data for the runoff generated on the NSG property is obtained from the drainage report for the project *Master Drainage Report for North Scottsdale Gateway*. Offsite, roadway, and scenic easement runoff volumes are calculated using the equation presented in section 4-1.807 of the DSPM. These calculations were done using a spreadsheet and can be found in **Appendix D**.

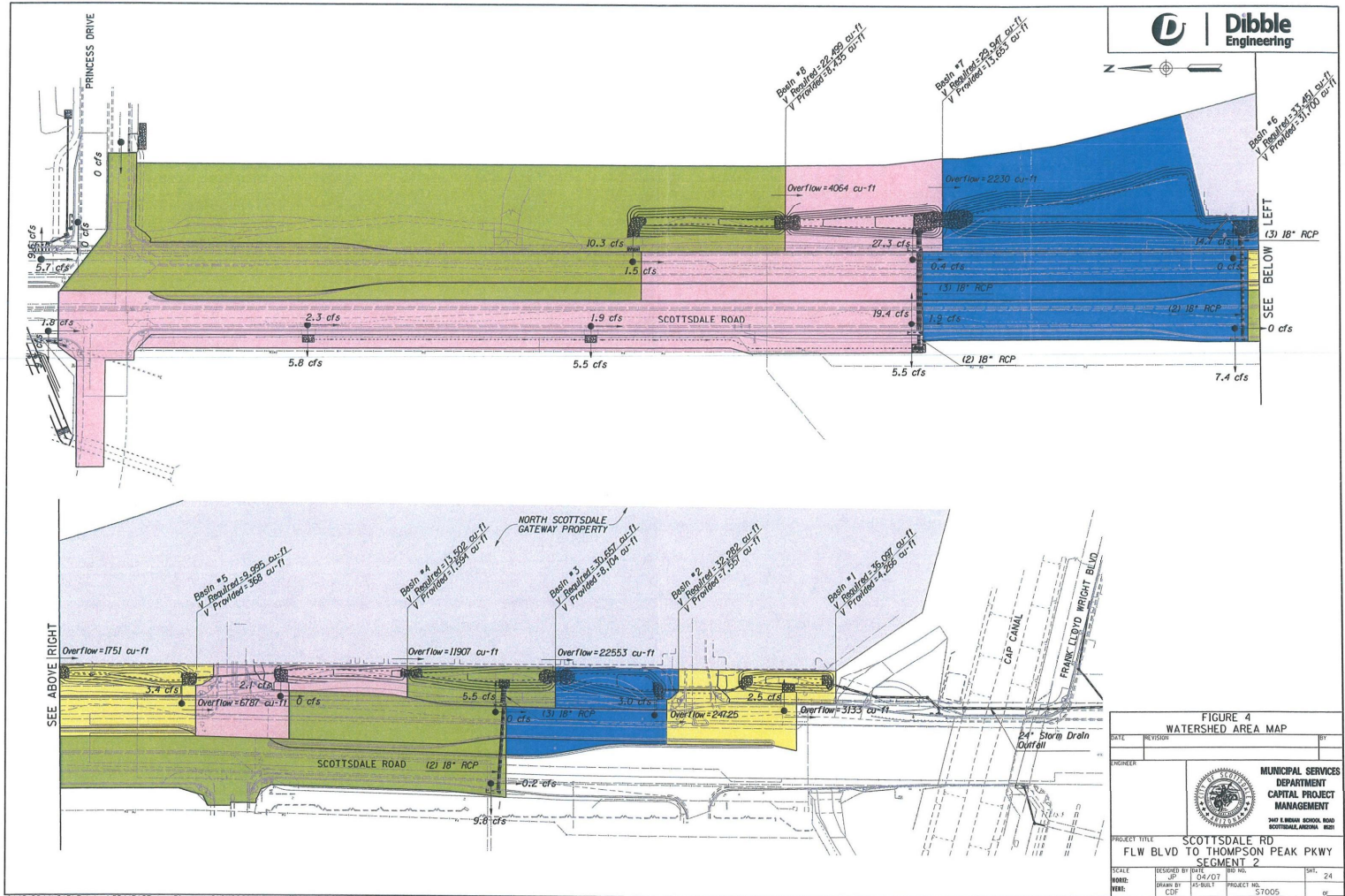
During the planning stage of this project, when it was discovered that the retention basins existing in the scenic easement fronting the NSG would not be large enough to accommodate the 100 year 2 hour runoff volume for both the onsite and offsite runoff reaching the development and the CAP boundary, alternatives were presented to the city for consideration. It was decided at that time that retention basins would be used in the remaining scenic easement area, and a 24 inch outflow pipe would extend from the southernmost basin, across the canal and Frank Lloyd Wright Boulevard, finally tying into an existing 24 inch storm drain at the Promenade development. It was understood that this option would likely not provide 100-yr or 10-yr retention of the watershed area (including the NSG property) but runoff in excess of the provided capacity would outfall in a controlled manner to Scottsdale Road and continue south. Meeting minutes relevant to these discussions are provided in **Appendix D. Table 2** and **Figure 4** present the summary of runoff calculations and the capacity of the associated retention basins. Retention basins are cascading, each overflowing into the next or returning to the street when its capacity is exceeded. Small diameter drain pipes connect each basin so they may drain slowly. It can be seen in **Table 2** that the percent of the 100-year and 10-year volumes that are provided are 72% and 81% respectively. This suggests that the peak runoff values from these storms will be attenuated significantly, reducing the load on the 24" outfall pipe. Based on modeling of the 24" storm drain outfall system, its capacity is approximately 22cfs. However, because of the uncertainties associated with the capacity of the Promenade storm drain it is possible that the system could back up and not be capable of draining runoff from the NSG retention basins. This would be a relatively rare occurrence and last for a short duration. The Hydraflow model for the NSG outfall storm drain system is provided in **Appendix D**, titled *FLW\_Stormdrain.stm*.



**Table 2 – North Scottsdale Gateway Retention Summary**

<b>100 yr 2 hr - Proposed Design</b>				
	Volume Req'd	Volume Provided	Difference	Cumulative Difference
<b>TOTAL BASIN #8</b>	22499	8435	14064	14064
<b>TOTAL BASIN #7</b>	15883	13653	2230	16294
<b>TOTAL BASIN #6</b>	17157	31700	-14543	1751
<b>TOTAL BASIN #5</b>	8204	3168	5036	6787
<b>TOTAL BASIN #4</b>	6715	1594	5121	11907
<b>TOTAL BASIN #3</b>	18750	8104	10646	22553
<b>TOTAL BASIN #2</b>	9729	7557	2172	24725
<b>TOTAL BASIN #1</b>	11372	4766	6606	31331
<b>Total</b>	<b>110308</b>	<b>78977</b>		<b>31331</b>
			<b>% Provided</b>	<b>0.72</b>
<b>10 yr 6 Hour - Proposed Design</b>				
	Volume Req'd	Volume Provided	Difference	Cumulative Difference
<b>TOTAL BASIN #8</b>	16649	8435	8214	8214
<b>TOTAL BASIN #7</b>	11753	13653	-1900	6314
<b>TOTAL BASIN #6</b>	12696	31700	-19004	0
<b>TOTAL BASIN #5</b>	6071	3168	2903	2903
<b>TOTAL BASIN #4</b>	4969	1594	3375	6277
<b>TOTAL BASIN #3</b>	13875	8104	5771	12048
<b>TOTAL BASIN #2</b>	7200	7557	-357	11691
<b>TOTAL BASIN #1</b>	8415	4766	3649	15340
<b>Total</b>	<b>81628</b>	<b>78977</b>		<b>15340</b>
			<b>% Provided</b>	<b>0.81</b>





**Dibble Engineering**

SEE ABOVE RIGHT

SEE BELOW LEFT

(3) 18" RCP

(2) 18" RCP

0 cfs

7.4 cfs

5.5 cfs

19.4 cfs

27.3 cfs

10.3 cfs

1.5 cfs

1.9 cfs

2.3 cfs

5.8 cfs

0 cfs

9.6 cfs

1.8 cfs

5.7 cfs

0 cfs

Princess Drive

Scottsdale Road

Frank Lloyd Wright Blvd

Cap Canal

Storm Drain Outfall

North Scottsdale Gateway Property

**FIGURE 4**  
**WATERSHED AREA MAP**

DATE	REVISION	BY

PROJECT: **SCOTTSDALE RD**  
**FLW BLVD TO THOMPSON PEAK PKWY**  
**SEGMENT 2**

DESIGNED BY: **DAV/OT**  
DRAWN BY: **CDP**  
CHECKED BY: **CDP**  
DATE: **04/07**  
SCALE: **AS SHOWN**  
SHEET: **24**  
TOTAL SHEETS: **24**

**MUNICIPAL SERVICES**  
**DEPARTMENT**  
**CAPITAL PROJECT**  
**MANAGEMENT**

3001 E BROAD AVENUE, SUITE 200  
SCOTTSDALE, ARIZONA 85261

In order to convey the 100-yr 2-hr runoff volume to the retention basins, scuppers, catchbasins and cross road culverts south of Princess Drive have been designed for the 100 -year peak flows using the rational method. Output from the 100-year Hydraflow surface calculations and culvert calculations are provided in **Appendix D**. The following models are provided:

<i>File Name</i>	<i>Description</i>
<i>100+74.44.stm</i>	Analysis of cross road culvert at Station 100+74.44. 100-year peak flow.
<i>107+23.stm</i>	Analysis of cross road culvert at Station 107+23. 100-year peak flow.
<i>111+82.stm</i>	Analysis of cross road culvert at Station 111+82. 100-year peak flow.

## REFERENCES

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7. Erickson & Meeks Engineering, L.L.C., *Preliminary Master Drainage Report for Discount Tire Corporate Headquarters*, Feb. 2001
8. Flood Control District of Maricopa County, Engineering Division, *Drainage Design Manual for Maricopa County, Arizona Volume I, Hydrology*, January 1, 1995.
9. Flood Control District of Maricopa County, Engineering Division, *Drainage Design Manual for Maricopa County, Arizona Volume II, Hydraulics*, January 28, 1996.
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12. KVL Consultants, Inc., *City of Scottsdale Stormwater Master Plan and Management System*, January 2005.
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14. Stanley Consultants Inc., *Scottsdale Road Corridor Drainage Master Plan, Technical Section – Volume 1, Hydrology Analysis Final Report*, November 2002.
15. Ward, Robert L., *Drainage Study, Core North/Core South*, Sep. 2001.
16. Wood, Patel & Associates, *Stacked 40s Rezoning Drainage Report*, Jul. 2002.
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ADOT - HIGHWAY DRAINAGE DESIGN MANUAL - HYDROLOGY  
RAINFALL DEPTH-DURATION-FREQUENCY (D-D-F) WORKSHEET

Project No.: 10-0244.2

TRACS No: N/A

Project Name: Scottsdale Road - Frank Lloyd Wright to

Date: 22-Mar-07

Thompson Peak Pkwy

Location/Sta: MARICOPA COUNTY, AZ

Designer: Josh Papworth

PART A

=====

Rainfall Depths from Isopluvials:

2-year, 6-hour =	1.30 in.
2-year, 24-hour =	1.70 in.
100-year, 6-hour =	3.30 in.
100-year, 24-hour =	4.05 in.

PART B

=====

2-year, 1-hour =	0.93 in.
100-year, 1-hour =	2.52 in.
2-year, 2-hour =	1.05 in.
2-year, 3-hour =	1.14 in.
2-year, 12-hour =	1.50 in.
100-year, 2-hour =	2.79 in.
100-year, 3-hour =	2.97 in.
100-year, 12-hour =	3.68 in.

PART C

=====

Zone = 8 (6 or 8)

2-year, 5-min =	0.31 in.
2-year, 10-min =	0.47 in.
2-year, 15-min =	0.57 in.
2-year, 30-min =	0.76 in.
100-year, 5-min =	0.76 in.
100-year, 10-min =	1.16 in.
100-year, 15-min =	1.49 in.
100-year, 30-min =	2.02 in.

Duration |---- Ratio ----|

(Min) 2-yr 100-yr

5	0.34	0.30
10	0.51	0.46
15	0.62	0.59
30	0.82	0.80

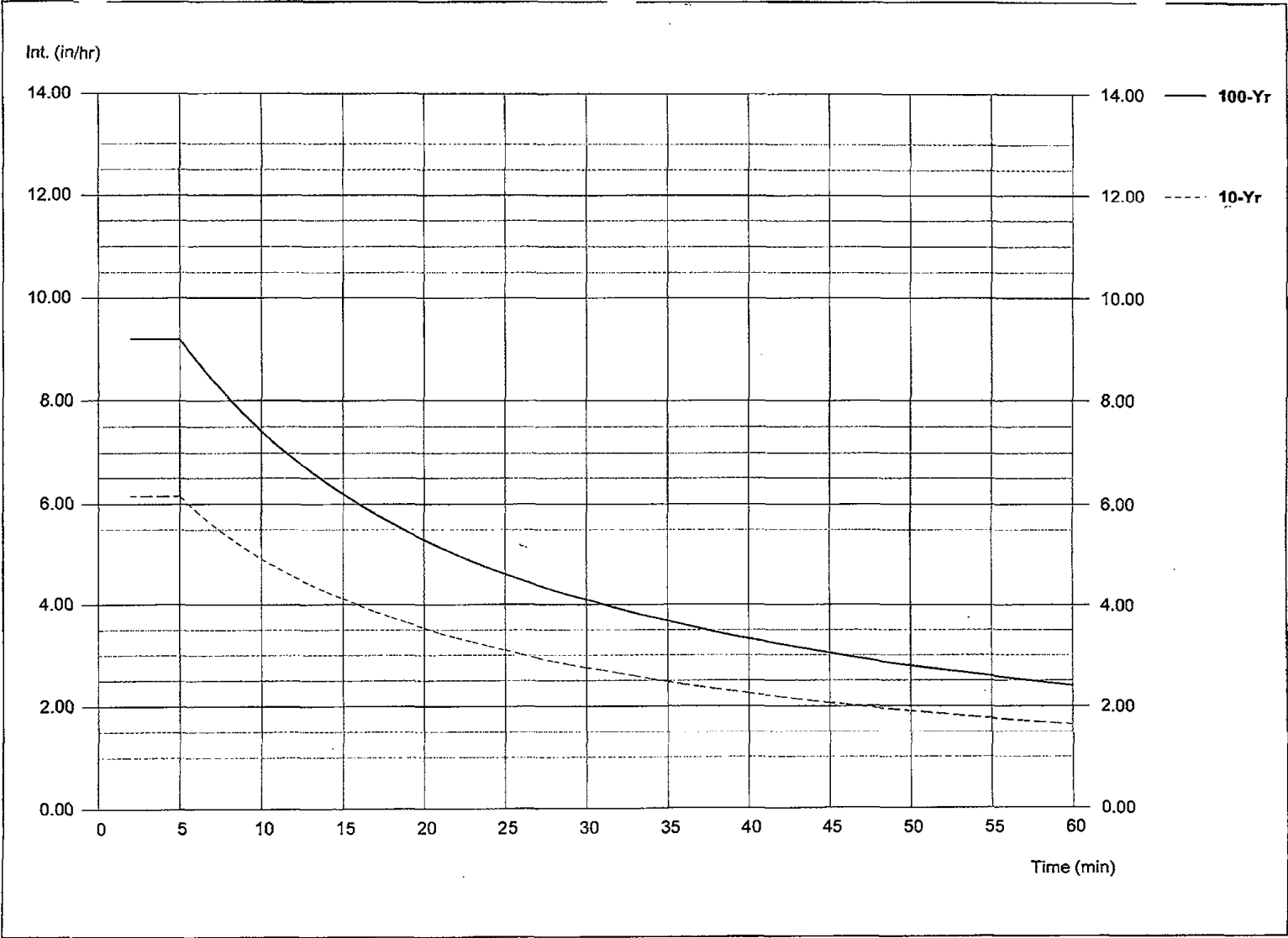
PART D & E

=====

Duration	Rainfall Depth, (in)					
	Frequency (yrs)					
	2-yr	5-yr	10-yr	25-yr	50-yr	500-yr
5-min =	0.31	0.42	0.50	0.60	0.68	0.94
10-min =	0.47	0.64	0.76	0.92	1.04	1.44
15-min =	0.57	0.80	0.95	1.16	1.33	1.86
30-min =	0.76	1.07	1.28	1.57	1.80	2.53
1-hour =	0.93	1.33	1.59	1.96	2.24	3.17
2-hour =	1.05	1.49	1.77	2.17	2.48	3.50
3-hour =	1.14	1.59	1.90	2.32	2.64	3.71
6-hour =	1.30	1.79	2.13	2.59	2.95	4.12
12-hour =	1.50	2.03	2.39	2.90	3.29	4.57
24-hour =	1.70	2.27	2.66	3.21	3.63	5.02

Storm Sewer IDF Curves

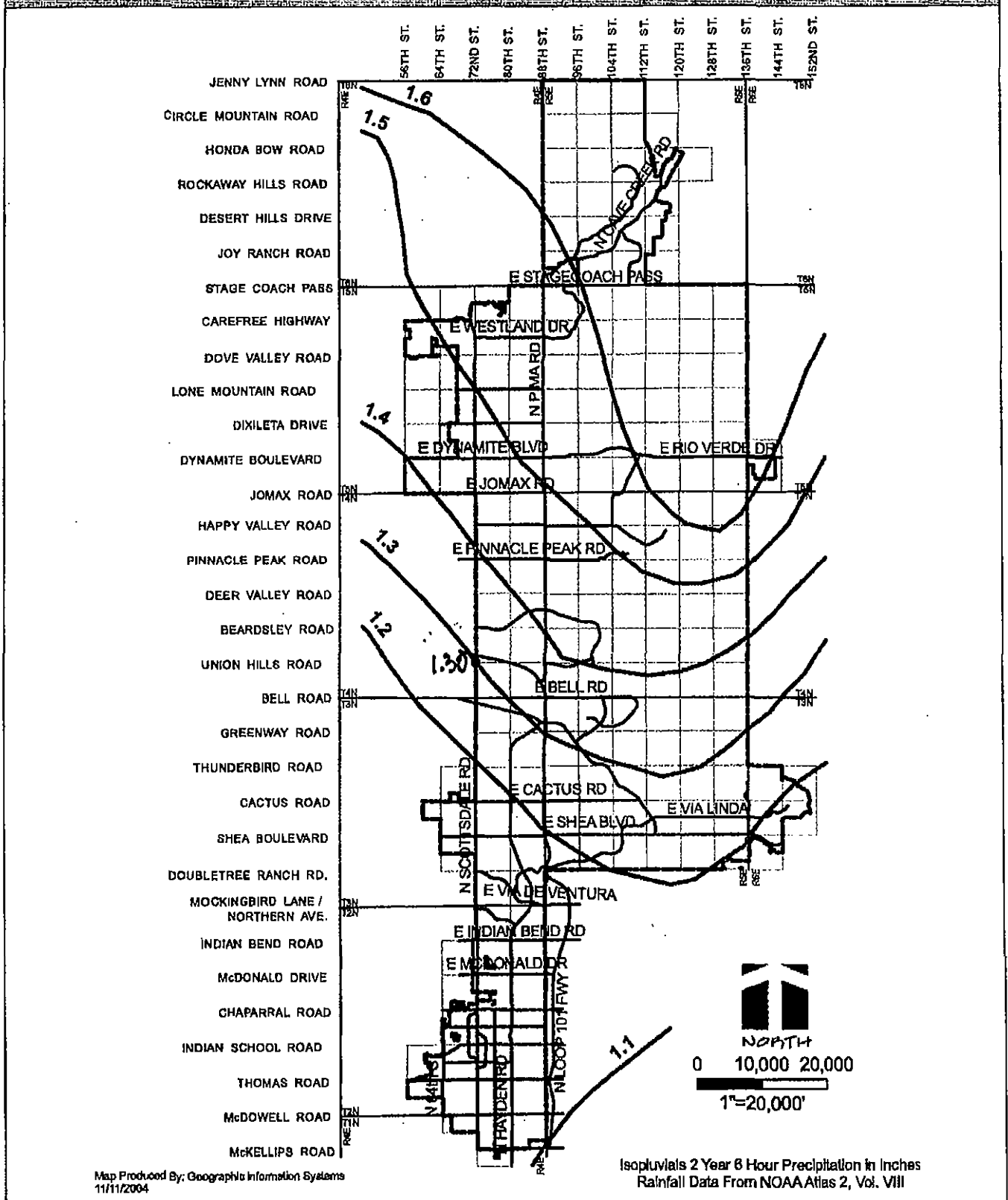
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# ISOPLUVIALS

## 2 Year 6 Hour Precipitation in Inches

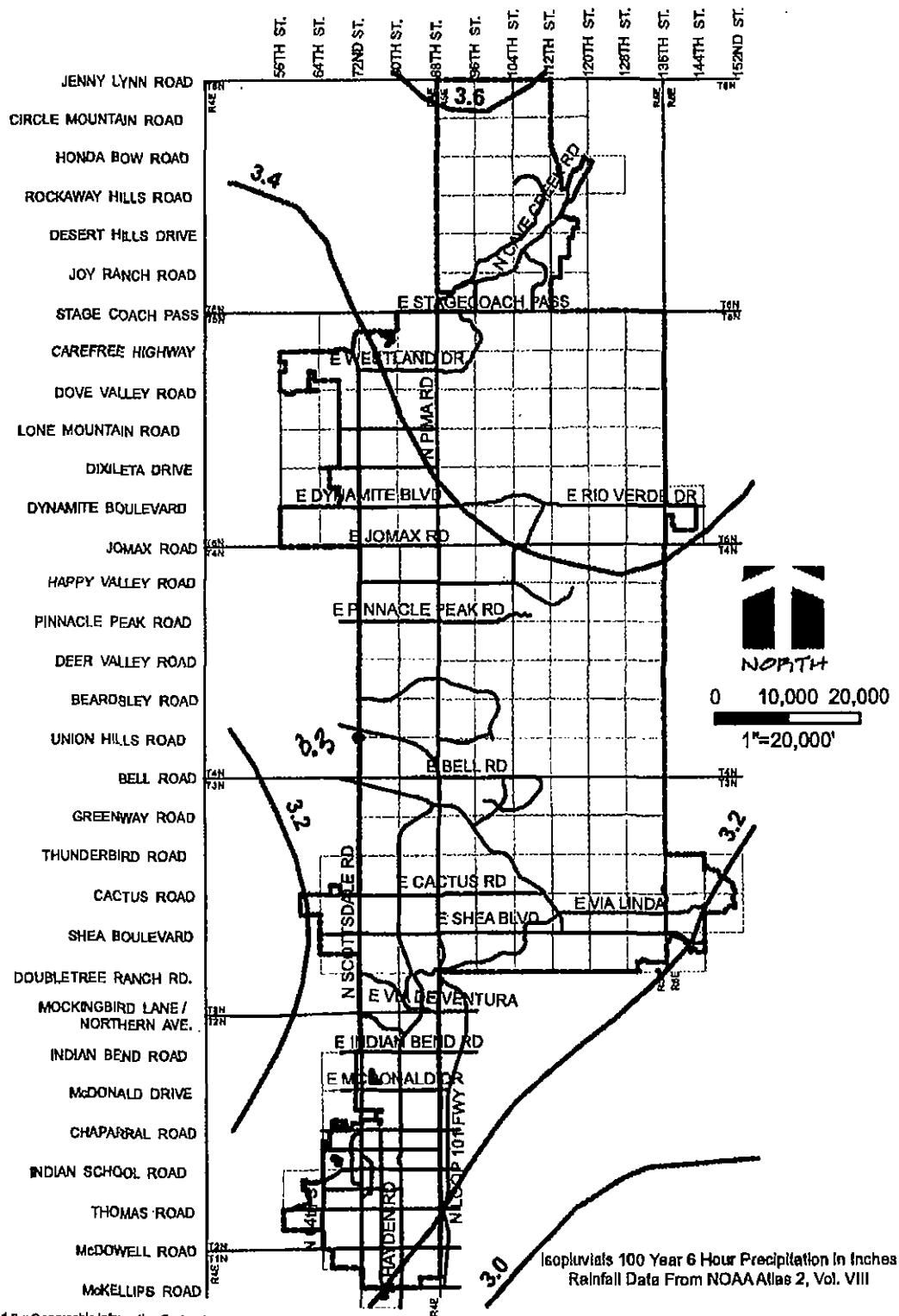






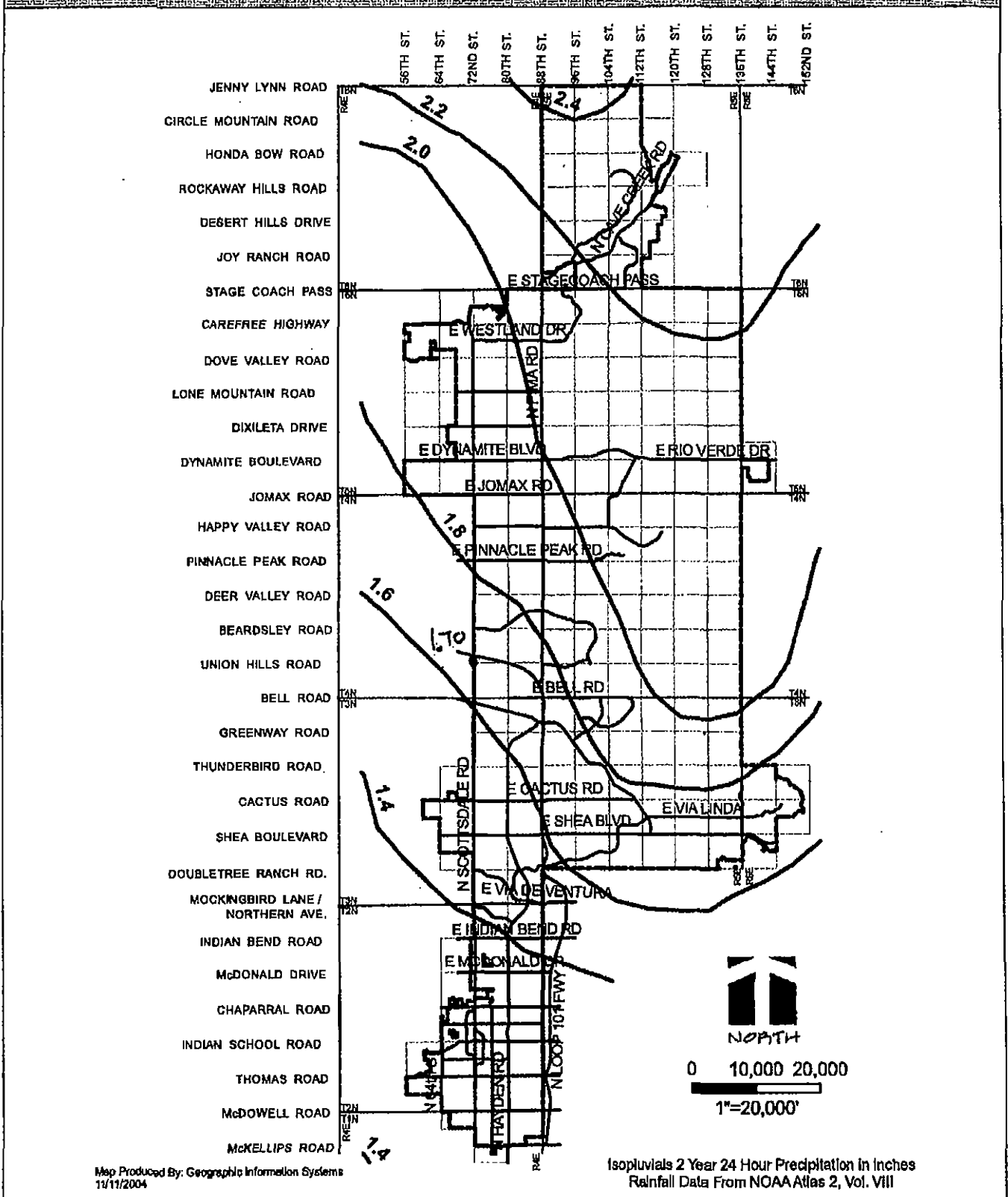
# ISOPLUVIALS

## 100 Year 6 Hour Precipitation in Inches



# ISOPLUVIALS

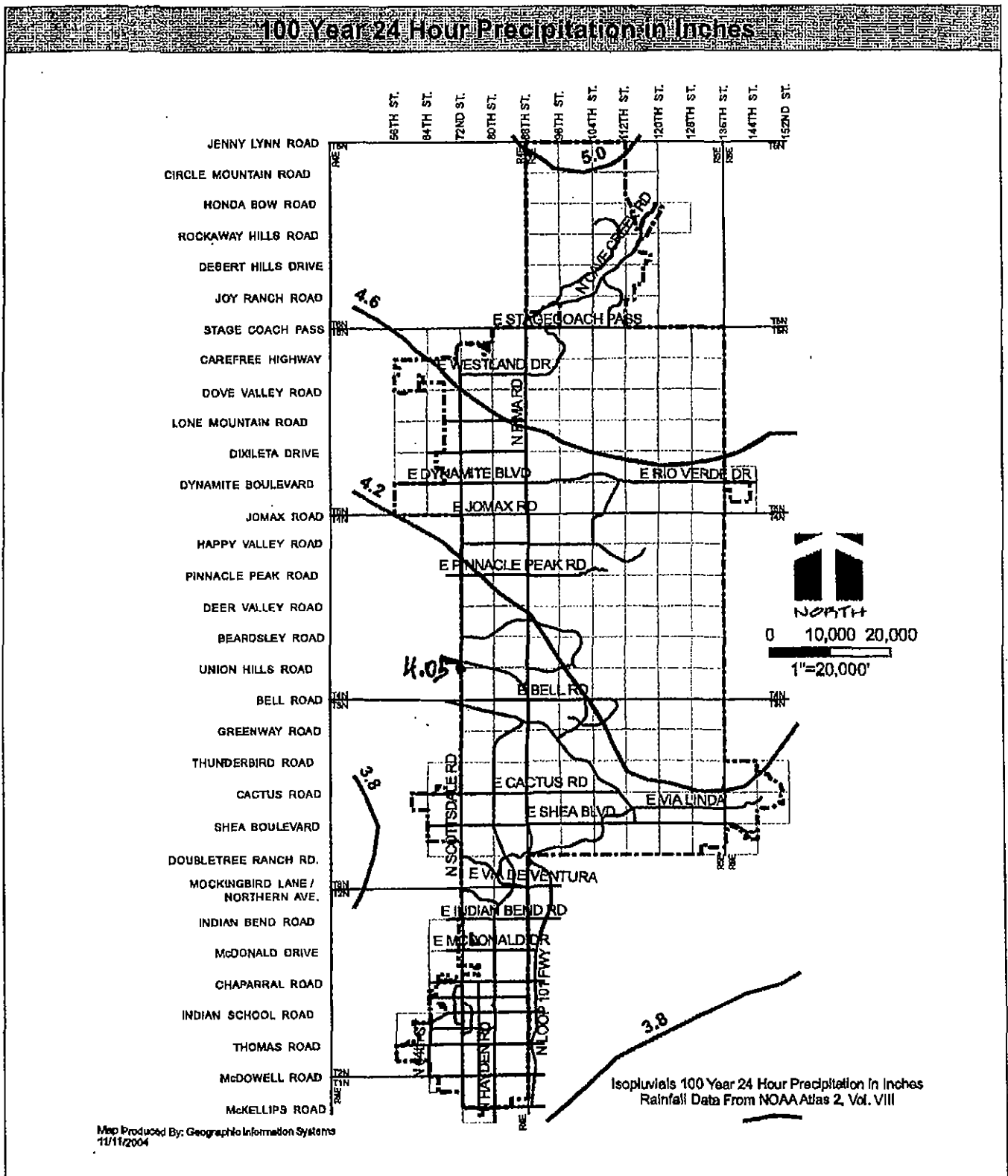
2 Year 24 Hour Precipitation in Inches





# ISOPLUVIALS

## 100 Year 24 Hour Precipitation in Inches



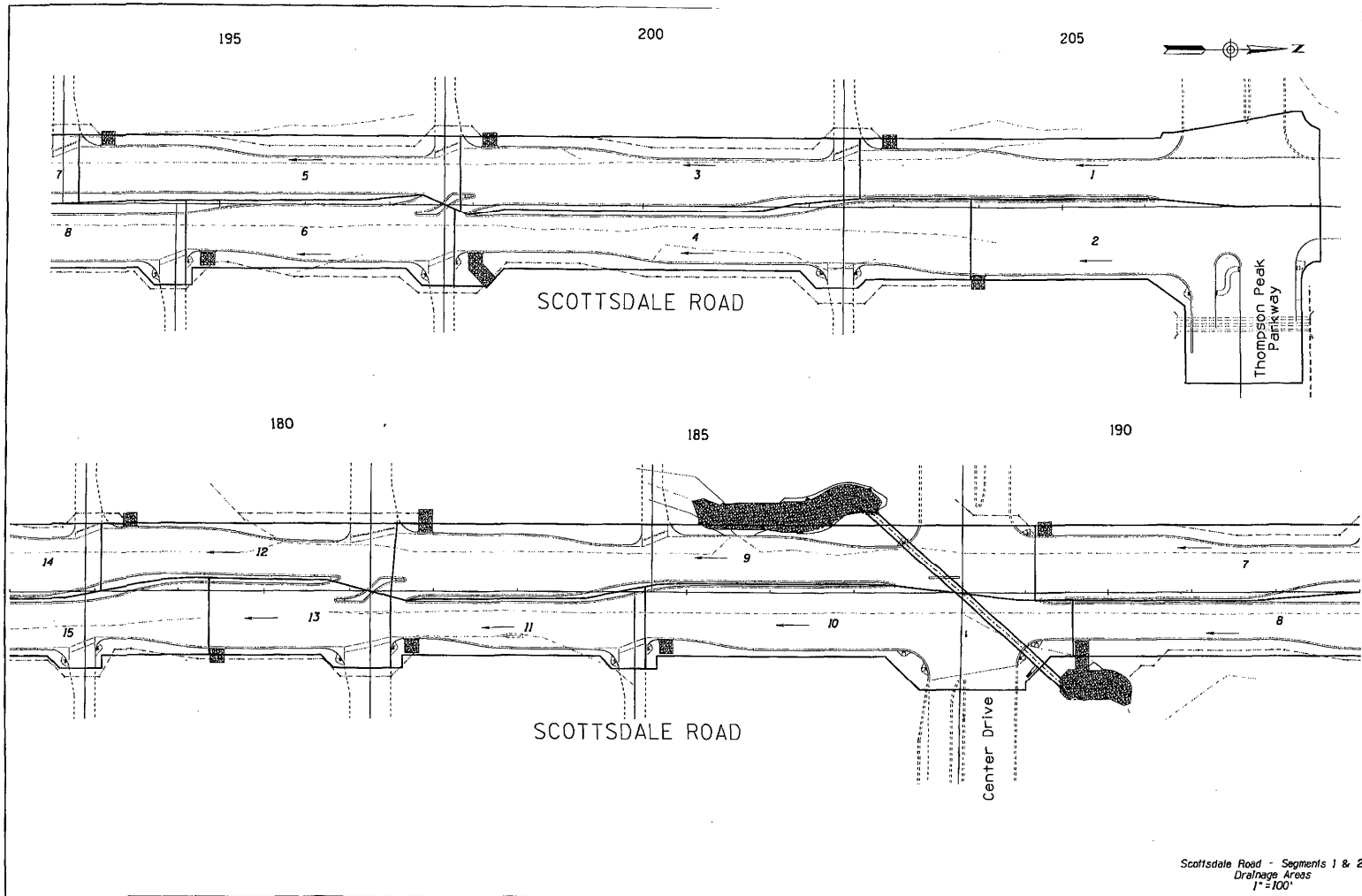




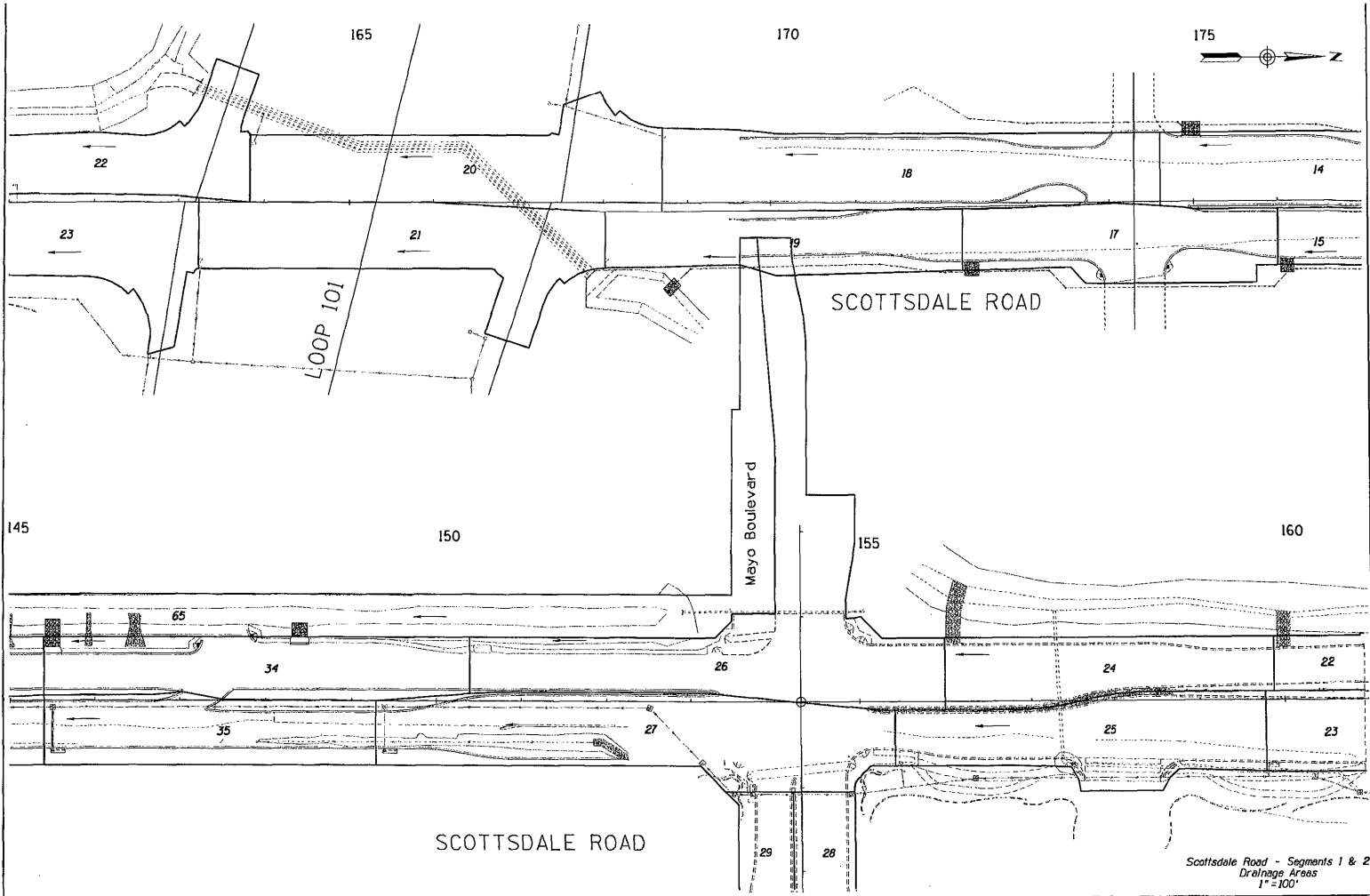


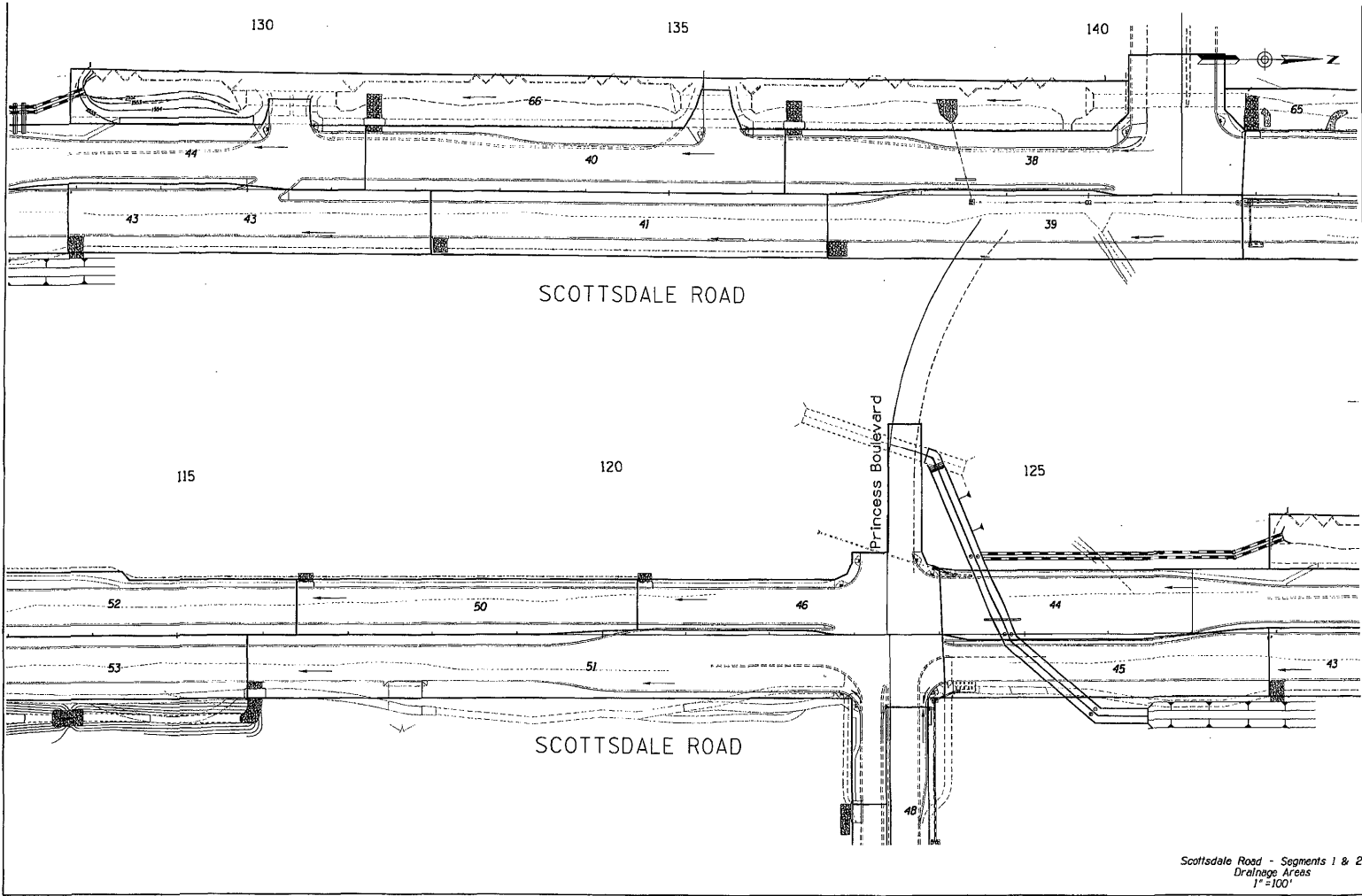
Scottsdale Road - Segment 2  
Drainage Area Summary Sheet

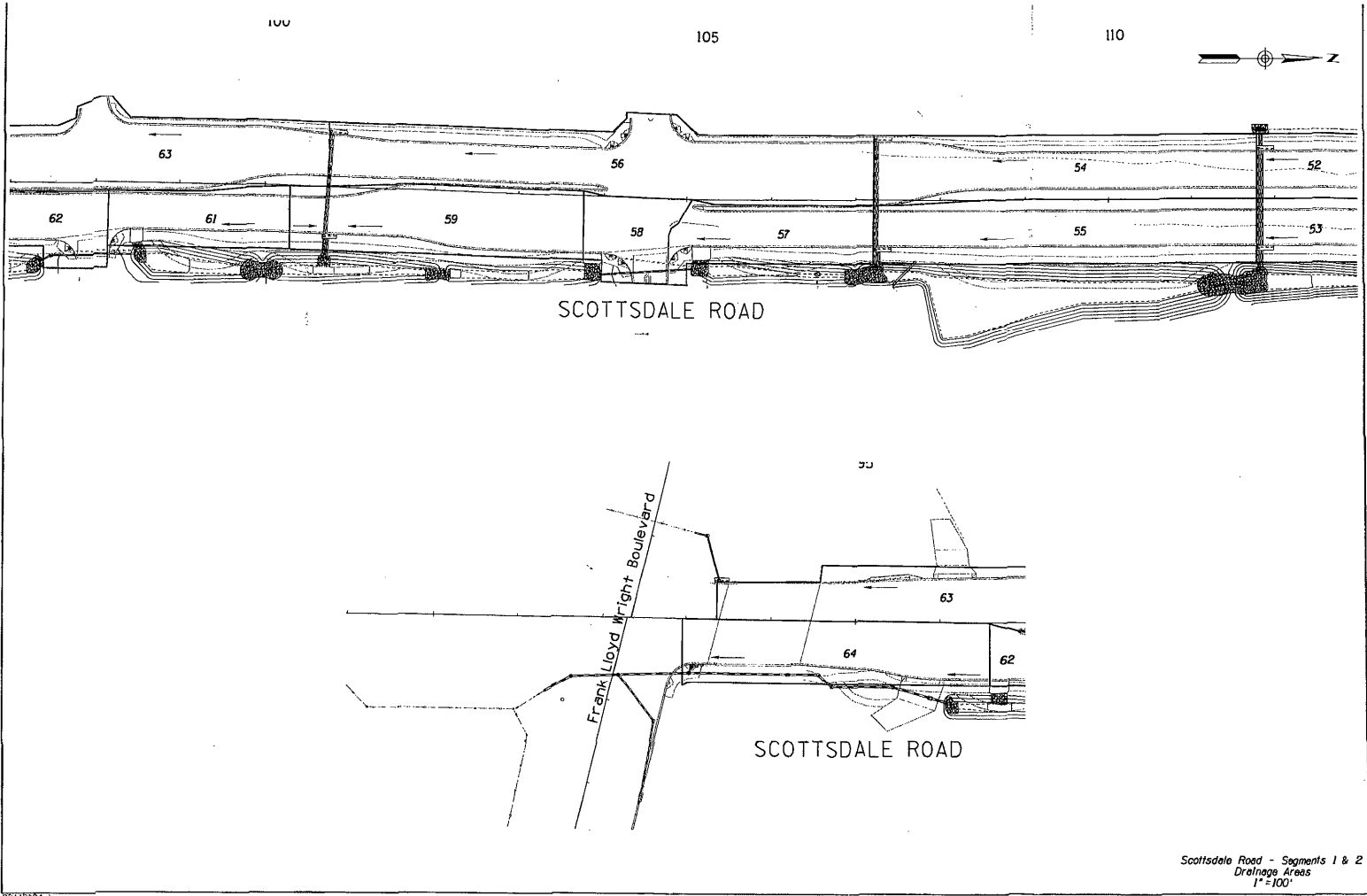
Drainage Area	AREA (ac)	S-1 (ft/ft)	S-x (ft/ft)	Lc (min.)
1	0.998	0.016	0.022	5
2	1.284	0.025	0.020	5
3	0.917	0.015	0.018	5
4	1.118	0.015	0.022	5
5	0.784	0.015	0.020	5
6	0.811	0.015	0.021	5
7	0.844	0.018	0.010	5
8	0.836	0.017	0.014	5
9	1.377	0.015	0.018	5
10	1.077	0.006	0.020	5
11	0.492	0.011	0.024	5
12	0.553	0.015	0.025	5
13	0.443	0.020	0.019	5
14	0.696	0.024	0.019	5
15	0.593	0.012	0.026	5
16	0.398	0.012	0.020	5
17	0.703	0.013	0.025	5
18	0.800	0.018	0.020	5
19	0.674	0.017	0.020	5
20	0.989	0.018	0.020	5
21	0.951	0.013	0.020	5
22	0.741	0.015	0.024	5
23	0.844	0.014	0.014	5
24	0.653	0.007	0.021	5
25	0.845	0.000	0.022	5
26	1.510	0.016	0.026	5
27	1.245	0.011	0.022	5
28	0.242	0.0072	0.013	5
29	0.238	0.0041	0.023	5
30	0.221	0.0055	0.017	5
31	0.809	0.0000	0.021	5
32	0.400	0.0040	0.023	5
33	0.694	0.0000	0.03	5
34	0.819	0.013	0.023	5
35	0.701	0.013	0.016	5
36	0.627	0.012	0.009	5
37	0.597	0.013	0.012	5
38	1.148	0.017	0.025	5
39	0.889	0.016	0.022	5
40	0.911	0.011	0.025	5
41	0.814	0.016	0.022	5
42	0.877	0.018	0.014	5
43	0.770	0.007	0.021	5
44	1.310	0.013	0.010	5
45	0.632	0.009	0.011	5
46	0.718	0.014	0.024	5
47	0.785	0.014	0.021	5
48	0.252	0.0060	0.017	5
49	0.100	0.0120	0.023	5
50	0.591	0.012	0.021	5
51	0.699	0.012	0.023	5
52	0.750	0.014	0.022	5
53	0.793	0.014	0.022	5
54	0.797	0.008	0.024	5
55	0.778	0.005	0.028	5
56	1.140	0.009	0.033	5
57	0.390	0.013	0.027	5
58	0.238	0.017	0.009	5
59	0.632	0.006	0.022	5
60	0.818	0.006	0.025	5
61	0.337	0.010	0.029	5
62	0.278	0.008	0.031	5
63	0.424	0.012	0.015	5
64	0.623	0.012	0.019	5
65	2.980	-	-	5
66	2.060	-	-	5











DIBBLE & ASSOCIATES  
CONSULTING ENGINEERS

Scottsdale Road  
Channel Design

Date 23-Mar-07  
Job No. 10-0244  
By JEP  
RCE  
Chk'd B.JF  
Filepath: J:\10-0244\EXCEL\RAINAGECHANNELDES.xls

# TYPICAL SECTION / MANNING'S RATING CURVE

Channel: SCOTTSDALE ROAD - Typical Calculation for Roadside Ditch - 10Yr

## INPUT DATA:

Manning's n = 0.024 Compacted Soil  
T allow = 0.30 lb/ft^2  
Sideslope Left = 4.0 :1  
Sideslope Right = 4.0 :1  
Bottom slope = 0.0 percent

Reach	Slope	BW (ft)	t	Topwidth											
				0.92	4.43	0.024	15.0	1.15	0.42	1.00	1.92	7.36	15.36	22.08	0.20
Roadside Ditch	0.0150	0.0	0.0	0.79	4.00	0.024	10.0	1.12	0.36	1.00	1.79	6.32	14.32	18.97	0.17
Roadside Ditch	0.0150	0.0	0.0	0.61	3.37	0.024	5.0	1.07	0.28	1.00	1.61	4.88	12.88	14.63	0.12
Roadside Ditch	0.0100	0.0	0.0	0.99	3.80	0.024	15.0	0.95	0.30	1.00	1.99	7.94	15.94	23.83	0.15
Roadside Ditch	0.0100	0.0	0.0	0.85	3.44	0.024	10.0	0.93	0.26	1.00	1.85	6.82	14.82	20.47	0.12
Roadside Ditch	0.0100	0.0	0.0	0.66	2.89	0.024	5.0	0.89	0.20	1.00	1.66	5.26	13.26	15.78	0.09
Roadside Ditch	0.0050	0.0	0.0	1.13	2.93	0.024	15.0	0.69	0.17	1.00	2.13	9.05	17.05	27.14	0.09
Roadside Ditch	0.0050	0.0	0.0	0.97	2.65	0.024	10.0	0.67	0.15	1.00	1.97	7.77	15.77	23.31	0.07
Roadside Ditch	0.0050	0.0	0.0	0.75	2.23	0.024	5.0	0.64	0.11	1.00	1.75	5.99	13.99	17.97	0.06

# Hydraflow Storm Sewers Extension for AutoCAD® Civil 3D® 2009 Plan

Outfall 1 93+40 L1 2 100+78 L1 3 107+84 L1 111+80 L1 116+50 L1 120+50 L1 124+20 L1 8 131+60 L1 136+50 L1

Project File: SurfaceCalcs\_West.stm

Number of lines: 23

Date: 03-02-2009

Hydraflow Storm Sewers Extension v6.066

# Hydraflow Storm Sewers Extension for AutoCAD® Civil 3D® 2009 Plan

+95 Lt 11    145+50 Lt 12    150+50 Lt SC 1    155+25 Lt SC 2    160+00 Lt SC 3    163+91 Lt    16    168+71 Lt 17    18    174+95 Lt    178+42 Lt 19    181+90 Lt

Project File: SurfaceCalcs\_West.stn

Number of lines: 23

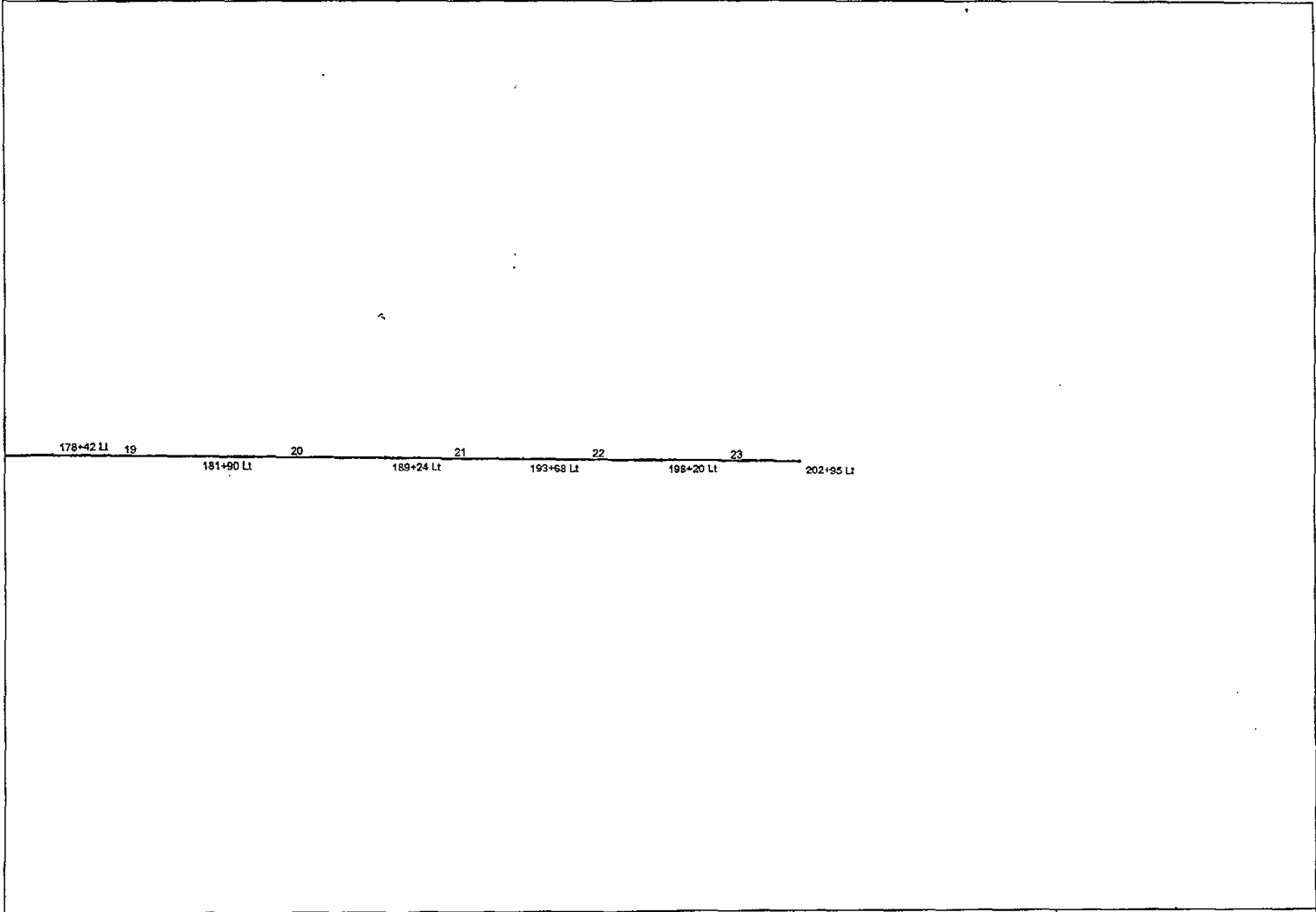
Date: 03-02-2009

Hydraflow Storm Sewers Extension v6.066

2/1



Hyd flow Storm Sewers Extension for AutoCAD® Civil 3D® 2009 Plan



178+42 Lt 19 181+80 Lt 20 189+24 Lt 21 193+68 Lt 22 198+20 Lt 23 202+95 Lt

Project File: SurfaceCalcs_West.stm	Number of lines: 23	Date: 03-02-2009
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112

# Storr Sewer Tabulation

Page 1

Station		Len (ft)	Dmg Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
1	End	50.0	1.06	20.99	0.95	1.01	19.94	5.0	310.9	0.4	7.52	0.00	0.27	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
2	1	840.0	1.14	19.93	0.95	1.08	18.93	5.0	295.7	0.4	7.49	0.00	0.26	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
3	2	730.0	0.80	18.79	0.95	0.76	17.85	5.0	282.4	0.4	7.38	0.00	0.26	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
4	3	270.0	0.75	17.99	0.95	0.71	17.09	5.0	277.4	0.4	7.18	0.00	0.25	72	0.00	1.00	1.00	7.01	7.00	0.00	0.00	Dummy Line
5	4	470.0	0.59	17.24	0.95	0.56	16.38	5.0	268.6	0.4	7.10	0.00	0.25	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
6	5	400.0	0.72	16.65	0.95	0.68	15.82	5.0	261.1	0.4	7.04	0.00	0.25	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
7	6	365.0	0.43	15.93	0.95	0.41	15.13	5.0	254.2	0.5	6.91	0.00	0.24	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
8	7	235.0	0.88	15.50	0.95	0.84	14.73	5.0	249.8	0.5	6.84	0.00	0.24	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
9	8	500.0	0.91	14.62	0.95	0.86	13.89	5.0	240.1	0.5	6.70	0.00	0.24	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
10	9	355.0	1.15	13.71	0.95	1.09	13.02	5.0	233.1	0.5	6.46	0.00	0.23	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
11	10	500.0	0.63	12.56	0.95	0.60	11.93	5.0	222.8	0.5	6.18	0.00	0.22	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
12	11	475.0	0.82	11.93	0.95	0.78	11.33	5.0	213.0	0.5	6.12	0.00	0.22	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
13	12	475.0	1.51	11.11	0.95	1.43	10.55	5.0	203.0	0.6	5.96	0.00	0.21	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
14	13	391.0	0.79	9.60	0.95	0.75	9.12	5.0	194.0	0.6	5.38	0.00	0.19	72	0.00	1.00	1.00	7.02	7.01	0.00	0.00	Dummy Line
15	14	475.0	0.75	8.81	0.95	0.71	8.37	5.0	182.6	0.6	5.22	0.00	0.18	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
16	15	391.0	0.68	8.06	0.95	0.65	7.66	5.0	172.9	0.7	5.02	0.00	0.18	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
17	16	874.0	1.20	7.38	0.95	1.14	7.01	5.0	152.1	0.7	5.18	0.00	0.18	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
18	17	359.2	0.70	6.18	0.95	0.67	5.87	5.0	142.4	0.8	4.60	0.00	0.16	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
19	18	540.0	0.55	5.48	0.95	0.52	5.21	5.0	127.3	0.9	4.52	0.00	0.16	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
20	19	515.0	1.38	4.93	0.95	1.31	4.68	5.0	112.9	1.0	4.52	0.00	0.16	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
21	20	685.0	0.84	3.55	0.95	0.80	3.37	5.0	89.6	1.2	3.99	0.00	0.14	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
Project File: SurfaceCalcs_West.stm																Number of lines: 24				Run Date: 03-22-2007		
NOTES: Intensity = 129.35 / (Inlet time + 15.50) ^ 1.01; Return period = 10 Yrs.																						

# Storm Sewer Tabulation

Page 2

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (I) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
22	21	500.0	0.79	2.71	0.95	0.75	2.57	5.0	69.8	1.5	3.75	0.00	0.13	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
23	22	500.0	0.92	1.92	0.95	0.87	1.82	5.0	45.4	2.1	3.74	0.00	0.13	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
24	23	500.0	1.00	1.00	0.95	0.95	0.95	5.0	5.0	6.1	5.84	0.00	0.21	72	0.00	1.00	1.00	7.02	7.02	0.00	0.00	Dummy Line
Project File: SurfaceCalcs_West.stm																Number of lines: 24				Run Date: 03-22-2007		
NOTES: Intensity = 129.35 / (Inlet time + 15.50) ^ 1.01; Return period = 10 Yrs.																						

# Inlet Report

Page 1

Line No	Inlet ID	Q = CIA (cfs)	Q carry (cfs)	Q capt (cfs)	Q byp (cfs)	Junc type	Curb Inlet		Grate Inlet			Gutter							Inlet			Byp line No
							Ht (in)	L (ft)	area (sqft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	Depth (ft)	Spread (ft)	Depth (ft)	Spread (ft)	Depr (in)	
1	93+40 Lt	6.19	0.00	4.92	1.27	Curb	3.0	12.80	0.00	0.00	0.00	0.012	1.42	0.058	0.015	0.015	0.30	15.86	0.47	14.67	3.0	Off
2	100+78 Lt	6.66	0.00	6.66	0.00	Curb	3.0	16.00	0.00	0.00	0.00	0.009	1.42	0.058	0.033	0.015	0.38	10.59	0.57	9.76	3.0	1
3	107+24 Lt	4.67	0.07	4.74	0.00	Curb	3.0	16.00	0.00	0.00	0.00	Sag	1.42	0.058	0.024	0.000	0.26	8.84	0.46	8.84	3.0	Off
4	111+80 Lt	4.38	0.72	5.03	0.07	Curb	3.0	16.00	0.00	0.00	0.00	0.014	1.42	0.058	0.022	0.015	0.30	11.27	0.47	10.09	3.0	3
5	116+50 Lt	3.44	0.73	3.45	0.72	Curb	3.0	9.60	0.00	0.00	0.00	0.012	1.42	0.058	0.021	0.015	0.28	11.07	0.45	9.76	3.0	4
6	120+50 Lt	4.20	0.04	3.51	0.73	Curb	3.0	9.60	0.00	0.00	0.00	0.014	1.42	0.058	0.024	0.015	0.29	9.95	0.46	8.67	3.0	5
7	124+20 Lt	7.65	2.88	10.49	0.04	Curb	3.0	29.60	0.00	0.00	0.00	0.010	1.42	0.058	0.013	0.015	0.35	22.59	0.52	21.68	3.0	6
8	131+60 Lt	5.32	3.11	5.55	2.88	Curb	3.0	9.60	0.00	0.00	0.00	0.011	1.42	0.058	0.025	0.015	0.38	13.25	0.56	12.40	3.0	7
9	136+50 Lt	6.71	3.55	7.15	3.11	Curb	3.0	12.80	0.00	0.00	0.00	0.017	1.42	0.058	0.025	0.015	0.37	13.13	0.56	12.28	3.0	8
10	141+95 Lt	3.68	3.64	3.77	3.55	Curb	3.0	9.60	0.00	0.00	0.00	0.012	1.42	0.058	0.009	0.015	0.28	23.27	0.45	22.00	3.0	9
11	145+50 Lt	4.79	4.35	5.49	3.64	Curb	3.0	9.60	0.00	0.00	0.00	0.013	1.42	0.058	0.023	0.015	0.37	13.93	0.55	13.04	3.0	10
12	150+50 Lt SC 1	8.82	1.35	5.82	4.35	Curb	3.0	9.60	0.00	0.00	0.00	0.016	1.42	0.058	0.026	0.015	0.38	12.91	0.56	12.08	3.0	11
13	155+25 Lt SC 2	4.61	1.40	4.67	1.35	Curb	3.0	9.60	0.00	0.00	0.00	0.007	1.42	0.058	0.021	0.015	0.35	14.12	0.53	13.19	3.0	12
14	160+00 Lt SC 3	4.38	1.08	4.06	1.40	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.024	0.015	0.31	10.82	0.48	9.67	3.0	13
15	163+91 Lt	3.97	2.38	5.27	1.08	Curb	3.0	12.80	0.00	0.00	0.00	0.013	1.42	0.058	0.020	0.015	0.32	13.20	0.49	12.10	3.0	14
16	168+71 Lt	7.01	1.27	5.90	2.38	Curb	3.0	12.80	0.00	0.00	0.00	0.018	1.42	0.058	0.020	0.015	0.33	13.75	0.50	12.70	3.0	15
17	174+95 Lt	4.09	3.90	6.72	1.27	Curb	3.0	12.80	0.00	0.00	0.00	0.012	1.42	0.058	0.029	0.015	0.38	11.65	0.56	10.79	3.0	16
18	178+42 Lt	3.21	6.31	5.62	3.90	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.025	0.015	0.37	13.09	0.55	12.20	3.0	17
19	181+90 Lt	8.06	3.96	5.72	6.31	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.018	0.015	0.37	17.51	0.55	16.67	3.0	18
20	189+24 Lt	4.90	2.78	3.73	3.96	Curb	3.0	9.60	0.00	0.00	0.00	0.018	1.42	0.058	0.010	0.015	0.27	20.58	0.44	19.20	3.0	19
21	193+68 Lt	4.61	2.75	4.58	2.78	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.020	0.015	0.33	13.60	0.50	12.55	3.0	20
22	198+20 Lt	5.37	1.75	4.37	2.75	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.018	0.015	0.31	14.34	0.49	13.22	3.0	21
23	202+95 Lt	5.84	0.00	4.09	1.75	Curb	3.0	9.60	0.00	0.00	0.00	0.016	1.42	0.058	0.022	0.015	0.31	11.59	0.48	10.41	3.0	22

Project File: SurfaceCalcs\_West.stm

Number of lines: 23

Run Date: 03-02-2009

NOTES: Inlet N-Values = 0.016 ; Intensity = 129.35 / (Inlet time + 15.50) ^ 1.01; Return period = 10 Yrs.; \* Indicates Known Q added. All curb Inlets are Horiz throat.

Hydraflow Storm Sewers Extension v6.06i

2/5

# Inlet Report

Page 1

Line No	Inlet ID	Q = CIA	Q carry	Q capt	Q byp	Junc type	Curb Inlet		Grate Inlet			Gutter						Inlet			Byp line No	
		(cfs)	(cfs)	(cfs)	(cfs)		Ht (in)	L (ft)	area (sqft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	Depth (ft)	Spread (ft)	Depth (ft)	Spread (ft)		Depr (in)
1	93+40 Lt	9.26	0.58	6.41	3.43	Curb	3.0	12.80	0.00	0.00	0.00	0.012	1.42	0.058	0.015	0.015	0.35	19.00	0.52	18.00	3.0	Off
2	100+78 Lt	9.96	0.00	9.38	0.58	Curb	3.0	16.00	0.00	0.00	0.00	0.009	1.42	0.058	0.033	0.015	0.44	12.35	0.63	11.64	3.0	1
3	107+24 Lt	6.99	1.96	8.95	0.00	Curb	3.0	16.00	0.00	0.00	0.00	Sag	1.42	0.058	0.024	0.000	0.37	13.53	0.57	13.53	3.0	Off
4	111+80 Lt	6.55	3.74	8.33	1.96	Curb	3.0	16.00	0.00	0.00	0.00	0.014	1.42	0.058	0.022	0.015	0.38	14.77	0.56	13.91	3.0	3
5	116+50 Lt	5.16	4.02	5.43	3.74	Curb	3.0	9.60	0.00	0.00	0.00	0.012	1.42	0.058	0.021	0.015	0.37	14.97	0.55	14.10	3.0	4
6	120+50 Lt	6.29	3.40	5.67	4.02	Curb	3.0	9.60	0.00	0.00	0.00	0.014	1.42	0.058	0.024	0.015	0.38	13.70	0.56	12.83	3.0	5
7	124+20Lt	11.45	9.53	17.57	3.40	Curb	3.0	29.60	0.00	0.00	0.00	0.010	1.42	0.058	0.013	0.015	0.43	29.39	0.61	28.72	3.0	6
8	131+60 Lt	7.96	9.89	8.32	9.53	Curb	3.0	9.60	0.00	0.00	0.00	0.011	1.42	0.058	0.025	0.015	0.49	17.65	0.67	17.00	3.0	7
9	136+50 Lt	10.05	10.27	10.44	9.89	Curb	3.0	12.80	0.00	0.00	0.00	0.017	1.42	0.058	0.025	0.015	0.47	17.05	0.66	16.40	3.0	8
10	141+95 Lt	5.51	10.12	5.35	10.27	Curb	3.0	9.60	0.00	0.00	0.00	0.012	1.42	0.058	0.009	0.015	0.35	31.16	0.52	30.22	3.0	9
11	145+50 Lt	7.17	10.78	7.83	10.12	Curb	3.0	9.60	0.00	0.00	0.00	0.013	1.42	0.058	0.023	0.015	0.46	18.01	0.65	17.35	3.0	10
12	150+50 Lt SC 1	13.20	5.62	8.03	10.78	Curb	3.0	9.60	0.00	0.00	0.00	0.016	1.42	0.058	0.026	0.015	0.47	16.33	0.66	15.69	3.0	11
13	155+25 Lt SC 2	6.90	5.87	7.15	5.62	Curb	3.0	9.60	0.00	0.00	0.00	0.007	1.42	0.058	0.021	0.015	0.45	18.83	0.63	18.19	3.0	12
14	160+00 Lt SC 3	6.55	5.64	6.33	5.87	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.024	0.015	0.40	14.74	0.58	13.96	3.0	13
15	163+91 Lt	5.94	8.03	8.33	5.64	Curb	3.0	12.80	0.00	0.00	0.00	0.013	1.42	0.058	0.020	0.015	0.41	17.85	0.59	17.10	3.0	14
16	168+71 Lt	10.49	6.16	8.62	8.03	Curb	3.0	12.80	0.00	0.00	0.00	0.018	1.42	0.058	0.020	0.015	0.41	17.95	0.59	17.20	3.0	15
17	174+95 Lt	6.12	10.55	10.50	6.16	Curb	3.0	12.80	0.00	0.00	0.00	0.012	1.42	0.058	0.029	0.015	0.49	15.41	0.68	14.79	3.0	16
18	178+42 Lt	4.81	13.70	7.96	10.55	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.025	0.015	0.47	16.85	0.65	16.20	3.0	17
19	181+90 Lt	12.06	9.22	7.57	13.70	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.018	0.015	0.45	21.79	0.63	21.11	3.0	18
20	189+24 Lt	7.34	6.79	4.91	9.22	Curb	3.0	9.60	0.00	0.00	0.00	0.018	1.42	0.058	0.010	0.015	0.33	25.98	0.50	25.00	3.0	19
21	193+68 Lt	6.90	6.04	6.15	6.79	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.020	0.015	0.39	16.90	0.57	16.10	3.0	20
22	198+20 Lt	8.04	3.63	5.64	6.04	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.018	0.015	0.37	17.34	0.55	16.44	3.0	21
23	202+95 Lt	8.74	0.00	5.11	3.63	Curb	3.0	9.60	0.00	0.00	0.00	0.016	1.42	0.058	0.022	0.015	0.35	13.54	0.53	12.55	3.0	22

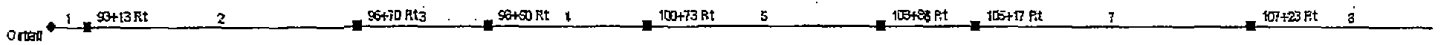
Project File: SurfaceCalcs\_West.stm

Number of lines: 23

Run Date: 03-02-2009

NOTES: Inlet N-Values = 0.016 ; Intensity = 301.57 / (Inlet time + 18.30) ^ 1.11; Return period = 100 Yrs ; \* Indicates Known Q added. All curb inlets are Horiz throat.

# Hydratow Plan View



Project file: SurfaceCalcsEast\_S\_Chauncey.stm

No. Lines: 13

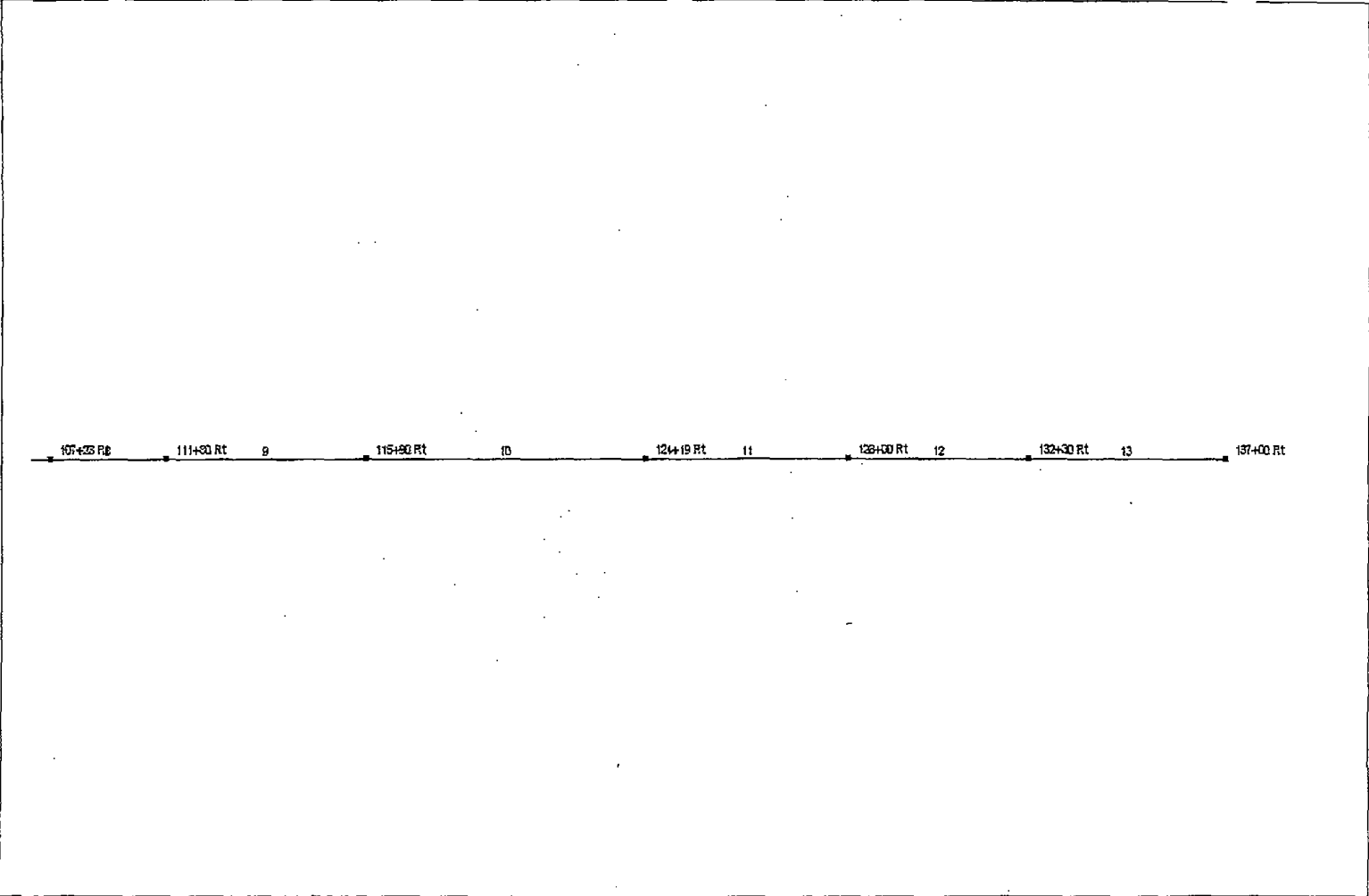
03-22-2007

Hydratow Storm Sewers 2003

41



Hydraflow Plan View



Project file: SurfaceCalcsEast_S_Chauncey.stm	No. Lines: 13	03-22-2007
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# Storm Sewer Tabulation

Page 1

Station		Len (ft)	Drng Area		Rnoff coeff (C)	Area x C		Tc		Rain (l) (in/hr)	Total flow (cfs)	Cap full (cfs)	Vel (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr (ac)	Total (ac)		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
1	End	50.0	0.62	8.72	0.95	0.59	8.29	5.0	173.5	0.7	6.03	0.00	3.03	72	0.00	1.00	1.00	1.88	1.64	0.00	0.00	Dummy Line
2	1	370.0	0.28	8.10	0.95	0.27	7.70	5.0	164.6	0.7	5.85	0.00	0.21	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
3	2	180.0	0.34	7.82	0.95	0.32	7.43	5.0	160.3	0.8	5.78	0.00	0.20	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
4	3	219.0	0.63	7.48	0.95	0.60	7.11	5.0	154.9	0.8	5.69	0.00	0.20	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
5	4	320.0	0.24	6.85	0.95	0.23	6.51	5.0	146.8	0.8	5.45	0.00	0.19	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
6	5	131.0	0.39	6.61	0.95	0.37	6.28	5.0	143.4	0.8	5.36	0.00	0.19	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
7	6	380.0	0.78	6.22	0.95	0.74	5.91	5.0	133.6	0.9	5.34	0.00	0.19	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
8	7	278.0	0.79	5.44	0.95	0.75	5.17	5.0	125.8	0.9	4.92	0.00	0.17	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
9	8	472.0	0.70	4.65	0.95	0.67	4.42	5.0	111.6	1.0	4.63	0.00	0.16	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
10	9	668.9	1.48	3.95	0.95	1.41	3.76	5.0	91.1	1.2	4.62	0.00	0.16	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
11	10	484.2	0.77	2.47	0.95	0.73	2.35	5.0	70.3	1.4	3.56	0.00	0.13	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
12	11	430.0	0.81	1.70	0.95	0.77	1.62	5.0	46.6	2.0	3.32	0.00	0.12	72	0.00	1.00	1.00	7.01	7.00	0.00	0.00	Dummy Line
13	12	470.0	0.89	0.89	0.95	0.85	0.85	5.0	5.0	6.1	5.33	0.00	0.19	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line

Project File: SurfaceCalcsEast\_S\_Chancey.stm

Number of lines: 13

Run Date: 03-22-2007

NOTES: Intensity =  $64.98 / (\text{Inlet time} + 10.30)^{0.87}$ ; Return period = 10 Yrs.

# Inlet Report

Page 1

Line No	Inlet ID	Q = CIA	Q carry	Q capt	Q byp	Junc type	Curb Inlet		Grate Inlet			Gutter							Inlet			Byp line No
		(cfs)	(cfs)	(cfs)	(cfs)		Ht (in)	L (ft)	area (sqft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	depth (ft)	spread (ft)	depth (ft)	spread (ft)	Dep (in)	
1	93+13 Rt	3.60	0.00	2.98	0.62	Curb	3.0	7.20	0.00	0.00	0.00	0.012	1.42	0.058	0.019	0.015	0.27	11.30	0.43	9.63	3.00	Off
2	96+70 Rt	1.63	0.00	1.63	0.00	Curb	3.0	12.80	0.00	0.00	0.00	0.008	1.42	0.058	0.031	0.015	0.24	6.51	0.40	4.87	3.00	1
3	98+50 Rt	1.97	0.00	1.97	0.00	Curb	3.0	9.60	0.00	0.00	0.00	0.010	1.42	0.058	0.029	0.015	0.25	7.20	0.41	5.38	3.00	2
4	100+73 Rt	3.66	0.00	3.66	0.00	Curb	3.0	16.00	0.00	0.00	0.00	Sag	1.42	0.058	0.022	0.000	0.23	8.10	0.43	8.10	3.00	Off
5	103+88 Rt	1.39	0.00	1.39	0.00	Curb	3.0	12.80	0.00	0.00	0.00	0.017	1.42	0.058	0.009	0.015	0.17	11.16	0.31	7.22	3.00	4
6	105+17 Rt	2.26	0.00	2.26	0.00	Curb	3.0	12.80	0.00	0.00	0.00	0.013	1.42	0.058	0.027	0.015	0.25	7.63	0.40	5.67	3.00	5
7	107+23 Rt	4.53	0.00	4.53	0.00	Curb	3.0	16.00	0.00	0.00	0.00	0.005	1.42	0.058	0.028	0.015	0.36	11.34	0.54	10.39	3.00	6
8	111+80 Rt	4.59	0.00	4.59	0.00	Curb	3.0	16.00	0.00	0.00	0.00	0.014	1.42	0.058	0.022	0.015	0.29	10.86	0.46	9.55	3.00	7
9	115+90 Rt	4.06	1.70	5.76	0.00	Curb	3.0	16.00	0.00	0.00	0.00	0.012	1.42	0.058	0.023	0.015	0.33	12.19	0.50	10.78	3.00	8
10	124+19 Rt	8.62	0.26	7.18	1.70	Curb	3.0	12.80	0.00	0.00	0.00	0.009	1.42	0.058	0.015	0.015	0.35	19.26	0.52	18.33	3.00	9
11	128+00 Rt	4.47	0.67	4.88	0.26	Curb	3.0	10.40	0.00	0.00	0.00	0.007	1.42	0.058	0.021	0.015	0.34	13.69	0.51	12.29	3.00	10
12	132+30 Rt	4.70	0.66	4.69	0.67	Curb	3.0	10.40	0.00	0.00	0.00	0.016	1.42	0.058	0.022	0.015	0.30	11.31	0.47	10.00	3.00	11
13	137+00 Rt	5.33*	0.00	4.67	0.66	Curb	3.0	10.40	0.00	0.00	0.00	0.016	1.42	0.058	0.022	0.015	0.30	11.31	0.47	9.95	3.00	12
Project File: SurfaceCalcsEast_S_Chauncey.stm I-D-F File: ScottsdaleIDF.IDF Number of lines: 13 Run Date: 03-22-2007																						
NOTES: Inlet N-Values = 0.016 ; Intensity = 64.98 / (Inlet time + 10.30) ^ 0.87; Return period = 10 Yrs.; * Indicates Known Q added																						

Hydraflo Storm Sewers 2000

5/1h

# Inlet Report

Page 1

Line No	Inlet ID	Q = CIA	Q carry	Q capt	Q byp	Junc type	Curb Inlet		Grate Inlet			Gutter							Inlet			Byp line No
		(cfs)	(cfs)	(cfs)	(cfs)		Ht (in)	L (ft)	area (sq ft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	depth (ft)	spread (ft)	depth (ft)	spread (ft)	Dep (in)	
1	93+13 Rt	5.42	0.00	3.73	1.69	Curb	3.0	7.20	0.00	0.00	0.00	0.012	1.42	0.058	0.019	0.015	0.31	13.40	0.47	11.84	3.00	Off
2	96+70 Rt	2.45	0.00	2.45	0.00	Curb	3.0	12.80	0.00	0.00	0.00	0.008	1.42	0.058	0.031	0.015	0.28	7.80	0.45	6.32	3.00	1
3	98+50 Rt	2.97	0.00	2.97	0.00	Curb	3.0	9.60	0.00	0.00	0.00	0.010	1.42	0.058	0.029	0.015	0.28	8.24	0.45	6.90	3.00	2
4	100+73 Rt	5.51	0.00	5.51	0.00	Curb	3.0	16.00	0.00	0.00	0.00	Sag	1.42	0.058	0.022	0.000	0.29	10.65	0.48	10.65	3.00	Off
5	103+88 Rt	2.10	0.00	2.10	0.00	Curb	3.0	12.80	0.00	0.00	0.00	0.017	1.42	0.058	0.009	0.015	0.19	13.38	0.34	10.33	3.00	4
6	105+17 Rt	3.41	0.00	3.41	0.00	Curb	3.0	12.80	0.00	0.00	0.00	0.013	1.42	0.058	0.027	0.015	0.28	8.74	0.45	7.26	3.00	5
7	107+23 Rt	6.82	0.44	7.26	0.00	Curb	3.0	16.00	0.00	0.00	0.00	0.005	1.42	0.058	0.028	0.015	0.43	13.84	0.61	12.82	3.00	6
8	111+80 Rt	6.90	1.52	7.98	0.44	Curb	3.0	16.00	0.00	0.00	0.00	0.014	1.42	0.058	0.022	0.015	0.36	14.04	0.53	12.73	3.00	7
9	115+90 Rt	6.12	5.67	10.27	1.52	Curb	3.0	16.00	0.00	0.00	0.00	0.012	1.42	0.058	0.023	0.015	0.41	15.67	0.59	14.83	3.00	8
10	124+19 Rt	12.97	2.29	9.58	5.67	Curb	3.0	12.80	0.00	0.00	0.00	0.009	1.42	0.058	0.015	0.015	0.42	23.93	0.59	23.00	3.00	9
11	128+00 Rt	6.73	2.75	7.19	2.29	Curb	3.0	10.40	0.00	0.00	0.00	0.007	1.42	0.058	0.021	0.015	0.41	17.02	0.59	16.05	3.00	10
12	132+30 Rt	7.08	2.03	6.36	2.75	Curb	3.0	10.40	0.00	0.00	0.00	0.016	1.42	0.058	0.022	0.015	0.36	14.04	0.53	12.82	3.00	11
13	137+00 Rt	7.94*	0.00	5.90	2.03	Curb	3.0	10.40	0.00	0.00	0.00	0.016	1.42	0.058	0.022	0.015	0.34	13.13	0.51	12.05	3.00	12

Project File: SurfaceCalcsEast\_S\_Chauncey.strm

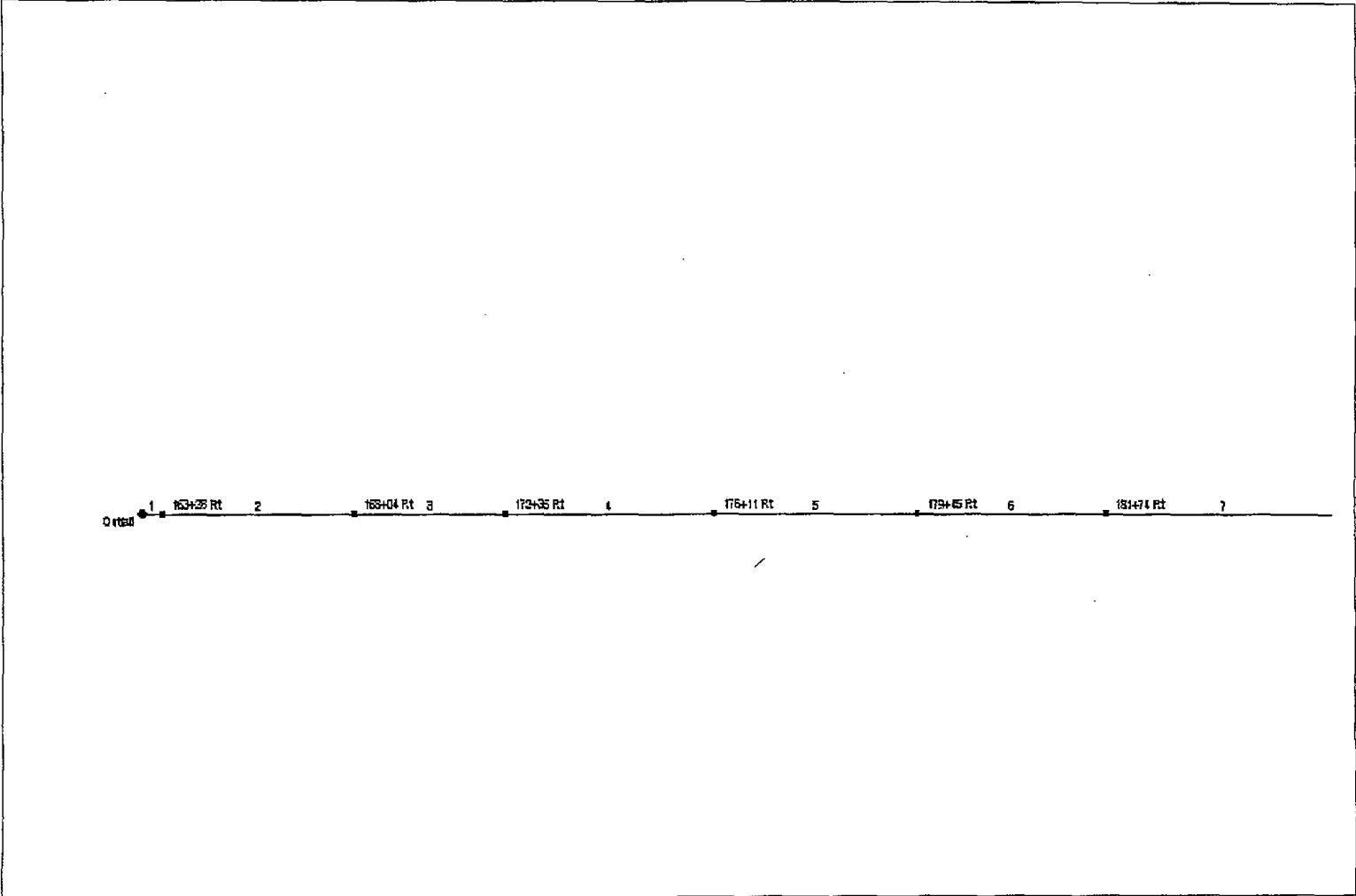
I-D-F File: ScottsdaleIDF.IDF

Number of lines: 13

Run Date: 03-23-2007

NOTES: Inlet N-Values = 0.016 ; Intensity = 301.57 / (Inlet time + 18.30) ^ 1.11; Return period = 100 Yrs ; \* Indicates Known Q added

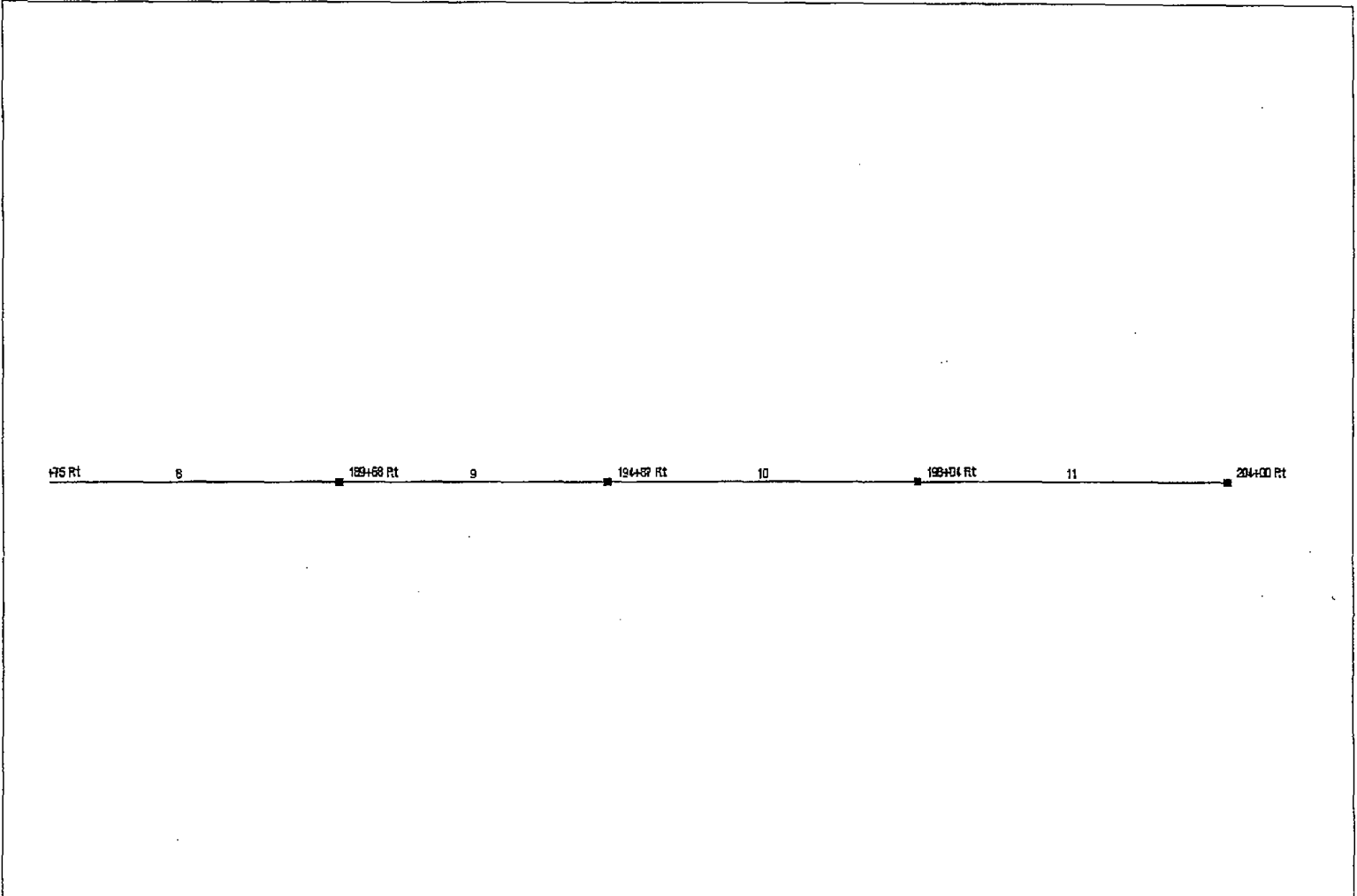
Hydraflow Plan View



Project file: SurfaceCalcsEast_N_101.stm	No. Lines: 11	03-22-2007
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11

Hydraflow Plan View



Project file: SurfaceCalcsEast_N_101.stm	No. Lines: 11	03-22-2007
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5/2

# Storm Sewer Tabulation

Page 1

Station		Len  (ft)	Drng Area		Rnoff coeff  (C)	Area x C		Tc		Rain (l)  (in/hr)	Total flow  (cfs)	Cap full  (cfs)	Vel  (ft/s)	Pipe		Invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr  (ac)	Total  (ac)		Incr  (min)	Total  (min)	Inlet  (min)	Syst  (min)					Size  (in)	Slope  (%)	Up  (ft)	Dn  (ft)	Up  (ft)	Dn  (ft)	Up  (ft)	Dn  (ft)	
1	End	50.0	0.48	8.31	0.95	0.45	7.89	5.0	165.8	0.7	5.38	0.00	2.84	72	0.00	1.00	1.00	1.83	1.63	0.00	0.00	Dummy Line
2	1	476.0	0.67	7.83	0.95	0.64	7.44	5.0	153.7	0.7	5.44	0.00	0.19	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
3	2	376.0	0.70	7.18	0.95	0.67	6.80	5.0	143.9	0.8	5.28	0.00	0.19	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
4	3	520.0	0.59	6.45	0.95	0.56	6.13	5.0	129.8	0.9	5.22	0.00	0.18	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
5	4	508.6	0.44	5.86	0.95	0.42	5.57	5.0	115.9	0.9	5.25	0.00	0.19	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
6	5	469.3	0.49	5.42	0.95	0.47	5.15	5.0	103.1	1.0	5.39	0.00	0.19	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
7	6	595.0	1.08	4.93	0.95	1.02	4.68	5.0	87.1	1.2	5.67	0.00	0.20	72	0.00	1.00	1.00	7.00	7.00	0.00	0.00	Dummy Line
8	7	510.0	0.84	3.85	0.95	0.79	3.66	5.0	71.4	1.4	5.24	0.00	0.19	72	0.00	1.00	1.00	7.01	7.00	0.00	0.00	Dummy Line
9	8	432.0	0.61	3.01	0.95	0.58	2.86	5.0	56.0	1.7	4.99	0.00	0.18	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
10	9	500.0	1.12	2.40	0.95	1.06	2.28	5.0	36.4	2.4	5.49	0.00	0.19	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
11	10	500.0	1.28	1.28	0.95	1.22	1.22	5.0	5.0	6.1	7.50	0.00	0.27	72	0.00	1.00	1.00	7.01	7.01	0.00	0.00	Dummy Line
Project File: SurfaceCalcsEast_N_101.stm																Number of lines: 11				Run Date: 03-22-2007		
NOTES: Intensity = 129.35 / (Inlet time + 15.50) ^ 1.01; Return period = 10 Yrs.																						



# Inlet report

Page 1

Line No	Inlet ID	Q = CIA	Q carry	Q capt	Q byp	Junc type	Curb Inlet		Grate Inlet			Gutter						Inlet			Byp line No	
		(cfs)	(cfs)	(cfs)	(cfs)		Ht (in)	L (ft)	area (sqft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	depth (ft)	spread (ft)	depth (ft)	spread (ft)		Dep (in)
1	163+28 Rt	2.77	0.01	2.79	0.00	Curb	3.0	12.80	0.00	0.00	0.00	0.013	1.42	0.058	0.020	0.015	0.25	9.80	0.41	7.90	3.00	Off
2	168+04 Rt	3.94	0.23	4.15	0.01	Curb	3.0	12.80	0.00	0.00	0.00	0.017	1.42	0.058	0.020	0.015	0.27	10.80	0.43	9.20	3.00	1
3	172+35 Rt	4.10	0.05	3.92	0.23	Curb	3.0	9.60	0.00	0.00	0.00	0.013	1.42	0.058	0.025	0.015	0.30	10.13	0.46	8.52	3.00	2
4	176+11 Rt	3.46	0.08	3.50	0.05	Curb	3.0	9.60	0.00	0.00	0.00	0.012	1.42	0.058	0.026	0.015	0.29	9.41	0.45	7.81	3.00	3
5	179+45 Rt	2.59	0.38	2.89	0.08	Curb	3.0	9.60	0.00	0.00	0.00	0.020	1.42	0.058	0.019	0.015	0.24	9.72	0.39	7.47	3.00	4
6	181+74 Rt	2.87	1.86	4.35	0.38	Curb	3.0	9.60	0.00	0.00	0.00	0.011	1.42	0.058	0.024	0.015	0.31	10.91	0.48	9.75	3.00	5
7	184+75 Rt	6.29	1.90	6.33	1.86	Curb	3.0	9.60	0.00	0.00	0.00	0.006	1.42	0.058	0.020	0.015	0.40	17.30	0.57	16.10	3.00	6
8	189+68 Rt	4.88	1.56	4.54	1.90	Curb	3.0	9.60	0.00	0.00	0.00	0.017	1.42	0.058	0.014	0.015	0.29	16.25	0.45	14.43	3.00	7
9	194+87 Rt	3.56	3.02	5.03	1.56	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.021	0.015	0.32	12.74	0.49	11.52	3.00	8
10	198+04 Rt	6.53	2.51	6.02	3.02	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.022	0.015	0.36	14.04	0.53	12.95	3.00	9
11	204+00 Rt	7.50	0.00	4.98	2.51	Curb	3.0	9.60	0.00	0.00	0.00	0.025	1.42	0.058	0.020	0.015	0.31	12.80	0.47	11.20	3.00	10

Project File: SurfaceCalcsEast_N_101.stm										I-D-F File: ScottsdaleIDF.IDF					Number of lines: 11					Run Date: 03-22-2007				
NOTES: Inlet N-Values = 0.016 ; Intensity = 129.35 / (Inlet time + 15.50) ^ 1.01; Return period = 10 Yrs ; * Indicates Known Q added																								

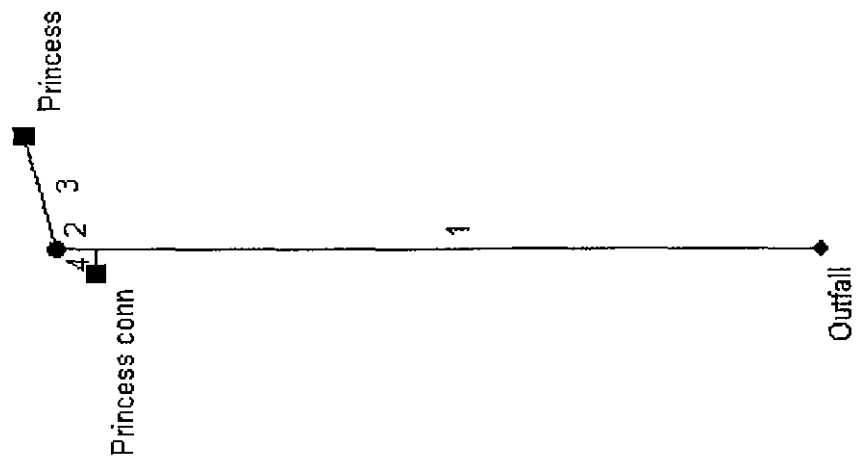
514

# Inlet Report

Page 1

Line No	Inlet ID	Q = CIA	Q carry	Q capt	Q byp	Junc type	Curb Inlet		Grate Inlet			Gutter							Inlet			Byp line No
		(cfs)	(cfs)	(cfs)	(cfs)		Ht (in)	L (ft)	area (sqft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	Depth (ft)	Spread (ft)	Depth (ft)	Spread (ft)	Depr (in)	
1	163+28 Rt	4.15	3.59	5.96	1.78	Curb	3.0	12.80	0.00	0.00	0.00	0.013	1.42	0.058	0.020	0.015	0.34	14.25	0.51	13.25	3.0	Off
2	168+04 Rt	5.89	4.43	6.74	3.59	Curb	3.0	12.80	0.00	0.00	0.00	0.017	1.42	0.058	0.020	0.015	0.36	15.10	0.53	14.20	3.0	1
3	172+35 Rt	6.14	4.37	6.08	4.43	Curb	3.0	9.60	0.00	0.00	0.00	0.013	1.42	0.058	0.025	0.015	0.40	13.97	0.58	13.16	3.0	2
4	176+11 Rt	5.18	5.49	6.30	4.37	Curb	3.0	9.60	0.00	0.00	0.00	0.012	1.42	0.058	0.026	0.015	0.41	13.91	0.59	13.12	3.0	3
5	179+45 Rt	3.87	6.82	5.20	5.49	Curb	3.0	9.60	0.00	0.00	0.00	0.020	1.42	0.058	0.019	0.015	0.35	15.35	0.52	14.37	3.0	4
6	181+74 Rt	4.30	9.75	7.23	6.82	Curb	3.0	9.60	0.00	0.00	0.00	0.011	1.42	0.058	0.024	0.015	0.44	16.49	0.63	15.83	3.0	5
7	184+75 Rt	9.41	9.18	8.85	9.75	Curb	3.0	9.60	0.00	0.00	0.00	0.006	1.42	0.058	0.020	0.015	0.52	23.10	0.70	22.50	3.0	6
8	189+68 Rt	7.31	7.58	5.70	9.18	Curb	3.0	9.60	0.00	0.00	0.00	0.017	1.42	0.058	0.014	0.015	0.37	21.75	0.54	20.86	3.0	7
9	194+87 Rt	5.33	8.77	6.52	7.58	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.021	0.015	0.41	16.93	0.59	16.14	3.0	8
10	198+04 Rt	9.77	6.03	7.02	8.77	Curb	3.0	9.60	0.00	0.00	0.00	0.015	1.42	0.058	0.022	0.015	0.43	17.18	0.61	16.45	3.0	9
11	204+00 Rt	11.22	0.00	5.19	6.03	Curb	3.0	9.60	0.00	0.00	0.00	0.025	1.42	0.058	0.020	0.015	0.34	14.50	0.52	13.50	3.0	10
Project File: SurfaceCalcsEast_N_101.stm													Number of lines: 11					Run Date: 03-02-2009				
NOTES: Inlet N-Values = 0.016 ; Intensity = 301.57 / (Inlet time + 18.30) ^ 1.11; Return period = 100 Yrs ; * Indicates Known Q added. All curb inlets are Horiz throat.																						

# Hydra ow Plan View



Project file: Princess\_StormDrain.stm

No. Lines: 4

03-22-2007

# Storm Sewer Infiltration

Page 1

Station		Len	Drng Area		Rnoff coeff	Area x C		Tc		Rain (l)	Total flow	Cap full	Vel	Pipe		invert Elev		HGL Elev		Grnd / Rim Elev		Line ID
Line	To Line		Incr	Total		Incr	Total	Inlet (min)	Syst (min)					Size (in)	Slope (%)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	Up (ft)	Dn (ft)	
		(ft)	(ac)	(ac)	(C)					(in/hr)	(cfs)	(cfs)	(ft/s)			(ft)	(ft)	(ft)	(ft)	(ft)	(ft)	
1	End	157.0	0.00	0.90	0.00	0.00	0.86	0.0	5.3	6.0	5.14	4.67	2.91	18	0.20	46.31	46.00	48.17	47.79	50.10	0.00	Inserted Line
2	1	8.6	0.00	0.63	0.00	0.00	0.60	0.0	5.2	6.0	3.61	5.07	2.04	18	0.23	46.33	46.31	48.31	48.30	50.20	50.10	Inserted Line
3	2	28.3	0.63	0.63	0.95	0.60	0.60	5.0	5.0	6.1	3.66	4.42	2.07	18	0.18	46.38	46.33	48.40	48.36	50.60	50.20	Inserted Line
4	1	5.7	0.27	0.27	0.95	0.26	0.26	5.0	5.0	6.1	1.57	18.64	0.89	18	3.15	46.49	46.31	48.30	48.30	49.30	50.10	Inserted Line
Project File: Princess_StormDrain.stm																Number of lines: 4				Run Date: 03-22-2007		
NOTES: Intensity = 64.98 / (Inlet time + 10.30) ^ 0.87; Return period = 10 Yrs.																						

# Inlet Report

Page 1

Line No	Inlet ID	Q = CIA (cfs)	Q carry (cfs)	Q capt (cfs)	Q byp (cfs)	Junc type	Curb Inlet		Grate Inlet			Gutter							Inlet			Byp line No
							Ht (in)	L (ft)	area (sqft)	L (ft)	W (ft)	So (ft/ft)	W (ft)	Sw (ft/ft)	Sx (ft/ft)	n	depth (ft)	spread (ft)	depth (ft)	spread (ft)	Dep (in)	
1	Princess Princess conn	0.00	0.00	0.00	0.00	None	0.0	0.00	0.00	0.00	0.00	Sag	0.00	0.000	0.000	0.000	0.00	0.00	0.00	0.00	0.00	Off
2		0.00	0.00	0.00	0.00	MH	0.0	0.00	0.00	0.00	0.00	Sag	0.00	0.000	0.000	0.000	0.00	0.00	0.00	0.00	0.00	Off
3		3.66	0.00	3.66	0.00	Curb	3.0	13.60	0.00	0.00	0.00	0.009	1.42	0.058	0.011	0.015	0.25	16.66	0.41	15.00	3.00	2
4		1.57	0.00	1.57	0.00	Curb	3.0	16.00	0.00	0.00	0.00	0.006	1.42	0.058	0.170	0.015	0.32	2.82	0.53	1.68	3.00	1
Project File: Princess_StormDrain.stm I-D-F File: ScottsdaleIDF.IDF Number of lines: 4 Run Date: 03-22-2007																						
NOTES: Inlet N-Values = 0.016 ; Intensity = 64.98 / (Inlet time + 10.30) ^ 0.87; Return period = 10 Yrs.; * Indicates Known Q added																						

Hydraflow Storm Sewers 2007

412

# Hydraulic Grade Line Computations

Page 1

Line	Size	Q	Downstream								Len	Upstream								Check		JL coeff	Minor loss
			Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)		Invert elev (ft)	HGL elev (ft)	Depth (ft)	Area (sqft)	Vel (ft/s)	Vel head (ft)	EGL elev (ft)	Sf (%)	Ave Sf (%)	Enrgy loss (ft)		
	(in)	(cfs)									(ft)											(K)	(ft)
1	18	5.14	46.00	47.79	1.50	1.77	2.91	0.13	47.92	0.240	157	46.31	48.17	1.50	1.77	2.91	0.13	48.30	0.239	0.239	0.376	1.00	0.13
2	18	3.61	46.31	48.30	1.50	1.77	2.04	0.06	48.36	0.118	8.6	46.33	48.31	1.50	1.77	2.04	0.06	48.37	0.118	0.118	0.010	0.85	0.06
3	18	3.66	46.33	48.36	1.50	1.77	2.07	0.07	48.43	0.121	28.3	46.38	48.40	1.50	1.77	2.07	0.07	48.46	0.121	0.121	0.034	0.50	0.03
4	18	1.57	46.31	48.30	1.50	1.77	0.89	0.01	48.31	0.022	5.7	46.49	48.30	1.50	1.77	0.89	0.01	48.31	0.022	0.022	0.001	0.50	0.01
Project File: Princess_StormDrain.stm														Number of lines: 4					Run Date: 03-22-2007				
NOTES: * Normal depth assumed., ** Critical depth assumed.																							







CULVERT #1 - CENTER PK.

## HY-8 Culvert Analysis Report

**Table 1 - Culvert Summary Table: 188+24.97**

Total Discharge (cfs)	Culvert Discharge (cfs)	Headwater Elevation (ft)	Inlet Control Depth (ft)	Outlet Control Depth (ft)	Flow Type	Normal Depth (ft)	Critical Depth (ft)	Outlet Depth (ft)	Tailwater Depth (ft)	Outlet Velocity (ft/s)	Tailwater Velocity (ft/s)
100.00	100.00	1632.28	2.616	2.616	1-S2n	1.487	1.697	1.489	2.240	8.395	0.000
120.00	120.00	1632.66	2.997	2.997	1-S2n	1.680	1.816	1.685	2.240	8.903	0.000
140.00	140.00	1633.04	3.380	3.380	5-S2n	1.868	2.123	1.872	2.240	9.347	0.000
160.00	160.00	1633.44	3.776	3.776	5-S2n	2.050	2.321	2.050	2.240	9.766	0.000
180.00	180.00	1633.85	4.194	4.194	5-S2n	2.225	2.511	2.230	2.240	10.092	0.000
200.00	200.00	1634.30	4.639	0.980	5-S2n	2.397	2.693	2.402	2.240	10.407	0.000
220.00	220.00	1634.78	5.118	0.980	5-S2n	2.563	2.870	2.569	2.240	10.705	0.000
224.00	224.00	1634.88	5.218	0.980	5-S2n	2.597	2.905	2.604	2.240	10.754	0.000
260.00	235.97	1635.19	5.526	5.249	5-S2n	2.696	3.000	2.900	2.240	10.171	0.000
280.00	238.96	1635.27	5.605	5.339	5-S2n	3.000	3.000	3.000	2.240	9.957	0.000
300.00	241.55	1635.33	5.674	5.417	5-S2n	3.000	3.000	3.000	2.240	10.064	0.000

\*\*\*\*\*  
Inlet Elevation (invert): 1629.66 ft, Outlet Elevation (invert): 1628.40 ft  
Culvert Length: 306.00 ft, Culvert Slope: 0.0041  
\*\*\*\*\*

### **Site Data - 188+24.97**

Site Data Option: Culvert Invert Data  
Inlet Station: 0.00 ft  
Inlet Elevation: 1629.66 ft  
Outlet Station: 306.00 ft  
Outlet Elevation: 1628.40 ft  
Number of Barrels: 1

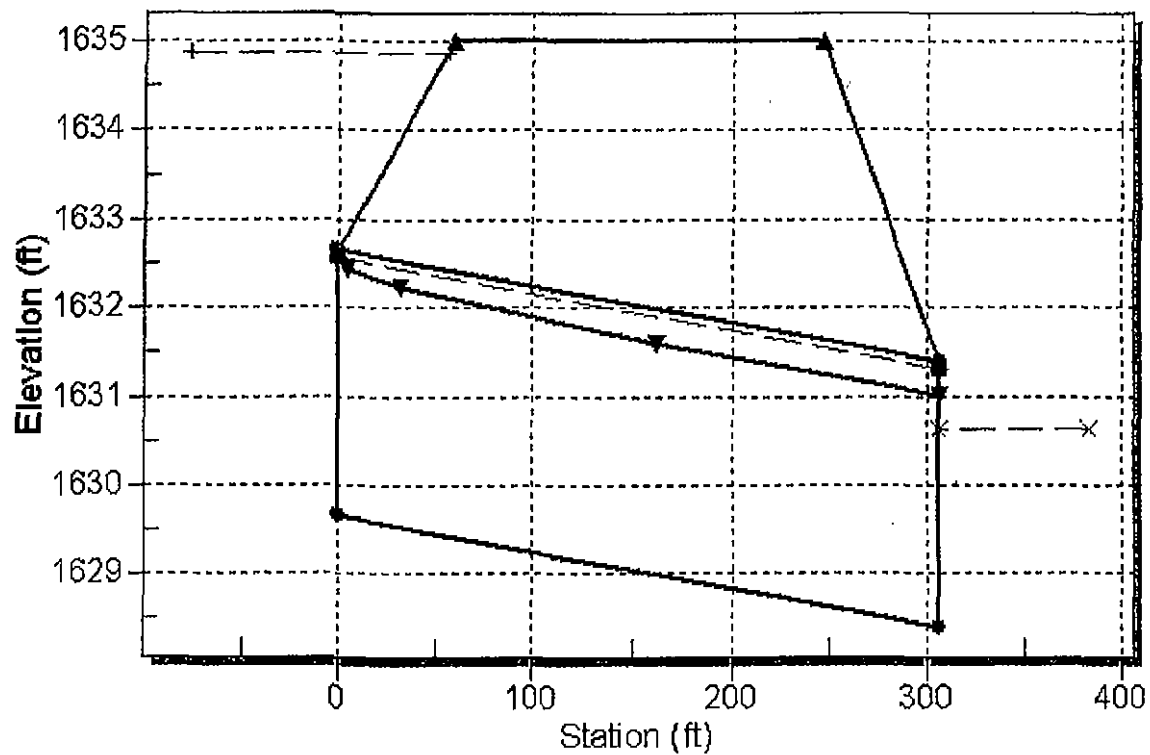
### **Culvert Data Summary - 188+24.97**

Barrel Shape: Concrete Box  
Barrel Span: 8.00 ft  
Barrel Rise: 3.00 ft  
Barrel Material: Concrete  
Barrel Manning's n: 0.0120  
Inlet Type: Conventional  
Inlet Edge Condition: 1:1 Bevel (45° flare) Wingwall  
Inlet Depression: None

Water Surface Profile Plot for Culvert: 188+24.97

Crossing - Scottsdale Road, Design Discharge - 224.0 cfs

Culvert - 188+24.97, Culvert Discharge - 224.0 cfs



**Table 2 - Downstream Channel Rating Curve (Crossing: Scottsdale Road)**

Flow (cfs)	Water Surface Elev (ft)	Depth (ft)
100.00	1630.64	2.24
120.00	1630.64	2.24
140.00	1630.64	2.24
160.00	1630.64	2.24
180.00	1630.64	2.24
200.00	1630.64	2.24
220.00	1630.64	2.24
224.00	1630.64	2.24
260.00	1630.64	2.24
280.00	1630.64	2.24
300.00	1630.64	2.24

**Tailwater Channel Data - Scottsdale Road**

Tailwater Channel Option: Enter Constant Tailwater Elevation

Constant Tailwater Elevation: 1630.64 ft

**Roadway Data for Crossing: Scottsdale Road**

Roadway Profile Shape: Constant Roadway Elevation

Crest Length: 100.00 ft

Crest Elevation: 1635.00 ft

Roadway Surface: Paved

Roadway Top Width: 188.00 ft

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Scottsdale Road  
Channel Design

Date  
Job No.  
By  
RCE  
Chk'd  
Filepath:

23-Mar-07  
10-0244  
JEP

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### CHANNEL DESIGN REFERENCES

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2. ASCE-Manuals and Reports on Engineering Practice-No. 54 "Sedimentation Engineering," Reprinted 1977.
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4. Morris and Wiggert, "Applied Hydraulics in Engineering," Second Edition, 1972
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7. Chow, Ven Te, "Open-Channel Hydraulics," 1959.
8. Simons, Li & Assoc. "Engineering Analysis of Fluvial Systems," 1982.
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10. FHWA H.E.C. No. 14 "Hydraulic Design of Energy Dissipators for Culverts and Channels," September 1983
11. MWE "Evaluation of and Design Recommendations for Drop Structures in the Denver Metropolitan Area," December 1986.
12. Simons, Li & Assoc. "Criteria for Channels and Hydraulic Structures on Sandy Soils," April 1981.
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# SCOTTSDALE ROAD - WANNING'S RATING CURVE

Channel: SCOTTSDALE ROAD - Offsite Channel 1A

## INPUT DATA:

Manning's n = 0.038  
 T allow = 2.00 lb/ft<sup>2</sup>  
 Sideslope Left = 3.0 :1  
 Sideslope Right = 3.0 :1  
 Bottom slope = 0.0 percent

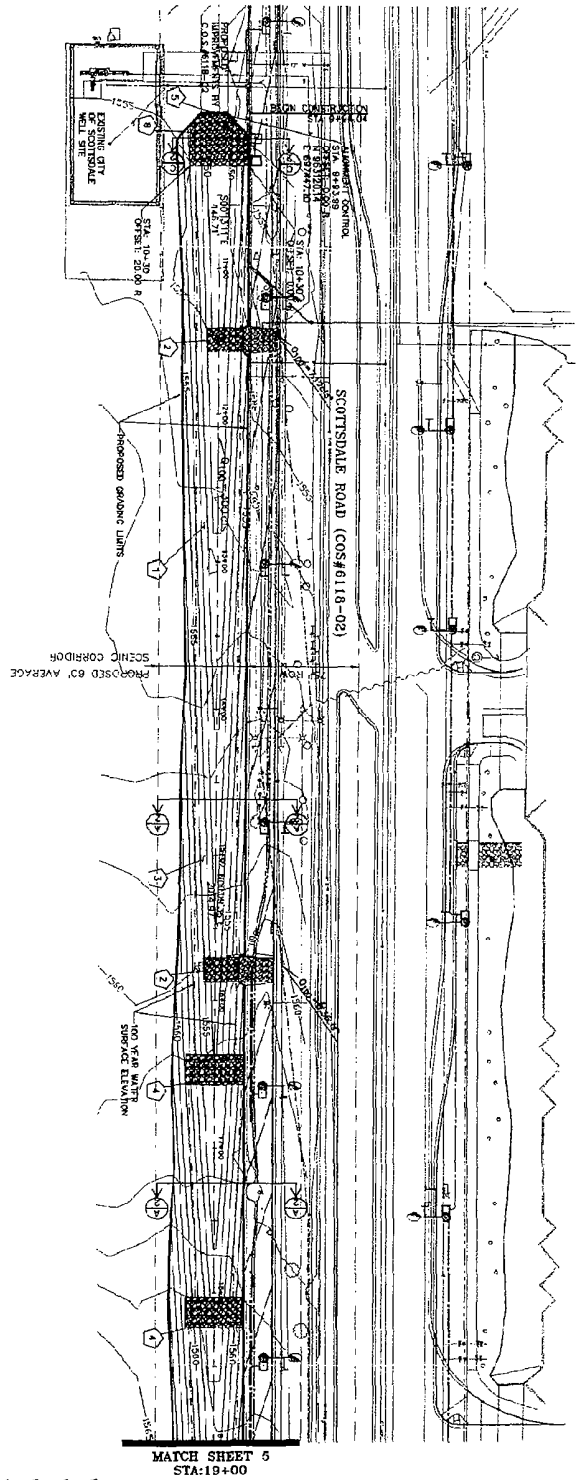
Reach	Slope	BW (ft)	t	Topwidth												
				2.22	2.34	0.038	224.0	0.25	0.16	0.26	1.08	5.30	35.32	41.78	105.97	0.06
Channel1A	0.0010	10.0	0.0	4.22	2.34	0.038	224.0	0.25	0.16	0.26	1.08	5.30	35.32	41.78	105.97	0.06
Channel1A	0.0020	10.0	0.0	3.58	3.02	0.038	224.0	0.35	0.28	0.45	1.00	4.58	31.45	37.45	94.36	0.09
Channel1A	0.0030	10.0	0.0	3.24	3.51	0.038	224.0	0.42	0.39	0.61	1.00	4.24	29.44	35.44	88.31	0.13
Channel1A	0.0040	10.0	0.0	3.02	3.90	0.038	224.0	0.48	0.49	0.75	1.00	4.02	28.11	34.11	84.32	0.16
Channel1A	0.0050	10.0	0.0	2.86	4.23	0.038	224.0	0.53	0.59	0.89	1.00	3.86	27.13	33.13	81.39	0.18
Channel1A	0.0060	10.0	0.0	2.73	4.52	0.038	224.0	0.58	0.68	1.02	1.00	3.73	26.37	32.37	79.10	0.21
Channel1A	0.0070	10.0	0.0	2.62	4.78	0.038	224.0	0.62	0.77	1.15	1.00	3.62	25.75	31.75	77.24	0.24
Channel1A	0.0080	10.0	0.0	2.54	5.01	0.038	224.0	0.66	0.86	1.27	1.00	3.54	25.22	31.22	75.67	0.26
Channel1A	0.0090	10.0	0.0	2.46	5.23	0.038	224.0	0.70	0.94	1.38	1.00	3.46	24.78	30.78	74.33	0.28
Channel1A	0.0100	10.0	0.0	2.39	5.43	0.038	224.0	0.73	1.03	1.47	1.00	3.39	24.42	30.42	73.09	0.30
Channel1A	0.0010	12.0	0.0	4.01	2.33	0.038	224.0	0.25	0.16	0.25	1.02	5.03	36.05	42.19	108.16	0.06
Channel1A	0.0020	12.0	0.0	3.38	3.00	0.038	224.0	0.35	0.28	0.42	1.00	4.38	32.27	38.27	96.81	0.09
Channel1A	0.0030	12.0	0.0	3.05	3.47	0.038	224.0	0.42	0.39	0.57	1.00	4.05	30.31	36.31	90.92	0.12
Channel1A	0.0040	12.0	0.0	2.84	3.85	0.038	224.0	0.48	0.48	0.71	1.00	3.84	29.02	35.02	87.05	0.15
Channel1A	0.0050	12.0	0.0	2.68	4.17	0.038	224.0	0.53	0.58	0.84	1.00	3.68	28.07	34.07	84.22	0.18
Channel1A	0.0060	12.0	0.0	2.56	4.46	0.038	224.0	0.58	0.67	0.96	1.00	3.56	27.33	33.33	82.00	0.21
Channel1A	0.0070	12.0	0.0	2.46	4.71	0.038	224.0	0.62	0.75	1.07	1.00	3.46	26.73	32.73	80.20	0.23
Channel1A	0.0080	12.0	0.0	2.37	4.94	0.038	224.0	0.66	0.84	1.18	1.00	3.37	26.23	32.23	78.69	0.25
Channel1A	0.0090	12.0	0.0	2.30	5.15	0.038	224.0	0.70	0.92	1.29	1.00	3.30	25.80	31.80	77.40	0.27
Channel1A	0.0150	12.0	0.0	2.01	6.18	0.038	224.0	0.89	1.37	1.88	1.00	3.01	24.06	30.06	72.18	0.40
Channel1A	0.0010	14.0	0.0	3.82	2.31	0.038	224.0	0.25	0.16	0.24	1.00	4.82	36.90	42.90	110.70	0.06
Channel1A	0.0020	14.0	0.0	3.20	2.96	0.038	224.0	0.35	0.28	0.40	1.00	4.20	33.21	39.21	99.63	0.09
Channel1A	0.0030	14.0	0.0	2.88	3.43	0.038	224.0	0.42	0.38	0.54	1.00	3.88	31.30	37.30	93.90	0.12
Channel1A	0.0040	14.0	0.0	2.68	3.80	0.038	224.0	0.48	0.48	0.67	1.00	3.68	30.05	36.05	90.15	0.15
Channel1A	0.0050	14.0	0.0	2.52	4.12	0.038	224.0	0.53	0.57	0.79	1.00	3.52	29.14	35.14	87.41	0.18
Channel1A	0.0060	14.0	0.0	2.40	4.39	0.038	224.0	0.58	0.65	0.90	1.00	3.40	28.42	34.42	85.27	0.20
Channel1A	0.0070	14.0	0.0	2.31	4.64	0.038	224.0	0.62	0.74	1.01	1.00	3.31	27.85	33.85	83.54	0.22
Channel1A	0.0080	14.0	0.0	2.23	4.86	0.038	224.0	0.66	0.82	1.11	1.00	3.23	27.36	33.36	82.08	0.24
Channel1A	0.0090	14.0	0.0	2.16	5.07	0.038	224.0	0.70	0.90	1.21	1.00	3.16	26.95	32.95	80.84	0.27
Channel1A	0.0150	14.0	0.0	1.88	6.07	0.038	224.0	0.88	1.33	1.76	1.00	2.88	25.28	31.28	75.84	0.38

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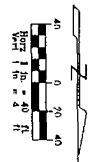
Date 23-Mar-07  
Job No. 10-0244  
By JEP  
RCE  
Chk'd BJF  
Filepath: J:\10-0244\EXCEL\DRAINAGE\CHANNELDES.xls

Scottsdale Road  
Channel Design

TYPICAL SECTION - MANNING'S RATING 5.0000															
Channel: SCOTTSDALE ROAD - Offsite Channel 1B															
INPUT DATA:															
Manning's n =	0.038	Riprap													
T allow =	2.00	lb/ft <sup>2</sup>													
Sideslope Left =	3.0 :1														
Sideslope Right =	3.0 :1														
Bottom slope =	0.0 percent														
														Topwidth	
Reach	Slope	BW (ft)	t												
Channel1B	0.0100	10.0	0.0	2.40	5.43	0.038	224.0	0.74	1.02	1.00	3.40	24.39	30.39	73.16	0.31
Channel1B	0.0101	10.0	0.0	2.39	5.45	0.038	224.0	0.74	1.03	1.00	3.39	24.35	30.35	73.05	0.31
Channel1B	0.0102	10.0	0.0	2.39	5.47	0.038	224.0	0.74	1.04	1.00	3.39	24.31	30.31	72.94	0.31
Channel1B	0.0103	10.0	0.0	2.38	5.49	0.038	224.0	0.75	1.05	1.00	3.38	24.28	30.28	72.83	0.31
Channel1B	0.0104	10.0	0.0	2.37	5.51	0.038	224.0	0.75	1.05	1.00	3.37	24.24	30.24	72.73	0.31
Channel1B	0.0105	10.0	0.0	2.37	5.53	0.038	224.0	0.75	1.06	1.00	3.37	24.21	30.21	72.62	0.32
Channel1B	0.0106	10.0	0.0	2.36	5.55	0.038	224.0	0.76	1.07	1.00	3.36	24.17	30.17	72.52	0.32
Channel1B	0.0107	10.0	0.0	2.36	5.57	0.038	224.0	0.76	1.08	1.00	3.36	24.14	30.14	72.42	0.32
Channel1B	0.0108	10.0	0.0	2.35	5.59	0.038	224.0	0.76	1.09	1.00	3.35	24.11	30.11	72.32	0.32
Channel1B	0.0109	10.0	0.0	2.35	5.61	0.038	224.0	0.77	1.09	1.00	3.35	24.07	30.07	72.22	0.33
Channel1B	0.0110	10.0	0.0	2.34	5.62	0.038	224.0	0.77	1.10	1.00	3.34	24.04	30.04	72.12	0.33
Channel1B	0.0111	10.0	0.0	2.33	5.64	0.038	224.0	0.77	1.11	1.00	3.33	24.01	30.01	72.02	0.33
Channel1B	0.0112	10.0	0.0	2.33	5.66	0.038	224.0	0.78	1.12	1.00	3.33	23.98	29.98	71.93	0.33
Channel1B	0.0113	10.0	0.0	2.32	5.68	0.038	224.0	0.78	1.13	1.00	3.32	23.94	29.94	71.83	0.33
Channel1B	0.0114	10.0	0.0	2.32	5.70	0.038	224.0	0.78	1.13	1.00	3.32	23.91	29.91	71.74	0.34
Channel1B	0.0115	10.0	0.0	2.31	5.72	0.038	224.0	0.79	1.14	1.00	3.31	23.88	29.88	71.64	0.34
Channel1B	0.0116	10.0	0.0	2.31	5.73	0.038	224.0	0.79	1.15	1.00	3.31	23.85	29.85	71.55	0.34
Channel1B	0.0117	10.0	0.0	2.30	5.75	0.038	224.0	0.79	1.16	1.00	3.30	23.82	29.82	71.46	0.34
Channel1B	0.0118	10.0	0.0	2.30	5.77	0.038	224.0	0.80	1.17	1.00	3.30	23.79	29.79	71.37	0.34
Channel1B	0.0119	10.0	0.0	2.29	5.79	0.038	224.0	0.80	1.17	1.00	3.29	23.76	29.76	71.28	0.35
Channel1B	0.0120	10.0	0.0	2.29	5.80	0.038	224.0	0.80	1.18	1.00	3.29	23.73	29.73	71.19	0.35
Channel1B	0.0121	10.0	0.0	2.28	5.82	0.038	224.0	0.81	1.19	1.00	3.28	23.70	29.70	71.10	0.35
Channel1B	0.0122	10.0	0.0	2.28	5.84	0.038	224.0	0.81	1.20	1.00	3.28	23.67	29.67	71.02	0.35
Channel1B	0.0123	10.0	0.0	2.27	5.86	0.038	224.0	0.81	1.20	1.00	3.27	23.64	29.64	70.93	0.35
Channel1B	0.0124	10.0	0.0	2.27	5.87	0.038	224.0	0.81	1.21	1.00	3.27	23.62	29.62	70.85	0.36
Channel1B	0.0125	10.0	0.0	2.26	5.89	0.038	224.0	0.82	1.22	1.00	3.26	23.59	29.59	70.76	0.36
Channel1B	0.0126	10.0	0.0	2.26	5.91	0.038	224.0	0.82	1.23	1.00	3.26	23.56	29.56	70.68	0.36
Channel1B	0.0127	10.0	0.0	2.26	5.92	0.038	224.0	0.82	1.24	1.00	3.26	23.53	29.53	70.60	0.36



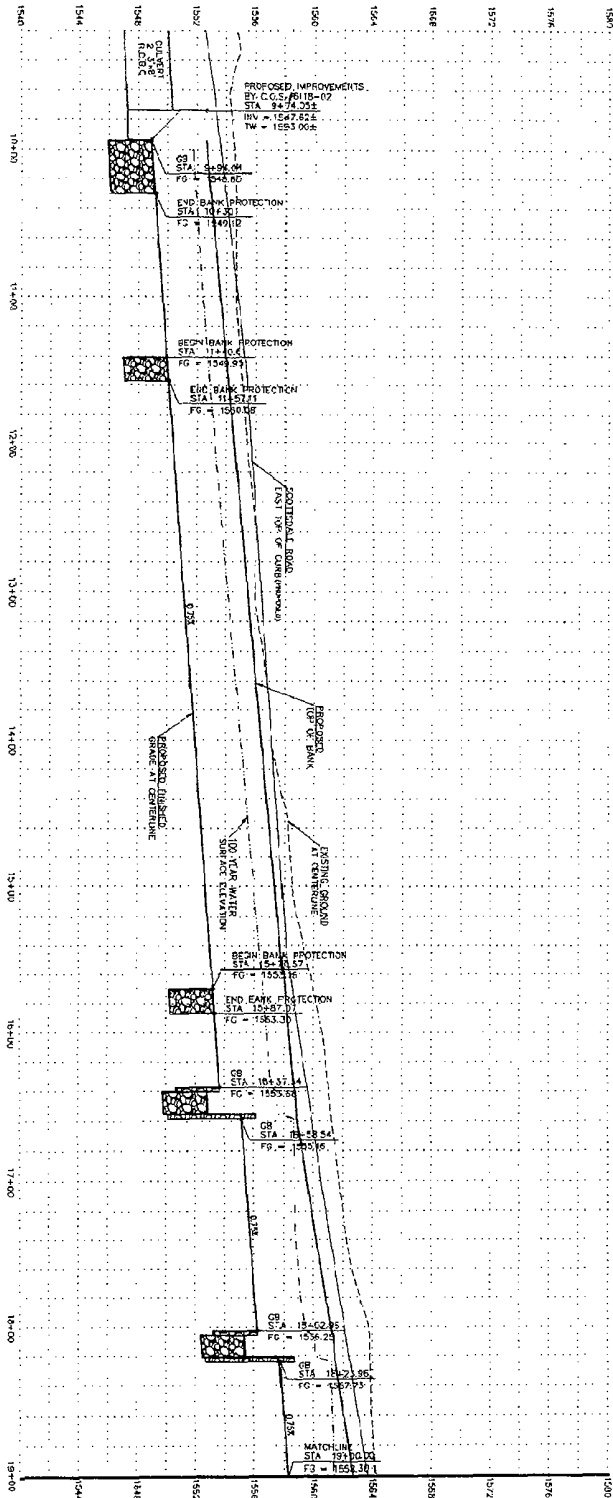
MATCH SHEET 5  
STA: 19+00



**CHANNEL CONSTRUCTION NOTES**

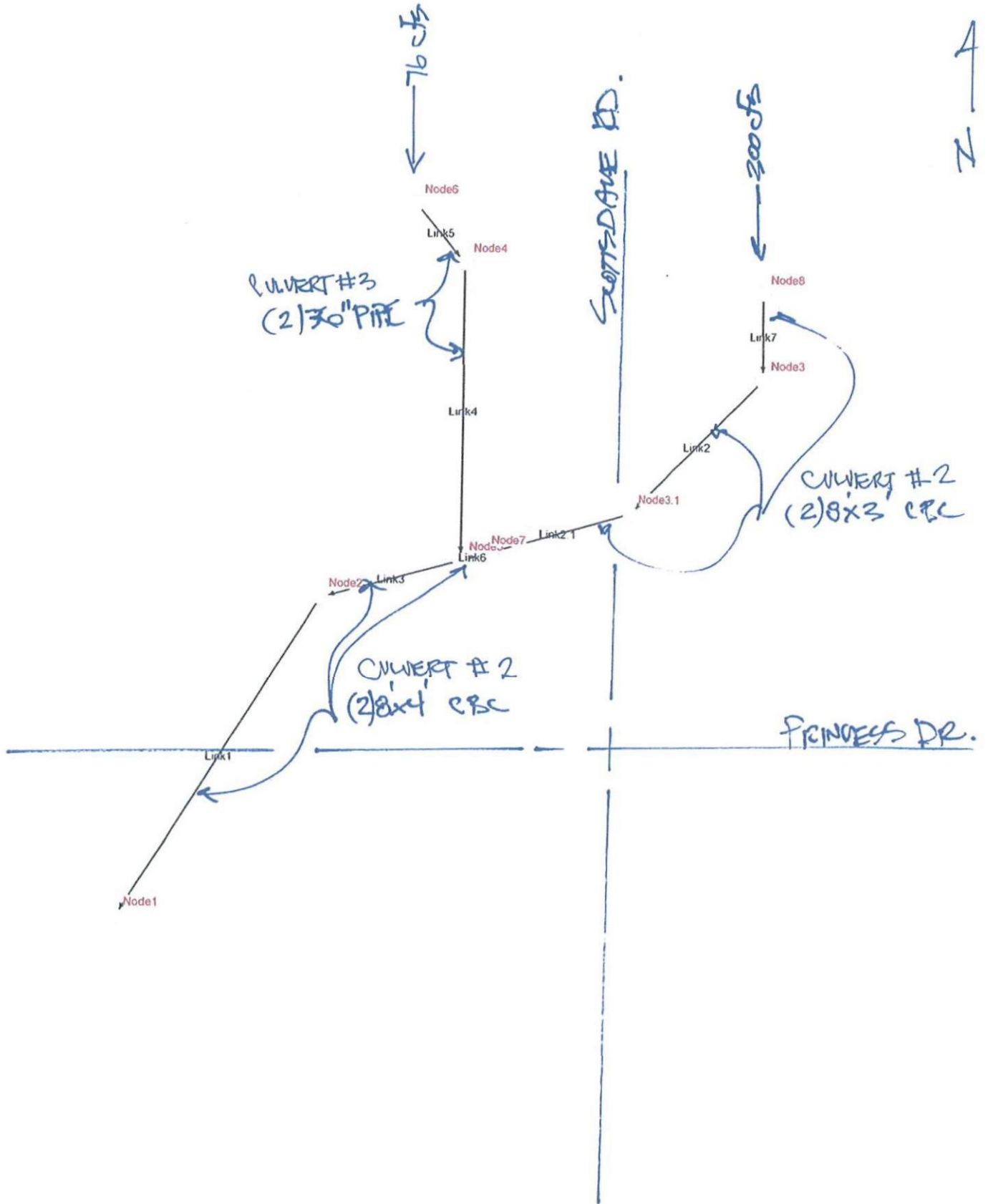
1. GRADE CHANNEL FOR PLAN AND PROFILE ELEVATION.
2. COMPACT FINE SOIL PER M.A.D. SPEC. 210.
3. EXISTING REPAIR SPILLWAY 20 FEET EAST FOR SCALPER.
4. EXISTING OF THE SHUTTLE, SECTION 210.
5. INTERLOCKED CHANNEL, 50L PER RECONSTRUCTION PLAN ON SHEET 1.
6. INTERLOCKED CHANNEL, 50L PER RECONSTRUCTION PLAN ON SHEET 2.
7. CONNECTION TO LOCATE EXISTING GUTTER AND SIDEWALK.
8. CHANNEL GRADE PROPOSED CHANNEL TO EXISTING SIDEWALK.
9. BROW PROTECTION DETAIL SHEET 2, SECTION C-C.

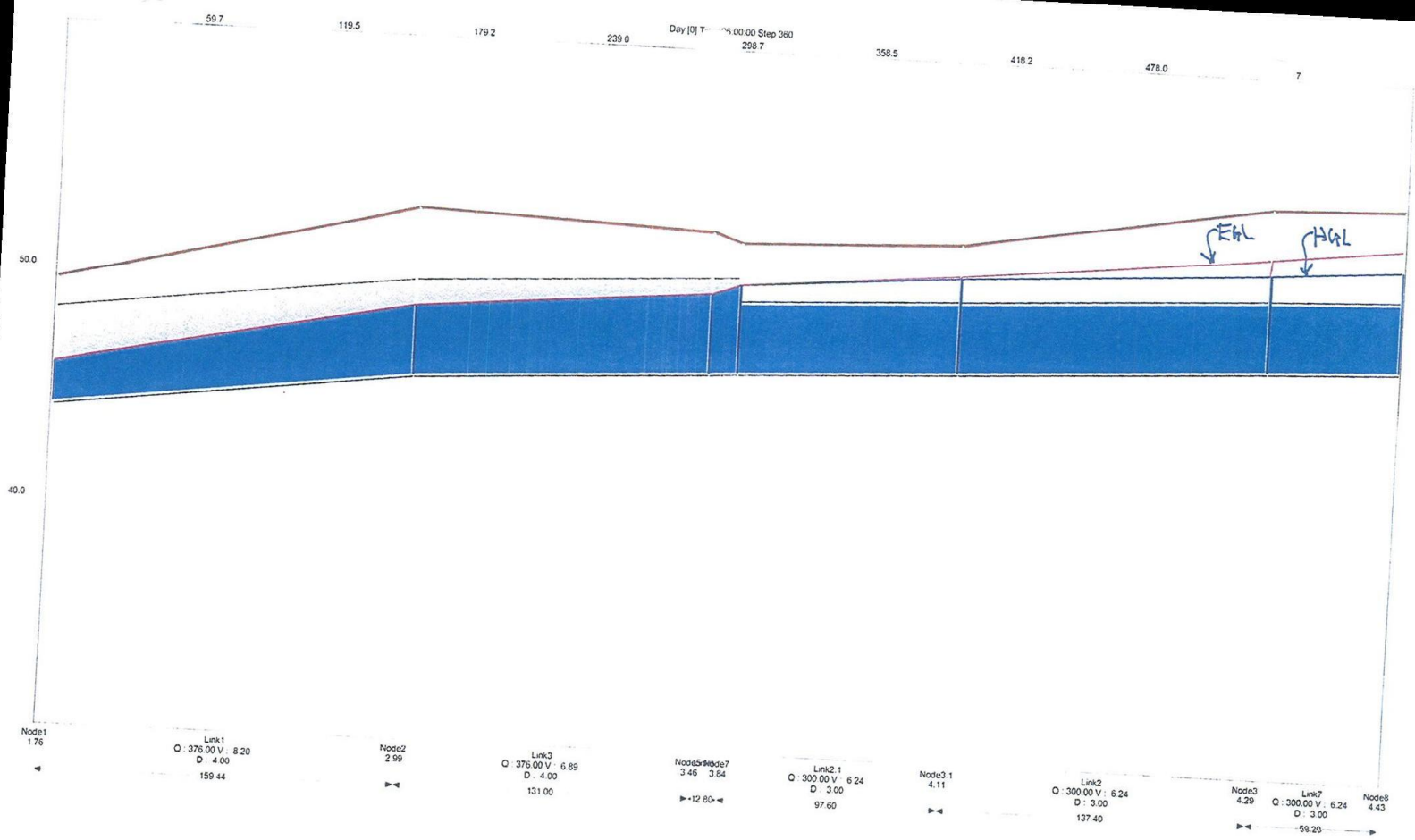
REGISTRATION FROM CITY OF SCOTTSDALE  
FORWARDED FOR COS#6118-02



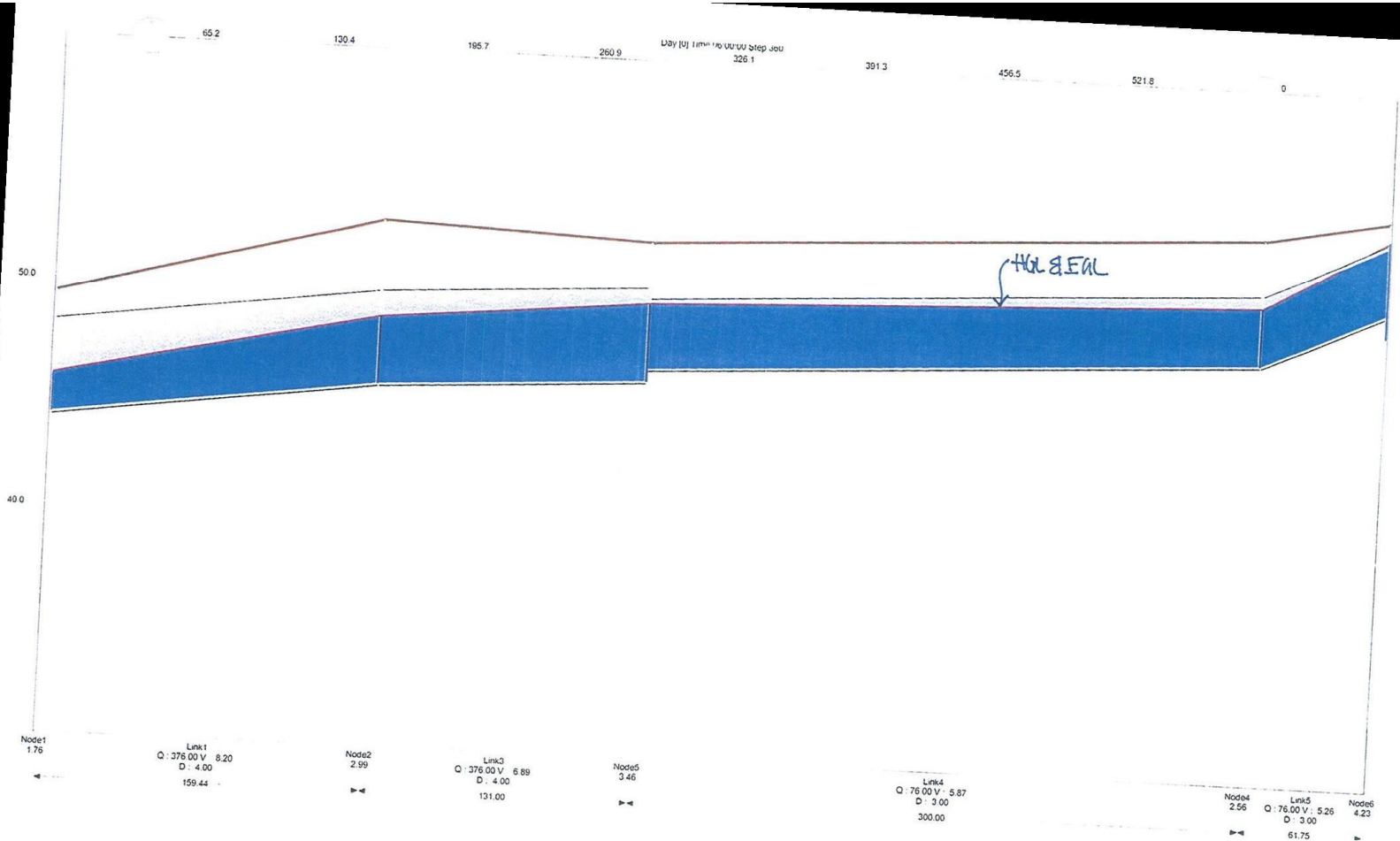
<p>5-SA-2008</p>	<p>19-ZN-2008</p>	<p>1672-08-1</p>	<p>Q.S.#38-45</p>	<p><b>INTERIM REGIONAL DRAINAGE CHANNEL</b></p> <p><b>CITY OF SCOTTSDALE, ARIZONA</b></p>	<p><b>WOOD/PATEL</b></p> <p>LAND DEVELOPMENT &amp; WATER RESOURCES STRUCTURES &amp; TRANSPORTATION/TRAFFIC WATER/WASTEWATER &amp; SURVEYING CONSTRUCTION MANAGEMENT</p> <p>(602) 355-6500</p> <p>PHOENIX • MESA • GORDON • TUCSON</p>
<p><b>PRELIMINARY NOT FOR CONSTRUCTION OR RECORDING</b></p>				<p><b>DMB</b></p>	

CULVERT #2 & #3





2/18

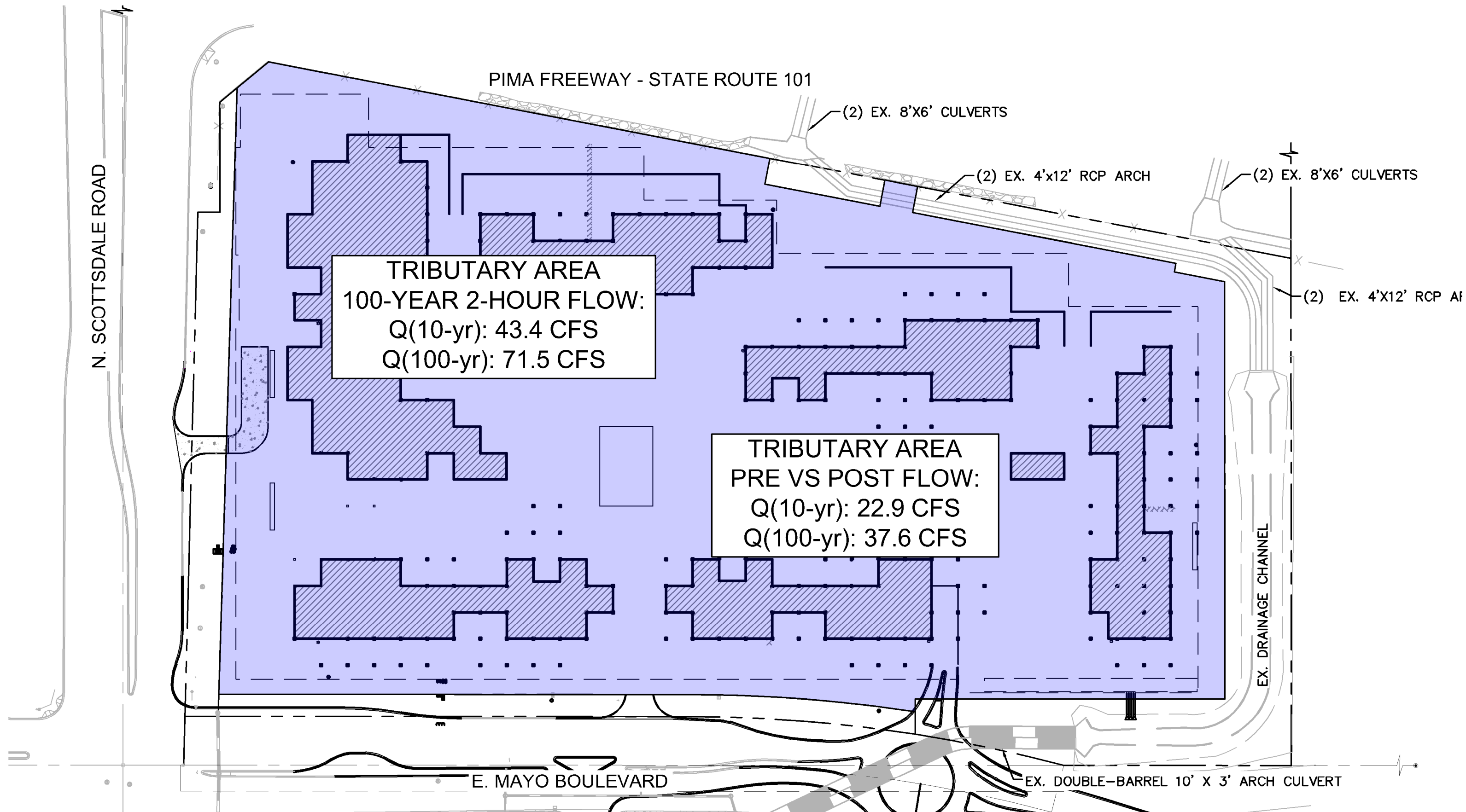


3/10

***Appendix J***

**Watershed Delineation**

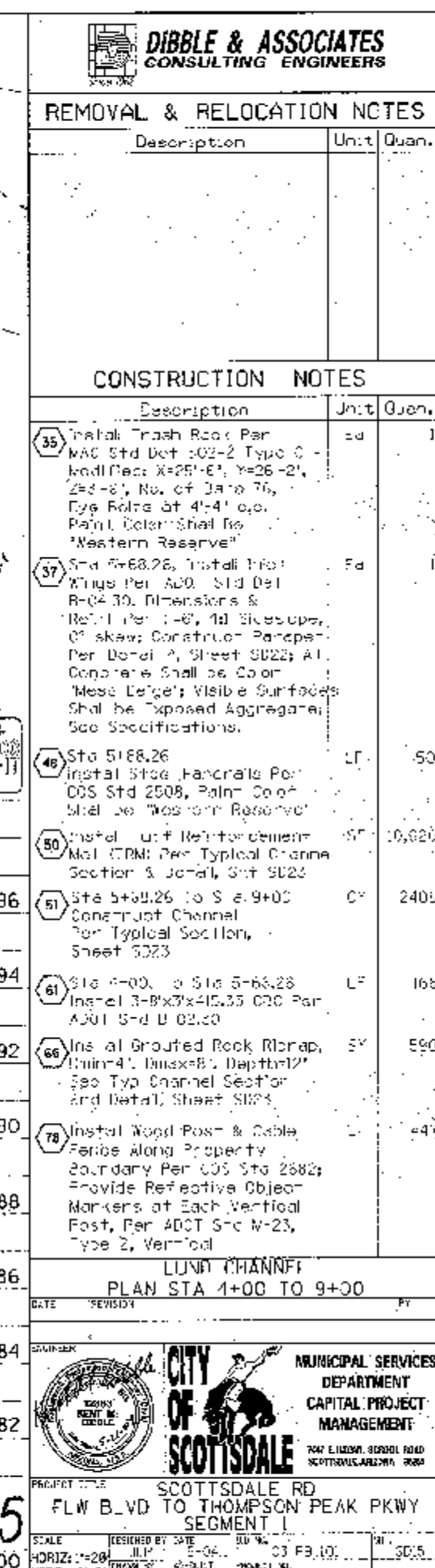




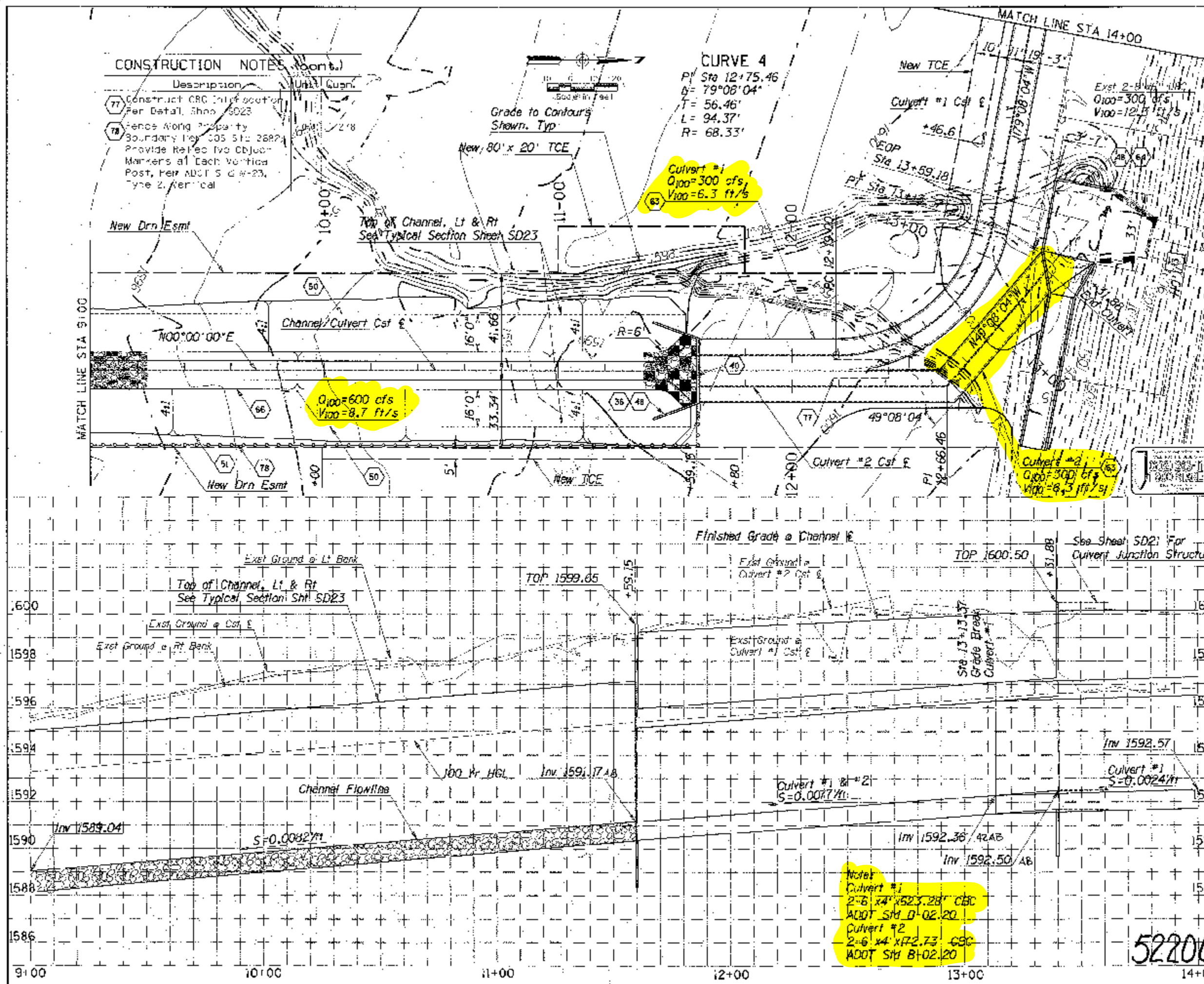
***Appendix K***

**As- Builts for Lund Channel**

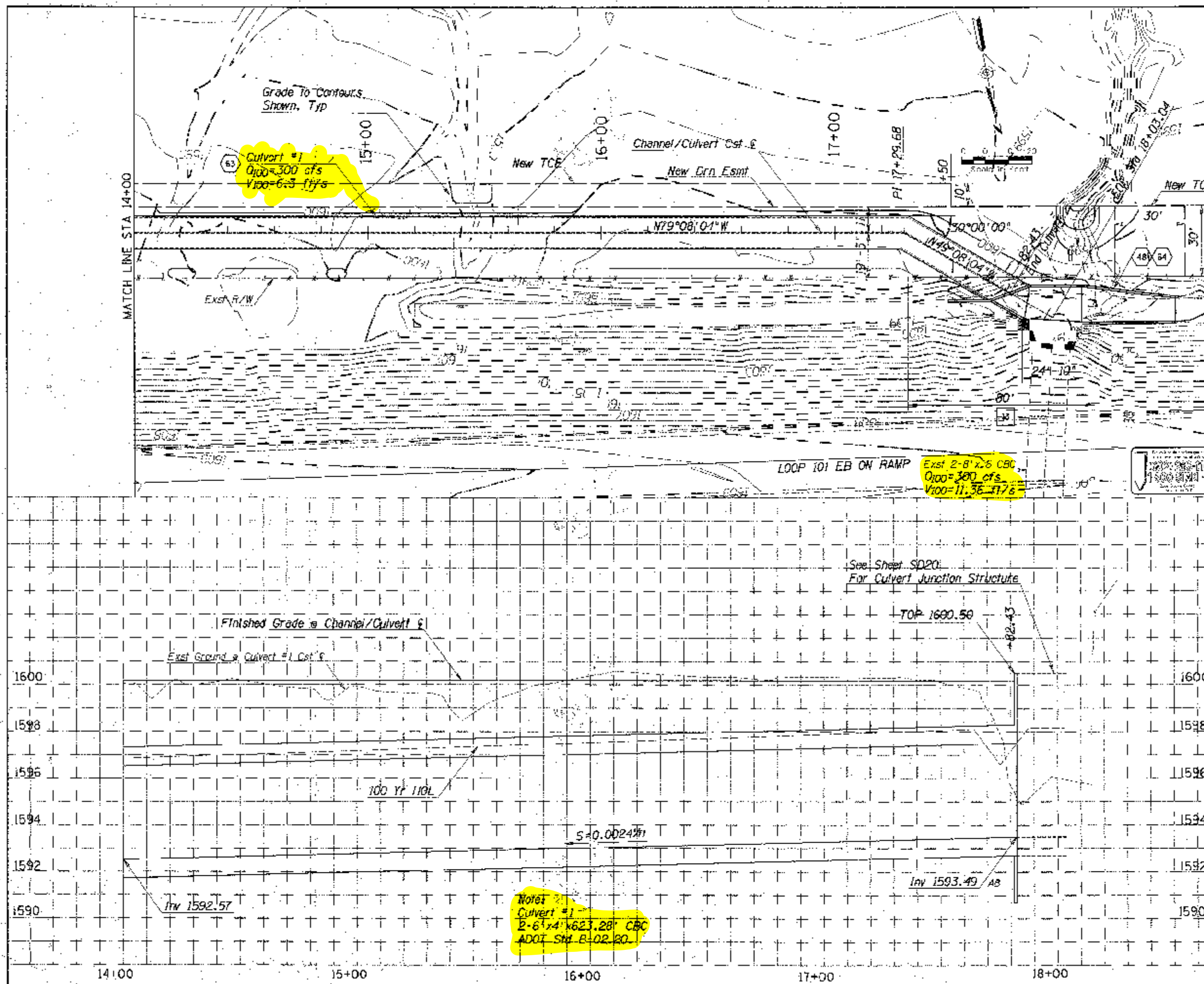




6118-02	Q.S.	37-45, 38-45, 39-45, 40-45	49-DR-2003
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6118-02 Q.S. 37-45, 38-45, 39-45, 40-45 49-DR-2003



**DIBBLE & ASSOCIATES**  
CONSULTING ENGINEERS

# REMOVAL & RELOCATION NOTES

Description	Unit	Quan.
13 Remove Existing Barb-wire Fence, Replace In Kind	LF	30

## CONSTRUCTION NOTES

Description	Unit	Quan.
48 Install Steel Landfill	F	100
Per CUS S & 250R		
Paint Color Shall be Western Reserve		
Sac Detail C, Silt 1020		
63 Sta 14+00 to Sta 17+12.73	LF	333
Gr. & 2' 6" x 4' x 330.43' CBC		
Per 4001 Sid B-0220		
64 Install Enclosed CEC Junction	EA	1
Per Detail C, Sheet SD20		

52207

LONG CHANNEL  
PLAN STA 14+00 TO 18+14.38 (EO)

DATE: 03/10/04



MUNICIPAL SERVICES  
DEPARTMENT  
CAPITAL PROJECT  
MANAGEMENT

PROJECT TITLE: SCOTTSDALE RD  
FLW B\_VD TO THOMPSON PEAK PKWY  
SEGMENT I

SCALE: HORIZONTAL: 1"=20' VERTICAL: 1"=2' DATE: 03 FEB 10. SHEET: SD17  
DRAWN BY: J. B. G. CHECKED BY: J. B. G. STATION: 52 OF 62

6118-02 O.S. 37-45, 38-45, 39-45, 40-45 49-DR-2003



***Appendix L***

**As- Builts for One Scottsdale South Drainage Basin Improvement Plans**



## ENGINEERS NOTES

- MARICOPA ASSOCIATION OF GOVERNMENTS (M.A.G.) UNIFORM STANDARD SPECIFICATIONS AND DETAILS FOR PUBLIC WORKS CONSTRUCTION (LATEST EDITION INCLUDING LATEST REVISION AND CURRENT SUPPLEMENTALS THEREOF PER THE LOCAL TOWN OR CITY) ARE INCORPORATED INTO THIS PLAN IN THEIR ENTIRETY.
- ALL WORK REQUIRED TO COMPLETE THE CONSTRUCTION COVERED BY THIS PLAN SHALL BE IN ACCORDANCE WITH THE M.A.G. STANDARD SPECIFICATIONS AND DETAILS AND CURRENT SUPPLEMENTALS THEREOF PER THE LOCAL CITY OR TOWN UNLESS SPECIFIED OTHERWISE IN THESE PLANS OR ELSEWHERE IN THE CONTRACT DOCUMENTS. CONTRACTORS SHALL FAMILIARIZE THEMSELVES WITH ALL REQUIRED STANDARD SPECIFICATIONS, DETAILS AND SUPPLEMENTALS PRIOR TO BIDDING THE WORK FOR THE CONSTRUCTION COVERED BY THIS PLAN.
- THE CONTRACTOR IS RESPONSIBLE FOR ALL METHODS, SEQUENCING, AND SAFETY CONCERNS ASSOCIATED WITH THIS PROJECT DURING CONSTRUCTION, UNLESS SPECIFICALLY ADDRESSED OTHERWISE IN THIS PLAN OR ELSEWHERE IN THE CONTRACT.
- THE CONTRACTOR IS TO COMPLY WITH ALL LOCAL, STATE, AND FEDERAL LAWS AND REGULATIONS APPLICABLE TO THE CONSTRUCTION COVERED BY THIS PLAN.
- THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING AND COMPLYING WITH ALL PERMITS REQUIRED TO COMPLETE ALL WORK COVERED BY THIS PLAN.
- THE QUANTITIES AND SITE CONDITIONS DEPICTED IN THESE PLANS ARE FOR INFORMATIONAL PURPOSES ONLY AND ARE SUBJECT TO ERROR AND OMISSION. CONTRACTORS SHALL SATISFY THEMSELVES AS TO ACTUAL QUANTITIES AND SITE CONDITIONS PRIOR TO BIDDING THE WORK FOR THE CONSTRUCTION COVERED BY THIS PLAN.
- A REASONABLE EFFORT HAS BEEN MADE TO SHOW THE LOCATIONS OF EXISTING UNDERGROUND FACILITIES AND UTILITIES IN THE CONSTRUCTION AREA. THE CONTRACTOR IS RESPONSIBLE FOR ANY DAMAGE TO UTILITIES AND/OR FACILITIES CAUSED DURING THEIR CONSTRUCTION OPERATIONS. THE CONTRACTOR SHALL CALL 48 HOURS IN ADVANCE FOR BLUE STAKE (1-800-STAKE-IT) PRIOR TO ANY EXCAVATION.
- THE CONTRACTOR IS RESPONSIBLE FOR ALL COORDINATION OF CONSTRUCTION AFFECTING UTILITIES AND THE COORDINATION OF ANY NECESSARY UTILITY RELOCATION WORK.
- ALL PAVING, GRADING, EXCAVATION, TRENCHING, PIPE BEDDING, CUT FILL AND BACKFILL SHALL COMPLY WITH THE RECOMMENDATIONS SET FORTH IN THE SOILS (GEOTECHNICAL) REPORT FOR THIS PROJECT IN ADDITION TO THE REFERENCED REQUIRED SPECIFICATIONS AND DETAILS. THE CONTRACTOR SHALL BE AWARE THAT CERTAIN UTILITIES REQUIRE PROPER ATTENTION AND CAREFUL PLANNING DURING SITE CONSTRUCTION. PLEASE NOTE THAT UTILITIES ON THESE PLANS MAY NOT EXHIBIT THE FULL PROTECTIVE COVER REQUIRED DURING THE SUBGRADE PREPARATION PHASE OF THE CONSTRUCTION. IN SUCH INSTANCES, THE CONTRACTOR SHALL PROVIDE ADDITIONAL PROTECTION (SUCH AS RAMPING) OR INCREASED PIPE STRENGTH TO PROVIDE THE NECESSARY PROTECTION REQUIRED TO PREVENT DAMAGE DURING THE CONSTRUCTION OF THIS PROJECT. THE CONTRACTOR SHALL HOLD THE ENGINEER HARMLESS IN ALL CASES FOR DAMAGES TO UTILITIES WHERE INADEQUATE PROTECTIVE MEASURES OCCUR.
- THE CONTRACTOR IS TO VERIFY THE LOCATION AND THE ELEVATIONS OF ALL EXISTING UTILITIES AT POINTS OF TIE-IN PRIOR TO COMMENCING ANY NEW CONSTRUCTION. SHOULD ANY LOCATION OR ELEVATION DIFFER FROM THAT SHOWN ON THESE PLANS, THE CONTRACTOR SHALL CONTACT THE OWNER'S AGENT.
- CONTRACTOR TO VERIFY AND COORDINATE ALL DIMENSIONS AND SITE LAYOUT WITH ARCHITECT'S FINAL SITE PLAN AND FINAL BUILDING DIMENSIONS BEFORE STARTING WORK. REPORT DISCREPANCIES TO OWNER'S AGENT.
- COORDINATION BETWEEN ALL PARTIES IS ESSENTIAL PART OF CONTRACT.
- CONTRACTOR IS RESPONSIBLE FOR PROJECT AND SITE CONDITIONS, AND TO WORK WITH WEATHER CONDITIONS AS THE PROJECT SITE MAY BE LOCATED IN A FLOOD PRONE AREA AND SUBJECT TO FLOODING AND ITS HAZARDS.
- THE CONTRACTOR IS TO VERIFY THE LOCATION, ELEVATION, CONDITION, AND PAVEMENT CROSS-SLOPE OF ALL EXISTING SURFACES AT POINTS OF TIE-IN AND MATCHLINES PRIOR TO COMMENCEMENT OF GRADING, PAVING, CURB AND GUTTER, OR OTHER SURFACE CONSTRUCTION. SHOULD EXISTING LOCATIONS, ELEVATIONS, CONDITION, OR PAVEMENT CROSS-SLOPE DIFFER FROM THAT SHOWN ON THESE PLANS, RESULTING IN THE DESIGN INTENT REFLECTED ON THESE PLANS NOT ABLE TO BE CONSTRUCTED, THE CONTRACTOR SHALL NOTIFY THE OWNER'S AGENT IMMEDIATELY FOR DIRECTION ON HOW TO PROCEED PRIOR TO COMMENCEMENT OF CONSTRUCTION. THE CONTRACTOR ACCEPTS RESPONSIBILITY FOR ALL COSTS ASSOCIATED WITH CORRECTIVE ACTION IF THESE PROCEDURES ARE NOT FOLLOWED.
- CONTRACTOR IS RESPONSIBLE TO COORDINATE UTILITY CROSSINGS AT CULVERT CROSSINGS BEFORE STARTING WORK ON CULVERT. COORDINATE WITH OWNER REPRESENTATIVE. VERIFY UTILITY LINES AND/OR CONDUITS ARE IN PLACE BEFORE STARTING CULVERT WORK.
- CONSTRUCT RETENTION BASIN AS SHOWN. CONTRACTOR TO SCARIFY BOTTOM OF BASIN TWO FEET DEEP AND NOT ALLOW COMPACTION OVER BOX.
- THIS PROJECT REQUIRES A REGULAR ONGOING MAINTENANCE PROGRAM FOR THE DESIGNED DRAINAGE SYSTEM(S) TO PRESERVE THE DESIGN INTEGRITY AND THE ABILITY TO PERFORM ITS OPERATIONAL INTENT. FAILURE TO PROVIDE MAINTENANCE WILL JEOPARDIZE THE DRAINAGE SYSTEM(S) PERFORMANCE AND MAY LEAD TO ITS INABILITY TO PERFORM PROPERLY AND/OR CAUSE DAMAGE ELSEWHERE IN THE PROJECT.
- SEWER LINES DESIGNED IN PROFILE AND PUBLIC WATER LINES ARE REQUIRED TO BE ASBUILT AND THE INSTALLATION AND TESTING WITNESSED BY A PROFESSIONAL ENGINEER IN ACCORDANCE WITH ARIZONA ADMINISTRATIVE CODES R18-9-E301 "4.01 GENERAL PERMIT: SEWAGE COLLECTIONS SYSTEMS" AND R18-4-507 AND 508 "APPROVAL OF CONSTRUCTION" AND "RECORD DRAWINGS", RESPECTIVELY. IT IS THE CONTRACTOR'S RESPONSIBILITY TO NOTIFY OWNER 72 HOURS IN ADVANCE WHEN THOSE SYSTEMS ARE READY TO BE WITNESSED.
- THE WORK PRODUCT PRESENTED IS BELIEVED TO BE COMPLIANT WITH THE INTENT OF THE CURRENT AMERICANS DISABILITIES ACT (ADA) REQUIREMENTS AS INTERPRETED BY THE REVIEWING AGENCY(S). IF CONSTRUCTION OF THE PROJECT IS DELAYED, THIS WORK PRODUCT SHOULD BE UPDATED TO ACCOUNT FOR ANY RELEVANT ADA UPDATES BEFORE CONSTRUCTION BEGINS.

## UTILITY NOTES

- THESE PLANS HAVE BEEN SUBMITTED TO THE FOLLOWING UTILITY COMPANIES AND THE WORK CONTAINED IN THESE PLANS HAS BEEN APPROVED BY THESE COMPANIES WITHIN THEIR AREA OF INTEREST. THE SIZE AND LOCATIONS, AS SHOWN, OF THE GAS, TELEPHONE AND POWER LINES, AND CONNECTIONS AGREE WITH THE INFORMATION CONTAINED IN THE UTILITY COMPANY RECORDS. WHERE THE WORK TO BE DONE CONFLICTS WITH ANY OF THESE UTILITIES, THE CONFLICTS SHALL BE RESOLVED AS SPECIFIED. CONFLICTS ARISING DURING THE COURSE OF CONSTRUCTION FROM UNFORESEEN CIRCUMSTANCES SHALL BE REPORTED TO THE INTERESTED UTILITY COMPANY AND BE RESOLVED BY THEM AND THE DESIGN ENGINEER AND APPROVED BY THE COS.
- THE CITY WILL NOT PARTICIPATE IN THE COST OF CONSTRUCTION OR UTILITY RELOCATION.
- IN ACCORDANCE WITH AAC R18-4-119, ALL MATERIALS ADDED AFTER JANUARY 1, 1993 WHICH MAY COME INTO CONTACT WITH DRINKING WATER SHALL CONFORM TO NATIONAL SANITATION FOUNDATION STANDARDS 60 AND 61.

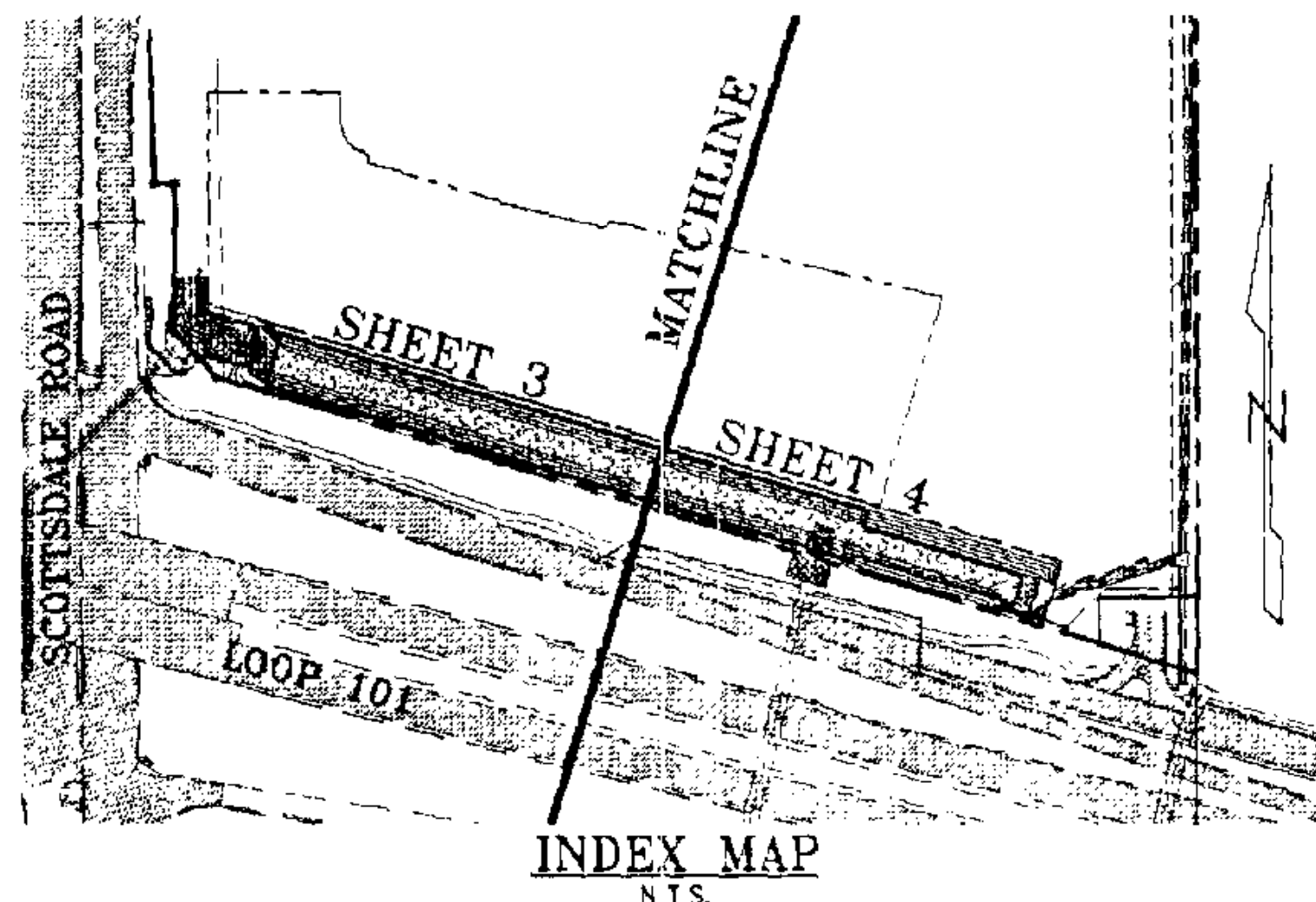
## HAUL ROUTE

HAUL ROUTE PERMITS ARE REQUIRED FOR ANY HAUL OPERATION WHICH UTILIZES CITY RIGHT-OF-WAY WITH A VOLUME EXCEEDING 5,000 C.Y.

# ONE SCOTTSDALE SOUTH DRAINAGE BASIN IMPROVEMENTS SCOTTSDALE, ARIZONA

## SHEET INDEX

1	COVER SHEET
2	NOTES/SECTIONS/LEGAL DESCRIPTION
3-4	PLAN SHEETS
5	DETAIL SHEET
STI-ST8	STORM TRAP UNDERGROUND DETENTION PLAN



## GENERAL NOTES

CITY OF SCOTTSDALE GENERAL CONSTRUCTION NOTES FOR PUBLIC WORKS CONSTRUCTION

- ALL CONSTRUCTION IN THE PUBLIC RIGHT-OF-WAY OR IN EASEMENTS GRANTED FOR PUBLIC USE MUST CONFORM TO THE LATEST MARICOPA ASSOCIATION OF GOVERNMENTS (MAG) UNIFORM STANDARD SPECIFICATIONS AND UNIFORM STANDARD DETAILS FOR PUBLIC WORKS CONSTRUCTION AS AMENDED BY THE LATEST VERSION OF THE CITY OF SCOTTSDALE (COS) SUPPLEMENTAL STANDARD SPECIFICATIONS AND SUPPLEMENTAL STANDARD DETAILS. IF THERE IS A CONFLICT, THE LATTER SHALL GOVERN.
- THE ENGINEERING DESIGNS ON THESE PLANS ARE ONLY APPROVED BY THE CITY IN SCOPE AND NOT IN DETAIL. IF CONSTRUCTION QUANTITIES ARE SHOWN ON THESE PLANS, THEY ARE NOT VERIFIED BY THE CITY.
- APPROVAL OF PLANS IS VALID FOR SIX (6) MONTHS. IF AN ENCROACHMENT PERMIT FOR THE CONSTRUCTION HAS NOT BEEN ISSUED WITHIN SIX MONTHS, THE PLANS SHALL BE RESUBMITTED TO THE CITY FOR RE-APPROVAL.
- A PUBLIC WORKS INSPECTOR WILL INSPECT ALL WORKS WITHIN THE CITY OF SCOTTSDALE RIGHT-OF-WAY AND IN EASEMENTS. NOTIFY INSPECTION SERVICES 24 HOURS PRIOR TO STARTING OF CONSTRUCTION (TELEPHONE 480-312-5750).
- WHENEVER EXCAVATION IS TO BE DONE, CALL THE "BLUE STAKE CENTER", 263-1100, TWO WORKING DAYS BEFORE EXCAVATION IS TO BEGIN. THE CENTER WILL SEE THAT THE LOCATION OF THE UNDERGROUND UTILITY LINES IS IDENTIFIED FOR THE PROJECT. CALL "COLLECT" IF NECESSARY.
- ENCROACHMENT PERMITS ARE REQUIRED FOR ALL WORK IN PUBLIC RIGHTS-OF-WAY AND EASEMENTS GRANTED FOR PUBLIC PURPOSES. AN ENCROACHMENT PERMIT WILL BE ISSUED BY THE CITY UPON RECEIPT OF PAYMENT OF A BASE FEE PLUS A FEE FOR INSPECTION SERVICES TO BE PROVIDED BY THE CITY. COPIES OF ALL PERMITS SHALL BE RETAINED ON-SITE AND SHALL BE AVAILABLE FOR INSPECTION AT ALL TIMES. FAILURE TO PRODUCE THE REQUIRED PERMITS WILL RESULT IN IMMEDIATE WORK STOPPAGE UNTIL THE PROPER PERMIT DOCUMENTATION IS OBTAINED.
- ALL EXCAVATION AND GRADING WHICH IS NOT IN THE PUBLIC RIGHTS-OF-WAY OR NOT IN EASEMENTS GRANTED FOR PUBLIC USE MUST CONFORM TO CHAPTER 70, EXCAVATION AND GRADING, OF THE LATEST EDITION OF THE UNIFORM BUILDING CODE PREPARED BY THE INTERNATIONAL CONFERENCE OF BUILDING OFFICIALS. A PERMIT FOR THIS GRADING MUST BE SECURED FROM THE CITY FOR A FEE ESTABLISHED BY THE UNIFORM BUILDING CODE.
- ALL CONCRETE SHALL BE SAN DIEGO BUFF.

## INDEMNITY:

- CITY OF SCOTTSDALE WILL NOT BE RESPONSIBLE FOR REMOVAL, REPAIR, OR REPLACEMENT OF SIDEWALKS, LANDSCAPING OR ANY OTHER IMPROVEMENTS LOCATED WITHIN CITY EASEMENT(S) AS A RESULT OF ACCESS TO MAINTENANCE OF, OR REPAIRS TO THE WATERLINE SHOWN ON THESE PLANS.
- CITY OF SCOTTSDALE WILL NOT BE RESPONSIBLE FOR REMOVAL, REPAIR, OR REPLACEMENT OF THE RETAINING WALLS OR OTHER IMPROVEMENTS WITHIN CITY EASEMENT(S) AS A RESULT OF ACCESS TO, MAINTENANCE OF, OR REPAIRS TO THE RETAINING WALLS SURROUNDING THE DETENTION BASINS SHOWN ON THESE PLANS.

\*THE ENGINEER OF RECORD ON THESE PLANS HAS RECEIVED A COPY OF THE APPROVED STIPULATIONS FOR THIS PROJECT AND HAS DESIGNED THESE PLANS IN CONFORMANCE WITH THE APPROVED STIPULATIONS.\*

ENGINEER: LISA L. CRANE, P.E.

## LAND SURVEY DATA

E/W STREET ALIGN	BEARDSLEY ROAD
N/S STREET	SCOTTSDALE ROAD ALIGN
DESCRIPTION	MC BC HH, N. BOUND LANE, DOWN D.B.
TOWNSHIP	4N
RANGE	4E
SEC	26
COR	NW
DATE UPDATED	NA
NORTHING (1)	15,283.524
EASTING (1)	27,356.033
NAYO '88 ELEV (1)	1,662.878

## BENCHMARK AND TOPO SOURCE

ALL TOPOGRAPHY WAS OBTAINED FROM AERIAL MAPPING COMPANY, INC., PROJECT NUMBER 04134, FLIGHT DATE JUNE 26, 2004

I HEREBY CERTIFY THAT ALL ELEVATIONS REPRESENTED ON THIS PLAN ARE BASED ON THE ELEVATION DATUM FOR THE CITY OF SCOTTSDALE BENCHMARK PROVIDED ABOVE.

## CITY OF SCOTTSDALE REVIEW & RECOMMENDED APPROVAL BY:

FIRE DEPT	N/A	GRADING & DRAINAGE	09/25/07
PLANNING	09/25/07	WATER SEWER	N/A
TRAFFIC	N/A	PAVING	N/A
STRUCTURAL	09/25/07	RET. WALL	09/25/07
APPROVED BY: <i>Lisa L. Crane</i> DATE: 10/23/07			
ENGINEERING COORDINATOR MANAGER OR DESIGNEE			

## NO CONFLICT SIGNATURE BLOCK

UTILITY	UTILITY COMPANY	NAME OF COMPANY REPRESENTATIVE	TELEPHONE NUMBER	DATE SENT
WATER	CITY OF SCOTTSDALE	CITY OF SCOTTSDALE	N/A	N/A
SANITARY SEWER	CITY OF SCOTTSDALE	CITY OF SCOTTSDALE	N/A	N/A
ELECTRIC	A.P.S.	BARBARA HEIMER	602-371-6688	02-13-07
TELEPHONE	QWEST COMM.	CONFLICT LIAISON DEPT.	602-630-0498	02-13-07
NATURAL GAS	SOUTHWEST GAS CORP.	POW JINTASAWANG	602-749-8550	02-13-07
CABLE TV	COX CABLE	THANH DOAN	623-322-7086	02-13-07
OTHER	-	-	-	-
OTHER	-	-	-	-

## ENGINEER'S CERTIFICATION:

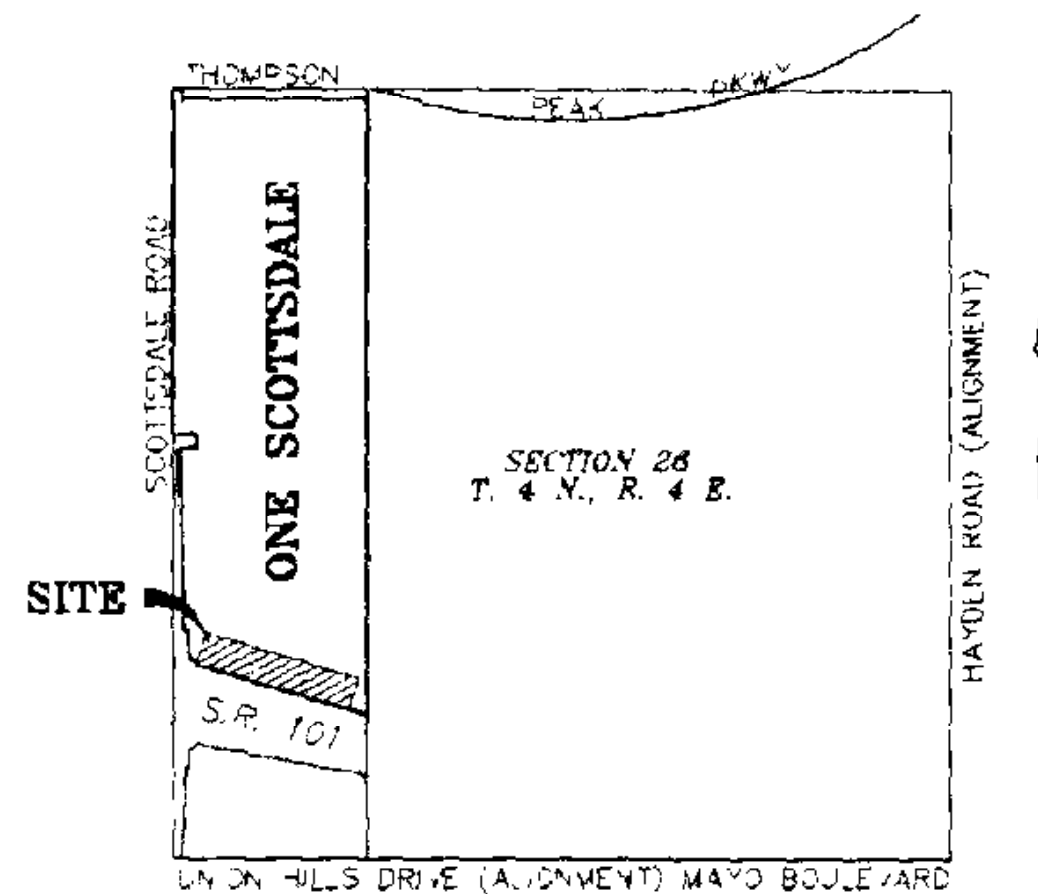
I, LISA L. CRANE, BEING THE PERSON RESPONSIBLE FOR DESIGNING THE FACILITIES NECESSARY TO SERVE THIS DEVELOPMENT, HEREBY CERTIFY THAT ALL OF THE UTILITY COMPANIES LISTED ABOVE, HAVE REVIEWED THIS PROJECT PROPOSAL AND ALL CONFLICTS HAVE BEEN RESOLVED AT THIS POINT. "NO CONFLICTS" FORMS HAVE BEEN OBTAINED FROM EACH UTILITY COMPANY AND ARE INCLUDED IN THIS SUBMITTAL. I ALSO CERTIFY THAT ALL ON-SITE TRANSFORMERS, CABLE BOXES AND ANY OTHER PUBLIC/PRIVATE UTILITY APPURTENANCES ARE PLACED SUCH THAT THEY DO NOT NEGATIVELY IMPACT THE USE OR INTENDED USE OF ANY DEDICATED EASEMENTS OR FACILITIES DEVELOPED WITH THIS PROJECT INCLUDING BUT NOT LIMITED TO STORMWATER STORAGE BASINS, SIGHT DISTANCE EASEMENTS AND NADS OR OTHER OPEN SPACE EASEMENTS.

SIGNATURE: *Lisa L. Crane* DATE: 10/23/07

## FLOOD INSURANCE RATE MAP (FIRM) INFORMATION

COMMUNITY NUMBER	PANEL NUMBER	SUFFIX	DATE OF FIRM	FIRM ZONE	BASE FLOOD ELEVATION (1 IN AO ZONE, USE DEPTH)
045012	1245	G	SEPT. 30, 2005	AO	1'

CALL TWO WORKING DAYS BEFORE YOU DO  
**263-1100**  
**1-800-STAKE-IT**  
(OUTSIDE MARICOPA COUNTY)



## VICINITY MAP N.T.S.

## OWNER / DEVELOPER

ONE SCOTTSDALE HOLDINGS LLC  
7600 E. DOUBLETREE RANCH RD. SUITE 300  
SCOTTSDALE, AZ 85258  
CONTACT: MR. ART NEHF  
TEL: (480) 367-7000  
FAX: (480) 367-7558

## ENGINEER

WOOD, PATEL & ASSOCIATES INC.  
2051 WEST NORTHERN, SUITE 100  
PHOENIX, ARIZONA 85021  
CONTACT: MS. LISA L. CRANE, P.E.  
(602) 335-8500  
(FAX) 335-8580

## EARTHWORK QUANTITIES

QUANTITIES ARE IN PLACE ESTIMATES. VOLUME OF CUT FOR UNDERGROUND STORAGE IS INCLUDED. NO SHRINK OR SWELL IS ASSUMED.

DESCRIPTION	QUANTITY
CUT	17,800 C.Y.
FILL	80 C.Y.

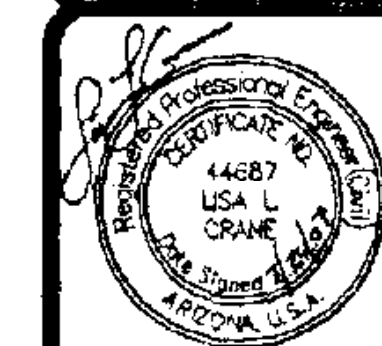
## DETENTION CALCULATIONS

THIS PLAN SHOULD BE REVIEWED WITH THE MASTER DRAINAGE REPORT DATED 09-26-06 PREPARED BY WOOD, PATEL & ASSOCIATES.

DMB

WOOD/PATEL  
Civil Engineers  
Hydrologists  
Construction Managers  
(602) 335-8500

ONE SCOTTSDALE  
SOUTH DRAINAGE BASIN IMPROVEMENTS  
SCOTTSDALE, ARIZONA



DRAWN	YLV
CHECKED	SAA
DATE	27 JULY 2007
SCALE	
JOB NO.	021584.14
SHEET	1 OF 5



## LEGAL DESCRIPTION

THE WEST HALF OF THE WEST HALF OF SECTION 26, TOWNSHIP 4 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER BASE AND MERIDIAN, MARICOPA COUNTY, ARIZONA;

EXCEPT THE NORTH 100 FEET OF THE WEST 165 FEET OF THAT PART OF THE NORTHWEST QUARTER OF SECTION 26, TOWNSHIP 4 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER BASE AND MERIDIAN, MARICOPA COUNTY, ARIZONA, LYING SOUTH OF AND ADJOINING A STRAIGHT LINE DRAWN AT A RIGHT ANGLE FROM A POINT ON THE WEST LINE OF SAID NORTHWEST QUARTER OF SAID SECTION 26, SAID POINT BEING 2367.00 FEET SOUTH OF THE NORTHWEST CORNER OF SAID SECTION 26; AND ALSO

EXCEPT THAT PORTION OF THE WEST HALF OF THE WEST HALF OF SECTION 26, TOWNSHIP 4 NORTH, RANGE 4 EAST OF THE GILA AND SALT RIVER BASE AND MERIDIAN, MARICOPA COUNTY, ARIZONA, WHICH LIES WITHIN THE PARCEL OF LAND DESCRIBED AS FOLLOWS:

BEGINNING AT A UNITED STATES GENERAL LAND OFFICE BRASS CAP MARKING THE SOUTHWEST CORNER OF SAID SECTION 26; THENCE ALONG THE WEST LINE OF SAID SECTION 26, NORTH 0 DEGREES 02 MINUTES 08 SECONDS WEST, 2642.06 FEET TO A MARICOPA COUNTY HIGHWAY DEPARTMENT BRASS CAP MARKING THE WEST QUARTER CORNER OF SAID SECTION 26; THENCE CONTINUING ALONG SAID WEST LINE, NORTH 0 DEGREES 02 MINUTES 08 SECONDS WEST 170.94 FEET TO A POINT 2467.00 FEET SOUTH OF THE NORTHWEST CORNER OF SAID SECTION 26; THENCE LEAVING SAID WEST LINE, NORTH 89 DEGREES 57 MINUTES 54 SECONDS EAST 52.30 FEET TO A POINT HEREINAFTER CALLED POINT "A"; THENCE SOUTH 01 DEGREES 52 MINUTES 53 SECONDS EAST, 1238.42 FEET TO A POINT HEREINAFTER CALLED POINT "B"; THENCE NORTH 89 DEGREES 57 MINUTES 54 SECONDS EAST, 25.00 FEET TO A LINE PARALLEL WITH AND 110.00 FEET EAST OF THE WEST LINE OF SAID SECTION 26; THENCE ALONG SAID PARALLEL LINE, SOUTH 0 DEGREES 02 MINUTES 08 SECONDS EAST, 175.00 FEET; THENCE SOUTH 42 DEGREES 29 MINUTES 44 SECONDS EAST, 74.07 FEET; THENCE SOUTH 73 DEGREES 12 MINUTES 54 SECONDS EAST, 1212.44 FEET TO THE EAST LINE OF SAID WEST HALF OF THE WEST HALF; THENCE ALONG SAID EAST LINE, SOUTH 0 DEGREES 01 MINUTES 50 SECONDS EAST, 421.98 FEET; THENCE NORTH 79 DEGREES 08 MINUTES 01 SECONDS WEST, 1176.82 FEET; THENCE SOUTH 50 DEGREES 34 MINUTES 39 SECONDS WEST, 71.10 FEET TO A LINE PARALLEL WITH AND 110.00 FEET EAST OF THE WEST LINE OF SAID SECTION 26; THENCE ALONG SAID PARALLEL LINE, SOUTH 0 DEGREES 02 MINUTES 08 SECONDS EAST, 125.00 FEET; THENCE SOUTH 89 DEGREES 57 MINUTES 54 SECONDS WEST, 25.00 FEET TO A POINT HEREINAFTER CALLED POINT "C"; THENCE SOUTH 01 DEGREES 28 MINUTES 41 SECONDS WEST, 825.30 FEET TO THE SOUTH LINE OF SAID SECTION 26 AND TO A POINT HEREINAFTER CALLED POINT "D"; THENCE ALONG SAID SOUTH LINE, NORTH 89 DEGREES 58 MINUTES 35 SECONDS WEST, 68.49 FEET TO THE POINT OF BEGINNING; AND ALSO

EXCEPT THAT PORTION OF THE SOUTHWEST QUARTER OF THE SOUTHWEST QUARTER OF SAID SECTION 26, DESCRIBED AS FOLLOWS:

COMMENCING AT A UNITED STATES GENERAL LAND OFFICE BRASS CAP MARKING THE SOUTHWEST CORNER OF SAID SECTION 26, BEING NORTH 89 DEGREES 58 MINUTES 35 SECONDS WEST 2641.00 FEET FROM A 3/4 INCH REBAR MARKING THE SOUTH QUARTER CORNER OF SAID SECTION 26; THENCE ALONG THE WEST LINE OF SAID SECTION 26, NORTH 0 DEGREES 02 MINUTES 28 SECONDS WEST 625.01 FEET TO A POINT BEING SOUTH 0 DEGREES 02 MINUTES 26 SECONDS EAST 2015.78 FEET FROM THE MARICOPA COUNTY HIGHWAY BRASS CAP MARKING THE WEST QUARTER CORNER OF SAID SECTION 26; THENCE NORTH 89 DEGREES 57 MINUTES 34 SECONDS EAST 110.00 FEET TO THE POINT OF BEGINNING ON THE SOUTHERLY RIGHT OF WAY LINE OF STATE ROUTE 101 (PIMA FREEWAY); THENCE ALONG SAID SOUTHERLY RIGHT OF WAY LINE, SOUTH 89 DEGREES 57 MINUTES 54 SECONDS WEST 25.00 FEET;

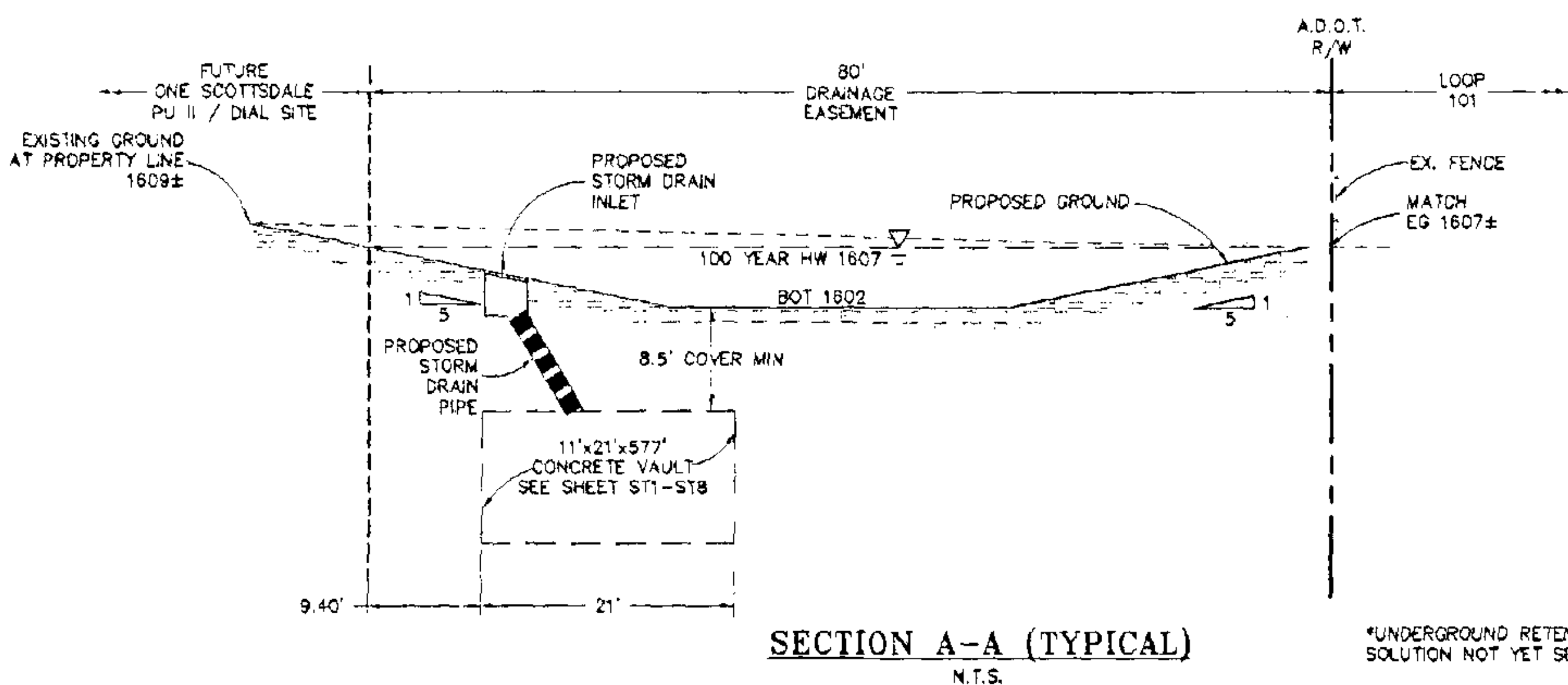
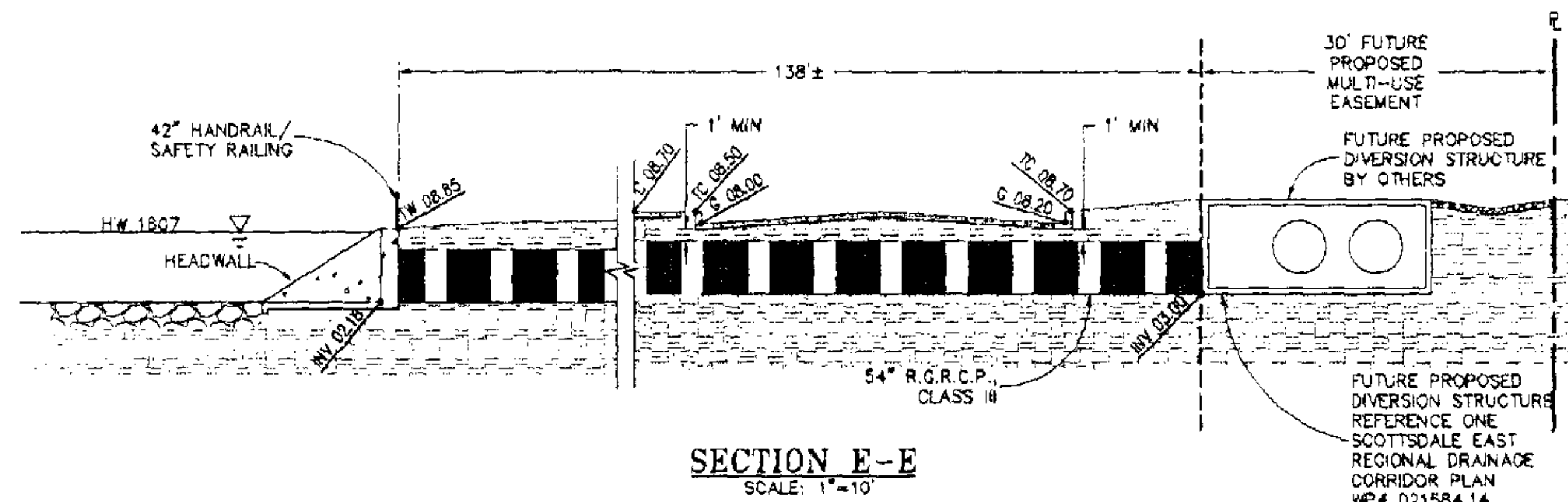
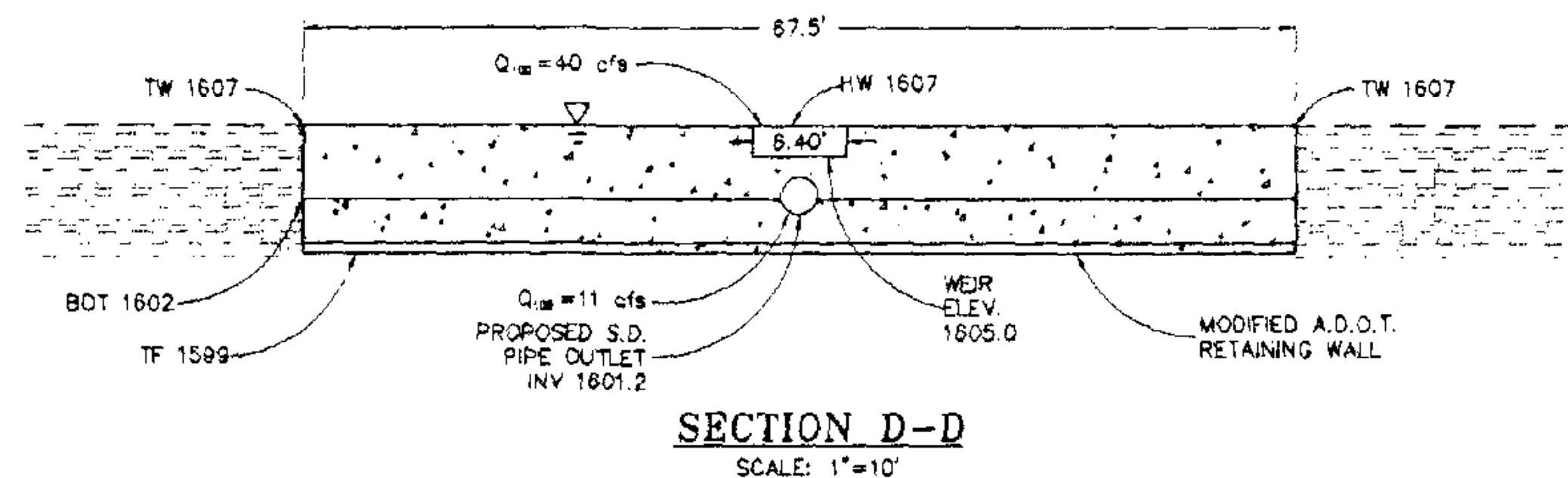
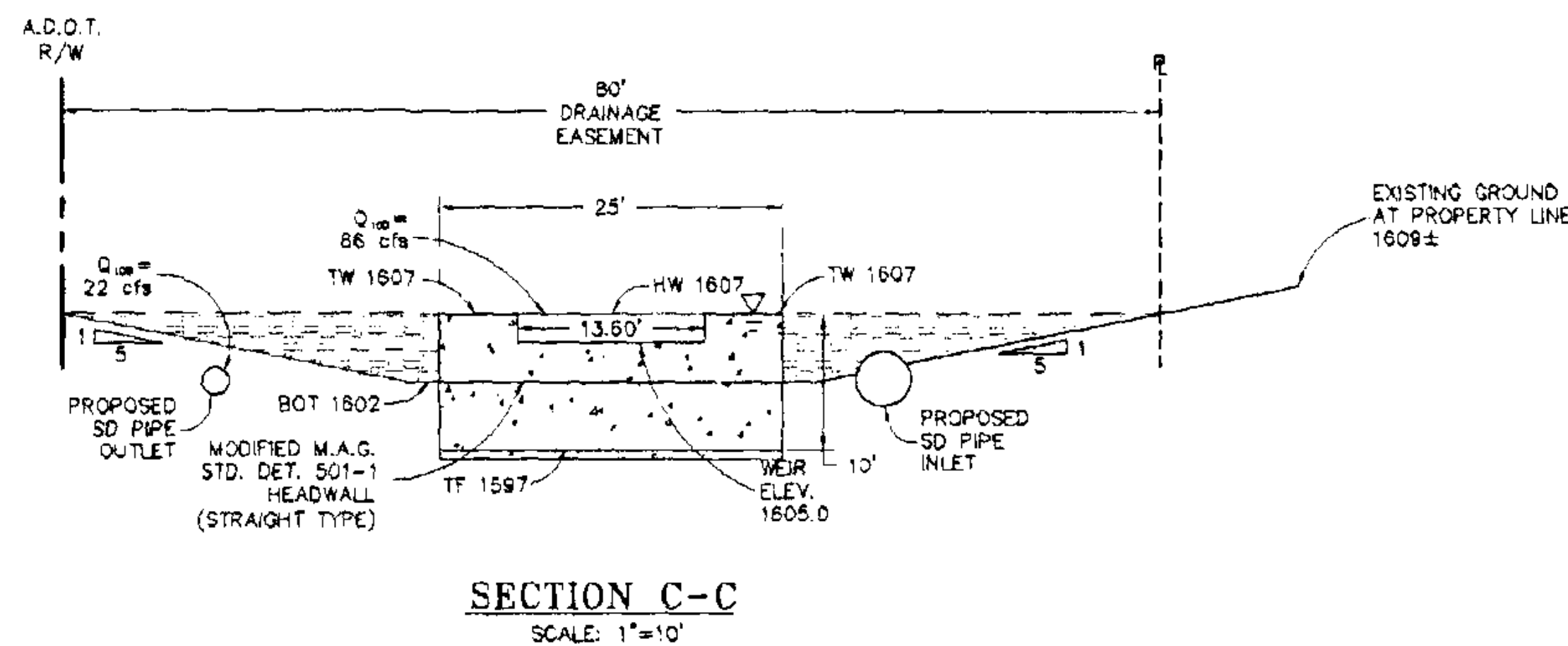
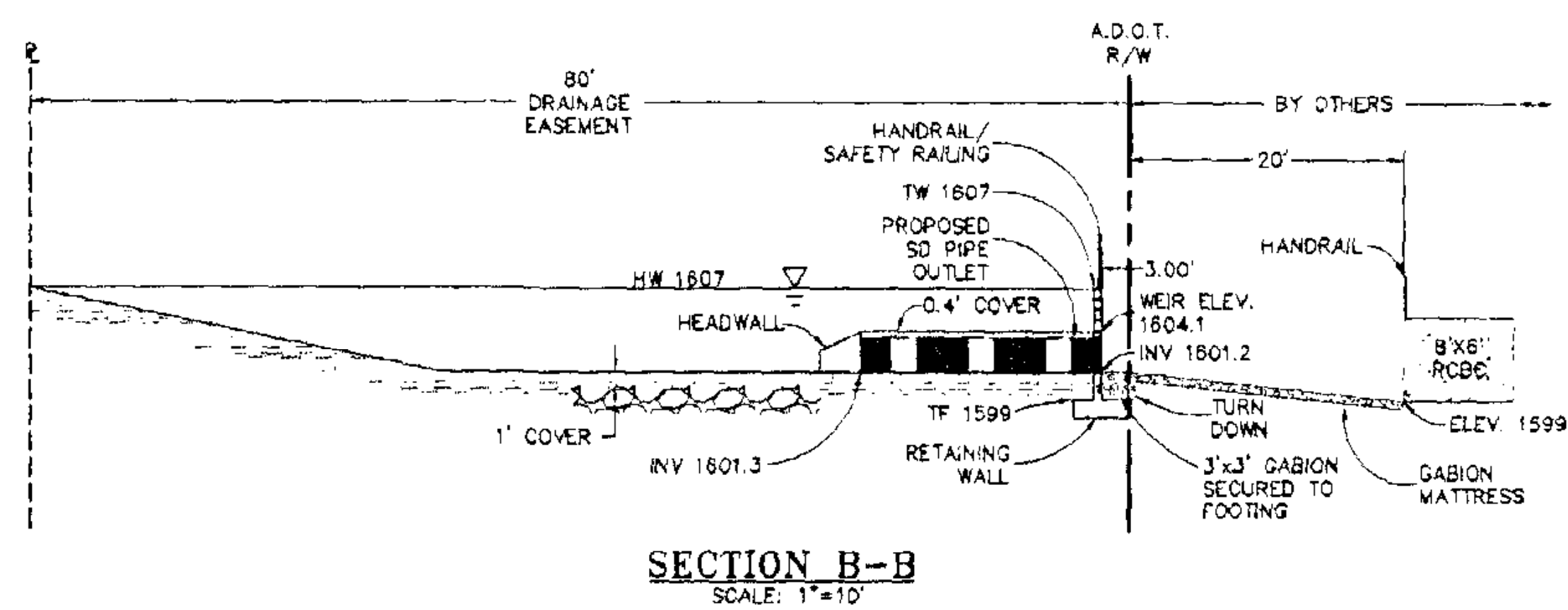
THENCE CONTINUING ALONG SAID SOUTHERLY RIGHT OF WAY LINE, SOUTH 01 DEGREES 28 MINUTES 41 SECONDS WEST 50.00 FEET; THENCE NORTH 27 DEGREES 44 MINUTES 09 SECONDS EAST 58.49 FEET TO THE POINT OF BEGINNING; AND ALSO

EXCEPT A PARCEL OF LAND LYING WITHIN SAID SECTION 26, MORE PARTICULARLY DESCRIBED AS FOLLOWS:

COMMENCING AT THE SOUTHWEST CORNER OF SAID SECTION 26; THENCE ALONG THE SOUTH LINE OF SAID SECTION, SOUTH 89 DEGREES 58 MINUTES 26 SECONDS EAST, A DISTANCE OF 68.49 FEET TO THE EASTERLY LINE OF PARCEL NO. 7-5398, TRACT NO. 1, AS RECORDED IN INSTRUMENT NO. 2002-0284002, AND THE POINT OF BEGINNING; THENCE LEAVING SAID SOUTH LINE ALONG SAID EASTERLY LINE, NORTH 01 DEGREES 28 MINUTES 38 SECONDS EAST, A DISTANCE OF 625.29 FEET; THENCE NORTH 89 DEGREES 57 MINUTES 52 SECONDS EAST, A DISTANCE OF 25.00 FEET; THENCE NORTH 00 DEGREES 02 MINUTES 08 SECONDS WEST, A DISTANCE OF 124.88 FEET; THENCE NORTH 50 DEGREES 34 MINUTES 37 SECONDS EAST, A DISTANCE OF 71.10 FEET; THENCE SOUTH 79 DEGREES 08 MINUTES 03 SECONDS EAST, A DISTANCE OF 1176.65 FEET TO THE EAST LINE OF THE WEST HALF OF THE WEST HALF OF SAID SECTION 26; THENCE LEAVING SAID EASTERLY LINE ALONG SAID EAST LINE, SOUTH 00 DEGREES 02 MINUTES 11 SECONDS EAST, A DISTANCE OF 573.88 FEET TO THE SOUTH LINE OF SAID SECTION; THENCE LEAVING SAID EAST LINE ALONG SAID SOUTH LINE, NORTH 89 DEGREES 58 MINUTES 26 SECONDS WEST, A DISTANCE OF 1251.89 FEET TO THE POINT OF BEGINNING.

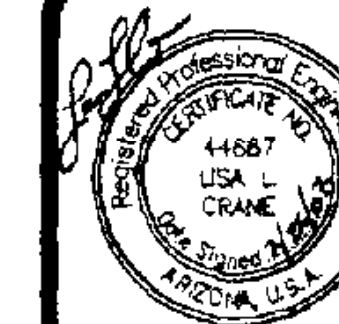
## LEGEND

	PROPOSED CONTOUR
	EXISTING CONTOUR
	PROPOSED RIGHT OF WAY
	ROADWAY CENTERLINE
	VERTICAL CURB & GUTTER
	PROPOSED INVERT ELEVATION
	TOP OF CURB ELEVATION (FROM CITY OF SCOTTSDALE DIBBLE PLAN)
	RIP-RAP AREA ID
	TOP OF DURB ELEVATION (FROM TOPO)
	GUTTER ELEVATION (FROM TOPO)
	NATURAL GROUND ELEVATION (FROM TOPO)
	PAVEMENT CENTERLINE ELEVATION (FROM ADOT PLANS)
	MEDIAN CENTERLINE ELEVATIONS (FROM ADOT PLANS)
	ARIZONA DEPARTMENT OF TRANSPORTATION
	TOP OF FOOTING
	TOP OF WALL
	RIGHT OF WAY
	HIGH WATER
	BOTTOM
	INVERT
	STORM DRAIN
	TYPICAL
	EXISTING GROUND
	ELEVATION
	CUBIC YARD
	REINFORCED CONCRETE PIPE
	REINFORCED CONCRETE BOX CULVERT
	PROPOSED STAND PIPE
	EXISTING STORM DRAIN
	PROPOSED STORM DRAIN
	PROPOSED CATCH BASIN
	EXISTING ROAD
	EXISTING CURB AND GUTTER
	FLOWLINE
	MISCELLANEOUS UTILITIES
	TRAFFIC SIGNAL
	SIGN
	HEADWALL WITH HANDRAIL
	LIMITS OF CONSTRUCTION



**ONE SCOTTSDALE**  
SOUTH DRAINAGE BASIN IMPROVEMENTS  
SCOTTSDALE, ARIZONA

**WOOD/PATEL**  
Civil Engineers  
Hydrologists  
Construction Managers  
(602) 335-8800



DRAWN: YLV  
CHECKED: SAA  
DATE: 27 JULY 2007  
SCALE:  
JOB NO.: 021584.14  
SHEET: 2 OF 5

CALL TWO WORKING DAYS BEFORE YOU DIG  
**283-1100**  
**1-800-STAKE-IT**  
(OUTSIDE MARICOPA COUNTY)



THOMPSON  
PEAK PARKWAY

NE CORNER, SEC. 27,  
T.4N., R.4E.  
C.O.S. B.C.H.H.  
STA: 207+13.42

FUTURE PROPOSED  
IMPROVEMENTS  
BOX CULVERT  
EXTENSION

FUTURE PROPOSED  
IMPROVEMENTS REFERENCE  
ONE SCOTTSDALE SOUTH  
END IMPROVEMENTS PLAN  
(WP # 052583.06)

SCENIC CORRIDOR  
(LOCATION FINALIZED PER  
FINAL DEVELOPMENT PLANS)

DIAL  
PROPERTY  
LINE

ONE SCOTTSDALE PU II

MATCH SHEET 4

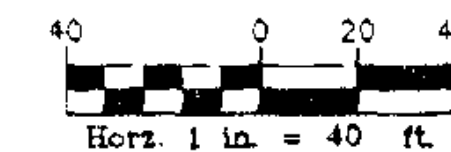
LOOP 101  
(FRONTAGE ROAD)

LOOP 101 (WEST BOUND LANES)

LOOP 101 (EAST BOUND LANES)

UNION HILLS  
DRIVE

SW CORNER, SEC. 26,  
T.4N., R.4E.  
B.C.H.H.  
STA: 154+31.64



### CONSTRUCTION NOTES

- 1 CONTRACTOR TO REMOVE EARTH, BUILD APPROVED CONTAINMENT STRUCTURE, PLACE FILL OVER STRUCTURE, AND GRADE FINAL BASIN PER PLAN AND APPROPRIATE SECTIONS.
- 2 INSTALL 3" THICK BURIED RIP-RAP,  $D_{50}=8"$  PER GRADATION TABLE AND RIP-RAP AREA TABLE. SEE SHEET 4. SEE BURIED RIP-RAP DETAIL, SHEET 5.
- 3 INSTALL TWO CATCH BASIN INLETS SIDE BY SIDE PER MODIFIED A.D.O.T. STD. DET. C-15.90. SEE SHEET 5 FOR MODIFICATIONS. CONNECT CATCH BASIN TO UNDERGROUND STORAGE VIA 18" H.D.P.E. STORM DRAIN PIPE.
- 4 INSTALL STORM TRAP UNDERGROUND CONTAINMENT STRUCTURE FOR STORM WATER STORAGE HOLDING 106,722 C.F. (2.45 AC. FT.). SLOPE STRUCTURE TO DRAIN TO EAST AT 0.0010 FT./FT. MINIMUM. SEE STORM TRAP PLAN, STI-5TB.
- 5 INSTALL HEADWALL PER MAG STD. DET. 501-4 WITH TRASH RACK PER MAG. STD. DETAIL 502-1 & 42" HANDRAIL PER C.O.S. STD. DETAIL 2508. COLOR TO BE SAN DIEGO BUFF.
- 9 INSTALL 24" R.G.R.C.P., CLASS III, TRENCH BEDDING & BACKFILL PER C.O.S. STD. DET. 2201.
- 13 INSTALL 48" PLUG FOR CONTINUATION SEE ONE SCOTTSDALE SOUTH END IMPROVEMENT PLAN. CONTRACTOR TO VERIFY HORIZONTAL AND VERTICAL LOCATION PRIOR TO START OF CONSTRUCTION AND NOTIFY OWNER OF ANY DISCREPANCIES.
- 14 INSTALL 48" R.G.R.C.P., CLASS II, TRENCH BEDDING & BACKFILL PER C.O.S. STD. DET. 2201.
- 15 CONSTRUCT 13.5' WIER IN MODIFIED M.A.G. STD. DET. 501-1 HEADWALL (STRAIGHT TYPE). SEE SHEET 2, SECTION C-C FOR MODIFICATIONS. COLOR TO BE SAN DIEGO BUFF.
- 17 CONSTRUCT STORM DRAIN MANHOLE PER M.A.G. STD. DET. 520 & 522. ADJUST MANHOLE RIM TO FINAL GRADE PER C.O.S. STD. DET. 2270.
- 20 INSTALL 19.5" ORIFICE PLATE OVER STORM DRAIN INLET PER DETAIL ON SHEET 5.
- 22 INSTALL STRAIGHT TYPE BLOCK HEADWALL PER M.A.G. STD. DET. 501-1 AND 501-2 WITH TRASH RACK PER M.A.G. STD. DET. 502-1 & 42" HANDRAIL PER C.O.S. STD. DET. 2508. CONNECT TO EXISTING A.D.O.T. HEADWALL COLOR TO BE SAN DIEGO BUFF.

DMB

WOOD/PATEL  
Civil Engineers  
Hydrologists  
Geologists  
Construction Managers  
(905) 955-8900

## ONE SCOTTSDALE

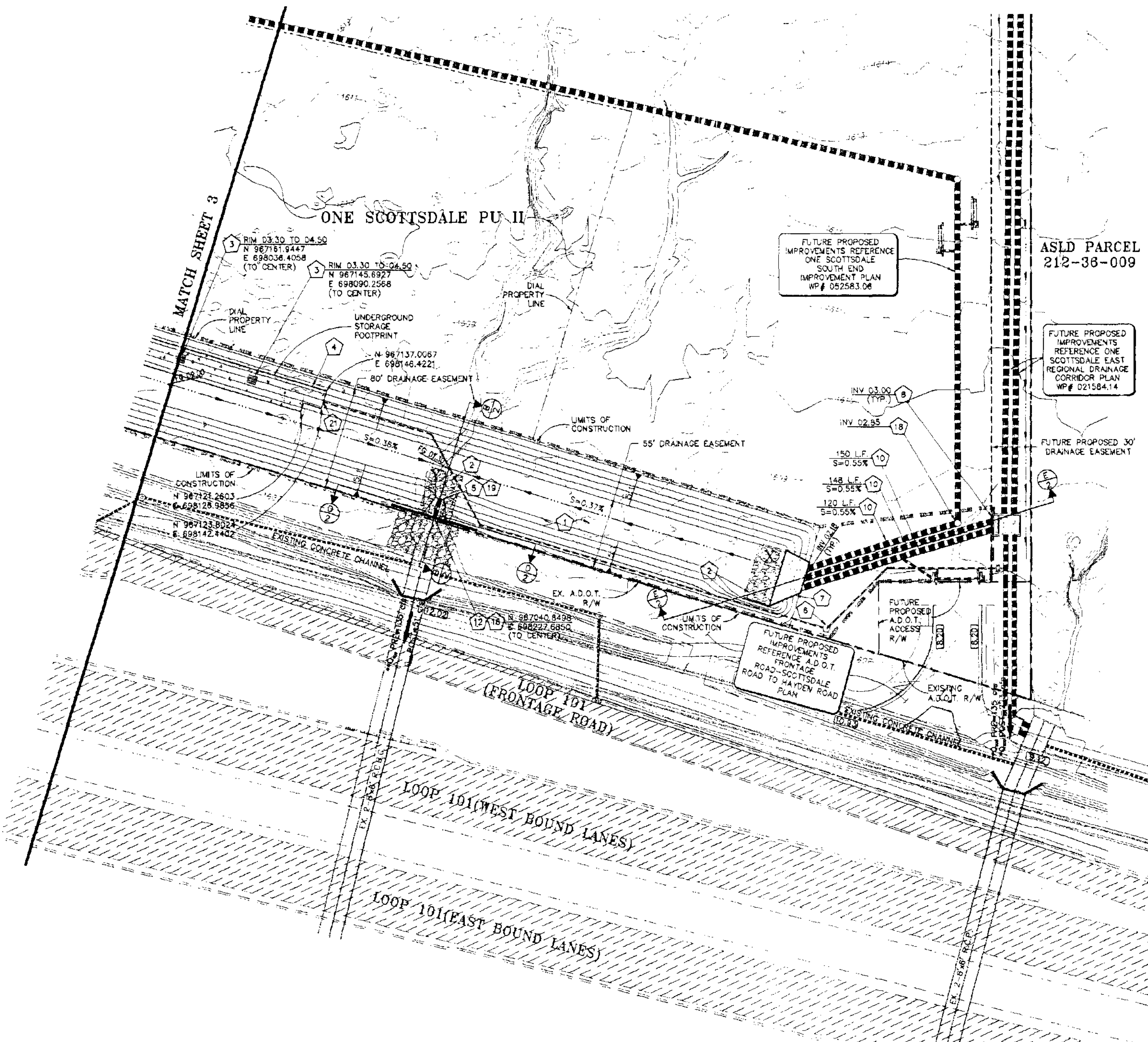
### SOUTH DRAINAGE BASIN IMPROVEMENTS SCOTTSDALE, ARIZONA



DRAWN	YU
CHECKED	SAA
DATE	27 JULY 2007
SCALE	1"=40'
JOB NO.	021584.14
SHEET	3 OF 5

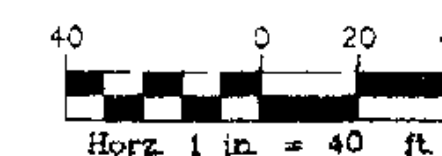
CALL TWO WORKING DAYS  
BEFORE YOU DIG  
**263-1100**  
**1-800-STAKE-IT**  
(OUTSIDE MARICOPA COUNTY)





# CONSTRUCTION NOTES

1. CONTRACTOR TO REMOVE EARTH, BUILD APPROVED CONTAINMENT STRUCTURE, PLACE FILL OVER STRUCTURE, AND GRADE FINAL BASIN PER PLAN AND APPROPRIATE SECTIONS.
2. INSTALL 3' THICK BURIED RIP-RAP, D<sub>50</sub>=8" PER GRADATION TABLE AND RIP-RAP AREA TABLE. SEE SHEET 4. SEE BURIED RIP-RAP DETAIL, SHEET 5.
3. INSTALL TWO CATCH BASIN INLETS SIDE BY SIDE PER MODIFIED A.D.O.T. STD. DET. C-13.90. SEE SHEET 5 FOR MODIFICATIONS. CONNECT CATCH BASIN TO UNDERGROUND STORAGE VIA 18" H.D.P.E. STORM DRAIN PIPE.
4. INSTALL STORM TRAP UNDERGROUND CONTAINMENT STRUCTURE FOR STORM WATER STORAGE HOLDING 470,448 C.F. (10.8 AC. FT.). SLOPE STRUCTURE TO DRAIN TO EAST 0.0010 FT/FT MINIMUM. SEE STORM TRAP PLAN, ST1-ST8.
5. INSTALL HEADWALL PER M.A.G. STD. DET. 501-4 WITH TRASH RACK PER M.A.G. STD. DET. 502-1 & 42" HANDRAIL PER C.O.S. STD. DET. 2508. COLOR TO BE SAN DIEGO BUFF.
6. REFERENCE WOOD/PATEL LIFT STATION PLAN.
7. CONSTRUCT MULTIPLE PIPE OUTLET PER ADOT STD. DET. B11.14 WITH 30' SKEW ANGLE & 4:1 WING WALLS. EXTEND SOUTH WING WALL PER PLAN AND DETAIL A OF A.D.O.T. STD. DET. B-11.12. INSTALL TRASH RACK PER MAG. STD. DETAIL 502-1 & HANDRAIL PER C.O.S. STD. DETAIL 2508. COLOR TO BE SAN DIEGO BUFF.
8. FOR CONTINUATION SEE EAST REGIONAL DRAINAGE CORRIDOR PLAN. CONTRACTOR TO VERIFY HORIZONTAL AND VERTICAL LOCATION PRIOR TO START OF CONSTRUCTION AND NOTIFY OWNER OF ANY DISCREPANCIES.
10. INSTALL 54" R.G.R.C.P. CLASS III. TRENCH BEDDING AND BACKFILL PER C.O.S. STD. DET. 2201.
12. CONSTRUCT A.D.O.T. RETAINING WALL (MODIFIED) WITH 6.4' WIDE WEIR OPENING. CONTRACTOR TO SELECT WALL TYPE, EITHER A.D.O.T. STD. DET. B-18.10 OR B-18.50. FOR B-18.10 USE H=8' AND W=5'-0". FOR B-18.50 USE H=8' AND W=5'-6". SEE SHEET 5 FOR DETAILS. SEE SECTION B-B AND D-D ON SHEET 2. COLOR TO BE SAN DIEGO BUFF.
18. INSTALL THREE 3'x3' GABIONS CENTERED BENEATH WEIR OPENING IN RETAINING WALL. CONTRACTOR TO SECURE GABIONS TO FOOTING. SEE SECTION B-B ON SHEET 2.
18. INSTALL 54" PLUG. FOR CONTINUATION SEE ONE SCOTTSDALE PLANNING UNIT II GRADING AND DRAINAGE PLAN. CONTRACTOR TO VERIFY HORIZONTAL AND VERTICAL LOCATION PRIOR TO START OF CONSTRUCTION AND NOTIFY OWNER OF ANY DISCREPANCIES.
19. INSTALL 13.6" ORIFICE PLATE OVER STORM DRAIN INVERT PER DETAIL ON SHEET 5.
21. REFERENCE STORM TRAP PLAN FOR SUMP INVERT.



## GRADATION TABLE\*

PERCENT PASSING	SIZE	D <sub>50</sub> CLASS, INCHES			
100 TO 90	2.0 D <sub>50</sub>	8	12	16	24
85 TO 70	1.5 D <sub>50</sub>	6	9	12	18
50 TO 30	1.0 D <sub>50</sub>	4	6	8	12
15 TO 5	0.67 D <sub>50</sub>	3	4	5	8
5 TO 0	0.33 D <sub>50</sub>	1	2	3	4

\*INDIGENOUS/NATIVE STONE

## RIP-RAP TABLE

AREA ID	AREA SIZE
W	40'x150'
X	20'x40'
Y	25'x35'
Z	25'x55'

\*THE 100 YEAR POST DEVELOPMENT DISCHARGE IS DESIGNED TO EXCEED THE 100 YEAR PRE DEVELOPMENT DISCHARGE DUE TO A DOWNSTREAM REGIONAL FLOOD CONTROL SOLUTION.

\*\*FLOWS FROM THE EXISTING A.D.O.T. BOX CULVERTS MERGE SOUTH OF THE LOOP 101. THE COMBINED 100 YEAR PRE DEVELOPMENT DISCHARGE IS APPROXIMATED AT 135 CFS.



**DMB**

WOOD/PATEL  
Civil Engineer  
Professional Seal  
Land Surveyor  
Construction Manager  
(602) 330-8600

**ONE SCOTTSDALE**  
SOUTH DRAINAGE BASIN IMPROVEMENTS  
SCOTTSDALE, ARIZONA



DRAWN YLU  
CHECKED SAA  
DATE 27 JULY 2007  
SCALE 1"=40'  
JOB NO. 021584.14  
SHEET 4 OF 5





***Appendix M***

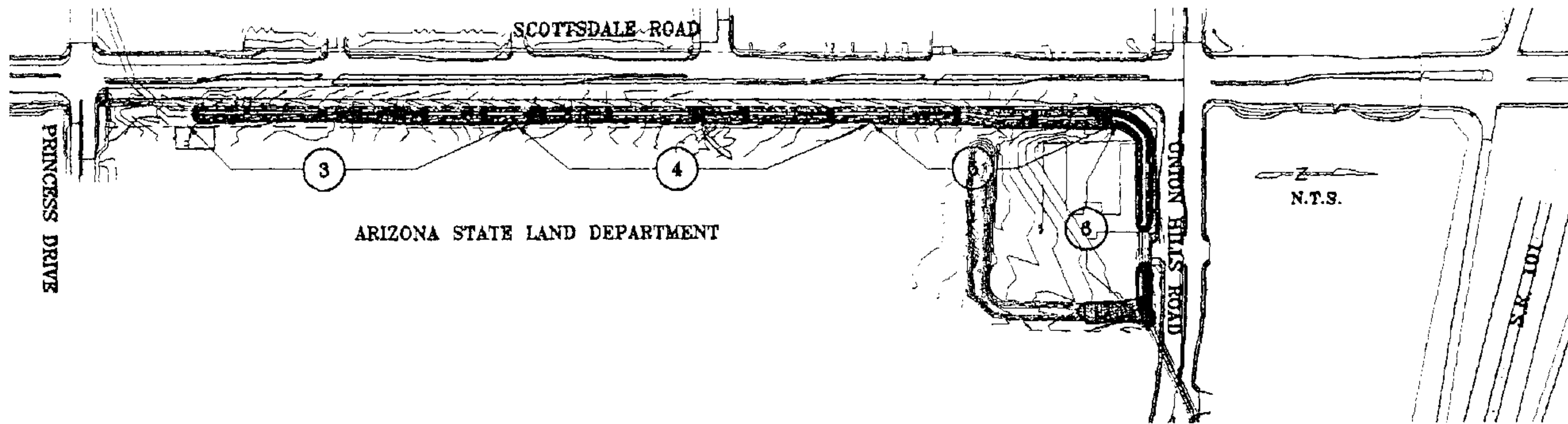
**As- Builts for Scottsdale Road Intrim Drainage Channel**



INTERIM REGIONAL DRAINAGE CHANNEL IMPROVEMENT PLAN  
A PORTION OF SECTION 35 T.4N., R.4E., OF THE G.&S.R.M.,  
MARICOPA COUNTY, ARIZONA

ENGINEERS NOTES

- MARICOPA ASSOCIATION OF GOVERNMENTS (M.A.G.) UNIFORM STANDARD SPECIFICATIONS AND DETAILS FOR PUBLIC WORKS CONSTRUCTION (LATEST EDITION INCLUDING LATEST REVISION AND CURRENT SUPPLEMENTALS THEREOF PER THE LOCAL TOWN OR CITY) ARE INCORPORATED INTO THIS PLAN IN THEIR ENTIRETY.
- ALL WORK REQUIRED TO COMPLETE THE CONSTRUCTION COVERED BY THIS PLAN SHALL BE IN ACCORDANCE WITH THE M.A.G. STANDARD SPECIFICATIONS AND DETAILS AND CURRENT SUPPLEMENTALS THEREOF PER THE LOCAL CITY OR TOWN UNLESS SPECIFIED OTHERWISE IN THESE PLANS OR ELSEWHERE IN THE CONTRACT DOCUMENTS. CONTRACTORS SHALL FAMILIARIZE THEMSELVES WITH ALL REQUIRED STANDARD SPECIFICATIONS, DETAILS AND SUPPLEMENTS PRIOR TO BIDDING THE WORK FOR THE CONSTRUCTION COVERED BY THIS PLAN.
- THE CONTRACTOR IS RESPONSIBLE FOR ALL METHODS, SEQUENCING, AND SAFETY CONCERNS ASSOCIATED WITH THIS PROJECT DURING CONSTRUCTION UNLESS SPECIFICALLY ADDRESSED OTHERWISE IN THIS PLAN OR ELSEWHERE IN THE CONTRACT.
- THE CONTRACTOR IS TO COMPLY WITH ALL LOCAL, STATE, AND FEDERAL LAWS AND REGULATIONS APPLICABLE TO THE CONSTRUCTION COVERED BY THIS PLAN.
- THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING AND COMPLYING WITH ALL PERMITS REQUIRED TO COMPLETE ALL WORK COVERED BY THIS PLAN.
- THE QUANTITIES AND SITE CONDITIONS DEPICTED IN THESE PLANS ARE FOR INFORMATIONAL PURPOSES ONLY AND ARE SUBJECT TO ERROR AND OMISSION. CONTRACTORS SHALL SATISFY THEMSELVES AS TO ACTUAL QUANTITIES AND SITE CONDITIONS PRIOR TO BIDDING THE WORK FOR THE CONSTRUCTION COVERED BY THIS PLAN.
- A REASONABLE EFFORT HAS BEEN MADE TO SHOW THE LOCATIONS OF EXISTING UTILITIES AND UTILITIES IN THE CONSTRUCTION AREA. THE CONTRACTOR IS RESPONSIBLE FOR ANY DAMAGE TO UTILITIES AND/OR FACILITIES CAUSED DURING THEIR CONSTRUCTION OPERATIONS. THE CONTRACTOR SHALL CALL 48 HOURS IN ADVANCE FOR BLUE STAKE (1-800-STAKE-IT) PRIOR TO ANY EXCAVATION.
- THE CONTRACTOR IS RESPONSIBLE FOR ALL COORDINATION OF CONSTRUCTION AFFECTING UTILITIES AND THE COORDINATION OF ANY NECESSARY UTILITY RELOCATION WORK.
- ALL PAVING, GRADING, EXCAVATION, TRENCHING, PIPE BEDDING, CUT FILL AND BACKFILL SHALL COMPLY WITH THE RECOMMENDATIONS SET FORTH IN THE SOILS (GEOTECHNICAL) REPORT FOR THIS PROJECT IN ADDITION TO THE REFERENCED REQUIRED SPECIFICATIONS AND DETAILS.
- THE CONTRACTOR IS TO VERIFY THE LOCATION AND THE ELEVATIONS OF ALL EXISTING UTILITIES AT POINTS OF TIE-IN PRIOR TO COMMENCING ANY NEW CONSTRUCTION. SHOULD ANY LOCATION OR ELEVATION DIFFER FROM THAT SHOWN ON THESE PLANS, THE CONTRACTOR SHALL CONTACT THE OWNER'S AGENT.
- CONTRACTOR TO VERIFY AND COORDINATE ALL DIMENSIONS AND SITE LAYOUT WITH ARCHITECTURE'S FINAL SITE PLAN AND FINAL BUILDING DIMENSIONS BEFORE STARTING WORK. REPORT DISCREPANCIES TO OWNER'S AGENT.
- COORDINATION BETWEEN ALL PARTIES IS ESSENTIAL PART OF CONTRACT.
- CONTRACTOR IS RESPONSIBLE FOR PROJECT AND SITE CONDITIONS, AND TO WORK WITH WEATHER CONDITIONS AS THE PROJECT SITE IS LOCATED IN A FLOOD PRONE AREA AND SUBJECT TO FLOODING AND ITS HAZARDS.
- THE CONTRACTOR IS TO VERIFY THE LOCATION, ELEVATION, CONDITION, AND PAVEMENT CROSS-SLOPE OF ALL EXISTING SURFACES AT POINTS OF TIE-IN AND WATCHING, PRIOR TO COMMENCEMENT OF GRADING, PAVING, CURB AND GUTTER, OR OTHER SURFACE CONSTRUCTION. SHOULD EXISTING LOCATIONS, ELEVATIONS, CONDITION, OR PAVEMENT CROSS-SLOPE DIFFER FROM THAT SHOWN ON THESE PLANS, RESULTING IN THE DESIGN INTENT REFLECTED ON THESE PLANS NOT ABLE TO BE CONSTRUCTED, THE CONTRACTOR SHALL NOTIFY THE OWNER'S AGENT IMMEDIATELY FOR DIRECTION ON HOW TO PROCEED PRIOR TO COMMENCEMENT OF CONSTRUCTION. THE CONTRACTOR ACCEPTS RESPONSIBILITY FOR ALL COSTS ASSOCIATED WITH CORRECTIVE ACTION IF THESE PROCEDURES ARE NOT FOLLOWED.
- CONTRACTOR IS RESPONSIBLE TO COORDINATE UTILITY CROSSINGS AT CULVERT CROSSINGS BEFORE STARTING WORK ON CULVERT. COORDINATE WITH OWNER REPRESENTATIVE, VERIFY UTILITY LINES AND/OR CONDUITS ARE IN PLACE BEFORE STARTING CULVERT WORK.
- THIS PROJECT REQUIRES A REGULAR ONGOING MAINTENANCE PROGRAM FOR THE DESIGNED DRAINAGE SYSTEM(S) TO PRESERVE THE DESIGN INTEGRITY AND THE ABILITY TO PERFORM ITS OPERATIONAL INTENT. FAILURE TO PROVIDE MAINTENANCE WILL DEGRADATE THE DRAINAGE SYSTEM(S) PERFORMANCE AND MAY LEAD TO ITS INABILITY TO PERFORM PROPERLY AND/OR CAUSE DAMAGE ELSEWHERE IN THE PROJECT.
- CONTRACTOR TO NOTIFY WOOD/PATEL IF ENGAGED, 72 HOURS PRIOR TO BEGINNING CONSTRUCTION FOR THE PURPOSE OF WITNESSING THE INSTALLATION OF ALL UNDERGROUND MET UTILITIES DIRECTED BY THIS PLAN. CONTRACTOR IS ALSO RESPONSIBLE FOR PROVIDING TO WOOD/PATEL IF ENGAGED, A SET OF REPRODUCIBLE AS-BUILTS OF SAID UTILITIES (5 DAY REVIEW TIME REQUIRED). CONTRACTOR TO NOTIFY WOOD/PATEL IF ENGAGED, 72 HOURS PRIOR TO ANY TESTING OF MET UTILITIES AND TO PROVIDE A COPY OF TEST RESULTS AFTER COMPLETION.
- THOSE SEWER LINES DESIGNED IN PROFILE ARE REQUIRED TO BE ASBUILT AND THE INSTALLATION AND TESTING WITNESSED BY A PROFESSIONAL ENGINEER IN ACCORDANCE WITH ARIZONA ADMINISTRATIVE CODE R18-9-0301 "4.01 GENERAL PERMIT: SEWAGE COLLECTION SYSTEMS". IT IS THE CONTRACTOR'S RESPONSIBILITY TO NOTIFY THE OWNER WHEN THOSE SERVICES ARE READY TO BE WITNESSED.
- THE PUBLIC WATER LINE INSTALLATION AND TESTING MAY BE REQUIRED TO BE WITNESSED BY A PROFESSIONAL ENGINEER IN ACCORDANCE WITH ARIZONA ADMINISTRATIVE CODES R18-4-507 AND 508 "APPROVAL OF CONSTRUCTION" AND "RECORD DRAWINGS", RESPECTIVELY. IT IS THE CONTRACTOR'S RESPONSIBILITY TO NOTIFY THE OWNER WHEN THOSE SERVICES ARE READY TO BE WITNESSED.
- LOWEST FLOOR (LF) REFERS TO EITHER FLOOR/SLAB ELEVATION OR TOP OF BASEMENT SLAB. IF ELEVATIONS ON THE GRADING AND DRAINAGE PLANS FOR RESIDENTIAL UNITS REFLECT SLAB ON GRADE CONDITIONS AND CANNOT BE LOWERED WITHOUT AGENCY APPROVAL IN LOCATIONS WHERE "SPECIAL FLOOD HAZARD AREAS" EXIST. IN NON-FLOOD HAZARD LOCATIONS, TO ENSURE THAT ADEQUATE RESIDENTIAL LOT DRAINAGE CAN BE ACHIEVED, A PROFESSIONAL ENGINEER SHOULD BE CONSULTED IF THE LF FOR THE SLAB IS PROPOSED TO BE LOWERED, OR IF A BASEMENT IS TO BE CONSTRUCTED.



GENERAL NOTES

CITY OF SCOTTSDALE  
GENERAL CONSTRUCTION NOTES  
FOR PUBLIC WORKS CONSTRUCTION

- ALL CONSTRUCTION IN THE PUBLIC RIGHT-OF-WAY OR IN EASEMENTS GRANTED FOR PUBLIC USE MUST CONFORM TO THE LATEST MARICOPA ASSOCIATION OF GOVERNMENTS (MAG) UNIFORM STANDARD SPECIFICATIONS AND UNIFORM STANDARD DETAILS FOR PUBLIC WORKS CONSTRUCTION AS AMENDED BY THE LATEST VERSION OF THE CITY OF SCOTTSDALE (COS) SUPPLEMENTAL STANDARD SPECIFICATIONS AND SUPPLEMENTAL STANDARD DETAILS. IF THERE IS A CONFLICT, THE LATTER SHALL GOVERN.
- THE ENGINEERING DESIGNS ON THESE PLANS ARE ONLY APPROVED BY THE CITY IN SCOPE AND NOT IN DETAIL. IF CONSTRUCTION QUANTITIES ARE SHOWN ON THESE PLANS, THEY ARE NOT VERIFIED BY THE CITY.
- APPROVAL OF PLANS IS VALID FOR SIX (6) MONTHS. IF AN ENCROACHMENT PERMIT FOR THE CONSTRUCTION HAS NOT BEEN ISSUED WITHIN SIX MONTHS, THE PLANS SHALL BE RESUBMITTED TO THE CITY FOR RE-APPROVAL.
- A PUBLIC WORKS INSPECTOR WILL INSPECT ALL WORKS WITHIN THE CITY OF SCOTTSDALE RIGHT-OF-WAY AND IN EASEMENTS. NOTIFY INSPECTION SERVICES 24 HOURS PRIOR TO STARTING OF CONSTRUCTION (TELEPHONE 480-312-5750).
- WHENEVER EXCAVATION IS TO BE DONE, CALL THE "BLUE STAKE CENTER", 263-1100. TWO WORKING DAYS BEFORE EXCAVATION IS TO BEGIN. THE CENTER WILL SEE THAT THE LOCATION OF THE UNDERGROUND UTILITY LINES IS IDENTIFIED FOR THE PROJECT. CALL "COLLECT" IF NECESSARY.
- ENCROACHMENT PERMITS ARE REQUIRED FOR ALL WORK IN PUBLIC RIGHTS-OF-WAY AND EASEMENTS GRANTED FOR PUBLIC PURPOSES. AN ENCROACHMENT PERMIT WILL BE ISSUED BY THE CITY UPON RECEIPT OF PAYMENT OF A BASE FEE PLUS A FEE FOR INSPECTION SERVICES. TO BE PROVIDED BY THE CITY. COPIES OF ALL PERMITS SHALL BE RETAINED ON-SITE AND SHALL BE AVAILABLE FOR INSPECTION AT ALL TIMES. FAILURE TO PRODUCE THE REQUIRED PERMITS WILL RESULT IN IMMEDIATE WORK STOPPAGE UNTIL THE PROPER PERMIT DOCUMENTATION IS OBTAINED.
- ALL EXCAVATION AND GRADING WHICH IS NOT IN THE PUBLIC RIGHTS-OF-WAY OR NOT IN EASEMENTS GRANTED FOR PUBLIC USE MUST CONFORM TO CHAPTER 70, EXCAVATION AND GRADING, OF THE LATEST EDITION OF THE UNIFORM BUILDING CODE PREPARED BY THE INTERNATIONAL CONFERENCE OF BUILDING OFFICIALS. A PERMIT FOR THIS GRADING MUST BE SECURED FROM THE CITY FOR A FEE ESTABLISHED BY THE UNIFORM BUILDING CODE.

UTILITY	UTILITY COMPANY	NAME OF COMPANY REPRESENTATIVE	TELEPHONE NUMBER	DATE SIGNED
ELECTRIC	ARIZONA PUBLIC SERVICE	MAP RECEIVED		4/21/08
TELEPHONE	GUEST COMMUNICATIONS	JAN HOLMES	(480) 758-4588	4/28/08
NATURAL GAS	SOUTHWEST GAS CO. ARIZONA	HOWARD WARREN	(480) 730-3843	4/18/08
CABLE TV	COX COMMUNICATIONS	ARTURO BAYLON	(623) 328-3625	4/21/08
OTHER	N/A	N/A	N/A	
OTHER	N/A	N/A	N/A	

ENGINEER'S CERTIFICATION  
I, Geoffrey G. Brownell, BEING THE PERSON RESPONSIBLE FOR DESIGNING THE FACILITIES NECESSARY TO SERVE THIS DEVELOPMENT, HEREBY CERTIFY THAT ALL OF THE UTILITY COMPANIES LISTED ABOVE, HAVE REVIEWED THIS PROJECT PROPOSAL AND ALL CONFLICTS HAVE BEEN RESOLVED AT THIS POINT. NO CONFLICT FORMS HAVE BEEN OBTAINED FROM EACH UTILITY COMPANY AND ARE INCLUDED IN THIS SUBMITTAL. I ALSO CERTIFY THAT ALL ON-SITE TRANSFORMERS, CABLE BOXES AND ANY OTHER PUBLIC/PRIVATE UTILITY APPURTENANCES ARE PLACED SUCH THAT THEY DO NOT NEGATIVELY IMPACT THE USE OR INTENDED USE OF ANY DEDICATED EASEMENTS OR FACILITIES DEVELOPED WITH THIS PROJECT INCLUDING BUT NOT LIMITED TO: TRANSFORMER STORAGE BASINS, SITE DISTANCE EASEMENTS AND RAO'S OR OTHER OPEN SPACE EASEMENTS.  
Geoffrey G. Brownell  
Signature  
12/12/08  
DATE

RELATED PROJECTS

SCOTTSDALE ROAD PUBLIC IMPROVEMENTS COS#6118-02

STIPULATION CONFORMANCE STATEMENT

THE ENGINEER OF RECORD ON THESE PLANS HAS RECEIVED A COPY OF THE APPROVED STIPULATIONS FOR THIS PROJECT AND HAS DESIGNED THESE PLANS IN CONFORMANCE WITH THE APPROVED STIPULATIONS.

NATURAL OPEN SPACE & LIMITS  
OF CONSTRUCTION PROTECTION PLAN

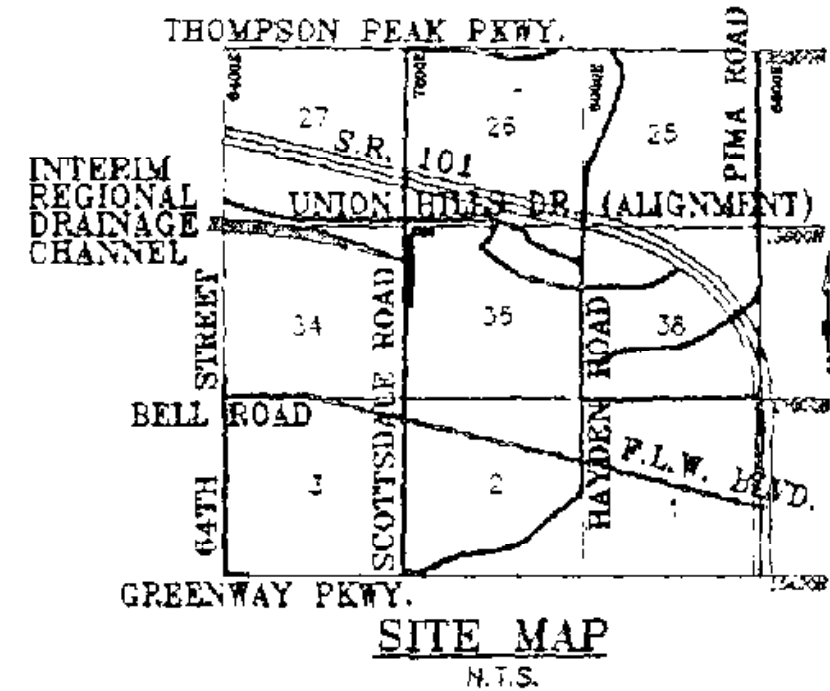
- NO BUILDING, GRADING, OR CONSTRUCTION ACTIVITY SHALL ENCROACH INTO AREAS DESIGNATED AS NOS.
- ALL NOS AND LOC AREAS SHALL BE PROTECTED FROM DAMAGE PRIOR TO AND DURING CONSTRUCTION BY THE FOLLOWING METHODS:  
\*A REGISTERED LAND SURVEYOR SHALL STAKE ALL NOS AND LOC AREAS BASED ON THIS EXHIBIT.  
\*THREE (3) FOOT TALL STEEL REBAR SHALL BE SET ALONG THE NOS AND LOC LINE AND CONNECTED WITH GOLD ROPING BY THE CONTRACTOR PRIOR TO ANY CLEARING OR GRADING.  
\*THE STAKING AND ROPING SHALL BE MAINTAINED INTACT BY THE CONTRACTOR DURING THE DURATION OF THE CONSTRUCTION ACTIVITY.
- THE CONTRACTOR SHALL REMOVE STAKING AND ROPING AFTER RECEIPT OF THE CERTIFICATE OF OCCUPANCY FROM THE CITY OF SCOTTSDALE FOR THE ADJACENT HOME OR CONSTRUCTION WORK.

UTILITY NOTES

- COMPANIES AND THE WORK CONTAINED IN THESE PLANS HAS BEEN APPROVED BY THESE COMPANIES WITHIN THEIR AREA OF INTEREST. THE SIZE AND LOCATIONS, AS SHOWN, OF THE GAS, TELEPHONE AND POWER LINES, AND CONNECTIONS AGREE WITH THE INFORMATION CONTAINED IN THE UTILITY COMPANY RECORDS. WHERE THE WORK TO BE DONE CONFLICTS WITH ANY OF THESE UTILITIES, THE CONFLICTS SHALL BE RESOLVED AS SPECIFIED. CONFLICTS ARISING DURING THE COURSE OF CONSTRUCTION FROM UNFORESEEN CIRCUMSTANCES SHALL BE REPORTED TO THE INTERESTED UTILITY COMPANY AND BE RESOLVED BY THEM AND THE DESIGN ENGINEER AND APPROVED BY C.O.S.
- THE CITY WILL NOT PARTICIPATE IN THE COST OF CONSTRUCTION OR UTILITY RELOCATION.
- IN ACCORDANCE WITH AAC R18-4-119, ALL MATERIALS ADDED AFTER JANUARY 1, 1993 WHICH MAY COME INTO CONTACT WITH DRINKING WATER SHALL CONFORM TO NATIONAL SANITATION FOUNDATION STANDARDS 60 AND 61.

CITY OF SCOTTSDALE			
REVIEW & RECOMMENDED APPROVAL BY:			
PAVING	By <i>[Signature]</i> 2-5-2009	TRAFFIC	N/A
C&D	By <i>[Signature]</i> 2-5-2009	PLANNING	By <i>[Signature]</i> 2/6/2009
M&S	N/A	FREE	By <i>[Signature]</i> 2-5-2009
RET-WALLS	N/A		

*[Signature]* Engineering Coordination Manager (or designee) Date 2-5-2009



LAND OWNER

ARIZONA STATE LAND DEPARTMENT  
1616 WEST ADAMS STREET  
PHOENIX, ARIZONA 85007  
TEL: (602) 542-2648

DEVELOPER

ONE SCOTTSDALE HOLDINGS, LLC  
C/O DMB ASSOCIATES, INC  
7630 EAST DOUBLETREE RANCH ROAD  
SUITE 300  
SCOTTSDALE, ARIZONA 85258  
CONTACT: ART NEHF  
TEL: (480) 387-7000

ENGINEER

WOOD, PATEL & ASSOCIATES INC.  
2051 WEST NORTHERN, SUITE 100  
PHOENIX, ARIZONA 85021  
CONTACT: MR. DARRELL WOOD P.E. R.L.S.  
MR. GEOFF BROWNELL P.E., CFM  
TEL: (602) 335-8500

BENCHMARK

CITY OF SCOTTSDALE BRASS CAP FLUSH  
IN CONCRETE MEDIAN.  
NORTHING 967398.39  
EASTING 697368.18  
ELEVATION = 1609.79 CITY OF  
SCOTTSDALE NAVD 88 DATUM

APN#

215-07-004-A  
215-07-005

NOTE

CONCRETE SHALL BE COLORED "SAN DIEGO BUFF".

ESTIMATED QUANTITIES

CABIN BASKETS 3'X3'X6'	76	EA
RIP-RAP	1,821	CY
HYDROSEED	14,793	SY

THE QUANTITIES AND SITE CONDITIONS DEPICTED IN THESE PLANS ARE FOR INFORMATIONAL PURPOSES ONLY AND ARE SUBJECT TO ERROR AND OMISSION. CONTRACTORS SHALL SATISFY THEMSELVES AS TO ACTUAL QUANTITIES AND SITE CONDITIONS PRIOR TO BIDDING THE WORK FOR THE CONSTRUCTION COVERED BY THESE PLANS.

GRADING QUANTITIES

RAW CUT	20,291	CY
RAW FILL	1,805	CY
NET RAW CUT	18,486	CY

ALL EARTHWORK QUANTITIES ARE IN PLACE QUANTITIES. NO EARTH SHRINKAGE HAS BEEN ESTIMATED.

HAUL ROUTE PERMITS ARE REQUIRED FOR ANY HAUL OPERATION WHICH UTILIZES CITY RIGHT OF WAY WITH A VOLUME EXCEEDING 5,000 C.Y.



INTERIM REGIONAL DRAINAGE CHANNEL

CITY OF SCOTTSDALE, ARIZONA

Q.S.#38-45

1672-08-1

19-ZN-2008

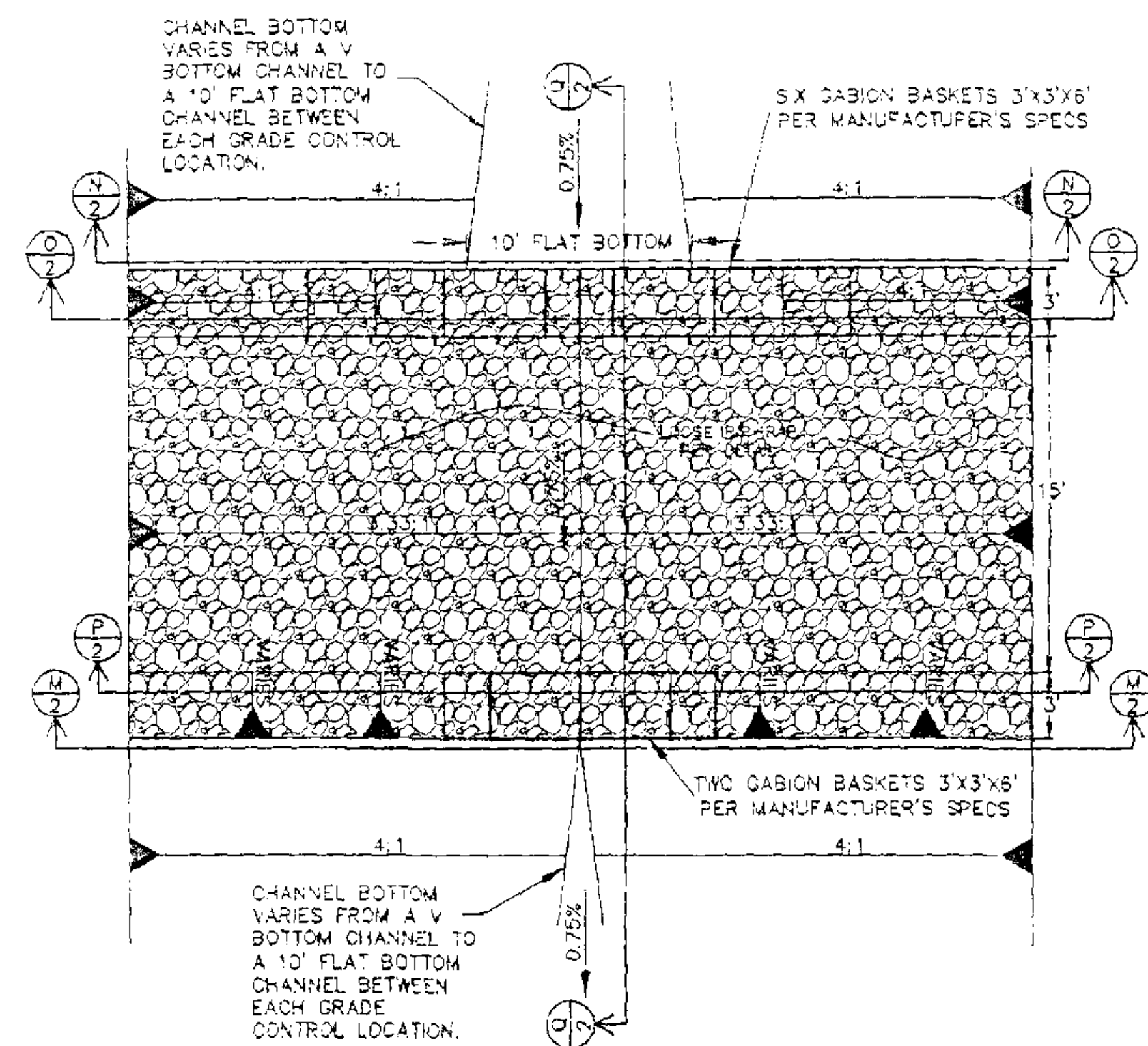
55-SA-2008

DMB  
WOOD/PATEL  
LAND DEVELOPMENT • WATER RESOURCES  
STRUCTURES • TRANSPORTATION/TRAFFIC  
WATER/WASTEWATER • SURVEYING  
CONSTRUCTION MANAGEMENT  
(602) 335-8500  
PHOENIX, MESA, GILBERT, TUCSON

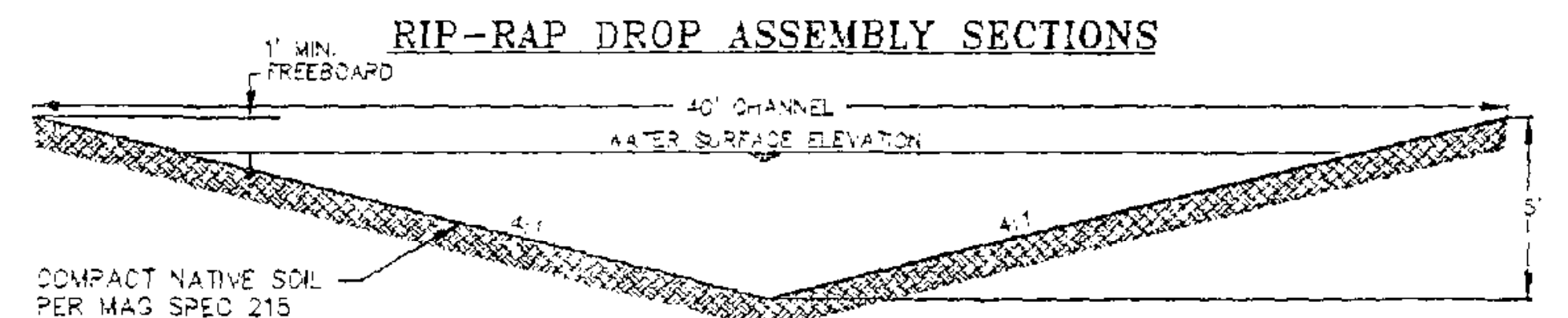


DESIGNED BY  
CHECKED BY  
DATE 11/03/08  
SCALE NO SCALE  
JOB NO 073022  
SHEET 1 of 8

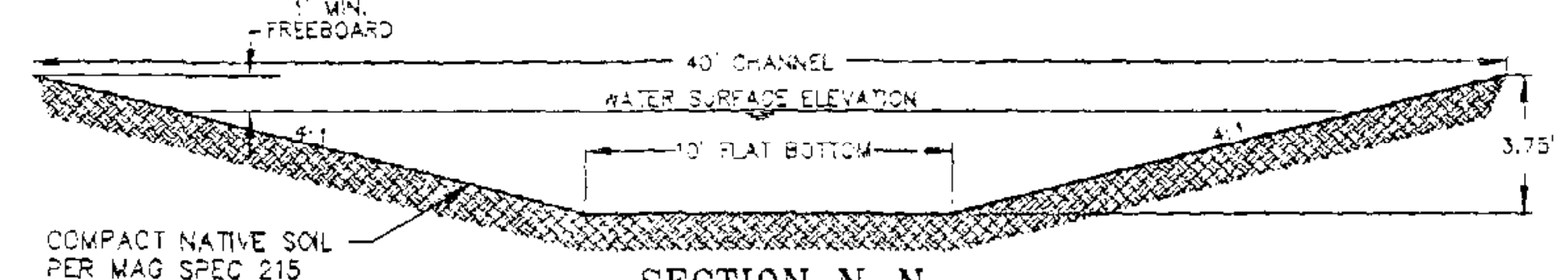




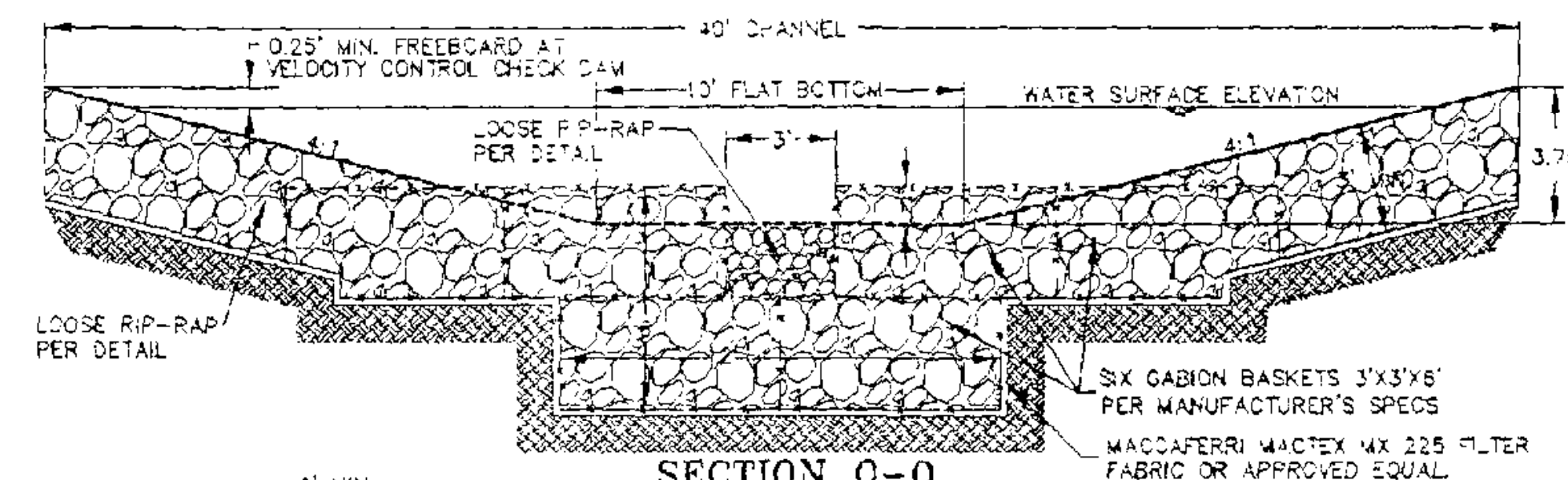
RIP-RAP DROP ASSEMBLY DETAIL



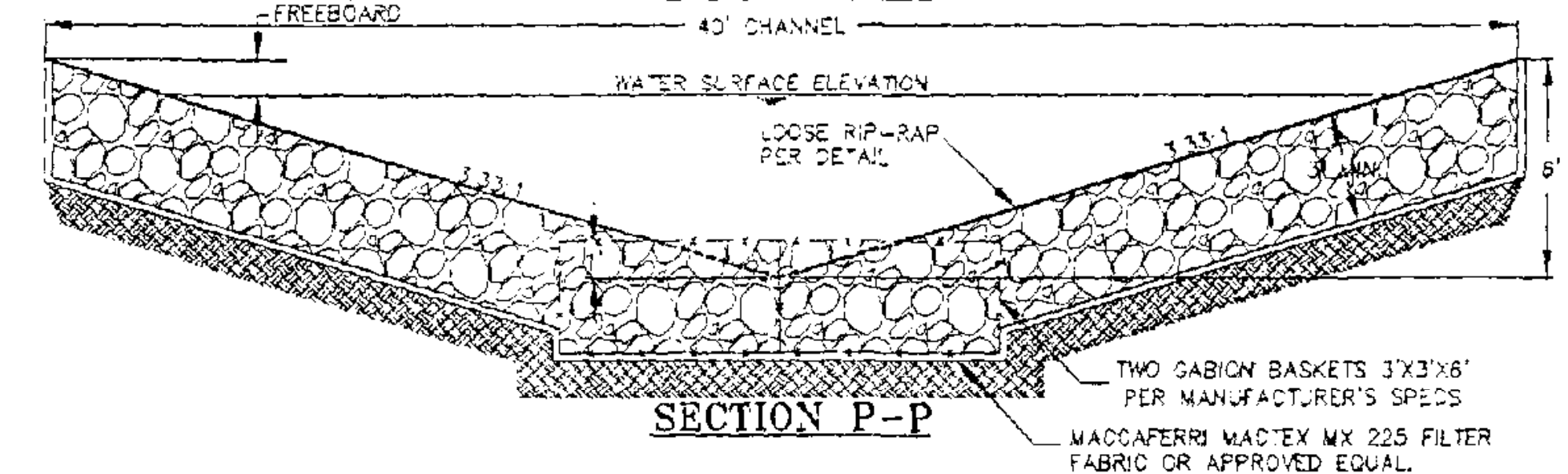
SECTION M-M



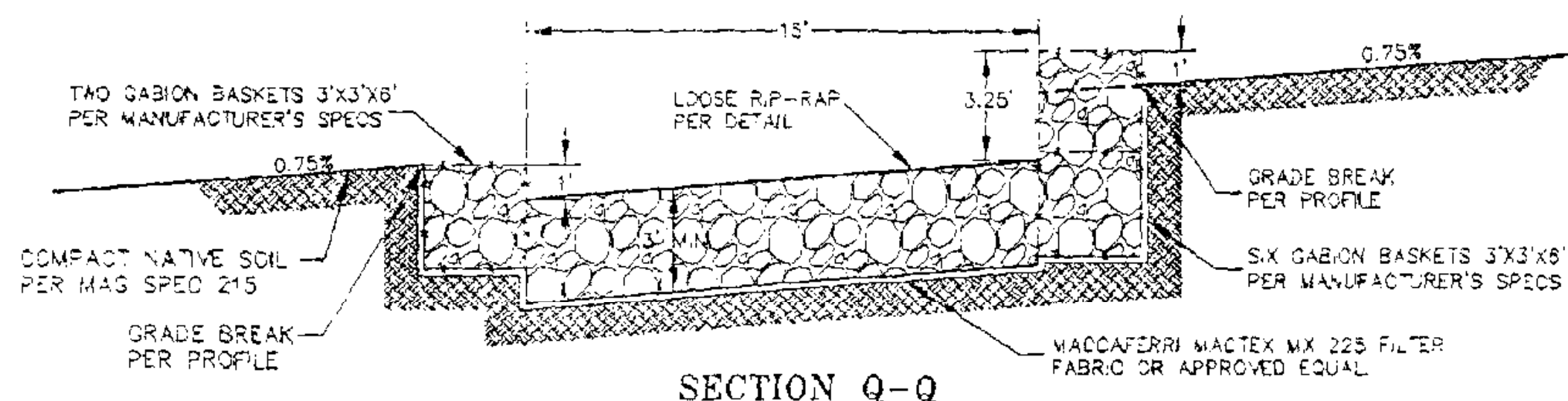
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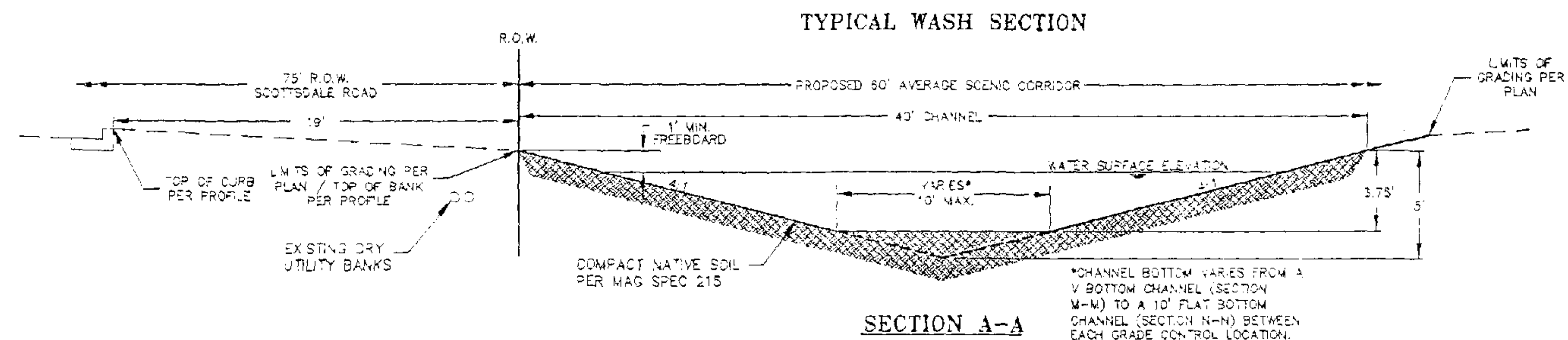
SECTION O-O



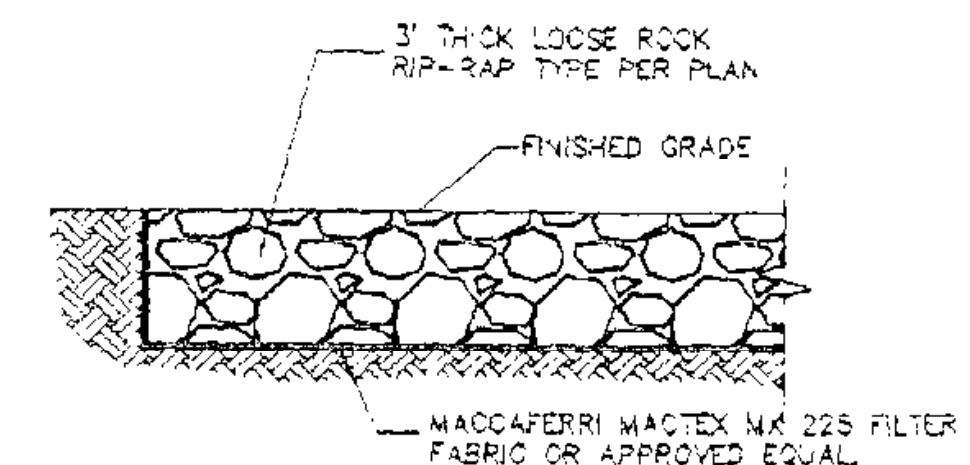
SECTION P-P



SECTION Q-Q



SECTION A-A



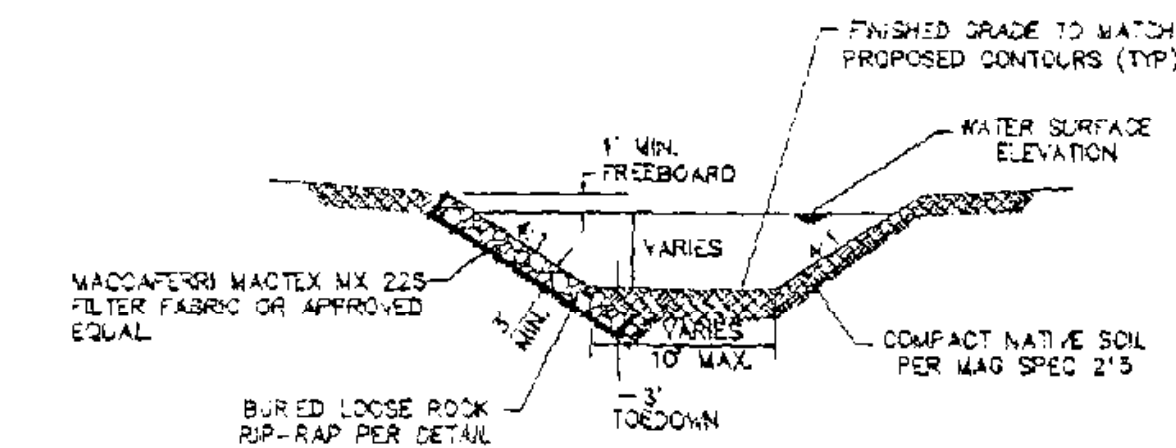
LOOSE ROCK RIP-RAP DETAIL

NOTE: RIP-RAP TO BE ANGULAR STONE OR APPROVED EQUAL

PERCENT FINER BY WEIGHT (G)	SEVE SIZE
15	4"
50	8"
85	14"
100	18"

INSTALL LOOSE RIP-RAP PER M.A.S. SPEC. 220  
\* INSTALL "MACCAFERRI MACTEX MX 225" OR APPROVED EQUAL FILTER FABRIC UNDER ALL LOOSE RIP-RAP

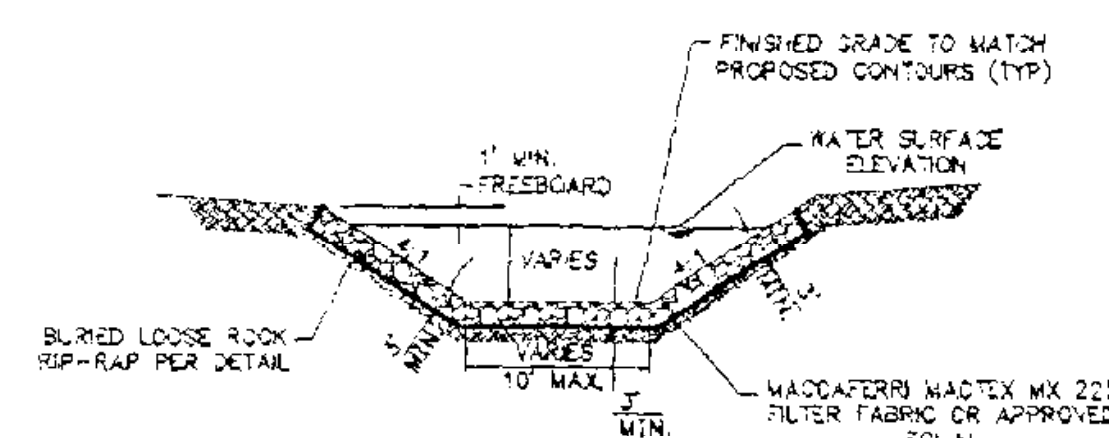
- NOTES:
- IF ADDITIONAL BURIED ROCK PROTECTION IS AVAILABLE, CONTRACTOR MAY INSTALL BURIED ROCK ON SIDE SLOPES IN ADDITION TO REQUIRED MINIMUM LOCATIONS SHOWN ON PLANS, PROVIDED THAT FILTER FABRIC IS INSTALLED BENEATH THE ROCK.
  - ROCK TYPE PER PLAN, GRADATION PER TABLE.



SECTION B-B

BANK EROSION PROTECTION DETAIL

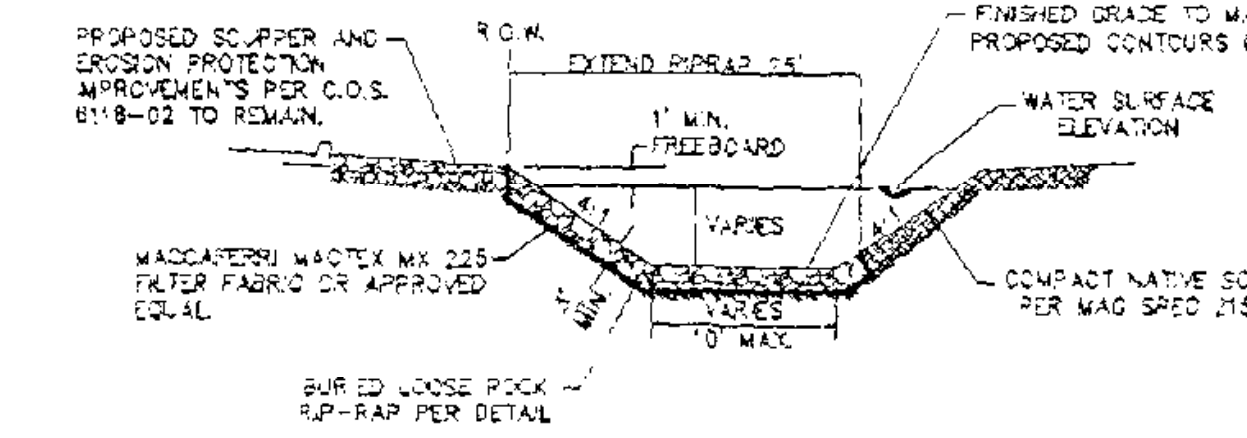
N.T.S.



SECTION C-C

CHANNEL EROSION PROTECTION DETAIL

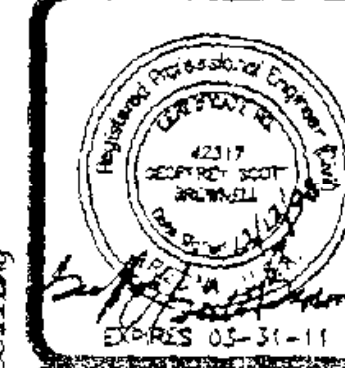
PROPOSED WASH AT BANK PROTECTION ON BOTH SIDES N.T.S.



SECTION D-D

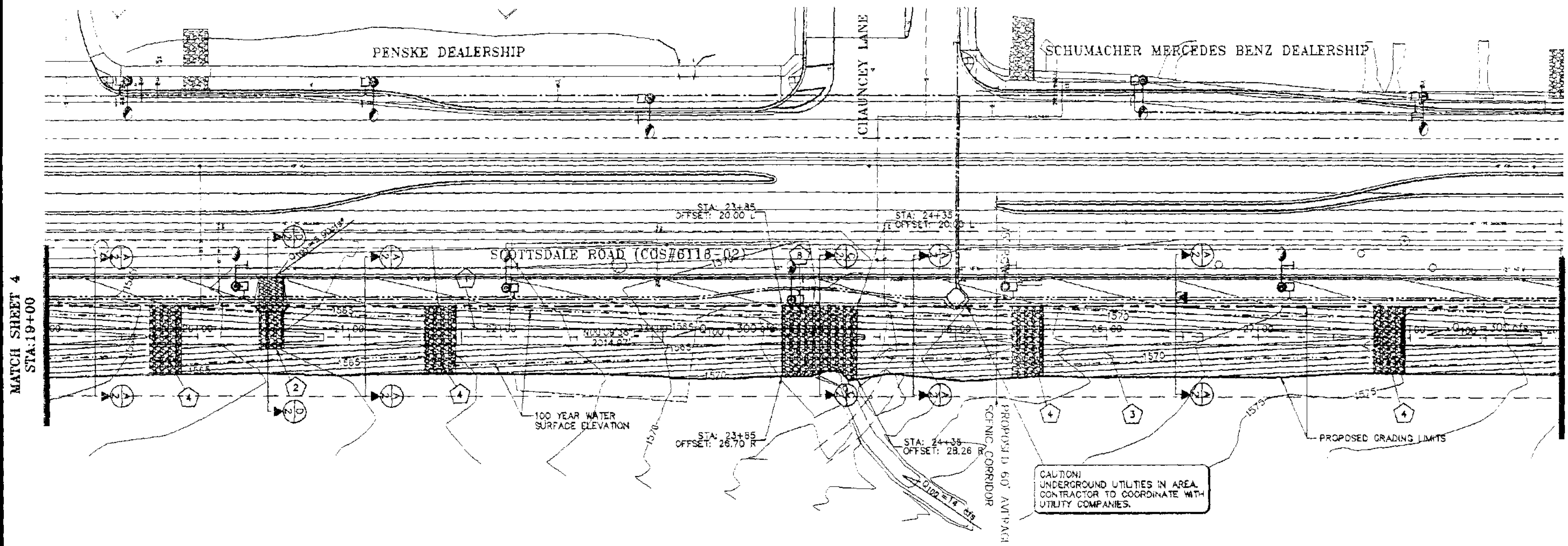
SCUPPER EXTENSION DETAIL

PROPOSED EXTENSION OF EXISTING SCUPPER N.T.S.



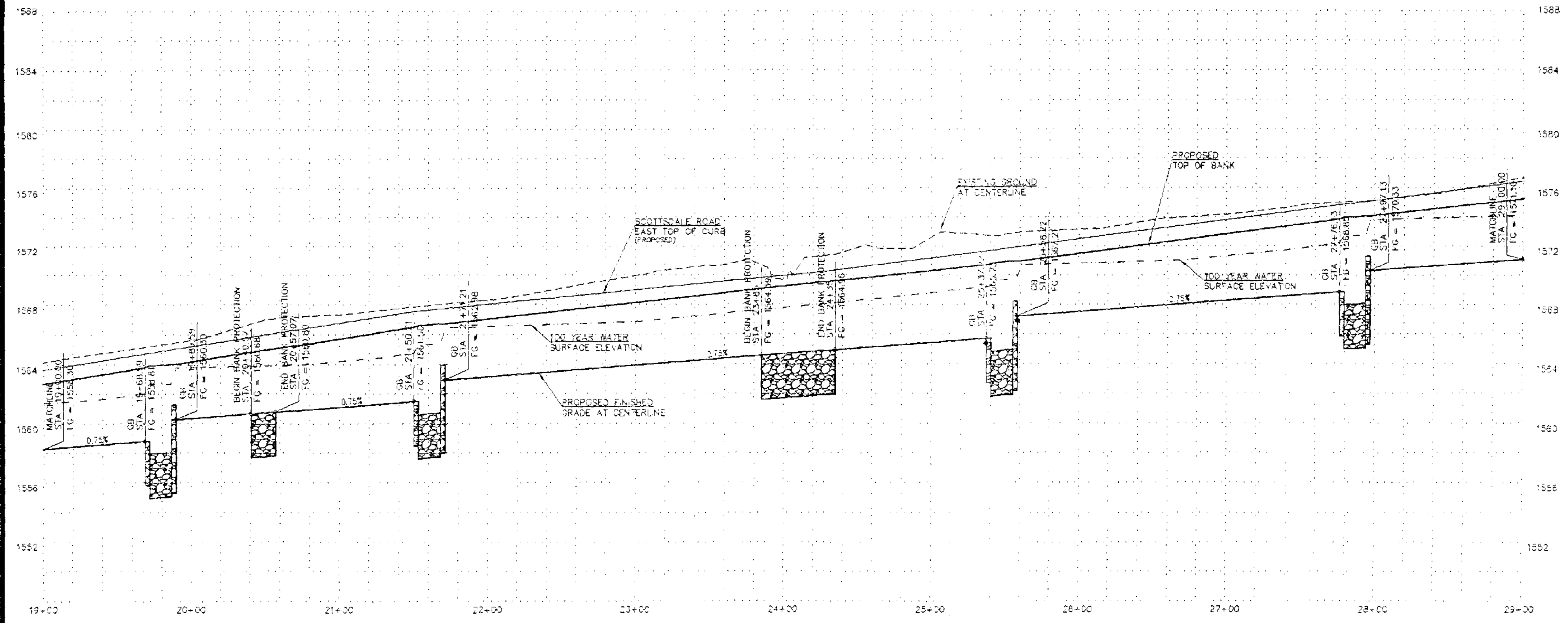






### CHANNEL CONSTRUCTION NOTES

- 1 GRADE CHANNEL PER PLAN AND PROFILE ELEVATION. COMPACT NATIVE SOIL PER M.A.S. SPEC. 215.
  - 2 EXTEND RIP-RAP SPILLWAY 25 FEET EAST PER SCOURPER EXTENSION DETAIL SHEET 2, SECTION D-D.
  - 3 HYDROSEED CHANNEL SOIL PER REVEGETATION PLAN ON SHEET 7.
  - 4 INSTALL RIP-RAP DROP ASSEMBLY PER RIP-RAP DROP ASSEMBLY DETAIL ON SHEET 2.
  - 5 INSTALL CHANNEL EROSION PROTECTION PER CHANNEL EROSION PROTECTION DETAIL SHEET 2, SECTION C-C.
- \*INFORMATION FROM CITY OF SCOTTSDALE FURNISHED FOR CDS#6118-02



DESIGNED	SV
CHECKED	GB
DATE	11/03/08
SCALE	1" = 40'
JOB NO.	073022
SHEET	4 OF 8

**WOOD/PATEL**

LAND DEVELOPMENT • WATER RESOURCES  
STRUCTURES • TRANSPORTATION/TRAFFIC  
PLANNING • CONSTRUCTION MANAGEMENT

(602) 336-8999

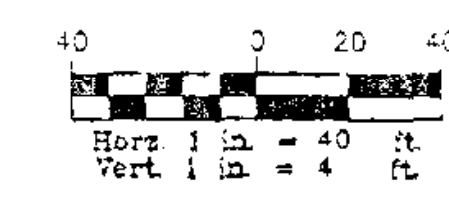
PHOENIX • MESA • GILBERT • TUCSON

## INTERIM REGIONAL DRAINAGE CHANNEL

CITY OF SCOTTSDALE, ARIZONA



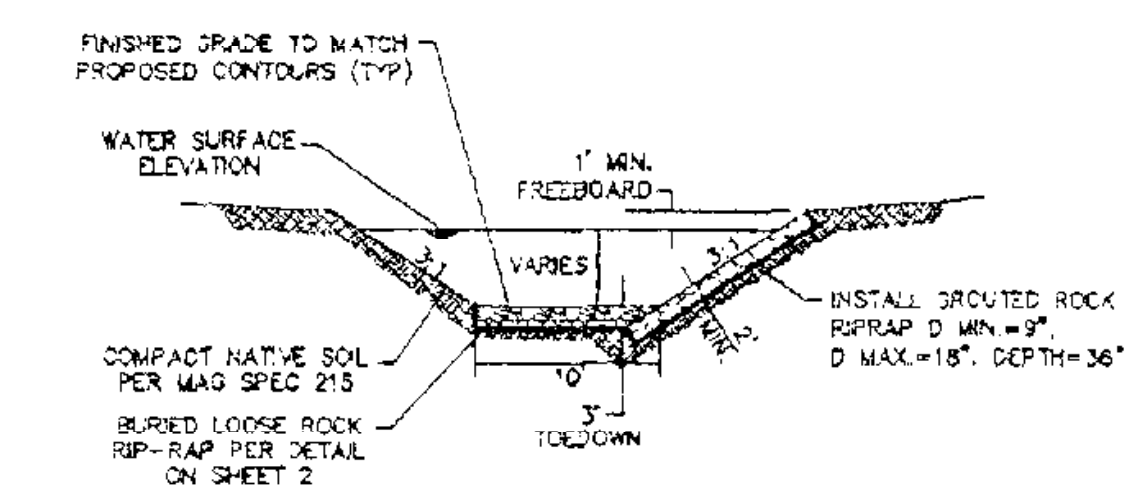




CURVE TABLE				
CURVE	DELTA	RADIUS	ARC TANGENT	CHORD
C3	36°46'55"	80.00	51.36	50.48
C4	53°03'29"	50.00	48.30	44.67
C5	25°31'53"	150.00	66.84	66.23

### CHANNEL CONSTRUCTION NOTES

- 1 GRADE CHANNEL PER PLAN AND PROFILE ELEVATION.  
COMPACT NATIVE SOIL PER W.A.G. SPEC. 215.
- 3 HYDROSEED CHANNEL SOIL PER REVEGETATION PLAN ON  
SHEET 7.
- 7 INSTALL BANK EROSION PROTECTION PER BANK EROSION  
PROTECTION DETAIL SHEET 2, SECTION B-B.
- 19 INSTALL 3'- 8" W x 3" H ARCH CONCRETE CULVERT PER  
A.O.T. STD. DET. B-0110 AND B-0230.
- 20 INSTALL STEEL HANDRAILS PER C.O.S. DET. 2508.  
ALL PAINT SAN DIEGO BUFF.
- 21 REMOVE EXISTING GROUDED RIPRAP IN AREAS OF  
CONFLICT WITH NEW CHANNEL
- 22 INSTALL GROUDED ROCK RIPRAP D MIN.=9", D MAX.=18",  
DEPTH=38". EXPOSE FACE OF ROCK
- 23 INSTALL CHANNEL EROSION PROTECTION PER CHANNEL  
EROSION PROTECTION DETAIL SHEET 6, SECTION G-G.
- 26 SAWCUT CONCRETE SLAB TO NEAT EDGE.  
REMOVE 692 S.Y.

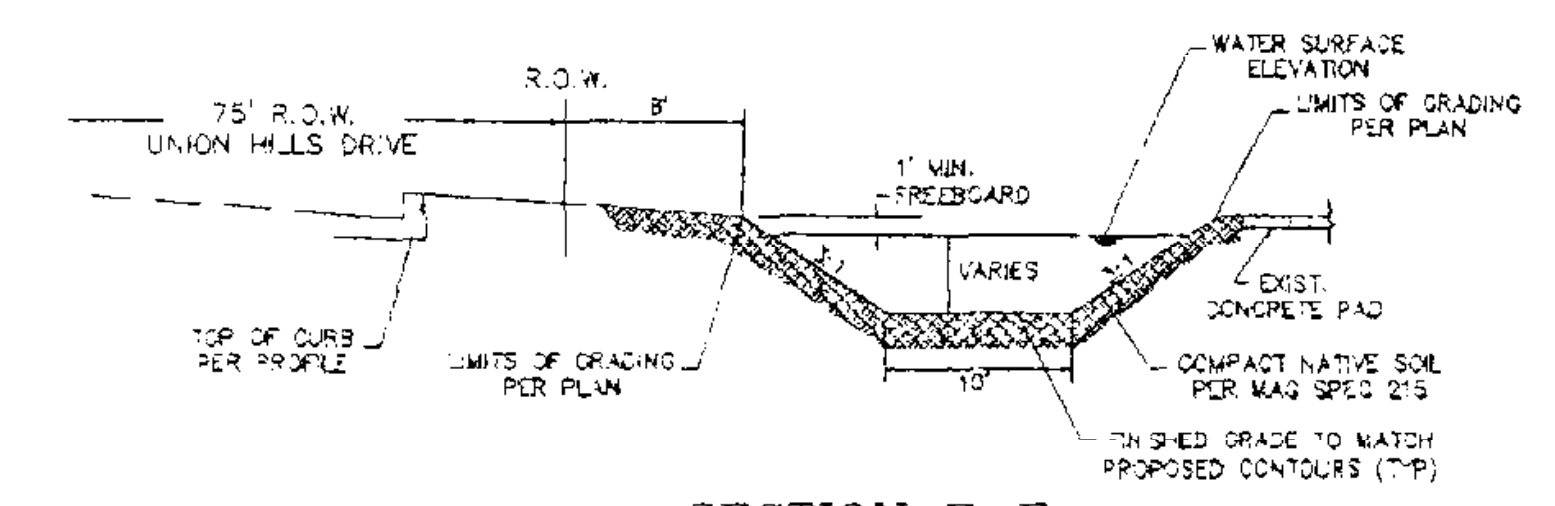


ON SHEET 2

SECTION E-E

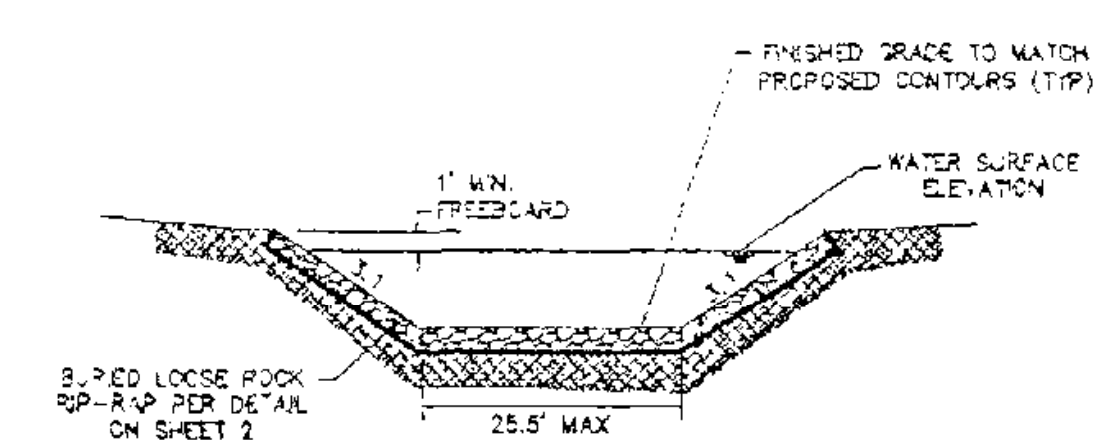
BANK EROSION PROTECTION DETAIL

N.T.S.



PROPOSE

SECTION F-F  
TYPICAL WASH SECTION  
N.T.S.

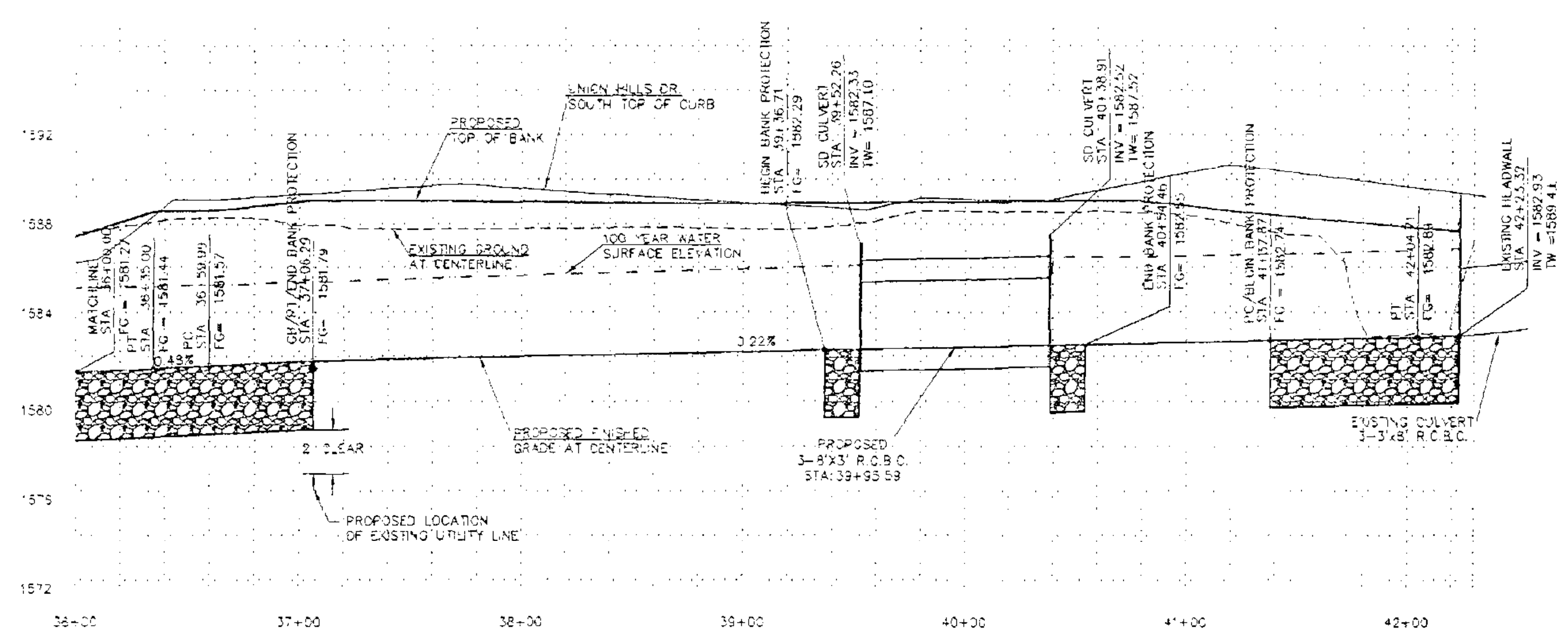


CM SHEET 2 25.5' MAX

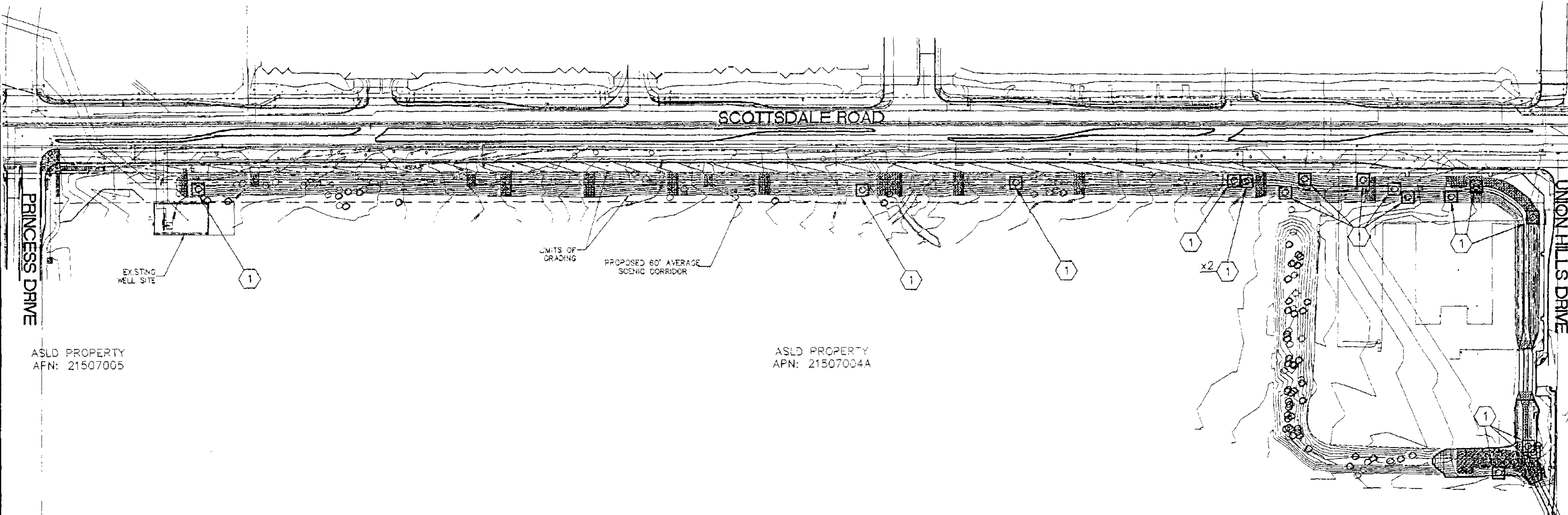
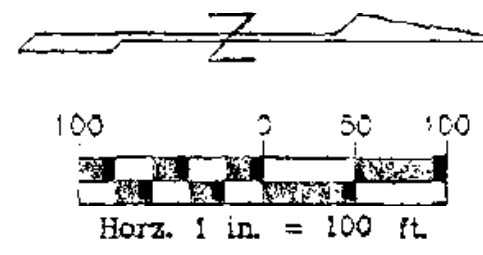
SECTION G-G

BANK EROSION PROTECTION DETAIL

N.T.S.







ASLD PROPERTY  
APN: 21507005

ASLD PROPERTY  
APN: 21507004A

#### CONSTRUCTION NOTE

- ① ONE OF SEVENTEEN PLANTS TO BE REMOVED. REFERENCE NATIVE PLANT INVENTORY PLANS BY DESIERTO VERDE DATED 3/31/08 AND 10/31/08 FOR PLANT INVENTORY TAG NUMBERS AND COLORS.

#### SUMMARY OF INVENTORY—PERFORMED BY DESIERTO VERDE

- NON-SALVAGEABLE (30) — BLUE TAG  
○ SALVAGEABLE (89) — RED TAG

TAKE PRECAUTION AND CARE TO AVOID CONTACT WITH OR DISRUPTION OF TREES TO REMAIN IN PLACE.

#### SALVAGE PLANTS

- TO BE REMOVED (17)  
○ TO REMAIN IN PLACE (72)

CALL THE MOVING DIALS  
BEFORE YOU GO  
602-283-1100  
1-800-STAKE-IT  
LAWRENCE, KANSAS 66044

WOOD/PATEL  
LAND DEVELOPMENT • WATER RESOURCES  
STRUCTURES • TRANSPORTATION/TRAFFIC  
PLANNING • CONSTRUCTION MANAGEMENT  
(602) 335-9500  
PHOENIX • MESA • GILBERT • TUCSON

**INTERIM REGIONAL  
DRAINAGE CHANNEL**  
CITY OF SCOTTSDALE, ARIZONA

19-ZN-2008 1672-08-1 55-SA-2008  
Q.S.#38-45

DESIGNED	GV
CHECKED	GB
DATE	11/03/08
SCALE	1" = 40'
JOB NO.	073022
SHEET	8 of 8



***Appendix N***

**As- Built for Interim Drainage Channel Report**

**FINAL DRAINAGE REPORT  
FOR  
INTERIM REGIONAL DRAINAGE CHANNEL**

October 1, 2008

WP# 073022

*Prepared for:*           **One Scottsdale Holdings, LLC  
c/o DMB Associates, Inc.  
7600 East Doubletree Ranch Road  
Suite 300  
Scottsdale, Arizona 85258  
Phone: (480) 367-7000  
Fax: (480) 367-7558**

*Submitted to:*           **City of Scottsdale  
7447 East Indian School Road  
Suite 300  
Scottsdale, Arizona 85251  
Phone: (480) 312-2352  
Fax: (480) 312-2672**

*Prepared by:*           **Wood, Patel & Associates, Inc.  
2051 West Northern Avenue  
Suite 100  
Phoenix, Arizona 85021  
Phone: (602) 335-8500  
Fax: (602) 335-8580  
Website: [www.woodpatel.com](http://www.woodpatel.com)**



*expires 3/31/11*

## TABLE OF CONTENTS

1.0	EXECUTIVE SUMMARY .....	1
2.0	GENERAL BACKGROUND .....	2
3.0	DESIGN CONCEPT .....	3
4.0	HYDROLOGY .....	4
5.0	HYDRAULICS .....	6
6.0	MAINTENANCE.....	8
7.0	REFERENCES.....	9

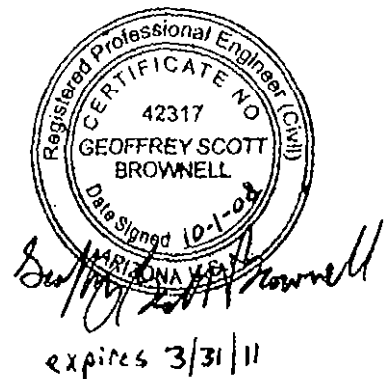
## APPENDICES

Appendix A	Hydrology
Appendix B	Hydraulic Calculations
Appendix C	Erosion Protection

## EXHIBITS

Exhibit 1	Vicinity Map
Exhibit 2	FEMA Map
Exhibit 3	Conceptual Grading and Drainage Plan
Exhibit 4	HEC-RAS Schematic

km  
Y:\WP\Reports\Hydrology\073022 Interim Regional Drainage Channel Final Drainage Report.doc



## 1.0 EXECUTIVE SUMMARY

- The Interim Regional Drainage Channel is a proposed 3,200-linear foot open channel along Union Hills Road and Scottsdale Road within the City of Scottsdale.
- The channel is intended to provide increased flood protection in a known floodplain, as well as protection for future improvements of Scottsdale Road.
- The Interim Regional Drainage Channel completes the downstream reach of City of Scottsdale initiated regional drainage improvements.
- The channel will convey flow from an existing culvert under Union Hills Drive. It will run east adjacent to Union Hills Drive, turn south and flow adjacent to the Scottsdale Road right-of-way within a future scenic corridor easement to a proposed box culvert under Scottsdale Road. Storm water will ultimately be retained in the Reach 11 Recreation Area of the Central Arizona Project canal.
- The maximum channel width is proposed to be 40 feet.
- The box culvert conveying flows under Scottsdale Road is currently under design by the City of Scottsdale.
- Grade control structures are incorporated in the design to maintain the 100-year flow velocities in the channel within permissible velocities appropriate for an unlined native channel.
- Riprap erosion protection will be incorporated into each grade control structure, as well as at horizontal turns in the channel alignment and inlet/outlet of culverts.
- The design flow for the Interim Regional Drainage Channel is 300 cubic feet per second.

## 2.0 GENERAL BACKGROUND

The Interim Regional Drainage Channel presents the opportunity for implementation of flood protection in the City of Scottsdale. It completes the downstream reach of drainage improvements initiated by the City of Scottsdale. In addition, it provides protection to proposed improvements to Scottsdale Road. It will be located within a scenic corridor easement and add aesthetic open space along a major arterial roadway. The solution is anticipated to prevent redundancies in the drainage system that could occur if development occurred in a disjointed manner.

The proposed Interim Regional Drainage Channel is located within the northwest quarter of Section 35, Township 4 North, Range 4 East, of the Gila and Salt River Base and Meridian. More specifically, the channel is located along the east side of the Scottsdale Road right-of-way between Union Hills Drive and Princess Drive. A map of the area can be seen on Exhibit 1 -- *Vicinity Map*.

The project site lies in a Federal Emergency Management Agency (FEMA) designated Zone "AO" Special Flood Hazard Area, with depths of one foot and velocities of three feet per second, per the Flood Insurance Rate Map (FIRM) panel number 04013C1245H, effective date September 30, 2005 (see Exhibit 2 -- *FEMA Map*).

Currently, drainage from the north passes south under the Loop 101 Freeway through existing box culverts. Flow is conveyed past Union Hills Drive via existing drainage improvements, then flows in an existing wash in a westerly and southerly direction across the Arizona State Land Department (ASLD) property. There is current planning for concrete box culverts that would convey this flow west under Scottsdale Road. An existing channel running west on the north side of Princess Drive would not be disturbed by the Interim Regional Drainage Channel and would continue to operate independently.

### 3.0 DESIGN CONCEPT

The alignment for the Interim Regional Drainage Channel was chosen with input from the Arizona State Land Department (ASLD) and the City of Scottsdale. The proposed alignment maintains connection with the existing drainage improvements south of Union Hills Drive. The proposed channel begins at the outlet of an existing culvert on the south side of Union Hills Drive. The channel will flow east adjacent to Union Hills Drive for approximately 550 feet where it turns south and flows for approximately 2,650 feet within a future scenic corridor easement adjacent to the Scottsdale Road right-of-way. The planned access to the ASLD parcel is a driveway off Union Hills Drive. The proposed channel will be conveyed through three (3) 3-foot by 8-foot concrete box culverts at the proposed driveway location. The proposed regional channel ultimately outfalls into proposed culverts that are currently under design by Dibble & Associates, Inc. The storm water then flows west under Scottsdale Road and into the Central Arizona Project Reach 11 Recreation Area retention. The proposed channel alignment is shown on Exhibit 3 -- *Conceptual Grading and Drainage Plan*.

The Interim Regional Drainage Channel is proposed to be an unlined earthen channel. Grade control structures are incorporated into the vertical design of the channel in order to maintain the 100-year flow velocities within appropriate ranges. A variable bottom width is employed in the channel in order to maintain a constant channel slope adjacent to a variable sloped roadway. A 10-foot wide bottom occurs at the upstream end of each grade control structure. The drop is created by extending the sideslopes down to make a triangular channel at the downstream end of the structure. The channel transitions back to the flat bottom at the upstream end of the next grade control structure.

Erosion protection was incorporated into the channel design. Riprap erosion protection was integrated as part of each grade control structure. This protection will be of sufficient length to include the hydraulic jump associated with each structure. Riprap erosion protection is also proposed at the bends in the channel alignment to reduce the possibility of breakout and lateral migration. Revegetation and hydrosced will be used along the length of the channel for aesthetic purposes and increased erosion control.

Typical cross sections for the Interim Regional Drainage Channel were selected to provide adequate conveyance for the 100-year storm. A minimum of one foot of freeboard is provided within the channel, and the top width of the channel, including freeboard, is limited to 40 feet. The channel side slopes are limited to 4:1 along Scottsdale Road, and 3:1 along Union Hills Drive.



#### 4.0 HYDROLOGY

The 100-year design flow for the Interim Regional Drainage Channel is 300 cfs. This is based on a 100-year, 6-hour design storm utilizing HEC-1 hydrology modeling software (Ref. 3). Results of this model are included in Appendix A -- *Hydrology*. These results are compared to those published in *Drainage Study Core North/Core South* by Robert L. Ward (Ref. 4).

The included HEC-1 model is an expansion of the hydrology model completed for the *One Scottsdale Master Drainage Plan*, by Wood, Patel & Associates, Inc. (Ref. 5). The One Scottsdale development lies upstream of the project site to the north of the Loop 101 Freeway. The model was revised to expand to the south to include the proposed improvements. Flow at the Loop 101 Freeway culverts (identifier 33E.1) is now routed through the Interim Regional Drainage Channel (identifier R33E.1). The runoff from the adjacent State Land parcel (identifier ASLD) joins at the outfall culvert under Scottsdale Road near Princess Road (identifier CPPRIN). This downstream flow of 300 cfs was used as the design flow for the entire channel. The ASLD sub basin was determined to be a 35-acre area with a curve number of 77, chosen to represent desert shrub with poor hydrologic conditions. The other revision to the *One Scottsdale Master Drainage Plan* hydrology model is modification to the storage routing to account for the changes in storm water storage requirements due to channel improvements proposed here. This resulted in increased runoff under the Loop 101 Freeway.

These results are compared to existing conditions and proposed conditions models published in *Core North/Core South* (Ref. 4). Both of these models also use a curve number of 77 for the State Land sub basin. The flows published in that model are lower than those proposed here, which is considered conservative. In a separate hydraulics section of that report, the culvert design flows for the Loop 101 Freeway culverts are listed as 300 cfs, including large offsite impacts. The report proposes that offsite impacts would not affect these culverts, and revises the design flow to 65 cfs. This further establishes that the design flow for the Interim Regional Drainage Channel of 300 cfs is conservative.

	Interim Regional Drainage Channel		Core North/South Existing Conditions		Core North/South Plan 1 Proposed Conditions	
	HEC-1 CP	Q100 (cfs)	HEC-1 CP	Q100 (cfs)	HEC-1 CP	Q100 (cfs)
Loop 101 Culvert	33E.1	256	SCNA1	129	N61.3	173
State Land	ASLD	90	3B	98	N63	98
Proposed Channel	R22E.1	252	3B.1	125	N63.1	169
Outfall Culvert	CPPRIN	300	3B.2	178	N63.2	256

An existing wash traverses the ASLD parcel in a southwesterly direction. This wash is a Section 404 jurisdictional wash. In the existing conditions, it is blocked on the upstream side from receiving flow by the existing retention basin near Station 36+00. It collects only local flow and discharges into the proposed channel near Station 24+00. This local flow is estimated as 14 cfs by a Rational Method calculation which is included in Appendix A -- *Hydrology*.

## 5.0 HYDRAULICS

Final design and analysis of the Interim Regional Drainage Channel was completed using HEC-RAS (Ref. 6) hydraulic modeling software. Grade control structures are specified to manage the longitudinal slope and maintain velocity within the design range. The results of the hydraulic model are the basis for analysis of erosion potential. Grade control structures are used in lieu of bank erosion protection along the entire channel reach.

Cross sections were cut upstream, downstream, and at each grade control structure, horizontal channel bends, changes in channel lining, and along the channel length. Roughness coefficients for the channel were selected to reflect graded earth with expected landscaping and vegetation. The downstream boundary condition was set as the calculated headwater required for the proposed culvert, currently under design by Dibble & Associates, Inc. This culvert is assumed to be a reinforced concrete box culvert with two (2) 8-foot wide by 3-foot tall barrels. Culvert headwater calculations were completed with *Bentley CulvertMaster* (Ref. 7). The culvert inlet loss coefficient was set as 0.7 to reflect a drop inlet with possible skew. The upstream boundary condition was set as critical depth to reflect flow exiting the existing culverts under Union Hills Drive. Hydraulic models of the 2-year and 10-year storms were also run to analyze hydraulic conditions. Flows for these storms were approximated as 10% and 35% of the 100-year discharge, respectively, per the *Drainage Design Manual* (Ref. 8). Input hydraulic data and results are located in Appendix B – *Hydraulic Calculations*.

Velocities within the channel for the 100-year storm were found to range from 3.5 to 7 feet per second. Supercritical flow was not found to occur. The highest velocities occur as the flow exits the proposed stilling basins and slows as it approaches normal depth through the length of the open channel. The lowest velocities occur within the proposed stilling basins and where under the influence of the backwater caused by rock check dams. Provided freeboard ranges from 0.25 feet to 3 feet within the 40-foot channel corridor. Less than one foot of freeboard occurs where flow is under the influence of backwater from the rock check dams. At each location with less than one foot of provided freeboard, additional freeboard will be provided outside of the easement in the grading to existing. In order to mitigate any flooding hazard low amounts of provided freeboard might create, it is reminded that according to City of Scottsdale requirements for development within FEMA flood Zone "AO" (1 foot, 3 feet per second), all adjacent buildings must have a lowest floor a minimum of 12 inches above the water surface elevation. ✓

Flow velocities for the 10-year storm range from 2 to 5.6 feet per second. This is within the recommended range to prevent sedimentation aggradation, as well as channel erosion. At least 1.3 feet of freeboard is provided in all locations. The flow velocities for the 2-year storm range from 1 to 4.5 feet per second. At least 2 feet of freeboard is provided in all locations.

Erosion potential was analyzed using the results of the hydraulic modeling. These analyses are included in Appendix C – *Erosion Protection*. An ADWR Level 1 scour analysis found the estimated scour depth to be 3 feet. A minimum erosion protection thickness of 3 feet is therefore specified. Bend scour around the outside bank of the horizontal turns in the channel was also analyzed. A minimum length of bank protection downstream of the bends is specified as 70 feet. Riprap was selected for use as erosion protection. A fiftieth percentile diameter of 9 inches was chosen for these locations. Gradation per the *Drainage Design Manual* (Ref. 1) is specified.

Scour erosion is not expected on the upstream side of the check dams. The purpose of the check dams is to slow the rate of flow. This would more likely result in aggradation. The flow velocity for each of these check dams in the 100-year storm is approximately 3.6 feet per second, with an energy grade slope of approximately 0.26%. Since the channel slope is 0.75%, this shows that the check dams effectively produce a backwater effect and scour is not anticipated. Additionally, these dams are constructed of rock-filled gabion baskets, and are keyed into the sides and bottom of the channel to reduce the possibility of overturning. The flow will become supercritical as it pours over the dams; so erosion protection is proposed on the downstream side. For a graphical and tabular representation, please see the HEC-RAS profiles and results included in Appendix B – *Hydraulics*. ✓

## 6.0 MAINTENANCE

Ongoing maintenance of the designed or recommended drainage systems is required to preserve the design integrity and purpose of the drainage system. Failure to provide maintenance can prevent the drainage system from performing to its intended design purpose and can result in reduced performance. Maintenance within the public right-of-way is the responsibility of the governing municipality. However, it is the responsibility of private developers, homeowners associations, etc. for facilities on private property within drainage easements, and includes private streets. A regular maintenance program is required to have drainage systems perform to the level of protection or service as presented in this report and related construction documents and specifications.

## 7.0 REFERENCES

1. *Drainage Design Manual for Maricopa County, Arizona, Hydraulics* (Draft), Flood Control District of Maricopa County, September 2003.
2. *Design Standards & Policies Manual, Chapter 4 – Grading and Drainage*, City of Scottsdale, August 2007.
3. *Flood Hydrograph Package (HEC-1), Version 4.1*, U.S. Army Corps of Engineers, June 1998.
4. *Drainage Study Core North/Core South Scottsdale, Arizona*, Robert L. Ward, Consulting Engineer, September 25, 2001.
5. *One Scottsdale Master Drainage Plan*, Wood, Patel & Associates, Inc., September 26, 2006.
6. *River Analysis System (HEC-RAS), Version 3.1.3*, U.S. Army Corps of Engineers, May 2005.
7. *Bentley CulvertMaster, Version 3.1, Service Pack 1*, Bentley Systems, Inc., copyright 2005.
8. *Drainage Design Manual for Maricopa County, Arizona, Hydrology* (Draft), Flood Control District of Maricopa County, September 2003.



## APPENDIX A

### Hydrology

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1996 *
* VERSION 4.1 *
* RUN DATE: 04FEB08 TIME: 15 12.09 *
*****

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```

*****
* U. S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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X X XXXX(X) XXXX X
X X X X X X
X X X X X X
XXXXXX XXXX X XXXXX X
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X X X X X X
X X XXXXXXX XXXXX XXX

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DR, AND HEC1KN

THE DEFINITIONS OF VARIABLES -RTIME- AND -RTION- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGE CALCULATION, DSS WRITE SLICE FREQUENCY, DSS ROAD TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE GREEN AND AMPT INFILTRATION, KINEMATIC WAVE, NEW FINITE DIFFERENCE ALGORITHM.

1

HEC-1 INPUT

PAGE 1

LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	ONE SCOTSDALE (STACKED 40S) POST DEVELOPMENT CONDITION 100-YR 6-HR STORM									
2	ID	OFFSITE HYDROLOGY & ONSITE HYDROLOGY FOR AREA GOVERNED BY PRE-POST CRITERIA									
3	ID	OPTION A - ASLD CHANNEL									
4	ID	FILE: 100YR-PICR.DAT									
5	ID	OPTION B - 34.1 ACRES OF ASLD PARCEL									
6	ID										
7	ID	BASED ON MODELS PREPARED BY: ROBERT L. WARD, P.E., CONSULTING ENGINEER									
8	ID										
9	ID	PRM-100 G1									
10	ID	C1 G1 (CENTER DRIVE PROJECT)									
11	ID	SAURX100 G1 (STACKED 10S EXISTING CONDITION)									
12	ID										
13	ID	ALL CURVE NUMBERS ADJUSTED TO 6-HOUR VALUES ON AUGUST 13, 2003									
14	ID	100 YEAR, 6-HOUR HYPOTHETICAL STORM									
15	ID										
16	ID	AREAL RAINFALL REDUCTION IS BASED ON A 14 SQUARE MILE STORM									
17	ID										
18	IT	5	300								
19	IO	5									
20											
21		BEGIN GRAYBARK - VILLAGE 1 DRAINAGE PLAN									
22		PREPARED BY: GILBERTSON ASSOCIATES, INC. HEC-1 FILE: UDIPLAN.DAT									
23		THIS GILBERTSON MODEL USES DSS UNIT HYDROGRAPH METHODOLOGY									
24		THE ORIGINAL MODEL WAS BASED ON A 1-MINUTE COMPUTATION INTERVAL.									
25											
26	KK	1A1									
27	LM	EXCESS RUNOFF FROM SUBAREA 1A1									
28	RM	RAINFALL REGION 3									
29	RA	0180									
30	PH	14	0.76	1.5	2.54	3.61	2.59	3.31			
31	LS	77	16								
32	UD	0.06									
33	KK	DETAL									
34	AM	DETENTION BASIN FOR SUBAREA 1A1									
35	RS	1	STOR	0							
36	SV	0	1.76								
37	SO	0	20								
38	SE	0	1.0								
39	SV	1.0	15	2.8	1.5						
40	KK	RA1-C4									
41	RM	ROUTE OUTFLOW FROM DETAL TO CPIC4									
42	PH	TRIANGULAR CHANNEL PER PLANS (110'-E-94 AND 190'-E-95)									
43	RM	SIDE SLOPE = 1:1 (H:V)									
44	RM	MAX DEPTH = 1.32 FT									
45	RS	1	FLOW	-1							
46	RC	0.025	0.025	0.025	670	0.0177					
47	KK	0	0.5	1.0	5.04	5.05	9.1	9.5	10		
48	RY	1.37	1.36	1.35	0	0	1.35	1.36	1.37		

PAGE 2

1

HEC-1 INPUT

LINE	ID	1	2	3	4	5	6	7	8	9	10
43	KK	1C4									
44	RM	EXCESS RUNOFF FROM SUBAREA 1C4									
45	RA	005									
46	LS	77	5								
47	UD	08									
48	KK	CPIC4									
49	RM	COMBINE HYDROGRAPHS FROM RA1-C4 AND 1C4									
50	HC	2									

51 KK RC4-C3  
 52 KM ROUTE OUTFLOW FROM CPIC3 TO CPIC17  
 53 KN TRIANGULAR CHANNEL PER PLANS 11182-E-94 AND 190-E-95  
 54 KN SIDE SLOPE = 3:1 (H:V)  
 55 KN MAX DEPTH = 1.5 FT.  
 56 RS 1 FLOW -1  
 57 RC 0.025 0.025 0.025 400 0.020  
 58 RX 0 0.5 1.0 4.49 5.5 9 9.5 10  
 59 RY 1.52 1.51 1.5 0 0 1.5 1.51 1.52  
 60 KK 1DA3  
 61 KM EXCESS RUNOFF FROM SUBAREA 1DA3  
 62 RA 0148  
 63 LS 77 31  
 64 UD .06  
 65 KK DE1DA3  
 66 KM DETENTION FOR SUBAREA 1DA3  
 67 KN OUTLET IS A 18" RGRUP WITH AN 8" ORIFICE PLATE PER PLANS 1905-E-95  
 68 RS 1 STOR 0  
 69 SV 0 1.27  
 70 SQ 0 4  
 71 SE 0 3.0  
 72 ST 3.0 15 2.8 1.5

73 KK 1DA4  
 74 KM EXCESS RUNOFF FROM SUBAREA 1DA4  
 75 RA 01  
 76 LS 77 16  
 77 UD .05

78 KK CP1DA4  
 79 KM COMBINE HYDROGRAPHS FROM 1DA4 AND DE1DA3  
 80 RC 2

81 KK DE1DA4  
 82 KM DETENTION FOR SUBAREA 1DA4  
 83 KN OUTLET IS A 18" PVC WITH AN 8" ORIFICE PLATE PER PLANS 1905-E-95  
 84 RS 1 STOR 0  
 85 SV 0 0.76  
 86 SQ 0 4  
 87 SE 0 3.0  
 88 ST 3.0 15 2.8 1.5  
 REC-1 INPUT

PAGE 3

LINE ID 1 2 3 4 5 6 7 8 9 10

89 KK 1DA5  
 90 KM EXCESS RUNOFF FROM SUBAREA 1DA5  
 91 RA 001  
 92 LS 77 5  
 93 UD .08  
 94 KK CP1C31  
 95 KM COMBINE HYDROGRAPHS FROM RC4-C3, 1DA5 AND DE1DA3  
 96 RC 3

97 KK RC3-C3  
 98 KM ROUTE OUTFLOW FROM CPIC31 TO DETIC3  
 99 KN TRIANGULAR CHANNEL PER PLANS 11182-E-94 AND 190-E-95  
 100 KN SIDE SLOPE = 3:1 (H:V)  
 101 KN MAX DEPTH = 2.35 FT.  
 102 RS 1 FLOW -1  
 103 RC 0.025 0.025 0.025 850 0.005  
 104 RX 0 0.5 1.0 8.04 8.05 15.1 15.5 16  
 105 RY 2.37 2.36 2.35 0 0 2.35 2.36 2.37  
 \* START AT OFF-SITE DALIN ON THE NORTHEAST CORNER OF VILLAGE 1 \*  
 \* .....

106 KK 011-1A  
 107 KM OFF-SITE CONTRIBUTING AREA LOCATED ON CITY'S LAND  
 108 RA 013  
 109 LS 77  
 110 UD .06

111 KK 1A2  
 112 KM EXCESS RUNOFF FROM SUBAREA 1A2  
 113 RA 004  
 114 LS 77 44  
 115 UD .06

116 KK 1A3  
 117 KM EXCESS RUNOFF FROM SUBAREA 1A3  
 118 RA 006  
 119 LS 77 40  
 120 UD .05

121 KK CPA3  
 122 KM COMBINE HYDROGRAPHS FROM 1A1, 011-1A AND 1A3  
 123 RC 3

124 KK DET1A3  
 125 KM DETENTION BASIN FOR SUBAREA 1A3  
 126 RS 1 STOR 0  
 127 SV 0 0.15  
 128 SQ 0 72  
 129 SE 0 2.5  
 130 ST 2.5 15 2.8 3.5  
 REC-1 INPUT

PAGE 4

LINE ID 1 2 3 4 5 6 7 8 9 10

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131 KK RA3-A6
132 KM ROUTE OUTFLOW HYDROGRAPH FROM DET1A1 TO DET1A6
133 FM TRAPEZOIDAL CHANNEL (ASSUMED)
134 KH SIDE SLOPE = 5:1 (H:V)
135 KU MAX DEPTH = 1.0 FT
136 KW ROT WIDTH = 10.0 FT
137 RS 1 FLOW 1
138 RC 0.025 0.025 0.025 550 0.0115
139 RX 0 0.5 1.0 6 16 21 21.5 22.0
140 RY 1.02 1.01 1.0 0 0 1.0 1.01 1.02

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141 KK LA6
142 KM EXCESS RUNOFF FROM SUBAREA LA6
143 FM
144 KH 77 14
145 KU 05

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146 KK CP1A6
147 KM COMBINE HYDROGRAPHS FROM RA3-A6 AND LA6
148 HC 2

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149 KK DET1A6
150 KM DETENTION BASIN FOR SUBAREA LA6
151 RS 1 STOR 0
152 SV 0 0.20
153 SQ 0 22
154 SE 0 2.5
155 ST 2.5 15 2.8 1.5

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156 KK LA5
157 KM EXCESS RUNOFF FROM SUBAREA LA5
158 FM
159 KH 77 46
160 KU 07

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161 KK CP1A5
162 KM COMBINE HYDROGRAPHS FROM DET1A6 AND LA5
163 HC 2

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164 KK DET1A5
165 KM DETENTION BASIN FOR SUBAREA LA5
166 RS 1 STOR 0
167 SV 0 0.65
168 SQ 0 34
169 SE 0 2.5
170 ST 3.5 15 2.8 1.5

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171 KK LA4
172 KM EXCESS RUNOFF FROM SUBAREA LA4
173 FM
174 KH 77 48
175 KU 07

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HSC-1 INPUT

PAGE 5

LINE 10 1 2 3 4 5 6 7 8 9 10

```

176 KK RA4-A7
177 KM ROUTE OUTFLOW FROM DET1A4 TO DET1A7
178 FM TRAPEZOIDAL CHANNEL (ASSUMED)
179 KH SIDE SLOPE = 10:1 (H:V)
180 KU MAX DEPTH = 1.0 FT
181 KW ROT WIDTH = 10.0 FT
182 RS 1 FLOW 1
183 RC 0.030 0.030 0.030 300 0.0175
184 RX 0 0.5 1.0 11 21 31 31.5 32.0
185 RY 1.02 1.01 1.0 0 0 1.0 1.01 1.02

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186 KK DET1A4
187 KM DETENTION BASIN FOR SUBAREA LA4
188 RS 1 STOR 0
189 SV 0 0.37
190 SQ 0 11
191 SE 0 2.5
192 ST 2.5 15 2.0 1.5

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193 KK LA7
194 KM EXCESS RUNOFF FROM SUBAREA LA7
195 FM
196 KH 77 27
197 KU 05

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198 KK CP1A7
199 KM COMBINE HYDROGRAPHS FROM DET1A5, DET1A4, AND LA7
200 HC 3

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201 KK DET1A7
202 KM DETENTION BASIN FOR SUBAREA LA7
203 RS 1 STOR 0
204 SV 0 0.93
205 SQ 0 11
206 SE 0 2.5
207 ST 2.5 15 2.8 1.5

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208 KK IC1
209 KM EXCESS RUNOFF FROM SUBAREA IC1
210 FM
211 KH 77 38
212 KU 09

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213 KK CP1C1
214 KM COMBINE HYDROGRAPHS FROM DET1A7, AND IC1

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215 HC 2

216 KK DETIC1  
 217 EM DETENTION BASIN FOR SUBAREA 1C1  
 218 EM STORAGE VOLUME PER PLANS (405-E-95)  
 219 EM OUTLET IS A 18" RORCP PER PLANS (405-E-95)  
 220 RS 1 STOR 0  
 221 SV 0 1 5  
 222 SQ 0 14

HEC-1 INPUT

LINE ID 1 2 3 4 5 6 7 8 9 10

223 SE 0 3 6  
 224 ST 3 6 15 2 8 1 5

225 KK 1C2  
 226 EM EXCESS RUNOFF FROM SUBAREA 1C2  
 227 BA .024  
 228 LS 77 12  
 229 UD 68

230 KK CPC12  
 231 EM COMBINE HYDROGRAPHS FROM DETIC1 AND 1C2  
 232 HC 2

233 KK DETIC2A  
 234 EM DETENTION BASIN FOR SUBAREA 1C2  
 235 EM STORAGE VOLUME PER PLANS (405-E-95)  
 236 EM OUTLET IS A 18" RORCP PER PLANS (405-E-95)  
 237 RS 1 STOR 0  
 238 SV 0 0 39  
 239 SQ 0 14  
 240 SE 0 1 6  
 241 ST 3 6 15 2 8 1 5

242 KK DETIC2B  
 243 EM DETENTION BASIN FOR SUBAREA 1C2  
 244 EM STORAGE VOLUME PER PLANS (405-E-95)  
 245 EM OUTLET IS A 18" RORCP PER PLANS (405-E-95)  
 246 RS 1 STOR 0  
 247 SV 0 0 22  
 248 SQ 0 14  
 249 SU 0 1 6  
 250 ST 3 6 15 2 8 1 5

251 KK DETIC2C  
 252 EM DETENTION BASIN FOR SUBAREA 1C2  
 253 EM STORAGE VOLUME PER PLANS (405-E-95)  
 254 EM OUTLET IS A 18" RORCP PER PLANS (405-E-95)  
 255 RS 1 STOR 0  
 256 SV 0 0 54  
 257 SQ 0 14  
 258 SE 0 1 6  
 259 ST 3 6 15 2 8 1 5

260 KK 1C3  
 261 EM EXCESS RUNOFF FROM SUBAREA 1C3  
 262 BA .076  
 263 LS 77 15  
 264 UD 66

265 KK CPC3  
 266 EM COMBINE HYDROGRAPHS FROM 1C2-C, DETIC2C, AND 1C3  
 267 HC 3

HEC-1 INPUT

LINE ID 1 2 3 4 5 6 7 8 9 10

268 KK DETIC3  
 269 EM DETENTION BASIN FOR SUBAREA 1C3  
 270 EM STORAGE VOLUME PER PLANS (405-E-95)  
 271 EM OUTLET IS A 6" W x 3" H CUP PER PLANS (1142-E-29 AND 190-E-95)  
 272 RS 1 STOR 0  
 273 SV 0 1 1  
 274 SQ 0 150  
 275 SE 0 3 5  
 276 ST 3 5 15 2 8 1 5

277 KK RCICOM  
 278 EM ROUTE OUTFLOW FROM DETIC3 TO WIDE DETCOM OUTFLOWS  
 279 RS 1 FLOW 1  
 280 RC 0.010 0 010 0 010 1000 0 016  
 281 RZ 0 5 10 20 30 40 50  
 282 RY 12 0 11 75 11 5 10 0 10 0 11 5 11 75 12 0

283 KK COMS  
 284 EM EXCESS RUNOFF FROM SUBAREA COMMERCIAL  
 285 BA .03  
 286 LS 77 90  
 287 UD 67

288 KK DETCOM  
 289 EM DETENTION FOR SUBAREA COMMERCIAL  
 290 RS 1 STOR 0  
 291 SV 0 1 1  
 292 SQ 0 13  
 293 SE 0 3  
 294 ST 3 15 2 8 1 5

295 KK CPCOM  
 296 EM COMBINE HYDROGRAPHS FROM RCICOM AND COMS  
 297 HC 2

PAGE 6

PAGE 7

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298 KK COMOFF1
299 KM ROUTE CPOCON TO CPOFF1
300 RS 1 FLOW .1
301 RC 0.030 0 030 0 030 900 0 0158
302 RX 0 5 10 20 30 40 45 50
303 RY 12 0 11.75 11.5 10.0 10.0 11.5 11.75 12.0
304 KK OFF1
305 KM EXCESS RUNOFF FROM SUBAREA OFF1
306 RA 02
307 LS 77 90
308 UD 05
309 KK DEOFF1
310 KM DETENTION FOR SUBAREA OFF1
311 RS 1 STOR 0
312 SV 0 2.4
313 SQ 0 13
314 SK 0 3

```

HEC-1 INPUT

PAGE 5

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LINE ID 1 2 3 4 5 6 7 8 9 10
315 ST 1 15 2.8 1.5
316 KK CPOFF1
317 KM COMBINE HYDROGRAPHS FROM COMOFF AND DEOFF1
318 RC 2
319 KK OF1OFF1
320 KM SOUTH CPOFF1 TO CPOFF1
321 RS 1 FLOW .1
322 RC 0 030 0 030 0 030 500 0 013
323 RX 0 5 10 20 30 40 45 50
324 RY 12 0 11.75 11.5 10.0 10.0 11.5 11.75 12.0
325 KK OFF1
326 KM EXCESS RUNOFF FROM SUBAREA OFF1
327 RA 016
328 LS 77 90
329 UD 07
330 KK DEOFF1
331 KM DETENTION FOR SUBAREA OFF1
332 RS 1 STOR 0
333 SV 0 2.34
334 SQ 0 13
335 SK 0 3
336 ST 3 15 2.8 1.5
337 KK CPOFF1
338 KM COMBINE HYDROGRAPHS FROM DEOFF1 AND OF1OFF1
339 RC 3
* START WEST SIDE OF STACKED 40 DESIGN CONCEPT CROSSING SCOTTSDALE RD
*
340 KK 33A1 CP
341 KM ROUTE CPOFF1 THROUGH SUB 33A
342 RK 1960 0161 045 TRAP 20 3
*
343 KK 33A 540
344 KM RUNOFF FROM SUB 33A. INCLUDES WEST SIDE OF CINDER DRIVE
345 RA 054
346 LS 77 35
347 RY 300 0 020 05 100
348 RK 2125 013 015 TRAP 20 3
*
349 KK 33A3 CP
350 KO 1
351 KM COMBINE SUB 33A, CP 33A1
352 RC 3
* END WEST SIDE OF STACKED 40 DESIGN CONCEPT CROSSING SCOTTSDALE RD
*
* BEGIN GILBERTSON MODEL FOR GRAYHAWK - VILLAGE 1
* START AT NORTHEAST CORNER OF PARCEL 10B AND GO SOUTHWEST THROUGH
* PROPOSED PARK SITE
*

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HEC-1 INPUT

PAGE 9

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LINE ID 1 2 3 4 5 6 7 8 9 10
353 KK 10B
354 KM EXCESS RUNOFF FROM SUBAREA 10B
355 RA 04
356 LS 77 35
357 UD 06
358 KK DE10B
359 KM DETENTION FOR SUBAREA 10B
360 RS 1 STOR 0
361 SV 0 2.7
362 SQ 0 13
363 GL 0 3.0
364 ST 3 0 15 2.8 1.5
365 KK 10a1
366 KM EXCESS RUNOFF FROM SUBAREA 10a1

```



1	LINE	10	1	2	3	4	5	6	7	8	9	10
458	KX DETAIL											
457	KX DETAIL											
456	KX DETAIL											
455	KX DETAIL											
454	KX DETAIL											
453	KX DETAIL											
452	KX DETAIL											
451	KX DETAIL											
450	KX DETAIL											
449	KX DETAIL											
448	KX DETAIL											
447	KX DETAIL											
446	KX DETAIL											
445	KX DETAIL											
444	KX DETAIL											
443	KX DETAIL											
442	KX DETAIL											
441	KX DETAIL											
440	KX DETAIL											
439	KX DETAIL											
438	KX DETAIL											
437	KX DETAIL											
436	KX DETAIL											
435	KX DETAIL											
434	KX DETAIL											
433	KX DETAIL											
432	KX DETAIL											
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359	KX DETAIL											
358	KX DETAIL											
357	KX DETAIL											

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449      RY      12 0   11 75   11 5   10 0   10 0   11 5   11 75   12 0
450      KK      1EC
451      KM      EXCESS RUNOFF FROM SUBAREA 1EC
452      BA      0089
453      LS              77   50
454      UD      06

455      KK      DET1EC
456      KM      DETENTION FOR SUBAREA 1EC
457      RS      1      STOR      0
458      SV      0      0 8
459      SQ      0      11
460      SE      0      1
461      ST      3      15   2 8   1 5

462      KK      CP1EC
463      KM      COMBINE HYDROGRAPHS FROM SCHULZ AND DET1EC
464      HC      2

465      KK      DECA2
466      KM      ROUTE OUTFLOW FROM CP1EC TO CP1EA2
467      RS      1      FLOW      -1
468      RC      0 030 0 030 0 030 500 0 009
469      RK      0      2 5      5      10      20      25      27.5      30
470      RY      12 0   11 75   11 5   10 0   10 0   11 5   11 75   12 0

471      KK      CP1EA
472      KM      COMBINE HYDROGRAPHS FROM CP1EC2, DECA2 AND PARK
473      HC      3

474      KK      REATPP
475      KM      ROUTE CP1EA TO THOMPSON PEAK PARKWAY
476      RS      1      FLOW      -1
477      RC      0 030 0 030 0 030 250 0 0166
478      RK      0      2 5      5      10      20      25      27.5      30
479      RY      12 0   11 75   11 5   10 0   10 0   11 5   11 75   12 0

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HUC-1 INPUT

PAGE 12

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LINE      ID      1      2      3      4      5      6      7      8      9      10

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480      KK      1cd
481      KM      EXCESS RUNOFF FROM SUBAREA 1cd
482      BA      .0576
483      LS              77   52
484      UD      08

485      KK      DET1CD
486      KM      DETENTION FOR PARCEL 1CD
487      RS      1      STOR      0
488      SV      0      4 9
489      SQ      0      52
490      SE      0      3
491      ST      3      15   2 8   1 5

492      KK      OFF2
493      KM      EXCESS RUNOFF FROM SUBAREA OFF2 PUMPED HOSPITAL FLOWS
494      BA      011
495      LS              77   99
496      UD      07

497      KK      DEOFF2
498      KM      DETENTION FOR SUBAREA OFF2 PUMPED HOSPITAL FLOWS
499      RS      1      STOR      0
500      SV      0      4 5
501      SQ      0      13
502      SE      0      1
503      ST      3      15   2 8   1 5

504      KK      CPOFF2
505      KM      COMBINE HYDROGRAPHS REATPP, DET1CD AND DEOFF2
506      HC      3

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\* END GILBERTSON MODEL FOR GRAYHAWK - VILLAGE 1

\* START EAST SIDE OF STACKED 40 DESIGN

```

507      KK      1Kc 1  ROUTE
508      KM      ROUTE CPOFF2 THROUGH SUB 1Kc
509      RK      840  0135  045      TRAP      10      2

510      KK      1Kc  SUB
511      KM      R/O FROM SUB 1Kc
512      BA      BA HAS BEEN REVISED TO REFLECT DEVELOPED SHAPE OF PARCEL 1K
513      LS      .0515
514      LS              77   55
515      UD      0 15

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HUC-1 INPUT

PAGE 13

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LINE      ID      1      2      3      4      5      6      7      8      9      10

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516      KK      DET1K
517      KM      DETENTION FOR SUBAREA 1Kc
518      RS      1      STOR      0
519      SV      0      4 6
520      SQ      0      20
521      SE      0      1
522      ST      3      15   2 8   1 5

```

526	1	ROUTE 1	1	MI	1.00	1.00	10/10/10	JD
527	2	ROUTE 2	1	MI	1.00	1.00	10/10/10	JD
528	3	ROUTE 3	1	MI	1.00	1.00	10/10/10	JD
529	4	ROUTE 4	1	MI	1.00	1.00	10/10/10	JD
530	5	ROUTE 5	1	MI	1.00	1.00	10/10/10	JD
531	6	ROUTE 6	1	MI	1.00	1.00	10/10/10	JD
532	7	ROUTE 7	1	MI	1.00	1.00	10/10/10	JD
533	8	ROUTE 8	1	MI	1.00	1.00	10/10/10	JD
534	9	ROUTE 9	1	MI	1.00	1.00	10/10/10	JD
535	10	ROUTE 10	1	MI	1.00	1.00	10/10/10	JD
536	11	ROUTE 11	1	MI	1.00	1.00	10/10/10	JD
537	12	ROUTE 12	1	MI	1.00	1.00	10/10/10	JD
538	13	ROUTE 13	1	MI	1.00	1.00	10/10/10	JD
539	14	ROUTE 14	1	MI	1.00	1.00	10/10/10	JD
540	15	ROUTE 15	1	MI	1.00	1.00	10/10/10	JD
541	16	ROUTE 16	1	MI	1.00	1.00	10/10/10	JD
542	17	ROUTE 17	1	MI	1.00	1.00	10/10/10	JD
543	18	ROUTE 18	1	MI	1.00	1.00	10/10/10	JD
544	19	ROUTE 19	1	MI	1.00	1.00	10/10/10	JD
545	20	ROUTE 20	1	MI	1.00	1.00	10/10/10	JD
546	21	ROUTE 21	1	MI	1.00	1.00	10/10/10	JD
547	22	ROUTE 22	1	MI	1.00	1.00	10/10/10	JD
548	23	ROUTE 23	1	MI	1.00	1.00	10/10/10	JD
549	24	ROUTE 24	1	MI	1.00	1.00	10/10/10	JD
550	25	ROUTE 25	1	MI	1.00	1.00	10/10/10	JD
551	26	ROUTE 26	1	MI	1.00	1.00	10/10/10	JD
552	27	ROUTE 27	1	MI	1.00	1.00	10/10/10	JD
553	28	ROUTE 28	1	MI	1.00	1.00	10/10/10	JD
554	29	ROUTE 29	1	MI	1.00	1.00	10/10/10	JD
555	30	ROUTE 30	1	MI	1.00	1.00	10/10/10	JD
556	31	ROUTE 31	1	MI	1.00	1.00	10/10/10	JD
557	32	ROUTE 32	1	MI	1.00	1.00	10/10/10	JD
558	33	ROUTE 33	1	MI	1.00	1.00	10/10/10	JD
559	34	ROUTE 34	1	MI	1.00	1.00	10/10/10	JD
560	35	ROUTE 35	1	MI	1.00	1.00	10/10/10	JD
561	36	ROUTE 36	1	MI	1.00	1.00	10/10/10	JD
562	37	ROUTE 37	1	MI	1.00	1.00	10/10/10	JD
563	38	ROUTE 38	1	MI	1.00	1.00	10/10/10	JD
564	39	ROUTE 39	1	MI	1.00	1.00	10/10/10	JD
565	40	ROUTE 40	1	MI	1.00	1.00	10/10/10	JD
566	41	ROUTE 41	1	MI	1.00	1.00	10/10/10	JD
567	42	ROUTE 42	1	MI	1.00	1.00	10/10/10	JD
568	43	ROUTE 43	1	MI	1.00	1.00	10/10/10	JD
569	44	ROUTE 44	1	MI	1.00	1.00	10/10/10	JD
570	45	ROUTE 45	1	MI	1.00	1.00	10/10/10	JD
571	46	ROUTE 46	1	MI	1.00	1.00	10/10/10	JD
572	47	ROUTE 47	1	MI	1.00	1.00	10/10/10	JD
573	48	ROUTE 48	1	MI	1.00	1.00	10/10/10	JD
574	49	ROUTE 49	1	MI	1.00	1.00	10/10/10	JD
575	50	ROUTE 50	1	MI	1.00	1.00	10/10/10	JD
576	51	ROUTE 51	1	MI	1.00	1.00	10/10/10	JD
577	52	ROUTE 52	1	MI	1.00	1.00	10/10/10	JD
578	53	ROUTE 53	1	MI	1.00	1.00	10/10/10	JD
579	54	ROUTE 54	1	MI	1.00	1.00	10/10/10	JD
580	55	ROUTE 55	1	MI	1.00	1.00	10/10/10	JD
581	56	ROUTE 56	1	MI	1.00	1.00	10/10/10	JD
582	57	ROUTE 57	1	MI	1.00	1.00	10/10/10	JD
583	58	ROUTE 58	1	MI	1.00	1.00	10/10/10	JD
584	59	ROUTE 59	1	MI	1.00	1.00	10/10/10	JD
585	60	ROUTE 60	1	MI	1.00	1.00	10/10/10	JD
586	61	ROUTE 61	1	MI	1.00	1.00	10/10/10	JD
587	62	ROUTE 62	1	MI	1.00	1.00	10/10/10	JD
588	63	ROUTE 63	1	MI	1.00	1.00	10/10/10	JD
589	64	ROUTE 64	1	MI	1.00	1.00	10/10/10	JD
590	65	ROUTE 65	1	MI	1.00	1.00	10/10/10	JD
591	66	ROUTE 66	1	MI	1.00	1.00	10/10/10	JD
592	67	ROUTE 67	1	MI	1.00	1.00	10/10/10	JD
593	68	ROUTE 68	1	MI	1.00	1.00	10/10/10	JD
594	69	ROUTE 69	1	MI	1.00	1.00	10/10/10	JD
595	70	ROUTE 70	1	MI	1.00	1.00	10/10/10	JD
596	71	ROUTE 71	1	MI	1.00	1.00	10/10/10	JD
597	72	ROUTE 72	1	MI	1.00	1.00	10/10/10	JD
598	73	ROUTE 73	1	MI	1.00	1.00	10/10/10	JD
599	74	ROUTE 74	1	MI	1.00	1.00	10/10/10	JD
600	75	ROUTE 75	1	MI	1.00	1.00	10/10/10	JD
601	76	ROUTE 76	1	MI	1.00	1.00	10/10/10	JD
602	77	ROUTE 77	1	MI	1.00	1.00	10/10/10	JD
603	78	ROUTE 78	1	MI	1.00	1.00	10/10/10	JD
604	79	ROUTE 79	1	MI	1.00	1.00	10/10/10	JD
605	80	ROUTE 80	1	MI	1.00	1.00	10/10/10	JD
606	81	ROUTE 81	1	MI	1.00	1.00	10/10/10	JD
607	82	ROUTE 82	1	MI	1.00	1.00	10/10/10	JD
608	83	ROUTE 83	1	MI	1.00	1.00	10/10/10	JD
609	84	ROUTE 84	1	MI	1.00	1.00	10/10/10	JD
610	85	ROUTE 85	1	MI	1.00	1.00	10/10/10	JD
611	86	ROUTE 86	1	MI	1.00	1.00	10/10/10	JD
612	87	ROUTE 87	1	MI	1.00	1.00	10/10/10	JD
613	88	ROUTE 88	1	MI	1.00	1.00	10/10/10	JD
614	89	ROUTE 89	1	MI	1.00	1.00	10/10/10	JD
615	90	ROUTE 90	1	MI	1.00	1.00	10/10/10	JD
616	91	ROUTE 91	1	MI	1.00	1.00	10/10/10	JD
617	92	ROUTE 92	1	MI	1.00	1.00	10/10/10	JD
618	93	ROUTE 93	1	MI	1.00	1.00	10/10/10	JD
619	94	ROUTE 94	1	MI	1.00	1.00	10/10/10	JD
620	95	ROUTE 95	1	MI	1.00	1.00	10/10/10	JD
621	96	ROUTE 96	1	MI	1.00	1.00	10/10/10	JD
622	97	ROUTE 97	1	MI	1.00	1.00	10/10/10	JD
623	98	ROUTE 98	1	MI	1.00	1.00	10/10/10	JD
624	99	ROUTE 99	1	MI	1.00	1.00	10/10/10	JD
625	100	ROUTE 100	1	MI	1.00	1.00	10/10/10	JD

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LINE      ID ..... 1 ..... 2 ..... 3 ..... 4 ..... 5 ..... 6 ..... 7 ..... 8 ..... 9 ..... 10 .....
590      DQ      0      2.7    10.4    22.6    38.7    58.4    80.8    105.4    133.6    158.5
591      DQ      185.7    212.3    230.2    246.9
*
592      KK      33C      SUB
593      KM      SUBBASIN 33C SOUTH OF CENTER DRIVE WEST SIDE OF PROPERTY
594      KM      MODIFIED AREA TO ACCOUNT FOR NEW SITE PLAN AND SUBS 04-27-06 - ADDED SOUTHWEST
595      BA      0 0296
596      LS      77      87
597      UK      200    .0068    .05    100
598      RK      1750    .017    .015          CIRC      5
*
599      KK      540CN      SUB
600      KM      SUB SOUTH OF CENTER DRIVE, CENTRAL BASIN FLOWING DIRECTLY INTO DET/RET
601      KM      INCLUDES DETENTION BASIN
602      BA      0448
603      LS      77      87
604      UK      250    .0075    .05    100
605      RK      1500    .009    .015          CIRC      4.5
*
606      KK      CT13 1 COMBINE
607      KM      COMBINE CT13.0, 33C FLOWS (Total Flow at the BASIN)
608      MC      3
*
609      KK      D_BAS
610      KM      BY-PASS FLOW THROUGH 36" PIPE (MAX Q = 30 CFS) BASIN OUTLETS PROVIDE
611      KM      EQUIVALENT AMOUNT OF DISCHARGE
612      DT      P-PIPE
613      DI      0      1 0      10 0      30 0      50      100.0      300.0      500.0      800.0
614      DQ      0      1.0      10.0      30.0      50      100      300      500      800
*
615      KK      D_BAS1
616      KM      DIVERT THE FIRST 1 AC-FT INTO THE SURFACE STORAGE
617      DT      D-BAS2      1.0
618      DI      0      1.0      10.0      30 0      50 0      100.0      300.0      500.0      800.0
619      DQ      0      1.0      10.0      30 0      50.0      100.0      300.0      500.0      800.0
*
620      KK      D_SURF
621      KM      DIVERT FLOW INTO SURF SURFACE STORAGE
622      KM      (1110' 10" DIAMETER PIPE, VOL = 2.0 AC-FT)
623      KO      1
624      DT      D-SURF      2
625      DI      0      1.0      10.0      30 0      50.0      100.0      300.0      500.0      800.0
626      DQ      0      1.0      10.0      30.0      50.0      100.0      300.0      500.0      800.0
*

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LINE      ID ..... 1 ..... 2 ..... 3 ..... 4 ..... 5 ..... 6 ..... 7 ..... 8 ..... 9 ..... 10 .....
627      KK      B_PIPE
628      KM      RETRIEVE DIVERTED PIPE FLOW
629      DK      P-PIPE
*
630      KK      B_SURF
631      KM      RETRIEVE DIVERTED SURFACE FLOW
632      DR      D-BAS2
*
633      KK      C5400 COMBINE
634      KO      1
635      KM      COMBINE PIPE FLOW, DIVERTED SURFACE FLOW AND REMAINING SURFACE FLOW
636      MC      3
*
637      KK      S40BAS
638      KO      3
639      KM      ROUTE DIVERTED FLOW THROUGH OFFLINE BASIN CONCEPT MAX H = 5.9
640      KM      ASSUMED 1000' X 80' BASIN WITH 5:1 SIDE SLOPES & 36" OUTLET
641      KM      24" BLEED-OFF PIPE PLUS 20' WIDE SPILLWAY AT 3 6"
642      RG      3      STOR      -2
643      SV      0      .001    .14    .87    1 84    3 01    4.49    5.16    5.49    5.87
644      SV      6.14
645      SE      0      .8      1      2      3      4      5      5.4      5.6      5.8
646      SE      6
647      SG      1      3.14    0.62    0.5
648      SS      3.8      20      2.8      1.5
*
649      KK      P33E.1
650      KO      1
651      KM      DIVIDE THE FLOW INTO TWO ADOT CULVERTS
652      DT      D33C.2
653      DI      0      100      200      400      600
654      DQ      0      68      136      272      408
*
655      KK      R_ADOT
656      KM      RETRIEVE DIVERTED ADOT CULVERT FLOW
657      DR      P_ADOT
*

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658 KK 33E.1 COMBINE  
 659 KO 1  
 660 KM COMBINED DISCHARGE AT ADOT CULVERT 5 AND 6  
 661 HC 2  
 \*

# HEC-1 INPUT

PAGE 17

LINE ID. . . . .1 . . . . .2 . . . . .3 . . . . .4 . . . . .5 . . . . .6 . . . . .7 . . . . .8 . . . . .9 . . . . .10

662 KK R33E.1 ROUTE  
 663 KO 1  
 664 KM ROUTE ADOT CULVERT 5 AND 6 FLOWS THROUGH ASLD LAND  
 665 KM OPTION 5 - PROPOSED CHANNEL SOUTH OF LUND CADILLAC TO SCOTTSDALE ROAD  
 666 KM FROM SCOTTSDALE ROAD SOUTH TO PRINCESS DRIVE  
 667 KM ROUTE L=4600', TRAP SECTION HW=19' Z=5, TWmax=39'  
 668 KM ASSUME GRASS LINED CHANNEL H=0.030 UP=1597 S DOWN=1553  
 669 RK 4600 0.0080 0.03 TRAP 19 5  
 \*

670 KK ASLD SUB  
 671 KO 1  
 672 KM ASLD PARCEL EAST OF SCOTTSDALE ROAD  
 673 BA 0.0533  
 674 LS 77  
 675 UK 89 0.0213 0.1 100  
 676 RK 2300 0.0080 0.03 TRAP 19 5  
 \*

677 KK CPTPIN COMBINE  
 678 KO 1  
 679 KM COMBINE ROUTED ADOT 5 AND 6 WITH ASLD PARCEL  
 680 HC 2  
 \*

681 KK D33C.2  
 682 KO 1  
 683 KM RETRIEVE DIVERTED PIPE FLOW  
 684 DR D33C.2  
 \*

685 KK S40E1 SUB  
 686 KO 1  
 687 KM SUB EAST OF SCOTTSDALE RD, FLOWING DIRECTLY INTO SCOTTSDALE RD  
 688 KM CULVERT, TAKES SCOTT'S RD HALF ST AND SCENIC CORRIDOR  
 689 BA 0.0063  
 690 LS 77 89  
 691 UK 50 .01 .05 100  
 692 RK 600 .01 .015 CIRC 4.5  
 \*

693 KK 33C.2 COMBINE  
 694 KO 1  
 695 KM COMBINED DISCHARGE AT SCOTTSDALE ROAD CULVERT  
 696 HC 2  
 \*

697 ZZ

## SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT  
 LINE (V) ROUTING (--->) DIRECTION OR PUMP FLOW  
 NO. (.) CONNECTOR (---) RETURN OF DIVERTED OR PUMPED FLOW

```

20 1A1
   V
   V
27 DET1A1
   V
   V
34 RA1-C1
   .
   .
43 1C1
   .
   .
46 CP1C1
   V
   V
51 RC1-C1
   .
   .
60 1Da3
   V
   V
65 DE1Da3
   .
   .
73 1Da4
   .
   .
78 CP1Da4
   V
   V
81 DE1Da4
   .
   .
89 1Da5
   .
   .
  
```

94	CP1C31.....	
	V	
97	RCJ-CJ	
	.	
106	Off-1A	
	.	
111		1A2
	.	
116		1A3
	.	
121	CPA3.....	
	V	
	V	
124	DET1A3	
	V	
	V	
131	RA3-A6	
	.	
141		1A6
	.	
146	CP1A6.....	
	V	
	V	
149	DET1A6	
	.	
156		1A5
	.	
161	CP1A5.....	
	V	
	V	
164	DET1A5	
	.	
171		1A4
	.	
176		RA5-A7
	.	
	.	
186		DET1A4
	.	
193		1A7
	.	
198	CP1A7.....	
	V	
	V	
201	DET1A7	
	.	
206		1C1
	.	
211	CP1C1.....	
	V	
	V	
216	DET1C1	
	.	
225		1C2
	.	
230	CP1C2.....	
	V	
	V	
233	DET1C2A	
	V	
	V	
242	DET1C2B	
	V	
	V	
251	DET1C2C	
	.	
260		1C3
	.	
265	CP1C3.....	
	V	
	V	
268	DET1C3	
	V	
	V	
277	RC3C03	
	.	
281	COM3	
	V	
	V	
288	DET1COM	
	.	
295	CP1C03.....	
	V	



```

      V
308  COMOFF
      .
309  .      OFF1
      .      V
      .      V
310  .      DEOFF1
      .
316  CPOFF1 . . . . .
      .      V
      .      V
319  OF1OF2
      .
325  .      OFF3
      .      V
      .      V
330  .      DEOFF3
      .
337  CPOFF3 . . . . .
      .      V
      .      V
340  JJA1
      .
341  .      JJA
      .
349  JJA3 . . . . .
      .
353  .      1Da1
      .      V
      .      V
358  .      DE1Da1
      .
365  .      1Da1
      .      V
      .      V
370  .      DE1Da1
      .
378  .      1Da2
      .
383  CU1Da2 . . . . .
      .      V
      .      V
386  RDa2E2
      .
396  .      1Ea1
      .      V
      .      V
401  .      DE1Ea1
      .
409  .      1Ea2
      .
414  .      CP1Ea2 . . . . .
      .      V
      .      V
417  .      DE1Ea2
      .
424  .      CP1Ea2 . . . . .
      .
427  .      PARK
      .
432  .      SCHOOL
      .      V
      .      V
437  .      DETSCH
      .      V
      .      V
444  .      SCHL2
      .
450  .      1Ec
      .      V
      .      V
455  .      DE1Ec
      .
462  .      CP1Ec . . . . .
      .      V
      .      V
465  .      1EcEa2
      .
471  .      CP1Ea
      .      V
      .      V
474  .      RENTTP
      .
480  .      1ED

```

[illegible]

```

658      336 1. . . .
      V
      V
662      336.1
      .
      .
670      336.1
      .
      .
677      336.1
      .
      .
684      336.1
      .
      .
691      336.1
      .
      .
698      336.1
      .
      .
699      336.1
      .
      .

```

(\*\*\*) RUPOFF ALSO COMPUTED AT THIS LOCATION

```

* FLOOD HYDROGRAPH PACKAGE (DEC-11)
* JUN 1998
* VERSION 1.1
* RUN DATE 04FEB08 TIME 15 17 09

```

```

* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104

```

ONE SCOTTSDALE (STACKED 105) POST DEVELOPMENT CONDITION 100-YR 6-HR STORM  
 OFFSITE HYDROLOGY & ONSITE HYDROLOGY FOR AREA COVERED BY PRE-POST CRITERIA  
 OPTION A - ASLO CHANNEL  
 FILE 100YR-prec.DAT  
 OPTION B - 34.1 ACRES OF ASLO PARCEL

BASED ON MODELS PREPARED BY: ROBERT L. KARD, P.E., CONSULTING ENGINEER

```

P25X100 61
C1 61 (CENTER DRIVE PROJECT)
S10X100 61 (STACKED 105 EXISTING CONDITION)

```

ALL CURVE NUMBERS ADJUSTED TO 6-HOUR VALUES ON AUGUST 11, 2002  
 100-YEAR, 6-HOUR HYDROLOGICAL STORM

AREAL RAINFALL REDUCTION IS BASED ON A 11 SQUARE MILE STORM

```

19 10 OUTPUT CONTROL VARIABLES
      IPRINT 5 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCALE 0 HYDROGRAPH PLOT SCALE

17 HYDROGRAPH TIME DATA
      NMIN 5 MINUTES IN COMPUTATION INTERVAL
      NDATE 1 0 STARTING DATE
      ITIME 0000 STARTING TIME
      NQ 100 NUMBER OF HYDROGRAPH ORDINATES
      NDATE 2 0 ENDING DATE
      NQTIME 0000 ENDING TIME
      ICALEN 19 CENTURY MARK

      COMPUTATION INTERVAL 00 HOURS
      TOTAL TIME BASE 21 00 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA SQUARE KILOM
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND

STORAGE VOLUME ACRE-Feet
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

```

\*\*\*

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*****
* 336.1 * CP
*****

```

```

350 20 OUTPUT CONTROL VARIABLES
      IPRINT 1 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCALE 0 HYDROGRAPH PLOT SCALE
      CONTINUE SUB 336.1 CP 336.1

```

```

352 20 HYDROGRAPH COMBINATION
      ICOMB 2 NUMBER OF HYDROGRAPHS TO COMBINE

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HYDROGRAPH AT STATION 33A3  
SUM OF 2 HYDROGRAPHS

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	2	0	*	1	0615	76	41	*	1	1230	151	51	*	1	1045	226	1	
1	0005	2	0	*	1	0620	77	40	*	1	1235	152	50	*	1	1050	227	1	
1	0010	3	0	*	1	0625	78	38	*	1	1240	153	49	*	1	1055	228	1	
1	0015	3	0	*	1	0630	79	37	*	1	1245	154	48	*	1	1100	229	1	
1	0020	5	0	*	1	0635	80	36	*	1	1250	155	47	*	1	1105	230	1	
1	0025	6	0	*	1	0640	81	35	*	1	1255	156	46	*	1	1110	231	1	
1	0030	7	1	*	1	0645	82	34	*	1	1300	157	45	*	1	1115	232	1	
1	0035	8	1	*	1	0650	83	33	*	1	1305	158	44	*	1	1120	233	1	
1	0040	9	2	*	1	0655	84	32	*	1	1310	159	43	*	1	1125	234	1	
1	0045	10	1	*	1	0700	85	31	*	1	1315	160	42	*	1	1130	235	1	
1	0050	11	3	*	1	0705	86	30	*	1	1320	161	41	*	1	1135	236	1	
1	0055	12	4	*	1	0710	87	29	*	1	1325	162	40	*	1	1140	237	1	
1	0100	13	4	*	1	0715	88	28	*	1	1330	163	39	*	1	1145	238	0	
1	0105	14	4	*	1	0720	89	27	*	1	1335	164	38	*	1	1150	239	0	
1	0110	15	5	*	1	0725	90	26	*	1	1340	165	37	*	1	1155	240	0	
1	0115	16	5	*	1	0730	91	25	*	1	1345	166	36	*	1	1200	241	0	
1	0120	17	5	*	1	0735	92	24	*	1	1350	167	35	*	1	1205	242	0	
1	0125	18	6	*	1	0740	93	23	*	1	1355	168	34	*	1	1210	243	0	
1	0130	19	6	*	1	0745	94	22	*	1	1400	169	33	*	1	1215	244	0	
1	0135	20	7	*	1	0750	95	21	*	1	1405	170	32	*	1	1220	245	0	
1	0140	21	7	*	1	0755	96	20	*	1	1410	171	31	*	1	1225	246	0	
1	0145	22	8	*	1	0800	97	19	*	1	1415	172	30	*	1	1230	247	0	
1	0150	23	8	*	1	0805	98	18	*	1	1420	173	29	*	1	1235	248	0	
1	0155	24	9	*	1	0810	99	17	*	1	1425	174	28	*	1	1240	249	0	
1	0200	25	9	*	1	0815	100	16	*	1	1430	175	27	*	1	1245	250	0	
1	0205	26	10	*	1	0820	101	15	*	1	1435	176	26	*	1	1250	251	0	
1	0210	27	11	*	1	0825	102	14	*	1	1440	177	25	*	1	1255	252	0	
1	0215	28	11	*	1	0830	103	13	*	1	1445	178	24	*	1	1300	253	0	
1	0220	29	12	*	1	0835	104	12	*	1	1450	179	23	*	1	1305	254	0	
1	0225	30	13	*	1	0840	105	11	*	1	1455	180	22	*	1	1310	255	0	
1	0230	31	13	*	1	0845	106	10	*	1	1500	181	21	*	1	1315	256	0	
1	0235	32	14	*	1	0850	107	9	*	1	1505	182	20	*	1	1320	257	0	
1	0240	33	15	*	1	0855	108	8	*	1	1510	183	19	*	1	1325	258	0	
1	0245	34	15	*	1	0900	109	7	*	1	1515	184	18	*	1	1330	259	0	
1	0250	35	16	*	1	0905	110	6	*	1	1520	185	17	*	1	1335	260	0	
1	0255	36	16	*	1	0910	111	5	*	1	1525	186	16	*	1	1340	261	0	
1	0300	37	16	*	1	0915	112	4	*	1	1530	187	15	*	1	1345	262	0	
1	0305	38	17	*	1	0920	113	3	*	1	1535	188	14	*	1	1350	263	0	
1	0310	39	17	*	1	0925	114	2	*	1	1540	189	13	*	1	1355	264	0	
1	0315	40	17	*	1	0930	115	1	*	1	1545	190	12	*	1	1400	265	0	
1	0320	41	18	*	1	0935	116	1	*	1	1550	191	11	*	1	1405	266	0	
1	0325	42	18	*	1	0940	117	0	*	1	1555	192	10	*	1	1410	267	0	
1	0330	43	18	*	1	0945	118	0	*	1	1600	193	9	*	1	1415	268	0	
1	0335	44	19	*	1	0950	119	0	*	1	1605	194	8	*	1	1420	269	0	
1	0340	45	19	*	1	0955	120	0	*	1	1610	195	7	*	1	1425	270	0	
1	0345	46	19	*	1	1000	121	0	*	1	1615	196	6	*	1	1430	271	0	
1	0350	47	19	*	1	1005	122	0	*	1	1620	197	5	*	1	1435	272	0	
1	0355	48	19	*	1	1010	123	0	*	1	1625	198	4	*	1	1440	273	0	
1	0400	49	19	*	1	1015	124	0	*	1	1630	199	3	*	1	1445	274	0	
1	0405	50	19	*	1	1020	125	0	*	1	1635	200	2	*	1	1450	275	0	
1	0410	51	19	*	1	1025	126	0	*	1	1640	201	1	*	1	1455	276	0	
1	0415	52	19	*	1	1030	127	0	*	1	1645	202	0	*	1	1500	277	0	
1	0420	53	19	*	1	1035	128	0	*	1	1650	203	0	*	1	1505	278	0	
1	0425	54	19	*	1	1040	129	0	*	1	1655	204	0	*	1	1510	279	0	
1	0430	55	19	*	1	1045	130	0	*	1	1700	205	0	*	1	1515	280	0	
1	0435	56	19	*	1	1050	131	0	*	1	1705	206	0	*	1	1520	281	0	
1	0440	57	19	*	1	1055	132	0	*	1	1710	207	0	*	1	1525	282	0	
1	0445	58	19	*	1	1100	133	0	*	1	1715	208	0	*	1	1530	283	0	
1	0450	59	19	*	1	1105	134	0	*	1	1720	209	0	*	1	1535	284	0	
1	0455	60	19	*	1	1110	135	0	*	1	1725	210	0	*	1	1540	285	0	
1	0500	61	19	*	1	1115	136	0	*	1	1730	211	0	*	1	1545	286	0	
1	0505	62	19	*	1	1120	137	0	*	1	1735	212	0	*	1	1550	287	0	
1	0510	63	19	*	1	1125	138	0	*	1	1740	213	0	*	1	1555	288	0	
1	0515	64	19	*	1	1130	139	0	*	1	1745	214	0	*	1	0000	289	0	
1	0520	65	19	*	1	1135	140	0	*	1	1750	215	0	*	1	0005	290	0	
1	0525	66	19	*	1	1140	141	0	*	1	1755	216	0	*	1	0010	291	0	
1	0530	67	19	*	1	1145	142	0	*	1	1800	217	0	*	1	0015	292	0	
1	0535	68	19	*	1	1150	143	0	*	1	1805	218	0	*	1	0020	293	0	
1	0540	69	19	*	1	1155	144	0	*	1	1810	219	0	*	1	0025	294	0	
1	0545	70	19	*	1	1200	145	0	*	1	1815	220	0	*	1	0030	295	0	
1	0550	71	19	*	1	1205	146	0	*	1	1820	221	0	*	1	0035	296	0	
1	0555	72	19	*	1	1210	147	0	*	1	1825	222	0	*	1	0040	297	0	
1	0600	73	19	*	1	1215	148	0	*	1	1830	223	0	*	1	0045	298	0	
1	0605	74	19	*	1	1220	149	0	*	1	1835	224	0	*	1	0050	299	0	
1	0610	75	19	*	1	1225	150	0	*	1	1840	225	0	*	1	0055	300	0	

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW	74 92 HR
(CFS)	(HR)	6-HR 24-HR 72-HR	
232	1 08	(CFS)	
		55 19 19 19	
		(INCHES)	1 384 2 334 2 314 2 334
		(AC FT)	12 38 30 38
CUMULATIVE AREA 11 SQ MI			

560 20 OUTPUT CONTROL VARIABLES

PRINT	5	PRINT CONTROL
PLOT	9	PLOT CONTROL
SCALE	0	HYDROGRAPH PLOT SCALE

HYDROGRAPHIC STATION NO. 1111 0  
NOV 10 1965

1	0605	75	64	*	1	1220	149	G.	*	1	1815	224	1	*	?	0050	299	0
1	0610	75	61	*	1	1225	150	G.	*	1	1840	225	1	*	?	0055	300	0

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (CFS)	72-HR (CFS)	24 92-HR (CFS)
340	3 17	92	26	25	25
		1.966	2.259	2.259	2.259
		45.	52	52	52

CUMULATIVE AREA = 41.50 MI

620 KK

\*\*\*\*\*  
D\_SURF  
\*\*\*\*\*

623 KO

OUTPUT CONTROL VARIABLES  
 PRINT 1 PRINT CONTROL  
 PLOT 0 PLOT CONTROL  
 Q/CAL 0 HYDROGRAPH PLOT SCALE

WT

DIVERSION  
 ESTAB D-SUB# DIVERSION HYDROGRAPH IDENTIFICATION  
 DETERM 2 00 MAXIMUM VOLUME TO BE DIVERTED

DI

INFLOW 00 1 00 10 00 40 00 70 00 100 00 100 00 500 00 800 00

IQ

DIVERTED FLOW 00 1 00 10 00 40 00 70 00 100 00 300 00 500 00 800 00

\*\*\*

# DIVERSION HYDROGRAPH D-SUB#

DA	MON	HR	MIN	SEC	FLOW	DA	MON	HR	MIN	SEC	FLOW	DA	MON	HR	MIN	SEC	FLOW	DA	MON	HR	MIN	SEC	FLOW
1	0000	1	0	*	1	0515	16	0	*	1	1210	151	0	*	1	1845	226	0					0
1	0005	2	0	*	1	0620	17	0	*	1	1235	152	0	*	1	1850	227	0					0
1	0010	3	0	*	1	0625	78	0	*	1	1240	153	0	*	1	1855	228	0					0
1	0015	4	0	*	1	0630	79	0	*	1	1245	154	0	*	1	1900	229	0					0
1	0020	5	0	*	1	0635	80	0	*	1	1250	155	0	*	1	1905	230	0					0
1	0025	6	0	*	1	0640	81	0	*	1	1255	156	0	*	1	1910	231	0					0
1	0030	7	0	*	1	0645	82	0	*	1	1300	157	0	*	1	1915	232	0					0
1	0035	8	0	*	1	0650	83	0	*	1	1305	158	0	*	1	1920	233	0					0
1	0040	9	0	*	1	0655	84	0	*	1	1310	159	0	*	1	1925	234	0					0
1	0045	10	0	*	1	0700	85	0	*	1	1315	160	0	*	1	1930	235	0					0
1	0050	11	0	*	1	0705	86	0	*	1	1320	161	0	*	1	1935	236	0					0
1	0055	12	0	*	1	0710	87	0	*	1	1325	162	0	*	1	1940	237	0					0
1	0100	13	0	*	1	0715	88	0	*	1	1330	163	0	*	1	1945	238	0					0
1	0105	14	0	*	1	0720	89	0	*	1	1335	164	0	*	1	1950	239	0					0
1	0110	15	0	*	1	0725	90	0	*	1	1340	165	0	*	1	1955	240	0					0
1	0115	16	0	*	1	0730	91	0	*	1	1345	166	0	*	1	2000	241	0					0
1	0120	17	0	*	1	0735	92	0	*	1	1350	167	0	*	1	2005	242	0					0
1	0125	18	0	*	1	0740	93	0	*	1	1355	168	0	*	1	2010	243	0					0
1	0130	19	0	*	1	0745	94	0	*	1	1400	169	0	*	1	2015	244	0					0
1	0135	20	0	*	1	0750	95	0	*	1	1405	170	0	*	1	2020	245	0					0
1	0140	21	0	*	1	0755	96	0	*	1	1410	171	0	*	1	2025	246	0					0
1	0145	22	0	*	1	0800	97	0	*	1	1415	172	0	*	1	2030	247	0					0
1	0150	23	0	*	1	0805	98	0	*	1	1420	173	0	*	1	2035	248	0					0
1	0155	24	0	*	1	0810	99	0	*	1	1425	174	0	*	1	2040	249	0					0
1	0200	25	0	*	1	0815	100	0	*	1	1430	175	0	*	1	2045	250	0					0
1	0205	26	0	*	1	0820	101	0	*	1	1435	176	0	*	1	2050	251	0					0
1	0210	27	0	*	1	0825	102	0	*	1	1440	177	0	*	1	2055	252	0					0
1	0215	28	0	*	1	0830	103	0	*	1	1445	178	0	*	1	2100	253	0					0
1	0220	29	0	*	1	0835	104	0	*	1	1450	179	0	*	1	2105	254	0					0
1	0225	30	0	*	1	0840	105	0	*	1	1455	180	0	*	1	2110	255	0					0
1	0230	31	0	*	1	0845	106	0	*	1	1500	181	0	*	1	2115	256	0					0
1	0235	32	0	*	1	0850	107	0	*	1	1505	182	0	*	1	2120	257	0					0
1	0240	33	0	*	1	0855	108	0	*	1	1510	183	0	*	1	2125	258	0					0
1	0245	34	0	*	1	0900	109	0	*	1	1515	184	0	*	1	2130	259	0					0
1	0250	35	0	*	1	0905	110	0	*	1	1520	185	0	*	1	2135	260	0					0
1	0255	36	0	*	1	0910	111	0	*	1	1525	186	0	*	1	2140	261	0					0
1	0300	37	0	*	1	0915	112	0	*	1	1530	187	0	*	1	2145	262	0					0
1	0305	38	237	*	1	0920	113	0	*	1	1535	188	0	*	1	2150	263	0					0
1	0310	39	0	*	1	0925	114	0	*	1	1540	189	0	*	1	2155	264	0					0
1	0315	40	0	*	1	0930	115	0	*	1	1545	190	0	*	1	2200	265	0					0
1	0320	41	0	*	1	0935	116	0	*	1	1550	191	0	*	1	2205	266	0					0
1	0325	42	0	*	1	0940	117	0	*	1	1555	192	0	*	1	2210	267	0					0
1	0330	43	0	*	1	0945	118	0	*	1	1600	193	0	*	1	2215	268	0					0
1	0335	44	0	*	1	0950	119	0	*	1	1605	194	0	*	1	2220	269	0					0
1	0340	45	0	*	1	0955	120	0	*	1	1610	195	0	*	1	2225	270	0					0
1	0345	46	0	*	1	1000	121	0	*	1	1615	196	0	*	1	2230	271	0					0
1	0350	47	0	*	1	1005	122	0	*	1	1620	197	0	*	1	2235	272	0					0
1	0355	48	0	*	1	1010	123	0	*	1	1625	198	0	*	1	2240	273	0					0
1	0400	49	0	*	1	1015	124	0	*	1	1630	199	0	*	1	2245	274	0					0
1	0405	50	0	*	1	1020	125	0	*	1	1635	200	0	*	1	2250	275	0					0
1	0410	51	0	*	1	1025	126	0	*	1	1640	201	0	*	1	2255	276	0					0
1	0415	52	0	*	1	1030	127	0	*	1	1645	202	0	*	1	2300	277	0					0
1	0420	53	0	*	1	1035	128	0	*	1	1650	203	0	*	1	2305	278	0					0
1	0425	54	0	*	1	1040	129	0	*	1	1655	204	0	*	1	2310	279	0					0

1	0430	55	0	*	1	1045	110	0	*	1	1700	205	0	*	1	2115	200	0
1	0435	56	0	*	1	1050	111	0	*	1	1705	206	0	*	1	2120	201	0
1	0440	57	0	*	1	1055	112	0	*	1	1710	207	0	*	1	2125	202	0
1	0445	58	0	*	1	1100	113	0	*	1	1715	208	0	*	1	2130	203	0
1	0450	59	0	*	1	1105	114	0	*	1	1720	209	0	*	1	2135	204	0
1	0455	60	0	*	1	1110	115	0	*	1	1725	210	0	*	1	2140	205	0
1	0500	61	0	*	1	1115	116	0	*	1	1730	211	0	*	1	2145	206	0
1	0505	62	0	*	1	1120	117	0	*	1	1735	212	0	*	1	2150	207	0
1	0510	63	0	*	1	1125	118	0	*	1	1740	213	0	*	1	2155	208	0
1	0515	64	0	*	1	1130	119	0	*	1	1745	214	0	*	1	0000	209	0
1	0520	65	0	*	1	1135	120	0	*	1	1750	215	0	*	1	0005	290	0
1	0525	66	0	*	1	1140	121	0	*	1	1755	216	0	*	1	0010	291	0
1	0530	67	0	*	1	1145	122	0	*	1	1800	217	0	*	1	0015	292	0
1	0535	68	0	*	1	1150	123	0	*	1	1805	218	0	*	1	0020	293	0
1	0540	69	0	*	1	1155	124	0	*	1	1810	219	0	*	1	0025	294	0
1	0545	70	0	*	1	1200	125	0	*	1	1815	220	0	*	1	0030	295	0
1	0550	71	0	*	1	1205	126	0	*	1	1820	221	0	*	1	0035	296	0
1	0555	72	0	*	1	1210	127	0	*	1	1825	222	0	*	1	0040	297	0
1	0600	73	0	*	1	1215	128	0	*	1	1830	223	0	*	1	0045	298	0
1	0605	74	0	*	1	1220	129	0	*	1	1835	224	0	*	1	0050	299	0
1	0610	75	0	*	1	1225	130	0	*	1	1840	225	0	*	1	0055	300	0

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24-92-HR
237	3 08	1	1	1	1
		(INCRESE)	(INCRESE)	(INCRESE)	(INCRESE)
		074	074	074	074
		2	2	2	2
		CUMULATIVE AREA = 51 SQ MI			

# HYDROGRAPH AT STATION 0+500

DA MON HRRM	ORD	FLOW	DA MON HRRM	ORD	FLOW	DA MON HRRM	ORD	FLOW	DA MON HRRM	ORD	FLOW
1	0000	1	0	1	0615	75	0	1	1830	151	0
1	0005	2	0	1	0620	77	0	1	1835	152	0
1	0010	3	0	1	0625	78	0	1	1840	153	0
1	0015	4	0	1	0630	79	0	1	1845	154	0
1	0020	5	0	1	0635	80	0	1	1850	155	0
1	0025	6	0	1	0640	81	0	1	1855	156	0
1	0030	7	0	1	0645	82	0	1	1900	157	0
1	0035	8	0	1	0650	83	0	1	1905	158	0
1	0040	9	0	1	0655	84	0	1	1910	159	0
1	0045	10	0	1	0700	85	0	1	1915	160	0
1	0050	11	0	1	0705	86	0	1	1920	161	0
1	0055	12	0	1	0710	87	0	1	1925	162	0
1	0100	13	0	1	0715	88	0	1	1930	163	0
1	0105	14	0	1	0720	89	0	1	1935	164	0
1	0110	15	0	1	0725	90	0	1	1940	165	0
1	0115	16	0	1	0730	91	0	1	1945	166	0
1	0120	17	0	1	0735	92	0	1	1950	167	0
1	0125	18	0	1	0740	93	0	1	1955	168	0
1	0130	19	0	1	0745	94	0	1	2000	169	0
1	0135	20	0	1	0750	95	0	1	2005	170	0
1	0140	21	0	1	0755	96	0	1	2010	171	0
1	0145	22	0	1	0800	97	0	1	2015	172	0
1	0150	23	0	1	0805	98	0	1	2020	173	0
1	0155	24	0	1	0810	99	0	1	2025	174	0
1	0200	25	0	1	0815	100	0	1	2030	175	0
1	0205	26	0	1	0820	101	0	1	2035	176	0
1	0210	27	0	1	0825	102	0	1	2040	177	0
1	0215	28	0	1	0830	103	0	1	2045	178	0
1	0220	29	0	1	0835	104	0	1	2050	179	0
1	0225	30	0	1	0840	105	0	1	2055	180	0
1	0230	31	0	1	0845	106	0	1	2100	181	0
1	0235	32	0	1	0850	107	0	1	2105	182	0
1	0240	33	0	1	0855	108	0	1	2110	183	0
1	0245	34	0	1	0900	109	0	1	2115	184	0
1	0250	35	0	1	0905	110	0	1	2120	185	0
1	0255	36	0	1	0910	111	0	1	2125	186	0
1	0300	37	0	1	0915	112	0	1	2130	187	0
1	0305	38	0	1	0920	113	0	1	2135	188	0
1	0310	39	0	1	0925	114	0	1	2140	189	0
1	0315	40	0	1	0930	115	0	1	2145	190	0
1	0320	41	0	1	0935	116	0	1	2150	191	0
1	0325	42	0	1	0940	117	0	1	2155	192	0
1	0330	43	0	1	0945	118	0	1	2200	193	0
1	0335	44	0	1	0950	119	0	1	2205	194	0
1	0340	45	0	1	0955	120	0	1	2210	195	0
1	0345	46	0	1	1000	121	0	1	2215	196	0
1	0350	47	0	1	1005	122	0	1	2220	197	0
1	0355	48	0	1	1010	123	0	1	2225	198	0
1	0400	49	0	1	1015	124	0	1	2230	199	0
1	0405	50	0	1	1020	125	0	1	2235	200	0
1	0410	51	0	1	1025	126	0	1	2240	201	0
1	0415	52	0	1	1030	127	0	1	2245	202	0
1	0420	53	0	1	1035	128	0	1	2250	203	0
1	0425	54	0	1	1040	129	0	1	2255	204	0
1	0430	55	0	1	1045	130	0	1	2300	205	0
1	0435	56	0	1	1050	131	0	1	2305	206	0
1	0440	57	0	1	1055	132	0	1	2310	207	0
1	0445	58	0	1	1100	133	0	1	2315	208	0
1	0450	59	0	1	1105	134	0	1	2320	209	0
1	0455	60	0	1	1110	135	0	1	2325	210	0
1	0500	61	0	1	1115	136	0	1	2330	211	0



1	0505	62	0	*	1	1120	137	0	*	1	1735	212	0	*	1	2150	267	0
1	0510	63	0	*	1	1125	138	0	*	1	1740	213	0	*	1	2155	268	0
1	0515	64	0	*	1	1130	139	0	*	1	1745	214	0	*	2	0000	269	0
1	0520	65	0	*	1	1135	140	0	*	1	1750	215	0	*	2	0005	270	0
1	0525	66	0	*	1	1140	141	0	*	1	1755	216	0	*	2	0010	271	0
1	0530	67	0	*	1	1145	142	0	*	1	1800	217	0	*	2	0015	272	0
1	0535	68	0	*	1	1150	143	0	*	1	1805	218	0	*	2	0020	273	0
1	0540	69	0	*	1	1155	144	0	*	1	1810	219	0	*	2	0025	274	0
1	0545	70	0	*	1	1200	145	0	*	1	1815	220	0	*	2	0030	275	0
1	0550	71	0	*	1	1205	146	0	*	1	1820	221	0	*	2	0035	276	0
1	0555	72	0	*	1	1210	147	0	*	1	1825	222	0	*	2	0040	277	0
1	0600	73	0	*	1	1215	148	0	*	1	1830	223	0	*	2	0045	278	0
1	0605	74	0	*	1	1220	149	0	*	1	1835	224	0	*	2	0050	279	0
1	0610	75	0	*	1	1225	150	0	*	1	1840	225	0	*	2	0055	280	0

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	24-72-HR
109	3 17	15 (INCHES) (AC-FT)	4 271 7	4 271 7	4 271 7
CUMULATIVE AREA ~		.51 SQ MI			

633 RK CS403 COMBINE

634 RD OUTPUT CONTROL VARIABLES

IPRNT	1	PRINT CONTROL
IPLOT	0	PLOT CONTROL
OSCAL	0	HYDROGRAPH PLOT SCALE
IPRCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	100	LAST ORDINATE PUNCHED OR SAVED
TIMEINT	.003	TIME INTERVAL IN HOURS

COMBINE PIPE FLOW, DIVERGED SURFACE FLOW AND REMAINING SURFACE FLOW

636 HC HYDROGRAPH COMBINATION

ICOMP	3	NUMBER OF HYDROGRAPHS TO COMBINE
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# HYDROGRAPH AT STATION CS403 (SUM OF 3 HYDROGRAPHS)

DA	HR	MIN	SEC	FLOW	DA	HR	MIN	SEC	FLOW	DA	HR	MIN	SEC	FLOW	DA	HR	MIN	SEC	FLOW
1	0000	1	0	0	1	0615	26	3	0	1	1230	151	0	0	1	1815	276	0	0
1	0005	2	0	0	1	0620	27	2	0	1	1235	152	0	0	1	1820	277	0	0
1	0010	3	0	0	1	0625	28	2	0	1	1240	153	0	0	1	1825	278	0	0
1	0015	4	0	0	1	0630	29	1	0	1	1245	154	0	0	1	1830	279	0	0
1	0020	5	1	0	1	0635	30	1	0	1	1250	155	0	0	1	1835	280	0	0
1	0025	6	1	0	1	0640	31	1	0	1	1255	156	0	0	1	1840	281	0	0
1	0030	7	2	0	1	0645	32	1	0	1	1300	157	0	0	1	1845	282	0	0
1	0035	8	2	0	1	0650	33	1	0	1	1305	158	0	0	1	1850	283	0	0
1	0040	9	1	0	1	0655	34	1	0	1	1310	159	0	0	1	1855	284	0	0
1	0045	10	1	0	1	0700	35	0	0	1	1315	160	0	0	1	1900	285	0	0
1	0050	11	1	0	1	0705	36	0	0	1	1320	161	0	0	1	1905	286	0	0
1	0055	12	1	0	1	0710	37	0	0	1	1325	162	0	0	1	1910	287	0	0
1	0100	13	5	0	1	0715	38	0	0	2	1330	163	0	0	2	1915	288	0	0
1	0105	14	5	0	1	0720	39	0	0	1	1335	164	0	0	1	1920	289	0	0
1	0110	15	5	0	1	0725	40	0	0	1	1340	165	0	0	1	1925	290	0	0
1	0115	16	5	0	1	0730	41	0	0	1	1345	166	0	0	1	1930	291	0	0
1	0120	17	5	0	1	0735	42	0	0	1	1350	167	0	0	1	1935	292	0	0
1	0125	18	6	0	1	0740	43	0	0	1	1355	168	0	0	1	1940	293	0	0
1	0130	19	6	0	1	0745	44	0	0	1	1400	169	0	0	1	1945	294	0	0
1	0135	20	6	0	1	0750	45	0	0	1	1405	170	0	0	1	1950	295	0	0
1	0140	21	6	0	1	0755	46	0	0	1	1410	171	0	0	1	1955	296	0	0
1	0145	22	7	0	1	0800	47	0	0	1	1415	172	0	0	1	2000	297	0	0
1	0150	23	7	0	1	0805	48	0	0	1	1420	173	0	0	1	2005	298	0	0
1	0155	24	7	0	1	0810	49	0	0	1	1425	174	0	0	1	2010	299	0	0
1	0200	25	8	0	1	0815	50	0	0	1	1430	175	0	0	1	2015	300	0	0
1	0205	26	8	0	1	0820	51	0	0	1	1435	176	0	0	1	2020	301	0	0
1	0210	27	9	0	1	0825	52	0	0	1	1440	177	0	0	1	2025	302	0	0
1	0215	28	10	0	1	0830	53	0	0	1	1445	178	0	0	1	2030	303	0	0
1	0220	29	10	0	1	0835	54	0	0	1	1450	179	0	0	1	2035	304	0	0
1	0225	30	11	0	1	0840	55	0	0	1	1455	180	0	0	1	2040	305	0	0
1	0230	31	11	0	1	0845	56	0	0	1	1500	181	0	0	1	2045	306	0	0
1	0235	32	10	0	1	0850	57	0	0	1	1505	182	0	0	1	2050	307	0	0
1	0240	33	20	0	1	0855	58	0	0	1	1510	183	0	0	2	2055	308	0	0
1	0245	34	39	0	1	0900	59	0	0	1	1515	184	0	0	1	2100	309	0	0
1	0250	35	57	0	1	0905	100	0	0	1	1520	185	0	0	1	2105	310	0	0
1	0255	36	74	0	1	0910	101	0	0	1	1525	186	0	0	1	2110	311	0	0
1	0300	37	99	0	1	0915	102	0	0	1	1530	187	0	0	1	2115	312	0	0
1	0305	38	156	0	1	0920	103	0	0	1	1535	188	0	0	2	2120	313	0	0
1	0310	39	229	0	1	0925	104	0	0	1	1540	189	0	0	1	2125	314	0	0

1	0315	40	219	*	1	0910	115	0	*	1	1545	190	0	*	1	2200	265	0
1	0320	41	161	*	1	0915	116	0	*	1	1550	191	0	*	1	2205	266	0
1	0325	42	111	*	1	0940	117	0	*	1	1555	192	0	*	1	2210	267	0
1	0330	43	112	*	1	0945	118	0	*	1	1600	193	0	*	1	2215	268	0
1	0335	44	90	*	1	0950	119	0	*	1	1605	194	0	*	1	2220	269	0
1	0340	45	68	*	1	0955	120	0	*	1	1610	195	0	*	1	2225	270	0
1	0345	46	51	*	1	1000	121	0	*	1	1615	196	0	*	1	2230	271	0
1	0350	47	40	*	1	1005	122	0	*	1	1620	197	0	*	1	2235	272	0
1	0355	48	33	*	1	1010	123	0	*	1	1625	198	0	*	1	2240	273	0
1	0400	49	27	*	1	1015	124	0	*	1	1630	199	0	*	1	2245	274	0
1	0405	50	22	*	1	1020	125	0	*	1	1635	200	0	*	1	2250	275	0
1	0410	51	20	*	1	1025	126	0	*	1	1640	201	0	*	1	2255	276	0
1	0415	52	18	*	1	1030	127	0	*	1	1645	202	0	*	1	2300	277	0
1	0420	53	16	*	1	1035	128	0	*	1	1650	203	0	*	1	2305	278	0
1	0425	54	14	*	1	1040	129	0	*	1	1655	204	0	*	1	2310	279	0
1	0430	55	12	*	1	1045	130	0	*	1	1700	205	0	*	1	2315	280	0
1	0435	56	11	*	1	1050	131	0	*	1	1705	206	0	*	1	2320	281	0
1	0440	57	9	*	1	1055	132	0	*	1	1710	207	0	*	1	2325	282	0
1	0445	58	8	*	1	1100	133	0	*	1	1715	208	0	*	1	2330	283	0
1	0450	59	7	*	1	1105	134	0	*	1	1720	209	0	*	1	2335	284	0
1	0455	60	7	*	1	1110	135	0	*	1	1725	210	0	*	1	2340	285	0
1	0500	61	7	*	1	1115	136	0	*	1	1730	211	0	*	1	2345	286	0
1	0505	62	7	*	1	1120	137	0	*	1	1735	212	0	*	1	2350	287	0
2	0510	63	6	*	1	1125	138	0	*	1	1740	213	0	*	1	2355	288	0
1	0515	64	6	*	1	1130	139	0	*	1	1745	214	0	*	2	0000	289	0
1	0520	65	6	*	1	1135	140	0	*	1	1750	215	0	*	2	0005	290	0
1	0525	66	6	*	1	1140	141	0	*	1	1755	216	0	*	2	0010	291	0
1	0530	67	5	*	1	1145	142	0	*	1	1800	217	0	*	2	0015	292	0
1	0535	68	5	*	1	1150	143	0	*	1	1805	218	0	*	2	0020	293	0
1	0540	69	5	*	1	1155	144	0	*	1	1810	219	0	*	2	0025	294	0
1	0545	70	5	*	1	1200	145	0	*	1	1815	220	0	*	2	0030	295	0
1	0550	71	5	*	1	1205	146	0	*	1	1820	221	0	*	2	0035	296	0
1	0555	72	5	*	1	1210	147	0	*	1	1825	222	0	*	2	0040	297	0
1	0600	73	5	*	1	1215	148	0	*	1	1830	223	0	*	2	0045	298	0
1	0605	74	4	*	1	1220	149	0	*	1	1835	224	0	*	2	0050	299	0
1	0610	75	3	*	1	1225	150	0	*	1	1840	225	0	*	2	0055	300	0

PEAK FLOW	TIME	6-HR	24-HR	72-HR	21 92-HR
(CFS)	(HR)				
339	3 17	30	7	7	7
	(INCHES)	1.540	1.544	544	514
	(AC FT)	15	15	15	15
CUMULATIVE AREA =		.51 SQ MI			

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632 KK  
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638 KD OUTPUT CONTROL VARIABLES  
 IPHRT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCALE 0. HYDROGRAPH PLOT SCALE  
 ROUTE DIVERTED FLOW THROUGH OFFLINE BASIN CONCEPT MAX H = 5.9  
 ASSUMED 1000' X 80' BASIN WITH 5:1 SIDE SLOPES & 16" OUTLET  
 21" BLEED-OFF PIPE PLUS 20' WIDE SPILLWAY AT 3.6'

# HYDROGRAPH ROUTING DATA

642 RS	STORAGE ROUTING	1	NUMBER OF SUBREACHES															
	ISTPS	STOR	TYPE OF INITIAL CONDITION															
	REVRIC	1.00	INITIAL CONDITION															
	X	00	WORKING R AND D COEFFICIENT															
643 SV	STORAGE	0	0	1	2	1.8	3.0	1.5	5.3	5.5	5.0							
		6.2																
645 SE	ELEVATION	00	80	1.00	2.00	3.00	4.00	5.00	6.40	5.60	5.80							
		6.00																
647 SL	LOW-LEVEL OUTLET	1.00	ELEVATION AT CENTER OF OUTLET															
	FLCPL	3.14	CROSS-SECTIONAL AREA															
	COOL	62	COEFFICIENT															
	EXPL	50	EXPONENT OF HEAD															
648 SS	SPILLWAY	3.80	SPILLWAY CREST ELEVATION															
	SPWID	20.00	SPILLWAY WIDTH															
	COOW	2.80	WEIR COEFFICIENT															
	EXPR	1.50	EXPONENT OF HEAD															

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# COMPUTED OUTFLOW-ELEVATION DATA

OUTFLOW	00	00	15.21	15.18	17.27	18.53	19.98	21.48	23.10	24.13								
ELEVATION	00	1.00	1.95	2.07	2.22	2.41	2.54	2.93	3.30	3.90								
OUTFLOW	26.75	28.09	31.54	41.68	54.26	72.26	96.63	128.34	168.16	217.65								
ELEVATION	3.84	2.92	4.03	4.19	4.39	4.63	4.91	5.23	5.60	6.00								



1	0640	81	7.	.5	1.4	*	1	1500	181	0.	.1	1.0	*	1	2320	281	0.	.1	1.0
1	0645	82	6.	.4	1.4	*	1	1505	182	0.	.1	1.0	*	1	2325	282	0.	.1	1.0
1	0650	83	5	.4	1.3	*	1	1510	183	0.	.1	1.0	*	1	2330	283	0.	.1	1.0
1	0655	84	5	.4	1.3	*	1	1515	184	0.	.1	1.0	*	1	2335	284	0.	.1	1.0
1	0700	85	4	.3	1.3	*	1	1520	185	0.	.1	1.0	*	1	2340	285	0.	.1	1.0
1	0705	86	4.	.3	1.2	*	1	1525	186	0.	.1	1.0	*	1	2345	286	0.	.1	1.0
1	0710	87	3.	.3	1.2	*	1	1530	187	0.	.1	1.0	*	1	2350	287	0.	.1	1.0
1	0715	88	3.	.3	1.2	*	1	1535	188	0.	.1	1.0	*	1	2355	288	0.	.1	1.0
1	0720	89	2.	.2	1.1	*	1	1540	189	0.	.1	1.0	*	1	0000	289	0.	.1	1.0
1	0725	90	2.	.2	1.1	*	1	1545	190	0.	.1	1.0	*	1	0005	290	0.	.1	1.0
1	0730	91	2.	.2	1.1	*	1	1550	191	0.	.1	1.0	*	1	0010	291	0.	.1	1.0
1	0735	92	2.	.2	1.1	*	1	1555	192	0.	.1	1.0	*	1	0015	292	0.	.1	1.0
1	0740	93	1.	.2	1.1	*	1	1600	193	0.	.1	1.0	*	1	0020	293	0.	.1	1.0
1	0745	94	1.	.2	1.1	*	1	1605	194	0.	.1	1.0	*	1	0025	294	0.	.1	1.0
1	0750	95	1.	.2	1.1	*	1	1610	195	0.	.1	1.0	*	1	0030	295	0.	.1	1.0
1	0755	96	1.	.2	1.1	*	1	1615	196	0.	.1	1.0	*	1	0035	296	0.	.1	1.0
1	0800	97	1.	.2	1.1	*	1	1620	197	0.	.1	1.0	*	1	0040	297	0.	.1	1.0
1	0805	98	1.	.2	1.0	*	1	1625	198	0.	.1	1.0	*	1	0045	298	0.	.1	1.0
1	0810	99	1.	.2	1.0	*	1	1630	199	0.	.1	1.0	*	1	0050	299	0.	.1	1.0
1	0815	100	1.	.2	1.0	*	1	1635	200	0.	.1	1.0	*	1	0055	300	0.	.1	1.0

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24.92-HR
159.	1.43	29	7.	1	7.
		(INCHES)	537	539	539
		(AC-FT)	14	15.	15.
PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)	6-HR	24-HR	72-HR	24.92-HR
5.	1.43	7	1	1	1
PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
(FEET)	(HR)	6-HR	24-HR	72-HR	24.92-HR
5.57	1.43	2.64	1.47	1.40	1.40
CUMULATIVE AREA		.51 SQ MI			

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*****
649 KA * 133E.1 *
*****

650 KO OUTPUT CONTROL VARIABLES
      1 PRINT CONTROL
      1 PLOT CONTROL
      0 PLOT CONTROL
      0. HYDROGRAPH PLOT SCALE
      DIVIDE THE FLOW INTO TWO ADJUT CULVERTS

DT DIVERSION
  1STAD 033C.2 DIVERSION HYDROGRAPH IDENTIFICATION

DI INFLOW 00 100.00 700.00 400.00 600.00

DQ DIVERTED FLOW .00 68.00 136.00 272.00 408.00

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DIVERSION HYDROGRAPH 033C.2																		
DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	
1	0000	1	0.	*	1	0615	76	9.	*	1	1230	154	0.	*	1	1815	226	0.
1	0005	2	0.	*	1	0620	77	0.	*	1	1235	152	0.	*	1	1850	227	0.
1	0010	3	0.	*	1	0625	78	7	*	1	1240	153	0	*	1	1855	228	0.
1	0015	4	0.	*	1	0630	79	6	*	1	1245	154	0.	*	1	1900	229	0.
1	0020	5	0.	*	1	0635	80	5.	*	1	1250	155	0.	*	1	1905	230	0
1	0025	6	0	*	1	0640	81	5	*	1	1255	156	0	*	1	1910	231	0.
1	0030	7	0	*	1	0645	82	4	*	1	1300	157	0.	*	1	1915	232	0.
1	0035	8	0	*	1	0650	83	4.	*	1	1305	158	0.	*	1	1920	233	0
1	0040	9	0	*	1	0655	84	3.	*	1	1310	159	0	*	1	1925	234	0
1	0045	10	0.	*	1	0700	85	3	*	1	1315	160	0.	*	1	1930	235	0.
1	0050	11	0.	*	1	0705	86	2.	*	1	1320	161	0.	*	1	1935	236	0.
1	0055	12	0.	*	1	0710	87	2	*	1	1325	162	0.	*	1	1940	237	0.
1	0100	13	0.	*	1	0715	88	2.	*	1	1330	163	0.	*	1	1945	238	0.
1	0105	14	1.	*	1	0720	89	2.	*	1	1335	164	0	*	1	1950	239	0.
1	0110	15	2.	*	1	0725	90	1	*	1	1340	165	0	*	1	1955	240	0.
1	0115	16	1.	*	1	0730	91	1.	*	1	1345	166	0.	*	1	2000	241	0.
1	0120	17	2.	*	1	0735	92	1	*	1	1350	167	0	*	1	2005	242	0.
1	0125	18	2.	*	1	0740	93	1.	*	1	1355	168	0	*	1	2010	243	0.
1	0130	19	2.	*	1	0745	94	1.	*	1	1400	169	0	*	1	2015	244	0.
1	0135	20	3.	*	1	0750	95	1.	*	1	1405	170	0.	*	1	2020	245	0.
1	0140	21	3.	*	1	0755	96	1.	*	1	1410	171	0.	*	1	2025	246	0
1	0145	22	3.	*	1	0800	97	1.	*	1	1415	172	0.	*	1	2030	247	0.
1	0150	23	3	*	1	0805	98	1.	*	1	1420	173	0.	*	1	2035	248	0.
1	0155	24	3.	*	1	0810	99	0.	*	1	1425	174	0.	*	1	2040	249	0.
1	0200	25	4	*	1	0815	100	0	*	1	1430	175	0.	*	1	2045	250	0.
1	0205	26	4	*	1	0820	101	0.	*	1	1435	176	0.	*	1	2050	251	0.

[illegible]

1	0245	34	5.	*	1	0900	109	0.	*	1	1515	104	0.	*	1	2130	259	0.
1	0250	35	5.	*	1	0905	110	0.	*	1	1520	185	0.	*	1	2135	260	0.
1	0255	36	6.	*	1	0910	111	0.	*	1	1525	186	0.	*	1	2140	261	0.
1	0300	37	7.	*	1	0915	112	0.	*	1	1530	187	0.	*	1	2145	262	0.
1	0305	38	8.	*	1	0920	113	0.	*	1	1535	188	0.	*	1	2150	263	0.
1	0310	39	22.	*	1	0925	114	0.	*	1	1540	189	0.	*	1	2155	264	0.
1	0315	40	45.	*	1	0930	115	0.	*	1	1545	190	0.	*	1	2200	265	0.
1	0320	41	51.	*	1	0935	116	0.	*	1	1550	191	0.	*	1	2205	266	0.
1	0325	42	10.	*	1	0940	117	0.	*	1	1555	192	0.	*	1	2210	267	0.
1	0330	43	15.	*	1	0945	118	0.	*	1	1600	193	0.	*	1	2215	268	0.
1	0335	44	41.	*	1	0950	119	0.	*	1	1605	194	0.	*	1	2220	269	0.
1	0340	45	35.	*	1	0955	120	0.	*	1	1610	195	0.	*	1	2225	270	0.
1	0345	46	30.	*	1	1000	121	0.	*	1	1615	196	0.	*	1	2230	271	0.
1	0350	47	25.	*	1	1005	122	0.	*	1	1620	197	0.	*	1	2235	272	0.
1	0355	48	20.	*	1	1010	123	0.	*	1	1625	198	0.	*	1	2240	273	0.
1	0400	49	17.	*	1	1015	124	0.	*	1	1630	199	0.	*	1	2245	274	0.
1	0405	50	15.	*	1	1020	125	0.	*	1	1635	200	0.	*	1	2250	275	0.
1	0410	51	13.	*	1	1025	126	0.	*	1	1640	201	0.	*	1	2255	276	0.
1	0415	52	11.	*	1	1030	127	0.	*	1	1645	202	0.	*	1	2300	277	0.
1	0420	53	10.	*	1	1035	128	0.	*	1	1650	203	0.	*	1	2305	278	0.
1	0425	54	9.	*	1	1040	129	0.	*	1	1655	204	0.	*	1	2310	279	0.
1	0430	55	8.	*	1	1045	130	0.	*	1	1700	205	0.	*	1	2315	280	0.
1	0435	56	0.	*	1	1050	131	0.	*	1	1705	206	0.	*	1	2320	281	0.
1	0440	57	0.	*	1	1055	132	0.	*	1	1710	207	0.	*	1	2325	282	0.
1	0445	58	0.	*	1	1100	133	0.	*	1	1715	208	0.	*	1	2330	283	0.
1	0450	59	8.	*	1	1105	134	0.	*	1	1720	209	0.	*	1	2335	284	0.
1	0455	60	8.	*	1	1110	135	0.	*	1	1725	210	0.	*	1	2340	285	0.
1	0500	61	0.	*	1	1115	136	0.	*	1	1730	211	0.	*	1	2345	286	0.
1	0505	62	7.	*	1	1120	137	0.	*	1	1735	212	0.	*	1	2350	287	0.
1	0510	63	7.	*	1	1125	138	0.	*	1	1740	213	0.	*	1	2355	288	0.
1	0515	64	7.	*	1	1130	139	0.	*	1	1745	214	0.	*	2	0000	289	0.
1	0520	65	7.	*	1	1135	140	0.	*	1	1750	215	0.	*	2	0005	290	0.
1	0525	66	7.	*	1	1140	141	0.	*	1	1755	216	0.	*	2	0010	291	0.
1	0530	67	6.	*	1	1145	142	0.	*	1	1800	217	0.	*	2	0015	292	0.
1	0535	68	6.	*	1	1150	143	0.	*	1	1805	218	0.	*	2	0020	293	0.
1	0540	69	6.	*	1	1155	144	0.	*	1	1810	219	0.	*	2	0025	294	0.
1	0545	70	6.	*	1	1200	145	0.	*	1	1815	220	0.	*	2	0030	295	0.
1	0550	71	6.	*	1	1205	146	0.	*	1	1820	221	0.	*	2	0035	296	0.
1	0555	72	5.	*	1	1210	147	0.	*	1	1825	222	0.	*	2	0040	297	0.
1	0600	73	5.	*	1	1215	148	0.	*	1	1830	223	0.	*	2	0045	298	0.
1	0605	74	5.	*	1	1220	149	0.	*	1	1835	224	0.	*	2	0050	299	0.
1	0610	75	5.	*	1	1225	150	0.	*	1	1840	225	0.	*	2	0055	300	0.

PEAK FLOW TIME  
 (CFS) (HR)  
 51 3 33  
 (INCHES) 9. 7. 7. 7.  
 (AC-FT) 170 .172 .172 .172  
 5. 5. 5. 5.  
 CUMULATIVE AREA = .51 SQ MI

658 KK \*\*\*\*\*  
 \* 33: 1 \* COMBINE  
 \* \*\*\*\*\*  
 659 KO OUTPUT CONTROL VARIABLES  
 IPNT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 OSCAL 0. HYDROGRAPH PLOT SCALE  
 COMBINED DISCHARGE AT ADOT CULVERT 5 AND 6  
 661 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE  
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# HYDROGRAPH AT STATION 335.1 SUM OF 2 HYDROGRAPHS

DA	MON	HR:MN	ORD	FLOW	DA	MON	HR:MN	ORD	FLOW	DA	MON	HR:MN	ORD	FLOW	DA	MON	HR:MN	ORD	FLOW
1	0000	1	0.	*	1	0615	76	62.	*	1	1230	251	5.	*	1	1845	226	1.	1.
1	0005	2	0.	*	1	0620	77	59.	*	1	1235	152	5.	*	1	1850	227	1.	1.
1	0010	3	0.	*	1	0625	78	56.	*	1	1240	153	5.	*	1	1855	228	1.	1.
1	0015	4	0.	*	1	0630	79	53.	*	1	1245	154	5.	*	1	1900	229	1.	1.
1	0020	5	0.	*	1	0635	80	51.	*	1	1250	155	5.	*	1	1905	230	1.	1.
1	0025	6	1.	*	1	0640	81	48.	*	1	1255	156	5.	*	1	1910	231	1.	1.
1	0030	7	1.	*	1	0645	82	46.	*	1	1300	157	5.	*	1	1915	232	1.	1.
1	0035	8	2.	*	1	0650	83	44.	*	1	1305	158	5.	*	1	1920	233	1.	1.
1	0040	9	3.	*	1	0655	84	42.	*	1	1310	159	4.	*	1	1925	234	1.	1.
1	0045	10	4.	*	1	0700	85	40.	*	1	1315	160	4.	*	1	1930	235	1.	1.
1	0050	11	5.	*	1	0705	86	39.	*	1	1320	161	4.	*	1	1935	236	1.	1.
1	0055	12	6.	*	1	0710	87	37.	*	1	1325	162	4.	*	1	1940	237	1.	1.
1	0100	13	7.	*	1	0715	88	36.	*	1	1330	163	4.	*	1	1945	238	1.	1.
1	0105	14	7.	*	1	0720	89	34.	*	1	1335	164	4.	*	1	1950	239	1.	1.
1	0110	15	8.	*	1	0725	90	33.	*	1	1340	165	4.	*	1	1955	240	1.	1.
1	0115	16	9.	*	1	0730	91	32.	*	1	1345	166	4.	*	1	2000	241	1.	1.
1	0120	17	9.	*	1	0735	92	31.	*	2	1350	167	4.	*	1	2005	242	1.	1.

[illegible]



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COMPUTED KINEMATIC PARAMETERS  
VARIABLE TIME STEP  
(DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	N	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
RAIN	.98	1.43	1.15	1533.3	255.01	701.54	1.92	7.18

CONTINUITY SUMMARY (AC-FT) : INFLOW= 5700E+02 EXCESS= 0000E+00 OUTFLOW= 5203E+02 BASIN STORAGE= 2409E+01 PERCENT ERROR= 1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

DATA	98	1.43	1.00	251.70	700.00	1.92
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HYDROGRAPH AT STATION R33E 1

DA	MON	HRNN	ORD	FLOW	DA	MON	HRNN	ORD	FLOW	DA	MON	HRNN	ORD	FLOW	DA	MON	HRNN	ORD	FLOW
1	0000	1	0	*	1	0615	76	69	*	1	1230	151	6	*	1	1845	726	1.	
1	0005	2	0	*	1	0620	77	66	*	1	1235	152	6	*	1	1850	727	1.	
1	0010	3	0	*	1	0625	78	63	*	1	1240	153	6	*	1	1855	728	1.	
1	0015	4	0	*	1	0630	79	60	*	1	1245	154	6	*	1	1900	729	1	
1	0020	5	0	*	1	0635	80	57	*	1	1250	155	5	*	1	1905	730	1	
1	0025	6	0	*	1	0640	81	54	*	1	1255	156	5	*	1	1910	731	1	
1	0030	7	0	*	1	0645	82	51	*	1	1300	157	5	*	1	1915	732	1	
1	0035	8	0	*	1	0650	83	49	*	1	1305	158	5	*	1	1920	733	1	
1	0040	9	0	*	1	0655	84	47	*	1	1310	159	5	*	1	1925	734	1	
1	0045	10	0	*	1	0700	85	45	*	1	1315	160	5	*	1	1930	735	1	
1	0050	11	0	*	1	0705	86	43	*	1	1320	161	5	*	1	1935	736	1	
1	0055	12	0	*	1	0710	87	41	*	1	1325	162	5	*	1	1940	737	1	
1	0100	13	1	*	1	0715	88	40	*	1	1330	163	4	*	1	1945	738	1	
1	0105	14	2	*	1	0720	89	38	*	1	1335	164	4	*	1	1950	739	1	
1	0110	15	3	*	1	0725	90	37	*	1	1340	165	4	*	1	1955	740	1	
1	0115	16	5	*	1	0730	91	35	*	1	1345	166	4	*	1	2000	741	1	
1	0120	17	6	*	1	0735	92	34	*	1	1350	167	4	*	1	2005	742	1	
1	0125	18	7	*	1	0740	93	33	*	1	1355	168	4	*	1	2010	743	1	
1	0130	19	8	*	1	0745	94	31	*	1	1400	169	4	*	1	2015	744	1	
1	0135	20	9	*	1	0750	95	30	*	1	1405	170	4	*	1	2020	745	1	
1	0140	21	10	*	1	0755	96	29	*	1	1410	171	4	*	1	2025	746	1	
1	0145	22	10	*	1	0800	97	28	*	1	1415	172	4	*	1	2030	747	1	
1	0150	23	11	*	1	0805	98	27	*	1	1420	173	4	*	1	2035	748	1	
1	0155	24	12	*	1	0810	99	26	*	1	1425	174	3	*	1	2040	749	1	
1	0200	25	13	*	1	0815	100	25	*	1	1430	175	3	*	1	2045	750	1	
1	0205	26	14	*	1	0820	101	24	*	1	1435	176	3	*	1	2050	751	1	
1	0210	27	15	*	1	0825	102	23	*	1	1440	177	3	*	1	2055	752	1	
1	0215	28	16	*	1	0830	103	21	*	1	1445	178	3	*	1	2100	753	1	
1	0220	29	17	*	1	0835	104	21	*	1	1450	179	3	*	1	2105	754	1	
1	0225	30	18	*	1	0840	105	21	*	1	1455	180	3	*	1	2110	755	1	
1	0230	31	19	*	1	0845	106	21	*	1	1500	181	3	*	1	2115	756	1	
1	0235	32	21	*	1	0850	107	20	*	1	1505	182	3	*	1	2120	757	2	
1	0240	33	22	*	1	0855	108	20	*	1	1510	183	3	*	1	2125	758	1	
1	0245	34	26	*	1	0900	109	19	*	1	1515	184	3	*	1	2130	759	1	
1	0250	35	32	*	1	0905	110	19	*	1	1520	185	3	*	1	2135	760	1	
1	0255	36	45	*	1	0910	111	18	*	1	1525	186	3	*	1	2140	761	1	
1	0300	37	61	*	1	0915	112	17	*	1	1530	187	3	*	1	2145	762	1	
1	0305	38	73	*	1	0920	113	17	*	1	1535	188	3	*	1	2150	763	1	
1	0310	39	106	*	1	0925	114	16	*	1	1540	189	3	*	1	2155	764	1	
1	0315	40	130	*	1	0930	115	16	*	1	1545	190	3	*	1	2200	765	1	
1	0320	41	152	*	1	0935	116	15	*	1	1550	191	3	*	1	2205	766	1	
1	0325	42	162	*	1	0940	117	15	*	1	1555	192	3	*	1	2210	767	0	
1	0330	43	163	*	1	0945	118	15	*	1	1600	193	3	*	1	2215	768	0	
1	0335	44	173	*	1	0950	119	14	*	1	1605	194	3	*	1	2220	769	0	
1	0340	45	172	*	1	0955	120	14	*	1	1610	195	2	*	1	2225	770	0	
1	0345	46	197	*	1	1000	121	13	*	1	1615	196	2	*	1	2230	771	0	
1	0350	47	197	*	1	1005	122	13	*	1	1620	197	2	*	1	2235	772	0	
1	0355	48	177	*	1	1010	123	13	*	1	1625	198	2	*	1	2240	773	0	
1	0400	49	165	*	1	1015	124	12	*	1	1630	199	2	*	1	2245	774	0	
1	0405	50	156	*	1	1020	125	12	*	1	1635	200	2	*	1	2250	775	0	
1	0410	51	140	*	1	1025	126	12	*	1	1640	201	2	*	1	2255	776	0	
1	0415	52	142	*	1	1030	127	11	*	1	1645	202	2	*	1	2300	777	0	
1	0420	53	137	*	1	1035	128	11	*	1	1650	203	2	*	1	2305	778	0	
1	0425	54	132	*	1	1040	129	11	*	1	1655	204	2	*	1	2310	779	0	
1	0430	55	128	*	1	1045	130	10	*	1	1700	205	2	*	1	2315	780	0	
1	0435	56	121	*	1	1050	131	10	*	1	1705	206	2	*	1	2320	781	0	
1	0440	57	121	*	1	1055	132	10	*	1	1710	207	2	*	1	2325	782	0	
1	0445	58	118	*	1	1100	133	10	*	1	1715	208	2	*	1	2330	783	0	
1	0450	59	115	*	1	1105	134	9	*	1	1720	209	2	*	1	2335	784	0	
1	0455	60	112	*	1	1110	135	9	*	1	1725	210	2	*	1	2340	785	0	
1	0500	61	108	*	1	1115	136	9	*	1	1730	211	2	*	1	2345	786	0	
1	0505	62	104	*	1	1120	137	9	*	1	1735	212	2	*	1	2350	787	0	
1	0510	63	102	*	1	1125	138	8	*	1	1740	213	2	*	1	2355	788	0	
1	0515	64	99	*	1	1130	139	8	*	1	1745	214	2	*	1	0000	789	0	
1	0520	65	96	*	1	1135	140	8	*	1	1750	215	1	*	2	0005	790	0	
1	0525	66	93	*	1	1140	141	8	*	1	1755	216	1	*	2	0010	791	0	
1	0530	67	90	*	1	1145	142	8	*	1	1800	217	1	*	2	0015	792	0	
1	0535	68	87	*	1	1150	143	7	*	1	1805	218	1	*	2	0020	793	0	
1	0540	69	85	*	1	1155	144	7	*	1	1810	219	1	*	2	0025	794	0	
1	0545	70	82	*	1	1200	145	7	*	1	1815	220	1	*	2	0030	795	0	
1	0550	71	80	*	1	1205	146	7	*	1	1820	221	1	*	2	0035	796	0	
1	0555	72	78	*	1	1210	147	7	*	1	1825	222	1	*	2	0040	797	0	
1	0600	73	75	*	1	1215	148	6	*	1	1830	223	1	*	2	0045	798	0	
1	0605	74	73	*	1	1220	149	6	*	1	1835	224	1	*	2	0050	799	0	
1	0610	75	71	*	1	1225	150	6	*	1	1840	225	1	*	2	0055	800	0	

```

.....
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
(CFS)          (HR)      6-HR      24-HR      72-HR      74 72-HR
*      252      3 33      (CFS)      91      76      75      24
      (INCHES)  1 655      1 916      1 916      1 916
      (AC-FT)   15.      52      52      52
      CUMULATIVE AREA = 51 50 MI

```

```

*****
670 KK      ASLO      SUB
*****

671 KO      OUTPUT CONTROL VARIABLES
      PRINT      1 PRINT CONTROL
      PLOT      0 PLOT CONTROL
      OSCAL      0 HYDROGRAPH PLOT SCALE
      ASLO PARCEL EAST OF SCOTTSDALE ROAD

```

SUBBASIN RUNOFF DATA

```

672 BA      SUBBASIN CHARACTERISTICS
      TAREA      05 SUBBASIN AREA

```

PRECIPITATION DATA

```

24 PH      DEPTHS FOR 0 PERCENT HYPOTHETICAL STORM
      HYDRO-15      TP-40
      5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 3-DAY 7-DAY 10-DAY
      76 1.50 2.55 2.83 2.88 3.33 00 00 00 00 00
      STORM AREA = 11 00

```

```

674 LS      SOIL LOSS RATE
      STRPL      60 INITIAL ABSTRACTION
      CHNBR      11.00 CURVE NUMBER
      RTIME      00 PERCENT IMPERVIOUS AREA

```

```

675 UX      KINEMATIC WAVE
      OVERLAND FLOW ELEMENT NO 1
      L      60 OVERLAND FLOW LENGTH
      S      0211 SLOPE
      N      .100 ROUGHNESS COEFFICIENT
      CA      100.0 PERCENT OF SUBBASIN
      DYNIN      5 MINIMUM NUMBER OF DX INTERVALS

```

```

676 RK      KINEMATIC WAVE
      RATH CHANNEL
      L      2100 CHANNEL LENGTH
      S      0088 SLOPE
      N      050 CHANNEL ROUGHNESS COEFFICIENT
      CA      05 CONTRIBUTING AREA
      SHAPE      TRAP CHANNEL SHAPE
      SD      12 00 BOTTOM WIDTH OR DIAMETER
      Z      5 00 SIDE SLOPE
      RDXMIN      2 MINIMUM NUMBER OF DX INTERVALS
      RUPSTQ      NO ROUTE UPSTREAM HYDROGRAPH

```

\*\*\*
COMPUTED KINEMATIC PARAMETERS
VARIABLE TIME STEP
(OF SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO	VOLUME	MAXIMUM
			(MIN)	(FT)	(CFS)	PEAK	(IN)	CCELERITY
						(MIN)		(FPS)
PLANE1	2 17	1 67	35	17 80	123.41	105 05	1 23	19
MAIN	33	1 43	1 70	525 00	91 71	190 76	1 22	5 16

CONTINUITY SUMMARY (AC-FT) : INFLOW= 0009+00 EXCESS= 3491E+01 OUTFLOW= 3478E+01 BASIN STORAGE= 2007E+01 PERCENT ERROR= 4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	98	1 13	5 00	39 79	190 00	1 71
------	----	------	------	-------	--------	------

HYDROGRAPH AT STATION ASLO

DA	MON	HR	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HR	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	00	00	00	0	*	1	1230	151	00	00	00	0	0
1	0005	2	01	01	00	0	*	1	1235	152	00	00	00	0	0
1	0010	3	01	01	00	0	*	1	1240	151	00	00	00	0	0
1	0015	4	01	01	00	0	*	1	1245	151	00	00	00	0	0
1	0020	5	01	01	00	0	*	1	1250	155	00	00	00	0	0

1	6025	6	01	01	00	0	*	1	1255	156	00	00	00	0
1	6030	7	01	01	00	0	*	1	1300	157	00	00	00	0
1	6035	8	01	01	00	0	*	1	1305	158	00	00	00	0
1	6040	9	01	01	00	0	*	1	1110	159	00	00	00	0
1	6045	10	01	01	00	0	*	1	1315	160	00	00	00	0
1	6050	11	01	01	00	0	*	1	1320	161	00	00	00	0
1	6055	12	01	01	00	0	*	1	1325	162	00	00	00	0
1	6100	13	01	01	00	0	*	1	1330	163	00	00	00	0
1	6105	14	01	01	00	0	*	1	1335	164	00	00	00	0
1	6110	15	01	01	00	0	*	1	1340	165	00	00	00	0
1	6115	16	01	01	00	0	*	1	1345	166	00	00	00	0
1	6120	17	01	01	00	0	*	1	1350	167	00	00	00	0
1	6125	18	01	01	00	0	*	1	1355	168	00	00	00	0
1	6130	19	01	01	00	0	*	1	1400	169	00	00	00	0
1	6135	20	01	01	00	0	*	1	1405	170	00	00	00	0
1	6140	21	01	01	00	0	*	1	1410	171	00	00	00	0
1	6145	22	02	02	00	0	*	1	1415	172	00	00	00	0
1	6150	23	02	02	00	0	*	1	1420	173	00	00	00	0
1	6155	24	02	02	00	0	*	1	1425	174	00	00	00	0
1	6200	25	02	02	00	0	*	1	1430	175	00	00	00	0
1	6205	26	02	02	00	0	*	1	1435	176	00	00	00	0
1	6210	27	02	02	00	0	*	1	1440	177	00	00	00	0
1	6215	28	02	02	00	0	*	1	1445	178	00	00	00	0
1	6220	29	02	02	00	0	*	1	1450	179	00	00	00	0
1	6225	30	03	03	00	0	*	1	1455	180	00	00	00	0
1	6230	31	03	03	00	0	*	1	1500	181	00	00	00	0
1	6235	32	08	08	00	0	*	1	1505	182	00	00	00	0
1	6240	33	09	09	00	0	*	1	1510	183	00	00	00	0
1	6245	34	10	10	00	0	*	1	1515	184	00	00	00	0
1	6250	35	11	11	01	0	*	1	1520	185	00	00	00	0
1	6255	36	12	12	01	0	*	1	1525	186	00	00	00	0
1	6300	37	10	28	12	5	*	1	1530	187	00	00	00	0
1	6305	38	09	16	11	17	*	1	1535	188	00	00	00	0
1	6310	39	08	16	10	20	*	1	1540	189	00	00	00	0
1	6315	40	15	06	09	69	*	1	1545	190	00	00	00	0
1	6320	41	11	01	07	17	*	1	1550	191	00	00	00	0
1	6325	42	09	01	06	15	*	1	1555	192	00	00	00	0
1	6330	43	08	01	05	29	*	1	1600	193	00	00	00	0
1	6335	44	03	01	02	23	*	1	1605	194	00	00	00	0
1	6340	45	02	01	02	10	*	1	1610	195	00	00	00	0
1	6345	46	01	01	02	13	*	1	1615	196	00	00	00	0
1	6350	47	02	01	02	11	*	1	1620	197	00	00	00	0
1	6355	48	02	01	01	9	*	1	1625	198	00	00	00	0
1	6400	49	02	01	01	0	*	1	1630	199	00	00	00	0
1	6405	50	02	01	01	7	*	1	1635	200	00	00	00	0
1	6410	51	02	01	01	6	*	1	1640	201	00	00	00	0
1	6415	52	02	01	01	5	*	1	1645	202	00	00	00	0
1	6420	53	02	00	01	5	*	1	1650	203	00	00	00	0
1	6425	54	02	00	01	4	*	1	1655	204	00	00	00	0
1	6430	55	01	00	01	3	*	1	1700	205	00	00	00	0
1	6435	56	01	00	01	2	*	1	1705	206	00	00	00	0
1	6440	57	01	00	01	4	*	1	1710	207	00	00	00	0
1	6445	58	01	00	01	1	*	1	1715	208	00	00	00	0
1	6450	59	01	00	01	2	*	1	1720	209	00	00	00	0
1	6455	60	01	00	01	3	*	1	1725	210	00	00	00	0
1	6500	61	01	00	01	4	*	1	1730	211	00	00	00	0
1	6505	62	01	00	01	4	*	1	1735	212	00	00	00	0
1	6510	63	01	00	01	3	*	1	1740	213	00	00	00	0
1	6515	64	01	00	01	3	*	1	1745	214	00	00	00	0
1	6520	65	01	00	01	1	*	1	1750	215	00	00	00	0
1	6525	66	01	00	01	1	*	1	1755	216	00	00	00	0
1	6530	67	01	00	01	2	*	1	1800	217	00	00	00	0
1	6535	68	01	00	01	3	*	1	1805	218	00	00	00	0
1	6540	69	01	00	01	3	*	1	1810	219	00	00	00	0
1	6545	70	01	00	01	2	*	1	1815	220	00	00	00	0
1	6550	71	01	00	01	1	*	1	1820	221	00	00	00	0
1	6555	72	01	00	01	1	*	1	1825	222	00	00	00	0
1	6600	73	01	00	01	3	*	1	1830	223	00	00	00	0
1	6605	74	00	00	00	2	*	1	1835	224	00	00	00	0
1	6610	75	00	00	00	2	*	1	1840	225	00	00	00	0
1	6615	76	00	00	00	2	*	1	1845	226	00	00	00	0
1	6620	77	00	00	00	2	*	1	1850	227	00	00	00	0
1	6625	78	00	00	00	1	*	1	1855	228	00	00	00	0
1	6630	79	00	00	00	1	*	1	1900	229	00	00	00	0
1	6635	80	00	00	00	1	*	1	1905	230	00	00	00	0
1	6640	81	00	00	00	1	*	1	1910	231	00	00	00	0
1	6645	82	00	00	00	1	*	1	1915	232	00	00	00	0
1	6650	83	00	00	00	0	*	1	1920	233	00	00	00	0
1	6655	84	00	00	00	0	*	1	1925	234	00	00	00	0
1	6700	85	00	00	00	0	*	1	1930	235	00	00	00	0
1	6705	86	00	00	00	0	*	1	1935	236	00	00	00	0
1	6710	87	00	00	00	0	*	1	1940	237	00	00	00	0
1	6715	88	00	00	00	0	*	1	1945	238	00	00	00	0
1	6720	89	00	00	00	0	*	1	1950	239	00	00	00	0
1	6725	90	00	00	00	0	*	1	1955	240	00	00	00	0
1	6730	91	00	00	00	0	*	1	2000	241	00	00	00	0
1	6735	92	00	00	00	0	*	1	2005	242	00	00	00	0
1	6740	93	00	00	00	0	*	1	2010	243	00	00	00	0
1	6745	94	00	00	00	0	*	1	2015	244	00	00	00	0
1	6750	95	00	00	00	0	*	1	2020	245	00	00	00	0
1	6755	96	00	00	00	0	*	1	2025	246	00	00	00	0
1	6800	97	00	00	00	0	*	1	2030	247	00	00	00	0
1	6805	98	00	00	00	0	*	1	2035	248	00	00	00	0
1	6810	99	00	00	00	0	*	1	2040	249	00	00	00	0
1	6815	100	00	00	00	0	*	1	2045	250	00	00	00	0
1	6820	101	00	00	00	0	*	1	2050	251	00	00	00	0
1	6825	102	00	00	00	0	*	1	2055	252	00	00	00	0
1	6830	103	00	00	00	0	*	1	2100	253	00	00	00	0
1	6835	104	00	00	00	0	*	1	2105	254	00	00	00	0
1	6840	105	00	00	00	0	*	1	2110	255	00	00	00	0
1	6845	106	00	00	00	0	*	1	2115	256	00	00	00	0
1	6850	107	00	00	00	0	*	1	2120	257	00	00	00	0
1	6855	108	00	00	00	0	*	1	2125	258	00	00	00	0
1	6900	109	00	00	00	0	*	1	2130	259	00	00	00	0

1	0925	110	00	00	.00	0	*	1	2115	260	.00	.00	00	0
1	0910	111	00	00	00	0	*	1	2140	261	00	00	00	0
1	0915	112	00	00	00	0	*	1	2145	262	00	.00	00	0
1	0920	113	00	00	00	0	*	1	2150	263	00	00	.00	0
1	0925	114	.00	00	.00	0	*	1	2155	264	00	00	.00	0
1	0930	115	00	.00	.00	0	*	1	2200	265	00	00	00	0
1	0935	116	00	00	00	0	*	1	2205	266	00	00	00	0
1	0940	117	00	00	.00	0	*	1	2210	267	00	00	.00	0
1	0945	118	00	00	00	0	*	1	2215	268	.00	00	00	0
1	0950	119	00	00	00	0	*	1	2220	269	00	00	00	0
1	0955	120	00	.00	.00	0	*	1	2225	270	00	00	00	0
1	1000	121	00	00	.00	0	*	1	2230	271	00	.00	.00	0
1	1005	122	00	00	00	0	*	1	2235	272	00	.00	.00	0
1	1010	123	00	00	00	0	*	1	2240	273	00	00	.00	0
1	1015	124	00	00	00	0	*	1	2245	274	00	00	00	0
1	1020	125	.00	00	.00	0	*	1	2250	275	00	00	.00	0
1	1025	126	00	00	00	0	*	1	2255	276	00	00	00	0
1	1030	127	00	.00	.00	0	*	1	2300	277	00	00	00	0
1	1035	128	00	00	00	0	*	1	2305	278	00	00	00	0
1	1040	129	00	00	00	0	*	1	2310	279	00	.00	00	0
1	1045	130	00	00	00	0	*	1	2315	280	00	00	00	0
1	1050	131	00	00	00	0	*	1	2320	281	00	00	00	0
1	1055	132	00	.00	.00	0	*	1	2325	282	.00	.00	.00	0
1	1100	133	00	00	00	0	*	1	2330	283	00	00	.00	0
1	1105	134	.00	00	.00	0	*	1	2335	284	00	00	00	0
1	1110	135	00	00	00	0	*	1	2340	285	.00	00	00	0
1	1115	136	00	00	00	0	*	1	2345	286	00	.00	00	0
1	1120	137	00	00	.00	0	*	1	2350	287	00	00	00	0
1	1125	138	00	00	00	0	*	1	2355	288	00	00	00	0
1	1130	139	00	00	.00	0	*	2	0000	289	00	00	00	0
1	1135	140	00	00	00	0	*	2	0005	290	00	00	.00	0
1	1140	141	00	00	00	0	*	2	0010	291	00	00	.00	0
1	1145	142	00	.00	00	0	*	2	0015	292	00	00	00	0
1	1150	143	00	00	00	0	*	2	0020	293	00	00	00	0
1	1155	144	.00	00	.00	0	*	2	0025	294	00	00	.00	0
1	1200	145	00	00	.00	0	*	2	0030	295	00	00	.00	0
1	1205	146	00	00	00	0	*	2	0035	296	00	00	00	0
1	1210	147	00	.00	00	0	*	2	0040	297	00	00	.00	0
1	1215	148	00	00	00	0	*	2	0045	298	00	00	00	0
1	1220	149	00	.00	00	0	*	2	0050	299	00	00	00	0
1	1225	150	00	.00	00	0	*	2	0055	300	00	00	00	0

TOTAL RAINFALL = 1.22, TOTAL LOSS = 1.99, TOTAL EXCESS = 1.23

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24-92-HR
(CFS)	(HR)				
90	3:17	7	7	7	7
	(INCHES)	1.224	1.226	1.226	1.226
	(AC-FY)	3	3	3	3

CUMULATIVE AREA = 05 SQ MI

677 KK CRRIN COMBINE

678 RD OUTPUT CONTROL VARIABLES  
 1 PRINT CONTROL  
 0 PLOT CONTROL  
 0 HYDROGRAPH PLOT SCALE  
 COMBINE ROUTED ABOUT 5 AND 5 WITH ASLD PARCU

680 HC HYDROGRAPH COMBINATION  
 1 COMB 2 NUMBER OF HYDROGRAPHS TO COMBINE

# HYDROGRAPH AT STATION CRRIN SUM OF 2 HYDROGRAPHS

DA MON HRRIN	ORD	FLOW	DA MON HRRIN	ORD	FLOW	DA MON HRRIN	ORD	FLOW	DA MON HRRIN	ORD	FLOW
1	0000	1	0	1	0615	26	31	1	1210	153	6
1	0005	2	0	1	0620	37	64	1	1215	152	6
1	0010	3	0	1	0625	48	64	1	1240	153	6
1	0015	4	0	1	0630	59	61	1	1245	151	6
1	0020	5	0	1	0635	60	57	1	1250	155	4
1	0025	6	0	1	0640	81	55	1	1255	156	4
1	0030	7	0	1	0645	92	52	1	1300	157	5
1	0035	8	0	1	0650	93	50	1	1305	158	5
1	0040	9	0	1	0655	84	47	1	1310	159	5
1	0045	10	0	1	0700	85	45	1	1315	160	5
1	0050	11	0	1	0705	86	43	1	1320	161	4
1	0055	12	0	1	0710	87	41	1	1325	162	5
1	0100	13	1	1	0715	88	40	1	1330	161	4
1	0105	14	2	1	0720	89	38	1	1335	164	4
1	0110	15	3	1	0725	90	37	1	1340	165	4
1	0115	16	5	1	0730	91	35	1	1345	166	3

1	0120	17	6	*	1	0715	92	31	*	1	1350	167	4	*	1	2005	212	1.
1	0125	18	7	*	1	0710	93	33	*	1	1355	168	4	*	1	2010	243	1.
1	0130	19	8	*	1	0745	94	37	*	1	1400	169	4	*	1	2015	244	1.
1	0135	20	9	*	1	0750	95	36	*	1	1405	170	1	*	1	2020	245	1.
1	0140	21	10	*	1	0755	96	29	*	1	1410	171	9	*	1	2025	246	1.
1	0145	22	10	*	1	0800	97	28	*	1	1415	172	4	*	1	2030	247	1.
1	0150	23	11	*	1	0805	98	37	*	1	1420	173	1	*	1	2035	248	1.
1	0155	24	12	*	1	0810	99	26	*	1	1425	174	3	*	1	2040	249	1.
1	0200	25	13	*	1	0815	100	26	*	1	1430	175	3	*	1	2045	250	1.
1	0205	26	14	*	1	0820	101	25	*	1	1435	176	3	*	1	2050	251	1.
1	0210	27	15	*	1	0825	102	24	*	1	1440	177	3	*	1	2055	252	1.
1	0215	28	16	*	1	0830	103	23	*	1	1445	178	3	*	1	2100	253	1.
1	0220	29	17	*	1	0835	104	22	*	1	1450	179	3	*	1	2105	254	1.
1	0225	30	18	*	1	0840	105	22	*	1	1455	180	5	*	1	2110	255	1.
1	0230	31	19	*	1	0845	106	21	*	1	1500	181	3	*	1	2115	256	1.
1	0235	32	21	*	1	0850	107	20	*	1	1505	182	1	*	1	2120	257	1.
1	0240	33	22	*	1	0855	108	20	*	1	1510	183	3	*	1	2125	258	1.
1	0245	34	26	*	1	0900	109	19	*	1	1515	184	3	*	1	2130	259	1.
1	0250	35	33	*	1	0905	110	19	*	1	1520	185	1	*	1	2135	260	1.
1	0255	36	45	*	1	0910	111	18	*	1	1525	186	3	*	1	2140	261	1.
1	0300	37	65	*	1	0915	112	17	*	1	1530	187	3	*	1	2145	262	1.
1	0305	38	130	*	1	0920	113	17	*	1	1535	188	3	*	1	2150	263	1.
1	0310	39	256	*	1	0925	114	16	*	1	1540	189	4	*	1	2155	264	1.
1	0315	40	300	*	1	0930	115	16	*	1	1545	190	2	*	1	2200	265	1.
1	0320	41	299	*	1	0935	116	15	*	1	1550	191	2	*	1	2205	266	1.
1	0325	42	207	*	1	0940	117	15	*	1	1555	192	2	*	1	2210	267	0.
1	0330	43	272	*	1	0945	118	15	*	1	1600	193	2	*	1	2215	268	0.
1	0335	44	257	*	1	0950	119	14	*	1	1605	194	2	*	1	2220	269	0.
1	0340	45	249	*	1	0955	120	14	*	1	1610	195	2	*	1	2225	270	0.
1	0345	46	221	*	1	1000	121	13	*	1	1615	196	2	*	1	2230	271	0.
1	0350	47	202	*	1	1005	122	13	*	1	1620	197	2	*	1	2235	272	0.
1	0355	48	186	*	1	1010	123	11	*	1	1625	198	2	*	1	2240	273	0.
1	0400	49	173	*	1	1015	124	12	*	1	1630	199	2	*	1	2245	274	0.
1	0405	50	163	*	1	1020	125	12	*	1	1635	200	3	*	1	2250	275	0.
1	0410	51	155	*	1	1025	126	12	*	1	1640	201	2	*	1	2255	276	0.
1	0415	52	140	*	1	1030	127	11	*	1	1645	202	2	*	1	2300	277	0.
1	0420	53	132	*	1	1035	128	11	*	1	1650	203	2	*	1	2305	278	0.
1	0425	54	137	*	1	1040	129	11	*	1	1655	204	2	*	1	2310	279	0.
1	0430	55	133	*	1	1045	130	10	*	1	1700	205	2	*	1	2315	280	0.
1	0435	56	123	*	1	1050	131	10	*	1	1705	206	2	*	1	2320	281	0.
1	0440	57	125	*	1	1055	132	10	*	1	1710	207	2	*	1	2325	282	0.
1	0445	58	122	*	1	1100	133	10	*	1	1715	208	2	*	1	2330	283	0.
1	0450	59	119	*	1	1105	134	9	*	1	1720	209	2	*	1	2335	284	0.
1	0455	60	116	*	1	1110	135	9	*	1	1725	210	2	*	1	2340	285	0.
1	0500	61	112	*	1	1115	136	9	*	1	1730	211	2	*	1	2345	286	0.
1	0505	62	108	*	1	1120	137	9	*	1	1735	212	3	*	1	2350	287	0.
1	0510	63	105	*	1	1125	138	8	*	1	1740	213	1	*	1	2355	288	0.
1	0515	64	102	*	1	1130	139	8	*	1	1745	214	1	*	1	0000	289	0.
1	0520	65	99	*	1	1135	140	8	*	1	1750	215	1	*	2	0005	290	0.
1	0525	66	96	*	1	1140	141	8	*	1	1755	216	1	*	2	0010	291	0.
1	0530	67	93	*	1	1145	142	8	*	1	1800	217	1	*	2	0015	292	0.
1	0535	68	90	*	1	1150	143	7	*	1	1805	218	1	*	2	0020	293	0.
1	0540	69	87	*	1	1155	144	7	*	1	1810	219	1	*	2	0025	294	0.
1	0545	70	85	*	1	1200	145	7	*	1	1815	220	1	*	2	0030	295	0.
1	0550	71	83	*	1	1205	146	7	*	1	1820	221	1	*	2	0035	296	0.
1	0555	72	80	*	1	1210	147	7	*	1	1825	222	1	*	2	0040	297	0.
1	0600	73	78	*	1	1215	148	6	*	1	1830	223	1	*	2	0045	298	0.
1	0605	74	76	*	1	1220	149	6	*	1	1835	224	1	*	2	0050	299	0.
1	0610	75	74	*	1	1225	150	5	*	1	1840	225	1	*	2	0055	300	0.

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PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24-92-HR
300	3 25	90	20	27	27
		(INCHES)	1.61	1.85	1.85
		(AC-FT)	40.	56	56
CUMULATIVE AREA =		56 SQ MI			

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 601 KK R11C 2  
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687 KD OUTPUT CONTROL VARIABLES  
 IPRT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCALE 0 HYDROGRAPH PLOT SCALE  
 RETRIEVE DIVERTED PIPE FLOW

681 DR RETRIEVE DIVERSION HYDROGRAPH  
 (ISAD) D11C 2 DIVERSION HYDROGRAPH IDENTIFICATION

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# HYDROGRAPH AT STATION R11C 2

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DA	MON	HR	MIN	ORD	FLOW	DA	MON	HR	MIN	ORD	FLOW	DA	MON	HR	MIN	ORD	FLOW	
1	0000	1	0	*	1	0615	26	9	*	1	1210	151	0	*	1	1845	225	0

1	PRINT CONTROL	0	HYDROGRAPH PLOT SCALE	0	SUN EAST OF SCOTTSBLVD RD. FLOWING DIRECTLY INTO SCOTTSBLVD RD
0	PILOT	0			
0	OSCAL				

CULVERT, TAKES SCOTTS RD HALF ST AND SCENIC CORRIDOR

SUBBASIN RUNOFF DATA

689 BA SUBBASIN CHARACTERISTICS  
TARPA 01 SUBBASIN AREA

PRECIPITATION DATA

24 PH DEPTH FOR 0-PERCENT HYPOTHETICAL STORM  
HYDRO-35 TP-40  
5-MIN 15-MIN 60-MIN 2 HR 3 HR 6 HR 12 HR 24 HR 2-DAY 4-DAY 7-DAY 10-DAY  
76 1 50 2 51 2 81 7 99 3 33 00 00 00 00 00 00

STORM AREA = 14.00

690 LY SCS LOSS RATE  
STPPL 60 INITIAL ABSTRACTION  
CVRBR 17.00 CURVE NUMBER  
PTIMP 69.00 PERCENT IMPERVIOUS AREA

691 UE KINEMATIC WAVE  
OVERLAND-FLOW ELEMENT NO. 1  
L 50 OVERLAND FLOW LENGTH  
S 0100 SLOPE  
N 050 ROUGHNESS COEFFICIENT  
PA 100.0 PERCENT OF SUBBASIN  
DYNIN 5 MINIMUM NUMBER OF DX INTERVALS

692 KE KINEMATIC WAVE  
MAIN CHANNEL  
L 500 CHANNEL LENGTH  
S 0100 SLOPE  
N 015 CHANNEL ROUGHNESS COEFFICIENT  
CA .01 CONFINING AREA  
SHAPE CIRC CHANNEL SHAPE  
WD 4.50 BOTTOM WIDTH OR DIAMETER  
Z 00 SIDE SLOPE  
DYNIN 5 MINIMUM NUMBER OF DX INTERVALS  
RUPSTO 00 ROUTE OUTSTREAM HYDROGRAPH

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COMPUTED KINEMATIC PARAMETERS  
VARIABLE TIME STEP  
(OT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(CU)	(FPS)
CHANNEL	2.98	1.67	12	10.06	11.73	184.81	3.00	54
MAIN	5.45	1.75	33	700.00	31.72	164.75	2.09	12.50

CONTINUITY SUMMARY (AC-FP) : INFLOW: 0000E+00 EXCESS: 1009E+01 OUTFLOW: 1009E+01 PAVN STORAGE: 4154E+05 PERCENT ERROR: 1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN 6.30 1.75 5.00 31.67 164.00 3.03

HYDROGRAPH AT STATION SCOUT

DA	MON	HRS	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HRS	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	00	00	00	00	0	1	1230	153	00	00	00	00	0
1	0005	2	01	00	01	0	0	1	1235	152	00	00	00	00	0
1	0010	3	01	00	01	0	0	1	1240	153	.00	00	00	00	0
1	0015	4	01	00	01	0	0	1	1245	154	00	00	00	00	0
1	0020	5	01	00	01	0	0	1	1250	155	00	00	00	00	0
1	0025	6	01	00	01	0	0	1	1255	156	00	00	00	00	0
1	0030	7	01	00	01	0	0	1	1300	157	00	00	00	00	0
1	0035	8	01	00	01	0	0	1	1305	158	00	00	00	00	0
1	0040	9	01	00	01	0	0	1	1310	159	00	00	00	00	0
1	0045	10	01	00	01	0	0	1	1315	160	00	00	00	00	0
1	0050	11	01	00	01	0	0	1	1320	161	00	00	00	00	0
1	0055	12	01	00	01	0	0	1	1325	162	00	00	00	00	0
1	0100	13	01	00	01	0	0	1	1330	163	00	00	00	00	0
1	0105	14	01	00	01	0	0	1	1335	164	00	00	00	00	0
1	0110	15	01	00	01	0	0	1	1340	165	00	00	00	00	0
1	0115	16	01	00	01	0	0	1	1345	166	00	00	00	00	0
1	0120	17	01	00	01	1	1	1	1350	167	00	00	00	00	0
1	0125	18	01	00	01	1	1	1	1355	168	00	00	00	00	0
1	0130	19	01	00	01	1	1	1	1400	169	00	00	00	00	0
1	0135	20	01	00	01	1	1	1	1405	170	00	00	00	00	0
1	0140	21	01	00	01	1	1	1	1410	171	00	00	00	00	0
1	0145	22	02	00	01	1	1	1	1415	172	00	00	00	00	0
1	0150	23	02	00	01	1	1	1	1420	173	00	00	00	00	0
1	0155	24	02	00	02	1	1	1	1425	174	.00	00	00	00	0
1	0200	25	02	00	02	1	1	1	1430	175	00	00	00	00	0
1	0205	26	02	00	02	1	1	1	1435	176	00	00	00	00	0
1	0210	27	02	00	02	1	1	1	1440	177	00	00	00	00	0
1	0215	28	02	00	02	1	1	1	1445	178	00	00	00	00	0
1	0220	29	02	00	02	1	1	1	1450	179	00	00	00	00	0
1	0225	30	01	00	02	1	1	1	1455	180	00	.00	00	00	0
1	0230	31	01	00	02	1	1	1	1500	181	00	00	00	00	0
1	0235	32	06	01	07	1	1	1	1505	182	00	00	00	00	0
1	0240	33	07	01	08	1	1	1	1510	183	00	00	00	00	0
1	0245	34	.10	01	09	1	1	1	1515	184	00	00	.00	.00	0



1	0250	35	.14	01	12	6	*	1	1520	105	00	00	00	0.
1	0255	36	.18	02	16	8.	*	1	1525	106	00	00	.00	0.
1	0300	37	.40	03	27	18.	*	1	1530	107	00	00	00	0
1	0305	38	.49	04	45	21.	*	1	1535	108	00	.00	00	0.
1	0310	39	.28	.01	26	13.	*	1	1540	109	00	00	00	0.
1	0315	40	.15	01	15	7	*	1	1545	110	00	.00	.00	0.
1	0320	41	.17	.00	10	5.	*	1	1550	111	.00	00	00	0
1	0325	42	.09	.00	09	4	*	1	1555	112	00	.00	.00	0.
1	0330	43	.08	00	08	4.	*	1	1600	113	00	00	.00	0
1	0335	44	.03	00	03	2	*	1	1605	114	00	00	.00	0
1	0340	45	.03	00	03	1	*	1	1610	115	00	00	.00	0
1	0345	46	.03	00	03	1.	*	1	1615	116	00	00	.00	0.
1	0350	47	.02	.00	02	1	*	1	1620	117	00	00	.00	0
1	0355	48	.02	.00	02	1	*	1	1625	118	00	00	.00	0
1	0400	49	.02	00	02	1	*	1	1630	119	.00	00	.00	0
1	0405	50	.02	.00	02	1	*	1	1635	120	00	00	.00	0
1	0410	51	.02	.00	02	1	*	1	1640	121	00	00	.00	0.
1	0415	52	.02	.00	02	1	*	1	1645	122	00	00	.00	0
1	0420	53	.03	.00	02	1.	*	1	1650	123	00	.00	.00	0.
1	0425	54	.02	.00	01	1	*	1	1655	124	.00	00	.00	0.
1	0430	55	.01	.00	01	1	*	1	1700	125	00	00	.00	0
1	0435	56	.01	.00	01	1	*	1	1705	126	00	00	.00	0
1	0440	57	.01	.00	01	1	*	1	1710	127	00	.00	.00	0
1	0445	58	.01	.00	01	1	*	1	1715	128	.00	.00	.00	0
1	0450	59	.01	.00	01	1	*	1	1720	129	00	00	.00	0
1	0455	60	.01	.00	01	1	*	1	1725	130	00	00	.00	0
1	0500	61	.01	.00	01	1	*	1	1730	131	00	00	.00	0
1	0505	62	.01	.00	01	1	*	1	1735	132	00	00	.00	0
1	0510	63	.01	.00	01	0	*	1	1740	133	00	00	.00	0
1	0515	64	.01	.00	01	0	*	1	1745	134	00	00	.00	0
1	0520	65	.01	.00	01	0	*	1	1750	135	00	00	.00	0
1	0525	66	.01	.00	01	0	*	1	1755	136	00	00	.00	0
1	0530	67	.01	.00	01	0	*	1	1800	137	00	00	.00	0
1	0535	68	.01	.00	01	0	*	1	1805	138	00	00	.00	0
1	0540	69	.01	.00	01	0	*	1	1810	139	00	00	.00	0
1	0545	70	.02	.00	02	0	*	1	1815	140	00	00	.00	0
1	0550	71	.01	.00	01	0	*	1	1820	141	00	00	.00	0
1	0555	72	.01	.00	01	0	*	1	1825	142	00	00	.00	0
1	0600	73	.01	.00	01	0	*	1	1830	143	00	.00	.00	0.
1	0605	74	.00	.00	00	0	*	1	1835	144	.00	00	.00	0
1	0610	75	.00	.00	00	0	*	1	1840	145	00	00	.00	0
1	0615	76	.00	.00	00	0	*	1	1845	146	00	00	.00	0
1	0620	77	.00	.00	00	0	*	1	1850	147	00	00	.00	0
1	0625	78	.00	.00	00	0	*	1	1855	148	00	00	.00	0
1	0630	79	.00	.00	00	0	*	1	1900	149	00	00	.00	0
1	0635	80	.00	.00	00	0	*	1	1905	150	00	00	.00	0
1	0640	81	.00	.00	00	0	*	1	1910	151	00	00	.00	0.
1	0645	82	.00	.00	00	0	*	1	1915	152	00	00	.00	0.
1	0650	83	.00	.00	00	0	*	1	1920	153	00	00	.00	0.
1	0655	84	.00	.00	00	0	*	1	1925	154	.00	.00	.00	0.
1	0700	85	.00	.00	00	0	*	1	1930	155	00	00	.00	0
1	0705	86	.00	.00	00	0	*	1	1935	156	00	00	.00	0
1	0710	87	.00	.00	00	0	*	1	1940	157	00	00	.00	0
1	0715	88	.00	.00	00	0	*	1	1945	158	00	00	.00	0
1	0720	89	.00	.00	00	0	*	1	1950	159	00	00	.00	0
1	0725	90	.00	.00	00	0	*	1	1955	160	00	00	.00	0
1	0730	91	.00	.00	00	0	*	1	2000	161	00	00	.00	0.
1	0735	92	.00	.00	00	0	*	1	2005	162	00	00	.00	0
1	0740	93	.00	.00	00	0	*	1	2010	163	00	00	.00	0
1	0745	94	.00	.00	00	0	*	1	2015	164	00	00	.00	0
1	0750	95	.00	.00	00	0	*	1	2020	165	00	00	.00	0.
1	0755	96	.00	.00	00	0	*	1	2025	166	00	00	.00	0
1	0800	97	.00	.00	00	0	*	1	2030	167	00	00	.00	0
1	0805	98	.00	.00	00	0	*	1	2035	168	00	.00	.00	0.
1	0810	99	.00	.00	00	0	*	1	2040	169	00	00	.00	0
1	0815	100	.00	.00	00	0	*	1	2045	170	00	00	.00	0
1	0820	101	.00	.00	00	0	*	1	2050	171	00	00	.00	0
1	0825	102	.00	.00	00	0	*	1	2055	172	00	00	.00	0.
1	0830	103	.00	.00	00	0	*	1	2100	173	00	00	.00	0
1	0835	104	.00	.00	00	0	*	1	2105	174	00	00	.00	0
1	0840	105	.00	.00	00	0	*	1	2110	175	00	00	.00	0
1	0845	106	.00	.00	00	0	*	1	2115	176	00	.00	.00	0.
1	0850	107	.00	.00	00	0	*	1	2120	177	00	00	.00	0
1	0855	108	.00	.00	00	0	*	1	2125	178	00	00	.00	0
1	0900	109	.00	.00	00	0	*	1	2130	179	00	00	.00	0
1	0905	110	.00	.00	00	0	*	1	2135	180	00	00	.00	0
1	0910	111	.00	.00	00	0	*	1	2140	181	00	00	.00	0
1	0915	112	.00	.00	00	0	*	1	2145	182	00	00	.00	0
1	0920	113	.00	.00	00	0	*	1	2150	183	00	00	.00	0
1	0925	114	.00	.00	00	0	*	1	2155	184	00	00	.00	0
1	0930	115	.00	.00	00	0	*	1	2200	185	00	00	.00	0
1	0935	116	.00	.00	00	0	*	1	2205	186	.00	00	.00	0.
1	0940	117	.00	.00	00	0	*	1	2210	187	00	00	.00	0
1	0945	118	.00	.00	00	0	*	1	2215	188	00	00	.00	0
1	0950	119	.00	.00	00	0	*	1	2220	189	00	00	.00	0
1	0955	120	.00	.00	00	0	*	1	2225	190	00	00	.00	0
1	1000	121	.00	.00	00	0	*	1	2230	191	00	00	.00	0
1	1005	122	.00	.00	00	0	*	1	2235	192	00	00	.00	0
1	1010	123	.00	.00	00	0	*	1	2240	193	00	00	.00	0
1	1015	124	.00	.00	00	0	*	1	2245	194	00	00	.00	0
1	1020	125	.00	.00	00	0	*	1	2250	195	00	00	.00	0
1	1025	126	.00	.00	00	0	*	1	2255	196	00	00	.00	0
1	1030	127	.00	.00	00	0	*	1	2300	197	00	00	.00	0
1	1035	128	.00	.00	00	0	*	1	2305	198	00	00	.00	0
1	1040	129	.00	.00	00	0	*	1	2310	199	00	00	.00	0
1	1045	130	.00	.00	00	0	*	1	2315	200	00	00	.00	0
1	1050	131	.00	.00	00	0	*	1	2320	201	00	00	.00	0
1	1055	132	.00	.00	00	0	*	1	2325	202	00	00	.00	0
1	1100	133	.00	.00	00	0	*	1	2330	203	00	00	.00	0
1	1105	134	.00	.00	00	0	*	1	2335	204	00	00	.00	0
1	1110	135	.00	.00	00	0	*	1	2340	205	00	00	.00	0
1	1115	136	.00	.00	00	0	*	1	2345	206	00	00	.00	0
1	1120	137	.00	.00	00	0	*	1	2350	207	.00	00	.00	0
1	1125	138	.00	.00	00	0	*	1	2355	208	00	00	.00	0

1	1110	139	.90	00	.00	0	*	2	0000	289	.00	.00	.00	0
1	1135	140	.90	.00	.00	0.	*	2	0005	290	.00	.00	.00	0
1	1140	141	.90	.00	.00	0	*	2	0010	291	.00	.00	.00	0
1	1145	142	.90	.00	.00	0.	*	2	0015	292	.00	.00	.00	0
1	1150	143	.90	.00	.00	0	*	2	0020	293	.00	.00	.00	0
1	1155	144	.90	.00	.00	0	*	2	0025	294	.00	.00	.00	0
1	1200	145	.90	.00	.00	0	*	2	0030	295	.00	.00	.00	0
1	1205	146	.90	.00	.00	0	*	2	0035	296	.00	.00	.00	0
1	1210	147	.90	.00	.00	0	*	2	0040	297	.00	.00	.00	0
1	1215	148	.90	.00	.00	0	*	2	0045	298	.00	.00	.00	0
1	1220	149	.90	.00	.00	0	*	2	0050	299	.00	.00	.00	0
1	1225	150	.90	.00	.00	0	*	2	0055	300	.00	.00	.00	0

TOTAL RAINFALL = 3.22, TOTAL LOSS = 32, TOTAL EXCESS = 3.00

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
(CFS) (HR) 6-HR 24-HR 72-HR 24 92-HR  
21. 3.08  
(INCHES) 2. 1. 0 0.  
(AC-FT) 3.004 3.013 3.013 3.013  
CUMULATIVE AREA = .01 SQ MI

693 KK 111 2 COMBINE

694 KO OUTPUT CONTROL VARIABLES  
IDPRNT 1 PRINT CONTROL  
IDPLOT 0 PLOT CONTROL  
QSCALE 0 HYDROGRAPH PLOT SCALE  
COMBINED DISCHARGE AT SCOTTSDALE ROAD CULVERT

695 UC HYDROGRAPH COMBINATION  
ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION 111 2  
SUM OF 2 HYDROGRAPHS

DA	MON	HRMM	ORD	FLOW	DA	MON	HRMM	ORD	FLOW	DA	MON	HRMM	ORD	FLOW	DA	MON	HRMM	ORD	FLOW
1	0000	1	0	*	1	0615	75	9	*	1	1230	151	0	*	1	1045	226	0	
1	0005	2	0	*	1	0620	77	8	*	1	1235	152	0	*	1	1050	227	0	
1	0010	3	0	*	1	0625	78	7	*	1	1240	153	0	*	1	1055	228	0	
1	0015	4	0	*	1	0630	79	6	*	1	1245	154	0	*	1	1000	229	0	
1	0020	5	0	*	1	0635	80	5	*	1	1250	155	0	*	1	1005	230	0	
1	0025	6	0	*	1	0640	81	5	*	1	1255	156	0	*	1	1010	231	0	
1	0030	7	0	*	1	0645	82	4	*	1	1300	157	0	*	1	1015	232	0	
1	0035	8	0	*	1	0650	83	1	*	1	1305	158	0	*	1	1020	233	0	
1	0040	9	0	*	1	0655	84	1	*	1	1310	159	0	*	1	1025	234	0	
1	0045	10	0	*	1	0700	85	3	*	1	1315	160	0	*	1	1030	235	0	
1	0050	11	0	*	1	0705	86	2	*	1	1320	161	0	*	1	1035	236	0	
1	0055	12	0	*	1	0710	87	2	*	1	1325	162	0	*	1	1040	237	0	
1	0100	13	1	*	1	0715	88	2	*	1	1330	163	0	*	1	1045	238	0	
1	0105	14	1	*	1	0720	89	2	*	1	1335	164	0	*	1	1050	239	0	
1	0110	15	2	*	1	0725	90	1	*	1	1340	165	0	*	1	1055	240	0	
1	0115	16	2	*	1	0730	91	1	*	1	1345	166	0	*	1	1000	241	0	
1	0120	17	2	*	1	0735	92	1	*	1	1350	167	0	*	1	1005	242	0	
1	0125	18	3	*	1	0740	93	1	*	1	1355	168	0	*	1	1010	243	0	
1	0130	19	3	*	1	0745	94	1	*	1	1400	169	0	*	1	1015	244	0	
1	0135	20	3	*	1	0750	95	1	*	1	1405	170	0	*	1	1020	245	0	
1	0140	21	3	*	1	0755	96	1	*	1	1410	171	0	*	1	1025	246	0	
1	0145	22	4	*	1	0800	97	1	*	1	1415	172	0	*	1	1030	247	0	
1	0150	23	4	*	1	0805	98	1	*	1	1420	173	0	*	1	1035	248	0	
1	0155	24	4	*	1	0810	99	0	*	1	1425	174	0	*	1	1040	249	0	
1	0200	25	5	*	1	0815	100	0	*	1	1430	175	0	*	1	1045	250	0	
1	0205	26	5	*	1	0820	101	0	*	1	1435	176	0	*	1	1050	251	0	
1	0210	27	5	*	1	0825	102	0	*	1	1440	177	0	*	1	1055	252	0	
1	0215	28	6	*	1	0830	103	0	*	1	1445	178	0	*	1	1100	253	0	
1	0220	29	6	*	1	0835	104	0	*	1	1450	179	0	*	1	1105	254	0	
1	0225	30	5	*	1	0840	105	0	*	1	1455	180	0	*	1	1110	255	0	
1	0230	31	7	*	1	0845	106	0	*	1	1500	181	0	*	1	1115	256	0	
1	0235	32	9	*	1	0850	107	0	*	1	1505	182	0	*	1	1120	257	0	
1	0240	33	11	*	1	0855	108	0	*	1	1510	183	0	*	1	1125	258	0	
1	0245	34	14	*	1	0900	109	0	*	1	1515	184	0	*	1	1130	259	0	
1	0250	35	17	*	1	0905	110	0	*	1	1520	185	0	*	1	1135	260	0	
1	0255	36	21	*	1	0910	111	0	*	1	1525	186	0	*	1	1140	261	0	
1	0300	37	33	*	1	0915	112	0	*	1	1530	187	0	*	1	1145	262	0	
1	0305	38	48	*	1	0920	113	0	*	1	1535	188	0	*	1	1150	263	0	
1	0310	39	59	*	1	0925	114	0	*	1	1540	189	0	*	1	1155	264	0	
1	0315	40	103	*	1	0930	115	0	*	1	1545	190	0	*	1	1200	265	0	
1	0320	41	114	*	1	0935	116	0	*	1	1550	191	0	*	1	1205	266	0	
1	0325	42	109	*	1	0940	117	0	*	1	1555	192	0	*	1	1210	267	0	
1	0330	43	100	*	1	0945	118	0	*	1	1600	193	0	*	1	1215	268	0	
1	0335	44	89	*	1	0950	119	0	*	1	1605	194	0	*	1	1220	269	0	
1	0340	45	77	*	1	0955	120	0	*	1	1610	195	0	*	1	1225	270	0	

1	0345	45	64	*	1	1000	121	0	*	1	1615	196	0	*	1	2230	271	0.
1	0350	47	63	*	1	1005	122	0	*	1	1620	197	0	*	1	2235	272	0.
1	0355	48	65	*	1	1010	123	0	*	1	1625	198	0	*	1	2240	273	0
1	0400	49	18	*	1	1015	124	0	*	1	1630	199	0	*	1	2245	274	0
1	0405	50	32	*	1	1020	125	0.	*	1	1635	200	0.	*	1	2250	275	0
1	0410	51	38	*	1	1025	126	0	*	1	1640	201	0	*	1	2255	276	0
1	0415	52	25	*	1	1030	127	0.	*	1	1645	202	0	*	1	2300	277	0
1	0420	53	22	*	1	1035	128	0	*	1	1650	203	0	*	1	2305	278	0
1	0425	54	20	*	1	1040	129	0.	*	1	1655	204	0	*	1	2310	279	0
1	0430	55	19.	*	1	1045	130	0.	*	1	1700	205	0.	*	1	2315	280	0
1	0435	56	18.	*	1	1050	131	0	*	1	1705	206	0	*	1	2320	281	0.
1	0440	57	18	*	1	1055	132	0	*	1	1710	207	0	*	1	2325	282	0.
1	0445	58	18	*	1	1100	133	0	*	1	1715	208	0.	*	1	2330	283	0
1	0450	59	17	*	1	1105	134	0	*	1	1720	209	0	*	1	2335	284	0
1	0455	60	17	*	1	1110	135	0.	*	1	1725	210	0	*	1	2340	285	0
1	0500	61	15.	*	1	1115	136	0	*	1	1730	211	0	*	1	2345	286	0.
1	0505	62	16	*	1	1120	137	0	*	1	1735	212	0	*	1	2350	287	0.
1	0510	61	16	*	1	1125	138	0	*	1	1740	213	0	*	1	2355	288	0
1	0515	63	15	*	1	1130	139	0.	*	1	1745	214	0	*	1	0000	289	0.
1	0520	64	15	*	1	1135	140	0.	*	1	1750	215	0	*	2	0005	290	0.
1	0525	66	15	*	1	1140	141	0	*	1	1755	216	0	*	2	0010	291	0
1	0530	67	13	*	1	1145	142	0.	*	1	1800	217	0	*	2	0015	292	0
1	0535	68	11	*	1	1150	143	0	*	1	1805	218	0.	*	2	0020	293	0.
1	0540	69	13	*	1	1155	144	0	*	1	1810	219	0.	*	2	0025	294	0.
1	0545	70	13	*	1	1200	145	0	*	1	1815	220	0.	*	2	0030	295	0
1	0550	71	12	*	1	1205	146	0	*	1	1820	221	0.	*	2	0035	296	0
1	0555	72	12	*	1	1210	147	0	*	1	1825	222	0.	*	2	0040	297	0.
1	0600	71	11	*	1	1215	148	0	*	1	1830	223	0	*	2	0045	298	0
1	0605	74	11	*	1	1220	149	0	*	1	1835	224	0	*	2	0050	299	0
1	0610	75	10	*	1	1225	150	0	*	1	1840	225	0	*	2	0055	300	0

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24-72-HR
(CFS)	(HR)				
114	3.13	27.1	6	5	5
		(DUCHE)	12.619	72.619	12.619
		(AC-FT)	11	11	11
		CUMULATIVE AREA	01 50 31		

RUNOFF SUMMARY  
FLOW IN CUBIC FEET PER SECOND  
TIME IN HOURS. AREA IN SQUARE MILES

[illegible]

[illegible]





[illegible]



33D NAME	2.02	64.29	192.41	1.27	5.00	61.02	150.00	1.22
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 2679E+01 OUTFLOW: 2627E+01 BASIN STORAGE: 1831E+01 PERCENT ERROR: 5								
510ET NAME	85	79.65	186.49	2.24	5.00	70.00	185.00	2.95
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 2873E+01 OUTFLOW: 2871E+01 BASIN STORAGE: 1120E+01 PERCENT ERROR: 0								
33C NAME	51	129.46	185.80	2.96	5.00	125.66	185.00	2.97
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 4670E+01 OUTFLOW: 4674E+01 BASIN STORAGE: 1952E+01 PERCENT ERROR: 1								
340CN NAME	57	187.23	186.05	3.96	5.00	179.92	185.00	2.97
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 7000E+01 OUTFLOW: 7077E+01 BASIN STORAGE: 4084E+01 PERCENT ERROR: 0								
RISE 1 NAME	3.45	255.03	201.54	1.92	5.00	251.70	200.00	1.97
CONTINUITY SUMMARY (AC-FT) - INFLOW: .5208E+02 EXCESS: .0000E+00 OUTFLOW: .5102E+02 BASIN STORAGE: 2102E+01 PERCENT ERROR: 1								
340D NAME	1.70	91.21	190.76	1.23	5.00	89.79	190.00	1.23
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 3491E+01 OUTFLOW: 3379E+01 BASIN STORAGE: 2007E+01 PERCENT ERROR: 4								
510ET NAME	33	51.72	184.75	3.00	5.00	31.47	185.00	3.01
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 1005E+01 OUTFLOW: 1008E+01 BASIN STORAGE: 4154E+05 PERCENT ERROR: 1								

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
		ELEVATION	00	1.00	3.00		
		STORAGE	0	1	2		
		OUTFLOW	0	20	20		
		RATIO OF PMP					
		MAXIMUM RESERVOIR DEPTH OVER DAM					
		MAXIMUM STORAGE AC-FT					
		MAXIMUM OUTFLOW CFS					
		DURATION OVER TOP HOURS					
		TIME OF MAX OUTFLOW HOURS					
		TIME OF FAILURE HOURS					
		1.00	1.73	00	12	00	3.50

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
		ELEVATION	00	1.00	3.00		
		STORAGE	0.	1	1		
		OUTFLOW	0	4.	4.		
		RATIO OF PMP					
		MAXIMUM RESERVOIR DEPTH OVER DAM					
		MAXIMUM STORAGE AC-FT					
		MAXIMUM OUTFLOW CFS					
		DURATION OVER TOP HOURS					
		TIME OF MAX OUTFLOW HOURS					
		TIME OF FAILURE HOURS					
		1.00	2.51	00	3	00	3.57

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
		ELEVATION	.00	3.00	3.00		
		STORAGE	0	1	1		
		OUTFLOW	0	4	4		
		RATIO OF PMP					
		MAXIMUM RESERVOIR DEPTH OVER DAM					
		MAXIMUM STORAGE AC-FT					
		MAXIMUM OUTFLOW CFS					
		DURATION OVER TOP HOURS					
		TIME OF MAX OUTFLOW HOURS					
		TIME OF FAILURE HOURS					
		1.50	3.14	14	4	1.42	3.58

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
		ELEVATION	00	2.50	2.50		
		STORAGE	0	0	0		
		OUTFLOW	0	22	22.		
		RATIO OF PMP					
		MAXIMUM RESERVOIR DEPTH OVER DAM					
		MAXIMUM STORAGE AC-FT					
		MAXIMUM OUTFLOW CFS					
		DURATION OVER TOP HOURS					
		TIME OF MAX OUTFLOW HOURS					
		TIME OF FAILURE HOURS					
		1.00	2.31	0	11	25	3.11

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	2.50	2.50			
	OUTFLOW	0.	0	0			
			12	12			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	2.87	.37	0.	35.	33	3.33
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	2.50	2.50			
	OUTFLOW	0	1	1.			
			14	14			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	2.94	.46	1	51	33	3.33
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	2.50	2.50			
	OUTFLOW	0	0	0			
			11.	11			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	2.65	.15	0	14	17	3.33
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	2.50	2.50			
	OUTFLOW	0	1	1			
			11	11.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	3.62	1.12	1	66	1.50	1.42
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	3.60	3.60			
	OUTFLOW	0	7.	2			
			14.	14.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	4.85	1.26	2	74	3.33	3.50
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELICIA (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	3.60	3.60			
	OUTFLOW	0	0	0			
			14	14			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	5.05	1.45	1	93	3.25	3.50
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELICIA (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	3.60	3.60			
	OUTFLOW	0	1	1			
			14	14			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	5.02	1.47	1	90	2.92	3.50
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELICIA (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					

(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM		
		ELEVATION	00	3 60	3 60			
		STORAGE	0	1.	1.			
		OUTFLOW	0	11	11			
1	1 00	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
		5 04	1.44	1.	92.	3 00	1.50	00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETIC3 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)						
PLAN 1		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM		
		ELEVATION	00	3 50	3 50			
		STORAGE	0	1	1			
		OUTFLOW	0	150.	150.			
1	1 00	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
		2 55	00	1	109	00	3 67	00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETCOM (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)						
PLAN 1		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM		
		ELEVATION	00	3 00	3 00			
		STORAGE	0	4	4			
		OUTFLOW	0	13	13.			
1	1 00	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
		2 55	00	3	11	00	3 67	00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION BROEFF1 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)						
PLAN 1		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM		
		ELEVATION	00	3 00	3 00			
		STORAGE	0	2	2			
		OUTFLOW	0	12	13.			
1	1 00	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
		2 41	00	2	11	00	1 50	00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION BROFFA (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)						
PLAN 1		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM		
		ELEVATION	00	3 00	3 00			
		STORAGE	0	2	2			
		OUTFLOW	0	11	13.			
1	1 00	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
		2 20	00	2	10	00	3 50	00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION BROFFB (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)						
PLAN 1		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM		
		ELEVATION	00	3 00	3 00			
		STORAGE	0	3	3.			
		OUTFLOW	0	11	11			
1	1 00	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
		2 29	00	3	11	00	3 50	00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION BROFFA1 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)						
PLAN 1		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM		
		ELEVATION	00	3 00	3 00			
		STORAGE	0	3	3			
		OUTFLOW	0	4	4			
1	1 00	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
		2 95	00	1	4	00	3 50	00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	3 00	3 00		
	STORAGE		0.	2.	2		
	OUTFLOW		0	1	1		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 81 60 1 1. 00 3 75 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		.00	1 00	3 00		
	STORAGE		0	2	2.		
	OUTFLOW		0	10.	10		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 3 25 25 2 16 67 3 50 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETECL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	3 00	3 00		
	STORAGE		0	1	1		
	OUTFLOW		0	13	13		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 84 00 1. 12 00 3.47 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETECL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	1 00	3 00		
	STORAGE		0	1	1		
	OUTFLOW		0	11	11		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 47 00 1 9 00 3 13 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETECL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	3 00	3 00		
	STORAGE		0	5	5		
	OUTFLOW		0.	53	52		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 36 00 1 10 00 3 50 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	1 00	3 00		
	STORAGE		0	5	5		
	OUTFLOW		0	11	11		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 57 00 4. 12 00 3 67 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETECL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	3 00	3 00		
	STORAGE		0	5	5.		
	OUTFLOW		0	20	20		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2.77 .00 3 18. 00 3.75 .00  
 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1H  
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 ...

		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	ELEVATION	00		3 00		3 00	
	STORAGE	0		3.		3	
	OUTFLOW	0		20.		70	

RATIO OF IMP	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1 00	3 70	70	4	49	.83	3 42	00

\*\*\* NORMAL END OF REC-1 \*\*\*

# RATIONAL FOR WINDOWS

Flood Control District of Maricopa County Rational Method

## Project Information

Project Name: Interim Regional Drainage Chan      Project Description:  
Drainage Point: 404 Wash      Location: Channel Station 24+00

## Drainage Basin Data

Water Course Length: 820.00 ft      Basin Area: 3.220 acres  
High Elevation: 1581.00 ft      Low Elevation: 1570.00 ft  
Average Slope: 0.0134 ft/ft      Roughness, Kb: 0.0368 (A)  
10-Year Runoff Coefficient: 0.400  
10-Year 6 Hour Rainfall Depth: 2.10 inches

## Hydrological Summary Table

Parameter	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year
Q (cfs)	4	6	7	9	12	14
C	0.400	0.400	0.400	0.440	0.480	0.500
Tc (min)	8.3	7.3	6.8	6.3	6.0	5.7
i (in/hr)	3.2	4.4	5.3	6.6	7.6	8.8

Computed by JMG, Wood, Patel & Associates  
Thursday, May 05, 2005 10:08:51 a

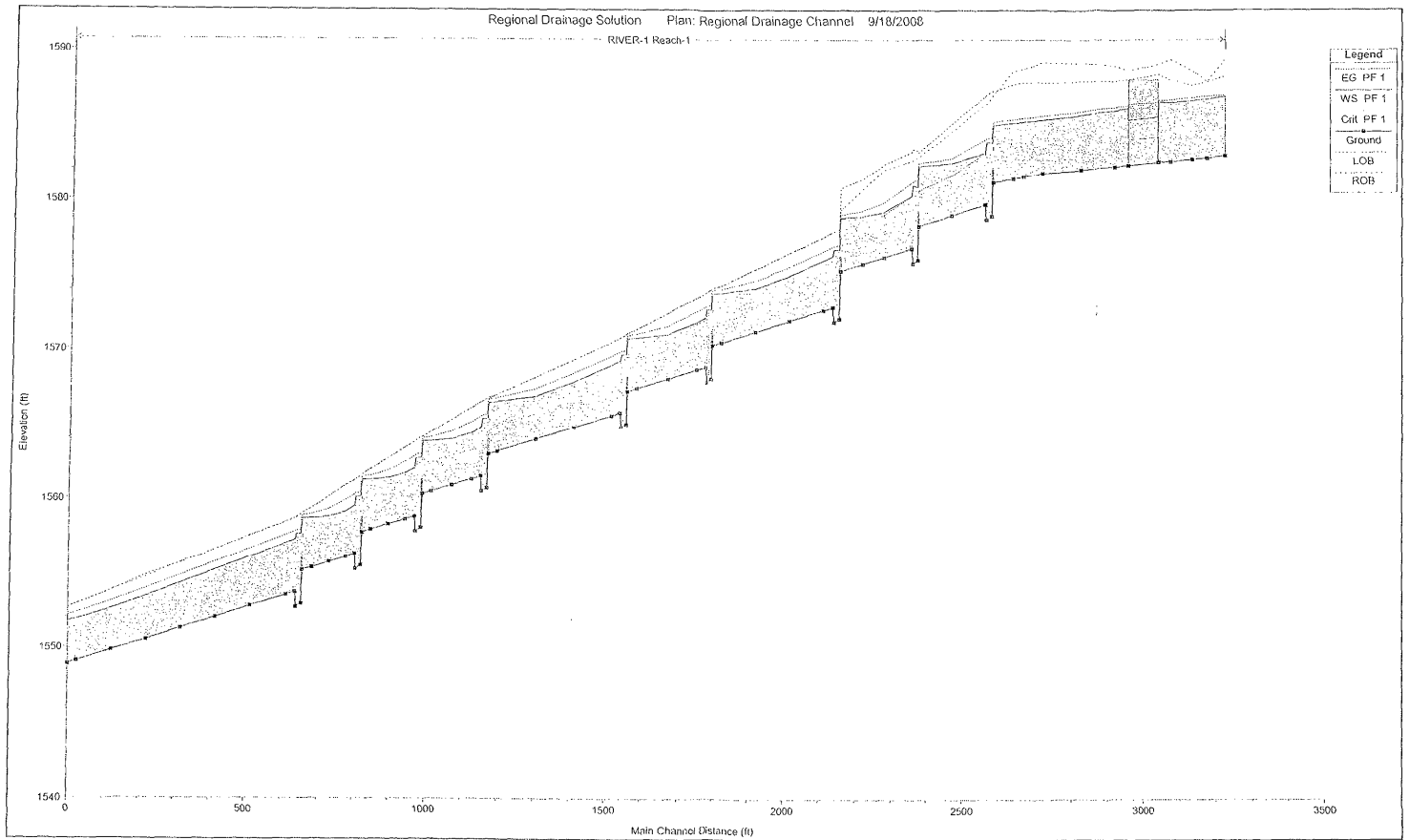
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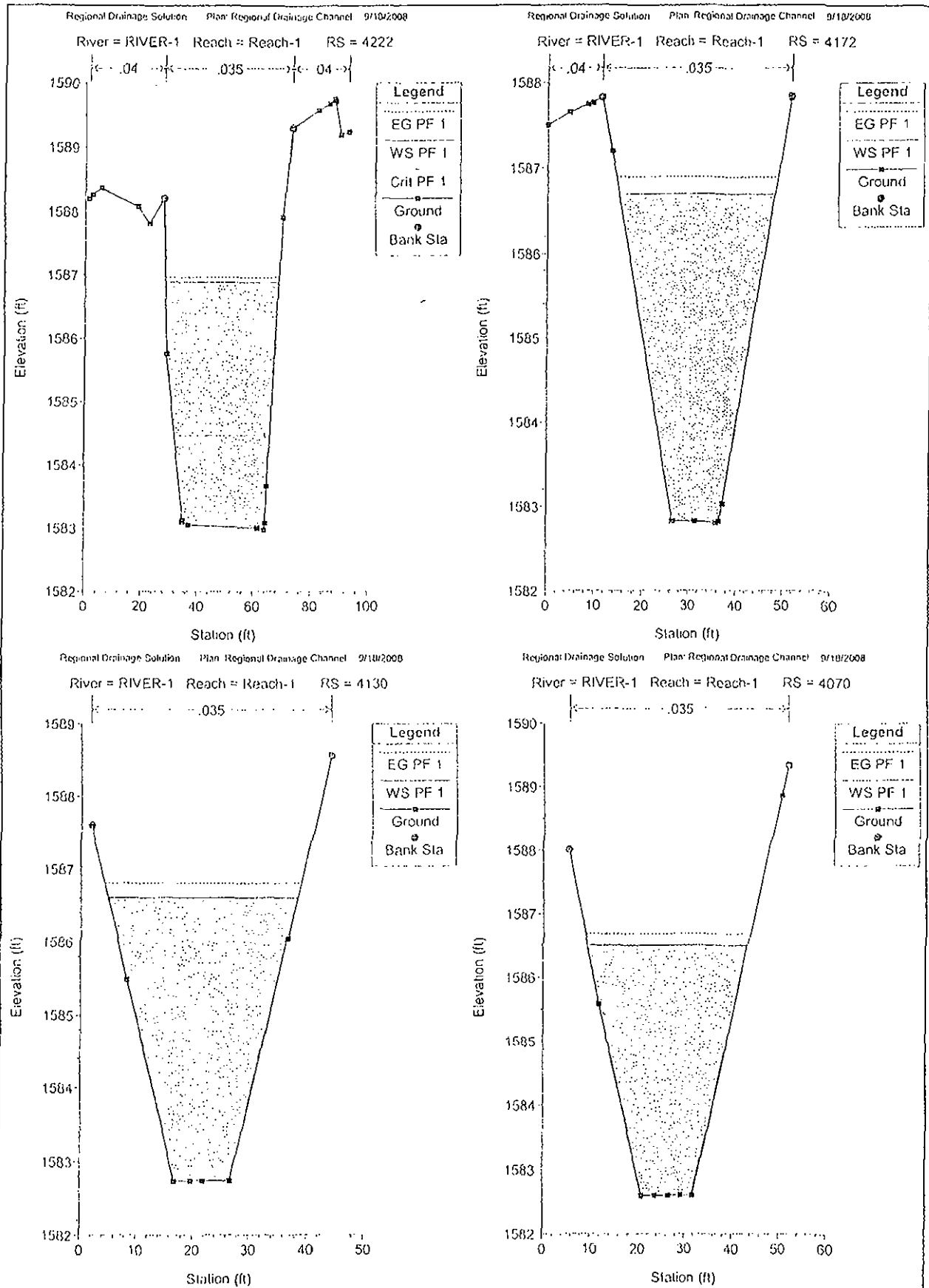
## **APPENDIX B**

### **Hydraulic Calculations**

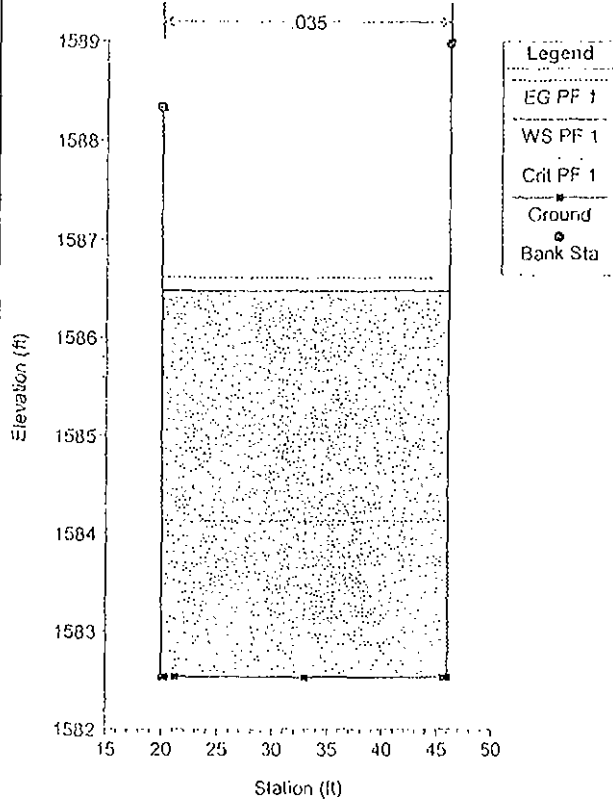


River Sta	Q Total (cfs)	Min Ch El (ft)	WS Elev (ft)	E G Elev (ft)	E G Slope (ft/l)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude #	Chl	LOB Elev (ft)	ROB Elev (ft)	Flow Depth (ft)	Freeboard Req (ft)	Freeboard Prov (ft)
4222	300	1582.97	1586.88	1586.95	0.000577	2.20	136.44	40.32	0.21	1588.20	1589.30	3.91	1.02	1.32	
4172	300	1582.80	1586.70	1586.89	0.002174	3.58	83.81	33.20	0.40	1587.82	1587.84	3.90	1.07	1.12	
4130	300	1582.73	1586.61	1586.80	0.002152	3.55	84.36	33.53	0.40	1587.60	1588.56	3.98	1.07	0.99	
4070	300	1582.59	1586.50	1586.68	0.001659	3.38	88.72	34.04	0.37	1588.00	1589.33	3.91	1.07	1.50	
4039	300	1582.53	1586.49	1586.62	0.001065	2.91	103.17	26.10	0.26	1588.33	1588.98	3.96	1.06	1.84	
4004	Culvert														
3953	300	1582.33	1586.12	1586.26	0.001218	3.04	98.73	26.07	0.28	1587.99	1588.61	3.79	1.02	1.87	
3915	300	1582.25	1585.96	1586.19	0.002674	3.87	77.54	31.91	0.44	1587.00	1588.90	3.71	1.04	1.94	
3819	300	1582.04	1585.68	1585.92	0.002809	3.93	76.32	31.87	0.45	1587.90	1589.11	3.64	1.03	2.22	
3715	300	1581.80	1585.36	1585.62	0.003119	4.09	73.44	31.32	0.47	1587.80	1589.14	3.56	1.02	2.44	
3663	300	1581.57	1585.22	1585.46	0.002787	3.92	76.60	31.99	0.45	1587.80	1588.70	3.65	1.03	2.58	
3635	300	1581.44	1585.15	1585.38	0.002613	3.83	78.43	32.32	0.43	1587.70	1588.57	3.71	1.04	2.55	
3582	300	1581.19	1585.03	1585.25	0.002239	3.75	78.99	29.78	0.40	1587.23	1587.03	3.94	1.07	2.00	
3581	Int Struct														
3579	300	1579.95	1583.86	1584.21	0.004005	4.74	63.31	25.18	0.53	1587.21	1586.88	4.90	1.40	3.02	
3594	300	1578.70	1583.90	1584.13	0.002489	3.84	78.11	30.25	0.42	1587.02	1586.40	5.20	1.41	2.50	
3561	300	1579.71	1583.16	1584.05	0.016160	7.55	39.76	23.04	1.01	1586.89	1586.40	3.45	1.31	3.24	
3467	300	1579.00	1582.50	1582.81	0.004580	4.51	66.59	33.05	0.56	1585.10	1584.55	3.50	1.03	2.05	
3374	300	1578.30	1582.30	1582.51	0.002052	3.70	81.10	28.57	0.39	1583.20	1582.91	4.00	1.11	0.61	
3373	Int Struct														
3371	300	1576.07	1580.98	1581.30	0.006706	5.66	52.99	22.05	0.64	1583.36	1582.90	4.81	1.45	2.02	
3359	300	1575.82	1581.00	1581.24	0.002647	3.91	76.65	30.23	0.43	1583.42	1582.70	5.18	1.41	1.70	
3353	300	1576.82	1580.29	1581.16	0.015790	7.48	40.09	23.11	1.00	1583.22	1582.64	3.47	1.30	2.35	
3276	300	1576.24	1579.23	1579.86	0.011545	6.38	47.00	27.66	0.86	1582.40	1582.03	2.99	1.06	2.00	
3216	300	1575.79	1578.94	1579.31	0.005728	4.87	61.57	32.20	0.62	1581.40	1580.73	3.15	1.00	1.79	
3156	300	1575.31	1578.04	1579.04	0.002516	3.56	84.27	38.12	0.42	1580.80	1579.34	3.50	1.00	0.50	
3155	Int Struct														
3152	300	1572.09	1576.77	1577.04	0.003261	4.13	72.56	31.02	0.48	1578.10	1578.13	4.68	1.30	1.33	
3138	300	1571.86	1576.76	1576.98	0.002956	3.77	79.48	32.42	0.42	1577.91	1577.91	4.90	1.34	1.15	
3135	300	1572.86	1576.31	1576.93	0.011152	6.29	47.70	27.67	0.84	1577.86	1577.90	3.45	1.17	1.55	
3110	300	1572.67	1576.04	1576.65	0.010850	6.25	47.99	27.72	0.84	1577.58	1577.58	3.37	1.15	1.54	
3014	300	1571.95	1575.00	1575.61	0.010923	6.25	47.99	27.94	0.84	1576.51	1576.51	3.05	1.07	1.51	
2918	300	1571.20	1574.18	1574.67	0.008218	5.59	53.71	30.00	0.74	1575.43	1575.43	2.98	1.00	1.25	
2822	300	1570.50	1573.89	1574.12	0.003236	3.92	76.54	35.19	0.47	1574.36	1574.36	3.39	1.00	0.47	
2797	300	1570.30	1573.84	1574.04	0.002621	3.63	82.62	37.37	0.43	1574.17	1574.17	3.54	1.00	0.33	
2796	Int Struct														
2794	300	1568.08	1572.74	1573.01	0.003367	4.19	71.66	30.83	0.48	1574.12	1574.12	4.66	1.30	1.38	
2779	300	1567.85	1572.72	1572.95	0.002625	3.81	78.66	32.24	0.43	1573.90	1573.90	4.87	1.33	1.18	
2776	300	1568.85	1572.20	1572.89	0.013016	6.65	45.11	26.93	0.91	1573.85	1573.85	3.35	1.18	1.65	
2751	300	1568.66	1571.84	1572.58	0.013511	6.79	44.21	26.63	0.93	1573.52	1573.52	3.18	1.15	1.68	
2668	300	1568.04	1571.02	1571.57	0.009690	5.57	50.23	23.66	0.80	1572.43	1572.43	2.98	1.02	1.41	
2586	300	1567.40	1570.78	1571.03	0.003459	4.03	74.45	35.48	0.49	1571.35	1571.35	3.38	1.00	0.57	
2561	300	1567.20	1570.74	1570.94	0.002633	3.64	82.40	37.34	0.43	1571.07	1571.10	3.54	1.00	0.33	
2559	Int Struct														
2557	300	1564.90	1569.66	1569.93	0.003263	4.14	72.51	31.01	0.48	1571.00	1571.02	4.68	1.30	1.34	
2543	300	1564.80	1569.65	1569.87	0.002573	3.78	79.42	32.50	0.43	1570.80	1570.80	4.85	1.32	1.15	
2540	300	1565.75	1569.23	1569.82	0.010714	6.18	48.52	27.91	0.83	1570.75	1570.75	3.48	1.17	1.52	
2513	300	1565.56	1568.96	1569.55	0.010483	6.17	48.03	27.92	0.82	1570.47	1570.47	3.40	1.15	1.51	
2408	300	1564.76	1567.84	1568.43	0.010601	6.18	48.55	28.14	0.83	1569.32	1569.32	3.00	1.07	1.46	
2302	300	1563.97	1566.87	1567.30	0.008824	5.73	52.37	29.71	0.76	1568.16	1568.16	2.90	1.00	1.29	
2196	300	1563.17	1566.52	1566.76	0.003297	3.94	76.09	36.17	0.48	1567.00	1567.00	3.35	1.00	0.48	
2171	300	1562.88	1566.47	1566.68	0.003607	3.66	81.91	37.25	0.44	1566.72	1566.82	3.49	1.00	0.25	
2170	Int Struct														
2168	300	1560.72	1565.30	1565.65	0.003387	4.10	71.69	30.74	0.48	1566.69	1566.77	4.66	1.30	1.31	
2153	300	1560.50	1565.36	1565.59	0.002655	3.83	78.23	32.12	0.43	1566.53	1566.50	4.86	1.33	1.14	
2150	300	1561.49	1564.78	1565.52	0.014412	6.93	43.32	26.32	0.95	1566.49	1566.49	3.29	1.20	1.71	
2125	300	1561.30	1564.40	1565.16	0.011646	7.00	42.84	26.16	0.96	1566.13	1566.10	3.10	1.16	1.70	
2071	300	1560.90	1563.98	1564.49	0.009524	5.69	52.99	29.33	0.75	1565.33	1565.33	3.09	1.02	1.35	
2015	300	1560.49	1563.85	1564.11	0.003655	4.12	72.78	34.92	0.50	1564.49	1564.49	3.36	1.00	0.64	
1950	300	1560.29	1563.82	1564.02	0.002561	3.60	83.30	37.49	0.43	1564.13	1564.13	3.53	1.00	0.31	
1969	Int Struct														
1968	300	1558.04	1562.70	1562.97	0.003360	4.17	71.94	30.82	0.48	1564.10	1564.08	4.88	1.30	1.38	
1972	300	1557.81	1562.69	1562.92	0.002601	3.80	78.85	32.25	0.43	1563.99	1563.98	4.88	1.33	1.17	
1959	300	1558.81	1562.04	1562.84	0.015946	7.19	41.71	25.88	1.00	1563.81	1563.81	3.23	1.21	1.77	
1944	300	1558.00	1561.69	1562.45	0.011631	6.93	42.89	26.22	0.96	1563.43	1563.40	3.09	1.15	1.71	
1896	300	1558.27	1561.37	1561.86	0.008189	5.61	53.49	29.55	0.73	1562.69	1562.69	3.10	1.02	1.32	
1849	300	1557.92	1561.27	1561.54	0.003791	4.19	71.68	34.47	0.51	1561.96	1562.62	3.35	1.00	0.69	
1824	300	1557.70	1561.24	1561.44	0.002625	3.63	82.56	37.35	0.43	1561.57	1561.60	3.54	1.00	0.33	
1822	Int Struct														
1821	300	1555.48	1560.14	1560.41	0.003364	4.18	71.70	30.83	0.48	1561.52	1561.52	4.68	1.30	1.39	
1806	300	1555.25	1560.12	1560.35	0.002643	3.82	78.61	32.23	0.43	1561.30	1561.30	4.87	1.33	1.18	
1803	300	1556.30	1559.51	1560.28	0.015862	7.05	42.58	26.10	0.97	1561.20	1561.25	3.21	1.19	1.69	
1778	300	1556.06	1559.11	1559.90	0.015490	7.15	41.96	25.92	0.99	1560.86	1560.90	3.05	1.16	1.75	
1731	300	1555.70	1558.80	1559.29	0.008204	5.61	53.44	29.53	0.74	1560.13	1560.13	3.10	1.02	1.33	
1683	300	1555.35	1558.70	1558.97	0.003793	4.18	71.72	34.54	0.51	1559.39	1559.40	3.35	1.00	0.69	
1658	300	1555.16	1558.66	1558.87	0.002707	3.67	81.66	37.17	0.44	1559.00	1559.00	3.50	1.00	0.34	
1657	Int Struct														
1655	300	1552.91	1557.63	1557.88	0.003131	4.07	73.68	31.12	0.47	1558.95	1558.95	4.72	1.31	1.32	
1640	300	1552.68	1557.61	1557.83	0.002403	3.73	80.39	32.63	0.42	1558.73	1558.70	4.93	1.34	1.09	
1631	300	1553.68	1557.24	1557.78	0.009394	5.91	50.80	28.45	0.78	1558.60	1558.70	3.56	1.16	1.44	
1612	300	1553.49	1557.00	1557.55	0.009394	5.92	50.69	28.53	0.78	1558.40	1558.44	3.51</			

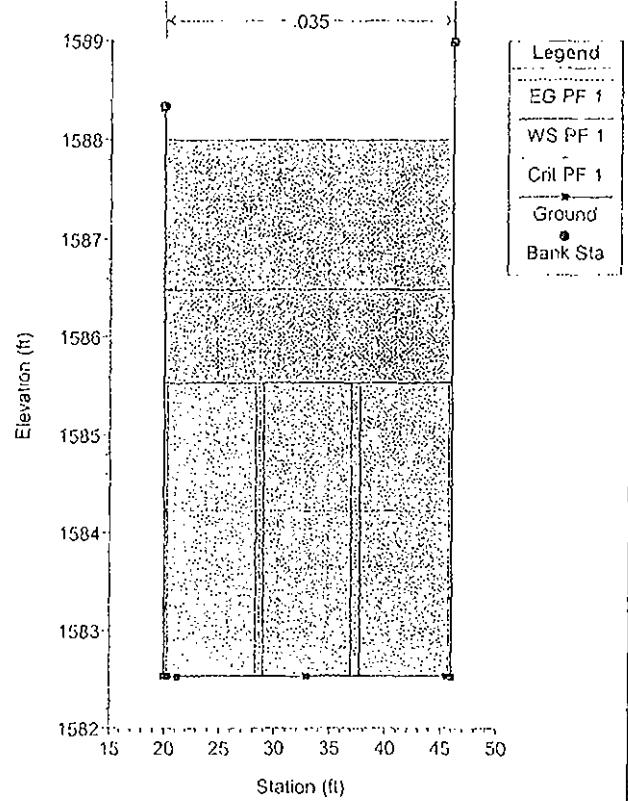




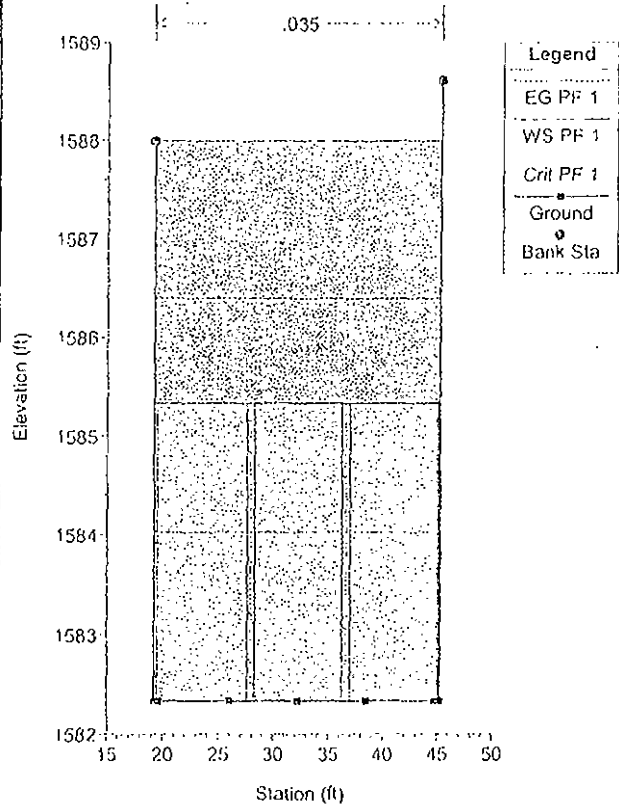
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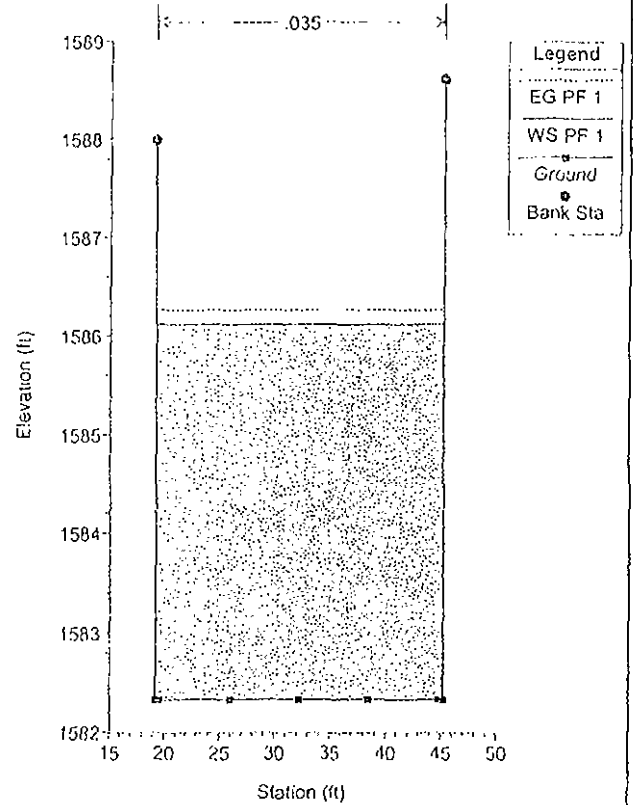
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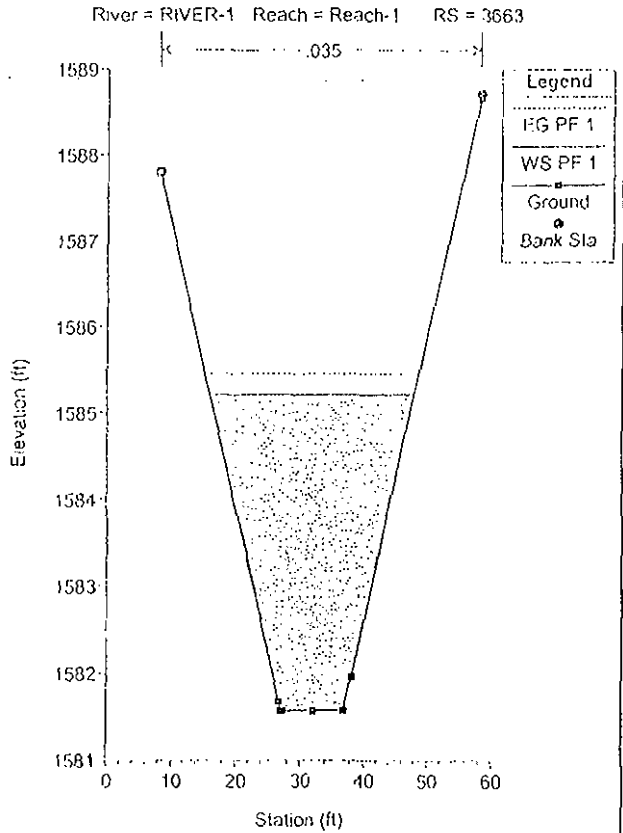
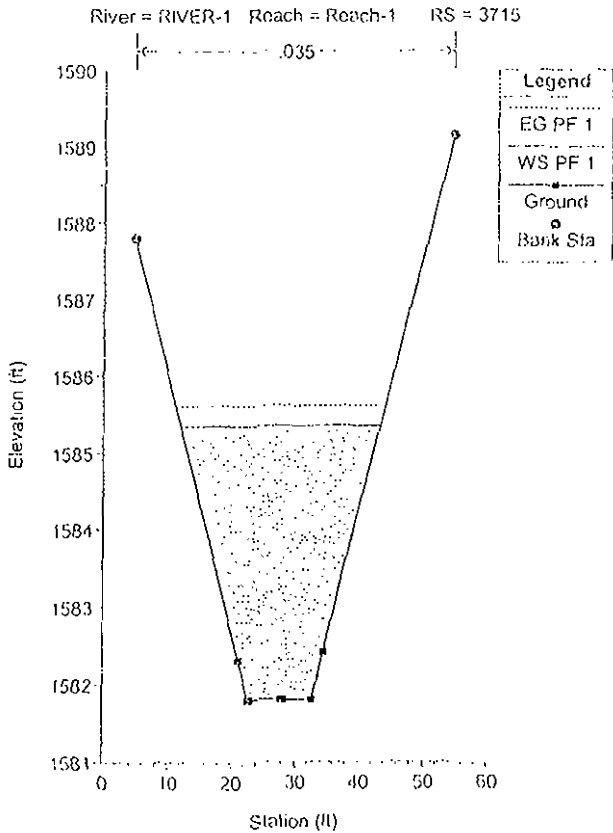
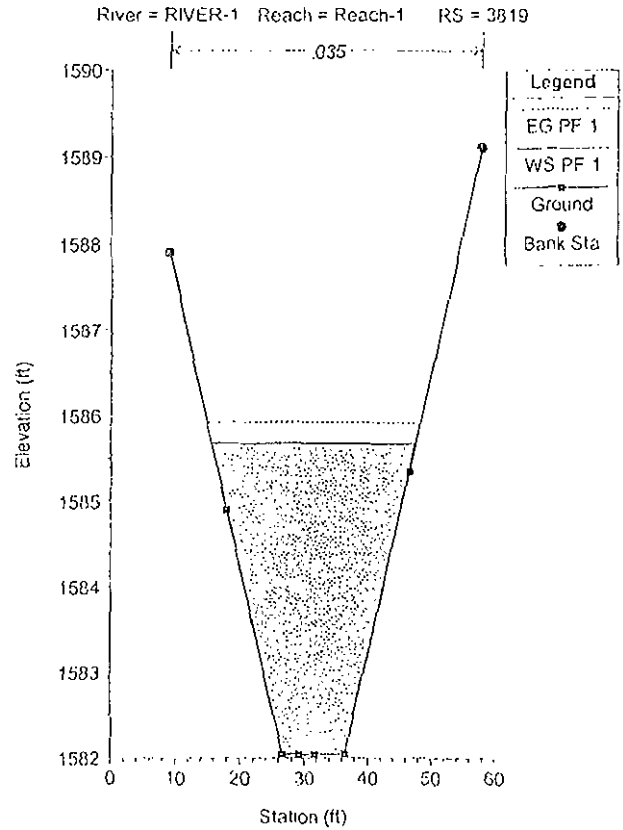
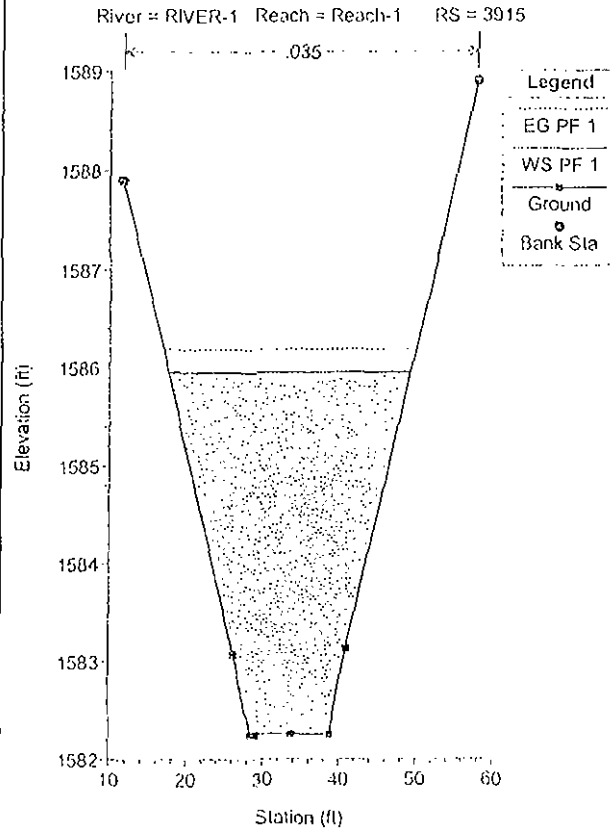


River = RIVER-1 Reach = Reach-1 RS = 4004 Culv

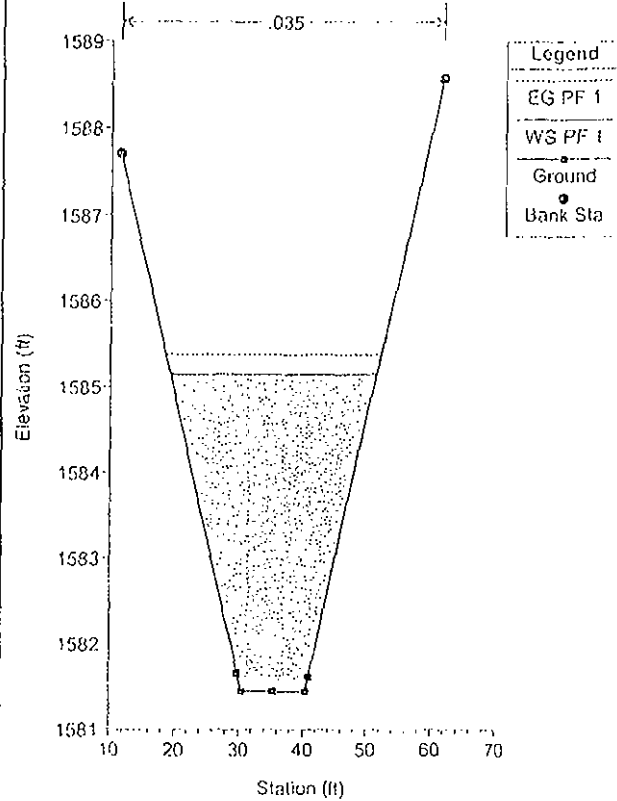


River = RIVER-1 Reach = Reach-1 RS = 3953

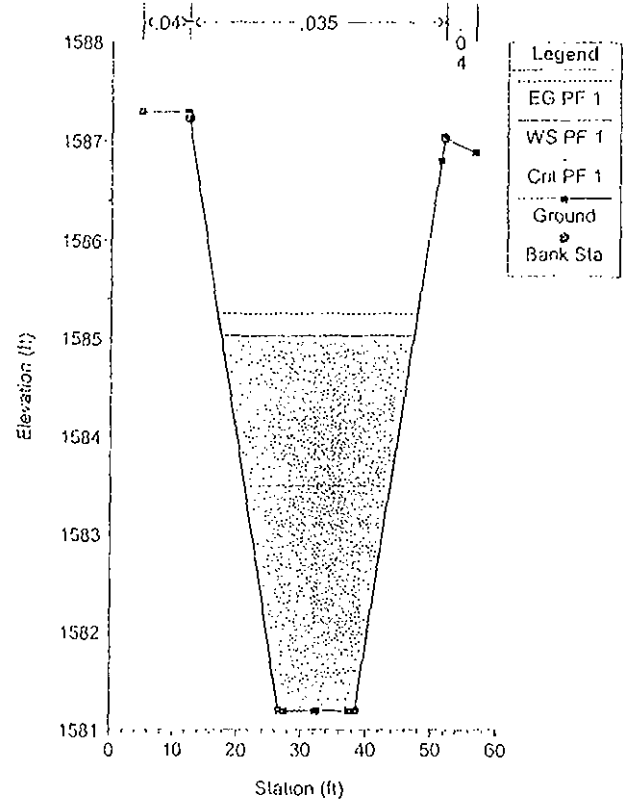




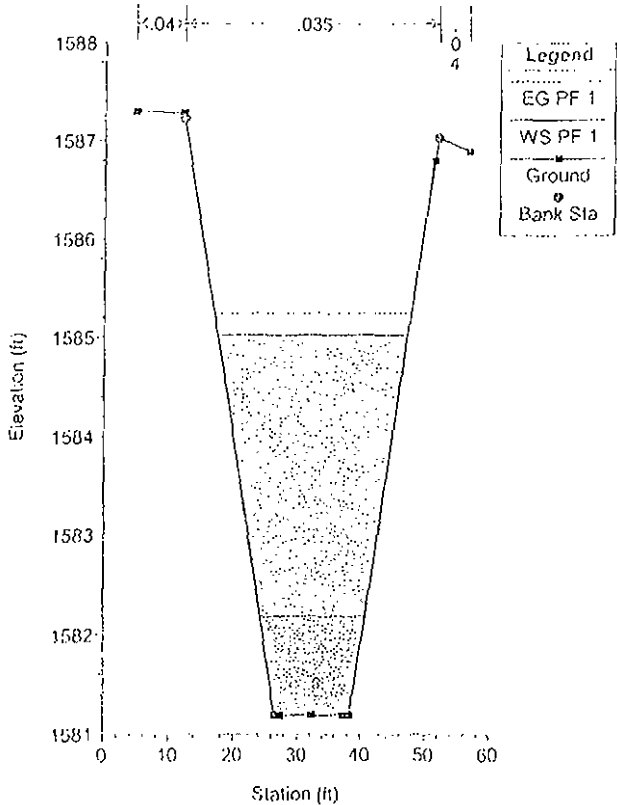
River = RIVER-1 Reach = Reach-1 RS = 3635



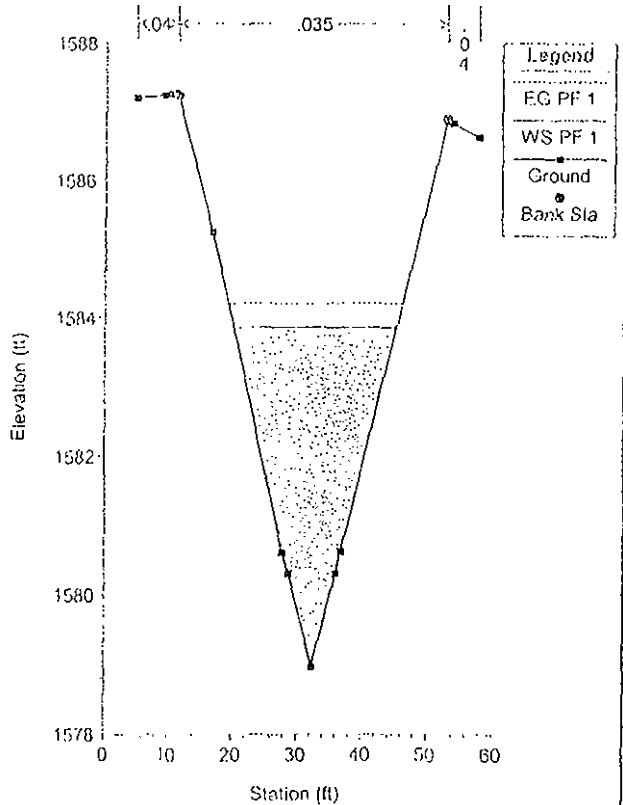
River = RIVER-1 Reach = Reach-1 RS = 3582



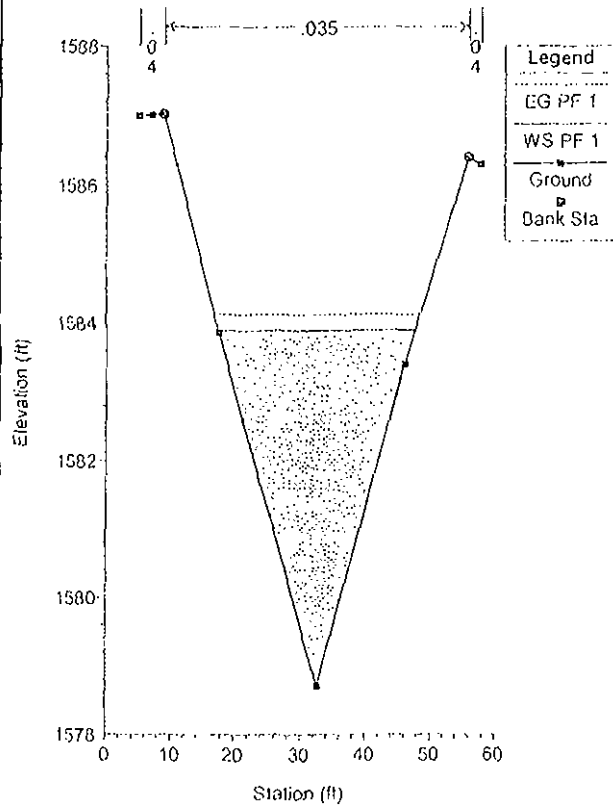
River = RIVER-1 Reach = Reach-1 RS = 3581 IS



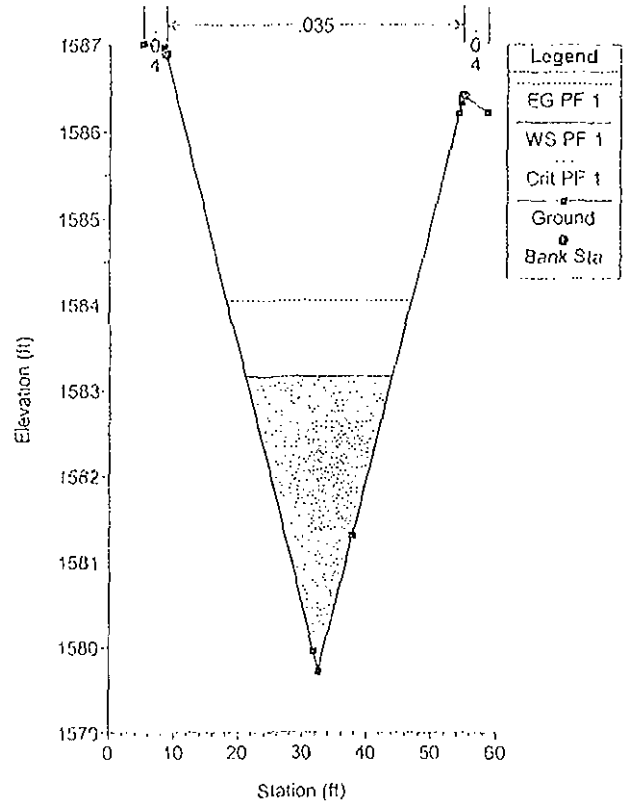
River = RIVER-1 Reach = Reach-1 RS = 3579



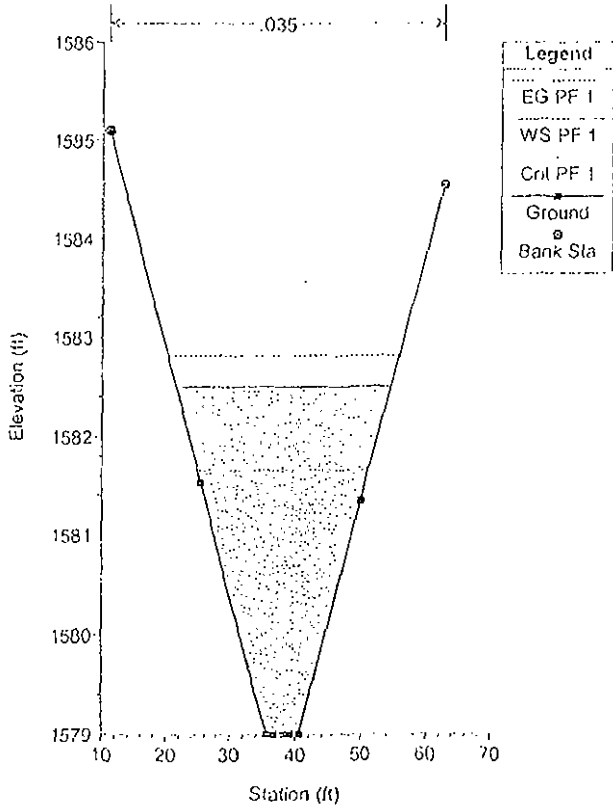
River = RIVER-1 Reach = Reach-1 RS = 3564



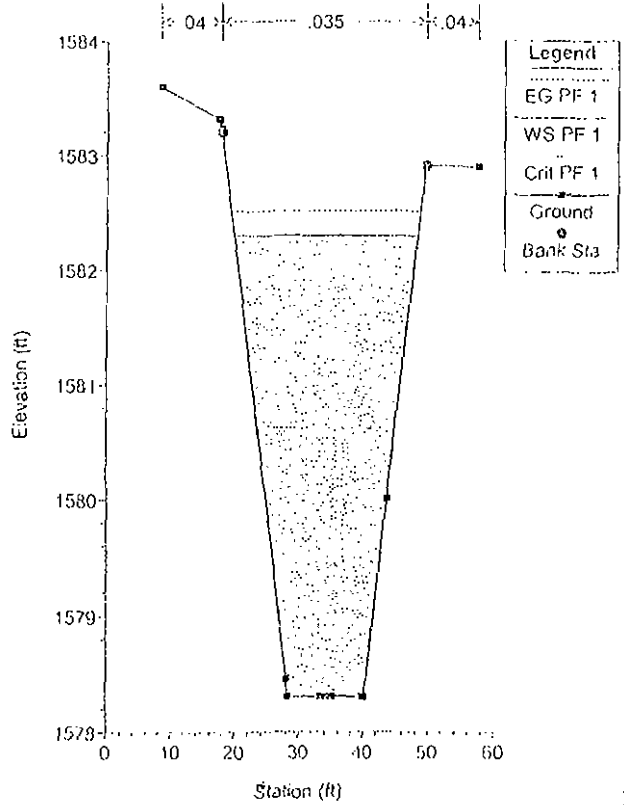
River = RIVER-1 Reach = Reach-1 RS = 3561



River = RIVER-1 Reach = Reach-1 RS = 3467

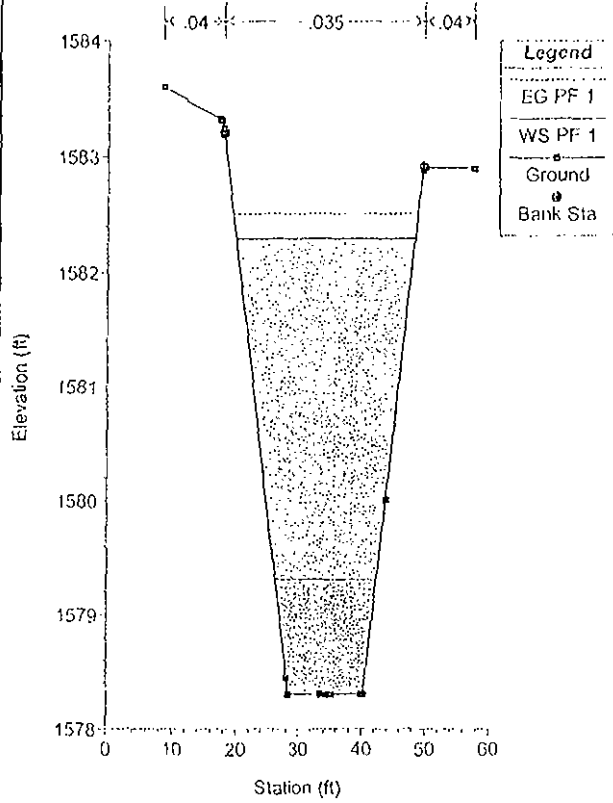


River = RIVER-1 Reach = Reach-1 RS = 3374

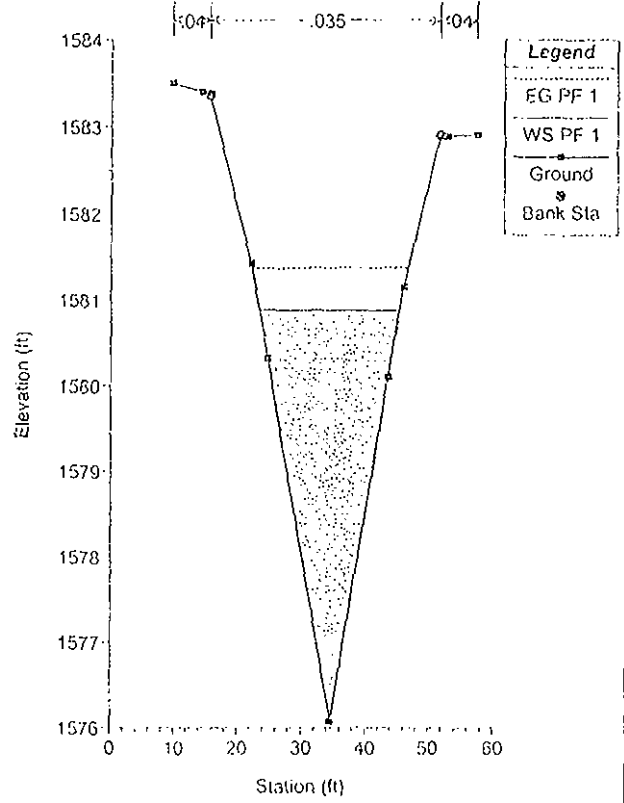




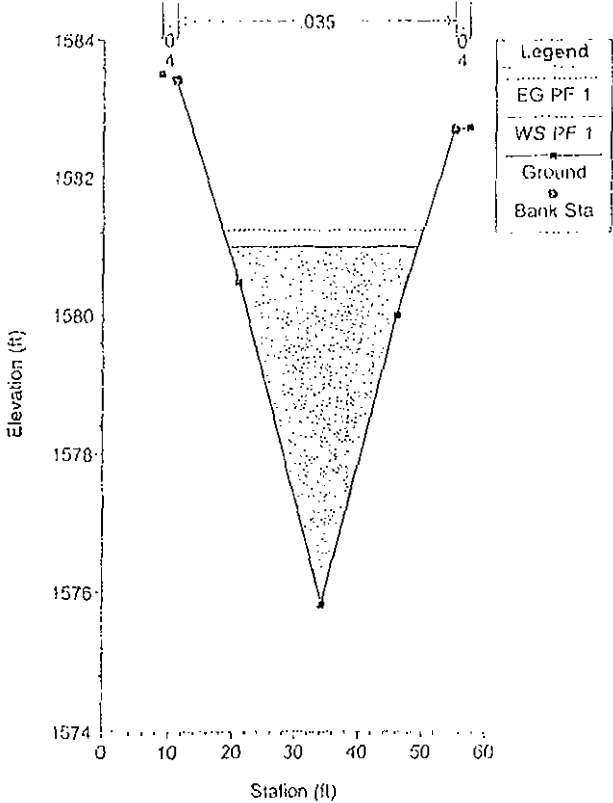
River = RIVER-1 Reach = Reach-1 RS = 3373 IS



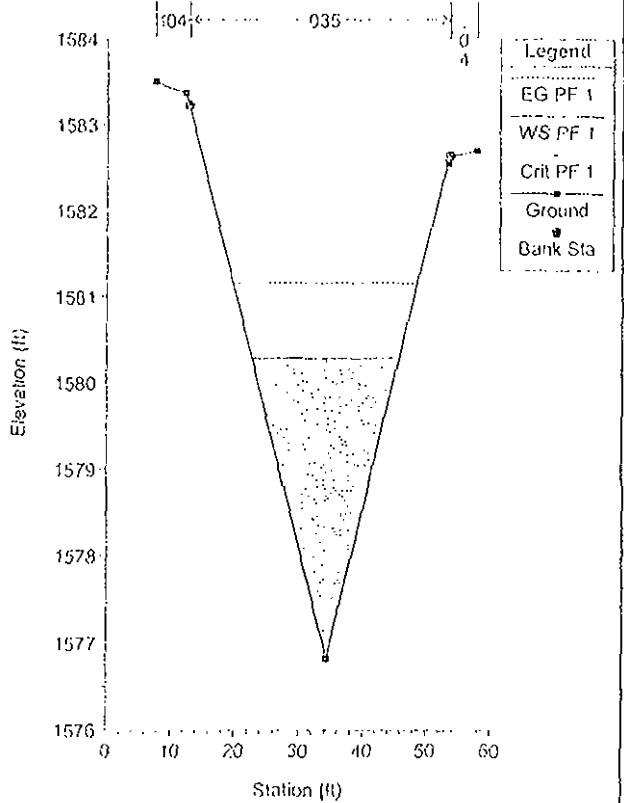
River = RIVER-1 Reach = Reach-1 RS = 3371



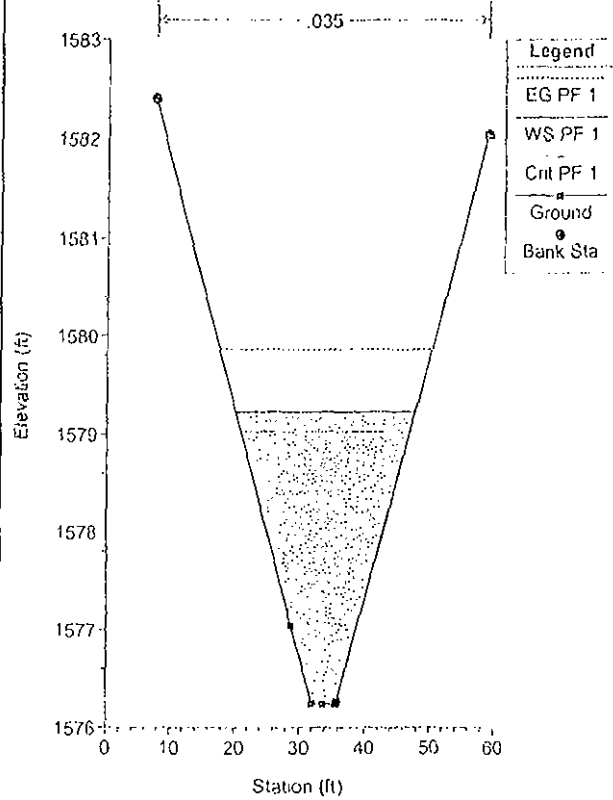
River = RIVER-1 Reach = Reach-1 RS = 3356



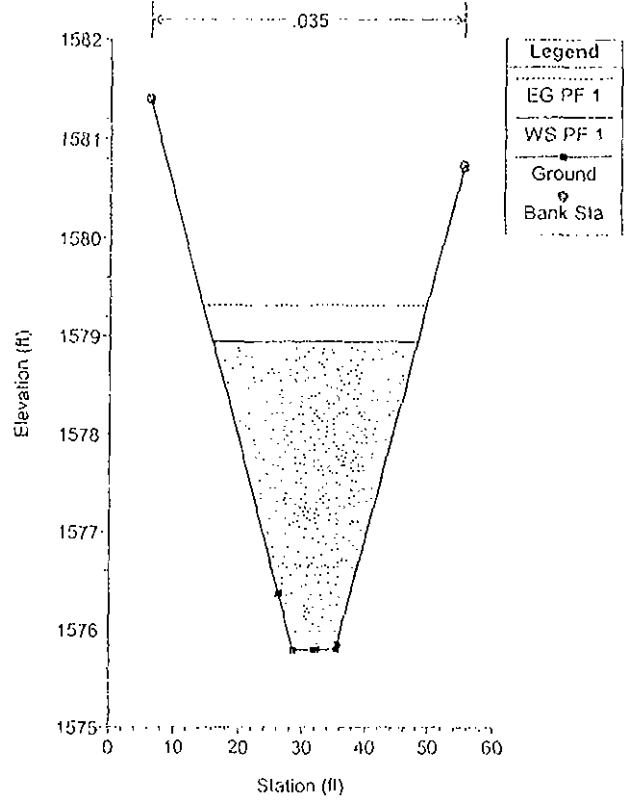
River = RIVER-1 Reach = Reach-1 RS = 3353



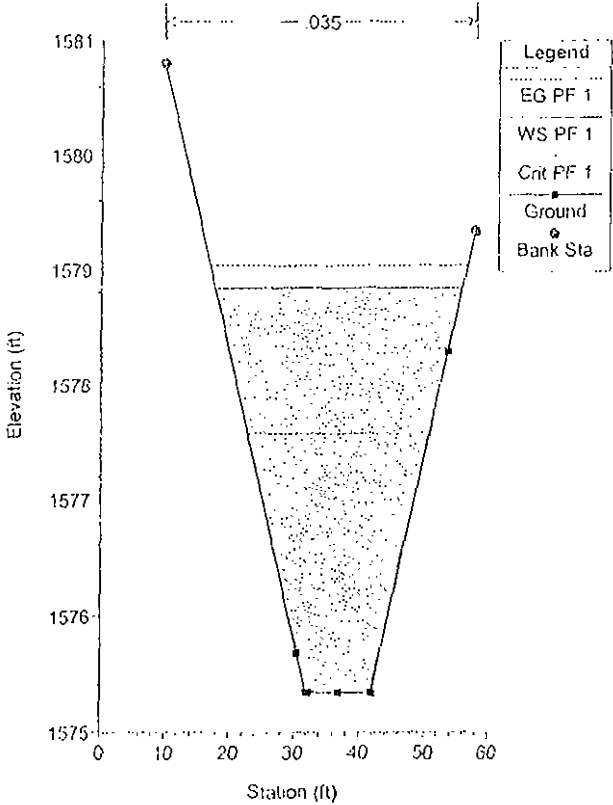
River = RIVER-1 Reach = Reach-1 RS = 3276



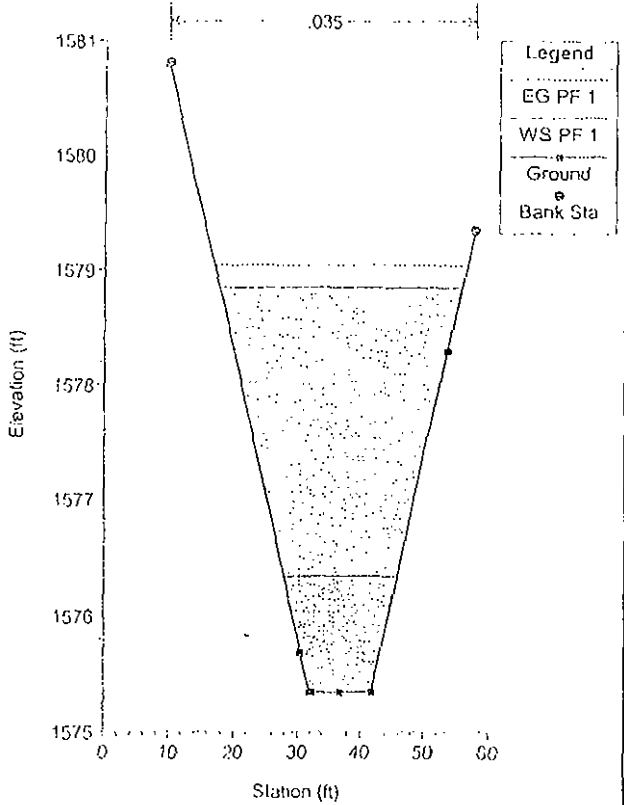
River = RIVER-1 Reach = Reach-1 RS = 3216



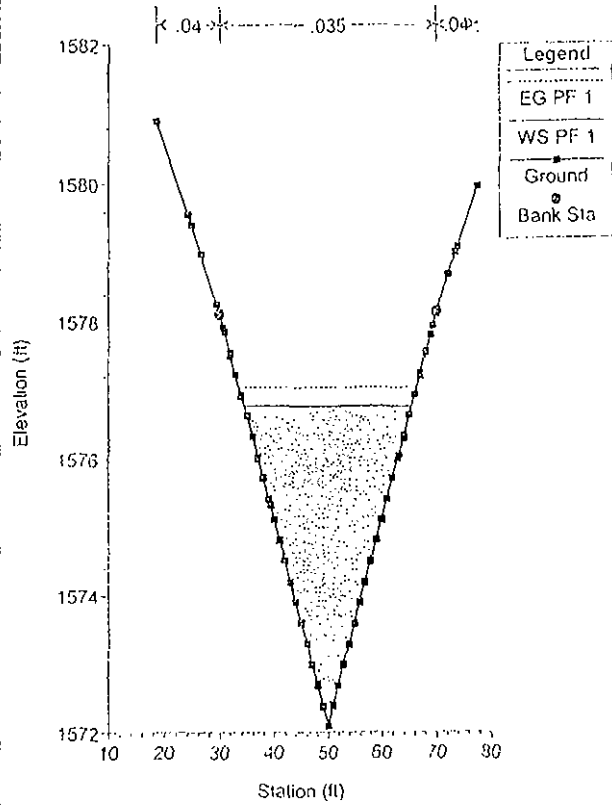
River = RIVER-1 Reach = Reach-1 RS = 3156



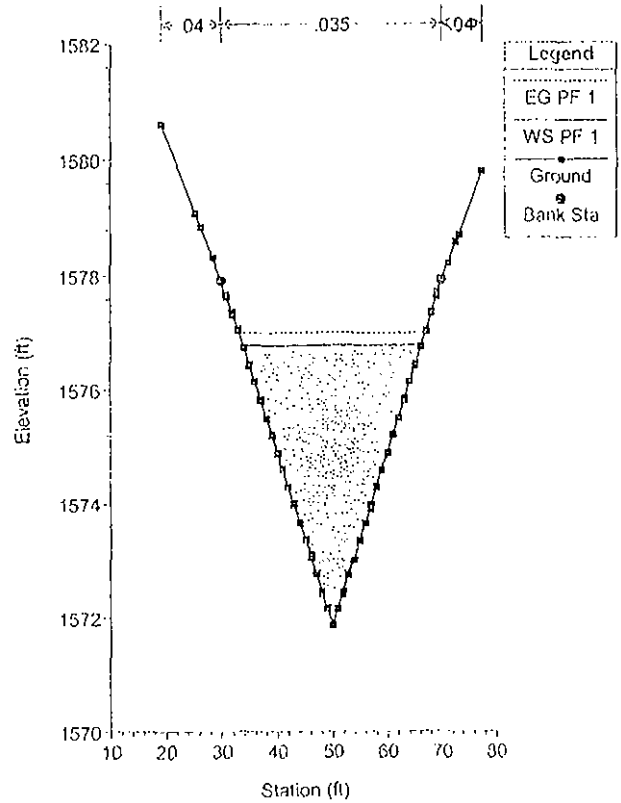
River = RIVER-1 Reach = Reach-1 RS = 3155 IS



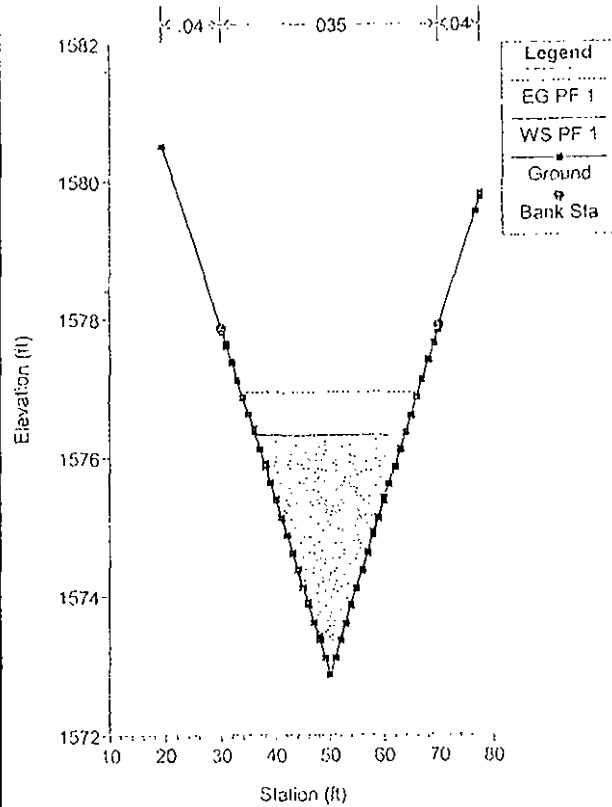
River = RIVER-1 Reach = Reach-1 RS = 3152



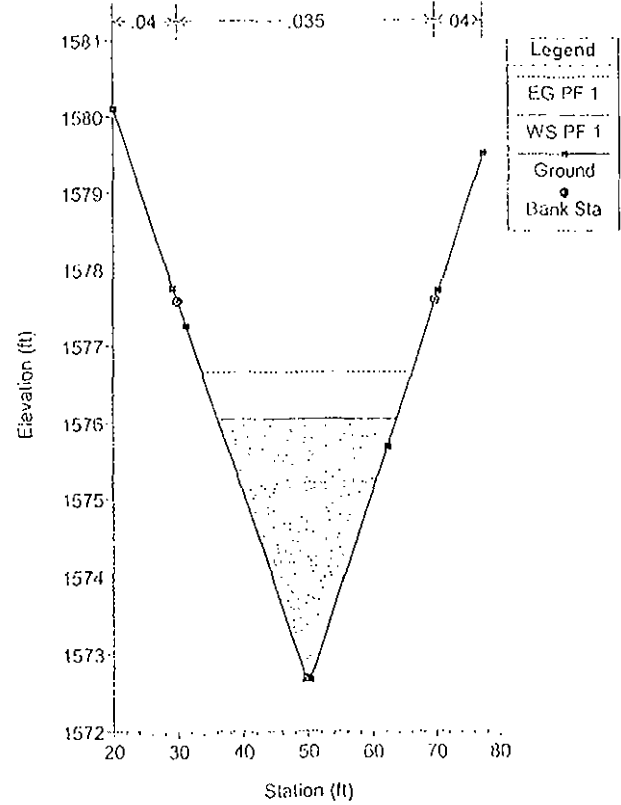
River = RIVER-1 Reach = Reach-1 RS = 3138

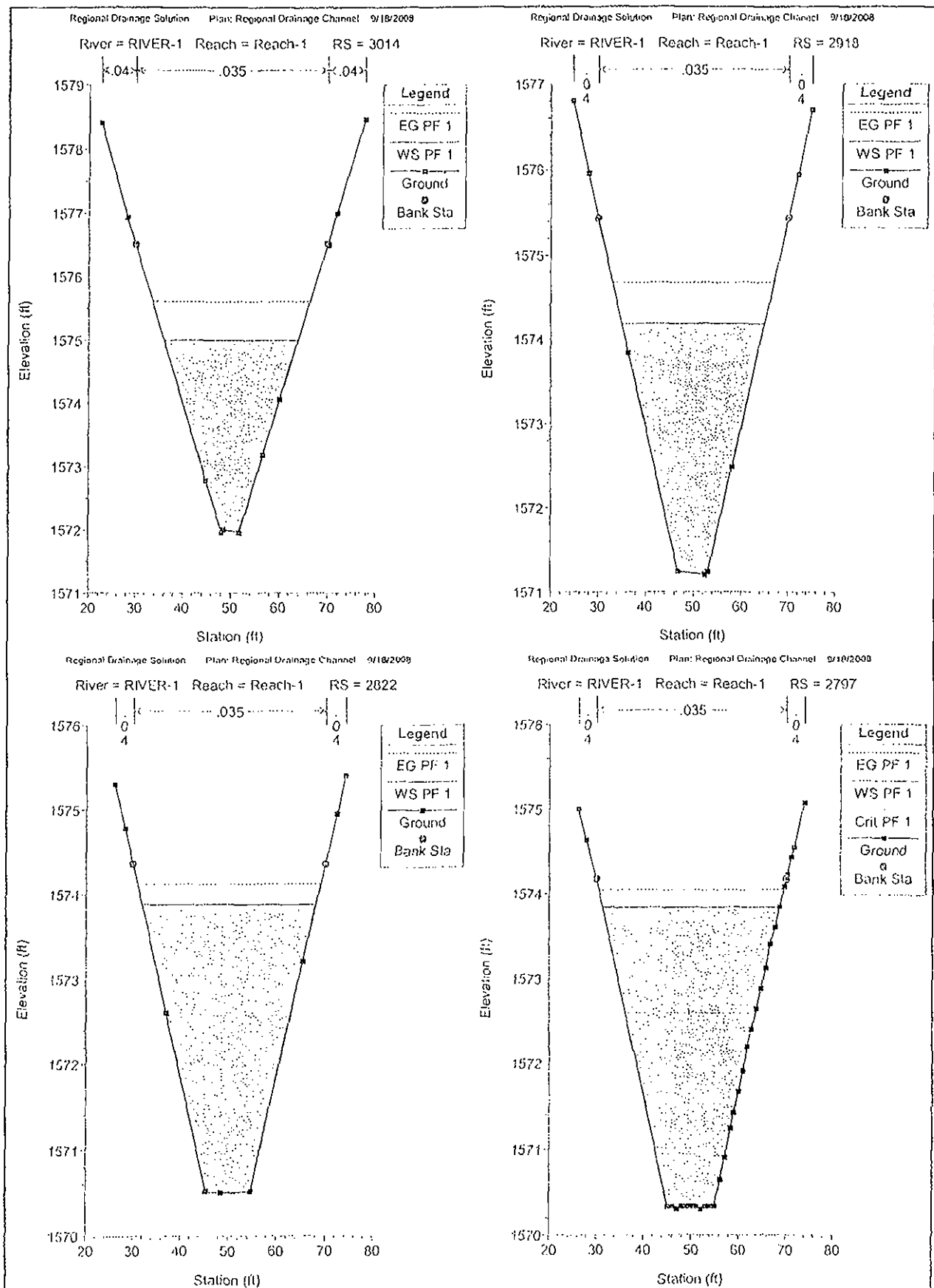


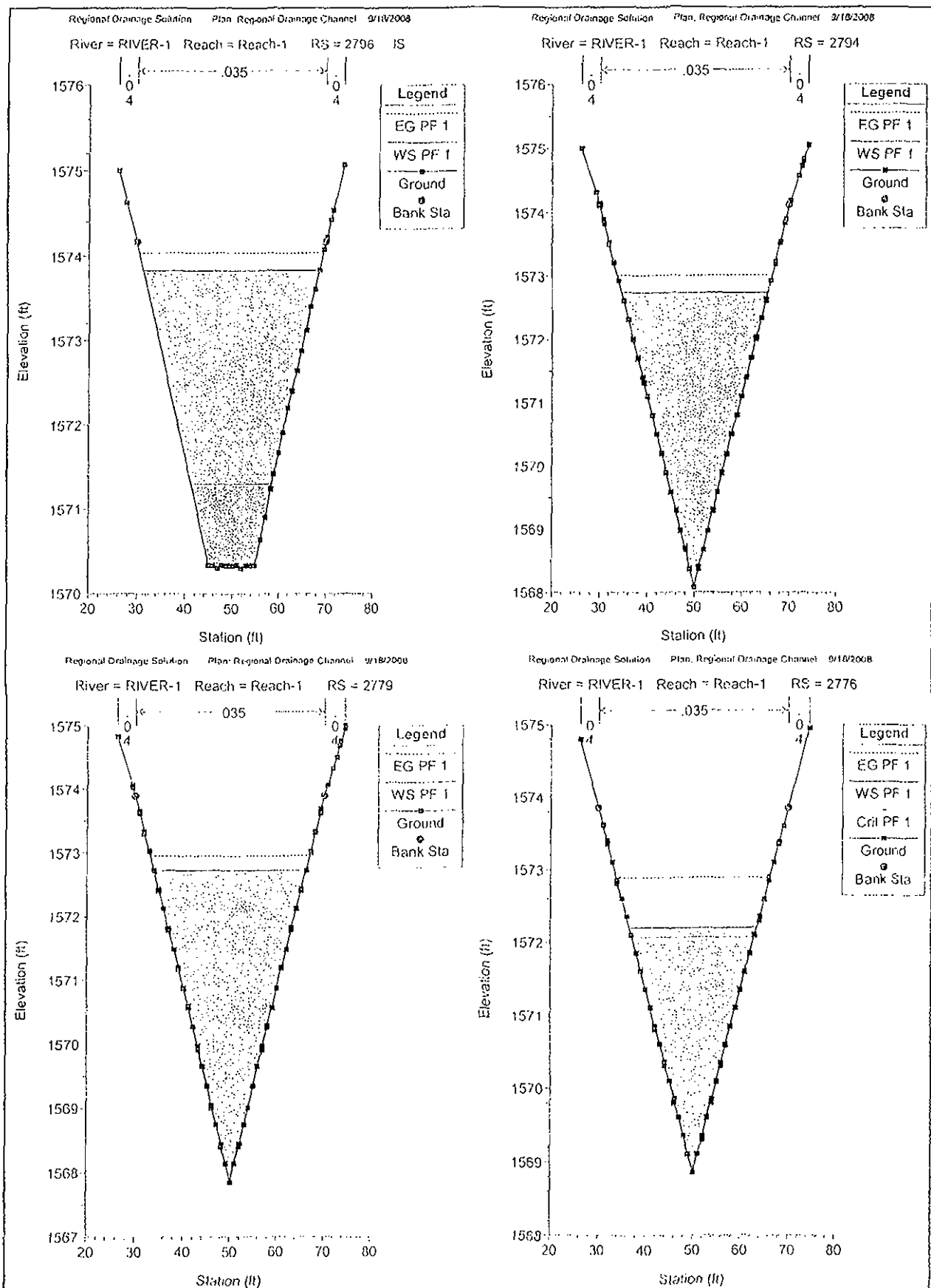
River = RIVER-1 Reach = Reach-1 RS = 3135

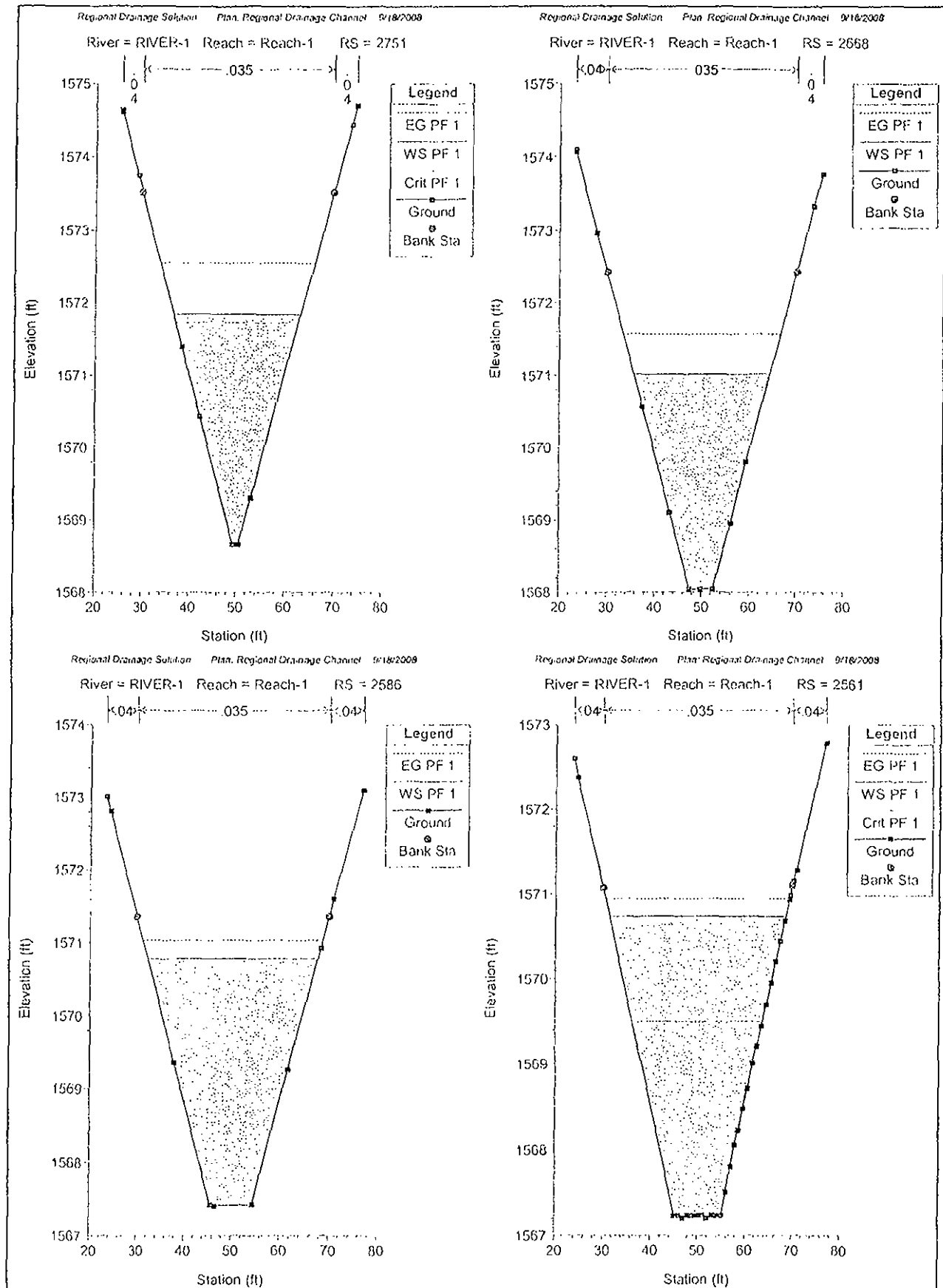


River = RIVER-1 Reach = Reach-1 RS = 3110

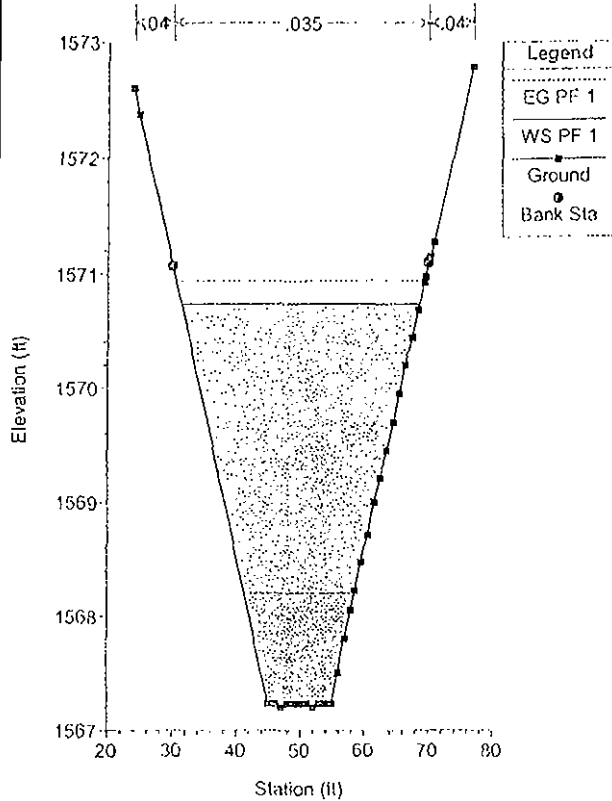




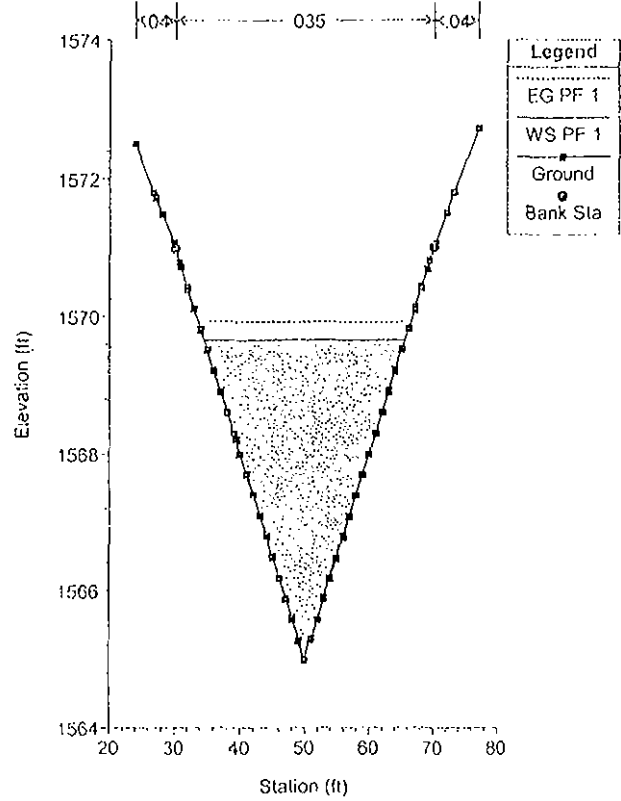




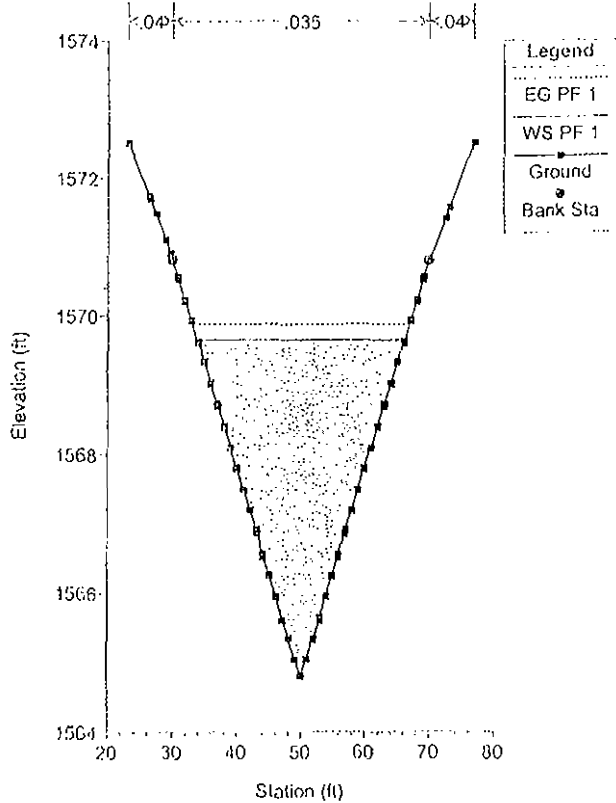
River = RIVER-1 Reach = Reach-1 RS = 2559 IS



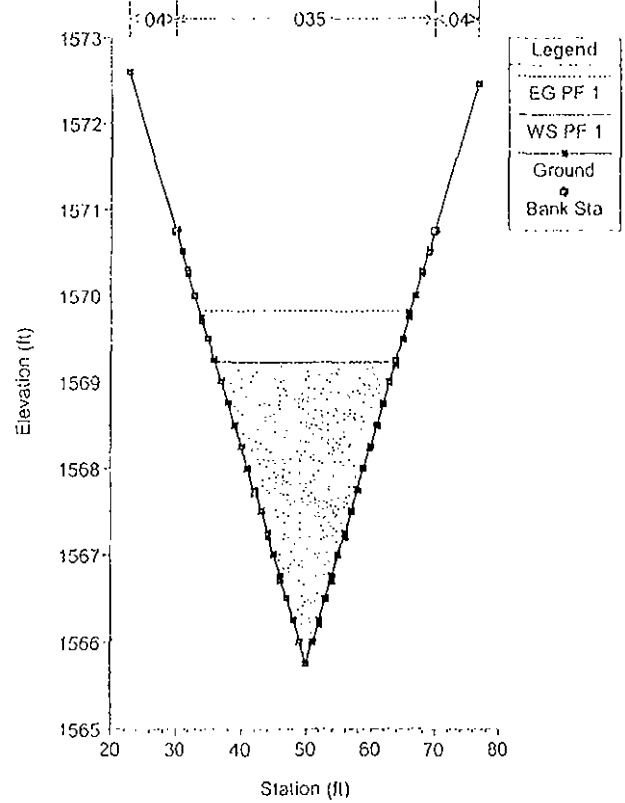
River = RIVER-1 Reach = Reach-1 RS = 2557



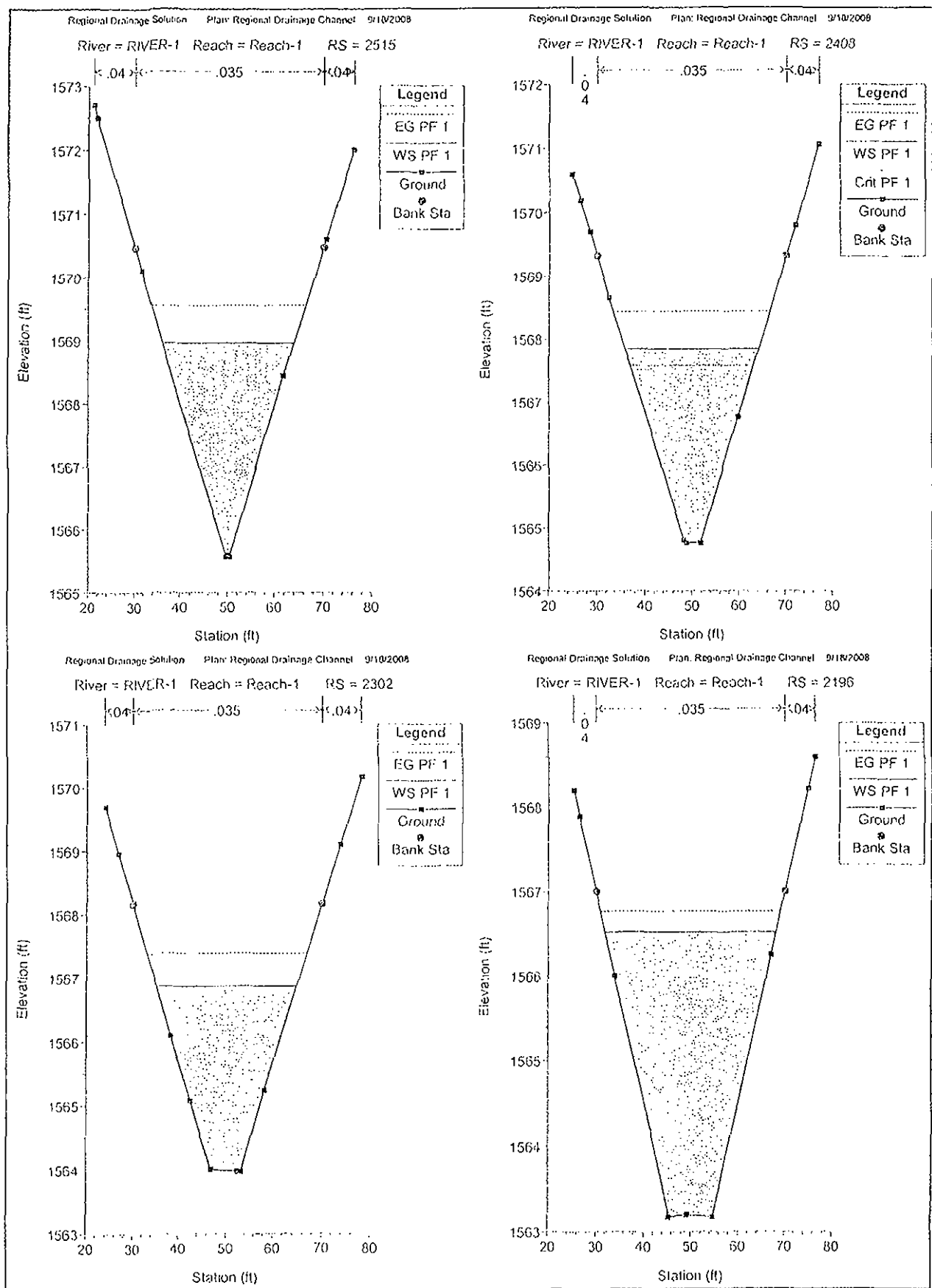
River = RIVER-1 Reach = Reach-1 RS = 2543



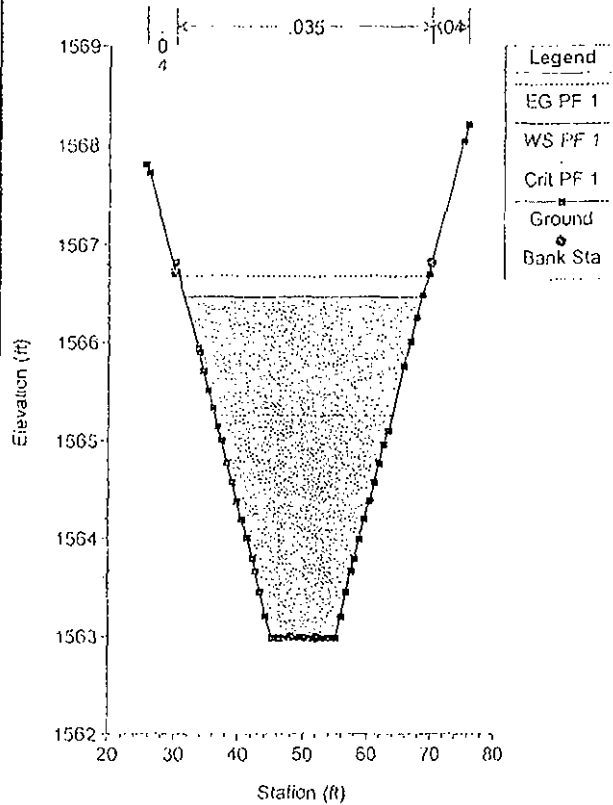
River = RIVER-1 Reach = Reach-1 RS = 2540



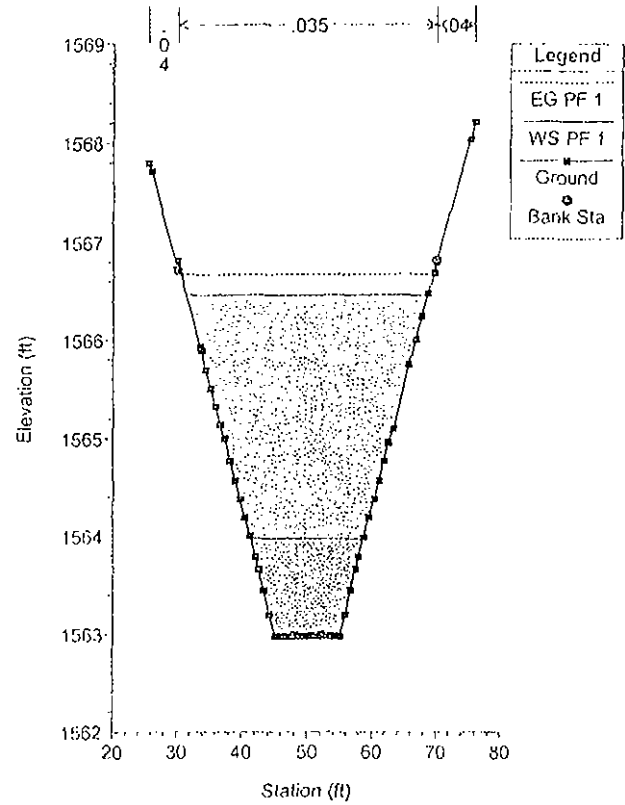




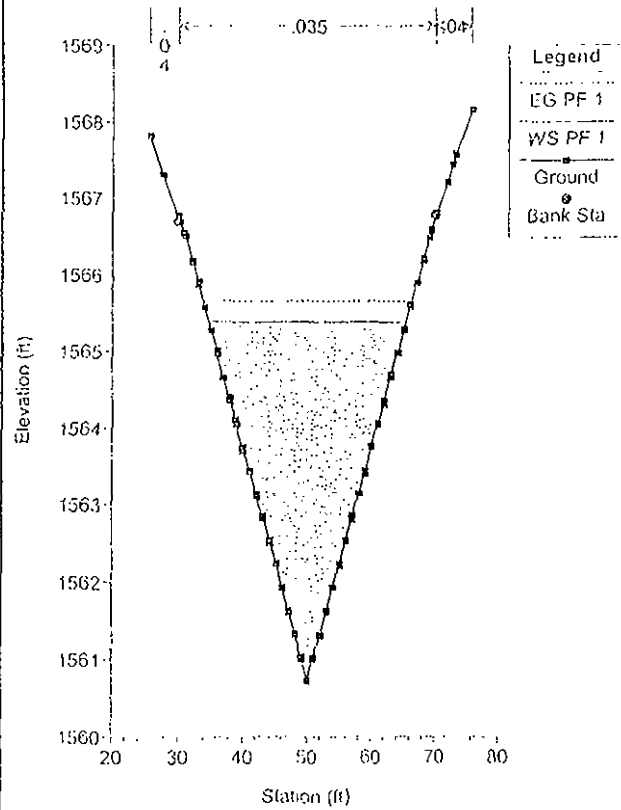
River = RIVER-1 Reach = Reach-1 RS = 2171



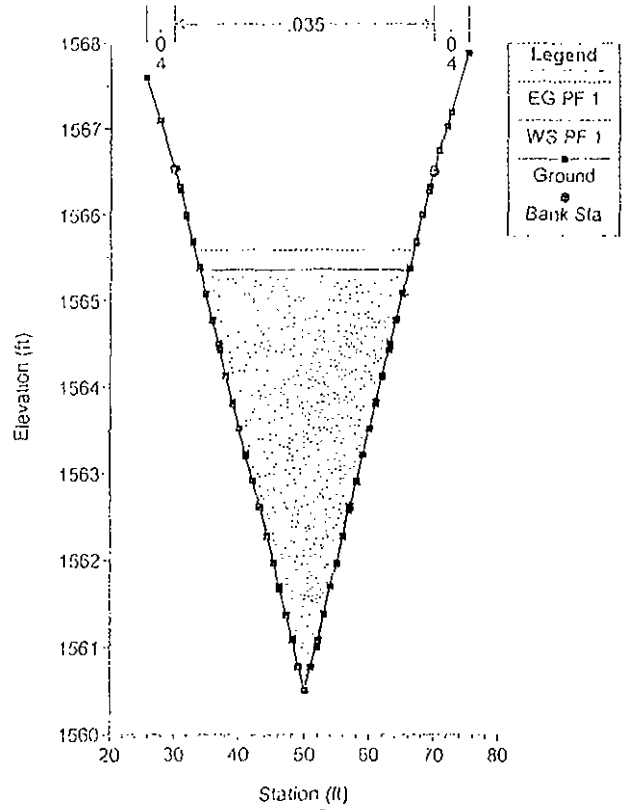
River = RIVER-1 Reach = Reach-1 RS = 2170 IS



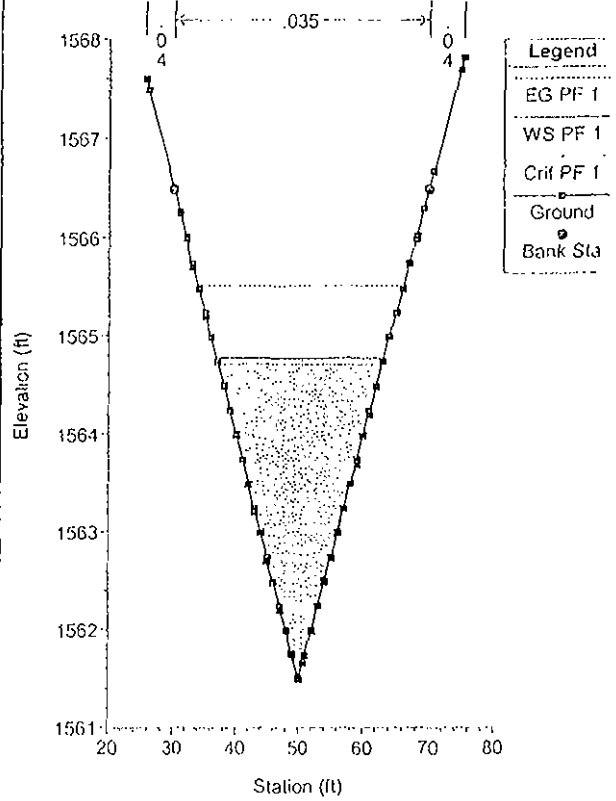
River = RIVER-1 Reach = Reach-1 RS = 2168



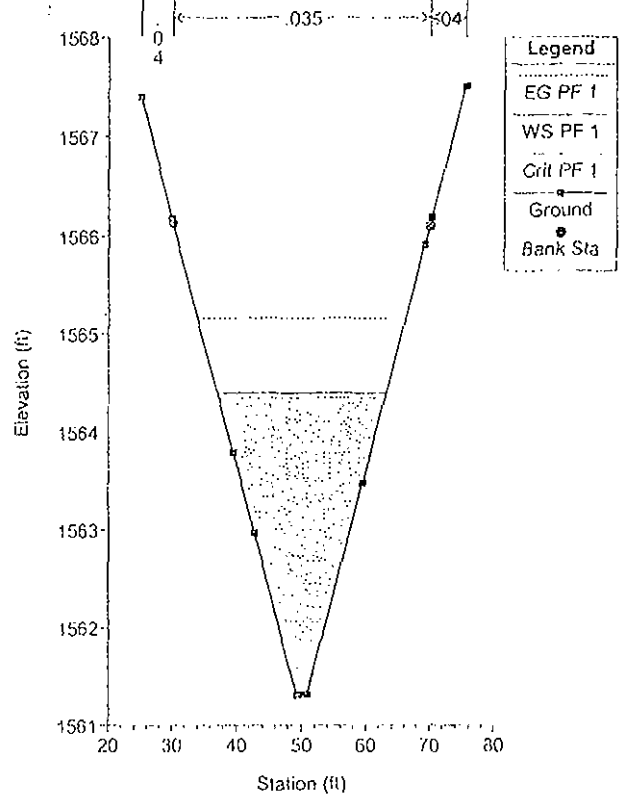
River = RIVER-1 Reach = Reach-1 RS = 2153



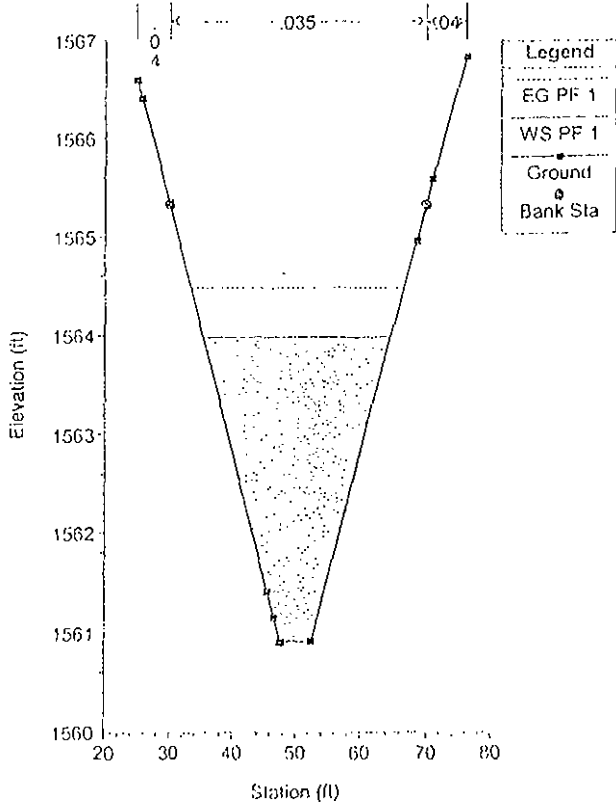
River = RIVER-1 Reach = Reach-1 RS = 2150



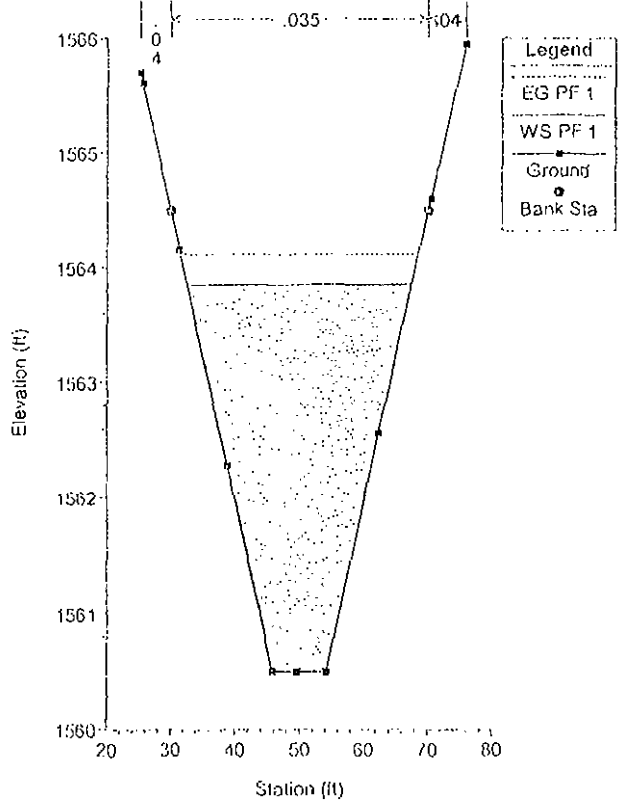
River = RIVER-1 Reach = Reach-1 RS = 2125

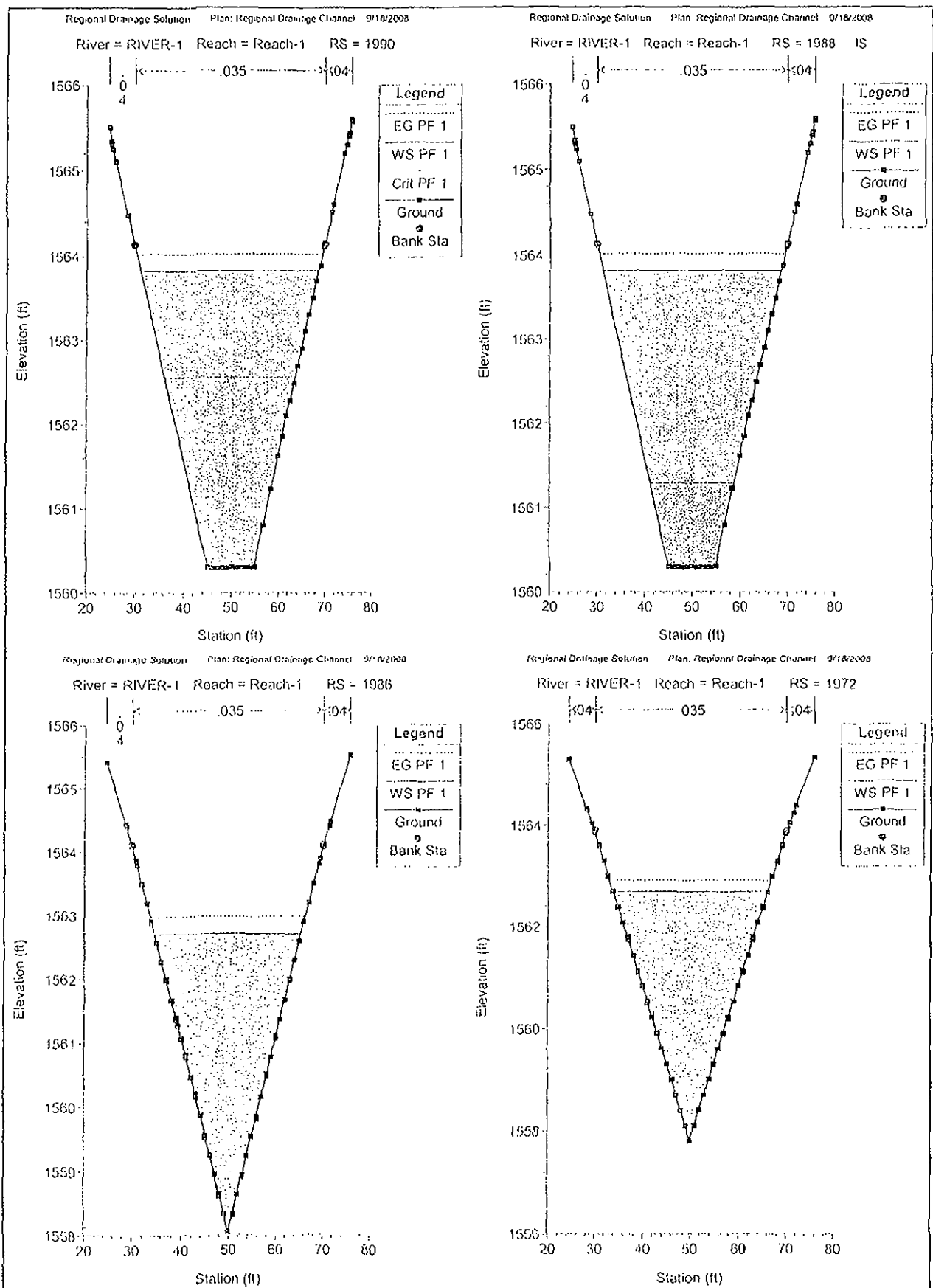


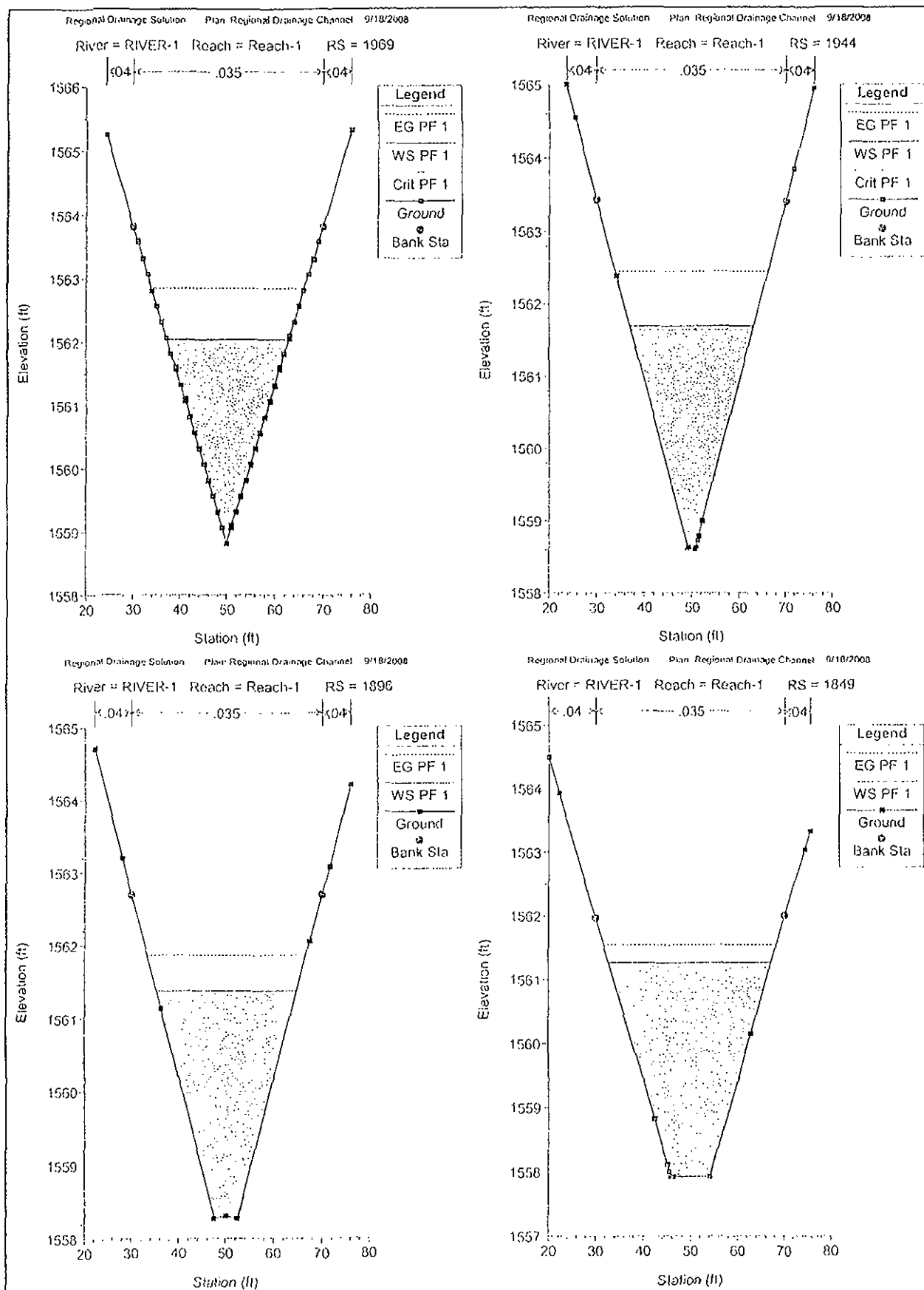
River = RIVER-1 Reach = Reach-1 RS = 2071



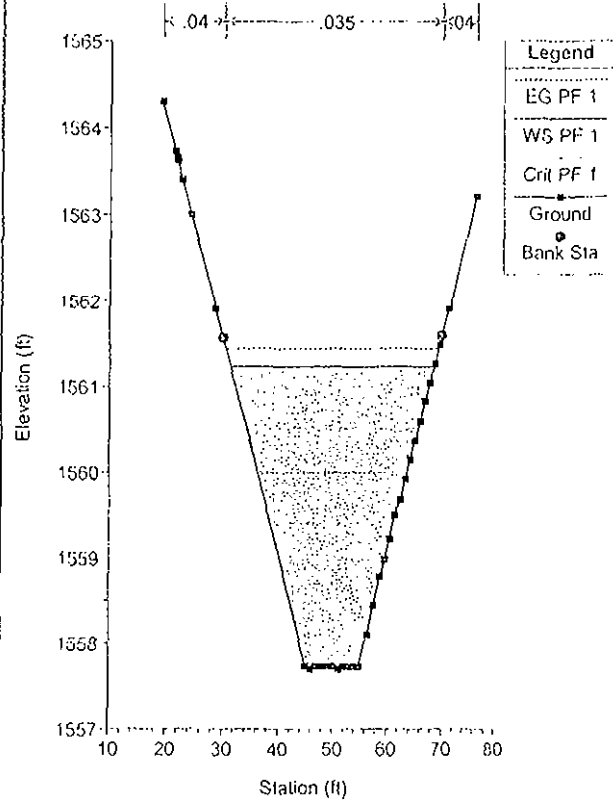
River = RIVER-1 Reach = Reach-1 RS = 2015



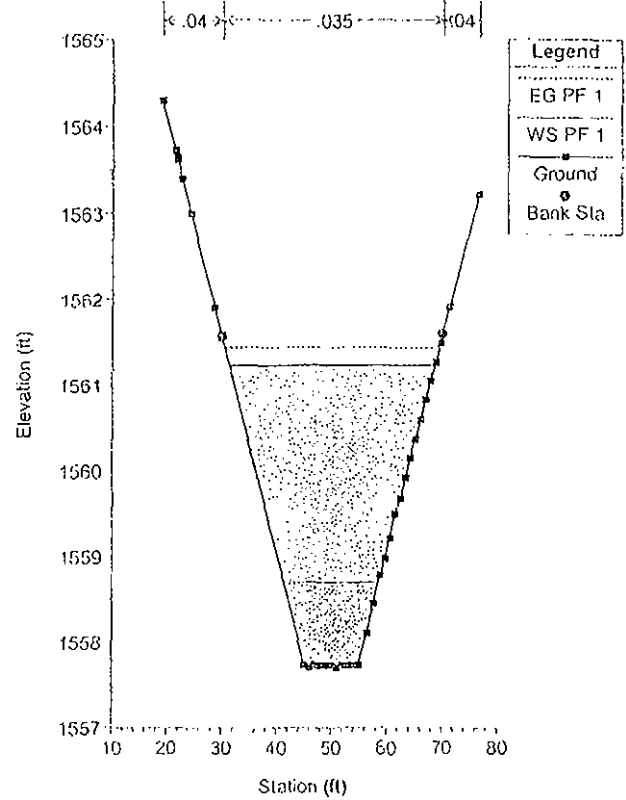




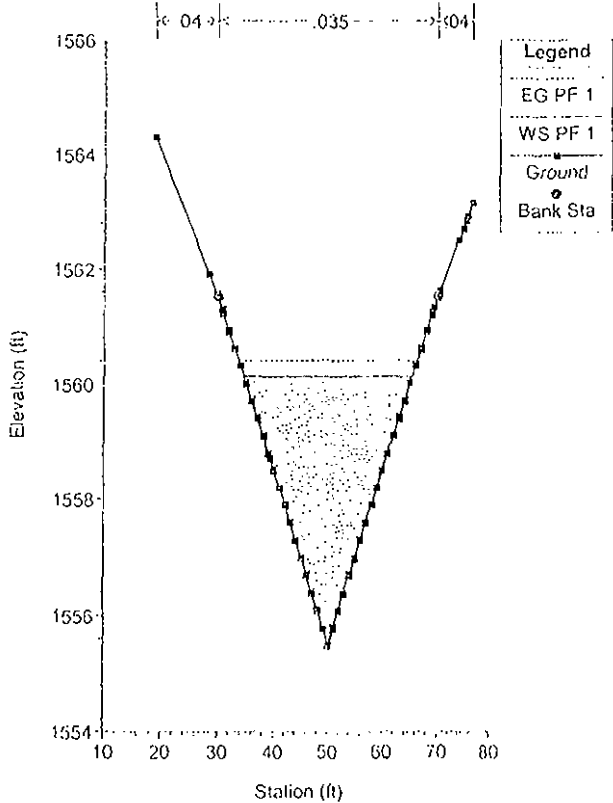
River = RIVER-1 Reach = Reach-1 RS = 1824



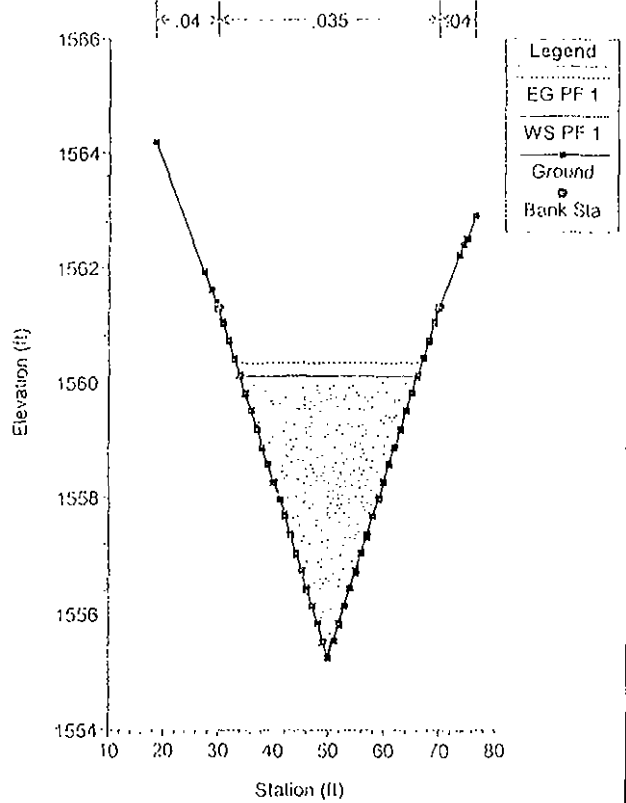
River = RIVER-1 Reach = Reach-1 RS = 1822 IS

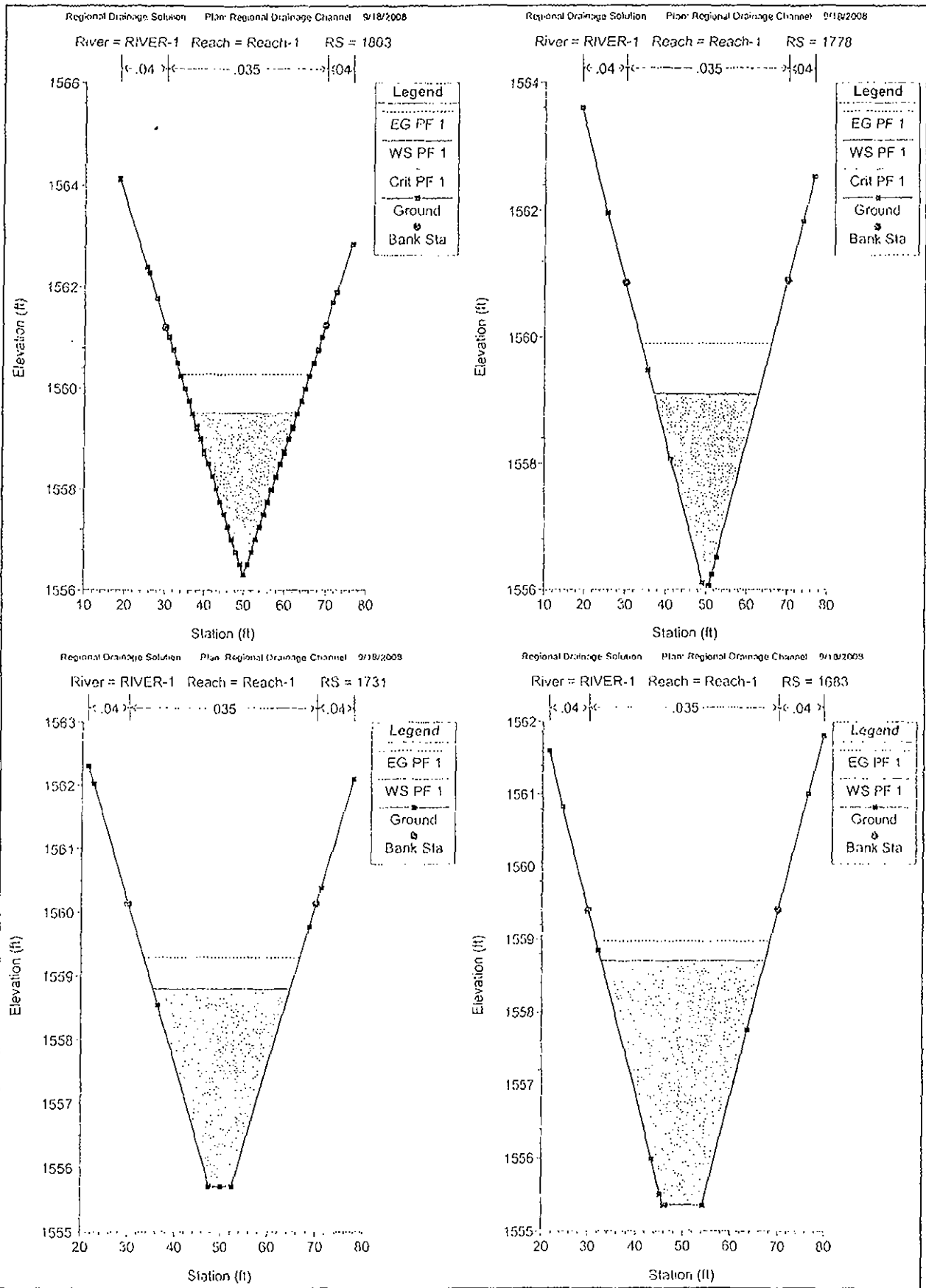


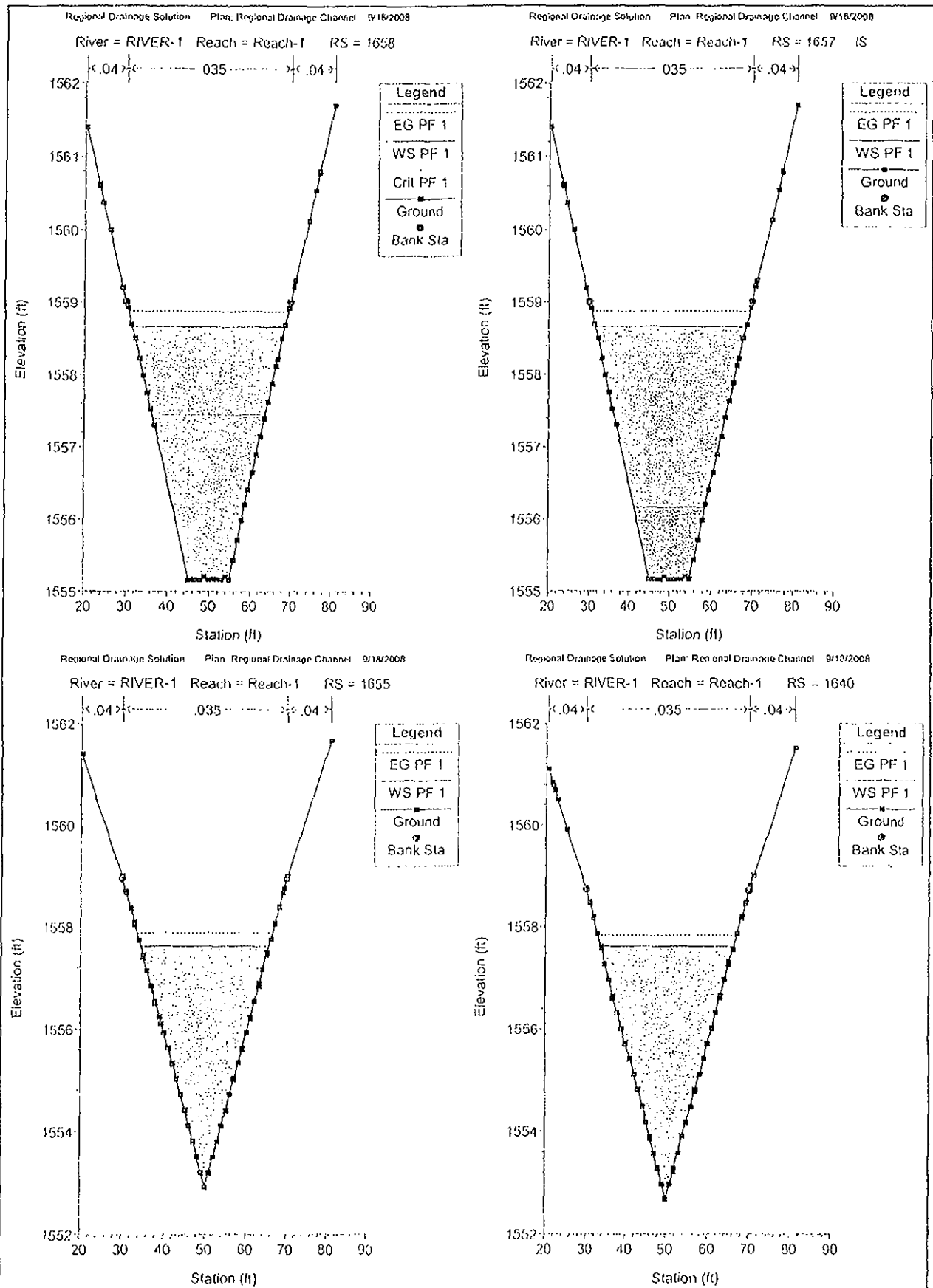
River = RIVER-1 Reach = Reach-1 RS = 1821



River = RIVER-1 Reach = Reach-1 RS = 1806

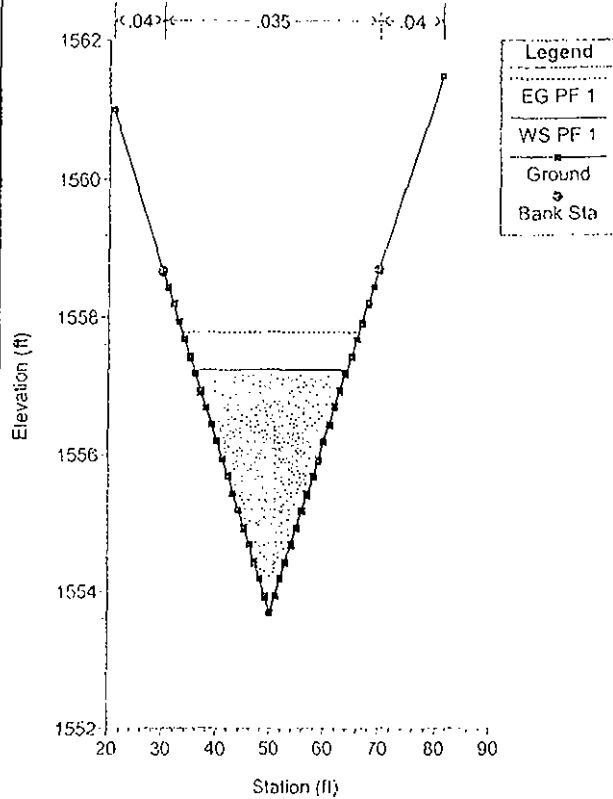




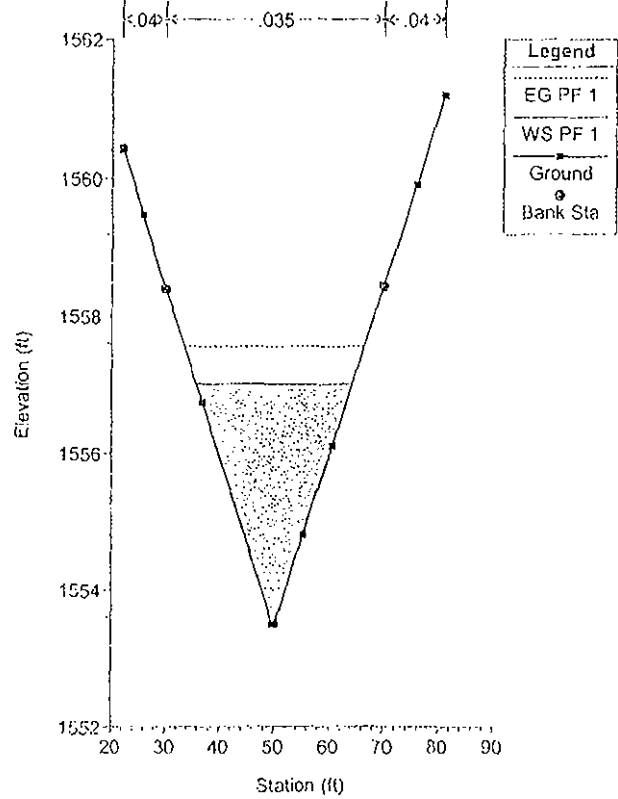




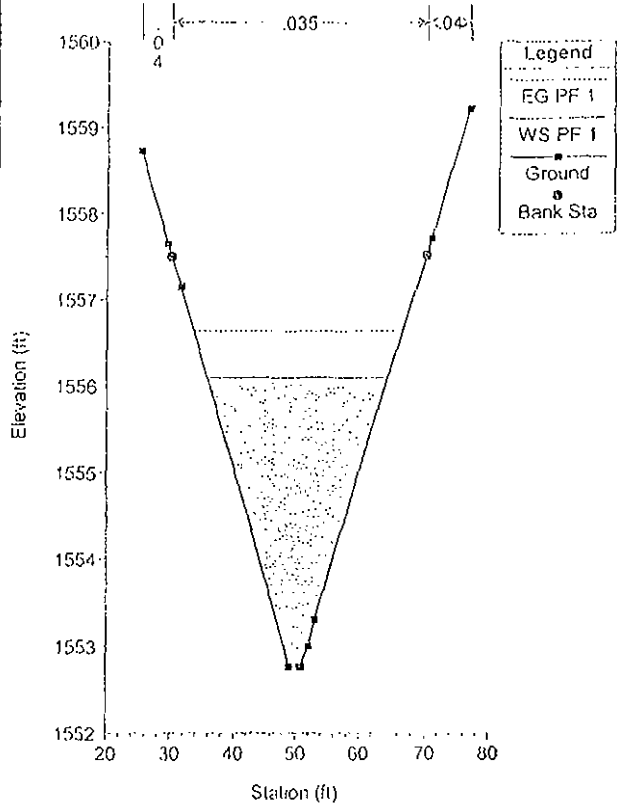
River = RIVER-1 Reach = Reach-1 RS = 1637



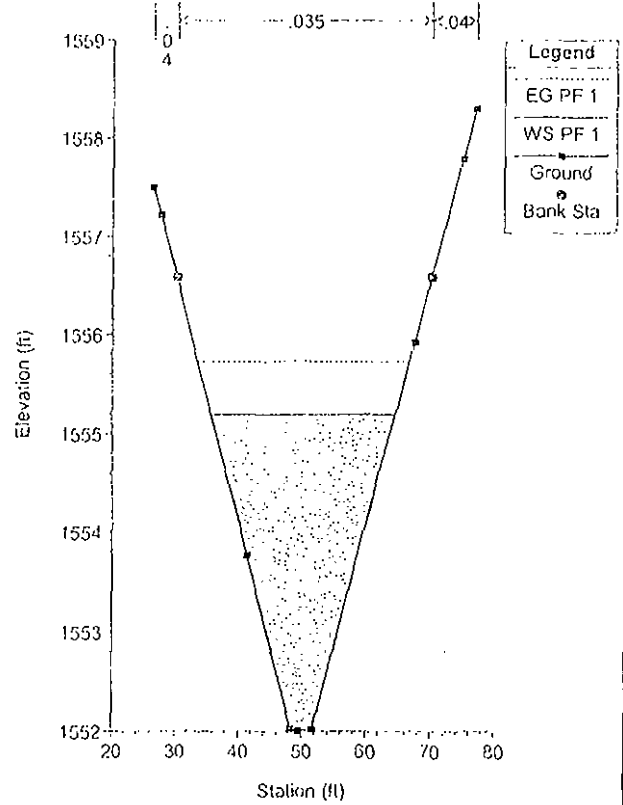
River = RIVER-1 Reach = Reach-1 RS = 1612



River = RIVER-1 Reach = Reach-1 RS = 1514

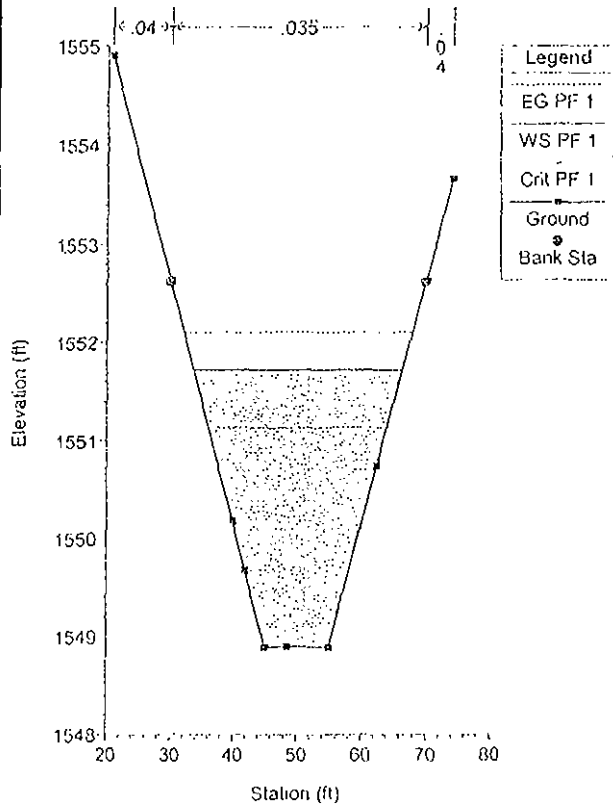


River = RIVER-1 Reach = Reach-1 RS = 1416





River = RIVER-1 Reach = Reach-1 RS = 1000



Plan: RDC 100yr RIVER-1 Reach-1 RS: 3581 Int Struct: Profile: PF 1

E.G. Elev (ft)	1585.25	Q Gates (cfs)	
W.S. Elev (ft)	1585.03	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1583.86
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	72.37	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	16.98	Gate Submerg	0.00
Weir Sta Rgt (ft)	47.77	Gate Invert (ft)	0.00
Weir Max Depth (ft)	3.06	Gate Weir Coef	0.000
Weir Avg Depth (ft)	2.35		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.44	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1582.20	Breach Flow Area (sq ft)	
Wt Top Width (ft)	30.79		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 3373 Int Struct: Profile: PF 1

E.G. Elev (ft)	1582.51	Q Gates (cfs)	
W.S. Elev (ft)	1582.30	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1580.88
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	73.03	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	19.30	Gate Submerg	0.00
Weir Sta Rgt (ft)	48.75	Gate Invert (ft)	0.00
Weir Max Depth (ft)	3.20	Gate Weir Coef	0.000
Weir Avg Depth (ft)	2.48		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.40	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1579.32	Breach Flow Area (sq ft)	
Wt Top Width (ft)	29.44		

#### Errors Warnings and Notes

Warning	The inline structure solution failed to converge. The program used the solution with the least error.
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Plan: RDC 100yr RIVER-1 Reach-1 RS: 3155 Int Struct: Profile: PF 1

E.G. Elev (ft)	1579.04	Q Gates (cfs)	
W.S. Elev (ft)	1578.84	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1576.77
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	77.91	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	16.94	Gate Submerg	0.00
Weir Sta Rgt (ft)	56.53	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.70	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.96		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.11	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1576.35	Breach Flow Area (sq ft)	
Wt Top Width (ft)	39.70		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 2796 Int Struct: Profile: PF 1

E.G. Elev (ft)	1574.04	Q Gates (cfs)	
W.S. Elev (ft)	1573.84	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1572.74
Q Weir (cfs)	300.00	Gate #Open	

Plan: RDC 100yr RIVER-1 Reach-1 RS: 2796 Inl Struct Profile: PF 1 (Continued)

Weir Flow Area (sq ft)	77.07	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.50	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.49	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.74	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.98		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.42	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1571.31	Breach Flow Area (sq ft)	
Wr Top Wdth (ft)	38.99		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 2559 Inl Struct Profile: PF 1

E.G. Elev (ft)	1570.94	Q Gates (cfs)	
W.S. Elev (ft)	1570.74	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1569.66
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	77.03	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.51	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.46	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.74	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.98		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.43	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1568.21	Breach Flow Area (sq ft)	
Wr Top Wdth (ft)	38.96		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 2170 Inl Struct Profile: PF 1

E.G. Elev (ft)	1566.68	Q Gates (cfs)	
W.S. Elev (ft)	1566.47	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1565.38
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	76.16	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.56	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.57	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.70	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.95		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.45	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1563.99	Breach Flow Area (sq ft)	
Wr Top Wdth (ft)	39.00		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 1988 Inl Struct Profile: PF 1

E.C. Elev (ft)	1564.02	Q Gates (cfs)	
W.S. Elev (ft)	1563.82	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1562.70
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	77.23	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.44	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.44	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.73	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.98		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.41	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1561.30	Breach Flow Area (sq ft)	

Plan: RDC 100yr RIVER-1 Reach-1 RS: 1988 Inl Struct: Profile: PF 1 (Continued)

Wr Top Width (ft)	39.01
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Plan: RDC 100yr RIVER-1 Reach-1 RS: 1822 Inl Struct: Profile: PF 1

E.G. Elev (ft)	1561.44	Q Gates (cfs)	
W.S. Elev (ft)	1561.24	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1560.14
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	77.05	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.50	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.47	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.74	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.98		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.42	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1558.71	Breach Flow Area (sq ft)	
Wr Top Width (ft)	38.97		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 1657 Inl Struct: Profile: PF 1

E.G. Elev (ft)	1558.87	Q Gates (cfs)	
W.S. Elev (ft)	1558.66	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1557.63
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	76.02	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.54	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.46	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.71	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.95		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.47	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1556.17	Breach Flow Area (sq ft)	
Wr Top Width (ft)	38.91		

# Culvert Calculator Report

## RDC Outfall 100yr

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	1,552.00 ft	Headwater Depth/Height	1.37
Computed Headwater Elev.	1,551.73 ft	Discharge	300.00 cfs
Inlet Control HW Elev.	1,551.51 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	1,551.73 ft	Control Type	Entrance Control

Grades			
Upstream Invert	1,547.62 ft	Downstream Invert	1,545.80 ft
Length	375.00 ft	Constructed Slope	0.004853 ft/ft

Hydraulic Profile			
Profile	S2	Depth, Downstream	1.96 ft
Slope Type	Steep	Normal Depth	1.96 ft
Flow Regime	Supercritical	Critical Depth	2.22 ft
Velocity Downstream	9.56 ft/s	Critical Slope	0.003401 ft/ft

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	8.00 ft
Section Size	8 x 3 ft	Rise	3.00 ft
Number Sections	2		

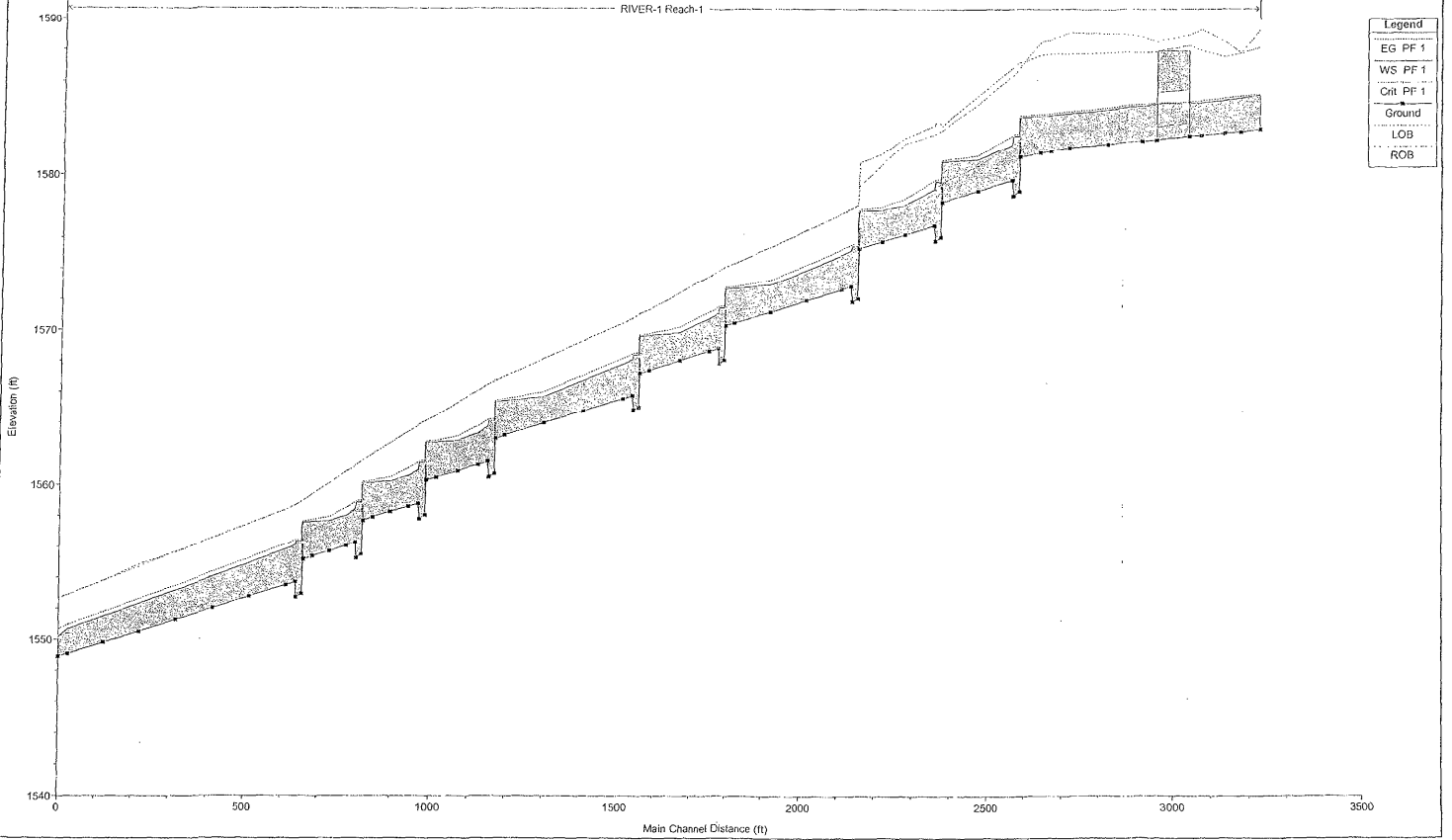
Outlet Control Properties			
Outlet Control HW Elev.	1,551.73 ft	Upstream Velocity Head	1.11 ft
Ke	0.70	Entrance Loss	0.78 ft

Inlet Control Properties			
Inlet Control HW Elev.	1,551.51 ft	Flow Control	Transition
Inlet Type	0° wingwall flares	Area Full	48.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

HEC-RAS Plan: RDC 10yr River: RIVER-1 Reach: Reach-1 Profile: PF 1																
River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	E.G. Elev (ft)	E.G. Slope (ft/m)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl	LOB Elev (ft)	ROB Elev (ft)	Flow Depth (ft)	Freeboard Req	Freeboard Prov		
4222	105.00	1582.97	1585.13	1585.17	0.000576	1.53	68.79	36.28	0.20	1588.20	1589.30	2.16	1.00	3.07		
4172	105	1582.80	1584.97	1585.10	0.002851	2.97	35.35	22.87	0.42	1587.82	1587.84	2.17	1.00	2.85		
4130	105	1582.73	1584.84	1584.98	0.003072	3.04	34.50	22.78	0.44	1587.60	1588.56	2.11	1.00	2.76		
4070	105	1582.59	1584.67	1584.80	0.002829	2.93	35.78	23.47	0.42	1588.00	1589.33	2.09	1.00	3.33		
4039	105	1582.53	1584.68	1584.73	0.000866	1.88	55.86	26.06	0.23	1588.33	1588.98	2.15	1.00	3.65		
4004	Culvert															
3953	105	1582.33	1584.63	1584.67	0.000701	1.76	59.80	26.06	0.20	1587.99	1588.61	2.30	1.00	3.36		
3915	105	1582.25	1584.50	1584.62	0.002423	2.81	37.38	23.22	0.39	1587.90	1588.90	2.25	1.00	3.40		
3819	105	1582.04	1584.26	1584.38	0.002524	2.84	36.96	23.33	0.40	1587.90	1589.11	2.22	1.00	3.64		
3715	105	1581.80	1583.98	1584.11	0.002715	2.92	35.99	23.06	0.41	1587.80	1589.14	2.18	1.00	3.82		
3663	105	1581.57	1583.87	1583.98	0.002203	2.70	38.84	23.84	0.37	1587.80	1588.70	2.30	1.00	3.93		
3635	105	1581.44	1583.81	1583.92	0.001941	2.58	40.64	24.27	0.35	1587.70	1589.57	2.37	1.00	3.89		
3582	105	1581.19	1583.75	1583.83	0.001308	2.30	45.62	23.80	0.29	1587.23	1587.03	2.56	1.00	3.28		
3501	Int Struct															
3579	105	1578.96	1582.52	1582.67	0.002612	3.10	33.89	18.55	0.40	1587.24	1586.88	3.56	1.00	4.36		
3564	105	1578.70	1582.52	1582.62	0.001559	2.49	42.23	22.09	0.32	1587.02	1586.40	3.82	1.00	3.88		
3581	105	1579.71	1581.98	1582.56	0.018555	6.11	17.18	15.14	1.01	1586.89	1586.40	2.27	1.00	4.42		
3467	105	1579.00	1581.01	1581.26	0.006804	3.90	26.31	21.14	0.63	1585.10	1584.55	2.01	1.00	3.54		
3374	105	1578.30	1580.89	1580.98	0.001296	2.33	45.07	22.76	0.29	1583.20	1582.91	2.59	1.00	2.02		
3373	Int Struct															
3371	105	1576.07	1579.59	1579.80	0.004030	3.70	28.34	16.12	0.49	1583.36	1582.90	3.52	1.00	3.31		
3356	105	1575.82	1579.63	1579.73	0.001646	2.55	41.25	21.67	0.35	1583.42	1582.70	3.81	1.00	3.07		
3353	105	1576.82	1579.12	1579.67	0.017321	5.96	17.62	15.32	0.98	1583.22	1582.64	2.30	1.00	3.52		
3276	105	1576.24	1578.11	1578.50	0.012316	5.01	20.97	18.69	0.83	1582.40	1582.03	1.87	1.00	3.92		
3216	105	1575.79	1577.82	1578.01	0.004652	3.43	30.57	23.21	0.53	1581.40	1580.73	2.03	1.00	2.91		
3156	105	1575.34	1577.75	1577.83	0.001469	2.21	47.48	29.38	0.31	1580.80	1579.34	2.41	1.00	1.59		
3155	Int Struct															
3152	105	1572.09	1575.51	1575.63	0.002130	2.71	38.71	22.68	0.37	1578.10	1578.13	3.42	1.00	2.59		
3138	105	1571.86	1575.50	1575.59	0.001522	2.39	43.91	24.10	0.31	1577.91	1577.91	3.64	1.00	2.41		
3135	105	1572.86	1575.19	1575.55	0.011170	4.84	21.70	18.69	0.79	1577.86	1577.90	2.33	1.00	2.67		
3110	105	1572.67	1574.92	1575.28	0.010755	4.79	21.91	18.74	0.78	1577.58	1577.58	2.25	1.00	2.66		
3014	105	1571.95	1573.91	1574.25	0.010566	4.73	22.21	19.20	0.77	1576.51	1576.51	1.96	1.00	2.60		
2918	105	1571.20	1573.00	1573.30	0.009150	4.42	23.78	20.49	0.72	1575.43	1575.43	1.80	1.00	2.43		
2822	105	1570.50	1572.76	1572.86	0.002187	2.57	40.84	27.16	0.37	1574.36	1574.36	2.26	1.00	1.80		
2797	105	1570.30	1572.73	1572.81	0.001569	2.28	46.08	28.60	0.32	1574.17	1574.17	2.43	1.00	1.44		
2796	Int Struct															
2794	105	1568.08	1571.47	1571.59	0.002228	2.76	38.07	22.48	0.37	1574.12	1574.12	3.39	1.00	2.65		
2779	105	1567.85	1571.47	1571.56	0.001577	2.42	43.32	23.90	0.32	1573.90	1573.90	3.62	1.00	2.43		
2778	105	1568.85	1571.11	1571.52	0.012857	5.09	20.82	18.12	0.84	1573.85	1573.85	2.28	1.00	2.74		
2751	105	1568.66	1570.78	1571.19	0.013134	5.16	20.34	18.08	0.86	1573.52	1573.52	2.12	1.00	2.74		
2668	105	1568.04	1569.85	1570.20	0.010667	4.73	22.21	19.30	0.78	1572.43	1572.43	1.81	1.00	2.58		
2586	105	1567.40	1569.66	1569.77	0.002339	2.65	39.68	26.58	0.38	1571.35	1571.35	2.26	1.00	1.69		
2561	105	1567.20	1569.63	1569.71	0.001574	2.28	46.03	28.60	0.32	1571.07	1571.10	2.43	1.00	1.44		
2539	Int Struct															
2557	105	1564.98	1568.40	1568.51	0.002147	2.72	38.60	22.63	0.37	1571.06	1571.02	3.42	1.00	2.60		
2543	105	1564.80	1568.39	1568.48	0.001526	2.40	43.80	24.01	0.31	1570.86	1570.80	3.59	1.00	2.41		
2540	105	1565.75	1568.09	1568.44	0.010724	4.76	22.08	18.76	0.77	1570.75	1570.75	2.34	1.00	2.66		
2515	105	1565.56	1567.83	1568.10	0.010577	4.76	22.06	18.81	0.77	1570.47	1570.47	2.27	1.00	2.64		
2408	105	1564.76	1566.76	1567.09	0.009827	4.60	22.80	19.44	0.75	1569.32	1569.32	2.00	1.00	2.56		
2302	105	1563.97	1565.69	1566.02	0.010257	4.60	22.84	20.25	0.76	1568.16	1568.16	1.72	1.00	2.47		
2196	105	1563.17	1565.42	1565.52	0.002158	2.55	41.11	27.34	0.37	1567.00	1567.00	2.25	1.00	1.58		
2171	105	1562.98	1565.39	1565.47	0.001567	2.27	46.23	28.80	0.32	1566.72	1566.82	2.41	1.00	1.33		
2170	Int Struct															
2160	105	1560.72	1564.11	1564.23	0.002236	2.76	38.10	22.46	0.37	1566.69	1566.77	3.39	1.00	2.58		
2153	105	1560.50	1564.10	1564.20	0.001615	2.44	42.95	23.88	0.32	1566.53	1566.50	3.60	1.00	2.40		
2150	105	1561.49	1563.72	1564.15	0.014208	5.29	19.86	17.90	0.88	1566.49	1566.49	2.23	1.00	2.77		
2125	105	1561.30	1563.32	1563.78	0.015240	5.47	19.21	17.54	0.92	1566.13	1566.10	2.02	1.00	2.78		
2071	105	1560.90	1562.85	1563.13	0.008222	4.29	24.47	20.31	0.69	1565.33	1565.33	1.95	1.00	2.48		
2015	105	1560.49	1562.73	1562.85	0.002487	2.71	38.70	26.11	0.39	1564.45	1564.49	2.24	1.00	1.76		
1990	105	1560.29	1562.71	1562.79	0.001522	2.25	46.61	28.76	0.31	1564.13	1564.13	2.42	1.00	1.42		
1988	Int Struct															
1986	105	1558.04	1561.43	1561.55	0.002241	2.76	38.07	22.34	0.37	1564.10	1564.00	3.39	1.00	2.65		
1972	105	1557.81	1561.42	1561.61	0.001587	2.43	43.20	23.89	0.32	1563.90	1563.88	3.61	1.00	2.44		
1969	105	1558.81	1560.99	1561.46	0.015562	5.50	19.08	17.41	0.93	1563.81	1563.81	2.18	1.00	2.82		
1944	105	1558.60	1560.60	1561.07	0.015615	5.51	19.06	17.52	0.93	1563.43	1563.40	2.00	1.00	2.80		
1895	105	1558.27	1560.24	1560.51	0.007838	4.17	25.17	20.61	0.67	1562.69	1562.69	1.97	1.00	2.45		
1849	105	1557.92	1560.15	1560.27	0.002592	2.76	38.04	25.81	0.40	1561.96	1562.00	2.23	1.00	1.01		
1824	105	1557.70	1560.13	1560.21	0.001571	2.29	46.04	29.56	0.32	1561.57	1561.60	2.43	1.00	1.44		
1822	Int Struct															
1821	105	1555.48	1558.88	1558.99	0.002224	2.76	38.09	22.49	0.37	1561.52	1561.52	3.40	1.00	2.64		
1806	105	1555.25	1558.87	1558.96	0.001595	2.43	43.26	23.91	0.32	1561.30	1561.30	3.62	1.00	2.43		
1803	105	1556.30	1558.48	1558.91	0.014540	5.36	19.59	17.75	0.90	1561.20	1561.25	2.16	1.00	2.74		
1778	105	1556.06	1558.03	1558.52	0.016815	5.63	18.65	17.40	0.96	1560.86	1560.90	1.97	1.00	2.83		
1731	105	1555.70	1557.69	1557.95	0.007342	4.11	25.52	20.73	0.65	1560.13	1560.13	1.99	1.00	2.44		
1683	105	1555.35	1557.60	1557.72	0.002481	2.72	38.65	25.98	0.39	1559.39	1559.40	2.25	1.00	1.79		
1658	105	1555.16	1557.58	1557.66	0.001562	2.28	46.14	28.59	0.32	1559.00	1559.00	2.42	1.00	1.42		
1657	Int Struct															
1655	105	1552.91	1556.36	1556.47	0.002036	2.66	39.42	22.88	0.36	1560.95	1560.85	3.45	1.00	2.59		
1640	105	1552.68	1556.35	1556.44	0.001473	2.36	44.45	24.27	0.31	1560.73	1560.70	3.67	1.00	2.35		
1637	105	1553.68	1556.00	1556.40	0.009380	4.53	23.19	19.30	0.73	1560.68	1560.70	2.40	1.00	2.60		
1612	105	1553.49	1555.85	1556.17	0.009400											



RIVER-1 Reach-1



# Culvert Calculator Report

## RDC Outfall 10yr

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	1,552.00 ft	Headwater Depth/Height	0.68
Computed Headwater Elev.	1,549.66 ft	Discharge	105.00 cfs
Inlet Control HW Elev.	1,549.48 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	1,549.66 ft	Control Type	Entrance Control

Grades			
Upstream Invert	1,547.62 ft	Downstream Invert	1,545.80 ft
Length	375.00 ft	Constructed Slope	0.004853 ft/ft

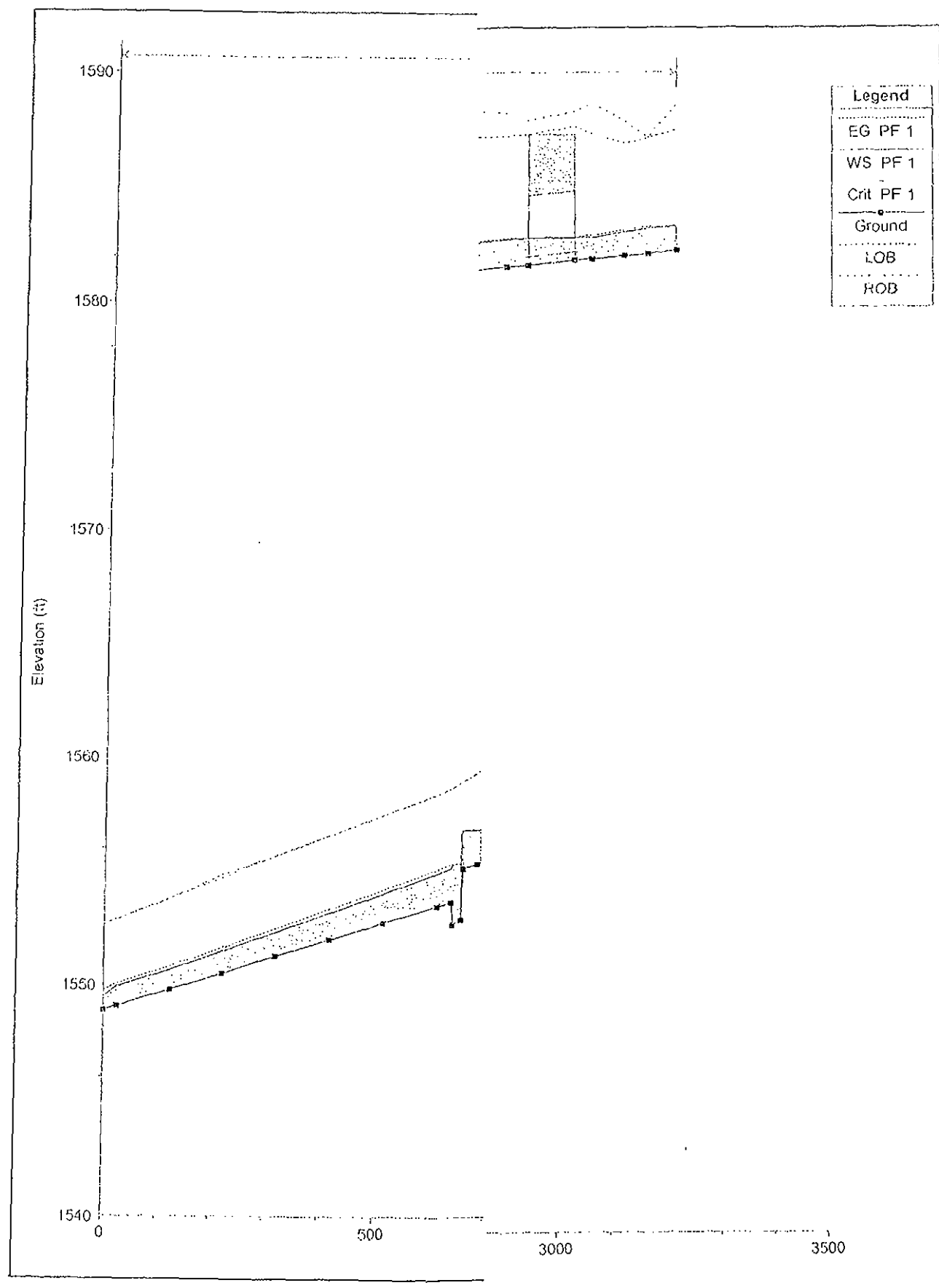
Hydraulic Profile			
Profile	S2	Depth, Downstream	0.97 ft
Slope Type	Sleep	Normal Depth	0.97 ft
Flow Regime	Supercritical	Critical Depth	1.10 ft
Velocity Downstream	6.76 ft/s	Critical Slope	0.003298 ft/ft

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	8.00 ft
Section Size	8 x 3 ft	Rise	3.00 ft
Number Sections	2		

Outlet Control Properties			
Outlet Control HW Elev.	1,549.66 ft	Upstream Velocity Head	0.55 ft
Ke	0.70	Entrance Loss	0.39 ft

Inlet Control Properties			
Inlet Control HW Elev	1,549.48 ft	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	48.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

River Sta	Q Total (cfs)	Min Ch Elev (ft)	W.S. Elev (ft)	E.G. Elev (ft)	E.G. (ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Friction Coeff	LOB Elev (ft)	ROB Elev (ft)	Flow Depth (ft)	Freeboard Req (ft)	Freeboard Prov (ft)
4222	30	1582.97	1584.03	1584.04	0.000583	0.99	30.71	32.42	0.18	1586.20	1589.30	1.06	1.00	4.17
4172	30	1582.80	1583.91	1583.98	0.002672	2.06	14.57	16.56	0.39	1587.82	1587.84	1.11	1.00	3.91
4130	30	1582.73	1583.77	1583.85	0.003454	2.19	13.70	16.32	0.42	1587.60	1588.56	1.04	1.00	3.83
4070	30	1582.59	1583.54	1583.62	0.004975	2.28	13.15	16.72	0.45	1588.00	1589.33	0.95	1.00	4.46
4039	30	1582.53	1583.53	1583.56	0.000903	1.15	26.13	26.03	0.20	1588.33	1588.96	1.00	1.00	4.80
4004	Culvert													
3953	30	1582.33	1583.51	1583.53	0.000470	0.97	30.84	26.05	0.16	1587.99	1588.61	1.18	1.00	4.48
3915	30	1582.25	1583.44	1583.49	0.002122	1.86	16.11	16.91	0.34	1587.90	1588.90	1.19	1.00	4.46
3819	30	1582.04	1583.24	1583.29	0.002089	1.84	16.28	17.19	0.33	1587.90	1589.11	1.20	1.00	4.66
3715	30	1581.80	1583.04	1583.09	0.001856	1.77	16.95	17.41	0.32	1587.80	1589.14	1.24	1.00	4.76
3663	30	1581.57	1582.97	1583.01	0.001175	1.50	19.94	18.45	0.26	1587.80	1588.70	1.40	1.00	4.83
3635	30	1581.44	1582.95	1582.98	0.000899	1.37	21.87	19.05	0.23	1587.70	1588.57	1.51	1.00	4.75
3582	30	1581.19	1582.92	1582.94	0.000446	1.09	27.59	19.97	0.16	1587.23	1587.03	1.73	1.00	4.11
3581	Int Struct													
3579	30	1578.96	1581.45	1581.50	0.001388	1.78	16.88	13.27	0.28	1587.24	1586.88	2.49	1.00	5.43
3564	30	1578.70	1581.45	1581.48	0.000744	1.30	21.78	15.06	0.21	1587.02	1586.40	2.75	1.00	4.95
3561	30	1579.71	1581.09	1581.44	0.021934	4.76	6.30	9.17	1.01	1586.89	1586.40	1.38	1.00	5.31
3467	30	1579.00	1580.08	1580.21	0.007705	3.00	10.01	13.62	0.62	1585.10	1584.55	1.08	1.00	4.47
3374	30	1578.30	1580.05	1580.07	0.000440	1.10	27.40	19.29	0.16	1583.20	1582.91	1.75	1.00	2.86
3373	Int Struct													
3371	30	1576.01	1578.95	1578.63	0.002092	2.12	14.16	11.40	0.33	1583.36	1582.90	2.49	1.00	4.34
3356	30	1575.82	1578.57	1578.60	0.000770	1.40	21.44	15.62	0.21	1583.42	1582.70	2.75	1.00	4.13
3353	30	1576.82	1578.32	1578.57	0.013852	4.01	7.49	9.99	0.82	1583.22	1582.64	1.50	1.00	4.32
3276	30	1576.24	1577.25	1577.47	0.014451	3.83	7.83	11.60	0.93	1582.40	1582.03	1.01	1.00	4.78
3216	30	1575.75	1577.04	1577.11	0.002727	2.01	14.01	16.94	0.38	1581.40	1582.73	1.25	1.00	3.69
3156	30	1575.34	1577.01	1577.03	0.000516	1.07	27.97	23.44	0.17	1580.80	1579.34	1.67	1.00	2.33
3155	Int Struct													
3152	30	1572.09	1574.51	1574.55	0.001096	1.55	19.39	16.01	0.25	1578.10	1578.13	2.42	1.00	3.59
3138	30	1571.86	1574.51	1574.53	0.000675	1.29	23.23	17.46	0.20	1577.91	1577.91	2.65	1.00	3.40
3135	30	1572.06	1574.32	1574.51	0.011228	3.54	8.47	11.69	0.73	1577.86	1577.90	1.46	1.00	3.54
3110	30	1572.67	1574.03	1574.23	0.011444	3.58	8.37	11.60	0.74	1577.58	1577.58	1.35	1.00	3.55
3014	30	1571.95	1573.11	1573.27	0.008627	3.17	9.47	12.87	0.85	1576.51	1576.51	1.16	1.00	3.40
2918	30	1571.20	1572.11	1572.29	0.011988	3.45	8.69	13.36	0.75	1575.43	1575.43	0.91	1.00	3.32
2822	30	1570.50	1572.00	1572.03	0.000974	1.33	22.51	21.08	0.23	1574.36	1574.36	1.60	1.00	2.36
2797	30	1570.30	1571.99	1572.01	0.000550	1.11	27.11	22.70	0.18	1574.17	1574.17	1.69	1.00	2.18
2795	Int Struct													
2794	30	1568.88	1570.40	1570.52	0.001158	1.58	19.02	15.88	0.25	1574.12	1574.12	2.40	1.00	3.64
2779	30	1567.85	1570.40	1570.50	0.000696	1.31	22.93	17.29	0.20	1573.90	1573.90	2.63	1.00	3.42
2776	30	1568.05	1570.25	1570.48	0.012992	3.72	8.07	11.51	0.78	1573.85	1573.85	1.41	1.00	3.59
2751	30	1568.08	1569.08	1570.17	0.011074	3.53	8.49	11.70	0.73	1573.52	1573.52	1.32	1.00	3.54
2698	30	1568.04	1568.98	1569.18	0.013124	3.63	8.27	12.62	0.79	1572.43	1572.43	0.94	1.00	3.45
2586	30	1567.40	1568.60	1568.93	0.000935	1.38	21.80	20.55	0.24	1571.35	1571.35	1.50	1.00	2.45
2561	30	1567.20	1568.09	1568.91	0.000554	1.11	27.02	22.64	0.18	1571.07	1571.10	1.69	1.00	2.18
2559	Int Struct													
2557	30	1564.93	1567.40	1567.44	0.001101	1.55	19.39	16.03	0.25	1571.00	1571.02	2.42	1.00	3.60
2543	30	1565.80	1567.40	1567.43	0.000677	1.29	23.24	17.24	0.20	1570.80	1570.80	2.60	1.00	3.40
2540	30	1565.75	1567.22	1567.40	0.010545	3.43	8.75	12.01	0.71	1570.75	1570.75	1.47	1.00	3.53
2515	30	1565.56	1566.90	1567.11	0.012611	3.72	8.07	11.40	0.78	1570.47	1570.47	1.34	1.00	3.57
2409	30	1564.76	1566.00	1566.13	0.006811	2.91	10.31	13.31	0.58	1569.32	1569.32	1.24	1.00	3.32
2302	30	1563.97	1564.77	1565.01	0.017535	3.93	7.63	12.86	0.90	1568.16	1568.16	0.80	1.00	3.39
2196	30	1563.17	1564.67	1564.70	0.000889	1.31	22.89	21.35	0.22	1567.00	1567.00	1.50	1.00	2.33
2171	30	1562.99	1564.66	1564.68	0.000536	1.09	27.41	22.89	0.18	1566.72	1566.82	1.60	1.00	2.06
2170	Int Struct													
2168	30	1560.72	1563.12	1563.16	0.001150	1.57	19.09	15.94	0.25	1566.69	1566.77	2.40	1.00	3.57
2153	30	1560.60	1563.12	1563.14	0.000731	1.33	22.62	17.38	0.20	1566.53	1566.50	2.62	1.00	3.38
2150	30	1561.49	1562.89	1563.12	0.013394	3.79	7.91	11.24	0.80	1566.49	1566.49	1.40	1.00	3.60
2125	30	1561.30	1562.48	1562.74	0.016579	4.12	7.28	10.87	0.89	1566.13	1566.10	1.18	1.00	3.62
2071	30	1560.90	1562.04	1562.16	0.005903	2.82	10.62	13.89	0.57	1565.33	1565.33	1.14	1.00	3.29
2015	30	1560.49	1561.38	1562.01	0.011053	1.41	21.28	20.18	0.24	1564.49	1564.49	1.49	1.00	2.51
1990	30	1560.29	1561.97	1561.99	0.000524	1.09	27.56	22.82	0.17	1564.13	1564.13	1.68	1.00	2.16
1988	Int Struct													
1946	30	1558.04	1560.44	1560.48	0.001137	1.57	19.12	15.75	0.25	1564.10	1564.08	2.40	1.00	3.64
1972	30	1557.91	1560.43	1560.46	0.000718	1.32	22.78	17.47	0.20	1563.90	1563.86	2.62	1.00	3.43
1969	30	1558.81	1560.20	1560.43	0.014411	3.90	7.70	11.13	0.83	1563.81	1563.81	1.39	1.00	3.61
1944	30	1558.60	1559.76	1560.03	0.017505	4.19	7.15	10.81	0.91	1563.43	1563.40	1.16	1.00	3.64
1896	30	1558.27	1559.45	1559.56	0.005499	2.85	11.31	14.33	0.53	1562.69	1562.69	1.18	1.00	3.24
1849	30	1557.92	1559.40	1559.44	0.001035	1.43	20.93	19.93	0.25	1561.96	1562.00	1.49	1.00	2.56
1824	30	1557.70	1559.39	1559.41	0.000541	1.10	27.22	22.65	0.18	1561.57	1561.60	1.69	1.00	2.18
1822	Int Struct													
1821	30	1555.48	1557.89	1557.93	0.001132	1.56	19.19	15.94	0.25	1561.52	1561.52	2.41	1.00	3.63
1800	30	1555.25	1557.89	1557.91	0.000556	1.30	23.03	17.36	0.20	1561.30	1561.30	2.64	1.00	3.41
1803	30	1556.30	1557.67	1557.89	0.012787	3.73	8.04	11.41	0.78	1561.20	1561.25	1.37	1.00	3.53
1778	30	1556.06	1557.19	1557.49	0.019991	4.40	6.82	10.81	0.97	1560.86	1560.90	1.13	1.00	3.67
1731	30	1555.70	1556.90	1557.00	0.005023	2.57	11.67	14.49	0.50	1560.13	1560.13	1.20	1.00	3.23
1683	30	1555.35	1556.86	1556.89	0.001013	1.39	21.52	20.15	0.24	1559.39	1559.40	1.51	1.00	2.53
1658	30	1555.16	1556.85	1556.87	0.000529	1.09	27.49	22.80	0.18	1559.00	1559.00	1.69	1.00	2.15
1657	Int Struct													
1655	30	1552.91	1556.36	1556.39	0.001048	1.52	19.77	16.24	0.24	1558.95	1558.95	2.44	1.00	3.60
1640	30	1552.68	1556.35	1556.37	0.000562	1.28	23.46	17.65	0.20	1558.73	1558.70	2.67	1.00	3.35
1637	30	1553.68	1555.18	1555.35	0.009335	3.01	9.07	12.63	0.67	1558.68	1558.70	1.50	1.00	3.50
1612	30	1553.49	1554.55	1555.12	0.009333	3.33	9.02	12.00	0.68	1558.40	1558.44	1.46	1.00	3.45
1514	30	1552.76	1554.05	1554.21	0.009165	3.28	9.12	12.23	0.67	1557.50	155			



# Culvert Calculator Report

## RDC Outfall 2yr

Solve For: Headwater Elevation

<b>Culvert Summary</b>			
Allowable HW Elevation	1,552.00 ft	Headwater Depth/Height	0.29
Computed Headwater Elev.	1,548.50 ft	Discharge	30.00 cfs
Inlet Control HW Elev.	1,548.42 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	1,548.50 ft	Control Type	Entrance Control
<b>Grades</b>			
Upstream Invert	1,547.62 ft	Downstream Invert	1,545.80 ft
Length	375.00 ft	Constructed Slope	0.004853 ft/ft
<b>Hydraulic Profile</b>			
Profile	S2	Depth, Downstream	0.44 ft
Slope Type	Steep	Normal Depth	0.44 ft
Flow Regime	Supercritical	Critical Depth	0.48 ft
Velocity Downstream	4.28 ft/s	Critical Slope	0.003661 ft/ft
<b>Section</b>			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	8.00 ft
Section Size	8 x 3 ft	Rise	3.00 ft
Number Sections	2		
<b>Outlet Control Properties</b>			
Outlet Control HW Elev	1,548.50 ft	Upstream Velocity Head	0.24 ft
Ke	0.70	Entrance Loss	0.17 ft
<b>Inlet Control Properties</b>			
Inlet Control HW Elev	1,548.42 ft	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	48.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

## APPENDIX C

### Erosion Protection

**Level I Scour**

Site: Interim Regional Drainage Channel

Location: Scottsdale, Arizona

Description: Rip Rap Design Calculations

Date: 9/16/2008

**Level I Analysis of Stream Degradation**

**Reference:** ADWR, Flood Warning and Dam Safety Section, 1996.  
State Standard 5-96: "Watercourse System Sediment Balance - Guideline 2:  
Channel Degradation Estimation for Alluvial Channels in Arizona"

**Assumptions:** Channel reaches without major disturbances, such as dams and bridges.

**Equations:**  $D_s = D_{gs} + D_{lts}$

where:

$D_s$  = total scour depth, in feet;

$D_{gs}$  = general degradation, in feet;

$D_{lts}$  = long term degradation, in feet;

For straight channel reaches:

$$D_{gs} = 0.157 * Q_{100}^{0.4}$$

For channel reaches with curvature:

$$D_{gs} = 0.219 * Q_{100}^{0.4}$$

Long term degradation:

$$D_{lts} = 0.02 * Q_{100}^{0.6}$$

**Project Name:** Regional Drainage Solution    **Location:** Scottsdale

**Input Data:**

$Q_{100} =$                       300 cfs

$D_s =$                       2.15 ft                      for straight channel

$D_s =$                       2.76 ft                      otherwise

**Recommended Scour Depth :**                      3.0 ft

Note: the minimum total scour depth,  $D_s$ , shall be 3 feet.

## Bend Scour Calculation

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Bend Scour Design Calculations  
 Date: 9/16/2008

## Bend Scour Calculation Sheet

Reference: ADWR, Design Manual for Engineering Analysis of Fluvial Systems, 1985 p5 105-5.110

Project Name: Regional Drainage Solution

Wood/Patch # 073022

## Scour Depth Equation:

$$Z_{bs} = (0.0685 \cdot Y \cdot V^{0.6}) [2.1 \cdot (\sin^2(a/2) / \cos(a))^{0.2} - 1] / (Yh^{0.4} \cdot Se^{0.3})$$

Where  $Z_{bs}$  = bend scour component of total scour depth (ft)  
 $V$  = mean velocity of upstream flow (fps)  
 $Y$  = maximum depth of upstream flow (ft)  
 $Yh$  = hydraulic depth of upstream flow (ft)  
 $Se$  = upstream energy slope (bed slope for uniform flow conditions, ft/ft)  
 $a$  = angle formed by the projection of the channel centerline from the point of curvature to a point which meets a line tangent to the outer bank of the channel (degrees)

## Scour Length Equation

$$X = 2.3 \cdot (C/g^{0.5}) \cdot Y$$

Where  $X$  = distance from the end of channel curvature (point of tangency  $P \cdot T$ ) to the downstream point at which secondary currents have dissipated (ft)  
 $C$  = Chezy coefficient =  $1.486 \cdot R^{1/6} / n$   
 $g$  = gravitational acceleration (32.2 ft/s<sup>2</sup>)  
 $Y$  = depth of flow (to be conservative, use maximum depth of flow, exclusive of scour, within the bend) (ft)

## Input Data

$V =$	4.1 (ft/s)	$n =$	0.035
$Y =$	3.56 (ft)	$A =$	73.54 (ft <sup>2</sup> )
$Yh =$	2.35 (ft)	$P =$	33 (ft)
$Se =$	0.003104	$R =$	2.23 (ft)
$a =$	40 (degree)	$C =$	48.52
	Stable bank side slope =		3 (H:V)

## Computed Scour Values

Scour Depth:	Scour Length:	Scour Width:
$Z_{bs} =$ 1.34 (ft)	$X =$ 70 (ft)	$W =$ 4.0 (ft)



**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

**References:** Department of the Army, U.S. Army Corps of Engineers,  
 Engineering and Design Hydraulic Design of Flood Control Channels.  
 No. 1110-2-1601, Dated 30 June 1994, Chapter 3 (Riprap Protection)

US DOT, FHWA, Highways in the River Environment  
 Hydraulic and Environmental Design Considerations  
 May 1975, pVI-24, (Suggested gradation for riprap).

$$D_{30} = S_f C_s C_v C_r d \left[ \left( \frac{\gamma_w}{\gamma_s - \gamma_w} \right)^{1/2} \cdot \frac{V}{\sqrt{K_1 g d}} \right]^{2.5}$$

**Project Name:** Interim Regional Drainage Channel  
**Location:** Inlet Driveway Culvert

**Inlet Riprap Size**

Safety Factor, $S_f$	1.3
Stability Coefficient, $C_s$	0.375 (Assume rounded rock)
Vertical Velocity Dist., $C_v$	1.00
Thickness Coefficient, $C_r$	1.00
Local Depth, $d$	3.94 ft
Unit Weight of Water, $\gamma_w$	62.4 lbs/ft <sup>3</sup>
Unit Weight of Stones, $\gamma_s$	165 lbs/ft <sup>3</sup>
Local Velocity, $V$	3.6 ft/sec
Bank Angle With Horizontal, $\theta$	18.43 °
Rip Rap Angle of Repose (Fig 6-8), $\phi$	37 °
Bank Angle Correction Factor, $K_1$	0.8509
Computed Riprap Size, $D_{30}$	0.9 inches
Computed Riprap Size, $D_{50}$	1.3 inches
Computed Riprap Size, $D_{15}$	0.6 inches
Computed Riprap Size, $D_{85}$	2.0 inches
<b>Design Riprap Size, <math>D_{50}</math></b>	<b>9 inches</b> <b>TYPE I</b>

**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

References: Department of the Army, U.S. Army Corps of Engineers,  
 Engineering and Design Hydraulic Design of Flood Control Channels.  
 No. 1110-2-1601, Dated 30 June 1994, Chapter 3 (Riprap Protection)

US DOT, FHWA, Highways in the River Environment  
 Hydraulic and Environmental Design Considerations  
 May 1975, pVI-24, (Suggested gradation for riprap).

$$D_{30} = S_f C_s C_v C_T d \left[ \left( \frac{\gamma_w}{\gamma_s - \gamma_w} \right)^{1/2} \frac{V}{\sqrt{K_1 g d}} \right]^{2.5}$$

Project Name: Interim Regional Drainage Channel  
 Location: Channel Bend

**Inlet Riprap Size**

Safety Factor, $S_f$	1.3	
Stability Coefficient, $C_s$	0.375	(Assume rounded rock)
Vertical Velocity Dist., $C_v$	1.15	
Thickness Coefficient, $C_T$	1.00	
Local Depth, $d$	3.56	ft
Unit Weight of Water, $\gamma_w$	62.4	lbs/ft <sup>3</sup>
Unit Weight of Stones, $\gamma_s$	165	lbs/ft <sup>3</sup>
Local Velocity, $V$	4.1	ft/sec
Bank Angle With Horizontal, $\theta$	18.43	°
Rip Rap Angle of Repose (Fig 6-8), $\phi$	39	°
Bank Angle Correction Factor, $K_1$	0.8647	
Computed Riprap Size, $D_{30}$	1.4	inches
Computed Riprap Size, $D_{50}$	2.1	inches
Computed Riprap Size, $D_{15}$	0.9	inches
Computed Riprap Size, $D_{85}$	3.1	inches
Design Riprap Size, $D_{50}$	9	inches TYPE I

**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

**References:** Department of the Army, U.S. Army Corps of Engineers,  
 Engineering and Design Hydraulic Design of Flood Control Channels,  
 No. 1110-2-1601, Dated 30 June 1994, Chapter 3 (Riprap Protection)

US DOT, FHWA, Highways in the River Environment  
 Hydraulic and Environmental Design Considerations  
 May 1975, pVI-24, (Suggested gradation for riprap).

$$D_{30} = S_f C_s C_v C_r d \left[ \left( \frac{\gamma_w}{\gamma_s - \gamma_w} \right)^{1/2} \frac{V}{\sqrt{K_1 g d}} \right]^{2.5}$$

**Project Name:** Interim Regional Drainage Channel  
**Location:** Culvert Under Scottsdale Road

**Inlet Riprap Size**

Safety Factor, $S_f$	1.3	
Stability Coefficient, $C_s$	0.375 (Assume rounded rock)	
Vertical Velocity Dist., $C_v$	1.00	
Thickness Coefficient, $C_r$	1.00	
Local Depth, $d$	2.84 ft	
Unit Weight of Water, $\gamma_w$	62.4 lbs/ft <sup>3</sup>	
Unit Weight of Stones, $\gamma_s$	165 lbs/ft <sup>3</sup>	
Local Velocity, $V$	5.0 ft/sec	
Bank Angle With Horizontal, $\theta$	14.1 °	
Rip Rap Angle of Repose (Fig 6-8), $\phi$	37 °	
Bank Angle Correction Factor, $K_1$	0.9144	
Computed Riprap Size, $D_{30}$	1.9 inches	
Computed Riprap Size, $D_{50}$	2.9 inches	
Computed Riprap Size, $D_{15}$	1.3 inches	
Computed Riprap Size, $D_{85}$	4.4 inches	
<b>Design Riprap Size, <math>D_{50}</math></b>	<b>9 inches</b>	<b>TYPE I</b>

**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

References: *US DOT, FHWA, Highways in the River Environment  
 Hydraulic and Environmental Design Considerations  
 May 1975, pVI-24.*

*US DOT, FHWA, Hydraulic Design of Energy Dissipaters  
 for Culverts and Channel. Sept. 1983, pII-5-II-9.*

*FCDMC, Drainage Design Manual for Maricopa County  
 Arizona, Vol. II - Hydraulics. January 1996, p5.75-5.77.*

Project Name: Interim Regional Drainage Channel  
 Project #: 073022

Structure ID: Union Hills Outlet  
 Culvert Size: 3- 8'x3' CBC

**1. Riprap Size D50**

Max. flow width $W_o =$	24.00 ft	
Max. culvert flow depth $h =$	3.00 ft	
Tailwater depth $TW =$	3.00 ft	
Exit Velocity $V_e =$	4.16 fps	
Tailwater velocity $V_d =$	2.20 fps	normal
Wash bottom width $=$	25.00 ft	
Computed Riprap Size D50 $=$	1.2 in	

Design Riprap Size D50 = 9 in  
 Sieve Size = TYPE 1

**2. Riprap Sizes D15 and D85**

Design Riprap Size D15 = 4 in  
 Design Riprap Size D85 = 14 in

**3. Riprap Apron Length**

Riprap Apron Length = 14 ft

**4. Riprap Apron Width**

Min. Riprap Apron Width = 30 ft  
 Max. Riprap Apron Width = 31 ft

**5. Riprap Thickness**

Riprap Thickness = 36 in

**6. Total Riprap Volume**

Riprap Rock Volume = 46 C.Y.

Please note fields highlighted are input values from the Culvert Modeling Summary

**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

References: *US DOT, FHWA, Highways in the River Environment Hydraulic and Environmental Design Considerations May 1975, pVI-24.*  
*US DOT, FHWA, Hydraulic Design of Energy Dissipaters for Culverts and Channel. Sept. 1983, pII-5-II-9.*  
*FCDMC, Drainage Design Manual for Maricopa County Arizona, Vol. II - Hydraulics. January 1996, p5.75-5.77.*

Project Name: Interim Regional Drainage Channel  
 Project #: 073022

Structure ID: Driveway Outlet  
 Culvert Size: 3- 8'x3' CBC

**1. Riprap Size D50**

Max. flow width $W_o =$	24.00 ft	
Max. culvert flow depth $h =$	3.00 ft	
Tailwater depth $TW =$	3.00	
Exit Velocity $V_e =$	4.17 fps	
Tailwater velocity $V_d =$	3.05 fps	normal
Wash bottom width $=$	25.00 ft	
Computed Riprap Size D50 $=$	12 in	
Design Riprap Size D50 $=$	9 in	
Sieve Size $=$	TYPE I	

**2. Riprap Sizes D15 and D85**

Design Riprap Size D15 $=$	4 in
Design Riprap Size D85 $=$	14 in

**3. Riprap Apron Length**

Riprap Apron Length $=$	8 ft
-------------------------	------

**4. Riprap Apron Width**

Min. Riprap Apron Width $=$	30 ft
Max. Riprap Apron Width $=$	31 ft

**5. Riprap Thickness**

Riprap Thickness $=$	36 in
----------------------	-------

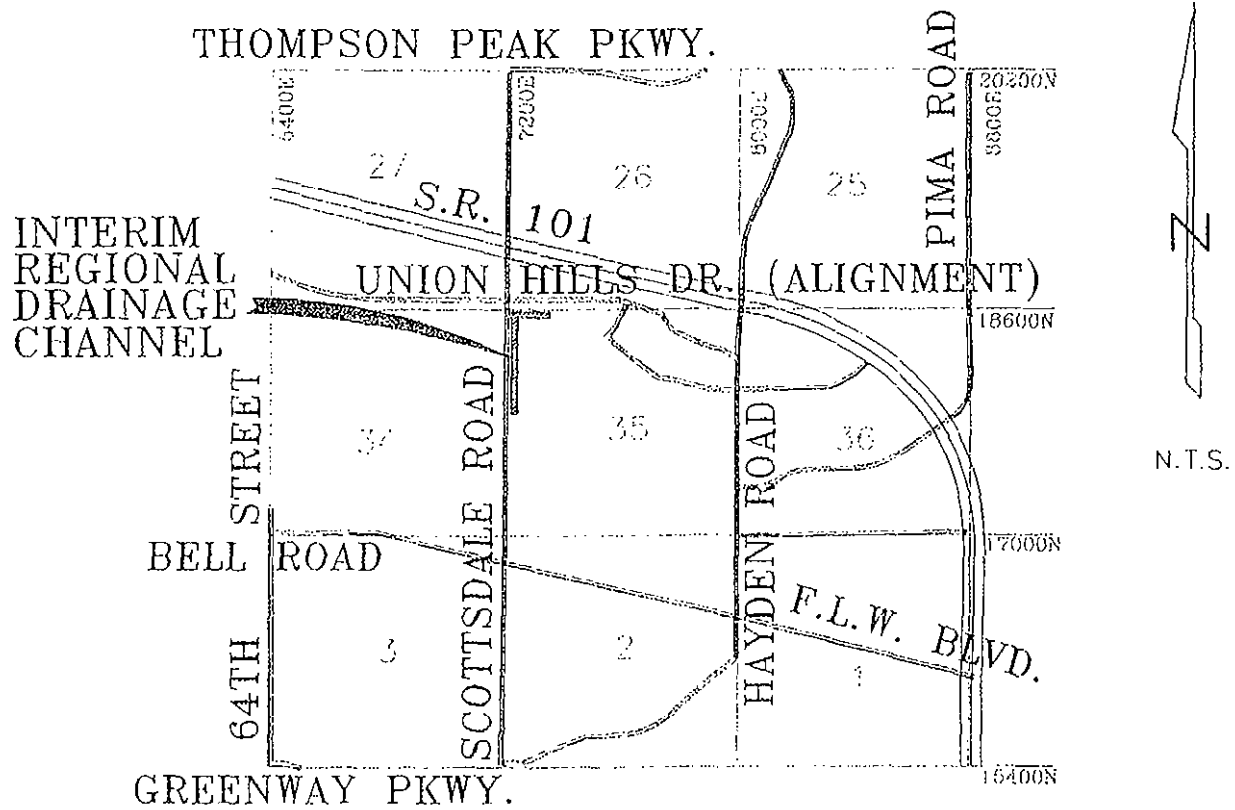
**6. Total Riprap Volume**

Riprap Rock Volume $=$	26 CY
------------------------	-------

Please note fields highlighted are input values from the Culvert Modeling Summary

## **EXHIBIT 1**

### **Vicinity Map**



## INTERIM REGIONAL DRAINAGE CHANNEL

### Exhibit 1 Vicinity Map

WOOD/PATEL  
LAND DEVELOPMENT • WATER RESOURCES  
TRANSPORTATION • TRAFFIC  
WATER / WASTEWATER • SURVEYING  
CONSTRUCTION MANAGEMENT  
(602) 335-8500  
PHOENIX • MESA • TUCSON

***Appendix O***

**As- Built for Interim Regional Channel Design Report**



**FINAL DRAINAGE REPORT  
FOR  
INTERIM REGIONAL DRAINAGE CHANNEL**

October 1, 2008

WP# 073022

*Prepared for:*           **One Scottsdale Holdings, LLC  
c/o DMB Associates, Inc.  
7600 East Doubletree Ranch Road  
Suite 300  
Scottsdale, Arizona 85258  
Phone: (480) 367-7000  
Fax: (480) 367-7558**

*Submitted to:*           **City of Scottsdale  
7447 East Indian School Road  
Suite 300  
Scottsdale, Arizona 85251  
Phone: (480) 312-2352  
Fax: (480) 312-2672**

*Prepared by:*           **Wood, Patel & Associates, Inc.  
2051 West Northern Avenue  
Suite 100  
Phoenix, Arizona 85021  
Phone: (602) 335-8500  
Fax: (602) 335-8580  
Website: [www.woodpatel.com](http://www.woodpatel.com)**



*Geoffrey Scott Brownell*  
expires 3/31/11

## TABLE OF CONTENTS

1.0	EXECUTIVE SUMMARY .....	1
2.0	GENERAL BACKGROUND .....	2
3.0	DESIGN CONCEPT .....	3
4.0	HYDROLOGY .....	4
5.0	HYDRAULICS .....	6
6.0	MAINTENANCE.....	8
7.0	REFERENCES.....	9

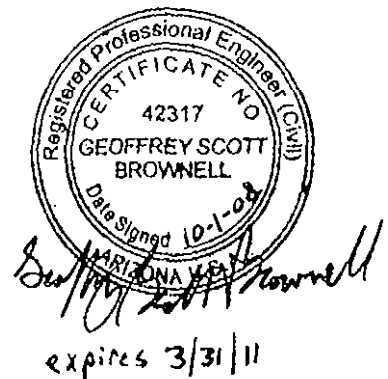
## APPENDICES

Appendix A	Hydrology
Appendix B	Hydraulic Calculations
Appendix C	Erosion Protection

## EXHIBITS

Exhibit 1	Vicinity Map
Exhibit 2	FEMA Map
Exhibit 3	Conceptual Grading and Drainage Plan
Exhibit 4	HEC-RAS Schematic

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## 1.0 EXECUTIVE SUMMARY

- The Interim Regional Drainage Channel is a proposed 3,200-linear foot open channel along Union Hills Road and Scottsdale Road within the City of Scottsdale.
- The channel is intended to provide increased flood protection in a known floodplain, as well as protection for future improvements of Scottsdale Road.
- The Interim Regional Drainage Channel completes the downstream reach of City of Scottsdale initiated regional drainage improvements.
- The channel will convey flow from an existing culvert under Union Hills Drive. It will run east adjacent to Union Hills Drive, turn south and flow adjacent to the Scottsdale Road right-of-way within a future scenic corridor easement to a proposed box culvert under Scottsdale Road. Storm water will ultimately be retained in the Reach 11 Recreation Area of the Central Arizona Project canal.
- The maximum channel width is proposed to be 40 feet.
- The box culvert conveying flows under Scottsdale Road is currently under design by the City of Scottsdale.
- Grade control structures are incorporated in the design to maintain the 100-year flow velocities in the channel within permissible velocities appropriate for an unlined native channel.
- Riprap erosion protection will be incorporated into each grade control structure, as well as at horizontal turns in the channel alignment and inlet/outlet of culverts.
- The design flow for the Interim Regional Drainage Channel is 300 cubic feet per second.

## 2.0 GENERAL BACKGROUND

The Interim Regional Drainage Channel presents the opportunity for implementation of flood protection in the City of Scottsdale. It completes the downstream reach of drainage improvements initiated by the City of Scottsdale. In addition, it provides protection to proposed improvements to Scottsdale Road. It will be located within a scenic corridor easement and add aesthetic open space along a major arterial roadway. The solution is anticipated to prevent redundancies in the drainage system that could occur if development occurred in a disjointed manner.

The proposed Interim Regional Drainage Channel is located within the northwest quarter of Section 35, Township 4 North, Range 4 East, of the Gila and Salt River Base and Meridian. More specifically, the channel is located along the east side of the Scottsdale Road right-of-way between Union Hills Drive and Princess Drive. A map of the area can be seen on Exhibit 1 -- *Vicinity Map*.

The project site lies in a Federal Emergency Management Agency (FEMA) designated Zone "AO" Special Flood Hazard Area, with depths of one foot and velocities of three feet per second, per the Flood Insurance Rate Map (FIRM) panel number 04013C1245H, effective date September 30, 2005 (see Exhibit 2 -- *FEMA Map*).

Currently, drainage from the north passes south under the Loop 101 Freeway through existing box culverts. Flow is conveyed past Union Hills Drive via existing drainage improvements, then flows in an existing wash in a westerly and southerly direction across the Arizona State Land Department (ASLD) property. There is current planning for concrete box culverts that would convey this flow west under Scottsdale Road. An existing channel running west on the north side of Princess Drive would not be disturbed by the Interim Regional Drainage Channel and would continue to operate independently.

### 3.0 DESIGN CONCEPT

The alignment for the Interim Regional Drainage Channel was chosen with input from the Arizona State Land Department (ASLD) and the City of Scottsdale. The proposed alignment maintains connection with the existing drainage improvements south of Union Hills Drive. The proposed channel begins at the outlet of an existing culvert on the south side of Union Hills Drive. The channel will flow east adjacent to Union Hills Drive for approximately 550 feet where it turns south and flows for approximately 2,650 feet within a future scenic corridor easement adjacent to the Scottsdale Road right-of-way. The planned access to the ASLD parcel is a driveway off Union Hills Drive. The proposed channel will be conveyed through three (3) 3-foot by 8-foot concrete box culverts at the proposed driveway location. The proposed regional channel ultimately outfalls into proposed culverts that are currently under design by Dibble & Associates, Inc. The storm water then flows west under Scottsdale Road and into the Central Arizona Project Reach 11 Recreation Area retention. The proposed channel alignment is shown on Exhibit 3 -- *Conceptual Grading and Drainage Plan*.

The Interim Regional Drainage Channel is proposed to be an unlined earthen channel. Grade control structures are incorporated into the vertical design of the channel in order to maintain the 100-year flow velocities within appropriate ranges. A variable bottom width is employed in the channel in order to maintain a constant channel slope adjacent to a variable sloped roadway. A 10-foot wide bottom occurs at the upstream end of each grade control structure. The drop is created by extending the sideslopes down to make a triangular channel at the downstream end of the structure. The channel transitions back to the flat bottom at the upstream end of the next grade control structure.

Erosion protection was incorporated into the channel design. Riprap erosion protection was integrated as part of each grade control structure. This protection will be of sufficient length to include the hydraulic jump associated with each structure. Riprap erosion protection is also proposed at the bends in the channel alignment to reduce the possibility of breakout and lateral migration. Revegetation and hydrosced will be used along the length of the channel for aesthetic purposes and increased erosion control.

Typical cross sections for the Interim Regional Drainage Channel were selected to provide adequate conveyance for the 100-year storm. A minimum of one foot of freeboard is provided within the channel, and the top width of the channel, including freeboard, is limited to 40 feet. The channel side slopes are limited to 4:1 along Scottsdale Road, and 3:1 along Union Hills Drive.

#### 4.0 HYDROLOGY

The 100-year design flow for the Interim Regional Drainage Channel is 300 cfs. This is based on a 100-year, 6-hour design storm utilizing HEC-1 hydrology modeling software (Ref. 3). Results of this model are included in Appendix A -- *Hydrology*. These results are compared to those published in *Drainage Study Core North/Core South* by Robert L. Ward (Ref. 4).

The included HEC-1 model is an expansion of the hydrology model completed for the *One Scottsdale Master Drainage Plan*, by Wood, Patel & Associates, Inc. (Ref. 5). The One Scottsdale development lies upstream of the project site to the north of the Loop 101 Freeway. The model was revised to expand to the south to include the proposed improvements. Flow at the Loop 101 Freeway culverts (identifier 33E.1) is now routed through the Interim Regional Drainage Channel (identifier R33E.1). The runoff from the adjacent State Land parcel (identifier ASLD) joins at the outfall culvert under Scottsdale Road near Princess Road (identifier CPPRIN). This downstream flow of 300 cfs was used as the design flow for the entire channel. The ASLD sub basin was determined to be a 35-acre area with a curve number of 77, chosen to represent desert shrub with poor hydrologic conditions. The other revision to the *One Scottsdale Master Drainage Plan* hydrology model is modification to the storage routing to account for the changes in storm water storage requirements due to channel improvements proposed here. This resulted in increased runoff under the Loop 101 Freeway.

These results are compared to existing conditions and proposed conditions models published in *Core North/Core South* (Ref. 4). Both of these models also use a curve number of 77 for the State Land sub basin. The flows published in that model are lower than those proposed here, which is considered conservative. In a separate hydraulics section of that report, the culvert design flows for the Loop 101 Freeway culverts are listed as 300 cfs, including large offsite impacts. The report proposes that offsite impacts would not affect these culverts, and revises the design flow to 65 cfs. This further establishes that the design flow for the Interim Regional Drainage Channel of 300 cfs is conservative.

	Interim Regional Drainage Channel		Core North/South Existing Conditions		Core North/South Plan 1 Proposed Conditions	
	HEC-1 CP	Q100 (cfs)	HEC-1 CP	Q100 (cfs)	HEC-1 CP	Q100 (cfs)
Loop 101 Culvert	33E.1	256	SCNA1	129	N61.3	173
State Land	ASLD	90	3B	98	N63	98
Proposed Channel	R22E.1	252	3B.1	125	N63.1	169
Outfall Culvert	CPPRIN	300	3B.2	178	N63.2	256

An existing wash traverses the ASLD parcel in a southwesterly direction. This wash is a Section 404 jurisdictional wash. In the existing conditions, it is blocked on the upstream side from receiving flow by the existing retention basin near Station 36+00. It collects only local flow and discharges into the proposed channel near Station 24+00. This local flow is estimated as 14 cfs by a Rational Method calculation which is included in Appendix A -- *Hydrology*.

## 5.0 HYDRAULICS

Final design and analysis of the Interim Regional Drainage Channel was completed using HEC-RAS (Ref. 6) hydraulic modeling software. Grade control structures are specified to manage the longitudinal slope and maintain velocity within the design range. The results of the hydraulic model are the basis for analysis of erosion potential. Grade control structures are used in lieu of bank erosion protection along the entire channel reach.

Cross sections were cut upstream, downstream, and at each grade control structure, horizontal channel bends, changes in channel lining, and along the channel length. Roughness coefficients for the channel were selected to reflect graded earth with expected landscaping and vegetation. The downstream boundary condition was set as the calculated headwater required for the proposed culvert, currently under design by Dibble & Associates, Inc. This culvert is assumed to be a reinforced concrete box culvert with two (2) 8-foot wide by 3-foot tall barrels. Culvert headwater calculations were completed with *Bentley CulvertMaster* (Ref. 7). The culvert inlet loss coefficient was set as 0.7 to reflect a drop inlet with possible skew. The upstream boundary condition was set as critical depth to reflect flow exiting the existing culverts under Union Hills Drive. Hydraulic models of the 2-year and 10-year storms were also run to analyze hydraulic conditions. Flows for these storms were approximated as 10% and 35% of the 100-year discharge, respectively, per the *Drainage Design Manual* (Ref. 8). Input hydraulic data and results are located in Appendix B – *Hydraulic Calculations*.

Velocities within the channel for the 100-year storm were found to range from 3.5 to 7 feet per second. Supercritical flow was not found to occur. The highest velocities occur as the flow exits the proposed stilling basins and slows as it approaches normal depth through the length of the open channel. The lowest velocities occur within the proposed stilling basins and where under the influence of the backwater caused by rock check dams. Provided freeboard ranges from 0.25 feet to 3 feet within the 40-foot channel corridor. Less than one foot of freeboard occurs where flow is under the influence of backwater from the rock check dams. At each location with less than one foot of provided freeboard, additional freeboard will be provided outside of the easement in the grading to existing. In order to mitigate any flooding hazard low amounts of provided freeboard might create, it is reminded that according to City of Scottsdale requirements for development within FEMA flood Zone "AO" (1 foot, 3 feet per second), all adjacent buildings must have a lowest floor a minimum of 12 inches above the water surface elevation. ✓



Flow velocities for the 10-year storm range from 2 to 5.6 feet per second. This is within the recommended range to prevent sedimentation aggradation, as well as channel erosion. At least 1.3 feet of freeboard is provided in all locations. The flow velocities for the 2-year storm range from 1 to 4.5 feet per second. At least 2 feet of freeboard is provided in all locations.

Erosion potential was analyzed using the results of the hydraulic modeling. These analyses are included in Appendix C – *Erosion Protection*. An ADWR Level 1 scour analysis found the estimated scour depth to be 3 feet. A minimum erosion protection thickness of 3 feet is therefore specified. Bend scour around the outside bank of the horizontal turns in the channel was also analyzed. A minimum length of bank protection downstream of the bends is specified as 70 feet. Riprap was selected for use as erosion protection. A fiftieth percentile diameter of 9 inches was chosen for these locations. Gradation per the *Drainage Design Manual* (Ref. 1) is specified.

Scour erosion is not expected on the upstream side of the check dams. The purpose of the check dams is to slow the rate of flow. This would more likely result in aggradation. The flow velocity for each of these check dams in the 100-year storm is approximately 3.6 feet per second, with an energy grade slope of approximately 0.26%. Since the channel slope is 0.75%, this shows that the check dams effectively produce a backwater effect and scour is not anticipated. Additionally, these dams are constructed of rock-filled gabion baskets, and are keyed into the sides and bottom of the channel to reduce the possibility of overturning. The flow will become supercritical as it pours over the dams; so erosion protection is proposed on the downstream side. For a graphical and tabular representation, please see the HEC-RAS profiles and results included in Appendix B – *Hydraulics*. ✓

## 6.0 MAINTENANCE

Ongoing maintenance of the designed or recommended drainage systems is required to preserve the design integrity and purpose of the drainage system. Failure to provide maintenance can prevent the drainage system from performing to its intended design purpose and can result in reduced performance. Maintenance within the public right-of-way is the responsibility of the governing municipality. However, it is the responsibility of private developers, homeowners associations, etc. for facilities on private property within drainage easements, and includes private streets. A regular maintenance program is required to have drainage systems perform to the level of protection or service as presented in this report and related construction documents and specifications.

## 7.0 REFERENCES

1. *Drainage Design Manual for Maricopa County, Arizona, Hydraulics* (Draft), Flood Control District of Maricopa County, September 2003.
2. *Design Standards & Policies Manual, Chapter 4 – Grading and Drainage*, City of Scottsdale, August 2007.
3. *Flood Hydrograph Package (HEC-1), Version 4.1*, U.S. Army Corps of Engineers, June 1998.
4. *Drainage Study Core North/Core South Scottsdale, Arizona*, Robert L. Ward, Consulting Engineer, September 25, 2001.
5. *One Scottsdale Master Drainage Plan*, Wood, Patel & Associates, Inc., September 26, 2006.
6. *River Analysis System (HEC-RAS), Version 3.1.3*, U.S. Army Corps of Engineers, May 2005.
7. *Bentley CulvertMaster, Version 3.1, Service Pack 1*, Bentley Systems, Inc., copyright 2005.
8. *Drainage Design Manual for Maricopa County, Arizona, Hydrology* (Draft), Flood Control District of Maricopa County, September 2003.

## APPENDIX A

### Hydrology

```

*****
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* JUN 1996 *
* VERSION 4.1 *
* RUN DATE: 04FEB08 TIME: 15 12.09 *
*****

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*****
* U. S. ARMY CORPS OF ENGINEERS *
* HYDROLOGIC ENGINEERING CENTER *
* 609 SECOND STREET *
* DAVIS, CALIFORNIA 95616 *
* (916) 756-1104 *
*****

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THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DR, AND HEC1KN

THE DEFINITIONS OF VARIABLES -RTIME- AND -RTION- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION. NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE, SINGLE EVENT DAMAGES CALCULATION, DSS WRITE SLICE FREQUENCY, DSS ROAD TIME SERIES AT DESIRED CALCULATION INTERVAL, LOSS RATE GREEN AND AMPT INFILTRATION, KINEMATIC WAVE, NEW FINITE DIFFERENCE ALGORITHM.

1 HEC-1 INPUT PAGE 1

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LINE ID 1 2 3 4 5 6 7 8 9 10
1 ID ONE SCOTSDALE (STACKED 40S) POST DEVELOPMENT CONDITION 100-YR 6-HR STORM
2 ID OFFSITE HYDROLOGY & ONSITE HYDROLOGY FOR AREA GOVERNED BY PRE-POST CRITERIA
3 ID OPTION A - ASLD CHANNEL
4 ID FILE: 100YR-PIR.DAT
5 ID OPTION B - 34.1 ACRES OF ASLD PARCEL
6 ID
7 ID BASED ON MODELS PREPARED BY: ROBERT L. WARD, P.E., CONSULTING ENGINEER
8 ID
9 ID
10 ID PRM-100 G1
11 ID C1 G1 (CENTER DRIVE PROJECT)
12 ID 540X100 G1 (STACKED 40S EXISTING CONDITION)
13 ID
14 ID ALL CURVE NUMBERS ADJUSTED TO 6-HOUR VALUES ON AUGUST 13, 2003
15 ID 100 YEAR, 6-HOUR HYPOTHETICAL STORM
16 ID AREAL RAINFALL REDUCTION IS BASED ON A 14 SQUARE MILE STORM
17 ID
18 ID
19 ID
20 ID
21 ID
22 ID
23 ID
24 ID
25 ID
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31 ID
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42 ID

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1 HEC-1 INPUT PAGE 2

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LINE ID 1 2 3 4 5 6 7 8 9 10
43 ID
44 ID
45 ID
46 ID
47 ID
48 ID
49 ID
50 ID

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51 KK RC4-C3  
 52 KM ROUTE OUTFLOW FROM CPIC3 TO CPIC17  
 53 EN TRIANGULAR CHANNEL PER PLANS 11182-E-94 AND 190-E-95  
 54 EN SIDE SLOPE = 3:1 (H:V)  
 55 EN MAX DEPTH = 1.5 FT.  
 56 RS 1 FLOW -1  
 57 RC 0.025 0.025 0.025 400 0.020  
 58 RX 0 0.5 1.0 4.49 5.5 9 9.5 10  
 59 RY 1.52 1.51 1.5 0 0 1.5 1.51 1.52  
 60 KK 1DA3  
 61 KM EXCESS RUNOFF FROM SUBAREA 1DA3  
 62 BA 0148  
 63 LS 77 31  
 64 UD .06  
 65 KK DE1DA3  
 66 KM DETENTION FOR SUBAREA 1DA3  
 67 EN OUTLET IS A 18" RGRUP WITH AN 8" ORIFICE PLATE PER PLANS 1905-E-95  
 68 RS 1 STOR 0  
 69 SV 0 1.27  
 70 SQ 0 4  
 71 SE 0 3.0  
 72 ST 3.0 15 2.8 1.5

73 KK 1DA4  
 74 KM EXCESS RUNOFF FROM SUBAREA 1DA4  
 75 BA 01  
 76 LS 77 16  
 77 UD .05

78 KK CP1DA4  
 79 KM COMBINE HYDROGRAPHS FROM 1DA4 AND DE1DA3  
 80 HC 2

81 KK DE1DA4  
 82 KM DETENTION FOR SUBAREA 1DA4  
 83 EN OUTLET IS A 18" PVC WITH AN 8" ORIFICE PLATE PER PLANS 1905-E-95  
 84 RS 1 STOR 0  
 85 SV 0 0.76  
 86 SQ 0 4  
 87 SE 0 3.0  
 88 ST 3.0 15 2.8 1.5  
 REC-1 INPUT

PAGE 3

LINE ID 1 2 3 4 5 6 7 8 9 10

89 KK 1DA5  
 90 KM EXCESS RUNOFF FROM SUBAREA 1DA5  
 91 BA 001  
 92 LS 77 5  
 93 UD 08  
 94 KK CP1C31  
 95 KM COMBINE HYDROGRAPHS FROM RC4-C3, 1DA5 AND DE1DA3  
 96 HC 3

97 KK RC3-C3  
 98 KM ROUTE OUTFLOW FROM CPIC31 TO DETIC3  
 99 EN TRIANGULAR CHANNEL PER PLANS 11182-E-94 AND 190-E-95  
 100 EN SIDE SLOPE = 3:1 (H:V)  
 101 EN MAX DEPTH = 2.35 FT.  
 102 RS 1 FLOW -1  
 103 RC 0.025 0.025 0.025 850 0.005  
 104 RX 0 0.5 1.0 8.04 8.05 15.1 15.5 16  
 105 RY 2.37 2.36 2.35 0 0 2.35 2.36 2.37  
 \* START AT OFF-SITE DALIN ON THE NORTHEAST CORNER OF VILLAGE 1 \*  
 \* .....

106 KK 011-1A  
 107 KM OFF-SITE CONTRIBUTING AREA LOCATED ON CITY'S LAND  
 108 BA 013  
 109 LS 77  
 110 UD 06

111 KK 1A2  
 112 KM EXCESS RUNOFF FROM SUBAREA 1A2  
 113 BA 004  
 114 LS 77 44  
 115 UD 06

116 KK 1A3  
 117 KM EXCESS RUNOFF FROM SUBAREA 1A3  
 118 BA 006  
 119 LS 77 40  
 120 UD 05

121 KK CPA3  
 122 KM COMBINE HYDROGRAPHS FROM 1A1, 011-1A AND 1A3  
 123 HC 3

124 KK DET1A3  
 125 KM DETENTION BASIN FOR SUBAREA 1A3  
 126 RS 1 STOR 0  
 127 SV 0 0.15  
 128 SQ 0 72  
 129 SE 0 2.5  
 130 ST 2.5 15 2.8 3.5  
 REC-1 INPUT

PAGE 4

LINE ID 1 2 3 4 5 6 7 8 9 10

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131 KK RA3-A6
132 KM ROUTE OUTFLOW HYDROGRAPH FROM DET1A1 TO DET1A6
133 PM TRAPEZOIDAL CHANNEL (ASSUMED)
134 KH SIDE SLOPE = 5:1 (H:V)
135 KH MAX DEPTH = 1.0 FT
136 KH ROT WIDTH = 10.0 FT
137 RS 1 FLOW 1
138 RC 0.025 0.025 0.025 550 0.0115
139 RX 0 0.5 1.0 6 21 21.5 22.0
140 RY 1.02 1.01 1.0 0 0 1.0 1.01 1.02

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141 KK LA6
142 KM EXCESS RUNOFF FROM SUBAREA 1A6
143 PM
144 KH 77 14
145 UD 05

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146 KK C1A6
147 KM COMBINE HYDROGRAPHS FROM RA3-A6 AND LA6
148 HC 2

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149 KK DET1A6
150 KM DETENTION BASIN FOR SUBAREA 1A6
151 RS 1 STOR 0
152 SV 0 0.20
153 SQ 0 22
154 SE 0 2.5
155 ST 2.5 15 2.8 1.5

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156 KK LA5
157 KM EXCESS RUNOFF FROM SUBAREA 1A5
158 PM
159 KH 77 46
160 UD 07

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161 KK C1A5
162 KM COMBINE HYDROGRAPHS FROM DET1A6 AND LA5
163 HC 2

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164 KK DET1A5
165 KM DETENTION BASIN FOR SUBAREA 1A5
166 RS 1 STOR 0
167 SV 0 0.65
168 SQ 0 34
169 SE 0 2.5
170 ST 3.5 15 2.8 1.5

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171 KK LA4
172 KM EXCESS RUNOFF FROM SUBAREA 1A4
173 PM
174 KH 77 48
175 UD 07

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HSC-1 INPUT

PAGE 5

LINE 10 1 2 3 4 5 6 7 8 9 10

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176 KK RA4-A7
177 KM ROUTE OUTFLOW FROM DET1A4 TO DET1A7
178 PM TRAPEZOIDAL CHANNEL (ASSUMED)
179 KH SIDE SLOPE = 10:1 (H:V)
180 KH MAX DEPTH = 1.0 FT
181 KH ROT WIDTH = 10.0 FT
182 RS 1 FLOW 1
183 RC 0.030 0.030 0.030 300 0.0175
184 RX 0 0.5 1.0 11 21 31 31.5 32.0
185 RY 1.02 1.01 1.0 0 0 1.0 1.01 1.02

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186 KK DET1A4
187 KM DETENTION BASIN FOR SUBAREA 1A4
188 RS 1 STOR 0
189 SV 0 0.37
190 SQ 0 11
191 SE 0 2.5
192 ST 2.5 15 2.0 1.5

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193 KK LA7
194 KM EXCESS RUNOFF FROM SUBAREA 1A7
195 PM
196 KH 77 27
197 UD 05

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198 KK C1A7
199 KM COMBINE HYDROGRAPHS FROM DET1A5, DET1A4, AND LA7
200 HC 3

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201 KK DET1A7
202 KM DETENTION BASIN FOR SUBAREA 1A7
203 RS 1 STOR 0
204 SV 0 0.93
205 SQ 0 11
206 SE 0 2.5
207 ST 2.5 15 2.8 1.5

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208 KK IC1
209 KM EXCESS RUNOFF FROM SUBAREA IC1
210 PM
211 KH 77 38
212 UD 09

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213 KK C1C1
214 KM COMBINE HYDROGRAPHS FROM DET1A7, AND IC1

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215 HC 2

216 KK DETIC1  
 217 EM DETENTION BASIN FOR SUBAREA 1C1  
 218 EM STORAGE VOLUME PER PLANS (405-E-95)  
 219 EM OUTLET IS A 18" RORCP PER PLANS (405-E-95)  
 220 RS 1 STOR 0  
 221 SV 0 1.5  
 222 SQ 0 14

HEC-1 INPUT

LINE ID 1 2 3 4 5 6 7 8 9 10

223 SE 0 3.6  
 224 ST 3.6 15 2.8 1.5

225 KK 1C2  
 226 EM EXCESS RUNOFF FROM SUBAREA 1C2  
 227 BA .024  
 228 LS 77 12  
 229 UD 68

230 KK CPLIC2  
 231 EM COMBINE HYDROGRAPHS FROM DETIC1 AND 1C2  
 232 HC 2

233 KK DETIC2A  
 234 EM DETENTION BASIN FOR SUBAREA 1C2  
 235 EM STORAGE VOLUME PER PLANS (405-E-95)  
 236 EM OUTLET IS A 18" RORCP PER PLANS (405-E-95)  
 237 RS 1 STOR 0  
 238 SV 0 0.39  
 239 SQ 0 14  
 240 SE 0 1.6  
 241 ST 3.6 15 2.8 1.5

242 KK DETIC2B  
 243 EM DETENTION BASIN FOR SUBAREA 1C2  
 244 EM STORAGE VOLUME PER PLANS (405-E-95)  
 245 EM OUTLET IS A 18" RORCP PER PLANS (405-E-95)  
 246 RS 1 STOR 0  
 247 SV 0 0.92  
 248 SQ 0 14  
 249 SU 0 3.6  
 250 ST 3.6 15 2.8 1.5

251 KK DETIC2C  
 252 EM DETENTION BASIN FOR SUBAREA 1C2  
 253 EM STORAGE VOLUME PER PLANS (405-E-95)  
 254 EM OUTLET IS A 18" RORCP PER PLANS (405-E-95)  
 255 RS 1 STOR 0  
 256 SV 0 0.54  
 257 SQ 0 14  
 258 SE 0 1.6  
 259 ST 3.6 15 2.8 1.5

260 KK 1C3  
 261 EM EXCESS RUNOFF FROM SUBAREA 1C3  
 262 BA .076  
 263 LS 77 15  
 264 UD 66

265 KK CPLIC3  
 266 EM COMBINE HYDROGRAPHS FROM 1C2-C1, DETIC2C, AND 1C3  
 267 HC 3

HEC-1 INPUT

LINE ID 1 2 3 4 5 6 7 8 9 10

268 KK DETIC3  
 269 EM DETENTION BASIN FOR SUBAREA 1C3  
 270 EM STORAGE VOLUME PER PLANS (405-E-95)  
 271 EM OUTLET IS A 6" W x 3" H CUL PER PLANS (1142-E-29 AND 190-E-95)  
 272 RS 1 STOR 0  
 273 SV 0 1.1  
 274 SQ 0 150  
 275 SE 0 3.5  
 276 ST 3.5 15 2.8 1.5

277 KK RCICOM  
 278 EM ROUTE OUTFLOW FROM DETIC3 TO WIDE DETCOM OUTFLOWS  
 279 RS 1 FLOW 1  
 280 RC 0.010 0.010 0.010 1000 0.016  
 281 RZ 0 5 10 20 30 40 50  
 282 RY 12.0 11.75 11.5 10.0 10.0 11.5 11.75 12.0

283 KK COMS  
 284 EM EXCESS RUNOFF FROM SUBAREA COMMERCIAL  
 285 BA .03  
 286 LS 77 90  
 287 UD 67

288 KK DETCOM  
 289 EM DETENTION FOR SUBAREA COMMERCIAL  
 290 RS 1 STOR 0  
 291 SV 0 1.1  
 292 SQ 0 13  
 293 SE 0 3  
 294 ST 3 15 2.8 1.5

295 KK CFCOM  
 296 EM COMBINE HYDROGRAPHS FROM RCICOM AND COMS  
 297 HC 2

PAGE 6

PAGE 7



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298 KK COMOFF1
299 KM ROUTE CPOCON TO CPOFF1
300 RS 1 FLOW .1
301 RC 0.030 0 030 0 030 900 0 0158
302 RX 0 5 10 20 30 40 45 50
303 RY 12 0 11.75 11.5 10.0 10.0 11.5 11.75 12.0
304 KK OFF1
305 KM EXCESS RUNOFF FROM SUBAREA OFF1
306 RA 02
307 LS 77 90
308 UD 05
309 KK DEOFF1
310 KM DETENTION FOR SUBAREA OFF1
311 RS 1 STOR 0
312 SV 0 2.4
313 SQ 0 13
314 SE 0 3

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REC-1 INPUT

PAGE 5

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LINE ID 1 2 3 4 5 6 7 8 9 10
315 ST 1 15 2.8 1.5
316 KK CPOFF1
317 KM COMBINE HYDROGRAPHS FROM COMOFF AND DEOFF1
318 RC 2
319 KK OF1OFF1
320 KM SOUTH CPOFF1 TO CPOFF1
321 RS 1 FLOW .1
322 RC 0 030 0 030 0 030 500 0 013
323 RX 0 5 10 20 30 40 45 50
324 RY 12 0 11.75 11.5 10.0 10.0 11.5 11.75 12.0
325 KK OFF1
326 KM EXCESS RUNOFF FROM SUBAREA OFF1
327 RA 016
328 LS 77 90
329 UD 07
330 KK DEOFF1
331 KM DETENTION FOR SUBAREA OFF1
332 RS 1 STOR 0
333 SV 0 2.34
334 SQ 0 13
335 SE 0 3
336 ST 3 15 2.8 1.5
337 KK CPOFF1
338 KM COMBINE HYDROGRAPHS FROM DEOFF1 AND OF1OFF1
339 RC 3
* START WEST SIDE OF STACKED 40 DESIGN CONCEPT CROSSING SCOTTSDALE RD
*
340 KK 33A1 CP
341 KM ROUTE CPOFF1 THROUGH SUB 33A
342 RK 1960 0161 045 TRAP 20 3
*
343 KK 33A 540
344 KM RUNOFF FROM SUB 33A. INCLUDES WEST SIDE OF CINDER DRIVE
345 RA 054
346 LS 77 35
347 RY 300 0 020 05 100
348 RK 2125 013 015 TRAP 20 3
*
349 KK 33A3 CP
350 KO 1
351 KM COMBINE SUB 33A, CP 33A1
352 RC 3
* END WEST SIDE OF STACKED 40 DESIGN CONCEPT CROSSING SCOTTSDALE RD
*
* BEGIN GILBERTSON MODEL FOR GRAYHAWK - VILLAGE 1
* START AT NORTHEAST CORNER OF PARCEL 10B AND GO SOUTHWEST THROUGH
* PROPOSED PARK SITE
*

```

REC-1 INPUT

PAGE 9

```

LINE ID 1 2 3 4 5 6 7 8 9 10
353 KK 10B
354 KM EXCESS RUNOFF FROM SUBAREA 10B
355 RA 04
356 LS 77 35
357 UD 06
358 KK DE10B
359 KM DETENTION FOR SUBAREA 10B
360 RS 1 STOR 0
361 SV 0 2.7
362 SQ 0 13
363 SE 0 3.0
364 ST 3 0 15 2.8 1.5
365 KK 10a1
366 KM EXCESS RUNOFF FROM SUBAREA 10a1

```



```

449      RY      12 0   11 75   11 5   10 0   10 0   11 5   11 75   12 0
450      KK      1EC
451      KM      EXCESS RUNOFF FROM SUBAREA 1EC
452      BA      0089
453      LS              77   50
454      UD      06

455      KK      DET1EC
456      KM      DETENTION FOR SUBAREA 1EC
457      RS      1      STOR      0
458      SV      0      0 8
459      SQ      0      11
460      SE      0      1
461      ST      3      15   2 8   1 5

462      KK      CP1EC
463      KM      COMBINE HYDROGRAPHS FROM SCHIA AND DET1EC
464      HC      2

465      KK      DECA2
466      KM      ROUTE OUTFLOW FROM CP1EC TO CP1EA2
467      RS      1      FLOW      -1
468      RC      0 030 0 030 0 030 500 0 009
469      RK      0      2 5      5      10      20      25      27.5      30
470      RY      12 0   11 75   11 5   10 0   10 0   11 5   11 75   12 0

471      KK      CP1EA
472      KM      COMBINE HYDROGRAPHS FROM CP1EC2, DECA2 AND PARK
473      HC      3

474      KK      REATPP
475      KM      ROUTE CP1EA TO THOMPSON PEAK PARKWAY
476      RS      1      FLOW      -1
477      RC      0 030 0 030 0 030 250 0 0166
478      RK      0      2 5      5      10      20      25      27.5      30
479      RY      12 0   11 75   11 5   10 0   10 0   11 5   11 75   12 0

```

HUC-1 INPUT

PAGE 12

```

LINE      ID      1      2      3      4      5      6      7      8      9      10

```

```

480      KK      1cd
481      KM      EXCESS RUNOFF FROM SUBAREA 1cd
482      BA      .0576
483      LS              77   52
484      UD      08

485      KK      DET1CD
486      KM      DETENTION FOR PARCEL 1CD
487      RS      1      STOR      0
488      SV      0      4 2
489      SQ      0      52
490      SE      0      3
491      ST      3      15   2 8   1 5

492      KK      OFF2
493      KM      EXCESS RUNOFF FROM SUBAREA OFF2 PUMPED HOSPITAL FLOWS
494      BA      011
495      LS              77   99
496      UD      07

497      KK      DEOFF2
498      KM      DETENTION FOR SUBAREA OFF2 PUMPED HOSPITAL FLOWS
499      RS      1      STOR      0
500      SV      0      4 5
501      SQ      0      13
502      SE      0      1
503      ST      3      15   2 8   1 5

504      KK      CPOFF2
505      KM      COMBINE HYDROGRAPHS REATPP, DET1CD AND DEOFF2
506      HC      3

```

\* END GILBERTSON MODEL FOR GRAYHAWK - VILLAGE 1

\* START EAST SIDE OF STACKED 40 DESIGN

```

507      KK      1Kc 1  ROUTE
508      KM      ROUTE CPOFF2 THROUGH SUB 1Kc
509      RK      840  0135  045      TRAP      10      2

510      KK      1Kc  SUB
511      KM      R/O FROM SUB 1Kc
512      BA      BA HAS BEEN REVISED TO REFLECT DEVELOPED SHAPE OF PARCEL 1K
513      LS      .0515
514      LS              77   55
515      UD      0 15

```

HUC-1 INPUT

PAGE 13

```

LINE      ID      1      2      3      4      5      6      7      8      9      10

```

```

516      KK      DET1K
517      KM      DETENTION FOR SUBAREA 1Kc
518      RS      1      STOR      0
519      SV      0      4 6
520      SQ      0      20
521      SE      0      1
522      ST      3      15   2 8   1 5

```

LINE	NO	DESCRIPTION	AMOUNT	DATE	BY	REMARKS
526	1	ROUTE 1	100	10/10/10	1	
527	2	ROUTE 2	100	10/10/10	2	
528	3	ROUTE 3	100	10/10/10	3	
529	4	ROUTE 4	100	10/10/10	4	
530	5	ROUTE 5	100	10/10/10	5	
531	6	ROUTE 6	100	10/10/10	6	
532	7	ROUTE 7	100	10/10/10	7	
533	8	ROUTE 8	100	10/10/10	8	
534	9	ROUTE 9	100	10/10/10	9	
535	10	ROUTE 10	100	10/10/10	10	
536	11	ROUTE 11	100	10/10/10	11	
537	12	ROUTE 12	100	10/10/10	12	
538	13	ROUTE 13	100	10/10/10	13	
539	14	ROUTE 14	100	10/10/10	14	
540	15	ROUTE 15	100	10/10/10	15	
541	16	ROUTE 16	100	10/10/10	16	
542	17	ROUTE 17	100	10/10/10	17	
543	18	ROUTE 18	100	10/10/10	18	
544	19	ROUTE 19	100	10/10/10	19	
545	20	ROUTE 20	100	10/10/10	20	
546	21	ROUTE 21	100	10/10/10	21	
547	22	ROUTE 22	100	10/10/10	22	
548	23	ROUTE 23	100	10/10/10	23	
549	24	ROUTE 24	100	10/10/10	24	
550	25	ROUTE 25	100	10/10/10	25	
551	26	ROUTE 26	100	10/10/10	26	
552	27	ROUTE 27	100	10/10/10	27	
553	28	ROUTE 28	100	10/10/10	28	
554	29	ROUTE 29	100	10/10/10	29	
555	30	ROUTE 30	100	10/10/10	30	
556	31	ROUTE 31	100	10/10/10	31	
557	32	ROUTE 32	100	10/10/10	32	
558	33	ROUTE 33	100	10/10/10	33	
559	34	ROUTE 34	100	10/10/10	34	
560	35	ROUTE 35	100	10/10/10	35	
561	36	ROUTE 36	100	10/10/10	36	
562	37	ROUTE 37	100	10/10/10	37	
563	38	ROUTE 38	100	10/10/10	38	
564	39	ROUTE 39	100	10/10/10	39	
565	40	ROUTE 40	100	10/10/10	40	
566	41	ROUTE 41	100	10/10/10	41	
567	42	ROUTE 42	100	10/10/10	42	
568	43	ROUTE 43	100	10/10/10	43	
569	44	ROUTE 44	100	10/10/10	44	
570	45	ROUTE 45	100	10/10/10	45	
571	46	ROUTE 46	100	10/10/10	46	
572	47	ROUTE 47	100	10/10/10	47	
573	48	ROUTE 48	100	10/10/10	48	
574	49	ROUTE 49	100	10/10/10	49	
575	50	ROUTE 50	100	10/10/10	50	
576	51	ROUTE 51	100	10/10/10	51	
577	52	ROUTE 52	100	10/10/10	52	
578	53	ROUTE 53	100	10/10/10	53	
579	54	ROUTE 54	100	10/10/10	54	
580	55	ROUTE 55	100	10/10/10	55	
581	56	ROUTE 56	100	10/10/10	56	
582	57	ROUTE 57	100	10/10/10	57	
583	58	ROUTE 58	100	10/10/10	58</	

```

LINE      ID ..... 1..... 2..... 3..... 4..... 5..... 6..... 7..... 8..... 9..... 10
590      DQ      0      2.7    10.4    22.6    38.7    58.4    80.8    105.4    133.6    158.5
591      DQ      185.7    212.3    230.2    246.9
*
592      KK      33C      SUB
593      KM      SUBBASIN 33C SOUTH OF CENTER DRIVE WEST SIDE OF PROPERTY
594      KM      MODIFIED AREA TO ACCOUNT FOR NEW SITE PLAN AND SUBS 04-27-06 - ADDED SOUTHWEST
595      BA      0 0296
596      LS      77      87
597      UK      200    .0068    .05    100
598      RK      1750    .017    .015          CIRC      5
*
599      KK      540CN      SUB
600      KM      SUB SOUTH OF CENTER DRIVE, CENTRAL BASIN FLOWING DIRECTLY INTO DET/RET
601      KM      INCLUDES DETENTION BASIN
602      BA      0448
603      LS      77      87
604      UK      250    .0075    .05    100
605      RK      1500    .009    .015          CIRC      4.5
*
606      KK      CT13 1 COMBINE
607      KM      COMBINE CT13.0, 33C FLOWS (Total Flow at the BASIN)
608      MC      3
*
609      KK      D_BAS
610      KM      BY-PASS FLOW THROUGH 36" PIPE (MAX Q = 30 CFS) BASIN OULETS PROVIDE
611      KM      EQUIVALENT AMOUNT OF DISCHARGE
612      DT      P-PIPE
613      DI      0      1 0      10 0      30 0      50      100.0    300.0    500.0    800.0
614      DQ      0      1.0      10.0      30.0      50      100      300      500      800
*
615      KK      D_BAS1
616      KM      DIVERT THE FIRST 1 AC-FT INTO THE SURFACE STORAGE
617      DT      D-BAS2      1.0
618      DI      0      1.0      10.0      30 0      50 0      100.0    300.0    500.0    800.0
619      DQ      0      1.0      10.0      30 0      50.0      100.0    300.0    500.0    800.0
*
620      KK      D_SURF
621      KM      DIVERT FLOW INTO SURFACE STORAGE
622      KM      (1110' 10" DIAMETER PIPE, VOL = 2.0 AC-FT)
623      KO      1
624      DT      D-SURF      2
625      DI      0      1.0      10.0      30 0      50.0      100.0    300.0    500.0    800.0
626      DQ      0      1.0      10.0      30.0      50.0      100.0    300.0    500.0    800.0
*

```

```

LINE      ID ..... 1..... 2..... 3..... 4..... 5..... 6..... 7..... 8..... 9..... 10
627      KK      B_PIPE
628      KM      RETRIEVE DIVERTED PIPE FLOW
629      DK      P-PIPE
*
630      KK      D_SURF
631      KM      RETRIEVE DIVERTED SURFACE FLOW
632      DR      D-BAS2
*
633      KK      C5400 COMBINE
634      KO      1
635      KM      COMBINE PIPE FLOW, DIVERTED SURFACE FLOW AND REMAINING SURFACE FLOW
636      MC      3
*
637      KK      540BAS
638      KO      3
639      KM      ROUTE DIVERTED FLOW THROUGH OFFLINE BASIN CONCEPT MAX H = 5.9
640      KM      ASSUMED 1000' X 80' BASIN WITH 5:1 SIDE SLOPES & 36" OUTLET
641      KM      24" BLEED-OFF PIPE PLUS 20' WIDE SPILLWAY AT 3 6"
642      RS      3      STOR      -2
643      SV      0      .001    .14    .87    1.84    3.01    4.49    5.16    5.49    5.87
644      SV      6.14
645      SE      0      .8      1      2      3      4      5      5.4    5.6    5.8
646      SE      6
647      SG      1      3.14    0.62    0.5
648      SS      3.8      20      2.8      1.5
*
649      KK      P33E.1
650      KO      1
651      KM      DIVIDE THE FLOW INTO TWO ADOT CULVERTS
652      DT      D33C.2
653      DI      0      100      200      400      600
654      DQ      0      68      136      272      408
*
655      KK      R_ADOT
656      KM      RETRIEVE DIVERTED ADOT CULVERT FLOW
657      DR      P_ADOT
*

```

658 KK 33E.1 COMBINE  
 659 KO 1  
 660 KM COMBINED DISCHARGE AT ADOT CULVERT 5 AND 6  
 661 HC 2  
 \*

# HEC-1 INPUT

PAGE 17

LINE ID. . . . .1 . . . . .2 . . . . .3 . . . . .4 . . . . .5 . . . . .6 . . . . .7 . . . . .8 . . . . .9 . . . . .10

662 KK R33E.1 ROUTE  
 663 KO 1  
 664 KM ROUTE ADOT CULVERT 5 AND 6 FLOWS THROUGH ASLD LAND  
 665 KM OPTION 5 - PROPOSED CHANNEL SOUTH OF LUND CADILLAC TO SCOTTSDALE ROAD  
 666 KM FROM SCOTTSDALE ROAD SOUTH TO PRINCESS DRIVE  
 667 KM ROUTE L=4600', TRAP SECTION HW=19' Z=5, TWmax=39'  
 668 KM ASSUME GRASS LINED CHANNEL H=0.030 UP=1597 S DOWN=1553  
 669 RK 4600 0.0080 0.03 TRAP 19 5  
 \*

670 KK ASLD SUB  
 671 KO 1  
 672 KM ASLD PARCEL EAST OF SCOTTSDALE ROAD  
 673 BA 0.0533  
 674 LS 77  
 675 UK 89 0.0213 0 1 100  
 676 RK 2300 0.0080 0.03 TRAP 19 5  
 \*

677 KK CPTPIN COMBINE  
 678 KO 1  
 679 KM COMBINE ROUTED ADOT 5 AND 6 WITH ASLD PARCEL  
 680 HC 2  
 \*

681 KK D33C.2  
 682 KO 1  
 683 KM RETRIEVE DIVERTED PIPE FLOW  
 684 DR D33C.2  
 \*

685 KK S40E1 SUB  
 686 KO 1  
 687 KM SUB EAST OF SCOTTSDALE RD, FLOWING DIRECTLY INTO SCOTTSDALE RD  
 688 KM CULVERT, TAKES SCOTT'S RD HALF ST AND SCENIC CORRIDOR  
 689 BA 0.0063  
 690 LS 77 89  
 691 UK 50 .01 .05 100  
 692 RK 600 .01 .015 CIRC 4.5  
 \*

693 KK 33C.2 COMBINE  
 694 KO 1  
 695 KM COMBINED DISCHARGE AT SCOTTSDALE ROAD CULVERT  
 696 HC 2  
 \*

697 ZZ

## SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT  
 LINE (V) ROUTING (--->) DIRECTION OR PUMP FLOW  
 NO. (.) CONNECTOR (---) RETURN OF DIVERTED OR PUMPED FLOW

```

20 1A1
   V
   V
27 DET1A1
   V
   V
34 RA1-C1
   .
   .
43 1C3
   .
   .
46 CP1C4
   V
   V
51 RC4-C3
   .
   .
60 1Da3
   V
   V
65 DE1Da3
   .
   .
73 1Da4
   .
   .
78 CP1Da4
   V
   V
81 DE1Da4
   .
   .
89 1Da5
   .
   .
  
```

```

94 CP1C31.....
  V
  V
97 RCJ-CJ)
.
.
106 . OFF-1A
.
.
111 . 1A2
.
.
116 . 1A3
.
.
121 . CPAJ.....
  V
  V
124 . DET1A3
  V
  V
131 . RAJ-A6
.
.
141 . 1A6
.
.
146 . CP1A6.....
  V
  V
149 . DET1A6
.
.
156 . 1A5
.
.
161 . CP1A5.....
  V
  V
164 . DET1A5
.
.
171 . 1A4
  V
  V
176 . RA5-A7
  V
  V
186 . DET1A6
.
.
193 . 1A7
.
.
198 . CP1A7.....
  V
  V
201 . DET1A7
.
.
200 . 1C1
.
.
211 . CP1C1.....
  V
  V
216 . DET1C1
.
.
225 . 1C2
.
.
230 . CP1C2.....
  V
  V
233 . DET1C2A
  V
  V
242 . DET1C2B
  V
  V
251 . DET1C2C
.
.
260 . 1C3
.
.
265 . CP1C3.....
  V
  V
268 . DET1C3
  V
  V
277 . RCJCOJ)
.
.
281 . COMA
  V
  V
288 . DET1COM
.
.
295 . CP1COM.....
  V

```

```

V
298 COMOFF)

301 . OFF1
V
309 . DEOFF1
V
316 CPOFF1 . . . . .
V
319 OF1OF2
V
325 . OFF3
V
330 . DEOFF3
V
337 CPOFF3 . . . . .
V
340 JJA1
V
341 . JJA
V
349 JJA3 . . . . .

353 . 1Da1
V
358 . DE1Da1
V
365 . 1Da1
V
370 . DE1Da1
V
378 . 1Da2
V
383 CU1Da2 . . . . .
V
386 RDa2E2
V
396 . 1Ea1
V
401 . DE1Ea1
V
409 . 1Ea2
V
414 CP1Ea2 . . . . .
V
417 DE1Ea2
V
424 CP1Ea2 . . . . .
V
427 PARK
V
432 . SCHOOL
V
437 . DETSCH
V
444 . SCHL2
V
450 . 1Ec
V
455 . DE1Ec
V
462 CP1Ec . . . . .
V
465 1EcEa2
V
471 CP1Ec . . . . .
V
474 RENTTP
V
480 1ED

```



[illegible]

```

658      336 1. . . .
      V
      V
662      336.1
      .
      .
670      336.1
      .
      .
677      336.1
      .
      .
684      336.1
      .
      .
691      336.1
      .
      .
698      336.1
      .
      .
699      336.1
      .
      .

```

(\*\*\*) SUBOFF ALSO COMPUTED AT THIS LOCATION

```

* FLOOD HYDROGRAPH PACKAGE (DEC-11)
* JUN 1998
* VERSION 1.1
* RUN DATE 04FEB08 TIME 15 17 09

```

```

* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 756-1104

```

ONE SCOTTSDALE (STACKED 105) POST DEVELOPMENT CONDITION 100-YR 6-HR STORM  
OFFSITE HYDROLOGY & ONSITE HYDROLOGY FOR AREA COVERED BY PRE-POST CRITERIA  
OPTION A - ASLO CHANNEL  
FILE 100YR-prec DAT  
OPTION B - 34.1 ACRES OF ASLO PARCEL

BASED ON MODELS PREPARED BY: ROBERT L. KARD, P.E., CONSULTING ENGINEER

```

P25X100 61
C1 61 (CENTER DRIVE PROJECT)
S10X100 61 (STACKED 105 EXISTING CONDITION)

```

ALL CURVE NUMBERS ADJUSTED TO 6-HOUR VALUES ON AUGUST 11, 2002  
100-YEAR, 6-HOUR HYDROLOGICAL STORM

AREAL RAINFALL REDUCTION IS BASED ON A 11 SQUARE MILE STORM

```

19 10 OUTPUT CONTROL VARIABLES
      IPRINT 5 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCALE 0 HYDROGRAPH PLOT SCALE

17 HYDROGRAPH TIME DATA
      NMIN 5 MINUTES IN COMPUTATION INTERVAL
      NDATE 1 0 STARTING DATE
      ITIME 0000 STARTING TIME
      NQ 100 NUMBER OF HYDROGRAPH ORDINATES
      NDATE 2 0 ENDING DATE
      NQTIME 0000 ENDING TIME
      ICALEN 19 CENTURY MARK

      COMPUTATION INTERVAL 00 HOURS
      TOTAL TIME BASE 21 00 HOURS

```

```

ENGLISH UNITS
DRAINAGE AREA SQUARE KILOM
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND

STORAGE VOLUME ACRE-Feet
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

```

\*\*\*

```

*****
* 336.1 * CP
*****

```

```

350 20 OUTPUT CONTROL VARIABLES
      IPRINT 1 PRINT CONTROL
      IPLOT 0 PLOT CONTROL
      QSCALE 0 HYDROGRAPH PLOT SCALE
      CONTINUE SUB 336.1 CP 336.1

```

```

352 20 HYDROGRAPH COMBINATION
      ICOMB 2 NUMBER OF HYDROGRAPHS TO COMBINE

```

\*\*\*

DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW	DA	MON	HRMN	ORD	FLOW
1	0000	2	0	*	1	0615	76	41	*	1	1230	151	5	*	1	1045	226	1	
1	0005	2	0	*	1	0620	77	40	*	1	1235	152	4	*	1	1050	227	1	
1	0010	3	0	*	1	0625	78	38	*	1	1240	153	3	*	1	1055	228	1	
1	0015	3	0	*	1	0630	79	37	*	1	1245	154	4	*	1	1100	229	1	
1	0020	5	0	*	1	0635	80	36	*	1	1250	155	4	*	1	1105	230	1	
1	0025	6	0	*	1	0640	81	35	*	1	1255	156	4	*	1	1110	231	1	
1	0030	7	0	*	1	0645	82	34	*	1	1300	157	5	*	1	1115	232	1	
1	0035	8	0	*	1	0650	83	33	*	1	1305	158	4	*	1	1120	233	1	
1	0040	9	2	*	1	0655	84	32	*	1	1310	159	5	*	1	1125	234	1	
1	0045	10	1	*	1	0700	85	31	*	1	1315	160	3	*	1	1130	235	1	
1	0050	11	3	*	1	0705	86	31	*	1	1320	161	3	*	1	1135	236	1	
1	0055	12	4	*	1	0710	87	30	*	1	1325	162	3	*	1	1140	237	1	
1	0100	13	4	*	1	0715	88	30	*	1	1330	163	3	*	1	1145	238	1	
1	0105	14	4	*	1	0720	89	29	*	1	1335	164	3	*	1	1150	239	0	
1	0110	15	5	*	1	0725	90	28	*	1	1340	165	3	*	1	1155	240	0	
1	0115	16	5	*	1	0730	91	28	*	1	1345	166	3	*	1	1200	241	0	
1	0120	17	5	*	1	0735	92	27	*	1	1350	167	3	*	1	1205	242	0	
1	0125	18	6	*	1	0740	93	26	*	1	1355	168	3	*	1	1210	243	0	
1	0130	19	6	*	1	0745	94	26	*	1	1400	169	3	*	1	1215	244	0	
1	0135	20	7	*	1	0750	95	25	*	1	1405	170	3	*	1	1220	245	0	
1	0140	21	7	*	1	0755	96	24	*	1	1410	171	3	*	1	1225	246	0	
1	0145	22	8	*	1	0800	97	23	*	1	1415	172	3	*	1	1230	247	0	
1	0150	23	8	*	1	0805	98	23	*	1	1420	173	2	*	1	1235	248	0	
1	0155	24	9	*	1	0810	99	22	*	1	1425	174	2	*	1	1240	249	0	
1	0200	25	9	*	1	0815	100	22	*	1	1430	175	2	*	1	1245	250	0	
1	0205	26	10	*	1	0820	101	21	*	1	1435	176	2	*	1	1250	251	0	
1	0210	27	11	*	1	0825	102	21	*	1	1440	177	2	*	1	1255	252	0	
1	0215	28	11	*	1	0830	103	20	*	1	1445	178	2	*	1	1300	253	0	
1	0220	29	12	*	1	0835	104	19	*	1	1450	179	2	*	1	1305	254	0	

560 ZO	OUTPUT CONTROL VARIABLES	
	IPRINT	1 PRINT CONTROL
	IPLOT	5 PLOT CONTROL
	OSCAL	0 HYDROGRAPH PLOT SCALE

DISAPPROVAL OF THE  
O.T.C. RULES IN REVENUE

1	0605	75	64	*	1	1220	149	G.	*	1	1815	224	1	*	?	0050	299	0
1	0610	75	61	*	1	1225	150	G.	*	1	1840	225	1	*	?	0055	300	0

PEAK FLOW (CFS)	TIME (HR)	6-HR (CFS)	24-HR (CFS)	72-HR (CFS)	24-72-HR (CFS)
340	3 17	92	26	25	25
		1.966	2.259	2.259	2.259
		45.	52	52	52

CUMULATIVE AREA = 41.50 MI

620 KK

\*\*\*\*\*  
D\_SURF  
\*\*\*\*\*

623 KO

OUTPUT CONTROL VARIABLES

IPRINT 1 PRINT CONTROL  
IPLOT 0 PLOT CONTROL  
QSCALE 0 HYDROGRAPH PLOT SCALE

WT

DIVERSION

ESTAB D-SUB# DIVERSION HYDROGRAPH IDENTIFICATION  
DSTPRX 2.00 MAXIMUM VOLUME TO BE DIVERTED

DI

INFLOW

00 1.00 10.00 40.00 70.00 100.00 100.00 500.00 800.00

IQ

DIVERTED FLOW

00 1.00 10.00 40.00 70.00 100.00 300.00 500.00 800.00

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DIVERSION HYDROGRAPH D-SUB#

DA	MON	HR	MIN	SEC	FLOW	DA	MON	HR	MIN	SEC	FLOW	DA	MON	HR	MIN	SEC	FLOW	DA	MON	HR	MIN	SEC	FLOW
1	0000	1	0	*	1	0515	16	0	*	1	1210	151	0	*	1	1845	226	0					0
1	0005	2	0	*	1	0620	17	0	*	1	1235	152	0	*	1	1850	227	0					0
1	0010	3	0	*	1	0625	18	0	*	1	1240	153	0	*	1	1855	228	0					0
1	0015	4	0	*	1	0630	19	0	*	1	1245	154	0	*	1	1900	229	0					0
1	0020	5	0	*	1	0635	20	0	*	1	1250	155	0	*	1	1905	230	0					0
1	0025	6	0	*	1	0640	21	0	*	1	1255	156	0	*	1	1910	231	0					0
1	0030	7	0	*	1	0645	22	0	*	1	1300	157	0	*	1	1915	232	0					0
1	0035	8	0	*	1	0650	23	0	*	1	1305	158	0	*	1	1920	233	0					0
1	0040	9	0	*	1	0655	24	0	*	1	1310	159	0	*	1	1925	234	0					0
1	0045	10	0	*	1	0700	25	0	*	1	1315	160	0	*	1	1930	235	0					0
1	0050	11	0	*	1	0705	26	0	*	1	1320	161	0	*	1	1935	236	0					0
1	0055	12	0	*	1	0710	27	0	*	1	1325	162	0	*	1	1940	237	0					0
1	0100	13	0	*	1	0715	28	0	*	1	1330	163	0	*	1	1945	238	0					0
1	0105	14	0	*	1	0720	29	0	*	1	1335	164	0	*	1	1950	239	0					0
1	0110	15	0	*	1	0725	30	0	*	1	1340	165	0	*	1	1955	240	0					0
1	0115	16	0	*	1	0730	31	0	*	1	1345	166	0	*	1	2000	241	0					0
1	0120	17	0	*	1	0735	32	0	*	1	1350	167	0	*	1	2005	242	0					0
1	0125	18	0	*	1	0740	33	0	*	1	1355	168	0	*	1	2010	243	0					0
1	0130	19	0	*	1	0745	34	0	*	1	1400	169	0	*	1	2015	244	0					0
1	0135	20	0	*	1	0750	35	0	*	1	1405	170	0	*	1	2020	245	0					0
1	0140	21	0	*	1	0755	36	0	*	1	1410	171	0	*	1	2025	246	0					0
1	0145	22	0	*	1	0800	37	0	*	1	1415	172	0	*	1	2030	247	0					0
1	0150	23	0	*	1	0805	38	0	*	1	1420	173	0	*	1	2035	248	0					0
1	0155	24	0	*	1	0810	39	0	*	1	1425	174	0	*	1	2040	249	0					0
1	0200	25	0	*	1	0815	40	0	*	1	1430	175	0	*	1	2045	250	0					0
1	0205	26	0	*	1	0820	41	0	*	1	1435	176	0	*	1	2050	251	0					0
1	0210	27	0	*	1	0825	42	0	*	1	1440	177	0	*	1	2055	252	0					0
1	0215	28	0	*	1	0830	43	0	*	1	1445	178	0	*	1	2100	253	0					0
1	0220	29	0	*	1	0835	44	0	*	1	1450	179	0	*	1	2105	254	0					0
1	0225	30	0	*	1	0840	45	0	*	1	1455	180	0	*	1	2110	255	0					0
1	0230	31	0	*	1	0845	46	0	*	1	1500	181	0	*	1	2115	256	0					0
1	0235	32	0	*	1	0850	47	0	*	1	1505	182	0	*	1	2120	257	0					0
1	0240	33	0	*	1	0855	48	0	*	1	1510	183	0	*	1	2125	258	0					0
1	0245	34	0	*	1	0900	49	0	*	1	1515	184	0	*	1	2130	259	0					0
1	0250	35	0	*	1	0905	50	0	*	1	1520	185	0	*	1	2135	260	0					0
1	0255	36	0	*	1	0910	51	0	*	1	1525	186	0	*	1	2140	261	0					0
1	0300	37	0	*	1	0915	52	0	*	1	1530	187	0	*	1	2145	262	0					0
1	0305	38	0	*	1	0920	53	0	*	1	1535	188	0	*	1	2150	263	0					0
1	0310	39	0	*	1	0925	54	0	*	1	1540	189	0	*	1	2155	264	0					0
1	0315	40	0	*	1	0930	55	0	*	1	1545	190	0	*	1	2200	265	0					0
1	0320	41	0	*	1	0935	56	0	*	1	1550	191	0	*	1	2205	266	0					0
1	0325	42	0	*	1	0940	57	0	*	1	1555	192	0	*	1	2210	267	0					0
1	0330	43	0	*	1	0945	58	0	*	1	1600	193	0	*	1	2215	268	0					0
1	0335	44	0	*	1	0950	59	0	*	1	1605	194	0	*	1	2220	269	0					0
1	0340	45	0	*	1	0955	60	0	*	1	1610	195	0	*	1	2225	270	0					0
1	0345	46	0	*	1	1000	61	0	*	1	1615	196	0	*	1	2230	271	0					0
1	0350	47	0	*	1	1005	62	0	*	1	1620	197	0	*	1	2235	272	0					0
1	0355	48	0	*	1	1010	63	0	*	1	1625	198	0	*	1	2240	273	0					0
1	0400	49	0	*	1	1015	64	0	*	1	1630	199	0	*	1	2245	274	0					0
1	0405	50	0	*	1	1020	65	0	*	1	1635	200	0	*	1	2250	275	0					0
1	0410	51	0	*	1	1025	66	0	*	1	1640	201	0	*	1	2255	276	0					0
1	0415	52	0	*	1	1030	67	0	*	1	1645	202	0	*	1	2300	277	0					0
1	0420	53	0	*	1	1035	68	0	*	1	1650	203	0	*	1	2305	278	0					0
1	0425	54	0	*	1	1040	69	0	*	1	1655	204	0	*	1	2310	279	0					0

1	0430	55	0	*	1	1045	110	0	*	1	1700	205	0	*	1	2115	200	0
1	0435	56	0	*	1	1050	111	0	*	1	1705	206	0	*	1	2120	201	0
1	0440	57	0	*	1	1055	112	0	*	1	1710	207	0	*	1	2125	202	0
1	0445	58	0	*	1	1100	113	0	*	1	1715	208	0	*	1	2130	203	0
1	0450	59	0	*	1	1105	114	0	*	1	1720	209	0	*	1	2135	204	0
1	0455	60	0	*	1	1110	115	0	*	1	1725	210	0	*	1	2140	205	0
1	0500	61	0	*	1	1115	116	0	*	1	1730	211	0	*	1	2145	206	0
1	0505	62	0	*	1	1120	117	0	*	1	1735	212	0	*	1	2150	207	0
1	0510	63	0	*	1	1125	118	0	*	1	1740	213	0	*	1	2155	208	0
1	0515	64	0	*	1	1130	119	0	*	1	1745	214	0	*	1	0000	209	0
1	0520	65	0	*	1	1135	120	0	*	1	1750	215	0	*	1	0005	290	0
1	0525	66	0	*	1	1140	121	0	*	1	1755	216	0	*	1	0010	291	0
1	0530	67	0	*	1	1145	122	0	*	1	1800	217	0	*	1	0015	292	0
1	0535	68	0	*	1	1150	123	0	*	1	1805	218	0	*	1	0020	293	0
1	0540	69	0	*	1	1155	124	0	*	1	1810	219	0	*	1	0025	294	0
1	0545	70	0	*	1	1200	125	0	*	1	1815	220	0	*	1	0030	295	0
1	0550	71	0	*	1	1205	126	0	*	1	1820	221	0	*	1	0035	296	0
1	0555	72	0	*	1	1210	127	0	*	1	1825	222	0	*	1	0040	297	0
1	0600	73	0	*	1	1215	128	0	*	1	1830	223	0	*	1	0045	298	0
1	0605	74	0	*	1	1220	129	0	*	1	1835	224	0	*	1	0050	299	0
1	0610	75	0	*	1	1225	130	0	*	1	1840	225	0	*	1	0055	300	0

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	6-HR	24-HR	72-HR	24-92-HR
237	3 08	1	1	1	1
		(INCRESE)	(INCRESE)	(INCRESE)	(INCRESE)
		074	074	074	074
		2	2	2	2
		CUMULATIVE AREA = 51 SQ MI			

# HYDROGRAPH AT STATION 0+500

DA MON HRRM	ORD	FLOW	DA MON HRRM	ORD	FLOW	DA MON HRRM	ORD	FLOW	DA MON HRRM	ORD	FLOW
1	0000	1	0	1	0615	75	0	1	1830	151	0
1	0005	2	0	1	0620	77	0	1	1835	152	0
1	0010	3	0	1	0625	78	0	1	1840	153	0
1	0015	4	0	1	0630	79	0	1	1845	154	0
1	0020	5	0	1	0635	80	0	1	1850	155	0
1	0025	6	0	1	0640	81	0	1	1855	156	0
1	0030	7	0	1	0645	82	0	1	1900	157	0
1	0035	8	0	1	0650	83	0	1	1905	158	0
1	0040	9	0	1	0655	84	0	1	1910	159	0
1	0045	10	0	1	0700	85	0	1	1915	160	0
1	0050	11	0	1	0705	86	0	1	1920	161	0
1	0055	12	0	1	0710	87	0	1	1925	162	0
1	0100	13	0	1	0715	88	0	1	1930	163	0
1	0105	14	0	1	0720	89	0	1	1935	164	0
1	0110	15	0	1	0725	90	0	1	1940	165	0
1	0115	16	0	1	0730	91	0	1	1945	166	0
1	0120	17	0	1	0735	92	0	1	1950	167	0
1	0125	18	0	1	0740	93	0	1	1955	168	0
1	0130	19	0	1	0745	94	0	1	2000	169	0
1	0135	20	0	1	0750	95	0	1	2005	170	0
1	0140	21	0	1	0755	96	0	1	2010	171	0
1	0145	22	0	1	0800	97	0	1	2015	172	0
1	0150	23	0	1	0805	98	0	1	2020	173	0
1	0155	24	0	1	0810	99	0	1	2025	174	0
1	0200	25	0	1	0815	100	0	1	2030	175	0
1	0205	26	0	1	0820	101	0	1	2035	176	0
1	0210	27	0	1	0825	102	0	1	2040	177	0
1	0215	28	0	1	0830	103	0	1	2045	178	0
1	0220	29	0	1	0835	104	0	1	2050	179	0
1	0225	30	0	1	0840	105	0	1	2055	180	0
1	0230	31	0	1	0845	106	0	1	2100	181	0
1	0235	32	0	1	0850	107	0	1	2105	182	0
1	0240	33	0	1	0855	108	0	1	2110	183	0
1	0245	34	0	1	0900	109	0	1	2115	184	0
1	0250	35	0	1	0905	110	0	1	2120	185	0
1	0255	36	0	1	0910	111	0	1	2125	186	0
1	0300	37	0	1	0915	112	0	1	2130	187	0
1	0305	38	0	1	0920	113	0	1	2135	188	0
1	0310	39	0	1	0925	114	0	1	2140	189	0
1	0315	40	0	1	0930	115	0	1	2145	190	0
1	0320	41	0	1	0935	116	0	1	2150	191	0
1	0325	42	0	1	0940	117	0	1	2155	192	0
1	0330	43	0	1	0945	118	0	1	2200	193	0
1	0335	44	0	1	0950	119	0	1	2205	194	0
1	0340	45	0	1	0955	120	0	1	2210	195	0
1	0345	46	0	1	1000	121	0	1	2215	196	0
1	0350	47	0	1	1005	122	0	1	2220	197	0
1	0355	48	0	1	1010	123	0	1	2225	198	0
1	0400	49	0	1	1015	124	0	1	2230	199	0
1	0405	50	0	1	1020	125	0	1	2235	200	0
1	0410	51	0	1	1025	126	0	1	2240	201	0
1	0415	52	0	1	1030	127	0	1	2245	202	0
1	0420	53	0	1	1035	128	0	1	2250	203	0
1	0425	54	0	1	1040	129	0	1	2255	204	0
1	0430	55	0	1	1045	130	0	1	2300	205	0
1	0435	56	0	1	1050	131	0	1	2305	206	0
1	0440	57	0	1	1055	132	0	1	2310	207	0
1	0445	58	0	1	1100	133	0	1	2315	208	0
1	0450	59	0	1	1105	134	0	1	2320	209	0
1	0455	60	0	1	1110	135	0	1	2325	210	0
1	0500	61	0	1	1115	136	0	1	2330	211	0

1	0505	62	0	*	1	1120	137	0	*	1	1735	212	0	*	1	2150	267	0
1	0510	63	0	*	1	1125	138	0	*	1	1740	213	0	*	1	2155	268	0
1	0515	64	0	*	1	1130	139	0	*	1	1745	214	0	*	2	0000	269	0
1	0520	65	0	*	1	1135	140	0	*	1	1750	215	0	*	2	0005	270	0
1	0525	66	0	*	1	1140	141	0	*	1	1755	216	0	*	2	0010	271	0
1	0530	67	0	*	1	1145	142	0	*	1	1800	217	0	*	2	0015	272	0
1	0535	68	0	*	1	1150	143	0	*	1	1805	218	0	*	2	0020	273	0
1	0540	69	0	*	1	1155	144	0	*	1	1810	219	0	*	2	0025	274	0
1	0545	70	0	*	1	1200	145	0	*	1	1815	220	0	*	2	0030	275	0
1	0550	71	0	*	1	1205	146	0	*	1	1820	221	0	*	2	0035	276	0
1	0555	72	0	*	1	1210	147	0	*	1	1825	222	0	*	2	0040	277	0
1	0600	73	0	*	1	1215	148	0	*	1	1830	223	0	*	2	0045	278	0
1	0605	74	0	*	1	1220	149	0	*	1	1835	224	0	*	2	0050	279	0
1	0610	75	0	*	1	1225	150	0	*	1	1840	225	0	*	2	0055	280	0

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	24-72-HR
109	3 17	15 (INCHES) (AC-FT)	4 271 7	4 271 7	4 271 7
CUMULATIVE AREA ~		.51 SQ MI			

633 RK CS403 COMBINE

634 RD OUTPUT CONTROL VARIABLES

IPRNT	1	PRINT CONTROL
IPLOT	0	PLOT CONTROL
OSCAL	0	HYDROGRAPH PLOT SCALE
IPRCH	0	PUNCH COMPUTED HYDROGRAPH
IOUT	21	SAVE HYDROGRAPH ON THIS UNIT
ISAV1	1	FIRST ORDINATE PUNCHED OR SAVED
ISAV2	100	LAST ORDINATE PUNCHED OR SAVED
TIMEINT	.003	TIME INTERVAL IN HOURS

COMBINE PIPE FLOW, DIVERGED SURFACE FLOW AND REMAINING SURFACE FLOW

636 HC HYDROGRAPH COMBINATION

ICOMP	3	NUMBER OF HYDROGRAPHS TO COMBINE
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# HYDROGRAPH AT STATION CS403 (SUM OF 3 HYDROGRAPHS)

DA	HR	MIN	SEC	FLOW	DA	HR	MIN	SEC	FLOW	DA	HR	MIN	SEC	FLOW	DA	HR	MIN	SEC	FLOW
1	0000	1	0	*	1	0615	76	3	*	1	1730	151	0	*	1	1815	276	0	
1	0005	2	0	*	1	0620	77	2	*	1	1735	152	0	*	1	1820	277	0	
1	0010	3	0	*	1	0625	78	2	*	1	1740	153	0	*	1	1825	278	0	
1	0015	4	0	*	1	0630	79	1	*	1	1745	154	0	*	1	1830	279	0	
1	0020	5	1	*	1	0635	80	1	*	1	1750	155	0	*	1	1835	280	0	
1	0025	6	1	*	1	0640	81	1	*	1	1755	156	0	*	1	1840	281	0	
1	0030	7	2	*	1	0645	82	1	*	1	1800	157	0	*	1	1845	282	0	
1	0035	8	2	*	1	0650	83	1	*	1	1805	158	0	*	1	1850	283	0	
1	0040	9	1	*	1	0655	84	1	*	1	1810	159	0	*	1	1855	284	0	
1	0045	10	1	*	1	0700	85	0	*	1	1815	160	0	*	1	1900	285	0	
1	0050	11	1	*	1	0705	86	0	*	1	1820	161	0	*	1	1905	286	0	
1	0055	12	1	*	1	0710	87	0	*	1	1825	162	0	*	1	1910	287	0	
1	0100	13	5	*	1	0715	88	0	*	1	1830	163	0	*	1	1915	288	0	
1	0105	14	5	*	1	0720	89	0	*	1	1835	164	0	*	1	1920	289	0	
1	0110	15	5	*	1	0725	90	0	*	1	1840	165	0	*	1	1925	290	0	
1	0115	16	5	*	1	0730	91	0	*	1	1845	166	0	*	1	1930	291	0	
1	0120	17	5	*	1	0735	92	0	*	1	1850	167	0	*	1	1935	292	0	
1	0125	18	6	*	1	0740	93	0	*	1	1855	168	0	*	1	1940	293	0	
1	0130	19	6	*	1	0745	94	0	*	1	1900	169	0	*	1	1945	294	0	
1	0135	20	6	*	1	0750	95	0	*	1	1905	170	0	*	1	1950	295	0	
1	0140	21	6	*	1	0755	96	0	*	1	1910	171	0	*	1	1955	296	0	
1	0145	22	7	*	1	0800	97	0	*	1	1915	172	0	*	1	2000	297	0	
1	0150	23	7	*	1	0805	98	0	*	1	1920	173	0	*	1	2005	298	0	
1	0155	24	7	*	1	0810	99	0	*	1	1925	174	0	*	1	2010	299	0	
1	0200	25	8	*	1	0815	100	0	*	1	1930	175	0	*	1	2015	300	0	
1	0205	26	8	*	1	0820	101	0	*	1	1935	176	0	*	1	2020	301	0	
1	0210	27	9	*	1	0825	102	0	*	1	1940	177	0	*	1	2025	302	0	
1	0215	28	10	*	1	0830	103	0	*	1	1945	178	0	*	1	2030	303	0	
1	0220	29	10	*	1	0835	104	0	*	1	1950	179	0	*	1	2035	304	0	
1	0225	30	11	*	1	0840	105	0	*	1	1955	180	0	*	1	2040	305	0	
1	0230	31	11	*	1	0845	106	0	*	1	2000	181	0	*	1	2045	306	0	
1	0235	32	10	*	1	0850	107	0	*	1	2005	182	0	*	1	2050	307	0	
1	0240	33	20	*	1	0855	108	0	*	1	2010	183	0	*	1	2055	308	0	
1	0245	34	39	*	1	0900	109	0	*	1	2015	184	0	*	1	2100	309	0	
1	0250	35	57	*	1	0905	110	0	*	1	2020	185	0	*	1	2105	310	0	
1	0255	36	74	*	1	0910	111	0	*	1	2025	186	0	*	1	2110	311	0	
1	0300	37	99	*	1	0915	112	0	*	1	2030	187	0	*	1	2115	312	0	
1	0305	38	156	*	1	0920	113	0	*	1	2035	188	0	*	1	2120	313	0	
1	0310	39	229	*	1	0925	114	0	*	1	2040	189	0	*	1	2125	314	0	

1	0315	40	219	*	1	0910	115	0	*	1	1545	190	0	*	1	2200	265	0
1	0320	41	161	*	1	0915	116	0	*	1	1550	191	0	*	1	2205	266	0
1	0325	42	111	*	1	0940	117	0	*	1	1555	192	0	*	1	2210	267	0
1	0330	43	112	*	1	0945	118	0	*	1	1600	193	0	*	1	2215	268	0
1	0335	44	90	*	1	0950	119	0	*	1	1605	194	0	*	1	2220	269	0
1	0340	45	68	*	1	0955	120	0	*	1	1610	195	0	*	1	2225	270	0
1	0345	46	51	*	1	1000	121	0	*	1	1615	196	0	*	1	2230	271	0
1	0350	47	40	*	1	1005	122	0	*	1	1620	197	0	*	1	2235	272	0
1	0355	48	33	*	1	1010	123	0	*	1	1625	198	0	*	1	2240	273	0
1	0400	49	27	*	1	1015	124	0	*	1	1630	199	0	*	1	2245	274	0
1	0405	50	22	*	1	1020	125	0	*	1	1635	200	0	*	1	2250	275	0
1	0410	51	20	*	1	1025	126	0	*	1	1640	201	0	*	1	2255	276	0
1	0415	52	18	*	1	1030	127	0	*	1	1645	202	0	*	1	2300	277	0
1	0420	53	16	*	1	1035	128	0	*	1	1650	203	0	*	1	2305	278	0
1	0425	54	14	*	1	1040	129	0	*	1	1655	204	0	*	1	2310	279	0
1	0430	55	12	*	1	1045	130	0	*	1	1700	205	0	*	1	2315	280	0
1	0435	56	11	*	1	1050	131	0	*	1	1705	206	0	*	1	2320	281	0
1	0440	57	9	*	1	1055	132	0	*	1	1710	207	0	*	1	2325	282	0
1	0445	58	8	*	1	1100	133	0	*	1	1715	208	0	*	1	2330	283	0
1	0450	59	7	*	1	1105	134	0	*	1	1720	209	0	*	1	2335	284	0
1	0455	60	7	*	1	1110	135	0	*	1	1725	210	0	*	1	2340	285	0
1	0500	61	7	*	1	1115	136	0	*	1	1730	211	0	*	1	2345	286	0
1	0505	62	7	*	1	1120	137	0	*	1	1735	212	0	*	1	2350	287	0
2	0510	63	6	*	1	1125	138	0	*	1	1740	213	0	*	1	2355	288	0
1	0515	64	6	*	1	1130	139	0	*	1	1745	214	0	*	2	0000	289	0
1	0520	65	6	*	1	1135	140	0	*	1	1750	215	0	*	2	0005	290	0
1	0525	66	6	*	1	1140	141	0	*	1	1755	216	0	*	2	0010	291	0
1	0530	67	5	*	1	1145	142	0	*	1	1800	217	0	*	2	0015	292	0
1	0535	68	5	*	1	1150	143	0	*	1	1805	218	0	*	2	0020	293	0
1	0540	69	5	*	1	1155	144	0	*	1	1810	219	0	*	2	0025	294	0
1	0545	70	5	*	1	1200	145	0	*	1	1815	220	0	*	2	0030	295	0
1	0550	71	5	*	1	1205	146	0	*	1	1820	221	0	*	2	0035	296	0
1	0555	72	5	*	1	1210	147	0	*	1	1825	222	0	*	2	0040	297	0
1	0600	73	5	*	1	1215	148	0	*	1	1830	223	0	*	2	0045	298	0
1	0605	74	4	*	1	1220	149	0	*	1	1835	224	0	*	2	0050	299	0
2	0610	75	3	*	1	1225	150	0	*	1	1840	225	0	*	2	0055	300	0

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*****
PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
* (CFS)        (HR)      6-HR      24-HR      72-HR      21 92-HR
* 339          3 17      (CFS)      30          7          7          7
      (INCHES)  1.540      1.544      544        514
      (AC FT)   15          15          15          15
      CUMULATIVE AREA = .51 SQ MI
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*****
632 KK      0.0000
*****

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638 KD      OUTPUT CONTROL VARIABLES
              INPUT      1 PRINT CONTROL
              IPILOT     0 PLOT CONTROL
              QSCALE     0. HYDROGRAPH PLOT SCALE
              ROUTE DIVERTED FLOW THROUGH OFFLINE BASIN CONCEPT MAX H = 5.9
              ASSUMED 1000' X 80' BASIN WITH 5:1 SIDE SLOPES & 16" OUTLET
              21" BLEED-OFF PIPE PLUS 20' WIDE SPILLWAY AT 3.6'

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#### HYDROGRAPH ROUTING DATA

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642 RS      STORAGE ROUTING
              NSTPS      1 NUMBER OF SUBREACHES
              ITYPE      5TOR TYPE OF INITIAL CONDITION
              RESPRIC     1.00 INITIAL COEFFICIENT
              X           00 WORKING R AND D COEFFICIENT

643 SV      STORAGE      0          0          1          2          1.8          3.0          1.5          5.2          5.5          5.0
                        6.2

645 SE      ELEVATION    00          80          1.00          2.00          3.00          4.00          5.00          6.40          5.60          5.80
                        6.00

647 SL      LOW-LEVEL OUTLET
              ELEV      1.00 ELEVATION AT CENTER OF OUTLET
              AREA      3.14 CROSS-SECTIONAL AREA
              COEF      62 COEFFICIENT
              EXPL      50 EXPONENT OF HEAD

648 SS      SPILLWAY
              CREL      3.80 SPILLWAY CREST ELEVATION
              SPWID     20.00 SPILLWAY WIDTH
              COEF      2.80 WEIR COEFFICIENT
              EXPR      1.50 EXPONENT OF HEAD

```

#### COMPUTED OUTFLOW-ELEVATION DATA

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      OUTFLOW      00          00          15.21          15.18          17.27          18.53          19.98          21.48          23.10          24.13
      ELEVATION    00          1.00          1.95          2.07          2.22          2.41          2.54          2.93          3.30          3.90

      OUTFLOW      26.75          28.09          31.54          41.68          54.26          72.26          96.61          128.34          168.16          217.65
      ELEVATION    3.84          2.92          4.03          4.19          4.39          4.63          4.91          5.23          5.60          6.00

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COMBINED STORAGE-OUTFLOW-ELEVATION DATA									
STORAGE	OUTFLOW	ELEVATION	STORAGE	OUTFLOW	ELEVATION	STORAGE	OUTFLOW	ELEVATION	STORAGE
0.00	0.00	1.00	0.00	0.00	1.00	0.00	0.00	1.00	0.00
0.0000	0.0000	1.0000	0.0000	0.0000	1.0000	0.0000	0.0000	1.0000	0.0000
0.0005	0.0005	1.0005	0.0005	0.0005	1.0005	0.0005	0.0005	1.0005	0.0005
0.0010	0.0010	1.0010	0.0010	0.0010	1.0010	0.0010	0.0010	1.0010	0.0010
0.0015	0.0015	1.0015	0.0015	0.0015	1.0015	0.0015	0.0015	1.0015	0.0015
0.0020	0.0020	1.0020	0.0020	0.0020	1.0020	0.0020	0.0020	1.0020	0.0020
0.0025	0.0025	1.0025	0.0025	0.0025	1.0025	0.0025	0.0025	1.0025	0.0025
0.0030	0.0030	1.0030	0.0030	0.0030	1.0030	0.0030	0.0030	1.0030	0.0030
0.0035	0.0035	1.0035	0.0035	0.0035	1.0035	0.0035	0.0035	1.0035	0.0035
0.0040	0.0040	1.0040	0.0040	0.0040	1.0040	0.0040	0.0040	1.0040	0.0040
0.0045	0.0045	1.0045	0.0045	0.0045	1.0045	0.0045	0.0045	1.0045	0.0045
0.0050	0.0050	1.0050	0.0050	0.0050	1.0050	0.0050	0.0050	1.0050	0.0050
0.0055	0.0055	1.0055	0.0055	0.0055	1.0055	0.0055	0.0055	1.0055	0.0055
0.0060	0.0060	1.0060	0.0060	0.0060	1.0060	0.0060	0.0060	1.0060	0.0060
0.0065	0.0065	1.0065	0.0065	0.0065	1.0065	0.0065	0.0065	1.0065	0.0065
0.0070	0.0070	1.0070	0.0070	0.0070	1.0070	0.0070	0.0070	1.0070	0.0070
0.0075	0.0075	1.0075	0.0075	0.0075	1.0075	0.0075	0.0075	1.0075	0.0075
0.0080	0.0080	1.0080	0.0080	0.0080	1.0080	0.0080	0.0080	1.0080	0.0080
0.0085	0.0085	1.0085	0.0085	0.0085	1.0085	0.0085	0.0085	1.0085	0.0085
0.0090	0.0090	1.0090	0.0090	0.0090	1.0090	0.0090	0.0090	1.0090	0.0090
0.0095	0.0095	1.0095	0.0095	0.0095	1.0095	0.0095	0.0095	1.0095	0.0095
0.0100	0.0100	1.0100	0.0100	0.0100	1.0100	0.0100	0.0100	1.0100	0.0100
0.0105	0.0105	1.0105	0.0105	0.0105	1.0105	0.0105	0.0105	1.0105	0.0105
0.0110	0.0110	1.0110	0.0110	0.0110	1.0110	0.0110	0.0110	1.0110	0.0110
0.0115	0.0115	1.0115	0.0115	0.0115	1.0115	0.0115	0.0115	1.0115	0.0115
0.0120	0.0120	1.0120	0.0120	0.0120	1.0120	0.0120	0.0120	1.0120	0.0120
0.0125	0.0125	1.0125	0.0125	0.0125	1.0125	0.0125	0.0125	1.0125	0.0125
0.0130	0.0130	1.0130	0.0130	0.0130	1.0130	0.0130	0.0130	1.0130	0.0130
0.0135	0.0135	1.0135	0.0135	0.0135	1.0135	0.0135	0.0135	1.0135	0.0135
0.0140	0.0140	1.0140	0.0140	0.0140	1.0140	0.0140	0.0140	1.0140	0.0140
0.0145	0.0145	1.0145	0.0145	0.0145	1.0145	0.0145	0.0145	1.0145	0.0145
0.0150	0.0150	1.0150	0.0150</						

1	0640	81	7.	.5	1.4	*	1	1500	181	0.	.1	1.0	*	1	2320	281	0.	.1	1.0
1	0645	82	6.	.4	1.4	*	1	1505	182	0.	.1	1.0	*	1	2325	282	0.	.1	1.0
1	0650	83	5	.4	1.3	*	1	1510	183	0.	.1	1.0	*	1	2330	283	0.	.1	1.0
1	0655	84	5	.4	1.3	*	1	1515	184	0.	.1	1.0	*	1	2335	284	0.	.1	1.0
1	0700	85	4	.3	1.3	*	1	1520	185	0.	.1	1.0	*	1	2340	285	0.	.1	1.0
1	0705	86	4.	.3	1.2	*	1	1525	186	0.	.1	1.0	*	1	2345	286	0.	.1	1.0
1	0710	87	3.	.3	1.2	*	1	1530	187	0.	.1	1.0	*	1	2350	287	0.	.1	1.0
1	0715	88	3.	.3	1.2	*	1	1535	188	0.	.1	1.0	*	1	2355	288	0.	.1	1.0
1	0720	89	2.	.2	1.1	*	1	1540	189	0.	.1	1.0	*	1	0000	289	0.	.1	1.0
1	0725	90	2.	.2	1.1	*	1	1545	190	0.	.1	1.0	*	1	0005	290	0.	.1	1.0
1	0730	91	2.	.2	1.1	*	1	1550	191	0.	.1	1.0	*	1	0010	291	0.	.1	1.0
1	0735	92	2.	.2	1.1	*	1	1555	192	0.	.1	1.0	*	1	0015	292	0.	.1	1.0
1	0740	93	1.	.2	1.1	*	1	1600	193	0.	.1	1.0	*	1	0020	293	0.	.1	1.0
1	0745	94	1.	.2	1.1	*	1	1605	194	0.	.1	1.0	*	1	0025	294	0.	.1	1.0
1	0750	95	1.	.2	1.1	*	1	1610	195	0.	.1	1.0	*	1	0030	295	0.	.1	1.0
1	0755	96	1.	.2	1.1	*	1	1615	196	0.	.1	1.0	*	1	0035	296	0.	.1	1.0
1	0800	97	1.	.2	1.1	*	1	1620	197	0.	.1	1.0	*	1	0040	297	0.	.1	1.0
1	0805	98	1.	.2	1.0	*	1	1625	198	0.	.1	1.0	*	1	0045	298	0.	.1	1.0
1	0810	99	1.	.2	1.0	*	1	1630	199	0.	.1	1.0	*	1	0050	299	0.	.1	1.0
1	0815	100	1.	.2	1.0	*	1	1635	200	0.	.1	1.0	*	1	0055	300	0.	.1	1.0

PEAK FLOW	TIME	6-HR	24-HR	72-HR	24.92-HR
(CFS)	(HR)				
159.	1.43	29	7.	1	7.
	(INCHES)	537	539	539	539
	(AC-FT)	14	15.	15.	15.

PEAK STORAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
(AC-FT)	(HR)				
5.	2 33	2	1	1	1

PEAK STAGE	TIME	6-HR	24-HR	72-HR	24.92-HR
(FEET)	(HR)				
5.57	1 23	2.64	1.47	1.40	1.40

CUMULATIVE AREA = .51 SQ MI

\*\*\*\*\*  
 649 KA \* H33E.1 \*  
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650 KO OUTPUT CONTROL VARIABLES  
 IPRT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCAL 0. HYDROGRAPH PLOT SCALE  
 DIVIDE THE FLOW INTO TWO ADJUT CULVERTS

DT	DIVERSION	1STAD	D33C.2	DIVERSION HYDROGRAPH IDENTIFICATION
DI	INFLOW	00	100.00	700.00 400.00 600.00
DQ	DIVERTED FLOW	.00	68.00	136.00 272.00 408.00

# DIVERSION HYDROGRAPH D33C 2

DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*	DA	MON	HRMN	ORD	FLOW	*
1		0000	1	0.	*	1		0615	76	9.	*	1		1230	154	0.	*	1		1815	226	0.	*
1		0005	2	0.	*	1		0620	77	9.	*	1		1235	152	0.	*	1		1850	227	0.	*
1		0010	3	0.	*	1		0625	78	7	*	1		1240	153	0.	*	1		1855	228	0.	*
1		0015	4	0.	*	1		0630	79	6	*	1		1245	154	0.	*	1		1900	229	0.	*
1		0020	5	0.	*	1		0635	80	5.	*	1		1250	155	0.	*	1		1905	230	0.	*
1		0025	6	0	*	1		0640	81	5	*	1		1255	156	0	*	1		1910	231	0.	*
1		0030	7	0	*	1		0645	82	4	*	1		1300	157	0.	*	1		1915	232	0.	*
1		0035	8	0	*	1		0650	83	4.	*	1		1305	158	0.	*	1		1920	233	0	*
1		0040	9	0	*	1		0655	84	3.	*	1		1310	159	0	*	1		1925	234	0	*
1		0045	10	0.	*	1		0700	85	3	*	1		1315	160	0.	*	1		1930	235	0.	*
1		0050	11	0.	*	1		0705	86	2.	*	1		1320	161	0.	*	1		1935	236	0.	*
1		0055	12	0.	*	1		0710	87	2	*	1		1325	162	0.	*	1		1940	237	0.	*
1		0100	13	0.	*	1		0715	88	2.	*	1		1330	163	0.	*	1		1945	238	0.	*
1		0105	14	1.	*	1		0720	89	2.	*	1		1335	164	0	*	1		1950	239	0.	*
1		0110	15	2.	*	1		0725	90	1	*	1		1340	165	0	*	2		1955	240	0.	*
1		0115	16	1.	*	1		0730	91	1.	*	1		1345	166	0.	*	1		2000	241	0.	*
1		0120	17	2.	*	1		0735	92	1	*	1		1350	167	0	*	1		2005	242	0.	*
1		0125	18	2.	*	1		0740	93	1.	*	1		1355	168	0	*	1		2010	243	0	*
1		0130	19	2.	*	2		0745	94	1.	*	1		1400	169	0	*	1		2015	244	0.	*
1		0135	20	3.	*	1		0750	95	1.	*	1		1405	170	0.	*	1		2020	245	0.	*
1		0140	21	3.	*	1		0755	96	1.	*	2		1410	171	0.	*	1		2025	246	0	*
1		0145	22	3.	*	2		0800	97	1.	*	2		1415	172	0.	*	1		2030	247	0	*
1		0150	23	3	*	1		0805	98	1.	*	1		1420	173	0.	*	1		2035	248	0.	*
1		0155	24	3.	*	1		0810	99	0.	*	1		1425	174	0.	*	1		2040	249	0.	*
1		0200	25	4	*	1		0815	100	0	*	1		1430	175	0.	*	1		2045	250	0.	*
1		0205	26	4	*	1		0820	101	0.	*	1		1435	176	0.	*	1		2050	251	0.	*



1	0245	34	5.	*	1	0900	109	0.	*	1	1515	104	0.	*	1	2130	259	0.
1	0250	35	5.	*	1	0905	110	0.	*	1	1520	185	0.	*	1	2135	260	0.
1	0255	36	6.	*	1	0910	111	0.	*	1	1525	186	0.	*	1	2140	261	0.
1	0300	37	7.	*	1	0915	112	0.	*	1	1530	187	0.	*	1	2145	262	0.
1	0305	38	8.	*	1	0920	113	0.	*	1	1535	188	0.	*	1	2150	263	0.
1	0310	39	22.	*	1	0925	114	0.	*	1	1540	189	0.	*	1	2155	264	0.
1	0315	40	45.	*	1	0930	115	0.	*	1	1545	190	0.	*	1	2200	265	0.
1	0320	41	51.	*	1	0935	116	0.	*	1	1550	191	0.	*	1	2205	266	0.
1	0325	42	10	*	1	0940	117	0.	*	1	1555	192	0.	*	1	2210	267	0.
1	0330	43	15.	*	1	0945	118	0.	*	1	1600	193	0.	*	1	2215	268	0.
1	0335	44	41.	*	1	0950	119	0.	*	1	1605	194	0.	*	1	2220	269	0.
1	0340	45	35.	*	1	0955	120	0.	*	1	1610	195	0.	*	1	2225	270	0.
1	0345	46	30.	*	1	1000	121	0.	*	1	1615	196	0.	*	1	2230	271	0.
1	0350	47	25.	*	1	1005	122	0.	*	1	1620	197	0.	*	1	2235	272	0.
1	0355	48	20.	*	1	1010	123	0.	*	1	1625	198	0.	*	1	2240	273	0.
1	0400	49	17.	*	1	1015	124	0.	*	1	1630	199	0.	*	1	2245	274	0.
1	0405	50	15.	*	1	1020	125	0.	*	1	1635	200	0.	*	1	2250	275	0.
1	0410	51	13.	*	1	1025	126	0.	*	1	1640	201	0.	*	1	2255	276	0.
1	0415	52	11.	*	1	1030	127	0.	*	1	1645	202	0.	*	1	2300	277	0.
1	0420	53	10.	*	1	1035	128	0.	*	1	1650	203	0.	*	1	2305	278	0.
1	0425	54	9.	*	1	1040	129	0.	*	1	1655	204	0.	*	1	2310	279	0.
1	0430	55	8.	*	1	1045	130	0.	*	1	1700	205	0.	*	1	2315	280	0.
1	0435	56	0.	*	1	1050	131	0.	*	1	1705	206	0.	*	1	2320	281	0.
1	0440	57	0.	*	1	1055	132	0.	*	1	1710	207	0.	*	1	2325	282	0.
1	0445	58	0.	*	1	1100	133	0.	*	1	1715	208	0.	*	1	2330	283	0.
1	0450	59	8.	*	1	1105	134	0.	*	1	1720	209	0.	*	1	2335	284	0.
1	0455	60	8.	*	1	1110	135	0.	*	1	1725	210	0.	*	1	2340	285	0.
1	0500	61	0.	*	1	1115	136	0.	*	1	1730	211	0.	*	1	2345	286	0.
1	0505	62	7.	*	1	1120	137	0.	*	1	1735	212	0.	*	1	2350	287	0.
1	0510	63	7.	*	1	1125	138	0.	*	1	1740	213	0.	*	1	2355	288	0.
1	0515	64	7.	*	1	1130	139	0.	*	1	1745	214	0.	*	2	0000	289	0.
1	0520	65	7.	*	1	1135	140	0.	*	1	1750	215	0.	*	2	0005	290	0.
1	0525	66	7.	*	1	1140	141	0.	*	1	1755	216	0.	*	2	0010	291	0.
1	0530	67	6.	*	1	1145	142	0.	*	1	1800	217	0.	*	2	0015	292	0.
1	0535	68	6.	*	1	1150	143	0.	*	1	1805	218	0.	*	2	0020	293	0.
1	0540	69	6.	*	1	1155	144	0.	*	1	1810	219	0.	*	2	0025	294	0.
1	0545	70	6.	*	1	1200	145	0.	*	1	1815	220	0.	*	2	0030	295	0.
1	0550	71	6.	*	1	1205	146	0.	*	1	1820	221	0.	*	2	0035	296	0.
1	0555	72	5.	*	1	1210	147	0.	*	1	1825	222	0.	*	2	0040	297	0.
1	0600	73	5.	*	1	1215	148	0.	*	1	1830	223	0.	*	2	0045	298	0.
1	0605	74	5.	*	1	1220	149	0.	*	1	1835	224	0.	*	2	0050	299	0.
1	0610	75	5.	*	1	1225	150	0.	*	1	1840	225	0.	*	2	0055	300	0.

PEAK FLOW TIME  
 (CFS) (HR)  
 51 3 33  
 (INCHES) 9. 7. 7. 7.  
 (AC-FT) 170 .172 .172 .172  
 5. 5. 5. 5.  
 CUMULATIVE AREA = .51 SQ MI

658 KK \*\*\*\*\*  
 \* 33: 1 \* COMBINE  
 \* \*\*\*\*\*  
 659 KO OUTPUT CONTROL VARIABLES  
 IPRINT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 OSCAL 0. HYDROGRAPH PLOT SCALE  
 COMBINED DISCHARGE AT ADOT CULVERT 5 AND 6  
 661 HC HYDROGRAPH COMBINATION  
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE  
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# HYDROGRAPH AT STATION 335.1 SUM OF 2 HYDROGRAPHS

DA	MON	HR:MN	ORD	FLOW	DA	MON	HR:MN	ORD	FLOW	DA	MON	HR:MN	ORD	FLOW	DA	MON	HR:MN	ORD	FLOW
1	0000	1	0.	*	1	0615	76	62.	*	1	1230	251	5.	*	1	1845	226	1.	1.
1	0005	2	0.	*	1	0620	77	59.	*	1	1235	152	5.	*	1	1850	227	1.	1.
1	0010	3	0.	*	1	0625	78	56.	*	1	1240	153	5.	*	1	1855	228	1.	1.
1	0015	4	0.	*	1	0630	79	53.	*	1	1245	154	5.	*	1	1900	229	1.	1.
1	0020	5	0.	*	1	0635	80	51.	*	1	1250	155	5.	*	1	1905	230	1.	1.
1	0025	6	1.	*	1	0640	81	48.	*	1	1255	156	5.	*	1	1910	231	1.	1.
1	0030	7	1.	*	1	0645	82	46.	*	1	1300	157	5.	*	1	1915	232	1.	1.
1	0035	8	2.	*	1	0650	83	44.	*	1	1305	158	5.	*	1	1920	233	1.	1.
1	0040	9	3.	*	1	0655	84	42.	*	1	1310	159	4.	*	1	1925	234	1.	1.
1	0045	10	4.	*	1	0700	85	40.	*	1	1315	160	4.	*	1	1930	235	1.	1.
1	0050	11	5.	*	1	0705	86	39.	*	1	1320	161	4.	*	1	1935	236	1.	1.
1	0055	12	6.	*	1	0710	87	37.	*	1	1325	162	4.	*	1	1940	237	1.	1.
1	0100	13	7.	*	1	0715	88	36.	*	1	1330	163	4.	*	1	1945	238	1.	1.
1	0105	14	7.	*	1	0720	89	34.	*	1	1335	164	4.	*	1	1950	239	1.	1.
1	0110	15	8.	*	1	0725	90	33.	*	1	1340	165	4.	*	1	1955	240	1.	1.
1	0115	16	9.	*	1	0730	91	32.	*	1	1345	166	4.	*	1	2000	241	1.	1.
1	0120	17	9.	*	1	0735	92	31.	*	2	1350	167	4.	*	1	2005	242	1.	1.

[illegible]

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COMPUTED KINEMATIC PARAMETERS  
VARIABLE TIME STEP  
(DT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	N	DT (MIN)	DX (FT)	PEAK (FPS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM CELERITY (FPS)
RAIN	.98	1.43	1.15	1533.3	255.01	701.54	1.92	7.18

CONTINUITY SUMMARY (AC-FT) : INFLOW= 5700E+02 EXCESS= 0000E+00 OUTFLOW= 5203E+02 BASIN STORAGE= 2409E+01 PERCENT ERROR= 1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

DATA	98	1.43	1.00	251.70	700.00	1.92
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HYDROGRAPH AT STATION R33E 1

DA	MON	HRNN	ORD	FLOW	DA	MON	HRNN	ORD	FLOW	DA	MON	HRNN	ORD	FLOW	DA	MON	HRNN	ORD	FLOW
1	0000	1	0	*	1	0615	76	69	*	1	1230	151	6	*	1	1845	726	1.	
1	0005	2	0	*	1	0620	77	66	*	1	1235	152	6	*	1	1850	727	1.	
1	0010	3	0	*	1	0625	78	63	*	1	1240	153	6	*	1	1855	728	1.	
1	0015	4	0	*	1	0630	79	60	*	1	1245	154	6	*	1	1900	729	1	
1	0020	5	0	*	1	0635	80	57	*	1	1250	155	5	*	1	1905	730	1	
1	0025	6	0	*	1	0640	81	54	*	1	1255	156	5	*	1	1910	731	1	
1	0030	7	0	*	1	0645	82	51	*	1	1300	157	5	*	1	1915	732	1	
1	0035	8	0	*	1	0650	83	49	*	1	1305	158	5	*	1	1920	733	1	
1	0040	9	0	*	1	0655	84	47	*	1	1310	159	5	*	1	1925	734	1	
1	0045	10	0	*	1	0700	85	45	*	1	1315	160	5	*	1	1930	735	1	
1	0050	11	0	*	1	0705	86	43	*	1	1320	161	5	*	1	1935	736	1	
1	0055	12	0	*	1	0710	87	41	*	1	1325	162	5	*	1	1940	737	1	
1	0100	13	1	*	1	0715	88	40	*	1	1330	163	4	*	1	1945	738	1	
1	0105	14	2	*	1	0720	89	38	*	1	1335	164	4	*	1	1950	739	1	
1	0110	15	3	*	1	0725	90	37	*	1	1340	165	4	*	1	1955	740	1	
1	0115	16	5	*	1	0730	91	35	*	1	1345	166	4	*	1	2000	741	1	
1	0120	17	6	*	1	0735	92	34	*	1	1350	167	4	*	1	2005	742	1	
1	0125	18	7	*	1	0740	93	33	*	1	1355	168	4	*	1	2010	743	1	
1	0130	19	8	*	1	0745	94	31	*	1	1400	169	4	*	1	2015	744	1	
1	0135	20	9	*	1	0750	95	30	*	1	1405	170	4	*	1	2020	745	1	
1	0140	21	10	*	1	0755	96	29	*	1	1410	171	4	*	1	2025	746	1	
1	0145	22	10	*	1	0800	97	28	*	1	1415	172	4	*	1	2030	747	1	
1	0150	23	11	*	1	0805	98	27	*	1	1420	173	4	*	1	2035	748	1	
1	0155	24	12	*	1	0810	99	26	*	1	1425	174	3	*	1	2040	749	1	
1	0200	25	13	*	1	0815	100	25	*	1	1430	175	3	*	1	2045	750	1	
1	0205	26	14	*	1	0820	101	24	*	1	1435	176	3	*	1	2050	751	1	
1	0210	27	15	*	1	0825	102	24	*	1	1440	177	3	*	1	2055	752	1	
1	0215	28	16	*	1	0830	103	23	*	1	1445	178	3	*	1	2100	753	1	
1	0220	29	17	*	1	0835	104	23	*	1	1450	179	3	*	1	2105	754	1	
1	0225	30	18	*	1	0840	105	22	*	1	1455	180	3	*	1	2110	755	1	
1	0230	31	19	*	1	0845	106	21	*	1	1500	181	3	*	1	2115	756	1	
1	0235	32	20	*	1	0850	107	20	*	1	1505	182	3	*	1	2120	757	2	
1	0240	33	22	*	1	0855	108	20	*	1	1510	183	3	*	1	2125	758	1	
1	0245	34	26	*	1	0900	109	19	*	1	1515	184	3	*	1	2130	759	1	
1	0250	35	32	*	1	0905	110	19	*	1	1520	185	3	*	1	2135	760	1	
1	0255	36	45	*	1	0910	111	18	*	1	1525	186	3	*	1	2140	761	1	
1	0300	37	61	*	1	0915	112	17	*	1	1530	187	3	*	1	2145	762	1	
1	0305	38	73	*	1	0920	113	17	*	1	1535	188	3	*	1	2150	763	1	
1	0310	39	106	*	1	0925	114	16	*	1	1540	189	3	*	1	2155	764	1	
1	0315	40	130	*	1	0930	115	16	*	1	1545	190	3	*	1	2200	765	1	
1	0320	41	152	*	1	0935	116	15	*	1	1550	191	3	*	1	2205	766	1	
1	0325	42	162	*	1	0940	117	15	*	1	1555	192	3	*	1	2210	767	0	
1	0330	43	163	*	1	0945	118	15	*	1	1600	193	3	*	1	2215	768	0	
1	0335	44	173	*	1	0950	119	14	*	1	1605	194	3	*	1	2220	769	0	
1	0340	45	172	*	1	0955	120	14	*	1	1610	195	2	*	1	2225	770	0	
1	0345	46	197	*	1	1000	121	13	*	1	1615	196	2	*	1	2230	771	0	
1	0350	47	197	*	1	1005	122	13	*	1	1620	197	2	*	1	2235	772	0	
1	0355	48	177	*	1	1010	123	13	*	1	1625	198	2	*	1	2240	773	0	
1	0400	49	165	*	1	1015	124	12	*	1	1630	199	2	*	1	2245	774	0	
1	0405	50	156	*	1	1020	125	12	*	1	1635	200	2	*	1	2250	775	0	
1	0410	51	140	*	1	1025	126	12	*	1	1640	201	2	*	1	2255	776	0	
1	0415	52	142	*	1	1030	127	11	*	1	1645	202	2	*	1	2300	777	0	
1	0420	53	137	*	1	1035	128	11	*	1	1650	203	2	*	1	2305	778	0	
1	0425	54	132	*	1	1040	129	11	*	1	1655	204	2	*	1	2310	779	0	
1	0430	55	128	*	1	1045	130	10	*	1	1700	205	2	*	1	2315	780	0	
1	0435	56	121	*	1	1050	131	10	*	1	1705	206	2	*	1	2320	781	0	
1	0440	57	121	*	1	1055	132	10	*	1	1710	207	2	*	1	2325	782	0	
1	0445	58	118	*	1	1100	133	10	*	1	1715	208	2	*	1	2330	783	0	
1	0450	59	115	*	1	1105	134	9	*	1	1720	209	2	*	1	2335	784	0	
1	0455	60	112	*	1	1110	135	9	*	1	1725	210	2	*	1	2340	785	0	
1	0500	61	108	*	1	1115	136	9	*	1	1730	211	2	*	1	2345	786	0	
1	0505	62	104	*	1	1120	137	9	*	1	1735	212	2	*	1	2350	787	0	
1	0510	63	102	*	1	1125	138	8	*	1	1740	213	2	*	1	2355	788	0	
1	0515	64	99	*	1	1130	139	8	*	1	1745	214	2	*	1	0000	789	0	
1	0520	65	96	*	1	1135	140	8	*	1	1750	215	2	*	1	0005	790	0	
1	0525	66	93	*	1	1140	141	8	*	1	1755	216	2	*	1	0010	791	0	
1	0530	67	90	*	1	1145	142	8	*	1	1800	217	2	*	1	0015	792	0	
1	0535	68	87	*	1	1150	143	7	*	1	1805	218	2	*	1	0020	793	0	
1	0540	69	85	*	1	1155	144	7	*	1	1810	219	2	*	1	0025	794	0	
1	0545	70	82	*	1	1200	145	7	*	1	1815	220	2	*	1	0030	795	0	
1	0550	71	80	*	1	1205	146	7	*	1	1820	221	2	*	1	0035	796	0	
1	0555	72	78	*	1	1210	147	7	*	1	1825	222	2	*	1	0040	797	0	
1	0600	73	75	*	1	1215	148	6	*	1	1830	223	2	*	1	0045	798	0	
1	0605	74	73	*	1	1220	149	6	*	1	1835	224	2	*	1	0050	799	0	
1	0610	75	71	*	1	1225	150	6	*	1	1840	225	2	*	1	0055	800	0	

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PEAK FLOW      TIME      MAXIMUM AVERAGE FLOW
(CFS)          (HR)      6-HR      24-HR      72-HR      74 72-HR
*      252      3 33      (CFS)      91      76      75      24
      (INCHES)  1 655      1 916      1 916      1 916
      (AC-FT)   15.      52      52      52
      CIRCULATIVE AREA = 51 50 MI

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*****
670 KK      *      ASLO      *      SUB
*****

671 KO      OUTPUT CONTROL VARIABLES
      PRINT      1      PRINT CONTROL
      PLOT      0      PLOT CONTROL
      OSCAL      0      HYDROGRAPH PLOT SCALE
      ASLO PARCEL EAST OF SCOTTSDALE ROAD

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SUBBASIN RUNOFF DATA

```

672 BA      SUBBASIN CHARACTERISTICS
      TAREA      05      SUBBASIN AREA

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PRECIPITATION DATA

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24 PH      DEPTHS FOR 0 PERCENT HYPOTHETICAL STORM
      HYDRO-15      TP-40
      5-MIN 15-MIN 60-MIN 2-HR 3-HR 6-HR 12-HR 24-HR 3-DAY 7-DAY 10-DAY
      76 1.50 2.55 2.83 2.88 3.33 00 00 00 00 00
      STORM AREA = 11 00

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674 LS      SOIL LOSS RATE
      STRPL      60      INITIAL ABSTRACTION
      CURVNR      11.00      CURVE NUMBER
      RFRMP      00      PERCENT IMPERVIOUS AREA

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675 UX      KINEMATIC WAVE
      OVERLAND FLOW ELEMENT NO 1
      L      60      OVERLAND FLOW LENGTH
      S      0211      SLOPE
      N      .100      ROUGHNESS COEFFICIENT
      PA      100.0      PERCENT OF SUBBASIN
      DYNIN      5      MINIMUM NUMBER OF DX INTERVALS

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676 RK      KINEMATIC WAVE
      RATH CHANNEL
      L      2100      CHANNEL LENGTH
      S      0088      SLOPE
      N      050      CHANNEL ROUGHNESS COEFFICIENT
      CA      05      CONTRIBUTING AREA
      SHAPE      TRAP      CHANNEL SHAPE
      SD      12 00      BOTTOM WIDTH OR DIAMETER
      Z      5 00      SIDE SLOPE
      RDXMIN      2      MINIMUM NUMBER OF DX INTERVALS
      RUPSTQ      NO      ROUTE UPSTREAM HYDROGRAPH

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COMPUTED KINEMATIC PARAMETERS  
VARIABLE TIME STEP  
(IF SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT (MIN)	DX (FT)	PEAK (CFS)	TIME TO PEAK (MIN)	VOLUME (IN)	MAXIMUM Celerity (FPS)
PLANE1	2 17	1 67	35	17 80	123.41	105 05	1 23	19
MAIN	33	1 43	1 70	525 00	91 71	190 76	1 22	5 16

CONTINUITY SUMMARY (AC-FT) : INFLOW= 0009+00 EXCESS= 3491E+01 OUTFLOW= 3478E+01 BASIN STORAGE= 2007E+01 PERCENT ERROR= 4

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

MAIN	98	1 13	5 00	39 79	190 00	1 71
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HYDROGRAPH AT STATION ASLO

DA	MON	HR	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HR	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	00	00	00	0	*	1	1230	151	00	00	00	0	*
1	0005	2	01	01	00	0	*	1	1235	152	00	00	00	0	*
1	0010	3	01	01	00	0	*	1	1240	151	00	00	00	0	*
1	0015	4	01	01	00	0	*	1	1245	151	00	00	00	0	*
1	0020	5	01	01	00	0	*	1	1250	155	00	00	00	0	*

1	6025	6	01	01	00	0	*	1	1255	156	00	00	00	0
1	6030	7	01	01	00	0	*	1	1300	157	00	00	00	0
1	6035	8	01	01	00	0	*	1	1305	158	00	00	00	0
1	6040	9	01	01	00	0	*	1	1110	159	00	00	00	0
1	6045	10	01	01	00	0	*	1	1315	160	00	00	00	0
1	6050	11	01	01	00	0	*	1	1320	161	00	00	00	0
1	6055	12	01	01	00	0	*	1	1325	162	00	00	00	0
1	6100	13	01	01	00	0	*	1	1330	163	00	00	00	0
1	6105	14	01	01	00	0	*	1	1335	164	00	00	00	0
1	6110	15	01	01	00	0	*	1	1340	165	00	00	00	0
1	6115	16	01	01	00	0	*	1	1345	166	00	00	00	0
1	6120	17	01	01	00	0	*	1	1350	167	00	00	00	0
1	6125	18	01	01	00	0	*	1	1355	168	00	00	00	0
1	6130	19	01	01	00	0	*	1	1400	169	00	00	00	0
1	6135	20	01	01	00	0	*	1	1405	170	00	00	00	0
1	6140	21	01	01	00	0	*	1	1410	171	00	00	00	0
1	6145	22	02	02	00	0	*	1	1415	172	00	00	00	0
1	6150	23	02	02	00	0	*	1	1420	173	00	00	00	0
1	6155	24	02	02	00	0	*	1	1425	174	00	00	00	0
1	6200	25	02	02	00	0	*	1	1430	175	00	00	00	0
1	6205	26	02	02	00	0	*	1	1435	176	00	00	00	0
1	6210	27	02	02	00	0	*	1	1440	177	00	00	00	0
1	6215	28	02	02	00	0	*	1	1445	178	00	00	00	0
1	6220	29	02	02	00	0	*	1	1450	179	00	00	00	0
1	6225	30	03	03	00	0	*	1	1455	180	00	00	00	0
1	6230	31	03	03	00	0	*	1	1500	181	00	00	00	0
1	6235	32	08	08	00	0	*	1	1505	182	00	00	00	0
1	6240	33	09	09	00	0	*	1	1510	183	00	00	00	0
1	6245	34	10	10	00	0	*	1	1515	184	00	00	00	0
1	6250	35	11	11	01	0	*	1	1520	185	00	00	00	0
1	6255	36	12	12	01	0	*	1	1525	186	00	00	00	0
1	6300	37	10	28	12	5	*	1	1530	187	00	00	00	0
1	6305	38	09	16	11	17	*	1	1535	188	00	00	00	0
1	6310	39	08	16	10	20	*	1	1540	189	00	00	00	0
1	6315	40	15	06	09	69	*	1	1545	190	00	00	00	0
1	6320	41	11	01	07	17	*	1	1550	191	00	00	00	0
1	6325	42	09	01	06	15	*	1	1555	192	00	00	00	0
1	6330	43	08	01	05	29	*	1	1600	193	00	00	00	0
1	6335	44	03	01	02	23	*	1	1605	194	00	00	00	0
1	6340	45	02	01	02	10	*	1	1610	195	00	00	00	0
1	6345	46	01	01	02	13	*	1	1615	196	00	00	00	0
1	6350	47	02	01	02	11	*	1	1620	197	00	00	00	0
1	6355	48	02	01	01	9	*	1	1625	198	00	00	00	0
1	6400	49	02	01	01	0	*	1	1630	199	00	00	00	0
1	6405	50	02	01	01	7	*	1	1635	200	00	00	00	0
1	6410	51	02	01	01	6	*	1	1640	201	00	00	00	0
1	6415	52	02	01	01	5	*	1	1645	202	00	00	00	0
1	6420	53	02	00	01	5	*	1	1650	203	00	00	00	0
1	6425	54	02	00	01	4	*	1	1655	204	00	00	00	0
1	6430	55	01	00	01	3	*	1	1700	205	00	00	00	0
1	6435	56	01	00	01	2	*	1	1705	206	00	00	00	0
1	6440	57	01	00	01	4	*	1	1710	207	00	00	00	0
1	6445	58	01	00	01	1	*	1	1715	208	00	00	00	0
1	6450	59	01	00	01	2	*	1	1720	209	00	00	00	0
1	6455	60	01	00	01	3	*	1	1725	210	00	00	00	0
1	6500	61	01	00	01	4	*	1	1730	211	00	00	00	0
1	6505	62	01	00	01	4	*	1	1735	212	00	00	00	0
1	6510	63	01	00	01	3	*	1	1740	213	00	00	00	0
1	6515	64	01	00	01	3	*	1	1745	214	00	00	00	0
1	6520	65	01	00	01	1	*	1	1750	215	00	00	00	0
1	6525	66	01	00	01	1	*	1	1755	216	00	00	00	0
1	6530	67	01	00	01	2	*	1	1800	217	00	00	00	0
1	6535	68	01	00	01	3	*	1	1805	218	00	00	00	0
1	6540	69	01	00	01	3	*	1	1810	219	00	00	00	0
1	6545	70	01	00	01	2	*	1	1815	220	00	00	00	0
1	6550	71	01	00	01	1	*	1	1820	221	00	00	00	0
1	6555	72	01	00	01	1	*	1	1825	222	00	00	00	0
1	6600	73	01	00	01	3	*	1	1830	223	00	00	00	0
1	6605	74	00	00	00	2	*	1	1835	224	00	00	00	0
1	6610	75	00	00	00	2	*	1	1840	225	00	00	00	0
1	6615	76	00	00	00	2	*	1	1845	226	00	00	00	0
1	6620	77	00	00	00	2	*	1	1850	227	00	00	00	0
1	6625	78	00	00	00	1	*	1	1855	228	00	00	00	0
1	6630	79	00	00	00	1	*	1	1900	229	00	00	00	0
1	6635	80	00	00	00	1	*	1	1905	230	00	00	00	0
1	6640	81	00	00	00	1	*	1	1910	231	00	00	00	0
1	6645	82	00	00	00	1	*	1	1915	232	00	00	00	0
1	6650	83	00	00	00	0	*	1	1920	233	00	00	00	0
1	6655	84	00	00	00	0	*	1	1925	234	00	00	00	0
1	6700	85	00	00	00	0	*	1	1930	235	00	00	00	0
1	6705	86	00	00	00	0	*	1	1935	236	00	00	00	0
1	6710	87	00	00	00	0	*	1	1940	237	00	00	00	0
1	6715	88	00	00	00	0	*	1	1945	238	00	00	00	0
1	6720	89	00	00	00	0	*	1	1950	239	00	00	00	0
1	6725	90	00	00	00	0	*	1	1955	240	00	00	00	0
1	6730	91	00	00	00	0	*	1	2000	241	00	00	00	0
1	6735	92	00	00	00	0	*	1	2005	242	00	00	00	0
1	6740	93	00	00	00	0	*	1	2010	243	00	00	00	0
1	6745	94	00	00	00	0	*	1	2015	244	00	00	00	0
1	6750	95	00	00	00	0	*	1	2020	245	00	00	00	0
1	6755	96	00	00	00	0	*	1	2025	246	00	00	00	0
1	6800	97	00	00	00	0	*	1	2030	247	00	00	00	0
1	6805	98	00	00	00	0	*	1	2035	248	00	00	00	0
1	6810	99	00	00	00	0	*	1	2040	249	00	00	00	0
1	6815	100	00	00	00	0	*	1	2045	250	00	00	00	0
1	6820	101	00	00	00	0	*	1	2050	251	00	00	00	0
1	6825	102	00	00	00	0	*	1	2055	252	00	00	00	0
1	6830	103	00	00	00	0	*	1	2100	253	00	00	00	0
1	6835	104	00	00	00	0	*	1	2105	254	00	00	00	0
1	6840	105	00	00	00	0	*	1	2110	255	00	00	00	0
1	6845	106	00	00	00	0	*	1	2115	256	00	00	00	0
1	6850	107	00	00	00	0	*	1	2120	257	00	00	00	0
1	6855	108	00	00	00	0	*	1	2125	258	00	00	00	0
1	6900	109	00	00	00	0	*	1	2130	259	00	00	00	0



1	0925	110	00	00	.00	0	*	1	2115	260	.00	.00	00	0
1	0910	111	00	00	00	0	*	1	2140	261	00	00	00	0
1	0915	112	00	00	00	0	*	1	2145	262	00	.00	00	0
1	0920	113	00	00	00	0	*	1	2150	263	00	00	.00	0
1	0925	114	.00	00	.00	0	*	1	2155	264	00	00	.00	0
1	0930	115	00	.00	.00	0	*	1	2200	265	00	00	00	0
1	0935	116	00	00	00	0	*	1	2205	266	00	00	00	0
1	0940	117	00	00	.00	0	*	1	2210	267	00	00	.00	0
1	0945	118	00	00	00	0	*	1	2215	268	.00	00	00	0
1	0950	119	00	00	00	0	*	1	2220	269	00	00	00	0
1	0955	120	00	.00	.00	0	*	1	2225	270	00	00	00	0
1	1000	121	00	00	.00	0	*	1	2230	271	00	.00	.00	0
1	1005	122	00	00	00	0	*	1	2235	272	00	.00	.00	0
1	1010	123	00	00	00	0	*	1	2240	273	00	00	.00	0
1	1015	124	00	00	00	0	*	1	2245	274	00	00	00	0
1	1020	125	.00	00	.00	0	*	1	2250	275	00	00	.00	0
1	1025	126	00	00	00	0	*	1	2255	276	00	00	00	0
1	1030	127	00	.00	.00	0	*	1	2300	277	00	00	00	0
1	1035	128	00	00	00	0	*	1	2305	278	00	00	00	0
1	1040	129	00	00	00	0	*	1	2310	279	00	.00	00	0
1	1045	130	00	00	00	0	*	1	2315	280	00	00	00	0
1	1050	131	00	00	00	0	*	1	2320	281	00	00	00	0
1	1055	132	00	.00	.00	0	*	1	2325	282	.00	.00	.00	0
1	1100	133	00	00	00	0	*	1	2330	283	00	00	.00	0
1	1105	134	.00	00	.00	0	*	1	2335	284	00	00	00	0
1	1110	135	00	00	00	0	*	1	2340	285	.00	00	00	0
1	1115	136	00	00	00	0	*	1	2345	286	00	.00	00	0
1	1120	137	00	00	.00	0	*	1	2350	287	00	00	00	0
1	1125	138	00	00	00	0	*	1	2355	288	00	00	00	0
1	1130	139	00	00	.00	0	*	2	0000	289	00	00	00	0
1	1135	140	00	00	00	0	*	2	0005	290	00	00	.00	0
1	1140	141	00	00	00	0	*	2	0010	291	00	00	.00	0
1	1145	142	00	.00	00	0	*	2	0015	292	00	00	00	0
1	1150	143	00	00	00	0	*	2	0020	293	00	00	00	0
1	1155	144	.00	00	.00	0	*	2	0025	294	00	00	.00	0
1	1200	145	00	00	.00	0	*	2	0030	295	00	00	00	0
1	1205	146	00	00	00	0	*	2	0035	296	00	00	00	0
1	1210	147	00	.00	00	0	*	2	0040	297	00	00	.00	0
1	1215	148	00	00	00	0	*	2	0045	298	00	00	00	0
1	1220	149	00	.00	00	0	*	2	0050	299	00	00	00	0
1	1225	150	00	.00	00	0	*	2	0055	300	00	00	00	0

TOTAL RAINFALL = 1.22, TOTAL LOSS = 1.99, TOTAL EXCESS = 1.23

PEAK FLOW TIME  
 (CFS) (HR)  
 90 3.17  
 (INCHES) 1.224  
 (AC-FY) 3  
 CUMULATIVE AREA = 05.80 MI

677 KK CRRIN COMBINE

678 RD OUTPUT CONTROL VARIABLES  
 1 PRINT CONTROL  
 0 PLOT CONTROL  
 0 HYDROGRAPH PLOT SCALE  
 COMBINE ROUTED ABOUT 5 AND 5 WITH ASLD PARCU

680 HC HYDROGRAPH COMBINATION  
 1 COMB 2 NUMBER OF HYDROGRAPHS TO COMBINE

# HYDROGRAPH AT STATION CRRIN SUM OF 2 HYDROGRAPHS

DA	MON	HRSN	ORD	FLOW	DA	MON	HRSN	ORD	FLOW	DA	MON	HRSN	ORD	FLOW	DA	MON	HRSN	ORD	FLOW
1		0000	1	0	1		0615	26	31	1		1210	151	6	1		1845	296	1
1		0005	2	0	1		0620	37	68	1		1215	152	6	1		1850	297	1
1		0010	3	0	1		0625	48	64	1		1240	153	6	1		1855	298	1
1		0015	4	0	1		0630	59	61	1		1245	154	6	1		1900	299	1
1		0020	5	0	1		0635	60	57	1		1250	155	5	1		1905	300	1
1		0025	6	0	1		0640	81	55	1		1255	156	5	1		1910	301	1
1		0030	7	0	1		0645	92	52	1		1300	157	5	1		1915	302	1
1		0035	8	0	1		0650	93	50	1		1305	158	5	1		1920	303	1
1		0040	9	0	1		0655	84	47	1		1310	159	5	1		1925	304	1
1		0045	10	0	1		0700	85	45	1		1315	160	5	1		1930	305	1
1		0050	11	0	1		0705	86	43	1		1320	161	5	1		1935	306	1
1		0055	12	0	1		0710	87	41	1		1325	162	5	1		1940	307	1
1		0100	13	1	1		0715	88	40	1		1330	163	4	1		1945	308	1
1		0105	14	2	1		0720	89	38	1		1335	164	4	1		1950	309	1
1		0110	15	3	1		0725	90	37	1		1340	165	4	1		1955	310	1
1		0115	16	5	1		0730	91	35	1		1345	166	3	1		2000	311	1

1	0120	17	6	*	1	0715	92	31	*	1	1350	167	4	*	1	2005	212	1.
1	0125	18	7	*	1	0710	93	33	*	1	1355	168	4	*	1	2010	243	1.
1	0130	19	8	*	1	0745	94	37	*	1	1400	169	4	*	1	2015	244	1.
1	0135	20	9	*	1	0750	95	36	*	1	1405	170	1	*	1	2020	245	1.
1	0140	21	10	*	1	0755	96	29	*	1	1410	171	9	*	1	2025	246	1.
1	0145	22	10	*	1	0800	97	28	*	1	1415	172	4	*	1	2030	247	1.
1	0150	23	11	*	1	0805	98	37	*	1	1420	173	1	*	1	2035	248	1.
1	0155	24	12	*	1	0810	99	26	*	1	1425	174	3	*	1	2040	249	1.
1	0200	25	13	*	1	0815	100	26	*	1	1430	175	3	*	1	2045	250	1.
1	0205	26	14	*	1	0820	101	25	*	1	1435	176	3	*	1	2050	251	1.
1	0210	27	15	*	1	0825	102	34	*	1	1440	177	3	*	1	2055	252	1.
1	0215	28	16	*	1	0830	103	23	*	1	1445	178	3	*	1	2100	253	1.
1	0220	29	17	*	1	0835	104	22	*	1	1450	179	3	*	1	2105	254	1.
1	0225	30	18	*	1	0840	105	22	*	1	1455	180	5	*	1	2110	255	1.
1	0230	31	19	*	1	0845	106	21	*	1	1500	181	3	*	1	2115	256	1.
1	0235	32	21	*	1	0850	107	20	*	1	1505	182	1	*	1	2120	257	1.
1	0240	33	22	*	1	0855	108	20	*	1	1510	183	3	*	1	2125	258	1.
1	0245	34	26	*	1	0900	109	19	*	1	1515	184	3	*	1	2130	259	1.
1	0250	35	33	*	1	0905	110	19	*	1	1520	185	1	*	1	2135	260	1.
1	0255	36	45	*	1	0910	111	10	*	1	1525	186	3	*	1	2140	261	1.
1	0300	37	65	*	1	0915	112	11	*	1	1530	187	3	*	1	2145	262	1.
1	0305	38	130	*	1	0920	113	17	*	1	1535	188	3	*	1	2150	263	1.
1	0310	39	256	*	1	0925	114	16	*	1	1540	189	4	*	1	2155	264	1.
1	0315	40	300	*	1	0930	115	16	*	1	1545	190	2	*	1	2200	265	1.
1	0320	41	299	*	1	0935	116	15	*	1	1550	191	2	*	1	2205	266	1.
1	0325	42	207	*	1	0940	117	15	*	1	1555	192	2	*	1	2210	267	0.
1	0330	43	272	*	1	0945	118	15	*	1	1600	193	2	*	1	2215	268	0.
1	0335	44	257	*	1	0950	119	14	*	1	1605	194	2	*	1	2220	269	0.
1	0340	45	249	*	1	0955	120	14	*	1	1610	195	2	*	1	2225	270	0.
1	0345	46	221	*	1	1000	121	13	*	1	1615	196	2	*	1	2230	271	0.
1	0350	47	202	*	1	1005	122	13	*	1	1620	197	2	*	1	2235	272	0.
1	0355	48	186	*	1	1010	123	11	*	1	1625	198	2	*	1	2240	273	0.
1	0400	49	173	*	1	1015	124	12	*	1	1630	199	2	*	1	2245	274	0.
1	0405	50	163	*	1	1020	125	12	*	1	1635	200	3	*	1	2250	275	0.
1	0410	51	155	*	1	1025	126	12	*	1	1640	201	2	*	1	2255	276	0.
1	0415	52	140	*	1	1030	127	11	*	1	1645	202	2	*	1	2300	277	0.
1	0420	53	132	*	1	1035	128	11	*	1	1650	203	2	*	1	2305	278	0.
1	0425	54	137	*	1	1040	129	11	*	1	1655	204	2	*	1	2310	279	0.
1	0430	55	133	*	1	1045	130	10	*	1	1700	205	2	*	1	2315	280	0.
1	0435	56	123	*	1	1050	131	10	*	1	1705	206	2	*	1	2320	281	0.
1	0440	57	125	*	1	1055	132	10	*	1	1710	207	2	*	1	2325	282	0.
1	0445	58	122	*	1	1100	133	10	*	1	1715	208	2	*	1	2330	283	0.
1	0450	59	119	*	1	1105	134	9	*	1	1720	209	2	*	1	2335	284	0.
1	0455	60	116	*	1	1110	135	9	*	1	1725	210	2	*	1	2340	285	0.
1	0500	61	112	*	1	1115	136	9	*	1	1730	211	2	*	1	2345	286	0.
1	0505	62	108	*	1	1120	137	9	*	1	1735	212	3	*	1	2350	287	0.
1	0510	63	105	*	1	1125	138	8	*	1	1740	213	1	*	1	2355	288	0.
1	0515	64	102	*	1	1130	139	8	*	1	1745	214	1	*	1	0000	289	0.
1	0520	65	99	*	1	1135	140	8	*	1	1750	215	1	*	2	0005	290	0.
1	0525	66	96	*	1	1140	141	8	*	1	1755	216	1	*	2	0010	291	0.
1	0530	67	93	*	1	1145	142	8	*	1	1800	217	1	*	2	0015	292	0.
1	0535	68	90	*	1	1150	143	7	*	1	1805	218	1	*	2	0020	293	0.
1	0540	69	87	*	1	1155	144	7	*	1	1810	219	1	*	2	0025	294	0.
1	0545	70	85	*	1	1200	145	7	*	1	1815	220	1	*	2	0030	295	0.
1	0550	71	83	*	1	1205	146	7	*	1	1820	221	1	*	2	0035	296	0.
1	0555	72	80	*	1	1210	147	7	*	1	1825	222	1	*	2	0040	297	0.
1	0600	73	78	*	1	1215	148	6	*	1	1830	223	1	*	2	0045	298	0.
1	0605	74	76	*	1	1220	149	6	*	1	1835	224	1	*	2	0050	299	0.
1	0610	75	74	*	1	1225	150	6	*	1	1840	225	1	*	2	0055	300	0.

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PEAK FLOW	TIME	6-HR	24-HR	72-HR	24-92-HR
(CFS)	(HR)				
300	3 25	90	20	27	27
		(INCHES)	1.61	1.85	1.85
		(AC-FT)	40.	56	56
CUMULATIVE AREA =		56 SQ MI			

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 601 KK R11C 2  
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687 KD OUTPUT CONTROL VARIABLES  
 IPRT 1 PRINT CONTROL  
 IPLOT 0 PLOT CONTROL  
 QSCALE 0 HYDROGRAPH PLOT SCALE  
 RETRIEVE DIVERTED PIPE FLOW

681 DR RETRIEVE DIVERSION HYDROGRAPH  
 ISCAL 2 DIVERSION HYDROGRAPH IDENTIFICATION

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 HYDROGRAPH AT STATION R11C 2  
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DA	MON	HR	MIN	SEC	FLOW	DA	MON	HR	MIN	SEC	FLOW	DA	MON	HR	MIN	SEC	FLOW	
1	0000	1	0	*	1	0615	26	9	*	1	1210	151	0	*	1	1845	225	0

PRINT	1	PRINT CONTROL
PLOT	0	PLOT CONTROL
OSCAL	0	HYDROGRAPH PLOT SCALE
SUM EAST OF SCOTTSDALE RD. FLOWING DIRECTLY INTO SCOTTSDALE SO		

CULVERT, TAKES SCOTTS RD HALF ST AND SCENIC CORRIDOR

SUBBASIN RUNOFF DATA

689 BA SUBBASIN CHARACTERISTICS  
TARPA 01 SUBBASIN AREA

PRECIPITATION DATA

24 PH DEPTH FOR 0-PERCENT HYPOTHETICAL STORM  
HYDRO-35 TP-40  
5-MIN 15-MIN 60-MIN 2 HR 3 HR 6 HR 12 HR 24 HR 2-DAY 4-DAY 7-DAY 10-DAY  
76 1 50 2 51 2 81 7 99 3 33 00 00 00 00 00 00

STORM AREA = 14.00

690 LY SCS LOSS RATE  
STPPL 60 INITIAL ABSTRACTION  
CVRBR 17.00 CURVE NUMBER  
PTIMP 69.00 PERCENT IMPERVIOUS AREA

691 UE KINEMATIC WAVE  
OVERLAND-FLOW ELEMENT NO. 1  
L 50 OVERLAND FLOW LENGTH  
S 0100 SLOPE  
N 050 ROUGHNESS COEFFICIENT  
PA 100.0 PERCENT OF SUBBASIN  
DYNIN 5 MINIMUM NUMBER OF DX INTERVALS

692 KE KINEMATIC WAVE  
MAIN CHANNEL  
L 500 CHANNEL LENGTH  
S 0100 SLOPE  
N 015 CHANNEL ROUGHNESS COEFFICIENT  
CA .01 CONFINING AREA  
SHAPE CIRC CHANNEL SHAPE  
WD 4.50 BOTTOM WIDTH OR DIAMETER  
Z 00 SIDE SLOPE  
DYNIN 5 MINIMUM NUMBER OF DX INTERVALS  
RUPSTO NO ROUTE OUTSTREAM HYDROGRAPH

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COMPUTED KINEMATIC PARAMETERS  
VARIABLE TIME STEP  
(OT SHOWN IS A MINIMUM)

ELEMENT	ALPHA	M	DT	DX	PEAK	TIME TO PEAK	VOLUME	MAXIMUM CELERITY
			(MIN)	(FT)	(CFS)	(MIN)	(CU)	(FPS)
OVERLND	2.98	1.67	12	10.06	11.73	184.81	1.00	54
MAIN	5.45	1.75	33	700.00	11.72	164.75	2.09	17.50

CONTINUITY SUMMARY (AC-FT) : INFLOW: 0000E+00 EXCESS: 1009E+01 OUTFLOW: 1009E+01 PAVN STORAGE: 4154E+05 PERCENT ERROR: 1

INTERPOLATED TO SPECIFIED COMPUTATION INTERVAL

RAIN 6.39 1.75 5.00 11.67 151.00 3.01

HYDROGRAPH AT STATION SCOUT

DA	MON	HRS	ORD	RAIN	LOSS	EXCESS	COMP Q	DA	MON	HRS	ORD	RAIN	LOSS	EXCESS	COMP Q
1	0000	1	00	00	00	00	0	1	1230	151	00	00	00	00	0
1	0005	2	01	00	01	0	0	1	1235	152	00	00	00	00	0
1	0010	3	01	00	01	0	0	1	1240	153	00	00	00	00	0
1	0015	4	01	00	01	0	0	1	1245	154	00	00	00	00	0
1	0020	5	01	00	01	0	0	1	1250	155	00	00	00	00	0
1	0025	6	01	00	01	0	0	1	1255	156	00	00	00	00	0
1	0030	7	01	00	01	0	0	1	1300	157	00	00	00	00	0
1	0035	8	01	00	01	0	0	1	1305	158	00	00	00	00	0
1	0040	9	01	00	01	0	0	1	1310	159	00	00	00	00	0
1	0045	10	01	00	01	0	0	1	1315	160	00	00	00	00	0
1	0050	11	01	00	01	0	0	1	1320	161	00	00	00	00	0
1	0055	12	01	00	01	0	0	1	1325	162	00	00	00	00	0
1	0100	13	01	00	01	0	0	1	1330	163	00	00	00	00	0
1	0105	14	01	00	01	0	0	1	1335	164	00	00	00	00	0
1	0110	15	01	00	01	0	0	1	1340	165	00	00	00	00	0
1	0115	16	01	00	01	0	0	1	1345	166	00	00	00	00	0
1	0120	17	01	00	01	0	0	1	1350	167	00	00	00	00	0
1	0125	18	01	00	01	0	0	1	1355	168	00	00	00	00	0
1	0130	19	01	00	01	0	0	1	1400	169	00	00	00	00	0
1	0135	20	01	00	01	0	0	1	1405	170	00	00	00	00	0
1	0140	21	01	00	01	0	0	1	1410	171	00	00	00	00	0
1	0145	22	02	00	01	0	0	1	1415	172	00	00	00	00	0
1	0150	23	02	00	01	0	0	1	1420	173	00	00	00	00	0
1	0155	24	02	00	02	0	0	1	1425	174	00	00	00	00	0
1	0200	25	02	00	02	0	0	1	1430	175	00	00	00	00	0
1	0205	26	02	00	02	0	0	1	1435	176	00	00	00	00	0
1	0210	27	02	00	02	0	0	1	1440	177	00	00	00	00	0
1	0215	28	02	00	02	0	0	1	1445	178	00	00	00	00	0
1	0220	29	02	00	02	0	0	1	1450	179	00	00	00	00	0
1	0225	30	01	00	02	0	0	1	1455	180	00	00	00	00	0
1	0230	31	01	00	02	0	0	1	1500	181	00	00	00	00	0
1	0235	32	06	01	07	0	0	1	1505	182	00	00	00	00	0
1	0240	33	07	01	08	0	0	1	1510	183	00	00	00	00	0
1	0245	34	10	01	09	0	0	1	1515	184	00	00	00	00	0

1	0250	35	.14	01	12	6	*	1	1520	105	00	00	00	0.
1	0255	36	.18	02	16	8.	*	1	1525	106	00	00	.00	0.
1	0300	37	.40	03	27	18.	*	1	1530	107	00	00	00	0
1	0305	38	.49	04	45	21.	*	1	1535	108	00	.00	00	0.
1	0310	39	.28	.01	26	13.	*	1	1540	109	00	00	00	0.
1	0315	40	.15	01	15	7	*	1	1545	110	00	.00	.00	0.
1	0320	41	.17	.00	10	5.	*	1	1550	111	.00	00	00	0
1	0325	42	.09	.00	09	4	*	1	1555	112	00	.00	.00	0.
1	0330	43	.08	00	08	4.	*	1	1600	113	00	00	.00	0
1	0335	44	.03	00	03	2	*	1	1605	114	00	00	.00	0
1	0340	45	.03	00	03	1	*	1	1610	115	00	00	.00	0
1	0345	46	.03	00	03	1.	*	1	1615	116	00	00	.00	0.
1	0350	47	.02	.00	02	1	*	1	1620	117	00	00	.00	0
1	0355	48	.02	.00	02	1	*	1	1625	118	00	00	.00	0
1	0400	49	.02	00	02	1	*	1	1630	119	.00	00	.00	0
1	0405	50	.02	.00	02	1	*	1	1635	120	00	00	.00	0
1	0410	51	.02	.00	02	1	*	1	1640	121	00	00	.00	0.
1	0415	52	.02	.00	02	1	*	1	1645	122	00	00	.00	0
1	0420	53	.03	.00	02	1.	*	1	1650	123	00	.00	.00	0.
1	0425	54	.02	.00	01	1	*	1	1655	124	.00	00	.00	0.
1	0430	55	.01	.00	01	1	*	1	1700	125	00	00	.00	0
1	0435	56	.01	.00	01	1	*	1	1705	126	00	00	.00	0
1	0440	57	.01	.00	01	1	*	1	1710	127	00	.00	.00	0
1	0445	58	.01	.00	01	1	*	1	1715	128	.00	.00	.00	0
1	0450	59	.01	.00	01	1	*	1	1720	129	00	00	.00	0
1	0455	60	.01	.00	01	1	*	1	1725	130	00	00	.00	0
1	0500	61	.01	.00	01	1	*	1	1730	131	00	00	.00	0
1	0505	62	.01	.00	01	1	*	1	1735	132	00	00	.00	0
1	0510	63	.01	.00	01	0	*	1	1740	133	00	00	.00	0
1	0515	64	.01	.00	01	0	*	1	1745	134	00	00	.00	0
1	0520	65	.01	.00	01	0	*	1	1750	135	00	00	.00	0
1	0525	66	.01	.00	01	0	*	1	1755	136	00	00	.00	0
1	0530	67	.01	.00	01	0	*	1	1800	137	00	00	.00	0
1	0535	68	.01	.00	01	0	*	1	1805	138	00	00	.00	0
1	0540	69	.01	.00	01	0	*	1	1810	139	00	00	.00	0
1	0545	70	.02	.00	02	0	*	1	1815	140	00	00	.00	0
1	0550	71	.01	.00	01	0	*	1	1820	141	00	00	.00	0
1	0555	72	.01	.00	01	0	*	1	1825	142	00	00	.00	0
1	0600	73	.01	.00	01	0	*	1	1830	143	00	.00	.00	0.
1	0605	74	.00	.00	00	0	*	1	1835	144	.00	00	.00	0
1	0610	75	.00	.00	00	0	*	1	1840	145	00	00	.00	0
1	0615	76	.00	.00	00	0	*	1	1845	146	00	00	.00	0
1	0620	77	.00	.00	00	0	*	1	1850	147	00	00	.00	0
1	0625	78	.00	.00	00	0	*	1	1855	148	00	00	.00	0
1	0630	79	.00	.00	00	0	*	1	1900	149	00	00	.00	0
1	0635	80	.00	.00	00	0	*	1	1905	150	00	00	.00	0
1	0640	81	.00	.00	00	0	*	1	1910	151	00	00	.00	0.
1	0645	82	.00	.00	00	0	*	1	1915	152	00	00	.00	0.
1	0650	83	.00	.00	00	0	*	1	1920	153	00	00	.00	0.
1	0655	84	.00	.00	00	0	*	1	1925	154	.00	.00	.00	0.
1	0700	85	.00	.00	00	0	*	1	1930	155	00	00	.00	0
1	0705	86	.00	.00	00	0	*	1	1935	156	00	00	.00	0
1	0710	87	.00	.00	00	0	*	1	1940	157	00	00	.00	0
1	0715	88	.00	.00	00	0	*	1	1945	158	00	00	.00	0
1	0720	89	.00	.00	00	0	*	1	1950	159	00	00	.00	0
1	0725	90	.00	.00	00	0	*	1	1955	160	00	00	.00	0
1	0730	91	.00	.00	00	0	*	1	2000	161	00	00	.00	0.
1	0735	92	.00	.00	00	0	*	1	2005	162	00	00	.00	0
1	0740	93	.00	.00	00	0	*	1	2010	163	00	00	.00	0
1	0745	94	.00	.00	00	0	*	1	2015	164	00	00	.00	0
1	0750	95	.00	.00	00	0	*	1	2020	165	00	00	.00	0.
1	0755	96	.00	.00	00	0	*	1	2025	166	00	00	.00	0
1	0800	97	.00	.00	00	0	*	1	2030	167	00	00	.00	0
1	0805	98	.00	.00	00	0	*	1	2035	168	00	.00	.00	0.
1	0810	99	.00	.00	00	0	*	1	2040	169	00	00	.00	0
1	0815	100	.00	.00	00	0	*	1	2045	170	00	00	.00	0
1	0820	101	.00	.00	00	0	*	1	2050	171	00	00	.00	0
1	0825	102	.00	.00	00	0	*	1	2055	172	00	00	.00	0.
1	0830	103	.00	.00	00	0	*	1	2100	173	00	00	.00	0
1	0835	104	.00	.00	00	0	*	1	2105	174	00	00	.00	0
1	0840	105	.00	.00	00	0	*	1	2110	175	00	00	.00	0
1	0845	106	.00	.00	00	0	*	1	2115	176	00	.00	.00	0.
1	0850	107	.00	.00	00	0	*	1	2120	177	00	00	.00	0
1	0855	108	.00	.00	00	0	*	1	2125	178	00	00	.00	0
1	0900	109	.00	.00	00	0	*	1	2130	179	00	00	.00	0
1	0905	110	.00	.00	00	0	*	1	2135	180	00	00	.00	0
1	0910	111	.00	.00	00	0	*	1	2140	181	00	00	.00	0
1	0915	112	.00	.00	00	0	*	1	2145	182	00	00	.00	0
1	0920	113	.00	.00	00	0	*	1	2150	183	00	00	.00	0
1	0925	114	.00	.00	00	0	*	1	2155	184	00	00	.00	0
1	0930	115	.00	.00	00	0	*	1	2200	185	00	00	.00	0
1	0935	116	.00	.00	00	0	*	1	2205	186	.00	00	.00	0.
1	0940	117	.00	.00	00	0	*	1	2210	187	00	00	.00	0
1	0945	118	.00	.00	00	0	*	1	2215	188	00	00	.00	0
1	0950	119	.00	.00	00	0	*	1	2220	189	00	00	.00	0
1	0955	120	.00	.00	00	0	*	1	2225	190	00	00	.00	0
1	1000	121	.00	.00	00	0	*	1	2230	191	00	00	.00	0
1	1005	122	.00	.00	00	0	*	1	2235	192	00	00	.00	0
1	1010	123	.00	.00	00	0	*	1	2240	193	00	00	.00	0
1	1015	124	.00	.00	00	0	*	1	2245	194	00	00	.00	0
1	1020	125	.00	.00	00	0	*	1	2250	195	00	00	.00	0
1	1025	126	.00	.00	00	0	*	1	2255	196	00	00	.00	0
1	1030	127	.00	.00	00	0	*	1	2300	197	00	00	.00	0
1	1035	128	.00	.00	00	0	*	1	2305	198	00	00	.00	0
1	1040	129	.00	.00	00	0	*	1	2310	199	00	00	.00	0
1	1045	130	.00	.00	00	0	*	1	2315	200	00	00	.00	0
1	1050	131	.00	.00	00	0	*	1	2320	201	00	00	.00	0
1	1055	132	.00	.00	00	0	*	1	2325	202	00	00	.00	0
1	1100	133	.00	.00	00	0	*	1	2330	203	00	00	.00	0
1	1105	134	.00	.00	00	0	*	1	2335	204	00	00	.00	0
1	1110	135	.00	.00	00	0	*	1	2340	205	00	00	.00	0
1	1115	136	.00	.00	00	0	*	1	2345	206	00	00	.00	0
1	1120	137	.00	.00	00	0	*	1	2350	207	.00	00	.00	0
1	1125	138	.00	.00	00	0	*	1	2355	208	00	00	.00	0

1	1110	139	.90	00	.00	0	*	2	0000	289	00	.00	.00	0
1	1135	140	.90	.00	.00	0	*	2	0005	290	.00	00	00	0
1	1140	141	.90	.00	.00	0	*	2	0010	291	.00	00	.00	0
1	1145	142	.90	.00	.00	0	*	2	0015	292	.00	00	.00	0
1	1150	143	.90	.00	.00	0	*	2	0020	293	.00	00	00	0
1	1155	144	.90	.00	.00	0	*	2	0025	294	.00	00	00	0
1	1200	145	.90	.00	.00	0	*	2	0030	295	.00	00	00	0
1	1205	146	.90	.00	.00	0	*	2	0035	296	.00	00	00	0
1	1210	147	.90	.00	.00	0	*	2	0040	297	.00	.00	00	0
1	1215	148	.90	.00	.00	0	*	2	0045	298	.00	.00	00	0
1	1220	149	.90	.00	.00	0	*	2	0050	299	.00	.00	00	0
1	1225	150	.90	.00	.00	0	*	2	0055	300	.00	.00	.00	0

TOTAL RAINFALL = 3.22, TOTAL LOSS = 32, TOTAL EXCESS = 3.00

PEAK FLOW TIME MAXIMUM AVERAGE FLOW  
(CFS) (HR) 6-HR 24-HR 72-HR 24 92-HR  
21. 3.08  
(INCHES) 2. 1. 0 0.  
(AC-FT) 3.004 3.013 3.013 3.013  
CUMULATIVE AREA = .01 SQ MI

693 KK 111 2 COMBINE

694 KO OUTPUT CONTROL VARIABLES  
IDPRNT 1 PRINT CONTROL  
IDPLOT 0 PLOT CONTROL  
QSCALE 0 HYDROGRAPH PLOT SCALE  
COMBINED DISCHARGE AT SCOTTSDALE ROAD CULVERT

695 UC HYDROGRAPH COMBINATION  
NCGRP 2 NUMBER OF HYDROGRAPHS TO COMBINE

HYDROGRAPH AT STATION 111 2  
SUM OF 2 HYDROGRAPHS

DA	MON	HRMM	ORD	FLOW	DA	MON	HRMM	ORD	FLOW	DA	MON	HRMM	ORD	FLOW	DA	MON	HRMM	ORD	FLOW
1	0000	1	0	*	1	0615	75	9	*	1	1230	151	0	*	1	1045	226	0	
1	0005	2	0	*	1	0620	77	8	*	1	1235	152	0	*	1	1050	227	0	
1	0010	3	0	*	1	0625	78	7	*	1	1240	153	0	*	1	1055	228	0	
1	0015	4	0	*	1	0630	79	6	*	1	1245	154	0	*	1	1000	229	0	
1	0020	5	0	*	1	0635	80	5	*	1	1250	155	0	*	1	1005	230	0	
1	0025	6	0	*	1	0640	81	5	*	1	1255	156	0	*	1	1010	231	0	
1	0030	7	0	*	1	0645	82	4	*	1	1300	157	0	*	1	1015	232	0	
1	0035	8	0	*	1	0650	83	1	*	1	1305	158	0	*	1	1020	233	0	
1	0040	9	0	*	1	0655	84	1	*	1	1310	159	0	*	1	1025	234	0	
1	0045	10	0	*	1	0700	85	3	*	1	1315	160	0	*	1	1030	235	0	
1	0050	11	0	*	1	0705	86	2	*	1	1320	161	0	*	1	1035	236	0	
1	0055	12	0	*	1	0710	87	2	*	1	1325	162	0	*	1	1040	237	0	
1	0100	13	1	*	1	0715	88	2	*	1	1330	163	0	*	1	1045	238	0	
1	0105	14	1	*	1	0720	89	2	*	1	1335	164	0	*	1	1050	239	0	
1	0110	15	2	*	1	0725	90	1	*	1	1340	165	0	*	1	1055	240	0	
1	0115	16	2	*	1	0730	91	1	*	1	1345	166	0	*	1	1000	241	0	
1	0120	17	2	*	1	0735	92	1	*	1	1350	167	0	*	1	1005	242	0	
1	0125	18	3	*	1	0740	93	1	*	1	1355	168	0	*	1	1010	243	0	
1	0130	19	3	*	1	0745	94	1	*	1	1400	169	0	*	1	1015	244	0	
1	0135	20	3	*	1	0750	95	1	*	1	1405	170	0	*	1	1020	245	0	
1	0140	21	3	*	1	0755	96	1	*	1	1410	171	0	*	1	1025	246	0	
1	0145	22	4	*	1	0800	97	1	*	1	1415	172	0	*	1	1030	247	0	
1	0150	23	4	*	1	0805	98	1	*	1	1420	173	0	*	1	1035	248	0	
1	0155	24	4	*	1	0810	99	0	*	1	1425	174	0	*	1	1040	249	0	
1	0200	25	5	*	1	0815	100	0	*	1	1430	175	0	*	1	1045	250	0	
1	0205	26	5	*	1	0820	101	0	*	1	1435	176	0	*	1	1050	251	0	
1	0210	27	5	*	1	0825	102	0	*	1	1440	177	0	*	1	1055	252	0	
1	0215	28	6	*	1	0830	103	0	*	1	1445	178	0	*	1	1100	253	0	
1	0220	29	6	*	1	0835	104	0	*	1	1450	179	0	*	1	1105	254	0	
1	0225	30	5	*	1	0840	105	0	*	1	1455	180	0	*	1	1110	255	0	
1	0230	31	7	*	1	0845	106	0	*	1	1500	181	0	*	1	1115	256	0	
1	0235	32	9	*	1	0850	107	0	*	1	1505	182	0	*	1	1120	257	0	
1	0240	33	11	*	1	0855	108	0	*	1	1510	183	0	*	1	1125	258	0	
1	0245	34	14	*	1	0900	109	0	*	1	1515	184	0	*	1	1130	259	0	
1	0250	35	17	*	1	0905	110	0	*	1	1520	185	0	*	1	1135	260	0	
1	0255	36	21	*	1	0910	111	0	*	1	1525	186	0	*	1	1140	261	0	
1	0300	37	33	*	1	0915	112	0	*	1	1530	187	0	*	1	1145	262	0	
1	0305	38	48	*	1	0920	113	0	*	1	1535	188	0	*	1	1150	263	0	
1	0310	39	59	*	1	0925	114	0	*	1	1540	189	0	*	1	1155	264	0	
1	0315	40	103	*	1	0930	115	0	*	1	1545	190	0	*	1	1200	265	0	
1	0320	41	114	*	1	0935	116	0	*	1	1550	191	0	*	1	1205	266	0	
1	0325	42	109	*	1	0940	117	0	*	1	1555	192	0	*	1	1210	267	0	
1	0330	43	100	*	1	0945	118	0	*	1	1600	193	0	*	1	1215	268	0	
1	0335	44	89	*	1	0950	119	0	*	1	1605	194	0	*	1	1220	269	0	
1	0340	45	77	*	1	0955	120	0	*	1	1610	195	0	*	1	1225	270	0	

[illegible]









[illegible]

33D NAME	2.02	64.29	192.41	1.27	5.00	61.02	150.00	1.22
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 2679E+01 OUTFLOW: 2627E+01 BASIN STORAGE: 1831E+01 PERCENT ERROR: 5								
510ET NAME	85	79.65	186.49	2.24	5.00	70.00	185.00	2.95
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 2873E+01 OUTFLOW: 2871E+01 BASIN STORAGE: 1120E+01 PERCENT ERROR: 0								
33C NAME	51	129.46	185.80	2.96	5.00	125.66	185.00	2.97
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 4670E+01 OUTFLOW: 4674E+01 BASIN STORAGE: 1952E+01 PERCENT ERROR: 1								
340CN NAME	57	187.33	186.05	3.96	5.00	179.92	185.00	2.97
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 7000E+01 OUTFLOW: 7077E+01 BASIN STORAGE: 4084E+01 PERCENT ERROR: 0								
RISE 1 NAME	3.45	255.03	201.54	1.92	5.00	251.70	200.00	1.97
CONTINUITY SUMMARY (AC-FT) - INFLOW: .5208E+02 EXCESS: .0000E+00 OUTFLOW: .5102E+02 BASIN STORAGE: 2102E+01 PERCENT ERROR: 1								
340D NAME	1.70	91.21	190.76	1.23	5.00	89.79	190.00	1.23
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 3491E+01 OUTFLOW: 3379E+01 BASIN STORAGE: 2007E+01 PERCENT ERROR: 4								
510ET NAME	33	31.72	184.75	3.00	5.00	31.47	185.00	3.01
CONTINUITY SUMMARY (AC-FT) - INFLOW: 0000E+00 EXCESS: 1005E+01 OUTFLOW: 1008E+01 BASIN STORAGE: 4154E+05 PERCENT ERROR: 1								

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
		ELEVATION	00	1.00	3.00		
		STORAGE	0	1	2		
		OUTFLOW	0	20	20		
		RATIO OF PMP					
		MAXIMUM RESERVOIR DEPTH OVER DAM					
		MAXIMUM STORAGE AC-FT					
		MAXIMUM OUTFLOW CFS					
		DURATION OVER TOP HOURS					
		TIME OF MAX OUTFLOW HOURS					
		TIME OF FAILURE HOURS					
	1.00	1.73	00	1	12	00	3.50

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
		ELEVATION	00	1.00	3.00		
		STORAGE	0.	1	1		
		OUTFLOW	0	4.	4.		
		RATIO OF PMP					
		MAXIMUM RESERVOIR DEPTH OVER DAM					
		MAXIMUM STORAGE AC-FT					
		MAXIMUM OUTFLOW CFS					
		DURATION OVER TOP HOURS					
		TIME OF MAX OUTFLOW HOURS					
		TIME OF FAILURE HOURS					
	1.00	2.51	00	1.	3	00	3.57

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
		ELEVATION	.00	3.00	3.00		
		STORAGE	0	1	1		
		OUTFLOW	0	4	4		
		RATIO OF PMP					
		MAXIMUM RESERVOIR DEPTH OVER DAM					
		MAXIMUM STORAGE AC-FT					
		MAXIMUM OUTFLOW CFS					
		DURATION OVER TOP HOURS					
		TIME OF MAX OUTFLOW HOURS					
		TIME OF FAILURE HOURS					
	1.50	3.14	14	1	4	1.42	3.58

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN	1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
		ELEVATION	00	2.50	2.50		
		STORAGE	0	0	0		
		OUTFLOW	0	22	22.		
		RATIO OF PMP					
		MAXIMUM RESERVOIR DEPTH OVER DAM					
		MAXIMUM STORAGE AC-FT					
		MAXIMUM OUTFLOW CFS					
		DURATION OVER TOP HOURS					
		TIME OF MAX OUTFLOW HOURS					
		TIME OF FAILURE HOURS					
	1.00	2.31	0	11	25	3.11	00

1 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DETAIL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	2.50	2.50			
	OUTFLOW	0.	0	0			
			12	12			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	2.87	.37	0.	35.	33	3.33
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	2.50	2.50			
	OUTFLOW	0	1	1.			
			14	14			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	2.94	.46	1	51	13	1.33
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	2.50	2.50			
	OUTFLOW	0	0	0			
			11.	11			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	2.65	.15	0	14	17	3.33
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	2.50	2.50			
	OUTFLOW	0	1	1			
			11	11.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	3.62	1.12	1	66	1.50	1.42
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	3.60	3.60			
	OUTFLOW	0	7.	2			
			14.	14.			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	4.85	1.26	2	74	1.33	3.50
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	3.60	3.60			
	OUTFLOW	0	0	0			
			14	14			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	5.05	1.45	1	93	2.25	3.50
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					
PLAN 1							
	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM			
	STORAGE	00	3.60	3.60			
	OUTFLOW	0	1	1			
			14	14			
	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS
1	1.00	5.02	1.47	1	90	2.92	3.50
							.00
		SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DELIAS (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)					

PLAN 1	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	00	1 60	1 60
STORAGE	0	1.	1.
OUTFLOW	0	14	14

PLAN 1	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	00	150	150
STORAGE	0	1	1
OUTFLOW	0	150.	150.

PLAN 1	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION	00	1 00	1 00
STORAGE	0	1	1
OUTFLOW	0	13	13.

PARAMETER	INITIAL VALUE	SPRIMARY CRIST	TOP OF DAM
ELEVATION	00	1 00	1.00
STORAGE	0	2	2
DIFFUSION	0	10	13.

PLAN 1	INITIAL VALUE	SPILLWAY CRIST	TOP OF DAM
ELEVATION	00	1.00	3.00
STORAGE	0	2	2
OUEFLOW	0	11	13.

PLAN	INITIAL VALUE	SPELLING CHECK	TOT OF DAM
ELEVATION	00	1 00	3 00
STORAGE	0	1	3.
OUTFLOW	0	13	13

ITEM	INITIAL VALUE	SPILLSAY CRUST	TOP OF DAM
ELEVATION	00	3 00	3 00
STORAGE	0	1	1
OUTFLOW	0	4	4

	RATIO OF PMF	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-F	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	1.00	2.95	00	1	4	00	1.50	00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	3 00	3 00		
	STORAGE		0.	2.	2		
	OUTFLOW		0	1	1		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 81 60 1 1. 00 3 75 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		.00	1 00	3 00		
	STORAGE		0	2	2.		
	OUTFLOW		0	10.	10		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 3 25 25 2 16 67 3 50 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	3 00	3 00		
	STORAGE		0	1	1		
	OUTFLOW		0	13	13		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 84 00 1. 12 00 3.47 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	1 00	3 00		
	STORAGE		0	1	1		
	OUTFLOW		0	11	11		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 47 00 1 9 00 3 13 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	3 00	3 00		
	STORAGE		0	5	5		
	OUTFLOW		0.	53	52		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 36 00 1 10 00 3 50 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	1 00	3 00		
	STORAGE		0	5	5		
	OUTFLOW		0	11	11		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2 57 00 1. 12 00 3 67 00

1

SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DEFEAL  
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1			INITIAL VALUE	SPILLWAY CREST	TOP OF DAM		
	ELEVATION		00	3 00	3 00		
	STORAGE		0	5	5.		
	OUTFLOW		0	20	20		

RATIO OF PMF	MAXIMUM RESERVOIR W S ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
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1 00 2.77 .00 3 18. 00 3.75 .00  
 SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION DET1H  
 (PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1 ...

		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
ELEVATION		00	3 00	3 00
STORAGE		0	3.	3
OUTFLOW		0	20.	70

RATIO OF IMP	MAXIMUM RESERVOIR W.S. ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
1 00	3 70	70	4	49	.83	3 42	00

\*\*\* NORMAL END OF REC-1 \*\*\*



# RATIONAL FOR WINDOWS

Flood Control District of Maricopa County Rational Method

## Project Information

Project Name: Interim Regional Drainage Chan      Project Description:  
Drainage Point: 404 Wash      Location: Channel Station 24+00

## Drainage Basin Data

Water Course Length: 820.00 ft      Basin Area: 3.220 acres  
High Elevation: 1581.00 ft      Low Elevation: 1570.00 ft  
Average Slope: 0.0134 ft/ft      Roughness, Kb: 0.0368 (A)  
10-Year Runoff Coefficient: 0.400  
10-Year 6 Hour Rainfall Depth: 2.10 inches

## Hydrological Summary Table

Parameter	2-Year	5-Year	10-Year	25-Year	50-Year	100-Year
Q (cfs)	4	6	7	9	12	14
C	0.400	0.400	0.400	0.440	0.480	0.500
Tc (min)	8.3	7.3	6.8	6.3	6.0	5.7
i (in/hr)	3.2	4.4	5.3	6.6	7.6	8.8

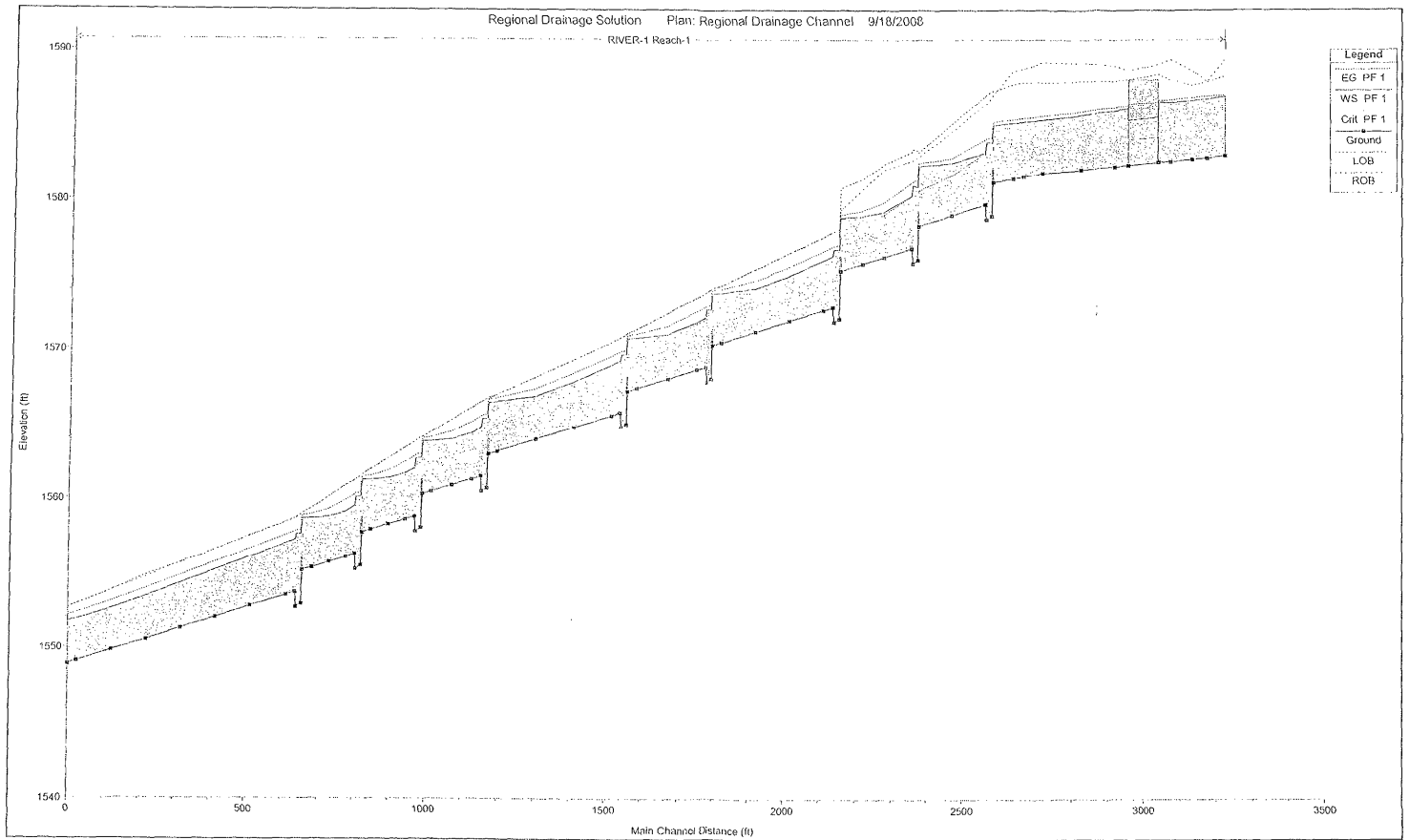
Computed by JMG, Wood, Patel & Associates  
Thursday, May 05, 2005 10:08:51 a

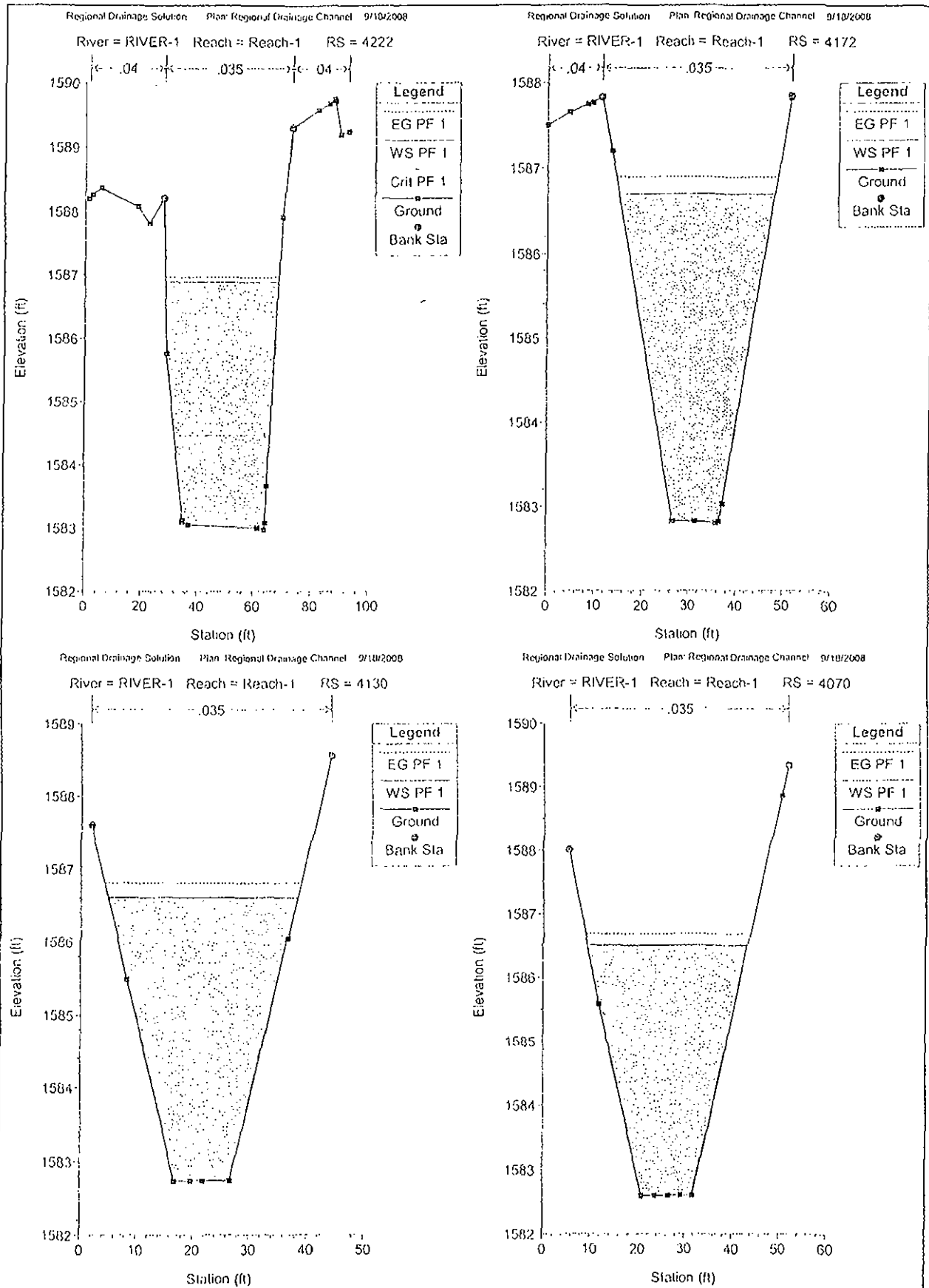
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## **APPENDIX B**

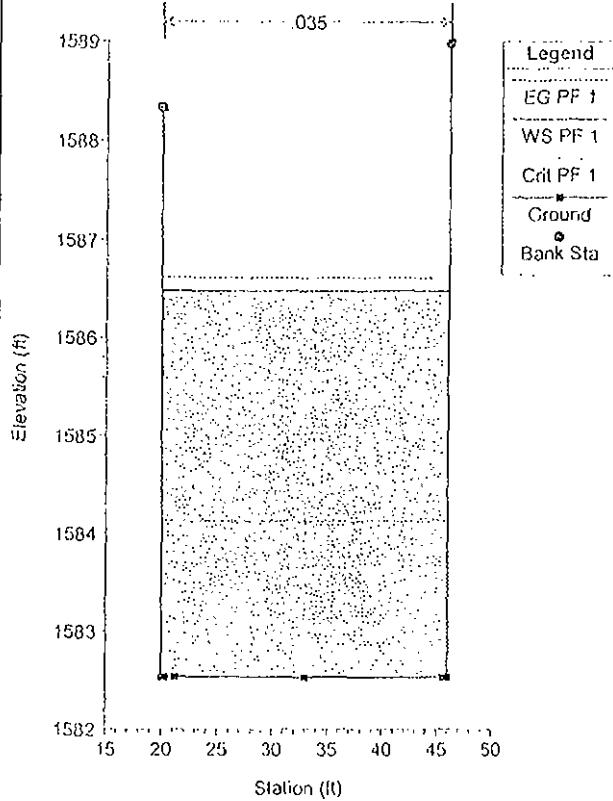
### **Hydraulic Calculations**

River Sta	Q Total (cfs)	Min Ch El (ft)	WS Elev (ft)	E G Elev (ft)	E G Slope (ft/l)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude #	Chl	LOB Elev (ft)	ROB Elev (ft)	Flow Depth (ft)	Freeboard Req (ft)	Freeboard Prov (ft)
4222	300	1582.97	1586.88	1586.95	0.000577	2.20	136.44	40.32	0.21	1588.20	1589.30	3.91	1.02	1.32	
4172	300	1582.80	1586.70	1586.89	0.002174	3.58	83.81	33.20	0.40	1587.82	1587.84	3.90	1.07	1.12	
4130	300	1582.73	1586.61	1586.80	0.002152	3.55	84.36	33.53	0.40	1587.60	1588.56	3.98	1.07	0.99	
4070	300	1582.59	1586.50	1586.68	0.001659	3.38	88.72	34.04	0.37	1588.00	1589.33	3.91	1.07	1.50	
4039	300	1582.53	1586.49	1586.62	0.001065	2.91	103.17	26.10	0.26	1588.33	1588.98	3.96	1.06	1.84	
4004	Culvert														
3953	300	1582.33	1586.12	1586.26	0.001218	3.04	98.73	26.07	0.28	1587.99	1588.61	3.79	1.02	1.87	
3915	300	1582.25	1585.96	1586.19	0.002674	3.87	77.54	31.91	0.44	1587.00	1588.90	3.71	1.04	1.94	
3819	300	1582.04	1585.68	1585.92	0.002809	3.93	76.32	31.87	0.45	1587.90	1589.11	3.64	1.03	2.22	
3715	300	1581.80	1585.36	1585.62	0.003119	4.09	73.44	31.32	0.47	1587.80	1589.14	3.56	1.02	2.44	
3663	300	1581.57	1585.22	1585.46	0.002787	3.92	76.60	31.99	0.45	1587.80	1588.70	3.65	1.03	2.58	
3635	300	1581.44	1585.15	1585.38	0.002613	3.83	78.43	32.32	0.43	1587.70	1588.57	3.71	1.04	2.55	
3582	300	1581.19	1585.03	1585.25	0.002239	3.75	78.99	29.78	0.40	1587.23	1587.03	3.94	1.07	2.00	
3581	Int Struct														
3579	300	1570.95	1583.86	1584.21	0.004005	4.74	63.31	25.18	0.53	1587.21	1586.88	4.90	1.40	3.02	
3594	300	1578.70	1583.90	1584.13	0.002489	3.84	78.11	30.25	0.42	1587.02	1586.40	5.20	1.41	2.50	
3561	300	1579.71	1583.16	1584.05	0.016160	7.55	39.76	23.04	1.01	1586.89	1586.40	3.45	1.31	3.24	
3467	300	1579.00	1582.50	1582.81	0.004580	4.51	66.59	33.05	0.56	1585.10	1584.55	3.50	1.03	2.05	
3374	300	1578.30	1582.30	1582.51	0.002052	3.70	81.10	28.57	0.39	1583.20	1582.91	4.00	1.11	0.61	
3373	Int Struct														
3371	300	1576.07	1580.98	1581.30	0.006706	5.66	52.99	22.05	0.64	1583.36	1582.90	4.81	1.45	2.02	
3359	300	1575.82	1581.00	1581.24	0.002647	3.91	76.65	30.23	0.43	1583.42	1582.70	5.18	1.41	1.70	
3353	300	1576.82	1580.29	1581.16	0.015790	7.48	40.09	23.11	1.00	1583.22	1582.64	3.47	1.30	2.35	
3276	300	1576.24	1579.23	1579.86	0.011545	6.38	47.00	27.66	0.86	1582.40	1582.03	2.99	1.06	2.00	
3216	300	1575.79	1578.94	1579.31	0.005728	4.87	61.57	32.20	0.62	1581.40	1580.73	3.15	1.00	1.79	
3156	300	1575.31	1578.04	1579.04	0.002516	3.56	84.27	38.12	0.42	1580.80	1579.34	3.50	1.00	0.50	
3155	Int Struct														
3152	300	1572.09	1576.77	1577.04	0.003261	4.13	72.56	31.02	0.48	1578.10	1578.13	4.68	1.30	1.33	
3138	300	1571.86	1576.76	1576.98	0.002956	3.77	79.48	32.42	0.42	1577.91	1577.91	4.90	1.34	1.15	
3135	300	1572.86	1576.31	1576.93	0.011152	6.29	47.70	27.67	0.84	1577.86	1577.90	3.45	1.17	1.55	
3110	300	1572.67	1576.04	1576.65	0.010850	6.25	47.99	27.72	0.84	1577.58	1577.58	3.37	1.15	1.54	
3014	300	1571.95	1575.00	1575.61	0.010923	6.25	47.99	27.94	0.84	1576.51	1576.51	3.05	1.07	1.51	
2918	300	1571.20	1574.18	1574.67	0.008218	5.59	53.71	30.00	0.74	1575.43	1575.43	2.98	1.00	1.25	
2822	300	1570.50	1573.89	1574.12	0.003236	3.92	76.54	35.19	0.47	1574.36	1574.36	3.39	1.00	0.47	
2797	300	1570.30	1573.84	1574.04	0.002621	3.63	82.62	37.37	0.43	1574.17	1574.17	3.54	1.00	0.33	
2796	Int Struct														
2794	300	1568.08	1572.74	1573.01	0.003367	4.19	71.66	30.83	0.48	1574.12	1574.12	4.66	1.30	1.38	
2779	300	1567.85	1572.72	1572.95	0.002625	3.81	78.66	32.24	0.43	1573.90	1573.90	4.87	1.33	1.18	
2776	300	1568.85	1572.20	1572.89	0.013016	6.65	45.11	26.93	0.91	1573.85	1573.85	3.35	1.18	1.65	
2751	300	1568.66	1571.84	1572.58	0.013511	6.79	44.21	26.63	0.93	1573.52	1573.52	3.18	1.15	1.68	
2668	300	1568.04	1571.02	1571.57	0.009690	5.57	50.23	23.66	0.80	1572.43	1572.43	2.98	1.02	1.41	
2586	300	1567.40	1570.78	1571.03	0.003459	4.03	74.45	35.48	0.49	1571.35	1571.35	3.38	1.00	0.57	
2561	300	1567.20	1570.74	1570.94	0.002633	3.64	82.40	37.34	0.43	1571.07	1571.10	3.54	1.00	0.33	
2559	Int Struct														
2557	300	1564.90	1569.66	1569.93	0.003263	4.14	72.51	31.01	0.48	1571.00	1571.02	4.68	1.30	1.34	
2543	300	1564.80	1569.65	1569.87	0.002573	3.78	79.42	32.59	0.43	1570.80	1570.80	4.85	1.32	1.15	
2540	300	1565.75	1569.23	1569.82	0.010714	6.18	48.52	27.91	0.83	1570.75	1570.75	3.48	1.17	1.52	
2513	300	1565.56	1568.96	1569.55	0.010483	6.17	48.03	27.92	0.82	1570.47	1570.47	3.40	1.15	1.51	
2408	300	1564.76	1567.84	1568.43	0.010601	6.18	48.55	28.14	0.83	1569.32	1569.32	3.00	1.07	1.46	
2302	300	1563.97	1566.87	1567.30	0.008824	5.73	52.37	29.71	0.76	1568.16	1568.16	2.90	1.00	1.29	
2196	300	1563.17	1566.52	1566.76	0.003297	3.94	76.09	36.17	0.48	1567.00	1567.00	3.35	1.00	0.48	
2171	300	1562.88	1566.47	1566.68	0.003607	3.66	81.91	37.25	0.44	1566.72	1566.82	3.49	1.00	0.25	
2170	Int Struct														
2168	300	1560.72	1565.30	1565.65	0.003387	4.10	71.69	30.74	0.48	1566.69	1566.77	4.66	1.30	1.31	
2153	300	1560.50	1565.36	1565.59	0.002655	3.83	78.23	32.12	0.43	1566.51	1566.50	4.86	1.33	1.14	
2150	300	1561.49	1564.78	1565.52	0.014412	6.93	43.32	26.32	0.95	1566.49	1566.49	3.29	1.20	1.71	
2125	300	1561.30	1564.40	1565.16	0.011646	7.00	42.84	26.16	0.96	1566.13	1566.10	3.10	1.16	1.70	
2071	300	1560.90	1563.98	1564.49	0.009524	5.69	52.99	29.33	0.75	1565.33	1565.33	3.09	1.02	1.35	
2015	300	1560.49	1563.85	1564.11	0.003655	4.12	72.78	34.92	0.50	1564.49	1564.49	3.36	1.00	0.64	
1950	300	1560.29	1563.82	1564.02	0.002561	3.60	83.30	37.49	0.43	1564.13	1564.13	3.53	1.00	0.31	
1969	Int Struct														
1968	300	1558.04	1562.70	1562.97	0.003360	4.17	71.94	30.82	0.48	1564.10	1564.08	4.88	1.30	1.38	
1972	300	1557.81	1562.69	1562.92	0.002601	3.80	78.85	32.25	0.43	1563.99	1563.98	4.88	1.33	1.17	
1959	300	1558.81	1562.04	1562.84	0.015946	7.19	41.71	25.88	1.00	1563.81	1563.81	3.23	1.21	1.77	
1944	300	1558.00	1561.69	1562.45	0.011631	6.93	42.89	26.22	0.96	1563.43	1563.40	3.09	1.15	1.71	
1896	300	1558.27	1561.37	1561.86	0.008189	5.61	53.49	29.55	0.73	1562.69	1562.69	3.10	1.02	1.32	
1849	300	1557.92	1561.27	1561.54	0.003791	4.19	71.68	34.47	0.51	1561.96	1562.62	3.35	1.00	0.69	
1824	300	1557.70	1561.24	1561.44	0.002625	3.63	82.56	37.35	0.43	1561.57	1561.60	3.54	1.00	0.33	
1822	Int Struct														
1821	300	1555.48	1560.14	1560.41	0.003364	4.18	71.70	30.83	0.48	1561.52	1561.52	4.68	1.30	1.39	
1806	300	1555.25	1560.12	1560.35	0.002643	3.82	78.61	32.23	0.43	1561.30	1561.30	4.87	1.33	1.18	
1803	300	1556.30	1559.51	1560.28	0.015862	7.05	42.58	26.10	0.97	1561.20	1561.25	3.21	1.19	1.69	
1778	300	1556.06	1559.11	1559.90	0.015490	7.15	41.96	25.92	0.99	1560.86	1560.90	3.05	1.16	1.75	
1731	300	1555.70	1558.80	1559.29	0.008204	5.61	53.44	29.53	0.74	1560.13	1560.13	3.10	1.02	1.33	
1683	300	1555.35	1558.70	1558.97	0.003793	4.18	71.72	34.54	0.51	1559.39	1559.40	3.35	1.00	0.69	
1658	300	1555.16	1558.66	1558.87	0.002707	3.67	81.66	37.17	0.44	1559.00	1559.00	3.50	1.00	0.34	
1657	Int Struct														
1655	300	1552.91	1557.63	1557.88	0.003131	4.07	73.68	31.12	0.47	1558.95	1558.95	4.72	1.31	1.32	
1640	300	1552.68	1557.61	1557.83	0.002403	3.73	80.39	32.63	0.42	1558.73	1558.70	4.93	1.34	1.09	
1631	300	1553.68	1557.24	1557.78	0.009394	5.91	50.80	28.45	0.78	1558.60	1558.70	3.56	1.16	1.44	
1612	300	1553.49	1557.00	1557.55	0.009394	5.92	50.69	28.53	0.78	1558.40	1558.44	3.51</			

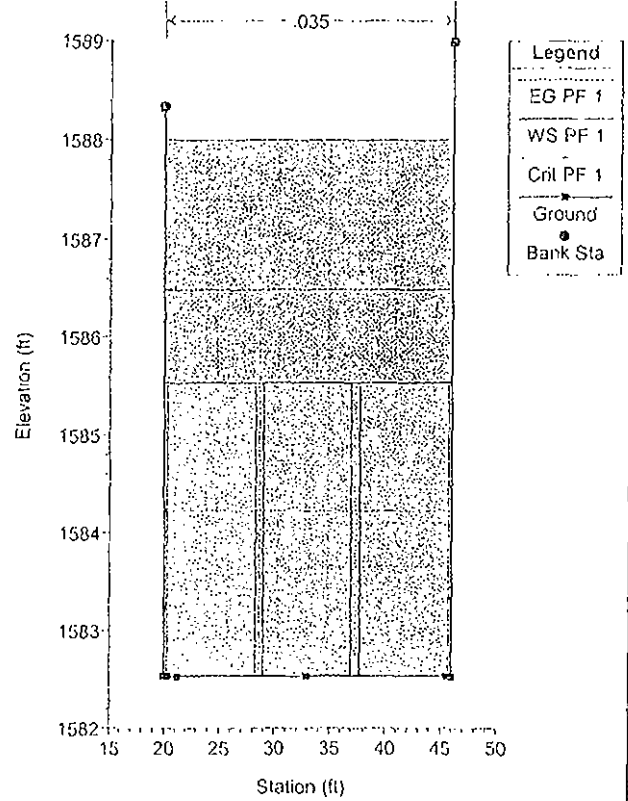




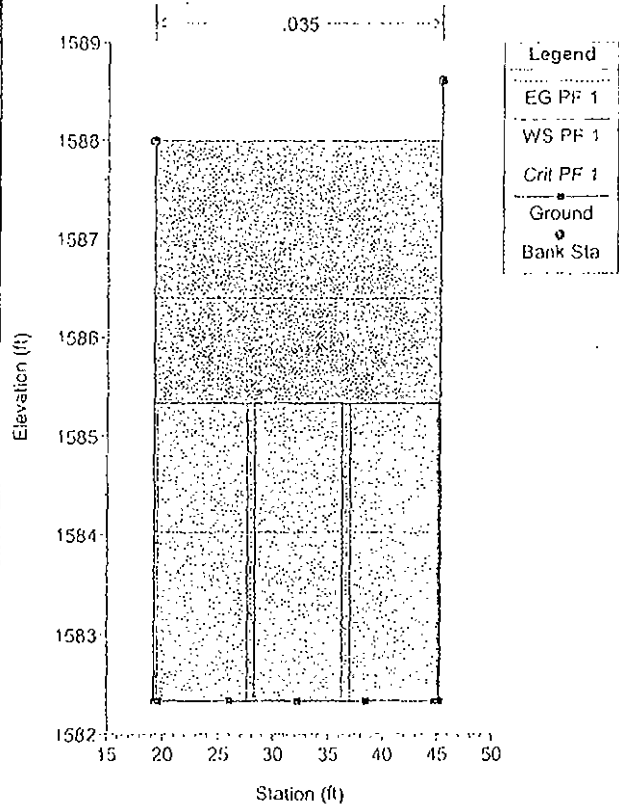
River = RIVER-1 Reach = Reach-1 RS = 4039



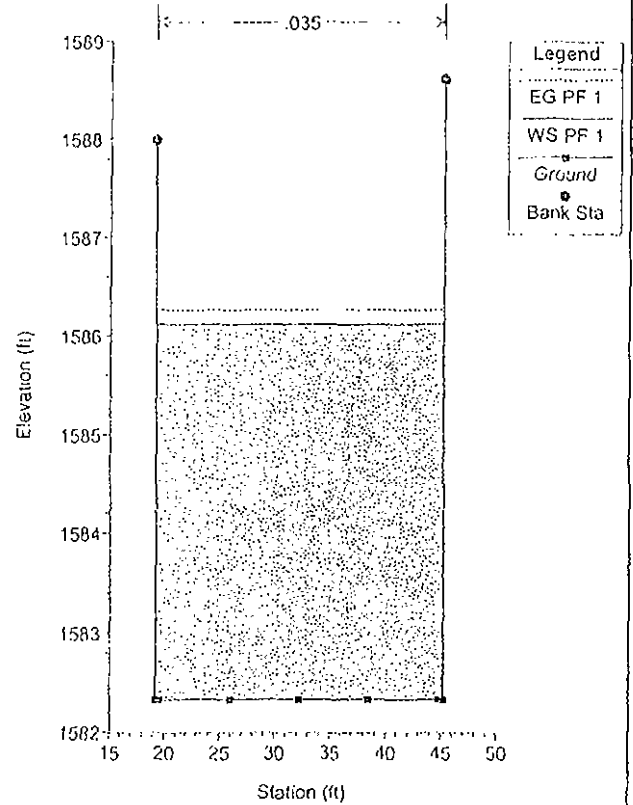
River = RIVER-1 Reach = Reach-1 RS = 4004 Culv

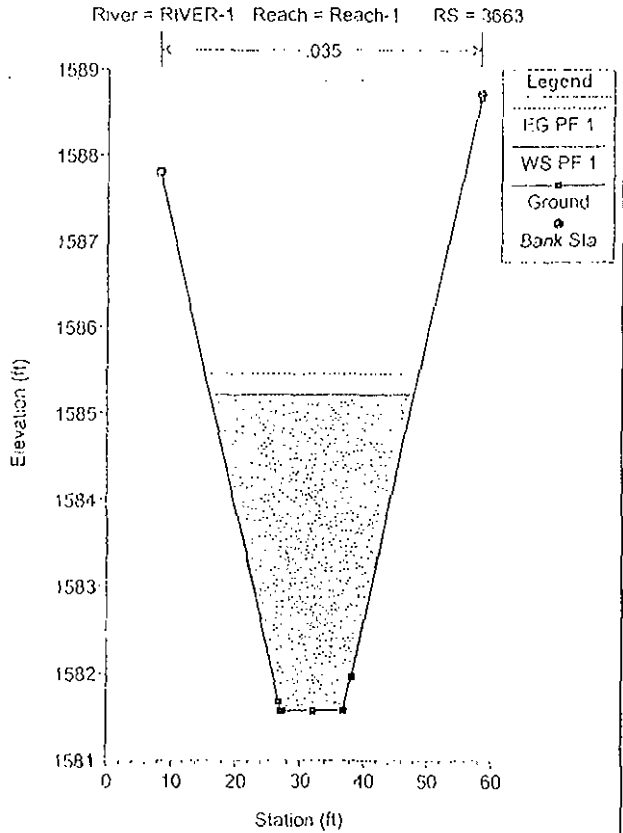
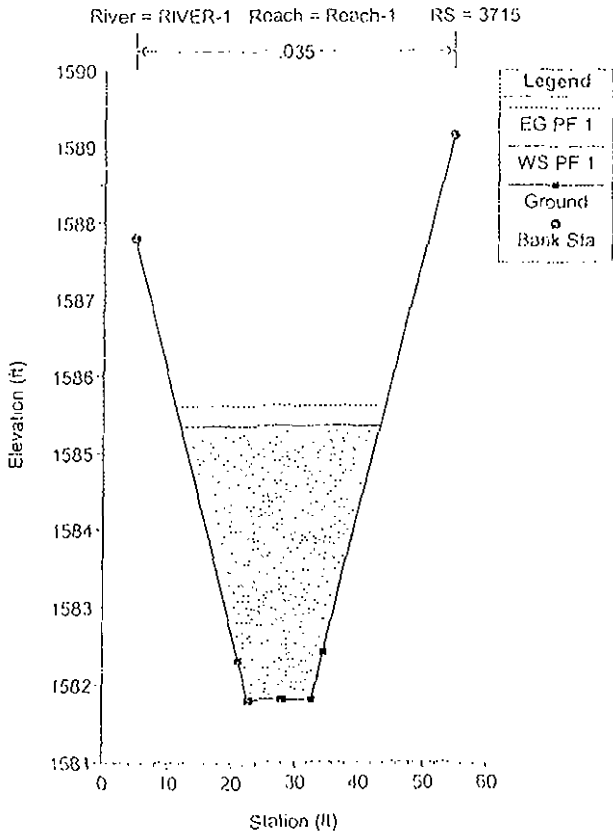
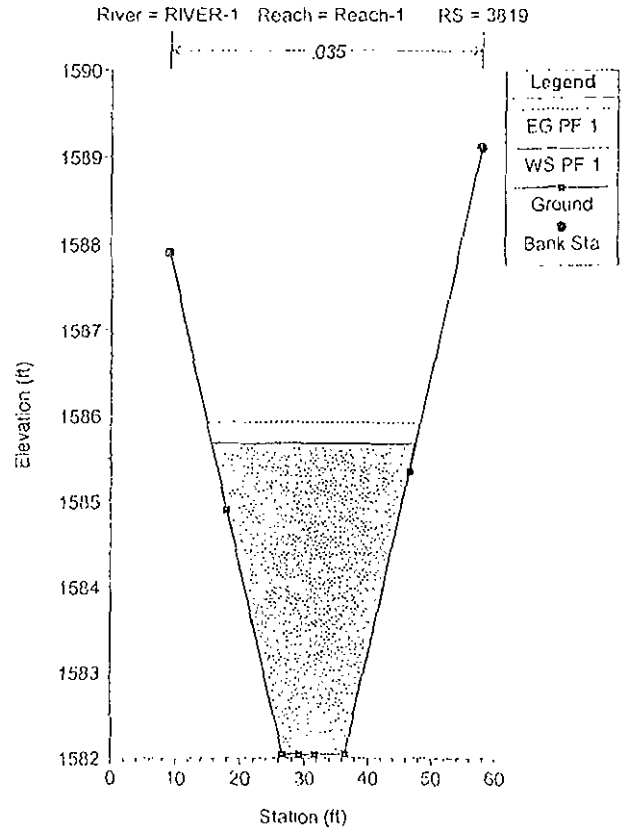
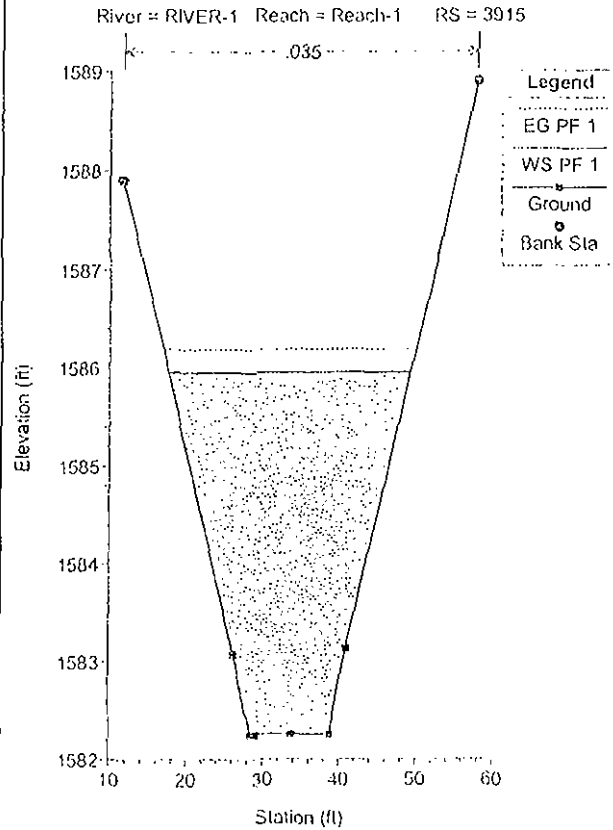


River = RIVER-1 Reach = Reach-1 RS = 4004 Culv

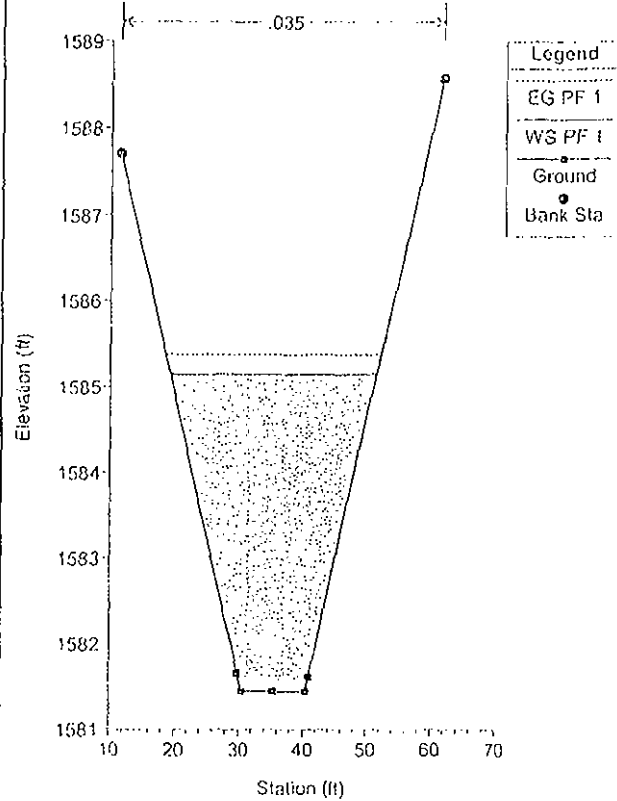


River = RIVER-1 Reach = Reach-1 RS = 3953

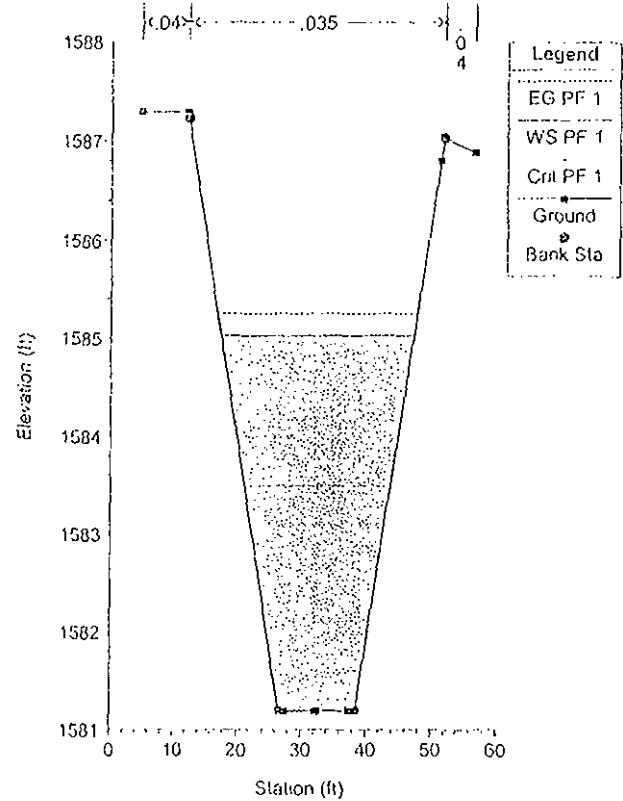




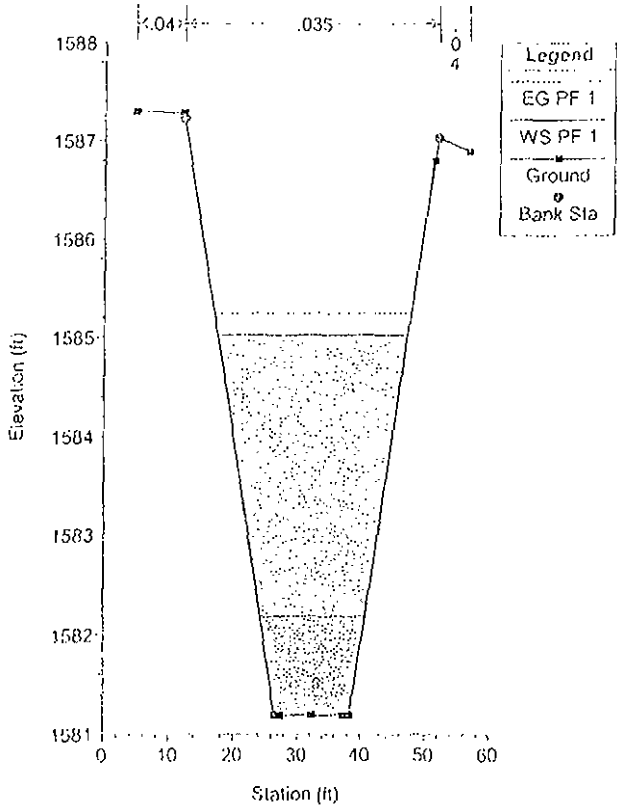
River = RIVER-1 Reach = Reach-1 RS = 3635



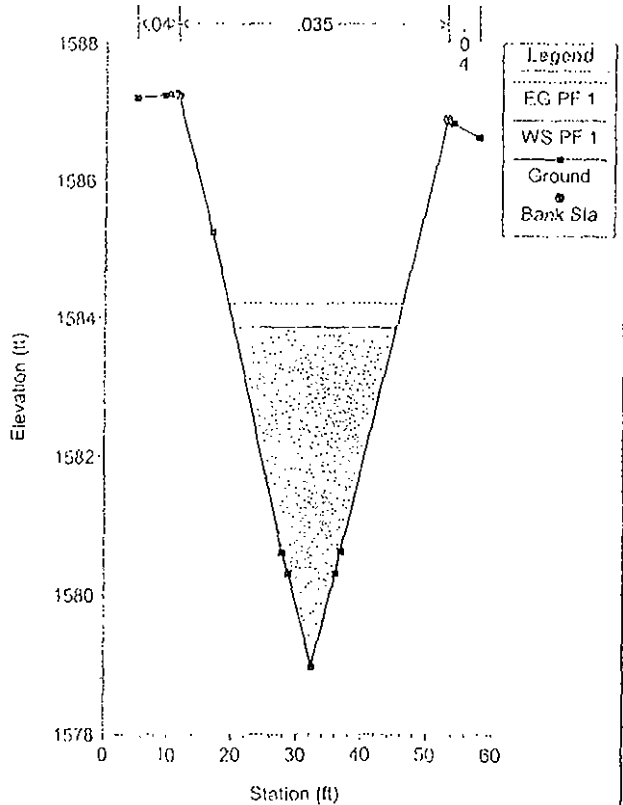
River = RIVER-1 Reach = Reach-1 RS = 3582



River = RIVER-1 Reach = Reach-1 RS = 3581 IS

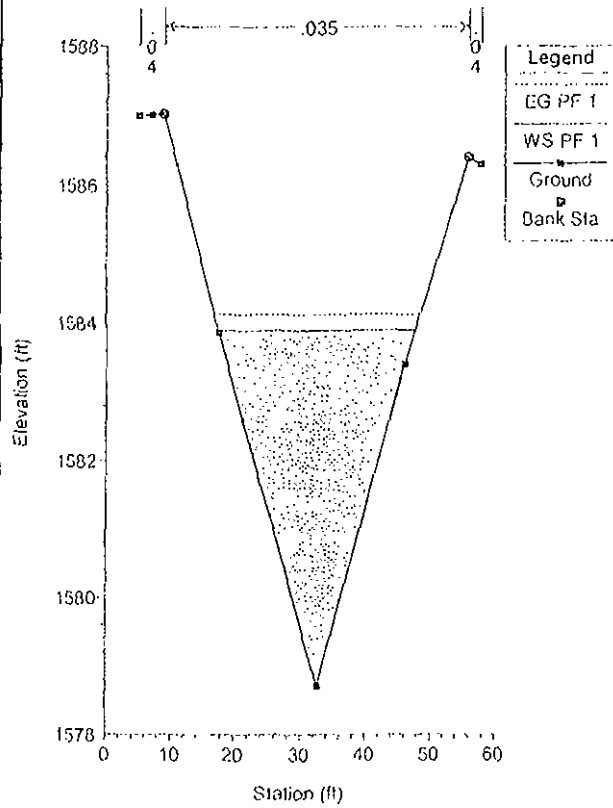


River = RIVER-1 Reach = Reach-1 RS = 3579

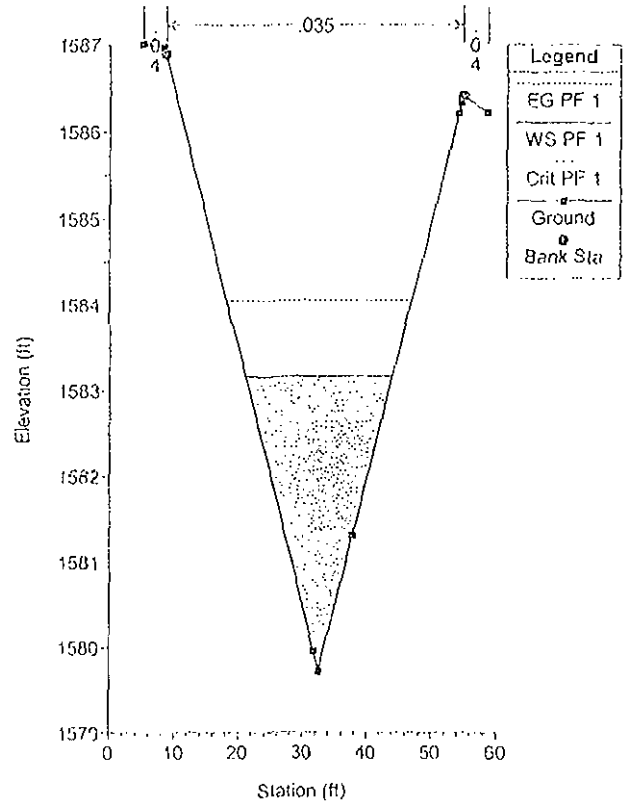




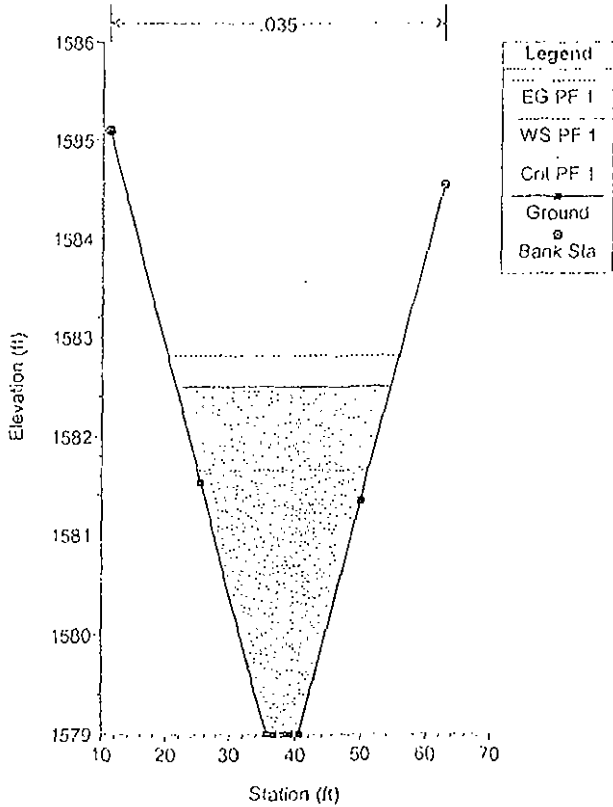
River = RIVER-1 Reach = Reach-1 RS = 3564



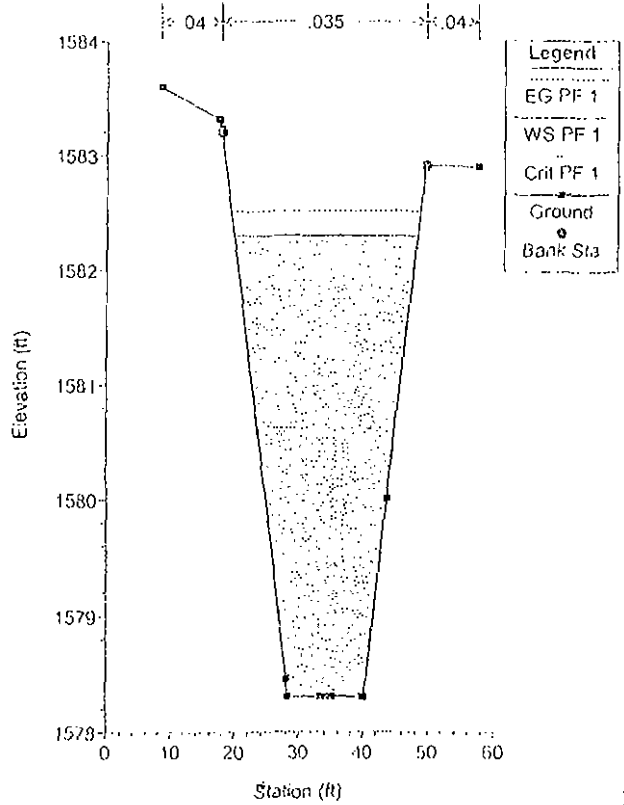
River = RIVER-1 Reach = Reach-1 RS = 3561



River = RIVER-1 Reach = Reach-1 RS = 3467

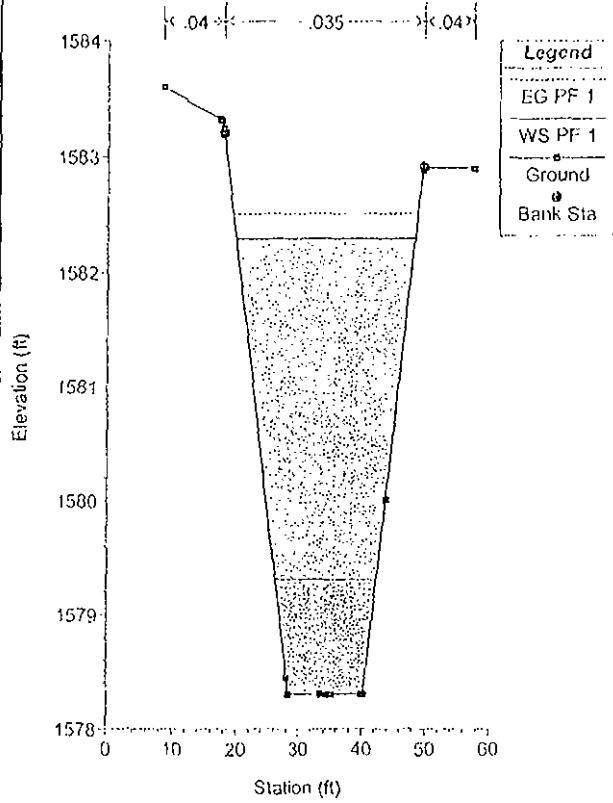


River = RIVER-1 Reach = Reach-1 RS = 3374



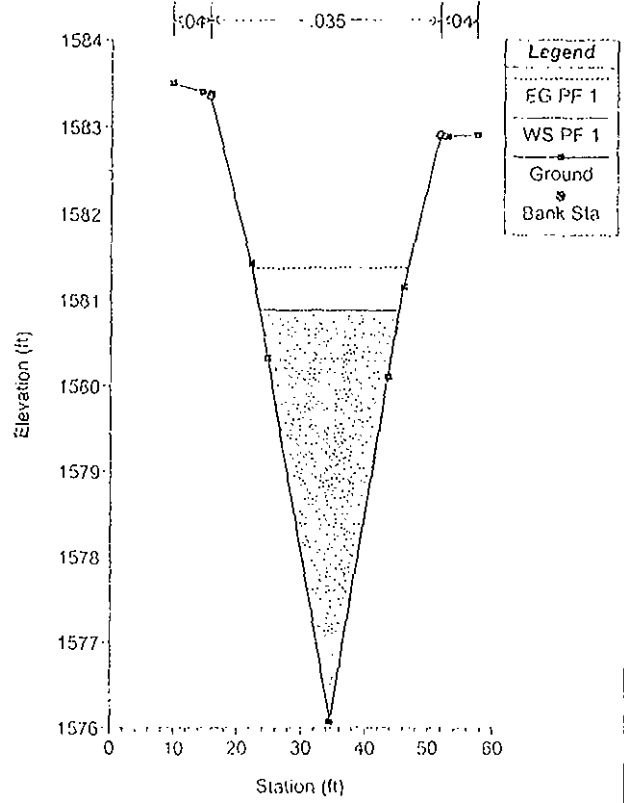
Regional Drainage Solution Plan: Regional Drainage Channel 9/18/2008

River = RIVER-1 Reach = Reach-1 RS = 3373 IS



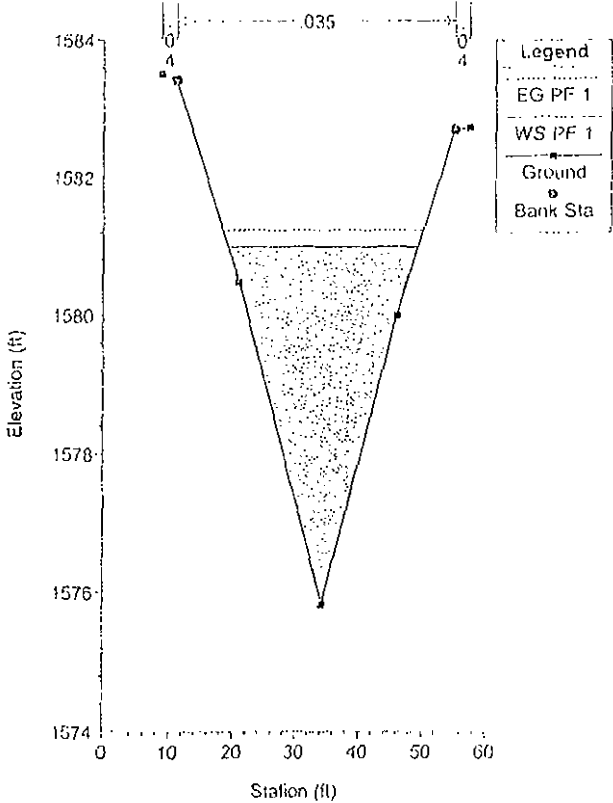
Regional Drainage Solution Plan: Regional Drainage Channel 9/18/2008

River = RIVER-1 Reach = Reach-1 RS = 3371



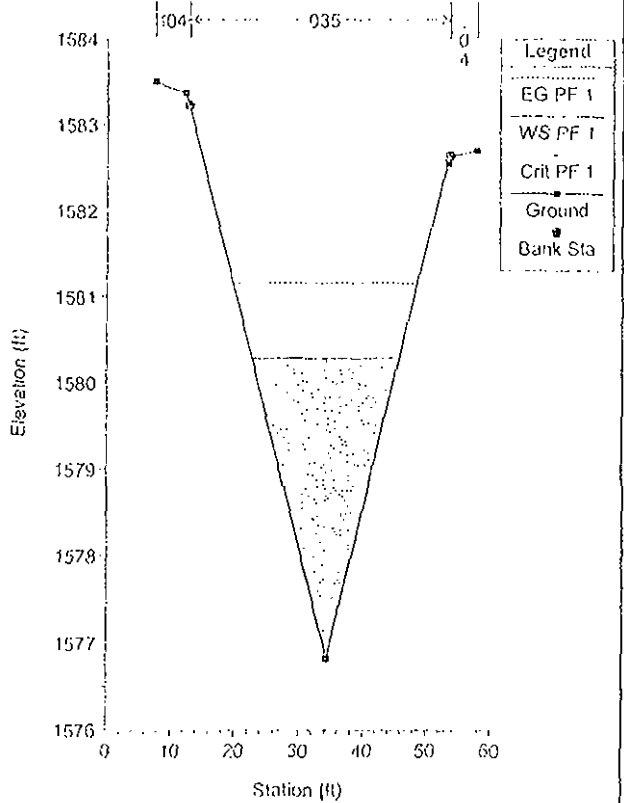
Regional Drainage Solution Plan: Regional Drainage Channel 9/18/2008

River = RIVER-1 Reach = Reach-1 RS = 3356

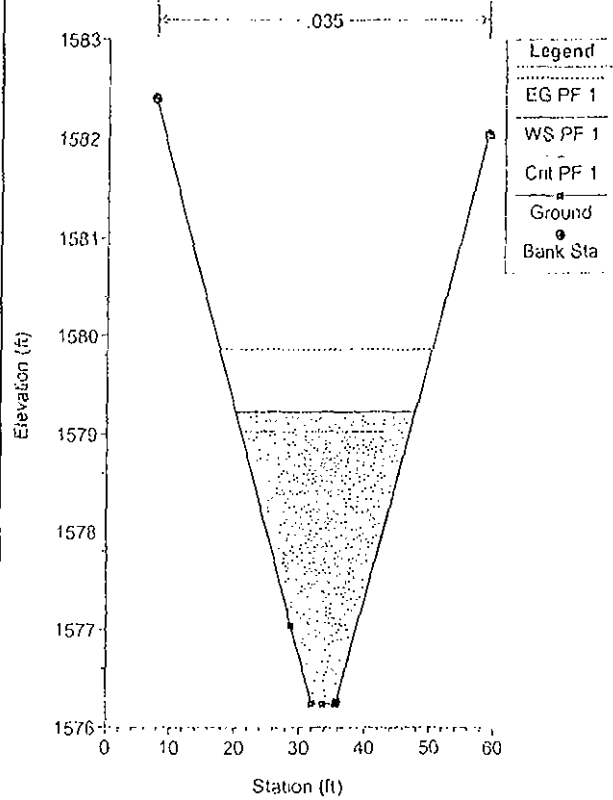


Regional Drainage Solution Plan: Regional Drainage Channel 9/18/2008

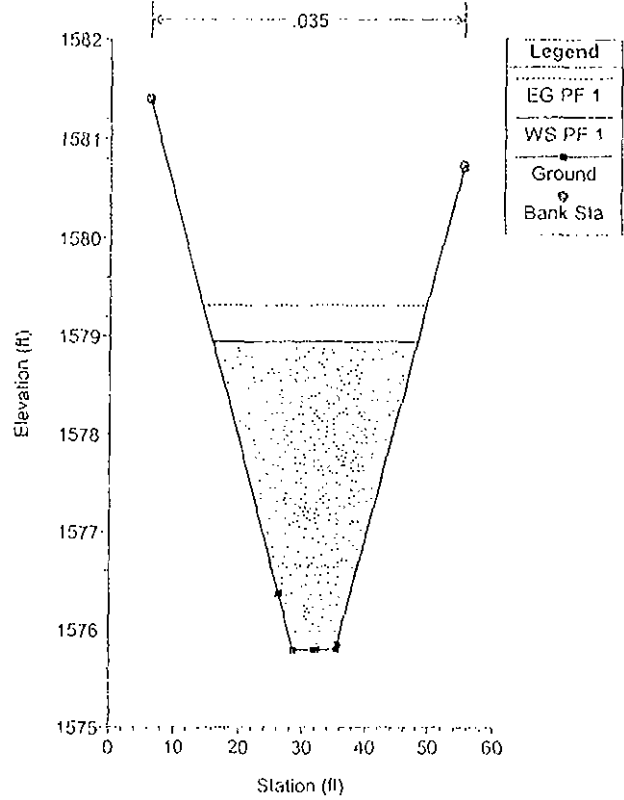
River = RIVER-1 Reach = Reach-1 RS = 3353



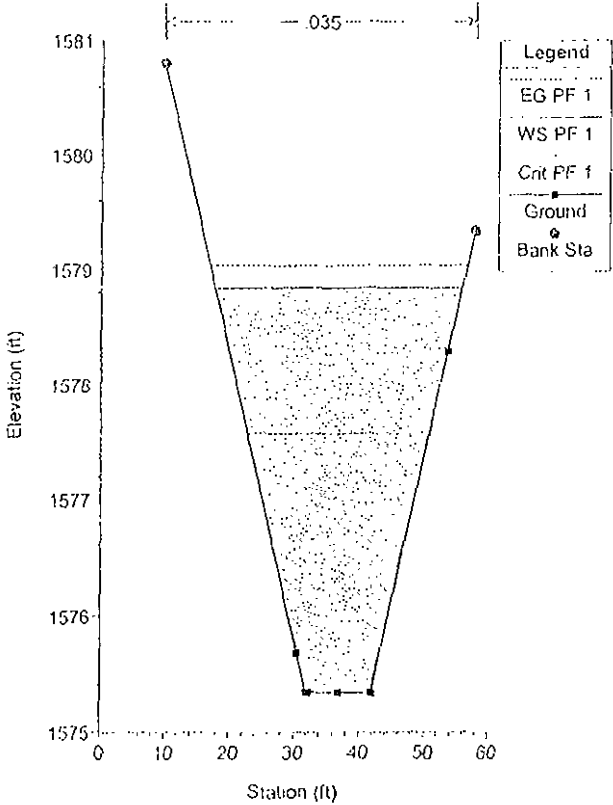
River = RIVER-1 Reach = Reach-1 RS = 3276



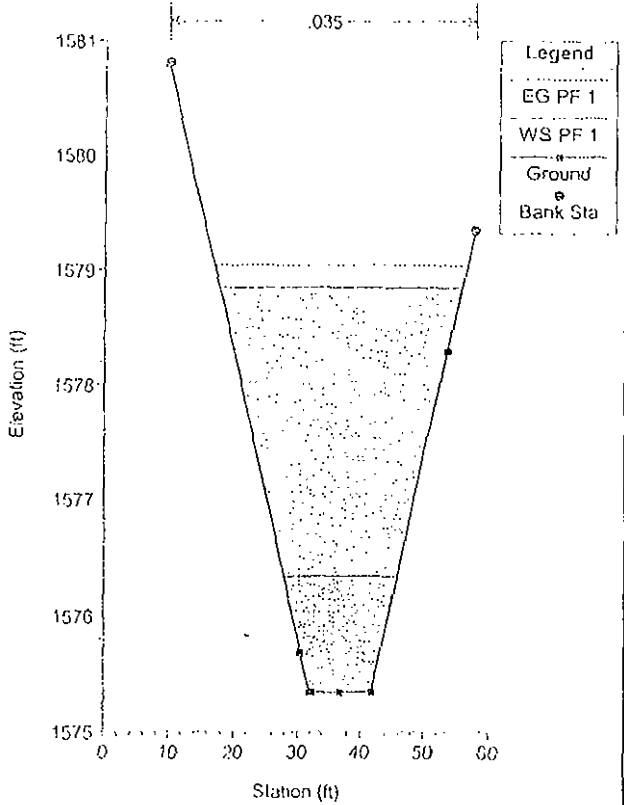
River = RIVER-1 Reach = Reach-1 RS = 3216



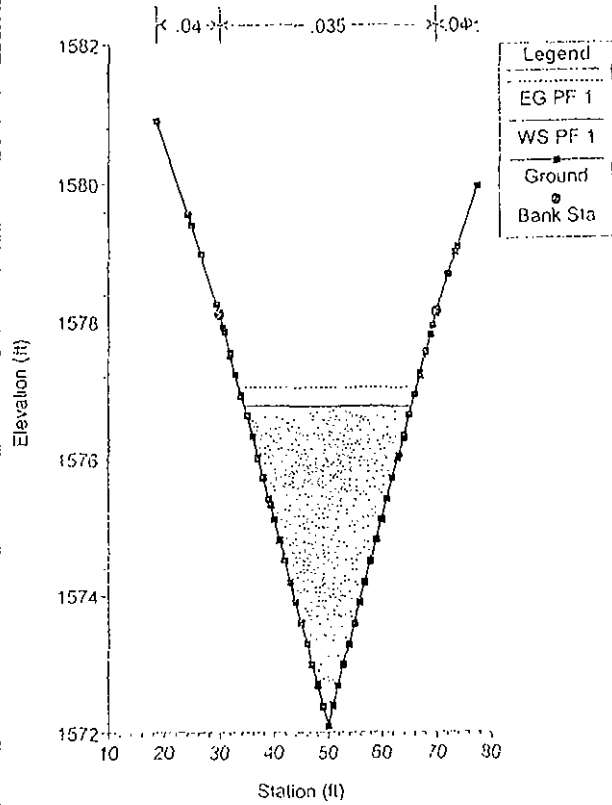
River = RIVER-1 Reach = Reach-1 RS = 3156



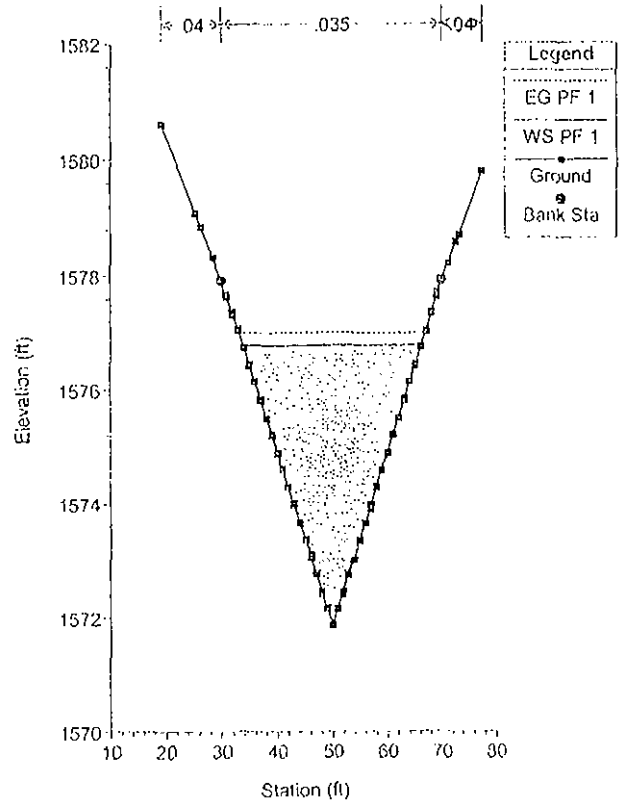
River = RIVER-1 Reach = Reach-1 RS = 3155 IS



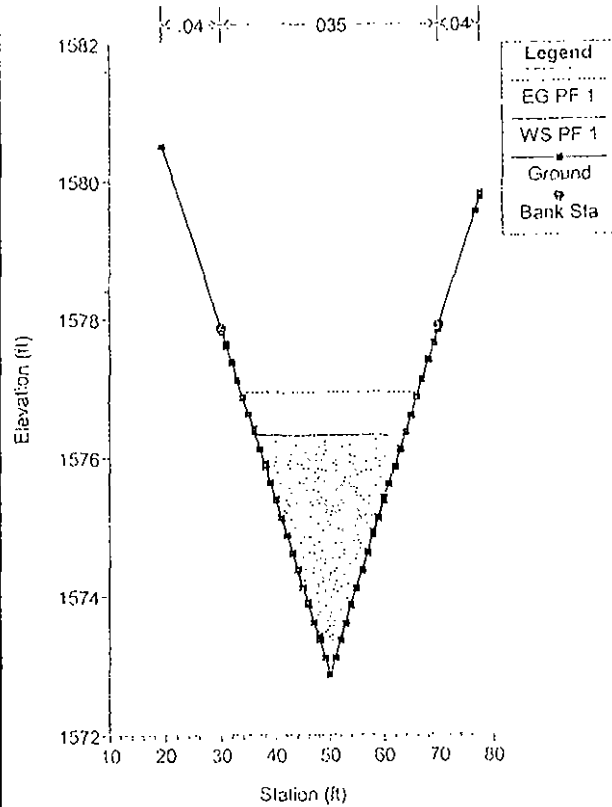
River = RIVER-1 Reach = Reach-1 RS = 3152



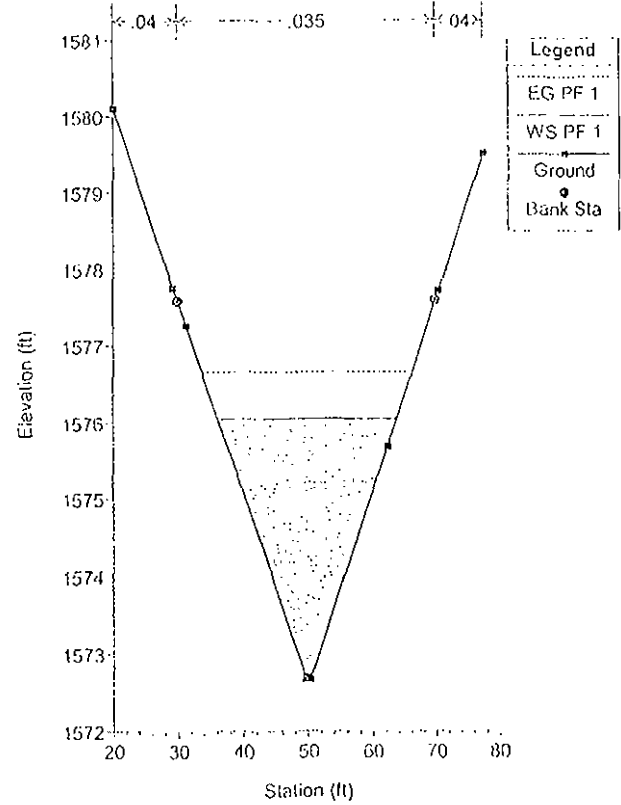
River = RIVER-1 Reach = Reach-1 RS = 3138

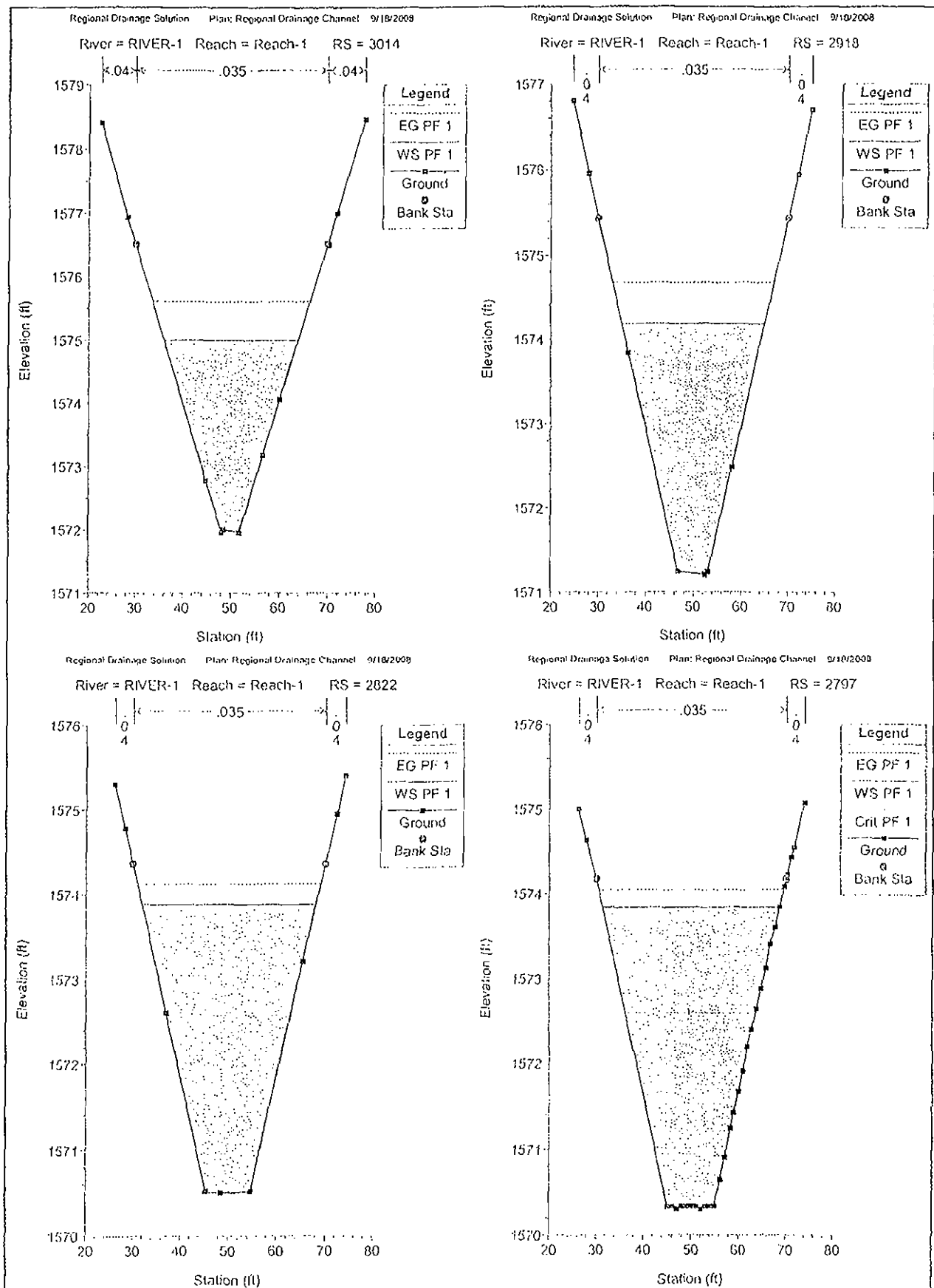


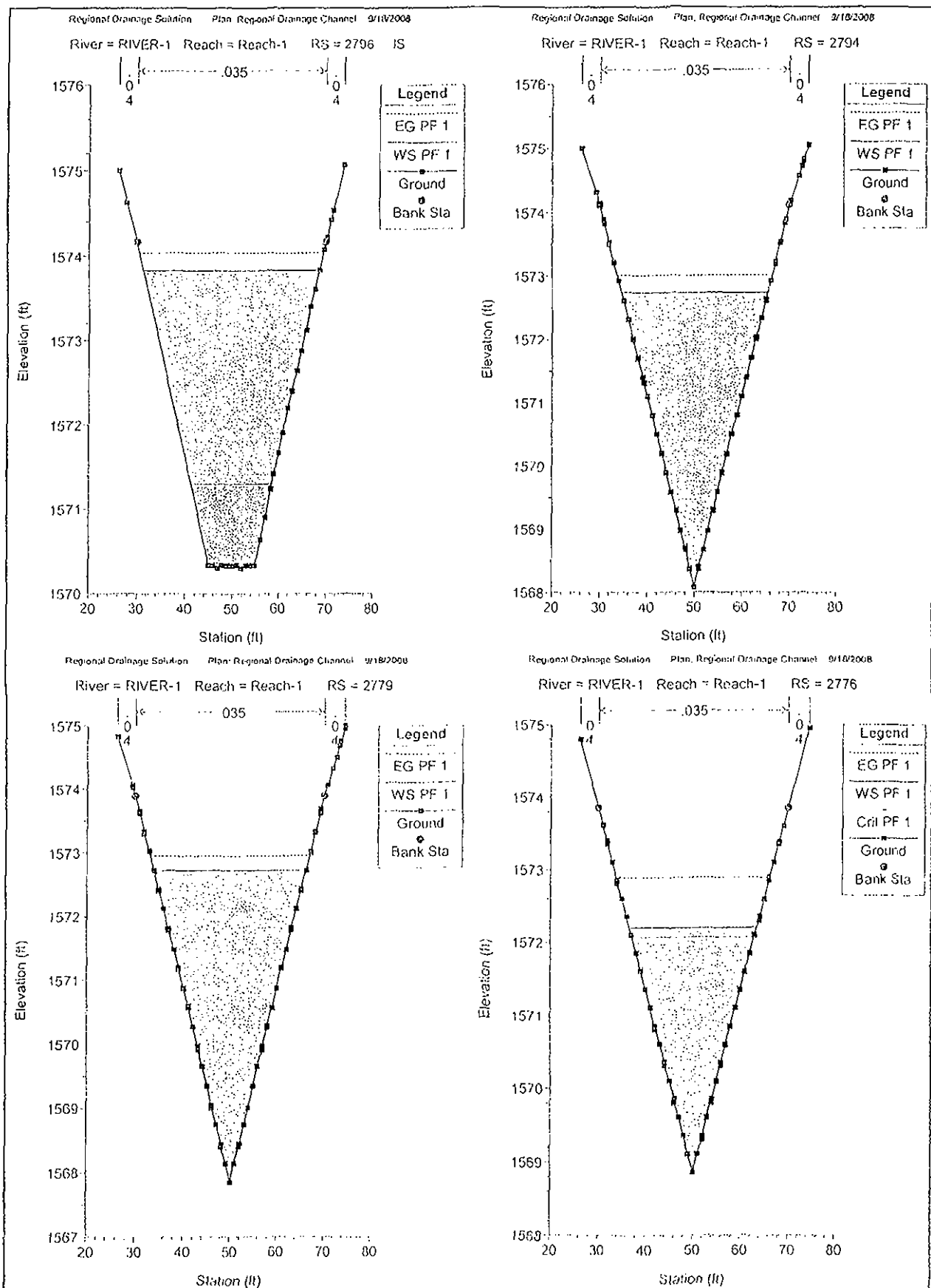
River = RIVER-1 Reach = Reach-1 RS = 3135

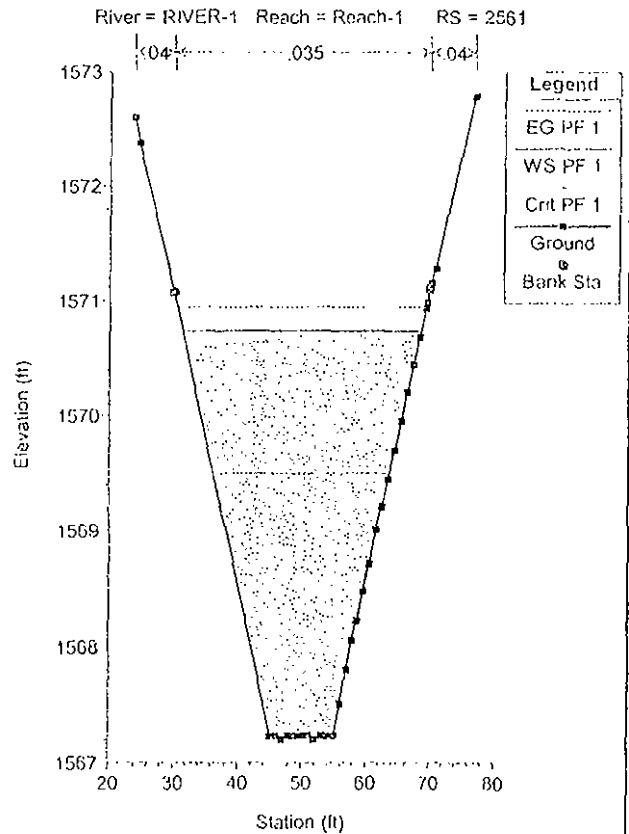
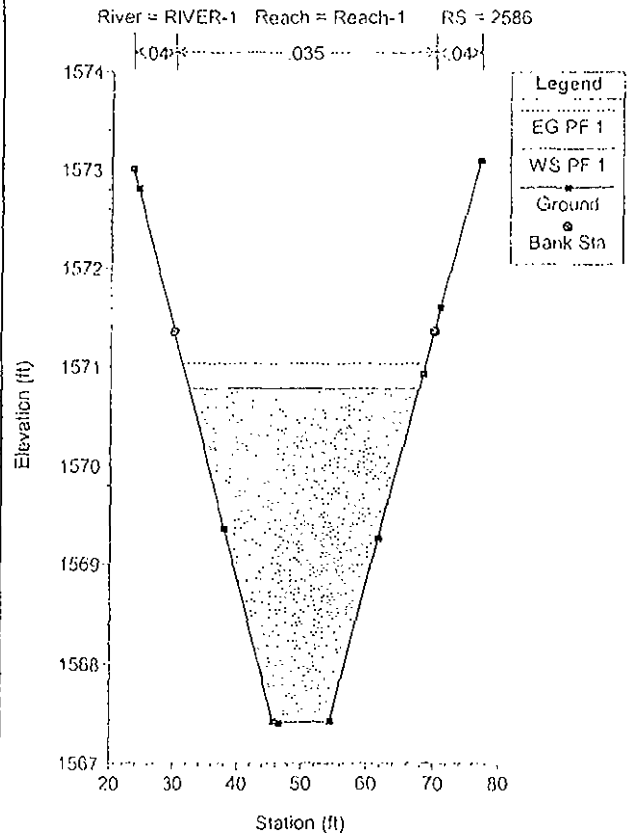
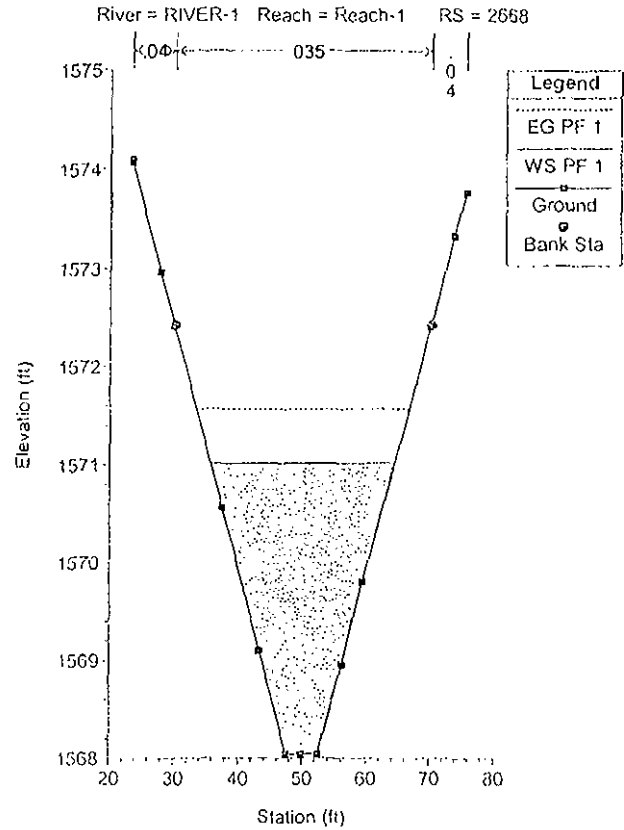
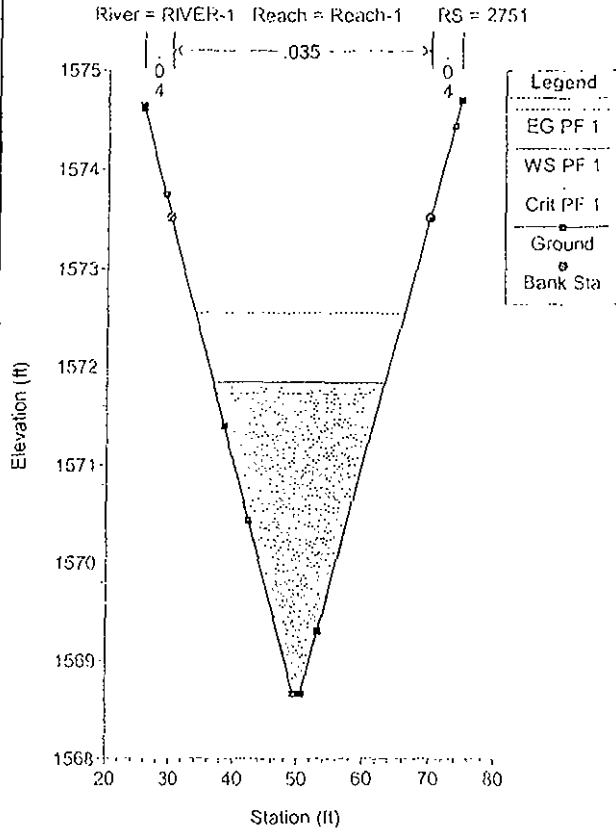


River = RIVER-1 Reach = Reach-1 RS = 3110

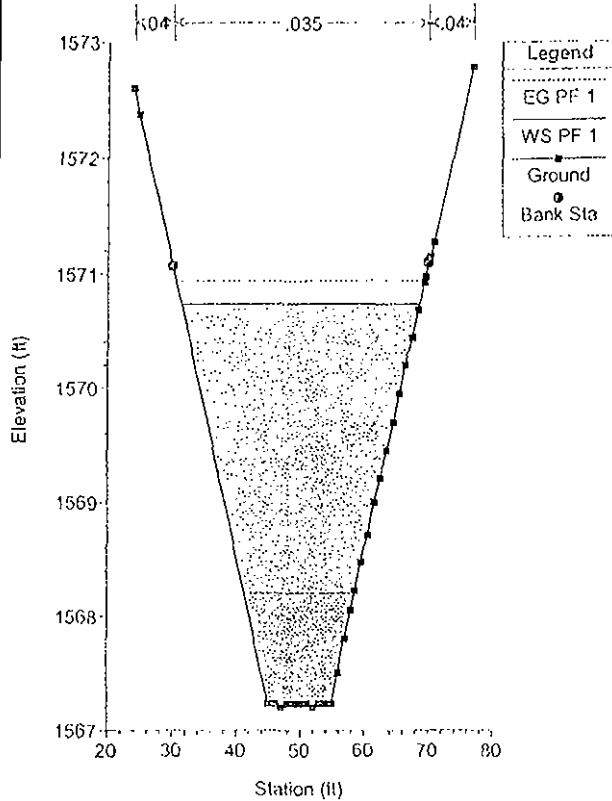




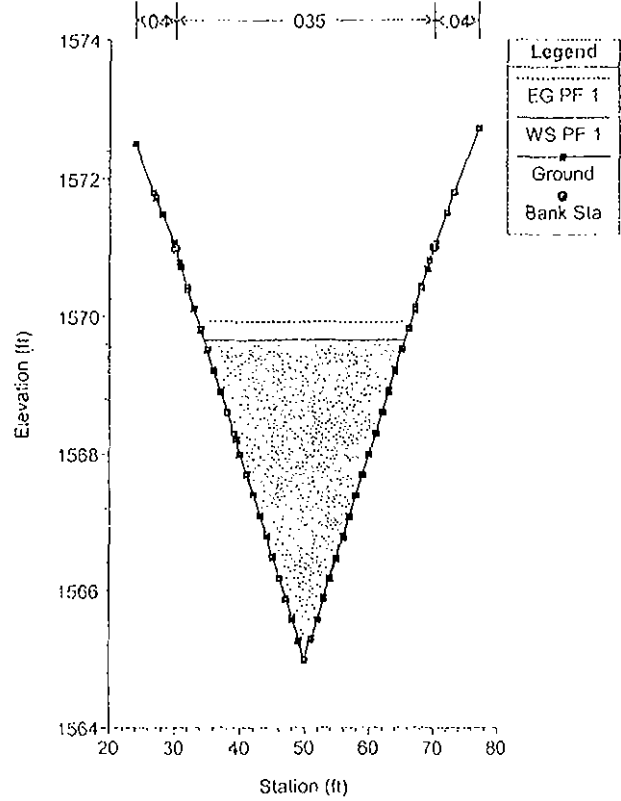




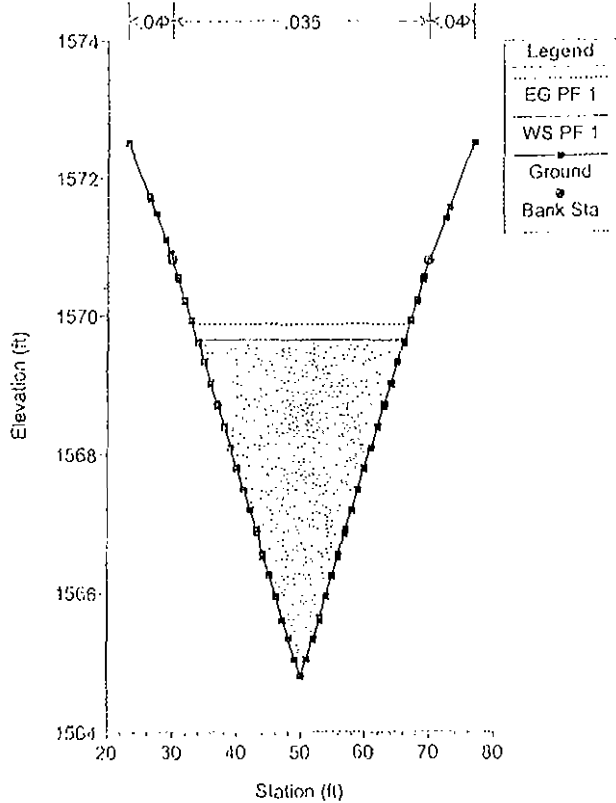
River = RIVER-1 Reach = Reach-1 RS = 2559 IS



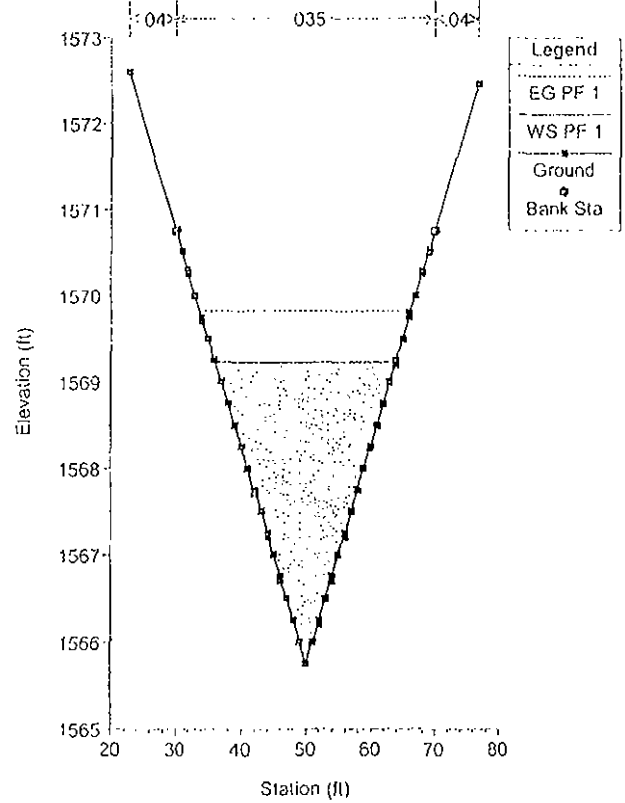
River = RIVER-1 Reach = Reach-1 RS = 2557



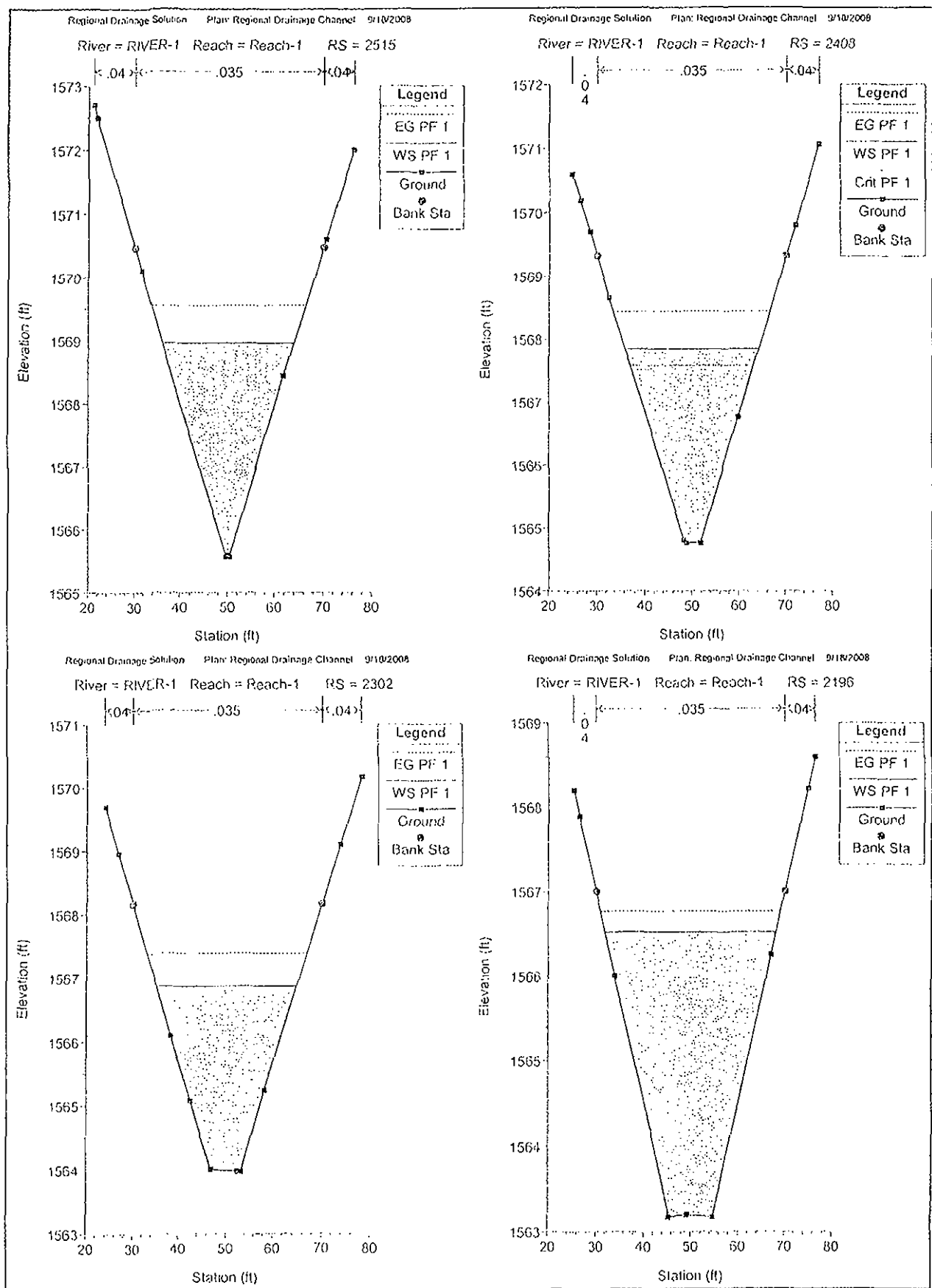
River = RIVER-1 Reach = Reach-1 RS = 2543



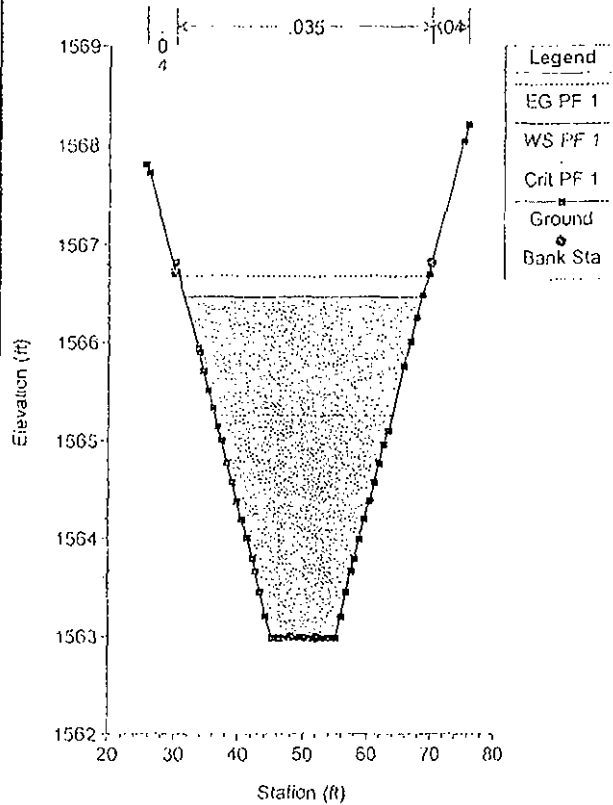
River = RIVER-1 Reach = Reach-1 RS = 2540



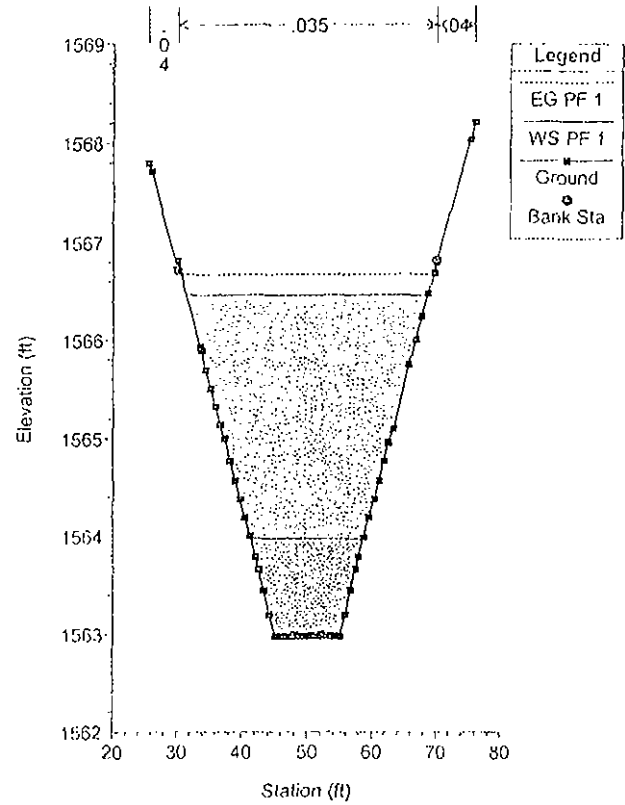




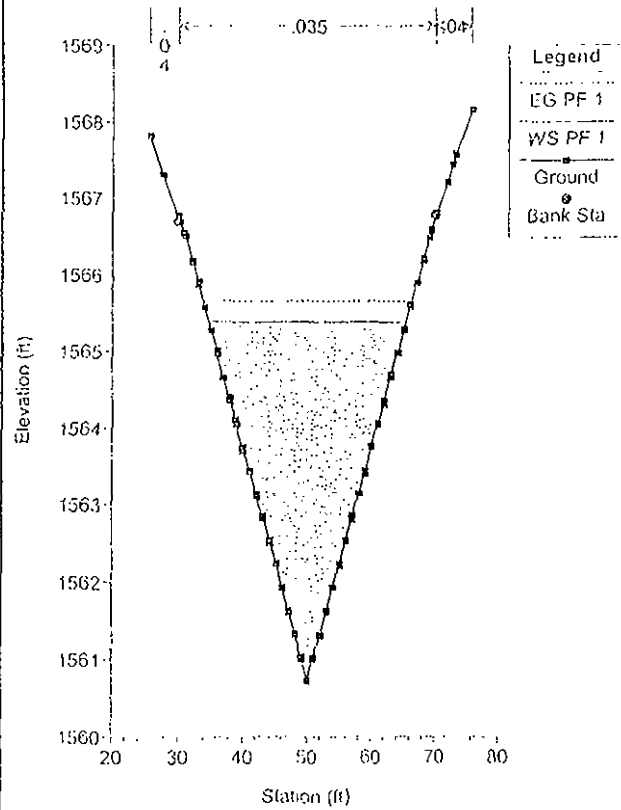
River = RIVER-1 Reach = Reach-1 RS = 2171



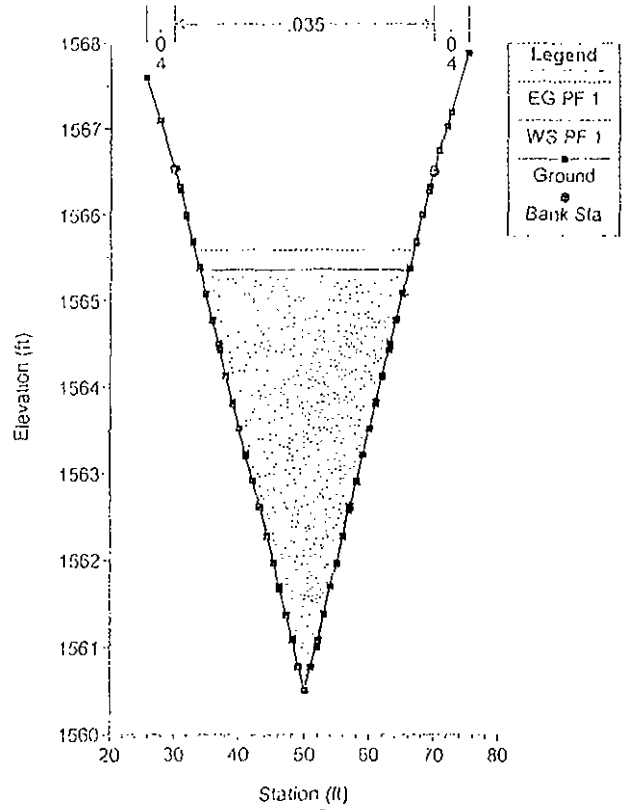
River = RIVER-1 Reach = Reach-1 RS = 2170 IS



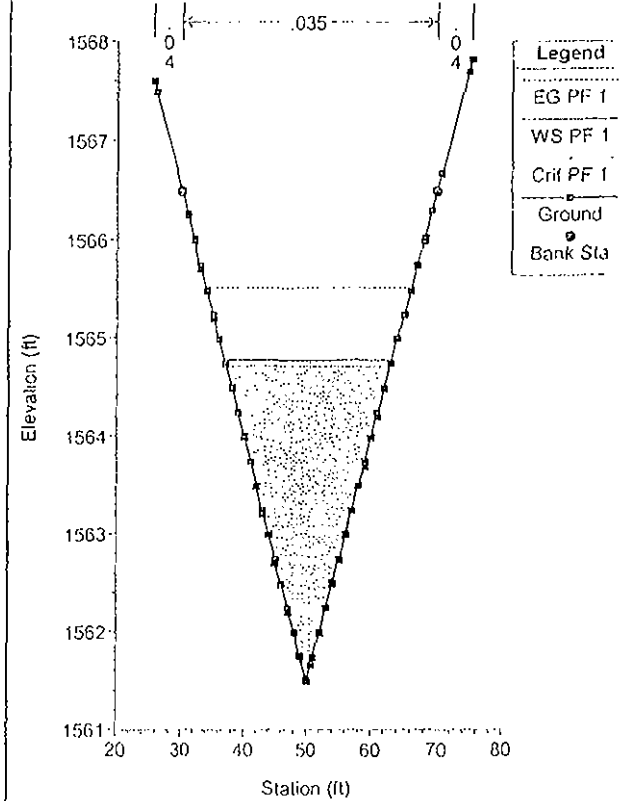
River = RIVER-1 Reach = Reach-1 RS = 2168



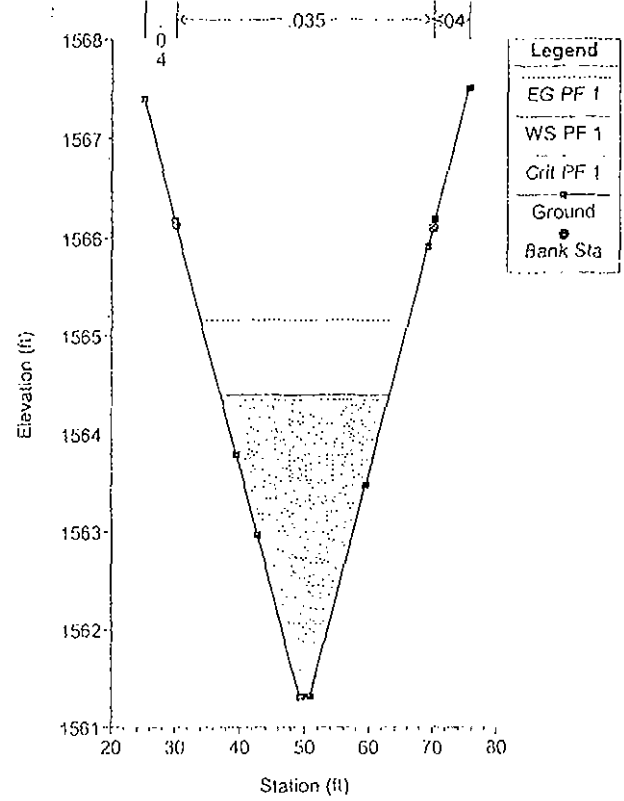
River = RIVER-1 Reach = Reach-1 RS = 2153



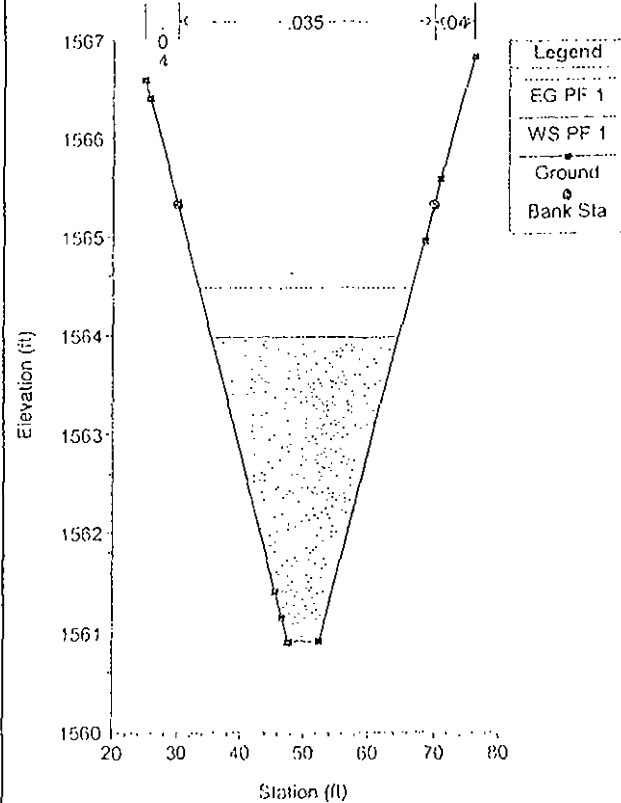
River = RIVER-1 Reach = Reach-1 RS = 2150



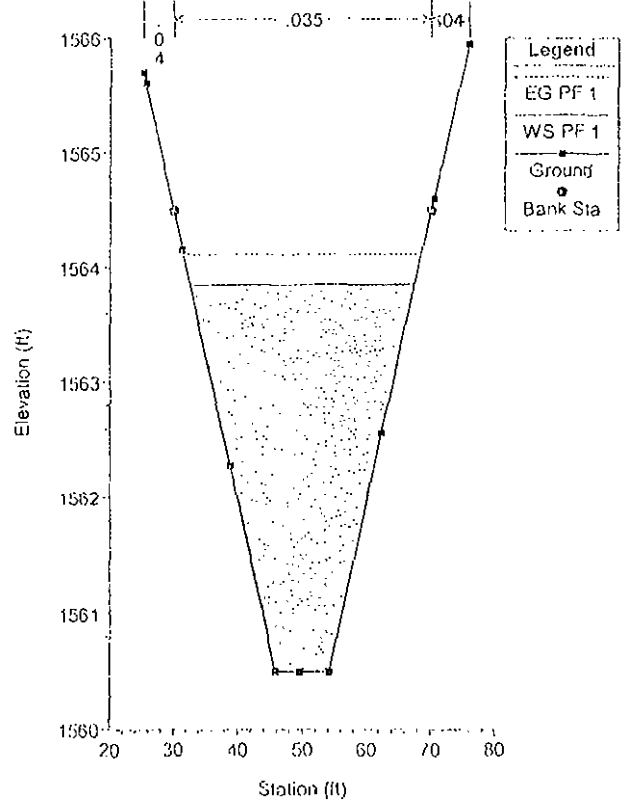
River = RIVER-1 Reach = Reach-1 RS = 2125

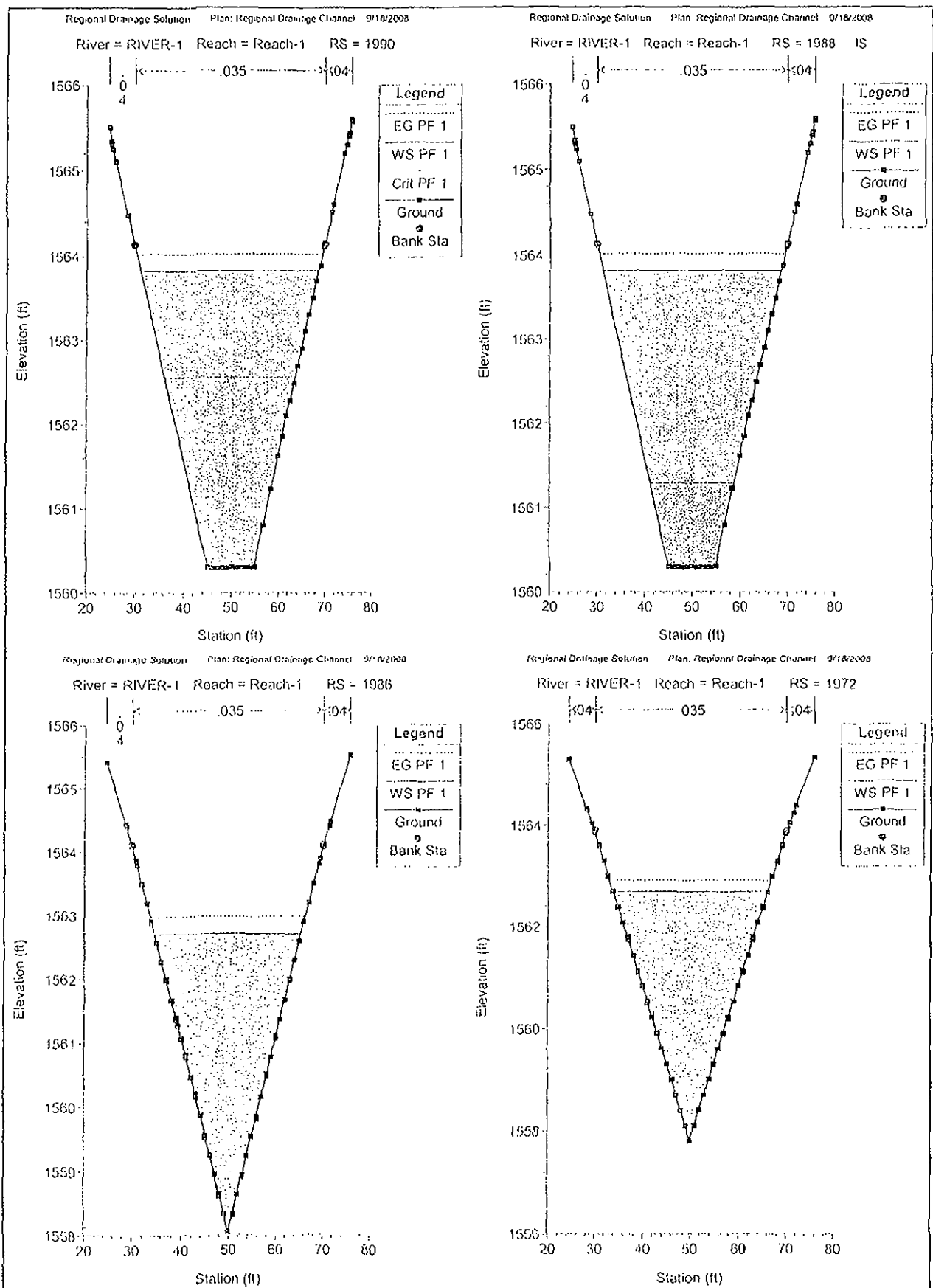


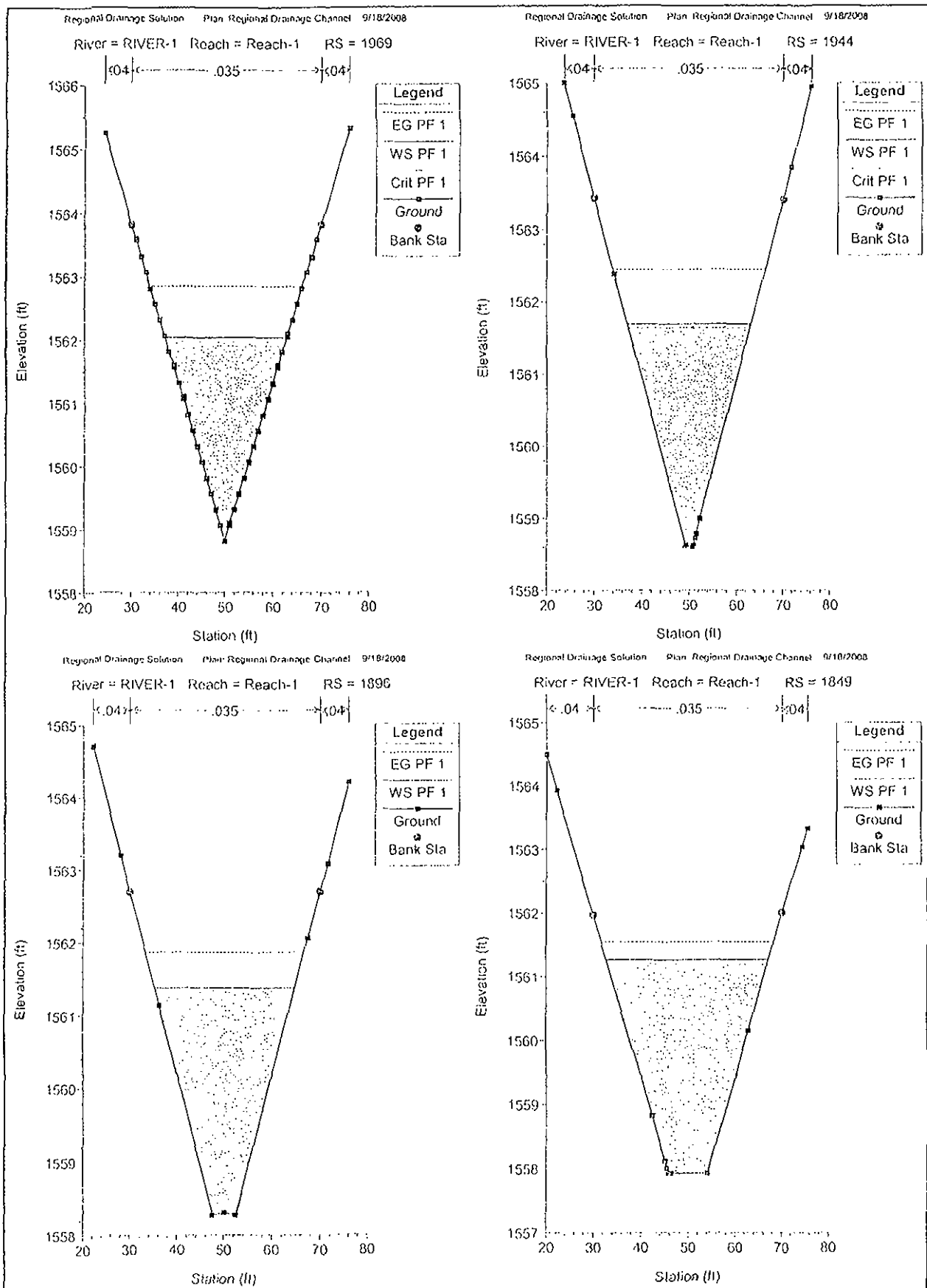
River = RIVER-1 Reach = Reach-1 RS = 2071



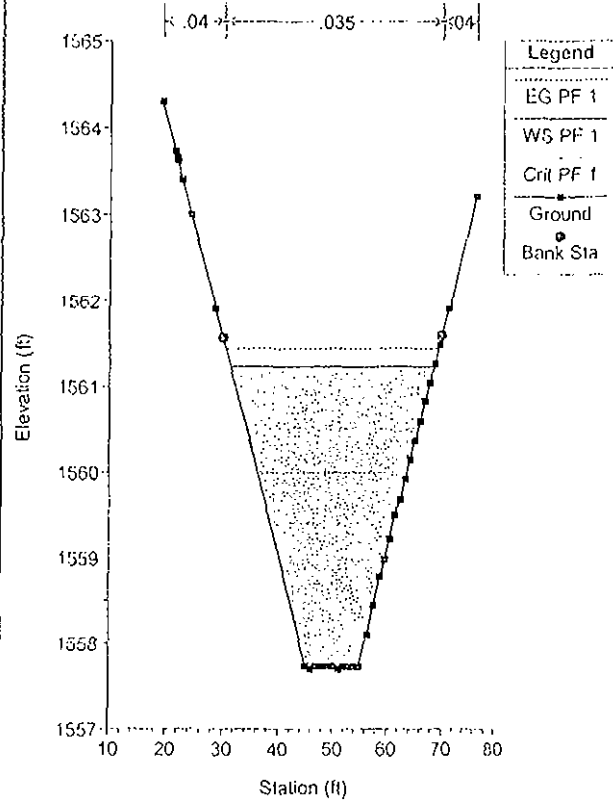
River = RIVER-1 Reach = Reach-1 RS = 2015



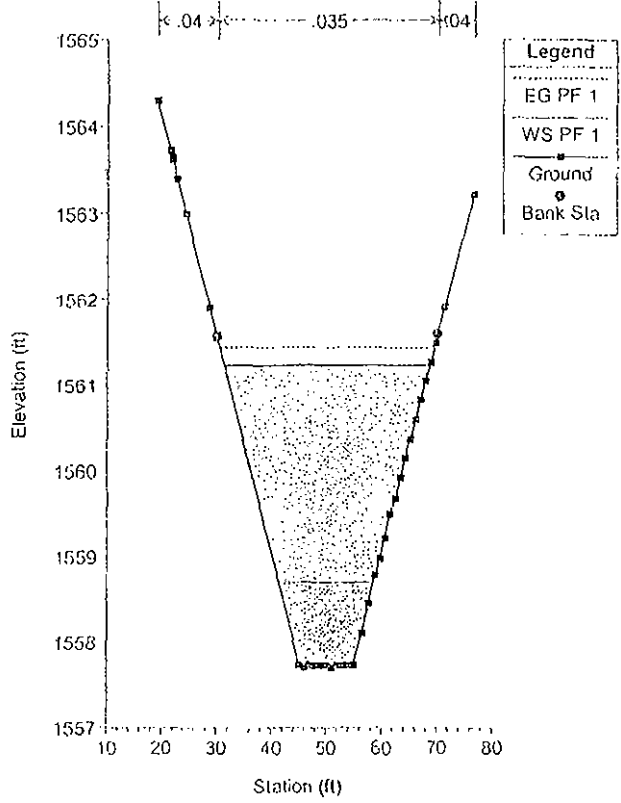




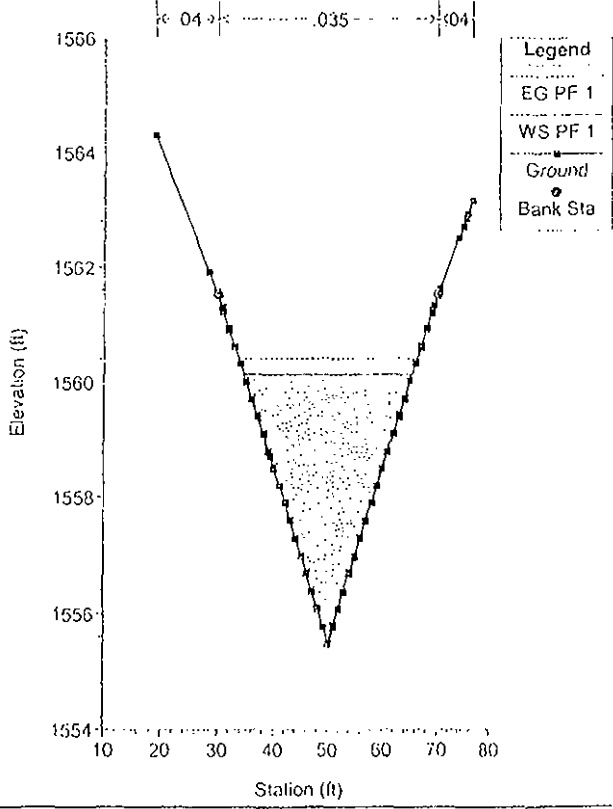
River = RIVER-1 Reach = Reach-1 RS = 1824



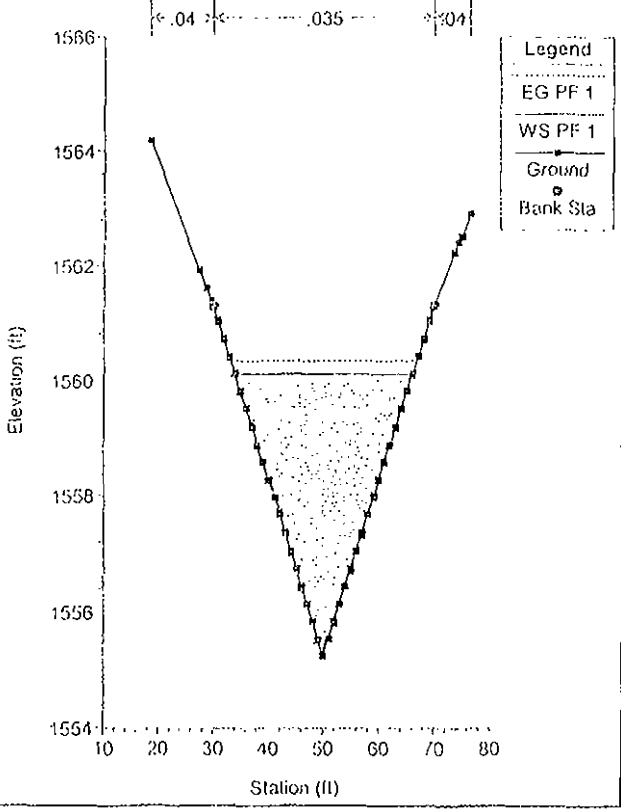
River = RIVER-1 Reach = Reach-1 RS = 1822 IS

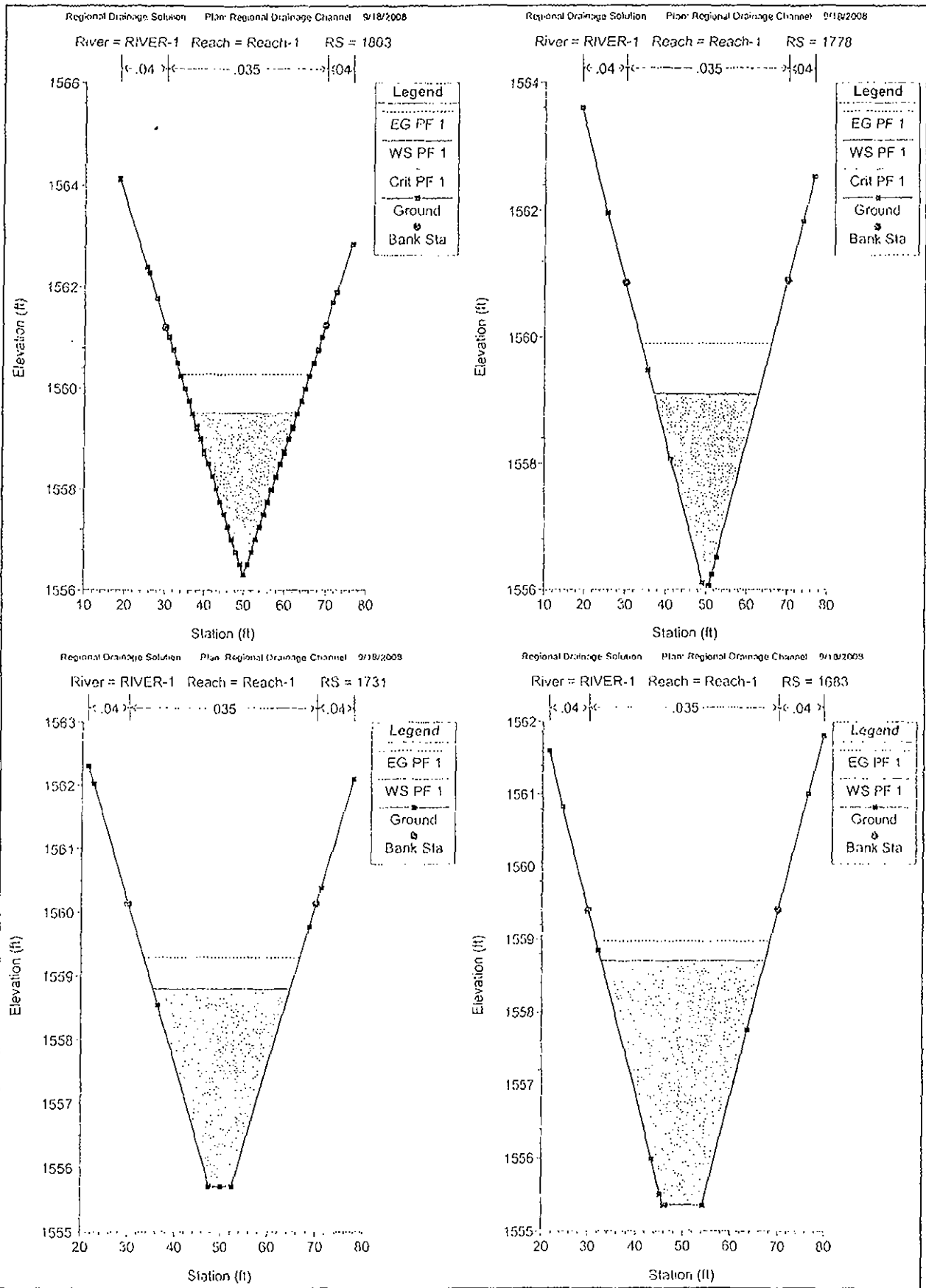


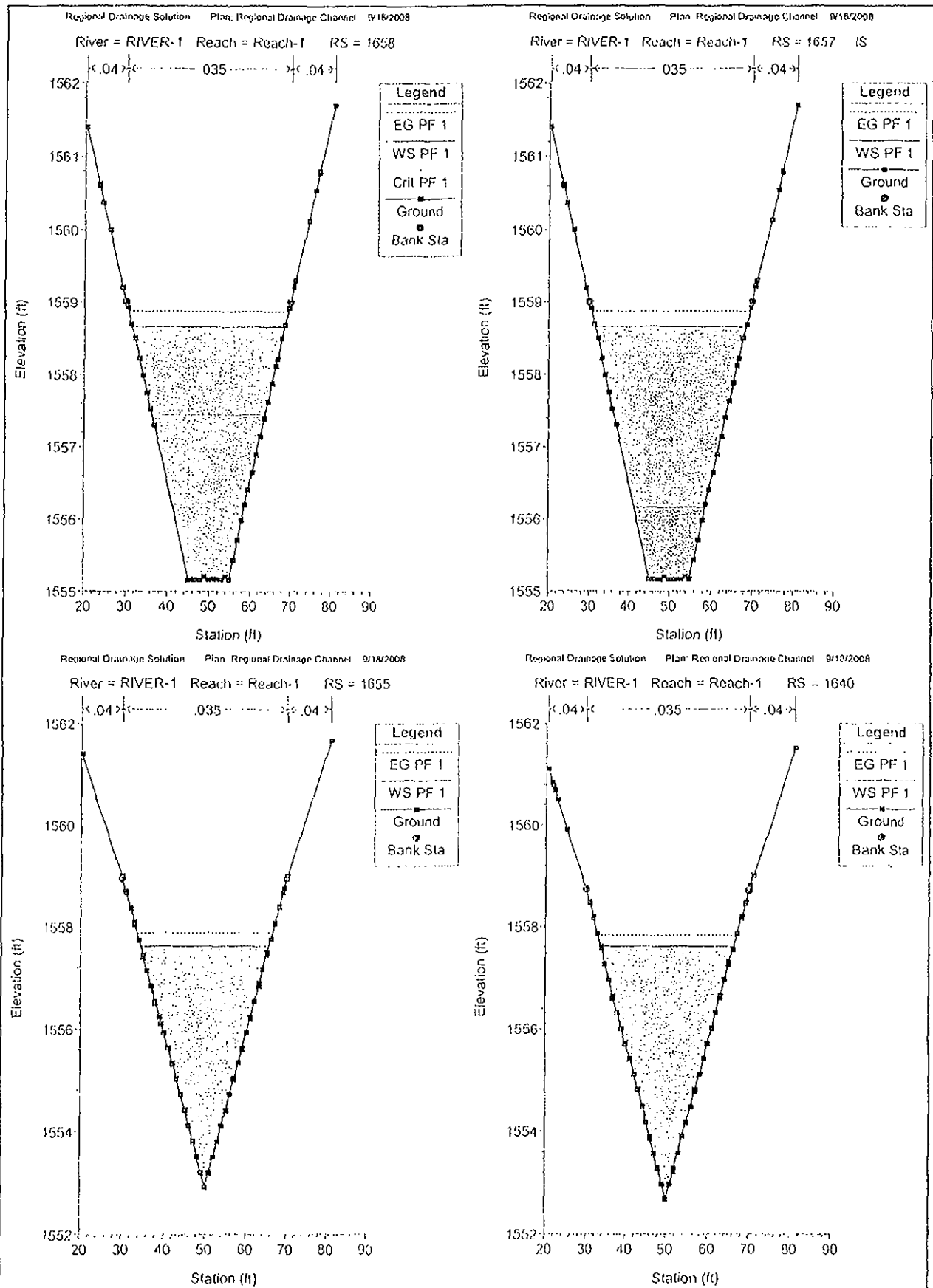
River = RIVER-1 Reach = Reach-1 RS = 1821



River = RIVER-1 Reach = Reach-1 RS = 1806

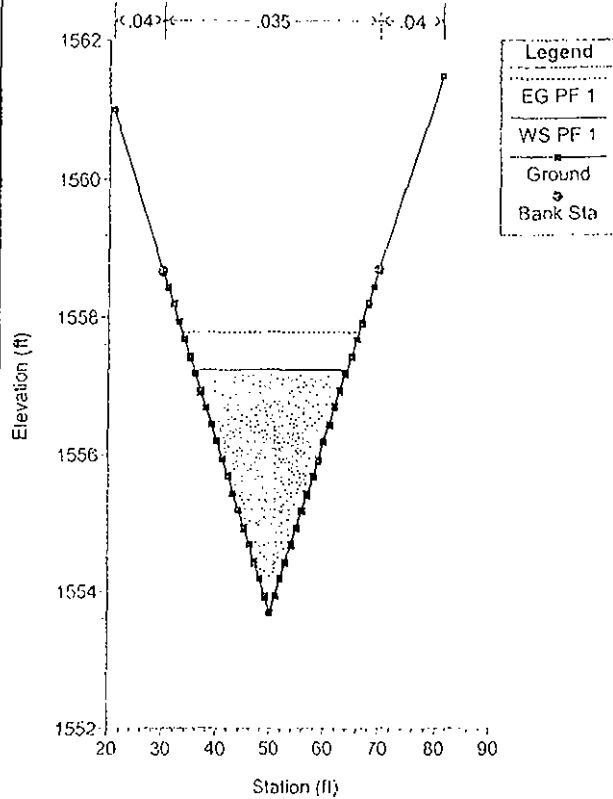




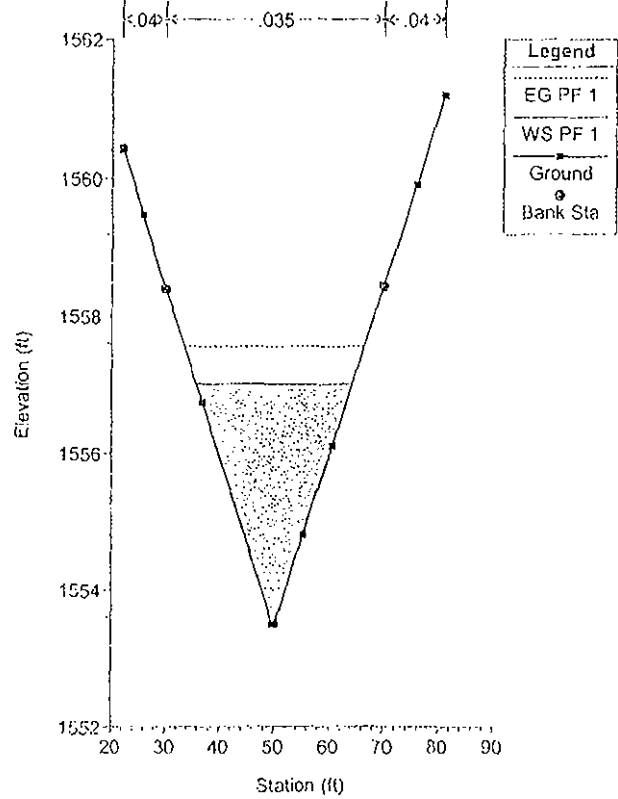




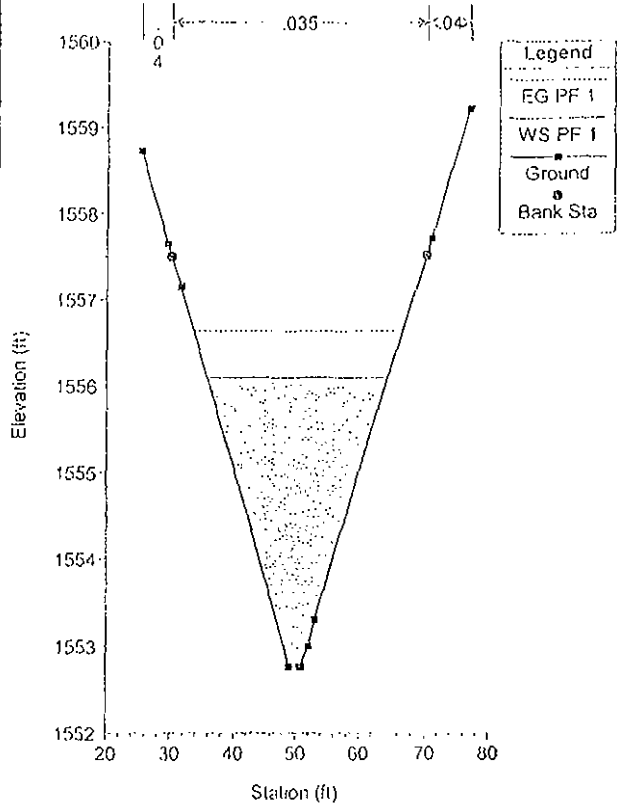
River = RIVER-1 Reach = Reach-1 RS = 1637



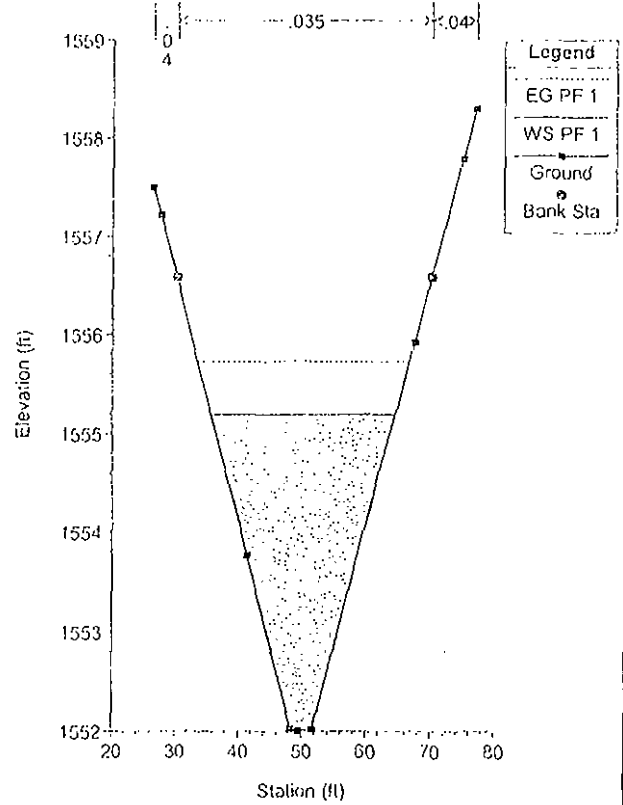
River = RIVER-1 Reach = Reach-1 RS = 1612



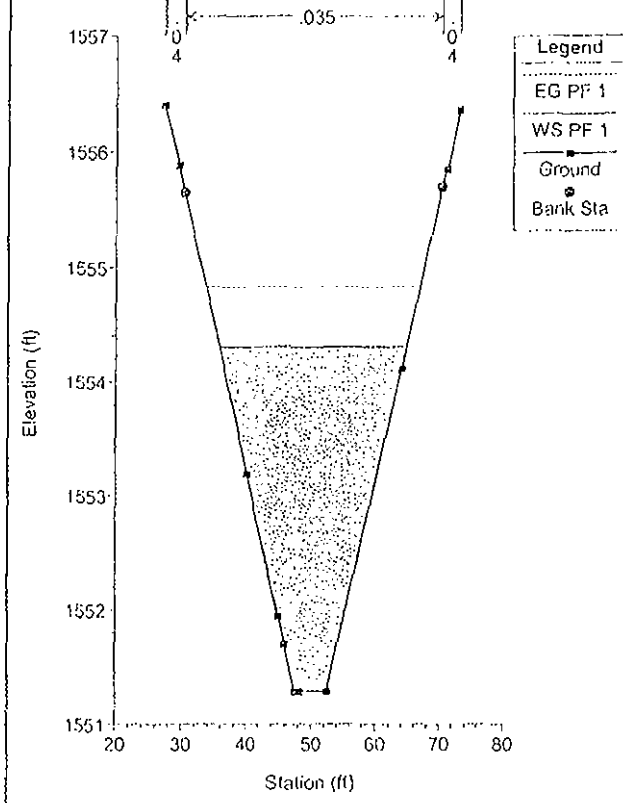
River = RIVER-1 Reach = Reach-1 RS = 1514



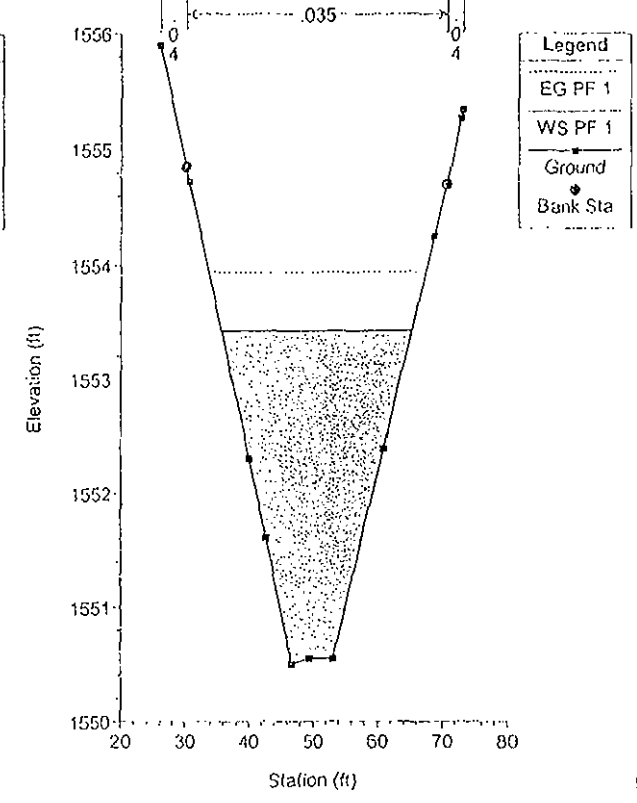
River = RIVER-1 Reach = Reach-1 RS = 1416



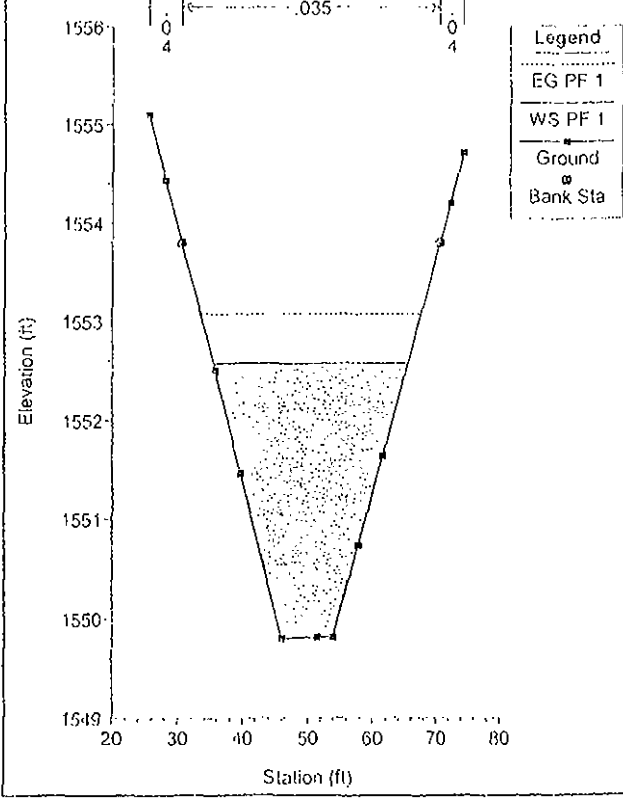
River = RIVER-1 Reach = Reach-1 RS = 1319



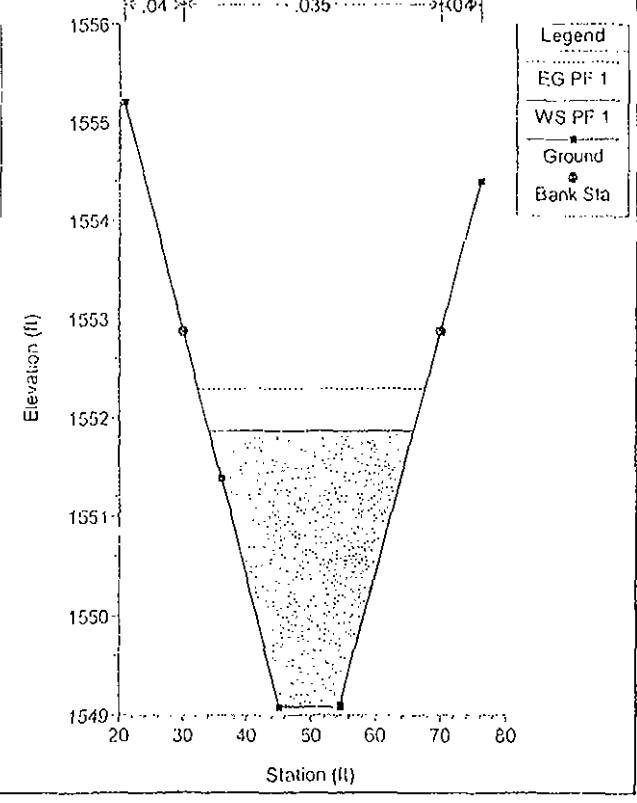
River = RIVER-1 Reach = Reach-1 RS = 1221



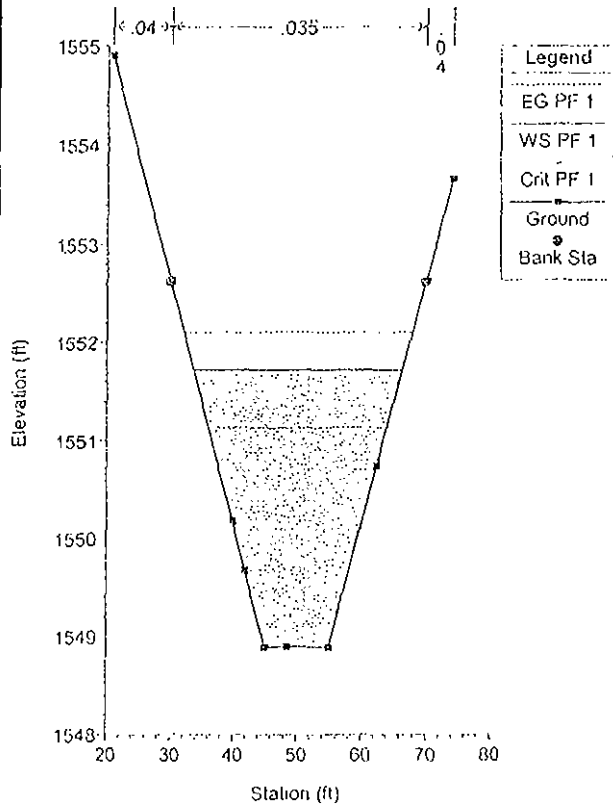
River = RIVER-1 Reach = Reach-1 RS = 1123



River = RIVER-1 Reach = Reach-1 RS = 1025



River = RIVER-1 Reach = Reach-1 RS = 1000



Plan: RDC 100yr RIVER-1 Reach-1 RS: 3581 Int Struct: Profile: PF 1

E.G. Elev (ft)	1585.25	Q Gates (cfs)	
W.S. Elev (ft)	1585.03	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1583.86
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	72.37	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	16.98	Gate Submerg	0.00
Weir Sta Rgt (ft)	47.77	Gate Invert (ft)	0.00
Weir Max Depth (ft)	3.06	Gate Weir Coef	0.000
Weir Avg Depth (ft)	2.35		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.44	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1582.20	Breach Flow Area (sq ft)	
Wt Top Width (ft)	30.79		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 3373 Int Struct: Profile: PF 1

E.G. Elev (ft)	1582.51	Q Gates (cfs)	
W.S. Elev (ft)	1582.30	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1580.88
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	73.03	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	19.30	Gate Submerg	0.00
Weir Sta Rgt (ft)	48.75	Gate Invert (ft)	0.00
Weir Max Depth (ft)	3.20	Gate Weir Coef	0.000
Weir Avg Depth (ft)	2.48		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.40	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1579.32	Breach Flow Area (sq ft)	
Wt Top Width (ft)	29.44		

#### Errors Warnings and Notes

Warning	The inline structure solution failed to converge. The program used the solution with the least error.
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Plan: RDC 100yr RIVER-1 Reach-1 RS: 3155 Int Struct: Profile: PF 1

E.G. Elev (ft)	1579.04	Q Gates (cfs)	
W.S. Elev (ft)	1578.84	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1576.77
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	77.91	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	16.94	Gate Submerg	0.00
Weir Sta Rgt (ft)	56.53	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.70	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.96		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.11	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1576.35	Breach Flow Area (sq ft)	
Wt Top Width (ft)	39.70		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 2796 Int Struct: Profile: PF 1

E.G. Elev (ft)	1574.04	Q Gates (cfs)	
W.S. Elev (ft)	1573.84	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1572.74
Q Weir (cfs)	300.00	Gate #Open	

Plan: RDC 100yr RIVER-1 Reach-1 RS: 2796 Inl Struct Profile: PF 1 (Continued)

Weir Flow Area (sq ft)	77.07	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.50	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.49	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.74	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.98		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.42	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1571.31	Breach Flow Area (sq ft)	
Wr Top Wdth (ft)	38.99		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 2559 Inl Struct Profile: PF 1

E.G. Elev (ft)	1570.94	Q Gates (cfs)	
W.S. Elev (ft)	1570.74	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1569.66
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	77.03	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.51	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.46	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.74	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.98		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.43	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1568.21	Breach Flow Area (sq ft)	
Wr Top Wdth (ft)	38.96		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 2170 Inl Struct Profile: PF 1

E.G. Elev (ft)	1566.68	Q Gates (cfs)	
W.S. Elev (ft)	1566.47	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1565.38
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	76.16	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.56	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.57	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.70	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.95		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.45	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1563.99	Breach Flow Area (sq ft)	
Wr Top Wdth (ft)	39.00		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 1988 Inl Struct Profile: PF 1

E.C. Elev (ft)	1564.02	Q Gates (cfs)	
W.S. Elev (ft)	1563.82	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1562.70
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	77.23	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.44	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.44	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.73	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.98		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.41	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1561.30	Breach Flow Area (sq ft)	

Plan: RDC 100yr RIVER-1 Reach-1 RS: 1988 Inl Struct: Profile: PF 1 (Continued)

Wr Top Width (ft)	39.01		
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Plan: RDC 100yr RIVER-1 Reach-1 RS: 1822 Inl Struct: Profile: PF 1

E.G. Elev (ft)	1561.44	Q Gates (cfs)	
W.S. Elev (ft)	1561.24	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1560.14
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	77.05	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.50	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.47	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.74	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.98		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.42	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1558.71	Breach Flow Area (sq ft)	
Wr Top Width (ft)	38.97		

Plan: RDC 100yr RIVER-1 Reach-1 RS: 1657 Inl Struct: Profile: PF 1

E.G. Elev (ft)	1558.87	Q Gates (cfs)	
W.S. Elev (ft)	1558.66	Q Gate Group (cfs)	0.00
Q Total (cfs)	300.00	Gate Open Ht (ft)	1557.63
Q Weir (cfs)	300.00	Gate #Open	
Weir Flow Area (sq ft)	76.02	Gate Area (sq ft)	1.00
Weir Sta Lft (ft)	30.54	Gate Submerg	0.00
Weir Sta Rgt (ft)	69.46	Gate Invert (ft)	0.00
Weir Max Depth (ft)	2.71	Gate Weir Coef	0.000
Weir Avg Depth (ft)	1.95		
Weir Coef	2.600	Q Breach (cfs)	
Weir Submerg	0.47	Breach Avg Velocity (ft/s)	
Min El Weir Flow (ft)	1556.17	Breach Flow Area (sq ft)	
Wr Top Width (ft)	38.91		

# Culvert Calculator Report

## RDC Outfall 100yr

Solve For: Headwater Elevation

Culvert Summary			
Allowable HW Elevation	1,552.00 ft	Headwater Depth/Height	1.37
Computed Headwater Elev.	1,551.73 ft	Discharge	300.00 cfs
Inlet Control HW Elev.	1,551.51 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	1,551.73 ft	Control Type	Entrance Control

Grades			
Upstream Invert	1,547.62 ft	Downstream Invert	1,545.80 ft
Length	375.00 ft	Constructed Slope	0.004853 ft/ft

Hydraulic Profile			
Profile	S2	Depth, Downstream	1.96 ft
Slope Type	Steep	Normal Depth	1.96 ft
Flow Regime	Supercritical	Critical Depth	2.22 ft
Velocity Downstream	9.56 ft/s	Critical Slope	0.003401 ft/ft

Section			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	8.00 ft
Section Size	8 x 3 ft	Rise	3.00 ft
Number Sections	2		

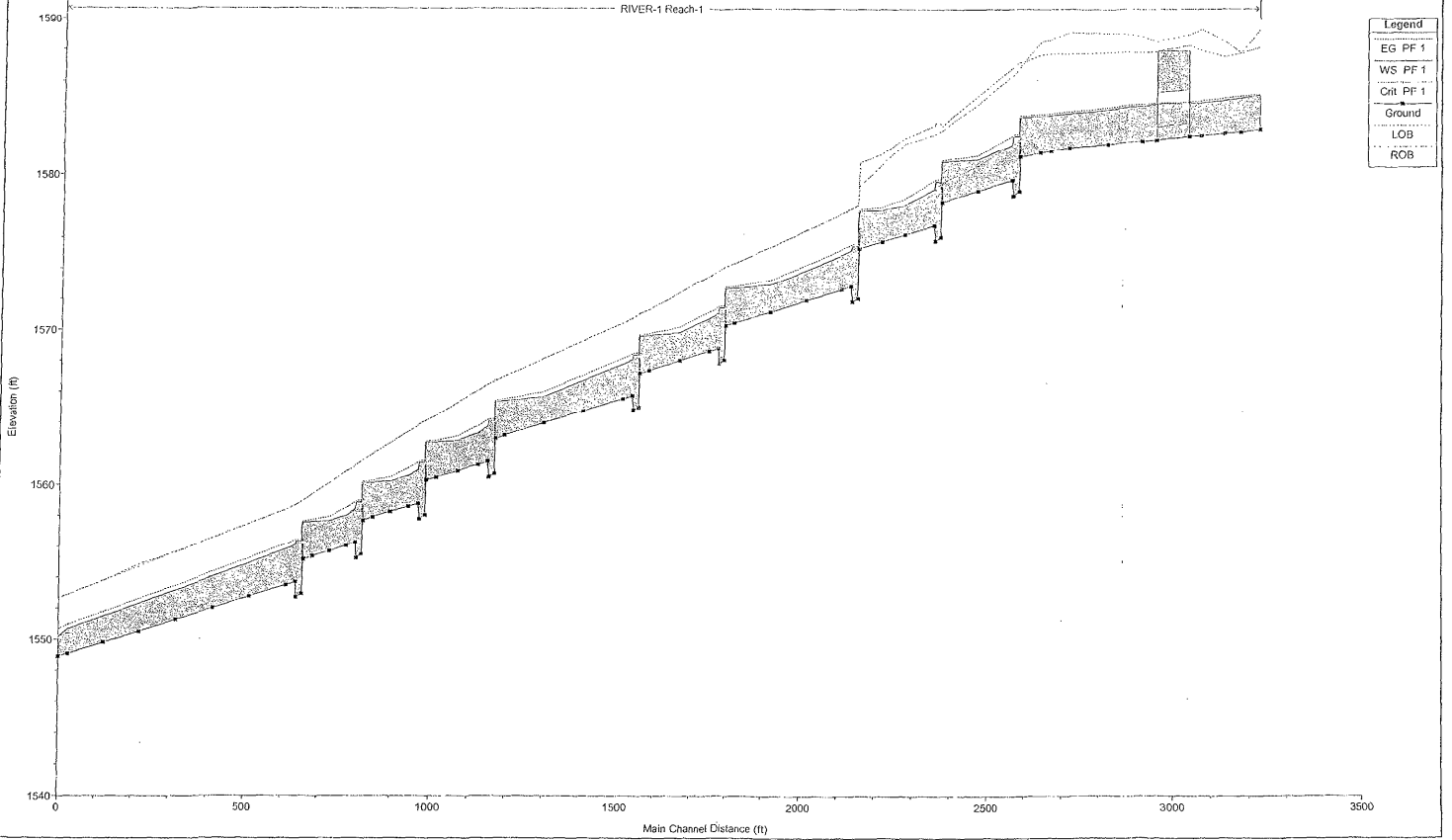
Outlet Control Properties			
Outlet Control HW Elev.	1,551.73 ft	Upstream Velocity Head	1.11 ft
Ke	0.70	Entrance Loss	0.78 ft

Inlet Control Properties			
Inlet Control HW Elev.	1,551.51 ft	Flow Control	Transition
Inlet Type	0° wingwall flares	Area Full	48.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

HEC-RAS Plan: RDC 10yr River: RIVER-1 Reach: Reach-1 Profile: PF 1																
River Sta	Q Total (cfs)	Min Ch El (ft)	W.S. Elev (ft)	E.G. Elev (ft)	E.G. Slope (ft/m)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Froude # Chl	LOB Elev (ft)	ROB Elev (ft)	Flow Depth (ft)	Freeboard Req	Freeboard Prov		
4222	105.00	1582.97	1585.13	1585.17	0.000576	1.53	68.79	36.28	0.20	1588.20	1589.30	2.16	1.00	3.07		
4172	105	1582.80	1584.97	1585.10	0.002851	2.97	35.35	22.87	0.42	1587.82	1587.84	2.17	1.00	2.85		
4130	105	1582.73	1584.84	1584.98	0.003072	3.04	34.50	22.78	0.44	1587.60	1588.56	2.11	1.00	2.76		
4070	105	1582.59	1584.67	1584.80	0.002829	2.93	35.78	23.47	0.42	1588.00	1589.33	2.09	1.00	3.33		
4039	105	1582.53	1584.68	1584.73	0.000866	1.88	55.86	26.06	0.23	1588.33	1588.98	2.15	1.00	3.65		
4004	Culvert															
3953	105	1582.33	1584.63	1584.67	0.000701	1.76	59.80	26.06	0.20	1587.99	1588.61	2.30	1.00	3.36		
3915	105	1582.25	1584.50	1584.62	0.002423	2.81	37.38	23.22	0.39	1587.90	1588.90	2.25	1.00	3.40		
3819	105	1582.04	1584.26	1584.38	0.002524	2.84	36.96	23.33	0.40	1587.90	1589.11	2.22	1.00	3.64		
3715	105	1581.80	1583.98	1584.11	0.002715	2.92	35.99	23.06	0.41	1587.80	1589.14	2.18	1.00	3.82		
3663	105	1581.57	1583.87	1583.98	0.002203	2.70	38.84	23.84	0.37	1587.80	1588.70	2.30	1.00	3.93		
3635	105	1581.44	1583.81	1583.92	0.001941	2.58	40.64	24.27	0.35	1587.70	1589.57	2.37	1.00	3.89		
3582	105	1581.19	1583.75	1583.83	0.001308	2.30	45.62	23.80	0.29	1587.23	1587.03	2.56	1.00	3.28		
3501	Int Struct															
3579	105	1578.96	1582.52	1582.67	0.002612	3.10	33.89	18.55	0.40	1587.24	1586.88	3.56	1.00	4.36		
3564	105	1578.70	1582.52	1582.62	0.001559	2.49	42.23	22.09	0.32	1587.02	1586.40	3.82	1.00	3.88		
3581	105	1579.71	1581.98	1582.56	0.018555	6.11	17.18	15.14	1.01	1586.89	1586.40	2.27	1.00	4.42		
3467	105	1579.00	1581.01	1581.26	0.006804	3.90	26.31	21.14	0.63	1585.10	1584.55	2.01	1.00	3.54		
3374	105	1578.30	1580.89	1580.98	0.001296	2.33	45.07	22.76	0.29	1583.20	1582.91	2.59	1.00	2.02		
3373	Int Struct															
3371	105	1576.07	1579.59	1579.80	0.004030	3.70	28.34	16.12	0.49	1583.36	1582.90	3.52	1.00	3.31		
3356	105	1575.82	1579.63	1579.73	0.001646	2.55	41.25	21.67	0.35	1583.42	1582.70	3.81	1.00	3.07		
3353	105	1576.82	1579.12	1579.67	0.017321	5.96	17.62	15.32	0.98	1583.22	1582.64	2.30	1.00	3.52		
3276	105	1576.24	1578.11	1578.50	0.012316	5.01	20.97	18.69	0.83	1582.40	1582.03	1.87	1.00	3.92		
3216	105	1575.79	1577.82	1578.01	0.004652	3.43	30.57	23.21	0.53	1581.40	1580.73	2.03	1.00	2.91		
3156	105	1575.34	1577.75	1577.83	0.001469	2.21	47.48	29.38	0.31	1580.80	1579.34	2.41	1.00	1.59		
3155	Int Struct															
3152	105	1572.09	1575.51	1575.63	0.002130	2.71	38.71	22.68	0.37	1578.10	1578.13	3.42	1.00	2.59		
3130	105	1571.86	1575.50	1575.59	0.001522	2.39	43.91	24.10	0.31	1577.91	1577.91	3.64	1.00	2.41		
3133	105	1572.86	1575.19	1575.55	0.011170	4.84	21.70	18.69	0.79	1577.86	1577.90	2.33	1.00	2.67		
3110	105	1572.67	1574.92	1575.28	0.010755	4.79	21.91	18.74	0.78	1577.58	1577.58	2.25	1.00	2.66		
3014	105	1571.95	1573.91	1574.25	0.010566	4.73	22.21	19.20	0.77	1576.51	1576.51	1.96	1.00	2.60		
2918	105	1571.20	1573.00	1573.30	0.009150	4.42	23.78	20.49	0.72	1575.43	1575.43	1.80	1.00	2.43		
2822	105	1570.50	1572.76	1572.86	0.002107	2.57	40.84	27.16	0.37	1574.36	1574.36	2.26	1.00	1.80		
2797	105	1570.30	1572.73	1572.81	0.001569	2.28	46.08	28.60	0.32	1574.17	1574.17	2.43	1.00	1.44		
2796	Int Struct															
2794	105	1568.08	1571.47	1571.59	0.002228	2.76	38.07	22.48	0.37	1574.12	1574.12	3.39	1.00	2.65		
2779	105	1567.85	1571.47	1571.56	0.001577	2.42	43.32	23.90	0.32	1573.90	1573.90	3.62	1.00	2.43		
2778	105	1568.85	1571.11	1571.52	0.012857	5.09	20.82	18.12	0.84	1573.85	1573.85	2.28	1.00	2.74		
2751	105	1568.66	1570.78	1571.19	0.013134	5.16	20.34	18.08	0.86	1573.52	1573.52	2.12	1.00	2.74		
2668	105	1568.04	1569.85	1570.20	0.010667	4.73	22.21	19.30	0.78	1572.43	1572.43	1.81	1.00	2.58		
2586	105	1567.40	1569.66	1569.77	0.002339	2.65	39.68	26.58	0.38	1571.35	1571.35	2.26	1.00	1.69		
2561	105	1567.20	1569.63	1569.71	0.001574	2.28	46.03	28.60	0.32	1571.07	1571.10	2.43	1.00	1.44		
2539	Int Struct															
2557	105	1564.98	1568.40	1568.51	0.002147	2.72	38.60	22.63	0.37	1571.06	1571.02	3.42	1.00	2.60		
2543	105	1564.80	1568.39	1568.48	0.001526	2.40	43.80	24.01	0.31	1570.86	1570.80	3.59	1.00	2.41		
2540	105	1565.75	1568.09	1568.44	0.010724	4.76	22.08	18.76	0.77	1570.75	1570.75	2.34	1.00	2.66		
2515	105	1565.56	1567.83	1568.10	0.010577	4.76	22.06	18.81	0.77	1570.47	1570.47	2.27	1.00	2.64		
2408	105	1564.76	1566.76	1567.09	0.009827	4.60	22.80	19.44	0.75	1569.32	1569.32	2.00	1.00	2.56		
2302	105	1563.97	1565.69	1566.02	0.010257	4.60	22.84	20.25	0.76	1568.16	1568.16	1.72	1.00	2.47		
2196	105	1563.17	1565.42	1565.52	0.002158	2.55	41.11	27.34	0.37	1567.00	1567.00	2.25	1.00	1.58		
2171	105	1562.98	1565.39	1565.47	0.001567	2.27	46.23	28.80	0.32	1566.72	1566.82	2.41	1.00	1.33		
2170	Int Struct															
2160	105	1560.72	1564.11	1564.23	0.002236	2.76	38.10	22.46	0.37	1566.69	1566.77	3.39	1.00	2.58		
2153	105	1560.50	1564.10	1564.20	0.001615	2.44	42.95	23.88	0.32	1566.53	1566.50	3.60	1.00	2.40		
2150	105	1561.49	1563.72	1564.15	0.014208	5.29	19.86	17.90	0.88	1566.49	1566.49	2.23	1.00	2.77		
2125	105	1561.30	1563.32	1563.78	0.015240	5.47	19.21	17.54	0.92	1566.13	1566.10	2.02	1.00	2.78		
2071	105	1560.90	1562.85	1563.13	0.008222	4.29	24.47	20.31	0.69	1565.33	1565.33	1.95	1.00	2.48		
2015	105	1560.49	1562.73	1562.85	0.002487	2.71	38.70	26.11	0.39	1564.45	1564.49	2.24	1.00	1.76		
1990	105	1560.29	1562.71	1562.79	0.001522	2.25	46.61	28.76	0.31	1564.13	1564.13	2.42	1.00	1.42		
1988	Int Struct															
1986	105	1558.04	1561.43	1561.55	0.002241	2.76	38.07	22.34	0.37	1564.10	1564.00	3.39	1.00	2.65		
1972	105	1557.81	1561.42	1561.61	0.001587	2.43	43.20	23.89	0.32	1563.90	1563.86	3.61	1.00	2.44		
1969	105	1558.81	1560.99	1561.46	0.015562	5.50	19.08	17.41	0.93	1563.81	1563.81	2.18	1.00	2.82		
1944	105	1558.60	1560.60	1561.07	0.015615	5.51	19.06	17.52	0.93	1563.43	1563.40	2.00	1.00	2.80		
1895	105	1558.27	1560.24	1560.51	0.007838	4.17	25.17	20.61	0.67	1562.69	1562.69	1.97	1.00	2.45		
1849	105	1557.92	1560.15	1560.27	0.002592	2.76	38.04	25.81	0.40	1561.96	1562.00	2.23	1.00	1.01		
1824	105	1557.70	1560.13	1560.21	0.001571	2.29	46.04	29.56	0.32	1561.57	1561.60	2.43	1.00	1.44		
1822	Int Struct															
1821	105	1555.48	1558.88	1558.99	0.002224	2.76	38.09	22.49	0.37	1561.52	1561.52	3.40	1.00	2.64		
1806	105	1555.25	1558.87	1558.96	0.001595	2.43	43.26	23.91	0.32	1561.30	1561.30	3.62	1.00	2.43		
1803	105	1556.30	1558.48	1558.91	0.014540	5.36	19.59	17.75	0.90	1561.20	1561.25	2.16	1.00	2.74		
1778	105	1556.06	1558.03	1558.52	0.016815	5.63	18.65	17.40	0.96	1560.86	1560.90	1.97	1.00	2.83		
1731	105	1555.70	1557.69	1557.95	0.007342	4.11	25.52	20.73	0.65	1560.13	1560.13	1.99	1.00	2.44		
1683	105	1555.35	1557.60	1557.72	0.002481	2.72	38.65	25.98	0.39	1559.39	1559.40	2.25	1.00	1.79		
1658	105	1555.16	1557.58	1557.66	0.001562	2.28	46.14	28.59	0.32	1559.00	1559.00	2.42	1.00	1.42		
1657	Int Struct															
1655	105	1552.91	1556.36	1556.47	0.002036	2.66	39.42	22.88	0.36	1560.95	1560.85	3.45	1.00	2.59		
1640	105	1552.68	1556.35	1556.44	0.001473	2.36	44.45	24.27	0.31	1560.73	1560.70	3.67	1.00	2.35		
1637	105	1553.68	1556.00	1556.40	0.009380	4.53	23.19	19.30	0.73	1560.68	1560.70	2.40	1.00	2.60		
1612	105	1553.49	1555.85	1556.17	0.009400											



RIVER-1 Reach-1



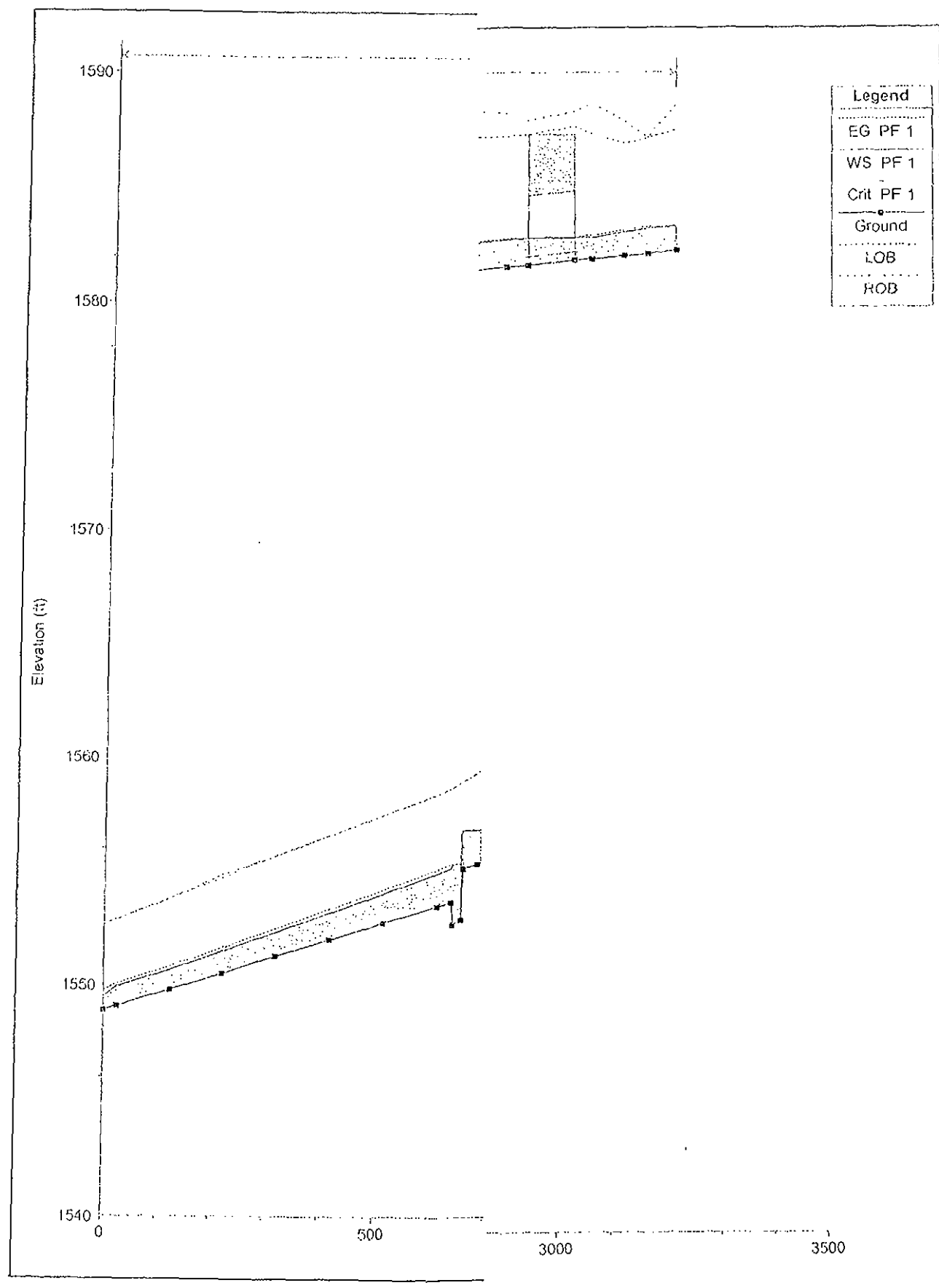
# Culvert Calculator Report

## RDC Outfall 10yr

Solve For: Headwater Elevation

<b>Culvert Summary</b>			
Allowable HW Elevation	1,552.00 ft	Headwater Depth/Height	0.68
Computed Headwater Elev.	1,549.66 ft	Discharge	105.00 cfs
Inlet Control HW Elev.	1,549.48 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	1,549.66 ft	Control Type	Entrance Control
<b>Grades</b>			
Upstream Invert	1,547.62 ft	Downstream Invert	1,545.80 ft
Length	375.00 ft	Constructed Slope	0.004853 ft/ft
<b>Hydraulic Profile</b>			
Profile	S2	Depth, Downstream	0.97 ft
Slope Type	Sleep	Normal Depth	0.97 ft
Flow Regime	Supercritical	Critical Depth	1.10 ft
Velocity Downstream	6.76 ft/s	Critical Slope	0.003298 ft/ft
<b>Section</b>			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	8.00 ft
Section Size	8 x 3 ft	Rise	3.00 ft
Number Sections	2		
<b>Outlet Control Properties</b>			
Outlet Control HW Elev.	1,549.66 ft	Upstream Velocity Head	0.55 ft
Ke	0.70	Entrance Loss	0.39 ft
<b>Inlet Control Properties</b>			
Inlet Control HW Elev	1,549.48 ft	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	48.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

River Sta	Q Total (cfs)	Min Ch Elev (ft)	W.S. Elev (ft)	E.G. Elev (ft)	Slope (ft/ft)	Vel Chnl (ft/s)	Flow Area (sq ft)	Top Width (ft)	Friction Coeff	LOB Elev (ft)	ROB Elev (ft)	Flow Depth (ft)	Freeboard Req (ft)	Freeboard Prov (ft)
4222	30	1582.97	1584.03	1584.04	0.000583	0.99	30.71	32.42	0.18	1586.20	1589.30	1.06	1.00	4.17
4172	30	1582.80	1583.91	1583.98	0.002672	2.06	14.57	16.56	0.39	1587.82	1587.84	1.11	1.00	3.91
4130	30	1582.73	1583.77	1583.85	0.003454	2.19	13.70	16.32	0.42	1587.60	1588.56	1.04	1.00	3.83
4070	30	1582.59	1583.54	1583.62	0.004975	2.28	13.15	16.72	0.45	1588.00	1589.33	0.95	1.00	4.46
4039	30	1582.53	1583.53	1583.56	0.000903	1.15	26.13	26.03	0.20	1588.33	1588.96	1.00	1.00	4.80
4004	Culvert													
3953	30	1582.33	1583.51	1583.53	0.000470	0.97	30.84	26.05	0.16	1587.99	1588.61	1.18	1.00	4.48
3915	30	1582.25	1583.44	1583.49	0.002122	1.86	16.11	16.91	0.34	1587.90	1588.90	1.19	1.00	4.46
3819	30	1582.04	1583.24	1583.29	0.002089	1.84	16.28	17.19	0.33	1587.90	1589.11	1.20	1.00	4.66
3715	30	1581.80	1583.04	1583.09	0.001856	1.77	16.95	17.41	0.32	1587.80	1589.14	1.24	1.00	4.76
3663	30	1581.57	1582.97	1583.01	0.001175	1.50	19.94	18.45	0.26	1587.80	1588.70	1.40	1.00	4.83
3635	30	1581.44	1582.95	1582.98	0.000899	1.37	21.87	19.05	0.23	1587.70	1588.57	1.51	1.00	4.75
3582	30	1581.19	1582.92	1582.94	0.000446	1.09	27.59	19.97	0.16	1587.23	1587.03	1.73	1.00	4.11
3581	Int Struct													
3579	30	1578.96	1581.45	1581.50	0.001388	1.78	16.88	13.27	0.28	1587.24	1586.88	2.49	1.00	5.43
3564	30	1578.70	1581.45	1581.48	0.000744	1.30	21.78	15.06	0.21	1587.02	1586.40	2.75	1.00	4.95
3561	30	1579.71	1581.09	1581.44	0.021934	4.76	6.30	9.17	1.01	1586.89	1586.40	1.38	1.00	5.31
3467	30	1579.00	1580.08	1580.21	0.007705	3.00	10.01	13.62	0.62	1585.10	1584.55	1.08	1.00	4.47
3374	30	1578.30	1580.05	1580.07	0.000440	1.10	27.40	19.29	0.16	1583.20	1582.91	1.75	1.00	2.86
3373	Int Struct													
3371	30	1576.07	1578.95	1578.63	0.002092	2.12	14.16	11.40	0.33	1583.36	1582.90	2.49	1.00	4.34
3356	30	1575.82	1578.57	1578.60	0.000770	1.40	21.44	15.62	0.21	1583.42	1582.70	2.75	1.00	4.13
3353	30	1576.82	1578.32	1578.57	0.013852	4.01	7.49	9.99	0.82	1583.22	1582.64	1.50	1.00	4.32
3276	30	1576.24	1577.25	1577.47	0.014457	3.83	7.83	11.60	0.93	1582.40	1582.03	1.01	1.00	4.78
3216	30	1575.75	1577.04	1577.11	0.002727	2.01	14.01	16.94	0.38	1581.40	1582.73	1.25	1.00	3.69
3156	30	1575.34	1577.01	1577.03	0.000516	1.07	27.97	23.44	0.17	1580.80	1579.34	1.67	1.00	2.33
3155	Int Struct													
3152	30	1572.09	1574.51	1574.55	0.001096	1.55	19.39	16.01	0.25	1578.10	1578.13	2.42	1.00	3.59
3138	30	1571.86	1574.51	1574.53	0.000675	1.29	23.23	17.46	0.20	1577.91	1577.91	2.65	1.00	3.40
3135	30	1572.06	1574.32	1574.51	0.011228	3.54	8.47	11.69	0.73	1577.86	1577.90	1.46	1.00	3.54
3110	30	1572.67	1574.03	1574.23	0.011444	3.58	8.37	11.60	0.74	1577.58	1577.58	1.35	1.00	3.55
3014	30	1571.95	1573.11	1573.27	0.008627	3.17	9.47	12.87	0.85	1576.51	1576.51	1.16	1.00	3.40
2918	30	1571.20	1572.11	1572.29	0.011988	3.45	8.69	13.36	0.75	1575.43	1575.43	0.91	1.00	3.32
2822	30	1570.50	1572.00	1572.03	0.000974	1.33	22.51	21.08	0.23	1574.36	1574.36	1.60	1.00	2.36
2797	30	1570.30	1571.99	1572.01	0.000550	1.11	27.11	22.70	0.18	1574.17	1574.17	1.69	1.00	2.18
2795	Int Struct													
2794	30	1568.88	1570.40	1570.52	0.001158	1.58	19.02	15.88	0.25	1574.12	1574.12	2.40	1.00	3.64
2779	30	1567.85	1570.40	1570.50	0.000696	1.31	22.93	17.29	0.20	1573.90	1573.90	2.63	1.00	3.42
2776	30	1568.05	1570.25	1570.48	0.012992	3.72	8.07	11.51	0.78	1573.85	1573.85	1.41	1.00	3.59
2751	30	1568.08	1569.08	1570.17	0.011074	3.53	8.49	11.70	0.73	1573.52	1573.52	1.32	1.00	3.54
2698	30	1568.04	1568.98	1569.18	0.013124	3.63	8.27	12.62	0.79	1572.43	1572.43	0.94	1.00	3.45
2586	30	1567.40	1568.60	1568.93	0.000935	1.38	21.80	20.55	0.24	1571.35	1571.35	1.50	1.00	2.45
2561	30	1567.20	1568.09	1568.91	0.000554	1.11	27.02	22.64	0.18	1571.07	1571.10	1.69	1.00	2.18
2559	Int Struct													
2557	30	1564.93	1567.40	1567.44	0.001101	1.55	19.39	16.03	0.25	1571.00	1571.02	2.42	1.00	3.60
2543	30	1565.80	1567.40	1567.43	0.000677	1.29	23.24	17.24	0.20	1570.80	1570.80	2.60	1.00	3.40
2540	30	1565.75	1567.22	1567.40	0.010545	3.43	8.75	12.01	0.71	1570.75	1570.75	1.47	1.00	3.53
2515	30	1565.56	1566.90	1567.11	0.012611	3.72	8.07	11.40	0.78	1570.47	1570.47	1.34	1.00	3.57
2409	30	1564.76	1566.00	1566.13	0.006811	2.91	10.31	13.31	0.58	1569.32	1569.32	1.24	1.00	3.32
2302	30	1563.97	1564.77	1565.01	0.017535	3.93	7.63	12.86	0.90	1568.16	1568.16	0.80	1.00	3.39
2196	30	1563.17	1564.67	1564.70	0.000889	1.31	22.89	21.35	0.22	1567.00	1567.00	1.50	1.00	2.33
2171	30	1562.99	1564.66	1564.68	0.000536	1.09	27.41	22.89	0.18	1566.72	1566.82	1.60	1.00	2.06
2170	Int Struct													
2168	30	1560.72	1563.12	1563.16	0.001150	1.57	19.09	15.94	0.25	1566.69	1566.77	2.40	1.00	3.57
2153	30	1560.60	1563.12	1563.14	0.000731	1.33	22.62	17.38	0.20	1566.53	1566.50	2.62	1.00	3.38
2150	30	1561.49	1562.89	1563.12	0.013394	3.79	7.91	11.24	0.80	1566.49	1566.49	1.40	1.00	3.60
2125	30	1561.30	1562.48	1562.74	0.016579	4.12	7.28	10.87	0.89	1566.13	1566.10	1.18	1.00	3.62
2071	30	1560.90	1562.04	1562.16	0.005903	2.82	10.62	13.89	0.57	1565.33	1565.33	1.14	1.00	3.29
2015	30	1560.49	1561.38	1562.01	0.011053	1.41	21.28	20.18	0.24	1564.49	1564.49	1.49	1.00	2.51
1990	30	1560.29	1561.97	1561.99	0.000524	1.09	27.56	22.82	0.17	1564.13	1564.13	1.68	1.00	2.16
1988	Int Struct													
1946	30	1558.04	1560.44	1560.48	0.001137	1.57	19.12	15.75	0.25	1564.10	1564.08	2.40	1.00	3.64
1972	30	1557.91	1560.43	1560.46	0.000718	1.32	22.78	17.47	0.20	1563.90	1563.86	2.62	1.00	3.43
1969	30	1558.81	1560.20	1560.43	0.014411	3.90	7.70	11.13	0.83	1563.81	1563.81	1.39	1.00	3.61
1944	30	1558.60	1559.76	1560.03	0.017505	4.19	7.15	10.81	0.91	1563.43	1563.40	1.16	1.00	3.64
1896	30	1558.27	1559.45	1559.56	0.005499	2.85	11.31	14.33	0.53	1562.69	1562.69	1.18	1.00	3.24
1849	30	1557.92	1559.40	1559.44	0.001035	1.43	20.93	19.93	0.25	1561.96	1562.00	1.49	1.00	2.56
1824	30	1557.70	1559.39	1559.41	0.000541	1.10	27.22	22.65	0.18	1561.57	1561.60	1.69	1.00	2.18
1822	Int Struct													
1821	30	1555.48	1557.89	1557.93	0.001132	1.56	19.19	15.94	0.25	1561.52	1561.52	2.41	1.00	3.63
1800	30	1555.25	1557.89	1557.91	0.000556	1.30	23.03	17.36	0.20	1561.30	1561.30	2.64	1.00	3.41
1803	30	1556.30	1557.67	1557.89	0.012787	3.73	8.04	11.41	0.78	1561.20	1561.25	1.37	1.00	3.53
1778	30	1556.06	1557.19	1557.49	0.019991	4.40	6.82	10.81	0.97	1560.86	1560.90	1.13	1.00	3.67
1731	30	1555.70	1556.90	1557.00	0.005023	2.57	11.67	14.49	0.50	1560.13	1560.13	1.20	1.00	3.23
1683	30	1555.35	1556.86	1556.89	0.001013	1.39	21.52	20.15	0.24	1559.39	1559.40	1.51	1.00	2.53
1658	30	1555.16	1556.85	1556.87	0.000529	1.09	27.49	22.80	0.18	1559.00	1559.00	1.69	1.00	2.15
1657	Int Struct													
1655	30	1552.91	1556.36	1556.39	0.001048	1.52	19.77	16.24	0.24	1558.95	1558.95	2.44	1.00	3.60
1640	30	1552.68	1556.35	1556.37	0.000562	1.28	23.46	17.65	0.20	1558.73	1558.70	2.67	1.00	3.35
1637	30	1553.68	1555.18	1555.35	0.009335	3.71	9.07	12.63	0.67	1558.68	1558.70	1.50	1.00	3.50
1612	30	1553.49	1554.55	1555.12	0.009333	3.33	9.02	12.00	0.68	1558.40	1558.44	1.46	1.00	3.45
1514	30	1552.76	1554.05	1554.21	0.009165	3.28	9.12	12.23	0.67	1557.50	15			



# Culvert Calculator Report

## RDC Outfall 2yr

Solve For: Headwater Elevation

<b>Culvert Summary</b>			
Allowable HW Elevation	1,552.00 ft	Headwater Depth/Height	0.29
Computed Headwater Elev.	1,548.50 ft	Discharge	30.00 cfs
Inlet Control HW Elev.	1,548.42 ft	Tailwater Elevation	0.00 ft
Outlet Control HW Elev.	1,548.50 ft	Control Type	Entrance Control
<b>Grades</b>			
Upstream Invert	1,547.62 ft	Downstream Invert	1,545.80 ft
Length	375.00 ft	Constructed Slope	0.004853 ft/ft
<b>Hydraulic Profile</b>			
Profile	S2	Depth, Downstream	0.44 ft
Slope Type	Steep	Normal Depth	0.44 ft
Flow Regime	Supercritical	Critical Depth	0.48 ft
Velocity Downstream	4.28 ft/s	Critical Slope	0.003661 ft/ft
<b>Section</b>			
Section Shape	Box	Mannings Coefficient	0.013
Section Material	Concrete	Span	8.00 ft
Section Size	8 x 3 ft	Rise	3.00 ft
Number Sections	2		
<b>Outlet Control Properties</b>			
Outlet Control HW Elev	1,548.50 ft	Upstream Velocity Head	0.24 ft
Ke	0.70	Entrance Loss	0.17 ft
<b>Inlet Control Properties</b>			
Inlet Control HW Elev	1,548.42 ft	Flow Control	Unsubmerged
Inlet Type	0° wingwall flares	Area Full	48.0 ft²
K	0.06100	HDS 5 Chart	8
M	0.75000	HDS 5 Scale	3
C	0.04230	Equation Form	1
Y	0.82000		

## APPENDIX C

### Erosion Protection

**Level I Scour**

Site: Interim Regional Drainage Channel

Location: Scottsdale, Arizona

Description: Rip Rap Design Calculations

Date: 9/16/2008

**Level I Analysis of Stream Degradation**

**Reference:** ADWR, Flood Warning and Dam Safety Section, 1996.  
State Standard 5-96: "Watercourse System Sediment Balance - Guideline 2:  
Channel Degradation Estimation for Alluvial Channels in Arizona"

**Assumptions:** Channel reaches without major disturbances, such as dams and bridges.

**Equations:**  $D_s = D_{gs} + D_{lts}$

where:

$D_s$  = total scour depth, in feet;

$D_{gs}$  = general degradation, in feet;

$D_{lts}$  = long term degradation, in feet;

For straight channel reaches:

$$D_{gs} = 0.157 * Q_{100}^{0.4}$$

For channel reaches with curvature:

$$D_{gs} = 0.219 * Q_{100}^{0.4}$$

Long term degradation:

$$D_{lts} = 0.02 * Q_{100}^{0.6}$$

**Project Name:** Regional Drainage Solution    **Location:** Scottsdale

**Input Data:**

$Q_{100} =$                       300 cfs

$D_s =$                       2.15 ft                      for straight channel

$D_s =$                       2.76 ft                      otherwise

**Recommended Scour Depth :**                      3.0 ft

Note: the minimum total scour depth,  $D_s$ , shall be 3 feet.

## Bend Scour Calculation

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Bend Scour Design Calculations  
 Date: 9/16/2008

## Bend Scour Calculation Sheet

Reference: ADWR, Design Manual for Engineering Analysis of Fluvial Systems, 1985 p5 105-5.110

Project Name: Regional Drainage Solution

Wood/Patel # 073022

## Scour Depth Equation:

$$Z_{bs} = (0.0685 \cdot Y \cdot V^{0.6}) [2.1 \cdot (\sin^2(a/2) / \cos(a))^{0.2} - 1] / (Yh^{0.4} \cdot Se^{0.3})$$

Where  $Z_{bs}$  = bend scour component of total scour depth (ft)  
 $V$  = mean velocity of upstream flow (fps)  
 $Y$  = maximum depth of upstream flow (ft)  
 $Yh$  = hydraulic depth of upstream flow (ft)  
 $Se$  = upstream energy slope (bed slope for uniform flow conditions, ft/ft)  
 $a$  = angle formed by the projection of the channel centerline from the point of curvature to a point which meets a line tangent to the outer bank of the channel (degrees)

## Scour Length Equation

$$X = 2.3 \cdot (C/g^{0.5}) \cdot Y$$

Where  $X$  = distance from the end of channel curvature (point of tangency  $P \cdot T$ ) to the downstream point at which secondary currents have dissipated (ft)  
 $C$  = Chezy coefficient =  $1.486 \cdot R^{1/6} / n$   
 $g$  = gravitational acceleration (32.2 ft/s<sup>2</sup>)  
 $Y$  = depth of flow (to be conservative, use maximum depth of flow, exclusive of scour, within the bend) (ft)

## Input Data

$V =$	4.1 (ft/s)	$n =$	0.035
$Y =$	3.56 (ft)	$A =$	73.54 (ft <sup>2</sup> )
$Yh =$	2.35 (ft)	$P =$	33 (ft)
$Se =$	0.003104	$R =$	2.23 (ft)
$a =$	40 (degree)	$C =$	48.52
	Stable bank side slope =		3 (H:V)

## Computed Scour Values

Scour Depth:	Scour Length:	Scour Width:
$Z_{bs} =$ 1.34 (ft)	$X =$ 70 (ft)	$W =$ 4.0 (ft)



**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

**References:** Department of the Army, U.S. Army Corps of Engineers,  
 Engineering and Design Hydraulic Design of Flood Control Channels.  
 No. 1110-2-1601, Dated 30 June 1994, Chapter 3 (Riprap Protection)

US DOT, FHWA, Highways in the River Environment  
 Hydraulic and Environmental Design Considerations  
 May 1975, pVI-24, (Suggested gradation for riprap).

$$D_{30} = S_f C_s C_v C_r d \left[ \left( \frac{\gamma_w}{\gamma_s - \gamma_w} \right)^{1/2} \cdot \frac{V}{\sqrt{K_1 g d}} \right]^{2.5}$$

**Project Name:** Interim Regional Drainage Channel  
**Location:** Inlet Driveway Culvert

**Inlet Riprap Size**

Safety Factor, $S_f$	1.3
Stability Coefficient, $C_s$	0.375 (Assume rounded rock)
Vertical Velocity Dist., $C_v$	1.00
Thickness Coefficient, $C_r$	1.00
Local Depth, $d$	3.94 ft
Unit Weight of Water, $\gamma_w$	62.4 lbs/ft <sup>3</sup>
Unit Weight of Stones, $\gamma_s$	165 lbs/ft <sup>3</sup>
Local Velocity, $V$	3.6 ft/sec
Bank Angle With Horizontal, $\theta$	18.43 °
Rip Rap Angle of Repose (Fig 6-8), $\phi$	37 °
Bank Angle Correction Factor, $K_1$	0.8509
Computed Riprap Size, $D_{30}$	0.9 inches
Computed Riprap Size, $D_{50}$	1.3 inches
Computed Riprap Size, $D_{15}$	0.6 inches
Computed Riprap Size, $D_{85}$	2.0 inches
<b>Design Riprap Size, <math>D_{50}</math></b>	<b>9 inches</b> <b>TYPE I</b>

**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

References: Department of the Army, U.S. Army Corps of Engineers,  
 Engineering and Design Hydraulic Design of Flood Control Channels.  
 No. 1110-2-1601, Dated 30 June 1994, Chapter 3 (Riprap Protection)

US DOT, FHWA, Highways in the River Environment  
 Hydraulic and Environmental Design Considerations  
 May 1975, pVI-24, (Suggested gradation for riprap).

$$D_{30} = S_f C_s C_v C_T d \left[ \left( \frac{\gamma_w}{\gamma_s - \gamma_w} \right)^{1/2} \frac{V}{\sqrt{K_1 g d}} \right]^{2.5}$$

Project Name: Interim Regional Drainage Channel  
 Location: Channel Bend

**Inlet Riprap Size**

Safety Factor, $S_f$	1.3	
Stability Coefficient, $C_s$	0.375	(Assume rounded rock)
Vertical Velocity Dist., $C_v$	1.15	
Thickness Coefficient, $C_T$	1.00	
Local Depth, $d$	3.56 ft	
Unit Weight of Water, $\gamma_w$	62.4 lbs/ft <sup>3</sup>	
Unit Weight of Stones, $\gamma_s$	165 lbs/ft <sup>3</sup>	
Local Velocity, $V$	4.1 ft/sec	
Bank Angle With Horizontal, $\theta$	18.43 °	
Rip Rap Angle of Repose (Fig 6-8), $\phi$	39 °	
Bank Angle Correction Factor, $K_1$	0.8647	
Computed Riprap Size, $D_{30}$	1.4 inches	
Computed Riprap Size, $D_{50}$	2.1 inches	
Computed Riprap Size, $D_{15}$	0.9 inches	
Computed Riprap Size, $D_{85}$	3.1 inches	
Design Riprap Size, $D_{50}$	9 inches	TYPE I

**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

**References:** Department of the Army, U.S. Army Corps of Engineers,  
 Engineering and Design Hydraulic Design of Flood Control Channels,  
 No. 1110-2-1601, Dated 30 June 1994, Chapter 3 (Riprap Protection)

US DOT, FHWA, Highways in the River Environment  
 Hydraulic and Environmental Design Considerations  
 May 1975, pVI-24, (Suggested gradation for riprap).

$$D_{30} = S_f C_s C_v C_r d \left[ \left( \frac{\gamma_w}{\gamma_s - \gamma_w} \right)^{1/2} \frac{V}{\sqrt{K_1 g d}} \right]^{2.5}$$

**Project Name:** Interim Regional Drainage Channel  
**Location:** Culvert Under Scottsdale Road

**Inlet Riprap Size**

Safety Factor, $S_f$	1.3	
Stability Coefficient, $C_s$	0.375 (Assume rounded rock)	
Vertical Velocity Dist., $C_v$	1.00	
Thickness Coefficient, $C_r$	1.00	
Local Depth, $d$	2.84 ft	
Unit Weight of Water, $\gamma_w$	62.4 lbs/ft <sup>3</sup>	
Unit Weight of Stones, $\gamma_s$	165 lbs/ft <sup>3</sup>	
Local Velocity, $V$	5.0 ft/sec	
Bank Angle With Horizontal, $\theta$	14.1 °	
Rip Rap Angle of Repose (Fig 6-8), $\phi$	37 °	
Bank Angle Correction Factor, $K_1$	0.9144	
Computed Riprap Size, $D_{30}$	1.9 inches	
Computed Riprap Size, $D_{50}$	2.9 inches	
Computed Riprap Size, $D_{15}$	1.3 inches	
Computed Riprap Size, $D_{85}$	4.4 inches	
<b>Design Riprap Size, <math>D_{50}</math></b>	<b>9 inches</b>	<b>TYPE I</b>

**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

References: *US DOT, FHWA, Highways in the River Environment  
 Hydraulic and Environmental Design Considerations  
 May 1975, pVI-24.*

*US DOT, FHWA, Hydraulic Design of Energy Dissipaters  
 for Culverts and Channel. Sept. 1983, pII-5-II-9.*

*FCDMC, Drainage Design Manual for Maricopa County  
 Arizona, Vol. II - Hydraulics. January 1996, p5.75-5.77.*

Project Name: Interim Regional Drainage Channel  
 Project #: 073022

Structure ID: Union Hills Outlet  
 Culvert Size: 3- 8'x3' CBC

**1. Riprap Size D50**

Max. flow width $W_o =$	24.00 ft	
Max. culvert flow depth $h =$	3.00 ft	
Tailwater depth $TW =$	3.00 ft	
Exit Velocity $V_e =$	4.16 fps	
Tailwater velocity $V_d =$	2.20 fps	normal
Wash bottom width $=$	25.00 ft	
Computed Riprap Size D50 $=$	1.2 in	

Design Riprap Size D50 = 9 in  
 Sieve Size = TYPE 1

**2. Riprap Sizes D15 and D85**

Design Riprap Size D15 = 4 in  
 Design Riprap Size D85 = 14 in

**3. Riprap Apron Length**

Riprap Apron Length = 14 ft

**4. Riprap Apron Width**

Min. Riprap Apron Width = 30 ft  
 Max. Riprap Apron Width = 31 ft

**5. Riprap Thickness**

Riprap Thickness = 36 in

**6. Total Riprap Volume**

Riprap Rock Volume = 46 C.Y

Please note fields highlighted are input values from the Culvert Modeling Summary

**Rip Rap Design**

Site: Interim Regional Drainage Channel  
 Location: Scottsdale, Arizona  
 Description: Rip Rap Design Calculations  
 Date: 9/15/2008

**Riprap Design Spreadsheet**

References: *US DOT, FHWA, Highways in the River Environment Hydraulic and Environmental Design Considerations May 1975, pVI-24.*  
*US DOT, FHWA, Hydraulic Design of Energy Dissipaters for Culverts and Channel. Sept. 1983, pII-5-II-9.*  
*FCDMC, Drainage Design Manual for Maricopa County Arizona, Vol. II - Hydraulics. January 1996, p5.75-5.77.*

Project Name: Interim Regional Drainage Channel  
 Project #: 073022

Structure ID: Driveway Outlet  
 Culvert Size: 3- 8'x3' CBC

**1. Riprap Size D50**

Max. flow width $W_o =$	24.00 ft	
Max. culvert flow depth $h =$	3.00 ft	
Tailwater depth $TW =$	3.00	
Exit Velocity $V_e =$	4.17 fps	
Tailwater velocity $V_d =$	3.05 fps	normal
Wash bottom width $=$	25.00 ft	
Computed Riprap Size D50 $=$	12 in	
Design Riprap Size D50 $=$	9 in	
Sieve Size $=$	TYPE I	

**2. Riprap Sizes D15 and D85**

Design Riprap Size D15 $=$	4 in
Design Riprap Size D85 $=$	14 in

**3. Riprap Apron Length**

Riprap Apron Length $=$	8 ft
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**4. Riprap Apron Width**

Min. Riprap Apron Width $=$	30 ft
Max. Riprap Apron Width $=$	31 ft

**5. Riprap Thickness**

Riprap Thickness $=$	36 in
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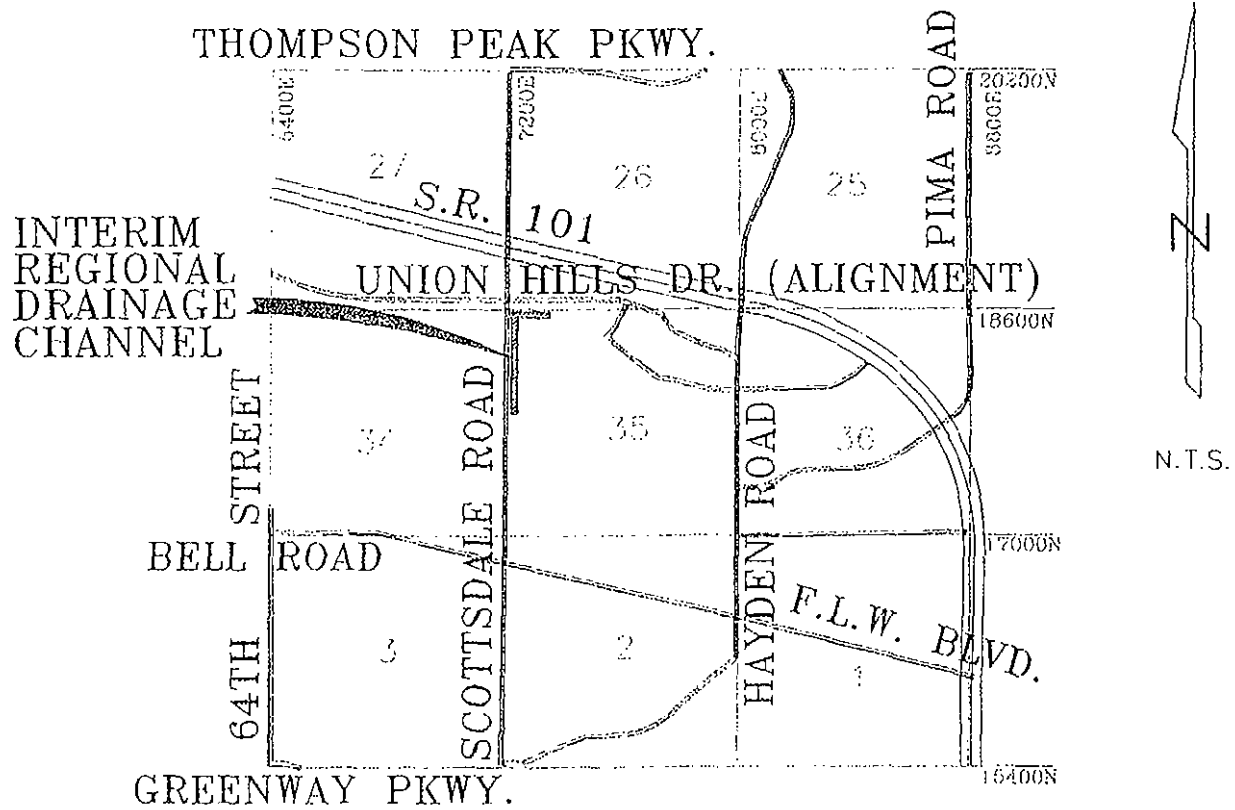
**6. Total Riprap Volume**

Riprap Rock Volume $=$	26 CY
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Please note fields highlighted are input values from the Culvert Modeling Summary

## **EXHIBIT 1**

### **Vicinity Map**



## INTERIM REGIONAL DRAINAGE CHANNEL

### Exhibit 1 Vicinity Map

WOOD/PATEL  
LAND DEVELOPMENT • WATER RESOURCES  
TRANSPORTATION • TRAFFIC  
WATER / WASTEWATER • SURVEYING  
CONSTRUCTION MANAGEMENT  
(602) 335-8500  
PHOENIX • MESA • TUCSON

**EXHIBIT 2**

**FEMA Map**



**SPECIAL FLOOD HAZARD AREAS SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD**

The 1% annual chance flood (100-year flood), also known as the base flood, is the flood that has a 1% chance of being equaled or exceeded in any given year. The Special Flood Hazard Area is the area subject to flooding by the 1% annual chance flood. Areas of Special Flood Hazard include Zones A, AE, AH, AO, AR, A99, V and VE. The Base Flood Elevation is the water-surface elevation of the 1% annual chance

ZONE A	No Base Flood Elevations determined.
ZONE AE	Base Flood Elevations determined.
ZONE AH	Flood depths of 1 to 3 feet (usually areas of ponds). Base Flood Elevations determined.
ZONE AO	Flood depths of 1 to 3 feet (usually shallow flow on sloping terrain); average depths determined. For areas of substantial flow flooding, velocities also determined.
ZONE AR	Special Flood Hazard Area formerly protected from the 1% annual chance flood by a flood control system that was subsequently declining. Zone AR indicates that the former flood control system is being restored to provide protection from the 1% annual chance flood or greater flood.
ZONE AS9	Area to be protected from 1% annual chance flood by a Federal flood protection system under construction, no Base Flood Elevations determined.
ZONE V	Coastal flood zone with velocity hazard (wave action); no Base Flood Elevations determined.
ZONE VE	Coastal flood zone with velocity hazard (wave action); Base Flood Elevations determined.

The floodway is the channel of a stream plus any adjacent floodplain areas that must be kept free of encroachment so that the 1% annual chance flood can be carried without

substantial increases in flood heights.

Areas of 0.2% annual chance flood; areas of 1% annual chance flood with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood.

☐ OTHER AREAS

 COASTAL BARRIER RESOURCES SYSTEM (CBRS) AREAS

☐ OTHERWISE PROTECTED AREAS (OPAs)

CBRS areas and OPAs are normally located within or adjacent to Special Flood Hazard Areas.

0.2% annual chance floodplain boundary

———— Zone D boundary  
\*\*\*\*\* CBRS and OPA boundary

Boundary dividing Special Flood Hazard Area Zones, and boundary dividing Special Flood Hazard Areas of different

Base Flood Elevation value where uniform within zone:

elevation in feet\*

 Cross section line

11-2005041 0078

<sup>43</sup>76<sup>WGS84</sup>E 1000-meter Universal Transverse Mercator grid tick values zone 12

875000 FT 5000-foot grid tick values: Arizona State Plane coordinate system, central zone (FIPSZONE 3176)

\* M15      Since M15

*Journal of Management Education* 36(7) 809-824

EFFECTIVE DATE OF COUNTYWIDE  
FLOOD INSURANCE RATE MAP

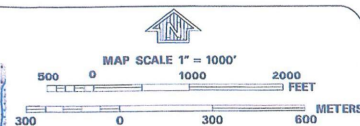
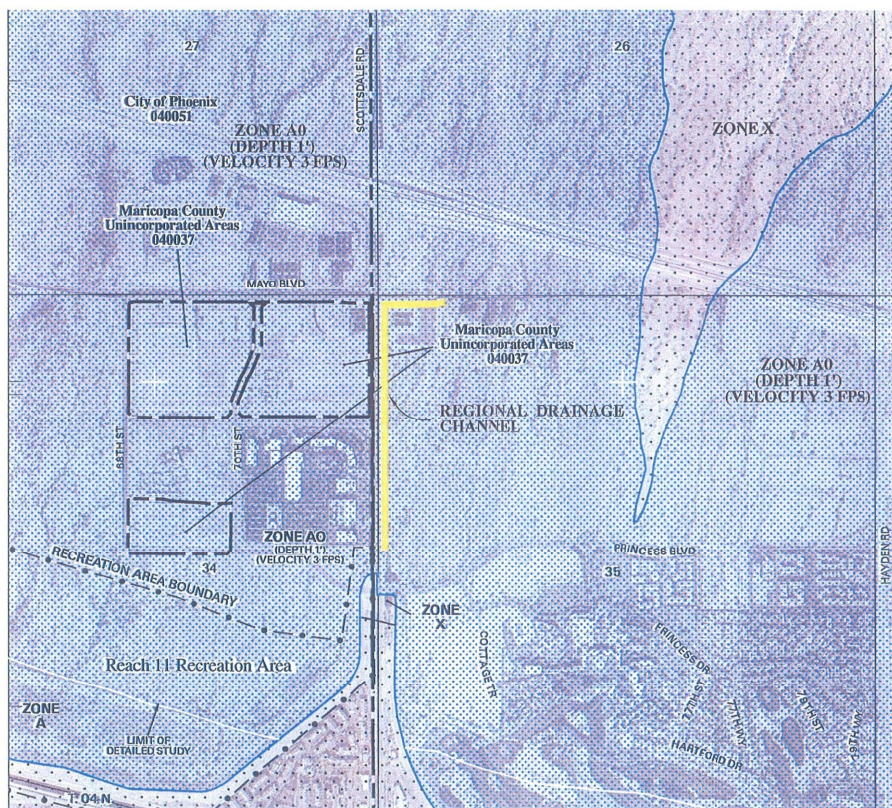
April 16, 1988

December 3, 1993, September 30, 1995, July 19, 2001

September 30, 2007, to update corporate limits, to change Base Flood Elevations, to add Base Flood Elevations, to add Special Flood Hazard Areas, to change Special Flood Hazard Areas, to change zone designations, to add roads and road names, to incorporate newly issued Letters of Map Revision, and to incorporate

For community and revision history prior to countywide mapping, refer to the Community Map History table located in the Flood Insurance Study report for this community.

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## PANEL 1245H

**FIRM  
FLOOD INSURANCE RATE MAP  
MARICOPA COUNTY,  
ARIZONA  
AND INCORPORATED AREAS**

## PANEL 1245 OF 4350

(SEE MAP INDEX FOR FIRM PANEL LAYOUT)

## CONTAINS

COMMUNITY	NUMBER	PANEL	SUFFIX
MANICOPA COUNTY	040007	1245	H
PHOENIX, CITY OF	040051	1245	H
SCOTTSDALE, CITY OF	041502	1245	H

Notice to User: The Map Number shown below should be used when placing map orders; the Community Number shown above should be used on insurance applications for the subject community.



**SEPTEMBER 30, 2005**  
Federal Emergency Management Agency

NOT FOR  
CONSTRUCTION  
OR RECORDING

INTERIM REGIONAL  
DRAINAGE CHANNEL

WP# 073022

DATE: 09-15-2008

EXHIBIT 2  
FEMA MAP

**WOOD/PATEL**  
LAND DEVELOPMENT & WATER RESOURCES

TRANSPORTATION / TRAFFIC  
WATER / WASTEWATER • SURVEYING  
CONSTRUCTION MANAGEMENT  
(602) 556-8500  
PHOENIX • MESA • TUCSON • GOODYEAR