



**DRAINAGE REPORT
FOR
FAIRMONT SCOTTSDALE PRINCESS
PARKING GARAGE**

June 2, 2023
WP# 215319.40

**STIPULATION SET
RETAIN FOR RECORDS
APPROVED**

08/22/2023

DATE


APPROVED BY

STAMPED ON BEHALF OF J. LYNCH



EXPIRES 06-30-25

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EXPIRES 06-30-25

1.0 INTRODUCTION

1.1 General Background

The Fairmont Scottsdale Princess Parking Garage (Site) is a proposed multi-level parking structure on approximately 3.9 acres of the approximate 9.02 parcel of the FMT Scottsdale Owner LLC in the City of Scottsdale (APN#215-08-694). The project will include hardscape, landscape, and utility improvements to support the development. This Site is east of Princess Drive and South of Princess Boulevard within Section 35, Township 4 North, Range 4 East of the Gila and Salt River Base and Meridian, Maricopa County, Arizona. Refer to Exhibit 1 – *Vicinity Map* for the project location. The existing property, zoned C-2, is an existing parking lot with sidewalks and landscaping.

This Drainage Report has been prepared in accordance with Wood, Patel & Associates, Inc.'s (WOODPATEL's) understanding of the City of Scottsdale technical drainage requirements (Ref. 1) and the *Drainage Design Manuals for Maricopa County Hydrology and Hydraulics (2018)* (Ref. 3 and 4), as applicable to the Site.

1.2 FEMA Regulated Flood Zones

The Federal Emergency Management Agency (FEMA) publishes Flood Insurance Rate Map (FIRM) information for communities that adhere to FEMA regulations. The FEMA FIRM panel for this Site is 04013C1320L, effective date October 16, 2013, and indicates the Site falls within "Zone AO" shaded (Refer to Exhibit 2 – *FEMA FIRM*).

"Zone AO" shaded is defined by FEMA as follows:

"Flood depths of 1 to 3 feet (usually sheet flow on sloping terrain); average depths determined. For areas of alluvial fan flooding, velocities also determined".

It is WOODPATEL's understanding, based on experience and interpretations of the City of Scottsdale floodplain ordinance, that development of land within FEMA Zone "AO" is acceptable if the lowest finish floor elevation is above or properly protected from the anticipated 100-year water surface elevation. This Site will be designed in accordance with the City's floodplain ordinance to comply with Federal and State regulations.

2.0 HYDROLOGY ANALYSIS

2.1 Offsite Hydrology

The proposed Site receives offsite flows from the half street of Princess Drive along its historical path. This flow is conveyed overland to two (2) proposed 4-foot curb openings where it enters the Site. In addition, offsite flows from Princess Boulevard and the properties north of Princess Boulevard do not enter the Site per an analysis of the topographic survey performed onsite. The stormwater flow entering the curb opening are 1.9 cfs for A-2 and 0.9 cfs for A-4 for the 10-year storm and 3.3 cfs for A-2 and 1.7 cfs for A-4 for the 100-year storm, respectively. (Refer to Appendix D – *Hydrologic and Hydraulic Calculations*)

Offsite peak flow rates for the proposed development were calculated using the Rational Method, as outlined in the *Drainage Design Manual for Maricopa County, Arizona: Volume I – Hydrology* (Ref 3). NOAA Atlas 14 precipitation data was obtained and utilized to develop Intensity-Duration-Frequency (I-D-F) curves for the Site. Rational Method peak flows were computed at concentration points within the Site at key design locations. Runoff coefficients were estimated to reflect post-development land use conditions for the 2-year, 10-year, and 100-year events. (Refer to Appendix D – *Hydrologic and Hydraulic Calculations*)

2.2 Onsite Hydrology

Per the existing stormwater waiver approved for the Site, no stormwater retention is existing or required. Refer to Appendix A - *Storm Water Storage Waiver / Proposed Drainage Improvements Exhibit*. Although retention is not required, the City of Scottsdale requires the First Flush Volume to be captured and treated to comply with Federal and State regulations. The First Flush Volume will be treated by the Contech CDS3020-6-C treatment system (CDS). Refer to Appendix F - *Contech CDS3020-6-C Treatment System* for the manufacturer's details. The CDS was sized based on the treatment rate of the system compared to the flow rate of the First Flush volume as calculated from Section 6.4.1 of the *Drainage Policies and Standards for Maricopa County* (Ref. 5). Refer to Appendix D - *Hydrologic and Hydraulic Calculations*, for the First Flush flow rate calculation. The First Flush flow required to be treated is 0.52 cfs for the proposed stormwater system.

Onsite peak flow rates for the proposed development were calculated using the Rational Method, as outlined in the *Drainage Design Manual for Maricopa County, Arizona: Volume I – Hydrology* (Ref 3). NOAA Atlas 14 precipitation data was obtained and utilized to develop Intensity-Duration-Frequency (I-D-F) curves for the Site. Rational Method peak flows were computed at concentration points within the Site at key design locations. Runoff coefficients were estimated to reflect post-development land use conditions for the 2-year, 10-year, and 100-year events. (Refer to Appendix D – *Hydrologic and Hydraulic Calculations*)

The proposed drainage system will include five (5) M.A.G. 535 catch basins, a 12-inch inlet concrete flared end section, a 30-inch outlet concrete flared end section, two (2) 48-inch storm drain manholes, a 60-inch precast concrete junction box, H.D.P.E pipe, RCP pipe, and the CDS. (Refer to Exhibit 4 – *Proposed Drainage Area Map*) The existing 24-inch CMP pipe culvert will be replaced with 30-inch RCP with the same length of pipe and at the same slope and inverts. The increase in size and pipe type normalizes the flow for the 10-year storm event. (Refer to Appendix E – *StormCAD Modeling Results*)

2.3 Establishing Lowest Finish Floor (LFF88 Elevations)

The Grading and Drainage Plan has been designed to comply with the City of Scottsdale floodplain ordinance for a Zone “AO” floodplain. It is our understanding, unless other flood-proof measures are presented and approved, the proposed Lowest habitable Finished Floor (LFF) elevation must be designed a minimum of 1-foot above the anticipated 100-year flood elevation plus the City of Scottsdale

requires an additional 1-foot above the flood depth, which results in a minimum finished floor elevation of 2 feet above the Highest Adjacent natural Grade (HAG) which is the regulatory flood elevation. Since the Site was disturbed after the Zone "AO" Special Flood Hazard Zone was established, the current condition of the Site could not determine the HAG. The HAG uses topographical information showing the pre-disturbed condition of the Site. (Refer to Appendix B - *Regional Contour Map / Opinion of Existing Highest Natural Grade Elevation*)

Utilizing Curry's Corner 7.5-minute Topographic Survey Map by USGS from 1964 for the pre-disturbed condition (Refer to Appendix C - *Curry's Corner Quadrangle Map*) with a contour interval of 10 feet, the approximate highest natural grade of this Site would require the conversion of NAVD29 datum to the NAVD88 datum by adding 1.749 feet to the NAVD29 datum.

Using AutoCAD Civil 3D, the quad map was aligned to the Site using common monument lines and previously surveyed monuments by WOODPATEL. The 10-foot interval contours were digitized, adjusted to NAVD88, and applied to a surface model. The surface model was supplemented with break lines at estimated ridge and flowline locations and used to display interpolated 1-foot contours for the pre-disturbed condition. The proposed parking garage was overlaid on the contour map to determine the HAG elevation of 1561.48. The regulatory flood elevation was calculated to be 1563.48. The proposed finish floor elevation for the second floor is 1566.50 which is 3.02 feet above the regulatory flood elevation. Refer to Appendix B - *Regional Contour Map / Opinion of Existing Highest Natural Grade Elevation* and Appendix C - *Curry's Corner Quadrangle Map*.

3.0 HYDRAULIC ANALYSIS

The existing storm drain system was designed to capture runoff through overland flow to an existing 24-inch CMP pipe culvert which discharges to an existing earthen channel that conveys it to the TPC Golf Course. With the runoff from the proposed improvements remaining virtually the same, the proposed storm drain system will capture the 100-year storm event through catch basins and convey it through a proposed treatment structure, Contech CDS3020-6-C. This system will treat the First Flush volume and discharge to the proposed 30-inch RCP, (Refer to Appendix F - *Contech CDS3020-6-C Treatment System*) to size the Contech model identified, the First Flush volume needed to be converted to a flow rate to compare the treatment rate of the model selected. The First Flush flow rate for the Site is 0.52 cfs. (Refer to Appendix D, Table 6 – *First Flush Flow*). Application of the calculated values noted in Appendix D – *Hydrologic and Hydraulic Calculations* were modeled in StormCAD with results shown in Appendix E – *StormCAD Modeling Results*. A total of 22.39 cfs was calculated using the Rational Method for the 10-year storm event. Per the plumbing engineer, the surface drainage for the roof (Area A-1) will be conveyed to a grease interceptor with a sump pump which will discharge to the proposed storm drain system at a rate of 2,900 gpm or 6.5 cfs. This is reflected for both the 10-year and 100-year storms. The storm drain network discharges to the existing channel southeast of the Site at a flow rate of 22.39 cfs and 38.78 cfs for the 10- and 100-year storm events respectively.

4.0 MAINTENANCE

Ongoing maintenance of the designed or recommended drainage systems is required to preserve the design integrity and purpose of the drainage system. Failure to provide maintenance can prevent the drainage system from performing to its intended design purpose and can result in reduced performance. Maintenance within the public right-of-way is the responsibility of the governing municipality. However, it is the responsibility of landowners (such as private developers or property owners' associations) for facilities on private property. Prior to ultimate condition build-out upstream of drainage structures, additional maintenance may be required due to an increase in sedimentation build-up. A regular maintenance program is required to have drainage systems perform to the level of protection or service, as presented in this report and the projects' plans and specifications.

5.0 CONCLUSIONS

Based on our analysis of the Site, the following conclusions can be made:

1. This Drainage Report has been prepared in accordance with WOODPATEL's understanding of the City of Scottsdale technical drainage requirements and the *Drainage Design Manuals for Maricopa County Hydrology and Hydraulics (2018)*, as applicable to the Site.
2. The Site is within a FEMA designated "Zone AO" shaded.
3. The Site is protected from offsite flows from the north by improvements, as outlined in the approved stormwater storage waiver.
4. No stormwater retention has been provided for this project, per the approved stormwater waiver.
5. The proposed Contech CDS3020-6-C treatment structure will treat the First Flush flow rate of 0.52 cfs.
6. The onsite 100-year storm event is to be conveyed southeast along its historic path through a proposed 30-inch RCP pipe culvert connected to the existing earthen channel which ultimately discharges to the existing TPC Golf Course.
7. The HAG is 1561.48 and the regulatory flood elevation is 1563.48 per the attached calculations. The first-floor elevation of the proposed parking garage is below the regulatory flood elevation and will be subject to additional requirements. The second-floor elevation is 3.02 feet above the regulatory flood elevation.
8. The proposed stormwater system will discharge 22.39 cfs of stormwater into the existing channel to the south east.
9. Ongoing maintenance is required for the existing drainage systems to maintain design performance. Maintenance is the responsibility of the private parties involved.

6.0 REFERENCES

1. *Design Standards & Policies Manual*, City of Scottsdale, 2018
2. *Curry's Corner Quadrangle, 7.5 Minute Series Topographic Map*, USGS, 1964
3. *Drainage Design Manual for Maricopa County, Volume I Hydrology*, Arizona, 2018
4. *Drainage Design Manual for Maricopa County, Volume II Hydraulics*, Arizona, 2018
5. *Drainage Policies and Standards for Maricopa County*, Arizona, 2016

**APPENDIX A – STORM WATER STORAGE WAIVER / PROPOSED DRAINAGE
IMPROVMENTS EXHIBIT**



Request for Stormwater Storage Waiver

292-SA-2007

City of Scottsdale Case Numbers:

- PA - - ZN - - UP - - DR - - PP - PC# 6332-07-7

The applicant/developer must complete and submit this form to the city for processing and obtain approval of waiver request *before* submitting improvement plans. Denial of the waiver may require the developer to submit a revised site plan to the Development Review Board.

Date 7/14/08 Project Name Fairmont Scottsdale Princess Resort
 Project Location 7575 East Princess Drive Scottsdale, AZ 85255
 Applicant Contact John Bulka Company Name Wood Patel & Associates
 Phone 480-834-3300 Fax 480-834-3320 E-mail jbulka@woodpatel.com
 Address 1855 N. Stapley Mesa, AZ 85203

Waiver Criteria

A waiver is an intentional relinquishment of a claim or right. A project must meet at least one of six criteria listed below for the city to consider waiving some or all required stormwater storage. Check the applicable box and provide a signed engineering report and supporting engineering analyses that demonstrate the project meets the criteria and that the effect of a waiver will not increase the potential for flooding on any property.

- ☐ 1. The runoff for the project has been included in a storage facility at another location. The applicant must demonstrate that the stormwater storage facility was specifically designed to accommodate runoff from the subject property and that the runoff will be conveyed to this location through an adequately designed conveyance facility.
- ☒ 2. The development is adjacent to a watercourse or channel that an engineering analysis shows is designed and constructed to handle the additional runoff without increasing the potential for flood damage to the subject property or to any other property.
- ☐ 3. The development is on a parcel less than one-half acre in size in an area where the engineering analysis demonstrates there is no significant increase in potential for flood damage due to its development.
- ☐ 4. Stormwater storage requirements conflict with requirements of the Environmentally Sensitive Lands Ordinance (ESLO). The applicant must demonstrate there is no increased potential for flood damage to the subject property or to any other property. Such conflicts with ESLO may include:
 - Total land requirements for storage basin, easements, setbacks, and NAOS prevent building allowable footprint per zoning.
 - Topography prevents building storage basin.
 - Creating a storage facility requires wash modification.
 - Instances where the Zoning Administrator cannot allow a modification to ESL requirements.
- ☐ 5. The project is located within the Downtown Fee Reduction Area as described and approved by City Council Resolution #6238 (see map). The applicant must demonstrate there is no increased potential for flood damage to any property. Even if the project is located in the Downtown area, if the project creates additional potential for increased flood damage, the developer must provide alternative mitigation methods to prevent the damage.
- ☐ 6. The project is located within a watershed that drains directly to the Salt River Pima-Maricopa Indian Community (SRPMIC) (see map). The project must provide the pre-development peak discharge flow to the SRPMIC, and attenuate flows over and above pre-development.

By signing below, I certify that the stated project meets the waiver criteria selected above as demonstrated by the attached documentation.

John Bulka
 Developer or Engineer (circle one)

7-16-08
 Date

Planning & Development Services Department

7447 E Indian School Road, Suite 105, Scottsdale, AZ 85251 • Phone: 480-312-7000 • Fax: 480-312-7088

10/23

SWW

6332-07-7



City of Scottsdale Case Numbers:

PC#_

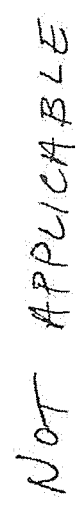


Figure 1. Designated Area for Downtown Stormwater Storage Waivers

Planning & Development Services Department

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- PA -

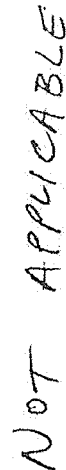
- ZN -

- UP -

- DR -

- PP -

PC#



Planning & Development Services Department

Request for Stormwater Storage Waiver



Request for Stormwater Storage Waiver

292. SA. 2007

City of Scottsdale Case Numbers:

- PA - _____ - ZN - _____ - UP - _____ - DR - _____ - PP - _____ PC# _____

CITY STAFF TO COMPLETE THIS PAGE

Project Name FAIRMONT SCOTTSDALE PRINCESS RESORT

Check Appropriate Boxes:

☐ Meets waiver criteria (specify): ☐ 1 ☐ 2 ☐ 3 ☐ 4 ☐ 5 ☐ 6

☒ Recommend approve waiver.

☐ Recommend deny waiver:

☐ None of waiver criteria met.

☐ Downstream conditions prohibit waiver of any storage.

☐ Other:

Explain: _____

☐ Return waiver request:

☐ Insufficient data provided.

☐ Other: _____

Explain: _____

Recommended Conditions of Waiver:

☒ All storage requirements waived.

☐ Pre development conditions must be maintained.

☒ Other:

Explain: In kind improvements exceed cost of in-lieu fee.

☒ Waiver approved per above conditions.

☐ Waiver denied.

C. Ashley Luch
Floodplain Administrator or Designee

10/23/08
Date

Planning & Development Services Department

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Request for Stormwater Storage Waiver

292-SA-2007

City of Scottsdale Case Numbers:

- PA - - ZN - - UP - - DR - - PP - PC#

In-Lieu Fee and In-Kind Contributions

If the city grants a waiver, the developer is required to calculate and contribute an In-Lieu Fee based on what it would cost the city to provide the waived storage volume, including costs such as land acquisition, construction, landscaping, design, construction management, and maintenance over a 75-year design life. For FY 2007/2008, this cost is \$3.22 per cubic foot of stormwater stored. This unit cost will be updated annually, but the city reserves the right to revise the unit cost at any time at its sole discretion.

The Floodplain Administrator considers in-kind contributions on a case-by-case basis. An in-kind contribution can serve as part of or instead of the calculated in-lieu fee. The Floodplain Administrator or designee must approve in-lieu fees and in-kind contributions.

Project Name Fairmont Scottsdale Princess Resort

The waived stormwater storage volume is calculated as follows:

$V = CRA$; where

V = stormwater storage volume required, in cubic feet,

C = weighted average runoff coefficient over disturbed area,

R = 100-year/2-hour precipitation depth, in feet (2.82 inches, or 0.235 feet, for all regions of Scottsdale), and

A = area of disturbed ground, in square feet

Furthermore,

$V_w = V - V_p$; where

V_w = volume waived,

V = volume required, and

V_p = volume provided

C = 0.9
A = 424,753
V = 89,826
 V_p = 0
 V_w = 89,826

☐ An In-Lieu Fee will be paid, based on the following calculations and supporting documentation:
In-lieu fee (\$) = V_w (cu. ft.) x \$3.22 per cubic foot = 289,240

☒ An In-Kind Contribution will be made, as follows:

See attachment. Princess Drive Bridge Reconstruction, in accordance with approved plans.

☐ No In-Lieu Fee is required. Reason:

Approved by:

C. Ashley Carlin

Floodplain Administrator or Designee

10/23/08

Date

Planning & Development Services Department

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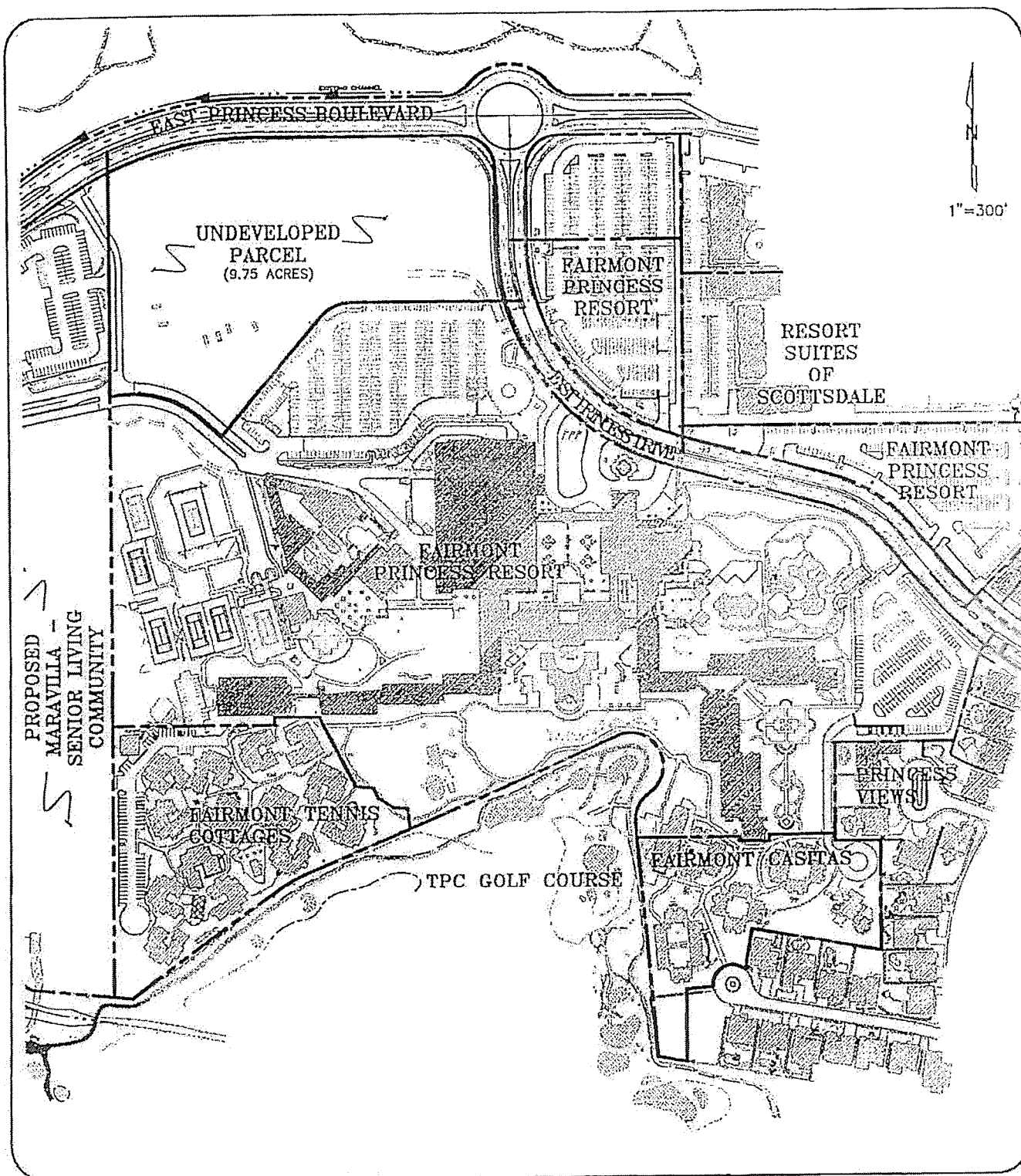


EXHIBIT 1

FAIRMONT SCOTTSDALE
PRINCESS RESORT

ENGINEER	J. Bulka
DESIGNER	J. Haywood
CAD TECHNICIAN	J. Sanchez

SCALE	1"=300'
DATE	07/14/08
JOB NUMBER	07910
REF. SHEET	1 OF 1

**WOOD/PATEL &
ASSOCIATES INC.**
Civil Engineers, Hydrologists
and Land Surveyors

1855 North Stapley Drive
Mesa, Arizona 85203
(480) 834-3300
(480) 834-3320 FAX

October 23, 2008

WP# 072910

Sheet 1 of 2

Attachment to Stormwater Storage Waiver Request
for Fairmont Scottsdale Princess Resort & Regional Flood Control

The Fairmont Scottsdale Princess Resort (Site) is a 60 acre resort located near the southwest corner of Princess Boulevard and Princess Drive. The Site is bounded by the Princess Blvd. to the north, the Maravilla Scottsdale Senior Living Community to the east, the TPC Golf Course to the south and existing residential developments to the west (see Exhibit 1, attached). The existing Fairmont Scottsdale Princess Resort consists of multiple hotel buildings, a ballroom, spa, tennis cottages, tennis courts, and parking. A majority of the site is developed and portions are being updated and renovated. At the north end of the site there is a 9.75 acre portion of the property that has yet to be developed, and other portions are scheduled for upgrades.

It is Wood/Patel's understanding that the ownership of the Fairmont Scottsdale Princess Resort, Strategic Hotels and Resorts, has agreed to fund regional flood control improvements to the public road/channel crossing at Princess Blvd and Scottsdale Road, in return for the City approving this waiver and it being applicable to the entire site. The improvements consist of removing the existing concrete box culvert crossing and replacing it with a bridge structure. The cost of a new bridge structure is estimated at \$1,053,000.

City of Scottsdale In-Lieu Fees:

$V(\text{req}) \text{ Volume required} = \text{CRA} = (0.90) \times (0.235 \text{ feet}) \times (9.75 \text{ acres}) = 89,826 \text{ cu-ft.}$

$C \text{ (Runoff Coefficient)} = 0.90$

$R \text{ (100-year/2-hour precipitation depth)} = 0.235 \text{ feet}$

$\text{Site area} = 9.75 \text{ acres}$

$\text{City of Scottsdale In-Lieu Fees} = V(\text{req}) \times \$3.22 = (89,826 \text{ cu-ft}) \times \$3.22 = \$289,240$

Summary:

Public Drainage Improvements = \$1,053,000 (*)

City of Scottsdale in Lieu Fee = \$289,240

(*) See Sheet 2 of 2 Engineering Preliminary Opinion of Probable Cost

October 23, 2008

WP# 072910

Sheet 2 of 2

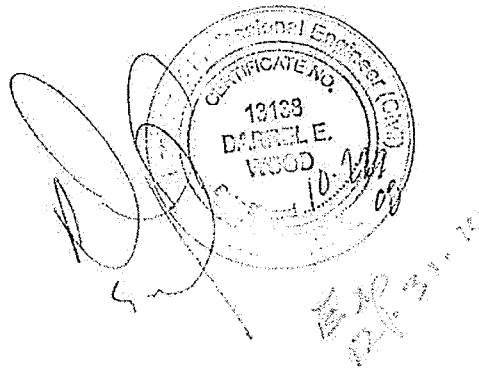
Attachment to Stormwater Storage Waiver Request
for Fairmont Scottsdale Princess Resort & Regional Flood Control

Engineering Preliminary Opinion of Probable Cost (*)

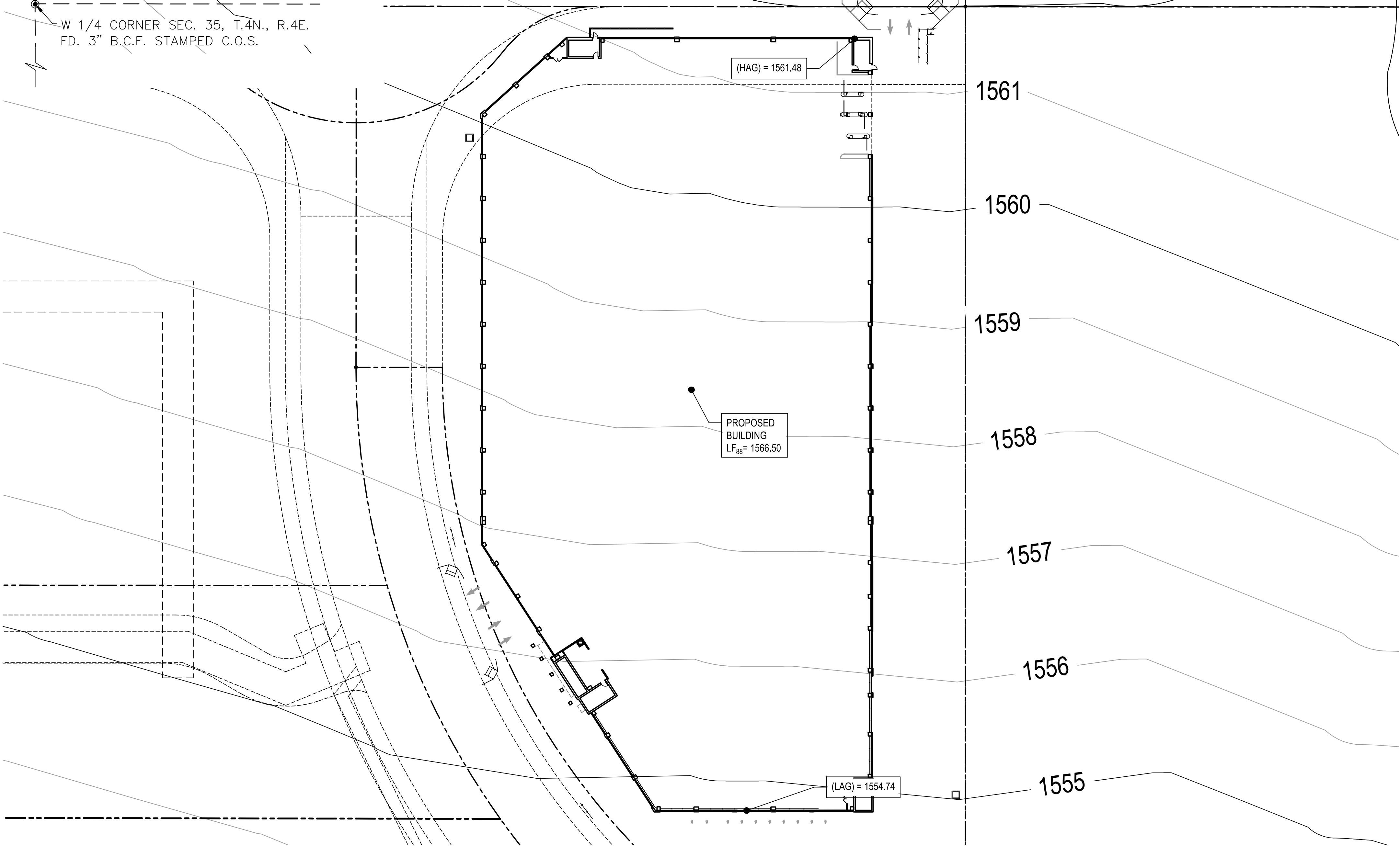
Proposed
Prepared Bridge Structure at Princess Drive, just east of Scottsdale Road serving unnamed wash.

Estimated Bridge Surface = 8,100 square feet x \$130/s.f. \$1,053,000

(*) Offered without the benefit of construction documents and specifications.



**APPENDIX B – REGIONAL CONTOUR MAP / OPINION OF EXISTING HIGHEST NATURAL
GRADE ELEVATION**



FEMA SUMMARY TABLE								
NAME	ADDRESS	LOWEST FINISHED FLOOR ELEVATION (LF88)	HIGHEST ADJACENT NATURAL GRADE	LOWEST ADJACENT NATURAL GRADE	REGULATORY FLOOD ELEVATION	FEMA REQUIREMENTS		
BUILDINGS						FLOOD VENTING	WET FLOODPROOFING	OTHER
VILLA 1	7575	1566.50	1,561.48	1,554.74	1,563.48	NO VENT	NOT REQUIRED	N/A

LEGEND

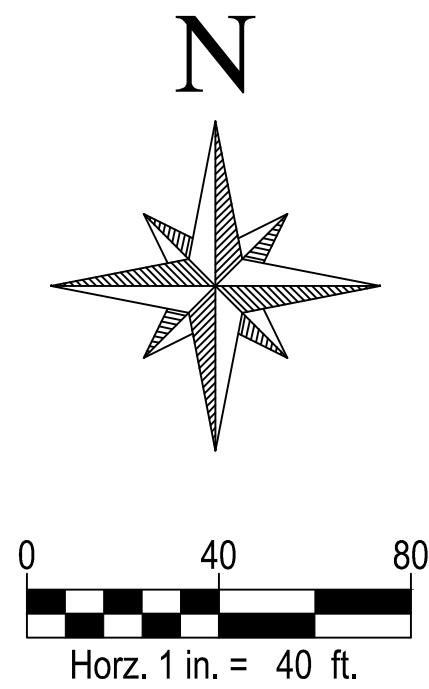
	PROPOSED BUILDING OUTLINE
	BOUNDARY LINE
	SECTION LINE
	ESTIMATED 5' CONTOUR NAVD88 DATUM
	ESTIMATED 1' CONTOUR NAVD88 DATUM
	ORIGINAL 1964 CURRYS CORNER CONTOURS ON NAVD88 DATUM
	HAG HIGHEST ADJACENT NATURAL GRADE
	LAG LOWEST ADJACENT NATURAL GRADE
	RFD REGULATORY FLOOD DEPTH = HAG +2' (ZONE AO DEPTH (1') = 1' FREEBOARD)
	LGF LOWEST GARAGE FLOOR

ELEVATION STATEMENT

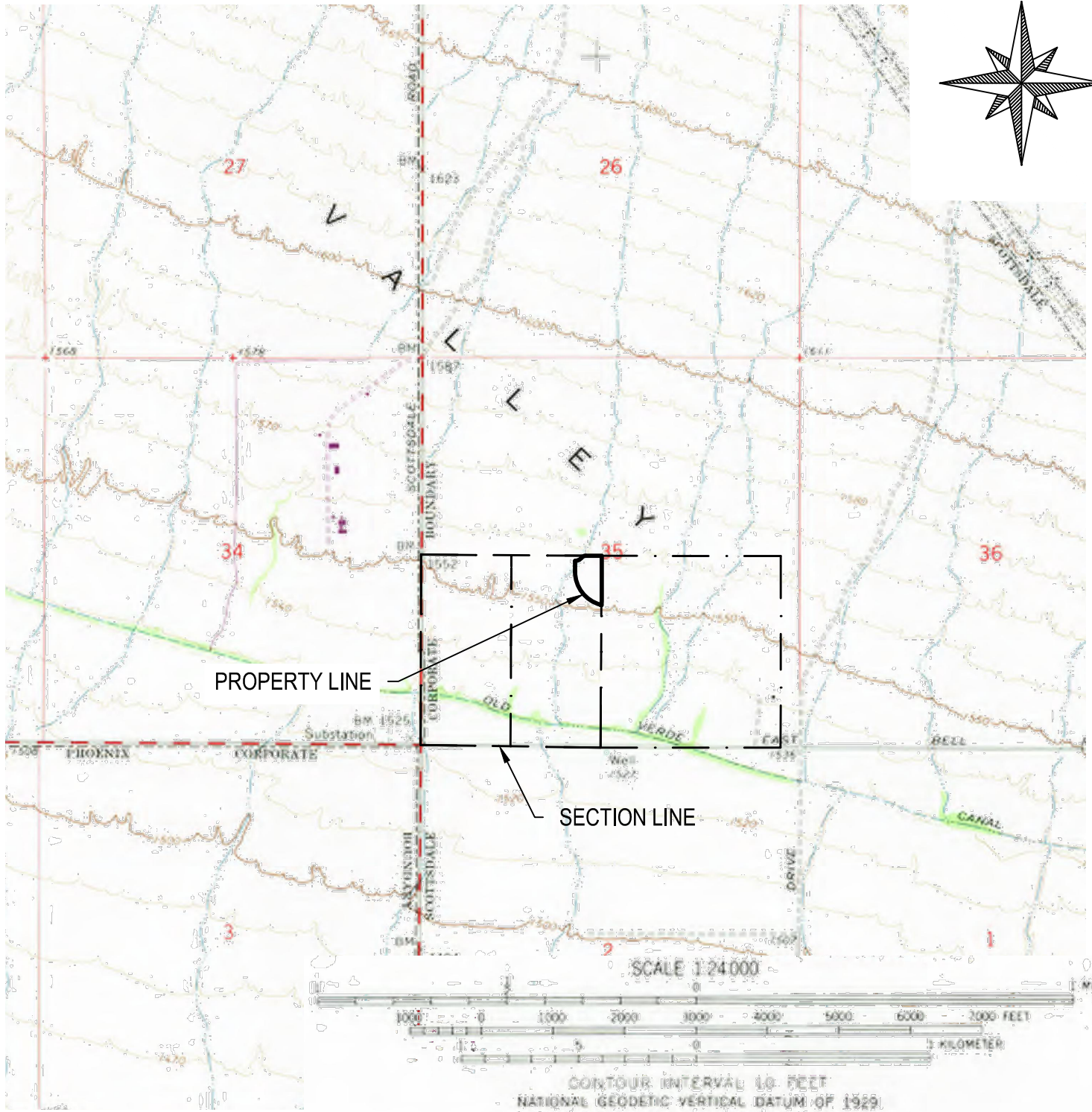
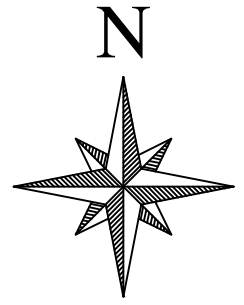
THE WORK PRODUCT PRESENTED IS THE RESULT OF OBTAINING BEST AVAILABLE HISTORICAL ELEVATION INFORMATION, AND EMPLOYING PROFESSIONAL JUDGMENT TO BEST PRESENT IN SITE GROUND ELEVATIONS. ELEVATIONS ARE BASED ON 1964 CURRYS CORNER NGVD29 DATUM CONVERTED TO NAVD88 USING MARICOPA LAND SURVEY CONVERSION OF 1.749 FT.

BENCHMARK

THE VERTICAL DATUM FOR THIS EXHIBIT IS BASED ON GDACS POINT 43017-1, 3 INCH CITY OF SCOTTSDALE BRASS CAP FLUSH LOCATED ON SCOTTSDALE ROAD SOUTH OF PRINCESS DRIVE HAVING AN ELEVATION OF 1552.985, CITY OF SCOTTSDALE NAVD88 DATUM.



- 1) WHEN REQUIRED AS INDICATED ABOVE, FLOOD VENTS SHALL BE PROVIDED ON AT LEAST 2 SEPARATE WALLS. THE FLOOD VENTS SHALL HAVE ONE SQUARE INCH OF OPENING SPACE FOR EVERY SQUARE FOOT OF ENCLOSED SPACE BELOW THE REGULATORY FLOOD ELEVATION, OR AS NOTED ABOVE. SEE ARCHITECTURAL PLANS FOR VENTS OPENINGS. PROPOSED GRADE ADJACENT TO BUILDING MAY EFFECT VENT LOCATIONS, CONSULT ENGINEER PRIOR TO CONSTRUCTION WITH ANY QUESTIONS.
- 2) WHEN REQUIRED AS INDICATED ABOVE, WET FLOODPROOFING SHALL BE PROVIDED UP TO THE REGULATORY FLOOD DEPTH. WET FLOODPROOFING CONSIST OF CONSTRUCTION WITH FLOOD RESISTANT MATERIALS.
- 3) WHEN REQUIRED AS NOTED ABOVE, ELECTRICAL AND MECHANICAL EQUIPMENT SHALL BE ELEVATED ABOVE THE REGULATORY FLOOD DEPTH.
- 4) PROPOSED BUILDING M1 WILL BE A STRUCTURALLY INDEPENDENT NON-RESIDENTIAL STRUCTURE.
- 5) FEMA DEFINES DRY FLOODPROOFING AS A COMBINATION OF MEASURES THAT RESULT IN A STRUCTURE, INCLUDING THE ATTENDANT UTILITIES AND EQUIPMENT, BEING WATERTIGHT WITH ALL ELEMENTS SUBSTANTIALLY IMPERMEABLE TO THE ENTRANCE OF FLOODWATER AND WITH STRUCTURAL COMPONENTS HAVING THE CAPACITY TO RESIST FLOOD LOADS.



**NOT
FOR
CONSTRUCTION
OR RECORDING**

**WOOD
PATEL**

PARKING GARAGE EXHIBIT

REGIONAL CONTOUR MAP/OPINION OF EXISTING HIGHEST NATURAL GRADE ELEVATION

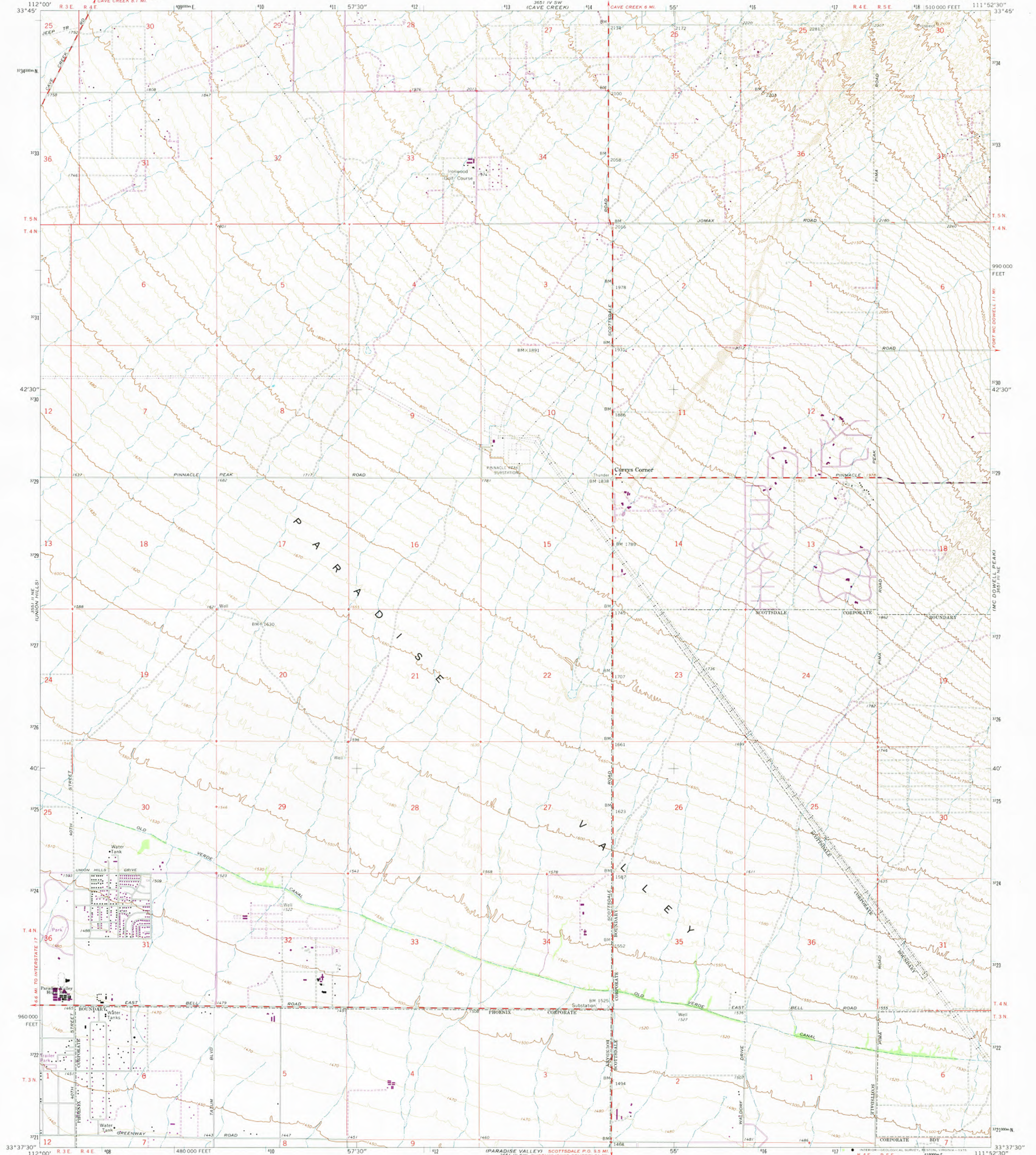
DATE	06/02/2023	SCALE	1" = 1'	SHEET	2 OF 2
JOB NO.	215319.40	DESIGN	RS	CHECK	RS
		DRAWN	AJS	RFI #	N/A

Z:\2021\215319\Project Support\Reports\5319.40 - Parking Structure\Drainage\Exhibits\5319.40 Exhibit - Regional Contour Map 2.dwg

APPENDIX C – CURRY’S CORNER QUADRANGLE MAP

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

CURRYS CORNER QUADRANGLE
ARIZONA—MARICOPA CO.
7.5 MINUTE SERIES (TOPOGRAPHIC)



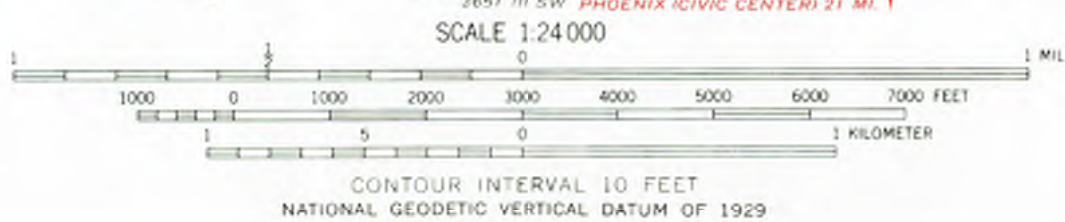
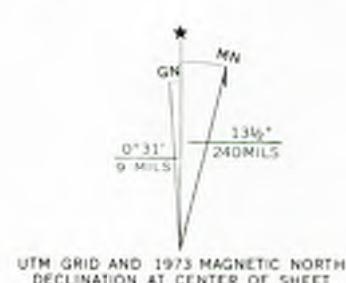
Mapped, edited, and published by the Geological Survey

Control by USGS and USC&GS

Topography by photogrammetric methods from aerial
photographs taken 1962. Field checked 1964

Polyconic projection. 1927 North American datum
10,000-foot grid based on Arizona coordinate system, central zone
1000-meter Universal Transverse Mercator grid ticks,
zone 12, shown in blue

Revisions shown in purple compiled from aerial photographs
taken 1973. This information not field checked



USGS
Historical File
Topographic Division

CURRYS CORNER, ARIZ.
N3337.5—W1152.5/7.5

1964
PHOTOREVISED 1973
AMS 3651 III NW—SERIES V898

MAR 20 1975

APPENDIX D – HYDROLOGIC AND HYDRAULIC CALCULATIONS

IDF DATA FROM FCDMC NOAA – ATLAS 14 PRECIPITATION DATA

SITE I-D-F CURVE

Project Fairmont Scottsdale Princess - Parking Structure
Location Scottsdale AZ
Project Number 215319.4
Project Engineer Darin Moore, PE

RAINFALL DEPTHS, INCHES

Duration	Average Recurrence Interval (years)					
	2	5	10	25	50	100
5-min	0.255	0.344	0.413	0.505	0.576	0.649
10-min	0.389	0.524	0.629	0.769	0.876	0.987
15-min	0.481	0.650	0.779	0.953	1.090	1.220
30-min	0.648	0.875	1.050	1.280	1.460	1.650
60-min	0.802	1.080	1.300	1.590	1.810	2.040
2-hr	0.927	1.230	1.470	1.790	2.030	2.290
3-hr	1.010	1.330	1.570	1.920	2.190	2.480
6-hr	1.200	1.540	1.800	2.160	2.440	2.740
12-hr	1.350	1.710	1.990	2.360	2.650	2.950
24-hr	1.590	2.060	2.430	2.950	3.360	3.780

RAINFALL INTENSITY, INCHES/HOUR

Duration minutes	Frequency, years					
	2	5	10	25	50	100
5	3.06	4.13	4.96	6.06	6.91	7.79
10	2.33	3.14	3.77	4.61	5.26	5.92
15	1.92	2.60	3.12	3.81	4.36	4.88
30	1.30	1.75	2.10	2.56	2.92	3.30
60	0.80	1.08	1.30	1.59	1.81	2.04
120	0.46	0.62	0.74	0.90	1.02	1.15
180	0.34	0.44	0.52	0.64	0.73	0.83
360	0.20	0.26	0.30	0.36	0.41	0.46
720	0.11	0.14	0.17	0.20	0.22	0.25
1440	0.07	0.09	0.10	0.12	0.14	0.16

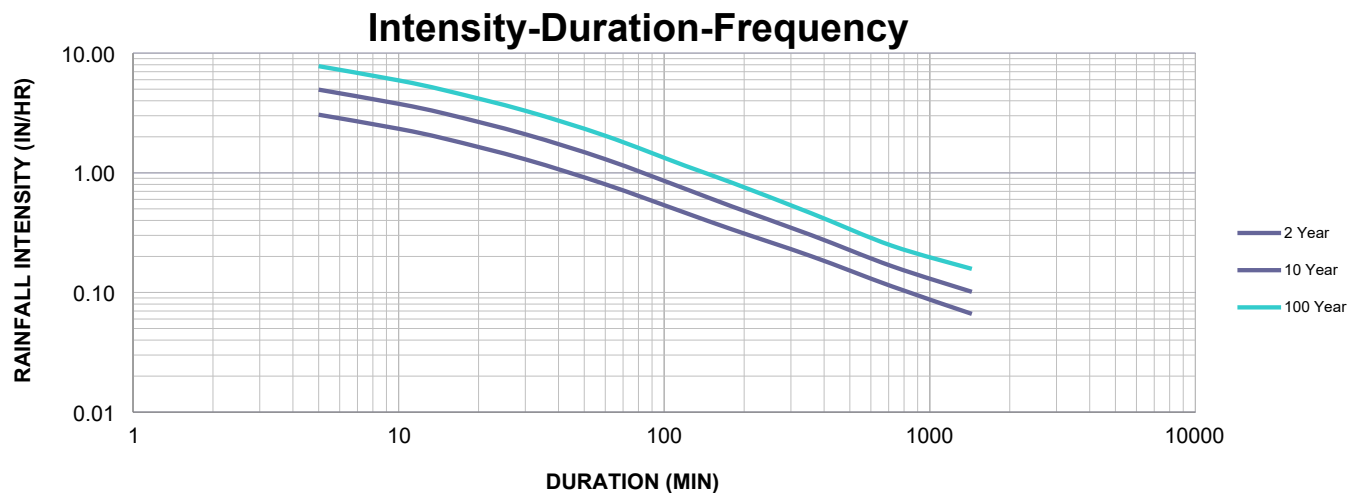


TABLE 1 – EXISTING WEIGHTED C VALUES

**COMPOSITE
WEIGHTED "C"
FACTOR
CALCULATIONS
100 YEAR**

Project Fairmont Scottsdale Princess - Parking Structure
Location Scottsdale AZ
Project Number 215319
Project Engineer Darin Moore, PE

Existing C Factor

Drainage Subbasin ID	Area	Paved		Desert		100 YR Runoff Coefficient
(Description/ID)	(Acres)	%	"C"	%	"C"	"C"
A-1	5.37	81.84	0.95	18.16	0.83	0.93

TABLE 2 – PROPOSED WEIGHTED C VALUES 100-YEAR

**COMPOSITE
WEIGHTED "C"
FACTOR
CALCULATIONS
100 YEAR**

Project Fairmont Scottsdale Princess - Parking Structure
Location Scottsdale AZ
Project Number 215319
Project Engineer Darin Moore, PE

Existing C Factor

Drainage Subbasin ID	Area	Paved		Desert		100 YR Runoff Coefficient
(Description/ID)	(Acres)	%	"C"	%	"C"	"C"
A-1	2.62	100	0.95	0	0.83	0.95
A-2	0.94	65	0.95	35	0.83	0.91
A-3	0.49	74	0.95	26	0.83	0.92
A-4	0.46	47	0.95	53	0.83	0.89
A-5	0.51	70	0.95	30	0.83	0.91
A-6	0.16	62	0.95	38	0.83	0.90
A-7	0.19	58	0.95	42	0.83	0.90

TABLE 3 – PROPOSED WEIGHTED C VALUES 10-YEAR

**COMPOSITE
WEIGHTED "C"
FACTOR
CALCULATIONS
10 YEAR**

Project Fairmont Scottsdale Princess - Parking Structure
Location Scottsdale AZ
Project Number 215319
Project Engineer Darin Moore, PE

Existing C Factor

Drainage Subbasin ID	Area	Paved		Desert		10 YR Runoff Coefficient
(Description/ID)	(Acres)	%	"C"	%	"C"	"C"
A-1	2.62	100	0.90	0	0.63	0.90
A-2	0.94	65	0.90	35	0.63	0.81
A-3	0.49	74	0.90	26	0.63	0.83
A-4	0.46	47	0.90	53	0.63	0.76
A-5	0.51	70	0.90	30	0.63	0.82
A-6	0.16	62	0.90	38	0.63	0.80
A-7	0.19	58	0.90	42	0.63	0.79

TABLE 4 – EXISTING RATIONAL METHOD



RATIONAL METHOD SUMMARY
100 YEAR, 10 YEAR

Project Fairmont Scottsdale Princess - Parking Structure
Location Scottsdale AZ
Project Number 215319.4
Project Engineer Darin Moore, PE

EXISTING ON-SITE WATERSHEDS										100 YEAR				10 YEAR			
Drainage Subbasin ID	Longest Watercourse 'L' (ft)	Longest Watercourse 'L' (mi)	Drainage Area 'A' (sf)	Drainage Area 'A' (Acres)	'K _b ' Type ¹	Watershed Resistance Coefficient 'K _b '	Top Elevation	Bottom Elevation	Basin Slope 'S' (ft/mi)	Calculated Q100 'Tc' (See Note 2) (min)	100 YEAR Intensity 'i' (in/hr)	100 YR Runoff Coefficient 'C'	Q100 Flow (cfs)	Calculated Q10 'Tc' (See Note 2) (min)	10 YEAR Intensity 'i' (in/hr)	10 YR Runoff Coefficient 'C'	Q10 Flow (cfs)
A1	617	0.117	233,883	5.37	A	0.0354	63.8	53.5	88.2	5.0	7.79	0.93	38.8	5.7	4.79	0.93	23.9
													38.8	23.9			

- Notes
- 1. Per Drainage Design Manual for Maricopa County, Vol. I, Hydrology (2013), Table 3.1: Equation for Estimating Kb in the Tc Equation
 - 2. Minimum Tc is 5 minutes.

TABLE 5 – PROPOSED RATIONAL METHOD



STORMCEPTOR RATIONAL METHOD SUMMARY

100 YEAR, 10 YEAR

Project Fairmont Scottsdale Princess - Parking Structure

Location Scottsdale AZ

Project Number 215319.4

Project Engineer Darin Moore, PE

PROPOSED ON-SITE WATERSHEDS										100 YEAR				10 YEAR			
Drainage Subbasin ID	Longest Watercourse 'L' (ft)	Longest Watercourse 'L' (mi)	Drainage Area 'A' (sf)	Drainage Area 'A' (Acres)	'K _b ' Type ¹	Watershed Resistance Coefficient 'K _b '	Top Elevation	Bottom Elevation	Basin Slope 'S' (ft/mi)	Calculated Q100 'Tc' (See Note 2) (min)	100 YEAR Intensity 'i' (in/hr)	100 YR Runoff Coefficient 'C'	Q100 Flow (cfs)	Calculated Q10 'Tc' (See Note 2) (min)	10 YEAR Intensity 'i' (in/hr)	10 YR Runoff Coefficient 'C'	Q10 Flow (cfs)
A-1	300	0.057	114,201	2.62	A	0.0374	3.0	0.0	52.8	5.0	7.79	0.95	19.4	5.0	4.96	0.90	11.7
A-2	424	0.080	40,881	0.94	A	0.0402	63.5	53.5	124.5	5.0	7.79	0.91	6.6	5.0	4.96	0.81	3.7
A-3	305	0.058	21,269	0.49	A	0.0419	63.4	54.5	154.1	5.0	7.79	0.92	3.5	5.0	4.96	0.83	2.0
A-4	395	0.075	20,017	0.46	A	0.0421	58.0	54.6	45.5	5.1	7.75	0.91	3.2	6.1	4.70	0.76	1.6
A-5	228	0.043	22,082	0.51	A	0.0418	56.0	55.3	16.2	5.3	7.68	0.91	3.6	6.4	4.63	0.82	1.9
A-6	72	0.014	6,916	0.16	A	0.0450	66.0	53.5	916.7	5.0	7.79	0.89	1.1	5.0	4.96	0.80	0.6
A-7	120	0.023	8,282	0.19	A	0.0445	66.0	53.5	550.0	5.0	7.79	0.91	1.4	5.0	4.96	0.79	0.7
Total			233,649	5.36									38.78				22.39

- Notes
1. Per Drainage Design Manual for Maricopa County, Vol. I, Hydrology (2013), Table 3.1: Equation for Estimating Kb in the Tc Equation
2. Minimum Tc is 5 minutes.

TABLE 6 – FIRST FLUSH FLOW

First Flush Flow

Project Fairmont Scottsdale Princess - Parking Structure
Location Scottsdale AZ
Project Number 215319.4
Project Engineer Darin Moore, PE

Proposed First Flush Flow

Drainage Subbasin ID	Runoff Coefficient 'C'	Time of Concentration 'T _c ' (min)	First Flush Intensity 'I _{FF} ' (in/hr)	Drainage Area 'A' (Acres)	First Flush Flow 'Q _{FF} ' (cfs)
A-1	1.00	5.00	0.100	2.62	0.26
A-2	1.00	5.00	0.100	0.94	0.09
A-3	1.00	5.00	0.100	0.49	0.05
A-4	1.00	6.12	0.082	0.46	0.04
A-5	1.00	6.43	0.078	0.51	0.04
A-6	1.00	5.00	0.100	0.16	0.02
A-7	1.00	5.00	0.100	0.19	0.02
Total					0.52

Notes

- Per Drainage Policies and Standards for Maricopa County, AZ, June 2016, Standard 6.4.1: First Flush

$$Q_{FF} = C I_{FF} A$$

$$I_{FF} = P_{FF} / T_C$$

$$P_{FF} = 0.5 \text{ inches}$$

TABLE 7 – CATCH BASIN INLET SUMMARY

CATCH BASIN INLET SUMMARY

CATCH BASIN INTERCEPTION CAPACITY AND BY-PASS FLOWS

Project Fairmont Scottsdale Princess - Parking Structure
Location Scottsdale AZ
Project Number 215319.40
Project Engineer Darin Moore, PE

Catch Basin ID	Catch Basin Type	On-Grade or Sump	Post Q10 Flow (cfs)	Post Q100 Flow (cfs)	Intercept Capacity (cfs)
CB-A3	MAG 535	Sump	2.2	3.4	5.0
CB-A4	MAG 535	Sump	1.3	2.0	5.0
CB-A5	MAG 535	Sump	2.1	3.6	5.0
CB-A6	MAG 535	Sump	0.7	1.1	5.0
CB-A7	MAG 535	Sump	0.9	1.4	5.0

Notes

APPENDIX E – STORMCAD MODELING RESULTS

FlexTable: Conduit Table

Label	Start Node	Invert (Start) (ft)	Stop Node	Invert (Stop) (ft)	Length (Scaled) (ft)	Slope (Calculated) (ft/ft)	Diameter (in)	Manning's n	Headloss (ft)	Flow (cfs)	Velocity (ft/s)
CO-1	CB-A1	1,556.00	CB-A3	1,554.40	120.3	0.013	15.0	0.013	1.22	6.50	5.30
CO-2	CB-A3	1,554.40	CB-A5	1,552.40	204.5	0.010	15.0	0.013	3.46	8.40	6.84
CO-3	CB-A5	1,552.40	MH-5	1,552.22	35.8	0.005	15.0	0.013	0.77	9.50	7.74
CO-4	MH-5	1,552.22	MH-6	1,551.90	66.6	0.005	15.0	0.013	1.44	9.50	7.74
CO-5	MH-6	1,551.90	MH-7	1,551.74	33.0	0.005	24.0	0.013	0.05	10.80	5.40
CO-6	MH-7	1,551.74	O-1	1,551.35	192.5	0.002	30.0	0.013	0.30	16.00	4.23
CO-7	H-A2	1,553.50	MH-8	1,552.60	196.1	0.005	12.0	0.013	2.12	3.70	4.71
CO-8	MH-8	1,552.60	CB-A4	1,552.52	31.3	0.003	12.0	0.013	0.34	3.70	4.71
CO-9	CB-A4	1,552.52	MH-7	1,551.74	138.9	0.006	12.0	0.013	2.96	5.20	6.62
CO-10	CB-A6	1,552.25	MH-6	1,551.90	68.5	0.005	12.0	0.013	0.02	0.60	0.76
CO-11	CB-A7	1,552.15	MH-6	1,551.90	48.6	0.005	12.0	0.013	0.02	0.70	0.89

Catch Basin FlexTable: CatchBasin Table

Label	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Flow (Additional Subsurface) (cfs)	Flow (Total Out) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
CB-A1	1,563.79	1,556.00	6.50	6.50	1,559.33	1,559.33
CB-A3	1,559.40	1,554.40	1.90	8.40	1,558.11	1,558.11
CB-A4	1,554.60	1,552.52	1.50	5.20	1,554.60	1,554.60
CB-A5	1,554.65	1,552.40	1.10	9.50	1,554.65	1,554.65
CB-A6	1,554.25	1,552.25	0.60	0.60	1,553.72	1,553.72
CB-A7	1,554.45	1,552.15	0.70	0.70	1,553.72	1,553.72

FlexTable: Manhole Table

Label	Elevation (Rim) (ft)	Flow (Total Out) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Absolute Headloss (ft)
MH-5	1,554.91	9.50	1,554.91	1,554.91	0.00
MH-6	1,555.91	10.80	1,553.70	1,553.70	0.00
MH-7	1,557.04	16.00	1,553.65	1,553.65	0.00
MH-8	1,554.86	3.70	1,554.86	1,554.86	0.00

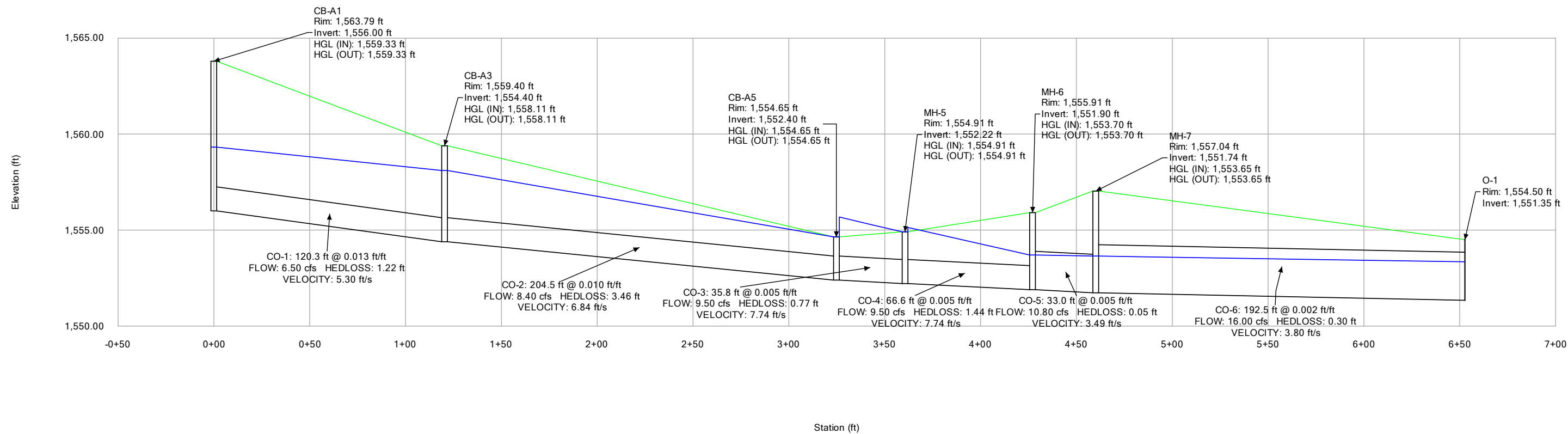
Label	Elevation (Invert) (ft)	Elevation (Ground) (ft)	Flow (Total Out) (cfs)	Boundary Condition Type	Network Boundary Type
H-A2	1,553.50	1,555.00	3.70	Free Outfall	Inlet

FlexTable: Headwall Table

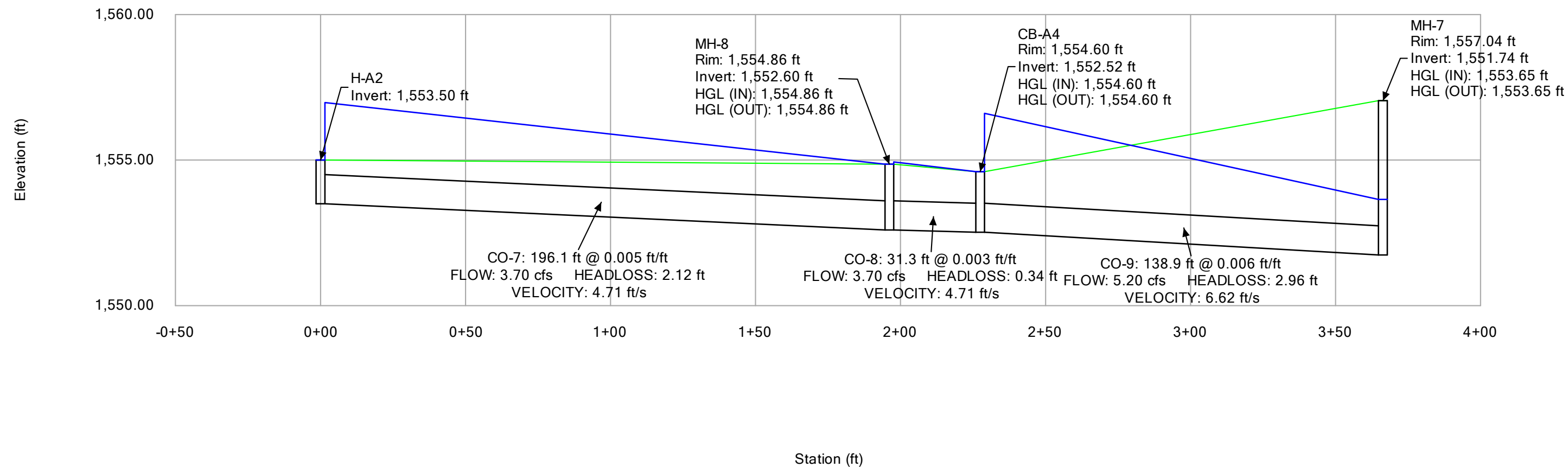
FlexTable: Outfall Table

Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)
O-1	1,554.50	1,551.35	User Defined Tailwater	1,553.35	1,553.35	16.00

Profile Report
Engineering Profile - CB-A1 TO O-1 (5319.40-StormCAD.stsw)



Profile Report
Engineering Profile - H-A2 TO MH-7 (5319.40-StormCAD.stsw)



APPENDIX F – CONTECH CDS3020-6-C TREATMENT SYSTEM

HYDRAULIC DESIGN SUMMARY FOR INLINE MODEL CDS3020

The following hydraulic summary supports the design of the CDS model proposed on the FAIRMONT SCOTTSDALE PRINCESS – SUNSET VILLAS & BUNGALOWS project located in SCOTTSDALE, AZ . The attached hydraulic calculations supporting the proposed CDS structure's design serve two purposes.

1. To ensure the proposed CDS model will achieve the design treatment capacity under the site-specific hydraulic conditions.

The proposed CDS model CDS3020 unit is designed to process a treatment flow of 0.54-cfs. Under the site-specific conditions, the proposed 17-inch tall diversion weir will generate the operational energy necessary to achieve the 0.54-cfs design treatment flow rate.

2. To quantify the hydraulic losses introduced to the conveyance system under peak design conditions.

A flow of 22.39-cfs represents the peak discharge generated by the contributing drainage area for a design storm having a 10 year return interval. Under these peak design conditions, all of the 22.39-cfs flow is assumed to be conveyed over the diversion weir. This conservative assumption predicts the worst-case resulting hydraulic condition and preserves the integrity of this calculation even if the structure is not properly maintained.

Based on the information provided, the proposed CDS model CDS3020 is predicted to increase the upstream Hydraulic Gradeline (ΔHGL) by 2.57 ft for the above cited peak design flow.

$$\Delta HGL = H_{CDS} = 2.57 \text{ ft}$$

The effective headloss coefficient across the proposed CDS model CDS3020 for the 10-year storm event may be estimated as a function of the velocity in the downstream pipe.

where,

$$\begin{aligned} K_{CDS} &= \text{CDS Headloss Coefficient:} \\ &= H_{CDS} / [V_{d/s}^2 / 2 \cdot g] \\ &= 3.52 \end{aligned}$$

If a software program is being used to develop the Hydraulic Gradeline (HGL) for the upstream conveyance system, the values listed above for H_{CDS} and/or K_{CDS} can be used as either a headloss factor to be multiplied by the downstream velocity head, or input the headloss amount for the proposed CDS model at the corresponding node.



**INLINE
HYDRAULIC CALCULATIONS**
FAIRMONT SCOTTSDALE PRINCESS – SUNSET VILLAS & BUNGALOWS
SCOTTSDALE, AZ
742047-20

**DESIGN PARAMETERS**

CDS Model No. = CDS3020
 Design Treatment Flow = 0.5 cfs
 Peak Design Flow = 22.39 cfs
 Peak Design Return Interval = 10 year
 Rim Elevation @ US Structure = 1557.59 ft

DETAILED CALCULATIONS**TREATMENT FLOW**

Tailwater Condition at Outfall, EL_0

$EL_0 =$ 1,551.80 ft (invert plus depth of flow at D/S outlet)

Exit Loss from DownStream Pipe, h_1

$$h_1 = k * [V^2 / (2 * g)]$$

where,

$$k = \frac{1.00}{V = Q / A_F}$$

$$= 1.98 \text{ fps}$$

$$h_1 = \frac{0.06}{\text{ft}}$$

$$EGL_1 = EL_0 + h_1$$

$$= \frac{1551.86}{\text{ft}}$$

Head Loss Through Downstream Pipe, h_2

Friction Losses, h_2

$$h_2 = S_{EGL} * L$$

where,

$$L = \frac{20}{\text{ft}}$$

$$S_{EGL} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\text{Dia.} = \frac{30}{\text{in}}$$

$$S_{PIPE} = \frac{0.0100}{\text{ft/ft}}$$

$$n = \frac{0.013}{\text{ft}}$$

Flow Characteristics

$$d_F = \frac{0.26}{\text{ft}}$$

$$A_F = \frac{0.27}{\text{sf}}$$

$$P_W = \frac{1.65}{\text{ft}}$$

$$R = \frac{0.17}{\text{ft}}$$

$$S_{EGL} = \underline{0.00327} \text{ ft / ft}$$

$$h_2 = \underline{0.0654} \text{ ft}$$

$$\begin{aligned} EGL_2' &= EGL_1 + h_2 \\ &= \underline{1551.93} \text{ ft} \end{aligned}$$

Check Entrance Condition for Critical Depth Control

$$EL_{CDS \text{ Inv.}} = \underline{1551.74} \text{ ft}$$

$$d_c = \underline{0.25} \text{ ft}$$

$$\begin{aligned} EGL_C &= EL_{CDS \text{ Inv.}} + d_c + V_{dc}^2 / (2 \cdot g) \\ &= \underline{1552.06} \text{ ft} \end{aligned}$$

Identify Controlling EGL

Friction based EGL controls.

$$EGL_2 = \underline{1551.93} \text{ ft}$$

Re-entry Loss into DownStream Pipe, h_3

$$h_3 = k \cdot [V^2 / (2 \cdot g)]$$

where,

$$k = \underline{0.20}$$

$$V = Q / A$$

$$= \underline{1.98} \text{ fps (area based on flow depth)}$$

$$h_3 = \underline{0.01} \text{ ft}$$

$$\begin{aligned} EGL_3' &= EGL_2 + h_3 \\ &= \underline{1551.94} \text{ ft} \end{aligned}$$

Oil Baffle Loss, h_4

$$h_4 = k \cdot [V^2 / (2 \cdot g)]$$

where,

$$k = \underline{1.00}$$

$$A_{\text{Baffle}} = \underline{6.49} \text{ sf}$$

$$V = Q / A_{\text{baffle}}$$

$$= \underline{0.08} \text{ fps}$$

$$h_4 = \underline{0.0001} \text{ ft}$$

$$\begin{aligned} EGL_4 &= EGL_3 + h_4 \\ &= \underline{1551.94} \text{ ft} \end{aligned}$$

Check Standard Weir Elevation

$$HL_{CDS} = \underline{0.50} \text{ ft}$$

$$\begin{aligned} EL_W' &= EGL_4 + HL_{CDS} \\ &= \underline{1552.44} \text{ ft} \end{aligned}$$

$$H_W' = EL_W' - EL_{CDS \text{ INV.}}$$

$$= \underline{0.70} \text{ ft, or } \underline{8.40} \text{ in}$$

$$\text{Std. Weir Height} = \underline{17.0} \text{ in}$$

Status **OK**

$$\text{Use } H_W = \underline{17} \text{ in, or } \underline{1.42} \text{ ft}$$

$$\begin{aligned} EL_W &= EL_{CDS \text{ INV.}} + H_W \\ &= \underline{1553.16} \text{ ft} \end{aligned}$$

PEAK CONVEYANCE FLOW

6/2/2023

Tailwater Condition at Outfall, EL_0

$$EL_0 = \underline{1,552.81} \text{ ft (invert plus depth of flow at D/S outlet)}$$

Exit Loss from DownStream Pipe, h_1

$$h_1 = k * [V^2 / (2 * g)]$$

where,

$$\begin{aligned} k &= \underline{1.00} \\ V &= Q / A_F \\ &= \underline{8.97} \text{ fps} \end{aligned}$$

$$h_1 = \underline{1.25} \text{ ft}$$

$$\begin{aligned} EGL_1 &= EL_0 + h_1 \\ &= \underline{1554.06} \text{ ft} \end{aligned}$$

Head Loss Through Downstream Pipe, h_2

Friction Losses, h_2

$$h_2 = S_{EGL} * L$$

where,

$$L = \underline{20} \text{ ft}$$

$$S_{EGL} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\begin{aligned} \text{Dia.} &= \underline{30} \text{ in} \\ S_{PIPE} &= \underline{0.0100} \text{ ft/ft} \\ n &= \underline{0.013} \end{aligned}$$

Flow Characteristics

$$\begin{aligned} d_n &= \underline{1.27} \text{ ft} \\ A_F &= \underline{2.49} \text{ sf} \\ P_W &= \underline{3.96} \text{ ft} \\ R &= \underline{0.63} \text{ ft} \end{aligned}$$

$$S_{EGL} = \underline{0.0114} \text{ ft / ft}$$

$$h_2 = \underline{0.23} \text{ ft}$$

$$\begin{aligned} EGL_2' &= EGL_1 + h_2 \\ &= \underline{1554.28} \text{ ft} \end{aligned}$$

Check Entrance Condition for Critical Depth Control

$$EL_{CDS \text{ Inv.}} = \underline{1551.74} \text{ ft}$$

$$d_c = \underline{1.58} \text{ ft}$$

$$\begin{aligned} EGL_C &= EL_{CDS \text{ Inv.}} + d_c + V_{dc}^2 / (2 * g) \\ &= \underline{1554.05} \text{ ft} \end{aligned}$$

Identify Controlling EGL

Flow enters pipe at critical depth, EGL_C controls.

$$EGL_2 = \underline{1554.05} \text{ ft}$$

Re-entry Loss into DownStream Pipe, h_3

$$h_3 = k * [V^2 / (2 * g)]$$

where,

$$k = \frac{0.20}{V = Q / A_F} = \frac{6.85}{\text{fps (area based on critical depth)}}$$

$$h_3 = \frac{0.15}{\text{ft}}$$

$$\begin{aligned} \text{EGL}_3 &= \text{EGL}_2 + h_3 \\ &= \frac{1554.19}{\text{ft}} \end{aligned}$$

Oil Baffle Loss, h_4

$$h_4 = k * [V^2 / (2 * g)]$$

where,

$$\begin{aligned} k &= \frac{0.00}{A_{\text{Baffle}} = \frac{6.49}{\text{sf}}} \quad (\text{Skirted-baffle model}) \\ V &= \frac{Q}{A_{\text{Baffle}}} = \frac{3.45}{\text{fps}} \end{aligned}$$

$$h_4 = \frac{0.00}{\text{ft}}$$

$$\begin{aligned} \text{EGL}_4 &= \text{EGL}_3 + h_4 \\ &= \frac{1554.19}{\text{ft}} \end{aligned}$$

$$\begin{aligned} \text{HGL}_4 &= \text{EGL}_4 - [V_P^2 / (2 * g)] \\ &= \frac{1553.47}{\text{ft}} \end{aligned}$$

Head over Diversion Weir, h_5

Elevation of Weir

$$\text{EL}_{\text{Weir}} = \frac{1553.16}{\text{ft (established above)}}$$

Headloss for Free Discharge Condition

$$h_{5a} = [Q / (C * L)]^{2/3}$$

where,

$$\begin{aligned} C &= \frac{3.1}{L = \frac{3.00}{\text{ft}}} \end{aligned}$$

$$h_{5a} = \frac{1.80}{\text{ft}}$$

$$\begin{aligned} \text{EGL}_{5a} &= \text{EL}_{\text{Weir}} + h_{5a} \\ &= \frac{1554.96}{\text{ft}} \end{aligned}$$

Headloss for Submerged Condition

$$d_{\text{Sub}} = \frac{0.31}{\text{ft (depth of submergence)}}$$

$$h_{5b} = \frac{2.18}{\text{ft (separate submerged weir calc.)}}$$

$$\begin{aligned} \text{EGL}_{5b} &= \text{EGL}_4 + h_{5b} \\ &= \frac{1556.38}{\text{ft}} \end{aligned}$$

Identify EGL U/S of Weir

$$\begin{aligned} \text{The discharge condition is } & \frac{\text{Submerged}}{\text{EGL}_5 = \frac{1556.38}{\text{ft}}}, \text{ therefore} \end{aligned}$$

Expansion Loss from U/S Pipe, h_6

6/2/2023

$$h_6 = k * [V^2 / (2 * g)]$$

where,

$$k = \underline{0.30}$$

$$V = Q / A_F$$

$$= \underline{7.13} \text{ fps}$$

$$h_6 = \underline{0.24} \text{ ft}$$

$$EGL_6 = EGL_5 + h_6$$

$$= \underline{1556.61} \text{ ft}$$

Head Loss Through Upstream Pipe, h_7 Friction Losses, h_7

$$h_7 = S_{EGL} * L$$

where,

$$L = \underline{20} \text{ ft}$$

$$S_{EGL} = [(Q * n) / (1.49 * A_F * R^{2/3})]^2$$

where,

Pipe Characteristics

$$\text{Dia.} = \underline{24} \text{ in}$$

$$S_{PIPE} = \underline{0.0100} \text{ ft/ft}$$

$$n = \underline{0.013}$$

Flow Characteristics

$$d_n = \underline{2.00} \text{ ft}$$

$$A_F = \underline{3.14} \text{ sf}$$

$$P_W = \underline{6.28} \text{ ft}$$

$$R = \underline{0.50} \text{ ft}$$

$$S_{EGL} = \underline{0.0098} \text{ ft / ft}$$

$$h_7 = \underline{0.20} \text{ ft}$$

$$EGL_7' = EGL_6 + h_7$$

$$= \underline{1556.81} \text{ ft}$$

Check Entrance Condition for Critical Depth Control

$$EL_{U/S \text{ Inv.}} = \underline{1551.94} \text{ ft}$$

$$d_c = \underline{1.67} \text{ ft}$$

$$EGL_C = EL_{CDS \text{ Inv.}} + d_c + V_{dc}^2 / (2 * g)$$

$$= \underline{1554.60} \text{ ft}$$

Identify Controlling EGL

Friction based EGL controls.

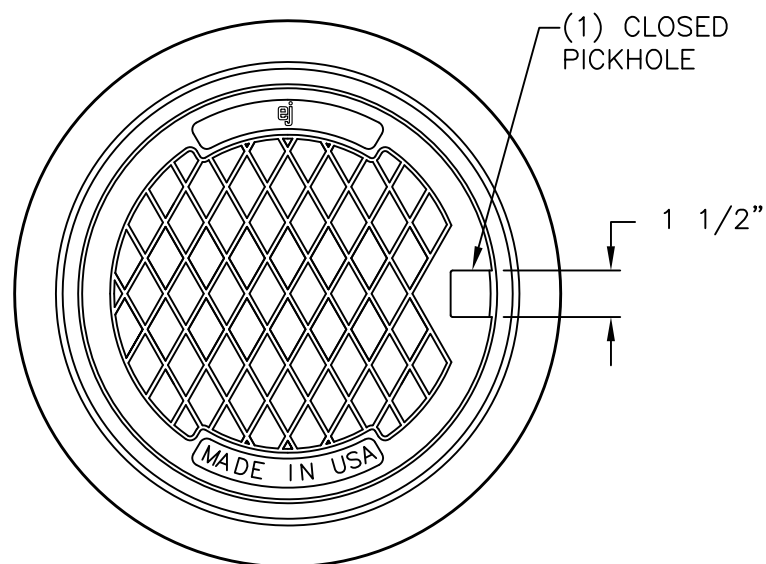
$$EGL_7 = \underline{1556.81} \text{ ft}$$

$$HGL_7 = EGL_7 - [V^2 / (2 * g)]$$

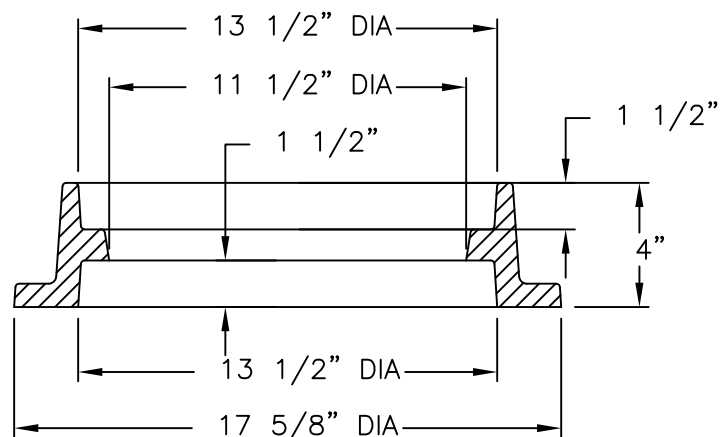
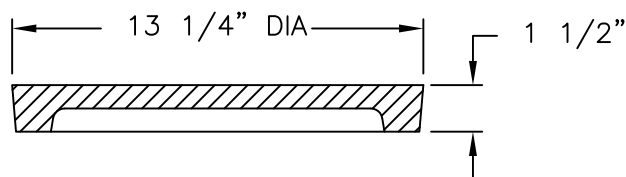
$$= \underline{1556.02} \text{ ft}$$

$$\text{Freeboard} = \underline{1.57} \text{ ft (at first upstream structure)}$$

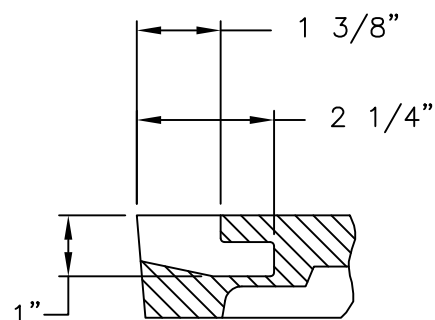
V1610-2BF RG V1610-2CV Assembly



BOTTOM FLANGE VIEW



SECTION VIEW



PICKHOLE DETAIL

NOTE:
RING IS REVERSIBLE AND CAN BE
INSTALLED AS A TOP FLANGE UNIT

Product Number

41610201

Design Features

- Materials
 - Cleanout/Monument Box Frame
 - Gray Iron (CL35B)
 - Cleanout/Monument Box Cover
 - Gray Iron (CL35B)

- Design Load
 - Heavy Duty
- Open Area
 - n/a
- Coating
 - Undipped
- ✓ Designates Machined Surface

Certification

- ASTM A48
-
-
- Country of Origin: USA

Major Components

41610210
41610220

Drawing Revision

06/12/2003 Designer: DAL
09/09/2015 Revised By: DVD

Disclaimer

Weights (lbs./kg) dimensions (inches/mm) and drawings provided for your guidance. We reserve the right to modify specifications without prior notice.

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Contact

800 626 4653
ejco.com

V1600-3 V1610-3 Assembly



Product Number

41600389

Design Features

-Materials

Frame

Gray Iron (CL35B)

Cover

Gray Iron (CL35B)

-Design Load

Heavy Duty

- Open Area

n/a

-Coating

Undipped

-√ Designates Machined Surface

Certification

-ASTM A48

-Country of Origin:USA

Major Components

41600310

41600374

Drawing Revision

05/02/2008 Designer: DEW

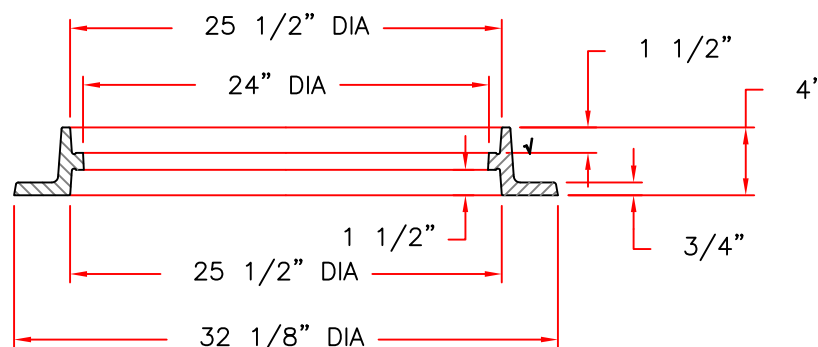
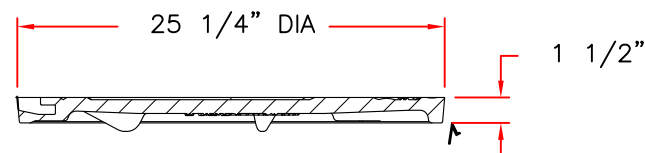
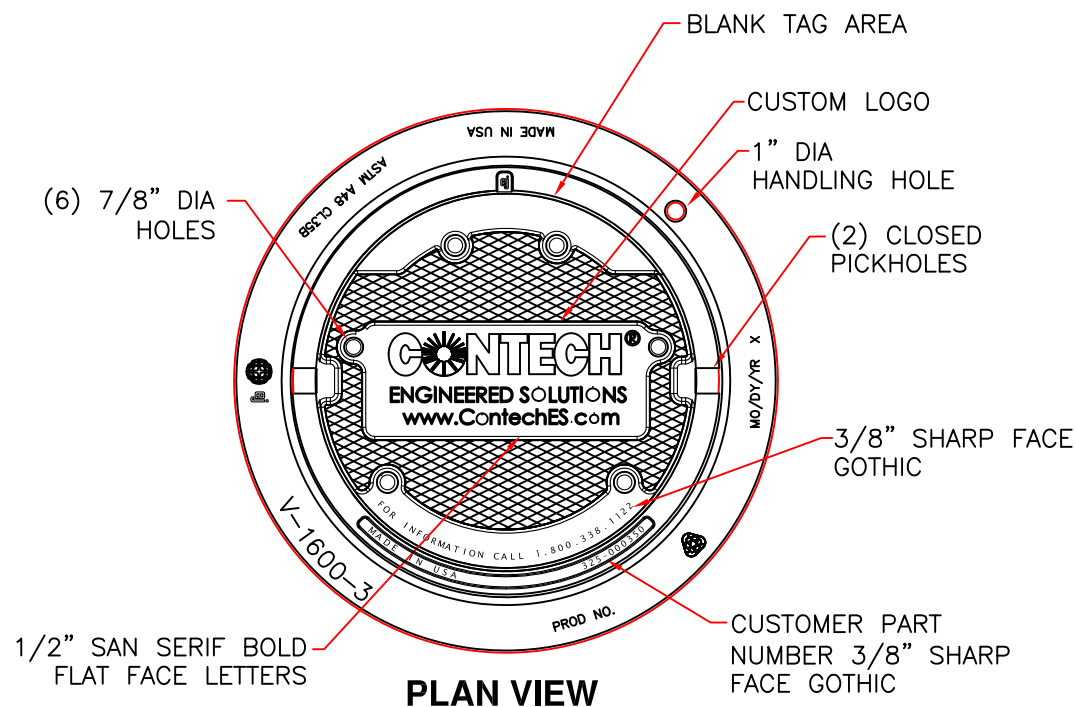
6/20/2017 Revised By: DAE

Disclaimer

Weights (lbs./kg) dimensions (inches/mm)
and drawings provided for your guidance. We
reserve the right to modify specifications without
prior notice.

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Contact
800 626 4653
ejco.com



**APPENDIX G – FAIRMONT SCOTTSDALE PRINCESS – PARKING GARAGE CONSTRUCTION
DOCUMENTS**

1. MARICOPA ASSOCIATION OF GOVERNMENTS (M.A.G.) UNIFORM STANDARD SPECIFICATIONS AND DETAILS FOR PUBLIC WORKS CONSTRUCTION (LATEST EDITION INCLUDING LATEST REVISION AND CURRENT SUPPLEMENTS THEREOF PER THE LOCAL TOWN OR CITY) ARE INCORPORATED INTO THIS PLAN IN THEIR ENTIRETY.
2. ALL WORK REQUIRED TO COMPLETE THE CONSTRUCTION COVERED BY THIS PLAN SHALL BE IN ACCORDANCE WITH THE M.A.G. STANDARD SPECIFICATIONS AND DETAILS AND CURRENT SUPPLEMENTS THEREOF PER THE LOCAL CITY OR TOWN, UNLESS SPECIFIED OTHERWISE IN THESE PLANS OR ELSEWHERE IN THE CONTRACT DOCUMENTS. CONTRACTORS SHALL FAMILIARIZE THEMSELVES WITH ALL REQUIRED STANDARD SPECIFICATIONS, DETAILS AND SUPPLEMENTS PRIOR TO BIDDING THE WORK FOR THE CONSTRUCTION COVERED BY THIS PLAN.
3. THE CONTRACTOR IS RESPONSIBLE FOR ALL METHODS, SEQUENCING, AND SAFETY CONCERNS ASSOCIATED WITH THIS PROJECT DURING CONSTRUCTION, UNLESS SPECIFICALLY ADDRESSED OTHERWISE IN THIS PLAN OR ELSEWHERE IN THE CONTRACT.
4. THE CONTRACTOR IS TO COMPLY WITH ALL LOCAL, STATE, AND FEDERAL LAWS AND REGULATIONS APPLICABLE TO THE CONSTRUCTION COVERED BY THIS PLAN.
5. THE CONTRACTOR IS RESPONSIBLE FOR OBTAINING AND COMPLYING WITH ALL PERMITS REQUIRED TO COMPLETE ALL WORK COVERED BY THIS PLAN.
6. THE QUANTITIES AND SITE CONDITIONS DEPICTED IN THESE PLANS ARE FOR GENERAL INFORMATIONAL PURPOSES ONLY AND MIGHT NOT REFLECT ACTUAL QUANTITIES AND SITE CONDITIONS. CONTRACTORS SHALL SATISFY THEMSELVES AS TO ACTUAL QUANTITIES AND SITE CONDITIONS PRIOR TO BIDDING THE WORK FOR THE CONSTRUCTION COVERED BY THIS PLAN.
7. A REASONABLE EFFORT HAS BEEN MADE TO SHOW THE LOCATIONS OF EXISTING UNDERGROUND FACILITIES AND UTILITIES IN THE CONSTRUCTION AREA. THE CONTRACTOR IS RESPONSIBLE FOR ANY DAMAGE TO UTILITIES AND/OR FACILITIES CAUSED DURING THEIR CONSTRUCTION OPERATIONS. THE CONTRACTOR SHALL CALL 48 HOURS IN ADVANCE FOR BLUE STAKE (1-800-STAKE-HI) PRIOR TO ANY EXCAVATION.
8. THE CONTRACTOR IS RESPONSIBLE FOR ALL COORDINATION OF CONSTRUCTION OF THE PROJECT WITH ALL EXISTING UTILITIES AND THE COORDINATION OF ANY NECESSARY UTILITY RELOCATION WORK.
9. ALL PAVING, GRADING, EXCAVATION, TRENCHING, PIPE BEDDING, CUT FILL AND BACKFILL SHALL COMPLY WITH THE RECOMMENDATIONS SET FORTH IN THE SOILS (GEOTECHNICAL) REPORT FOR THIS PROJECT IN ADDITION TO THE REFERENCED REQUIRED SPECIFICATIONS AND DETAILS. THE CONTRACTOR SHALL BE AWARE THAT CERTAIN UTILITIES REQUIRE PROPER ATTENTION AND CAREFUL PLANNING DURING CONSTRUCTION. THE CONTRACTOR SHALL BE RESPONSIBLE FOR PROTECTING AND NOT EXHIBIT THE FULL PROTECTIVE COVER REQUIRED DURING THE SUBGRADE PREPARATION PHASE OF THE CONSTRUCTION, IN SUCH INSTANCES, THE CONTRACTOR SHALL PROVIDE ADDITIONAL PROTECTION (SUCH AS RAMPING) OR INCREASED PIPE STRENGTH TO PROVIDE THE NECESSARY PROTECTION REQUIRED TO PREVENT DAMAGE DURING THE CONSTRUCTION OF THIS PROJECT. THE CONTRACTOR SHALL HOLD THE ENGINEER HARMLESS IN ALL CASES FOR DAMAGES TO UTILITIES WHERE INADEQUATE PROTECTIVE MEASURES OCCUR.
10. THE CONTRACTOR IS TO VERIFY THE LOCATION AND THE ELEVATIONS OF ALL EXISTING UTILITIES AT POINTS OF TIE-IN PRIOR TO COMMENCING ANY NEW CONSTRUCTION. SHOULD ANY LOCATION OR ELEVATION DIFFER FROM THAT SHOWN ON THESE PLANS, THE CONTRACTOR SHALL CONTACT THE OWNER'S AGENT.
11. CONTRACTOR TO VERIFY AND COORDINATE ALL DIMENSIONS AND SITE LAYOUT WITH ARCHITECT'S FINAL SITE PLAN AND FINAL BUILDING DIMENSIONS BEFORE STARTING WORK. REPORT DISCREPANCIES TO OWNERS AGENT.
12. COORDINATION BETWEEN ALL PARTIES IS ESSENTIAL PART OF CONTRACT.
13. THE CONTRACTOR IS RESPONSIBLE FOR DETERMINING ALL SITE CONDITIONS, AND TO WORK WITH WEATHER CONDITIONS AS THE PROJECT SITE MAY BE LOCATED IN A FLOOD PRONE AREA AND SUBJECT TO FLOODING AND ITS HAZARDS.
14. THE CONTRACTOR IS TO VERIFY THE LOCATION, ELEVATION, CONDITION, AND PAVEMENT CROSS-SLOPE OF ALL EXISTING SURFACES AT POINTS OF TIE-IN AND MATCHING, PRIOR TO COMMENCEMENT OF GRADING, PAVING, CURB AND GUTTER OR OTHER SURFACE CONSTRUCTION. SHOULD EXISTING LOCATIONS, ELEVATIONS, CONDITION, OR PAVEMENT CROSS-SLOPE DIFFER FROM THAT SHOWN ON THESE PLANS, THE CONTRACTOR SHALL CONTACT THE OWNER'S AGENT. SPECIAL WORK IS TO BE CONSTRUCTED. THE CONTRACTOR SHALL NOTIFY THE OWNER'S AGENT IMMEDIATELY FOR DIRECTION ON HOW TO PROCEED PRIOR TO COMMENCEMENT OF CONSTRUCTION. THE CONTRACTOR ACCEPTS RESPONSIBILITY FOR ALL COSTS ASSOCIATED WITH CORRECTIVE ACTION IF THESE PROCEDURES ARE NOT FOLLOWED.
15. CONTRACTOR IS RESPONSIBLE TO COORDINATE UTILITY CROSSINGS AT CULVERT CROSSINGS BEFORE STARTING WORK ON CULVERT. COORDINATE WITH OWNER REPRESENTATIVE. VERIFY UTILITY LINES AND/OR CONDUITS ARE IN PLACE BEFORE STARTING CULVERT WORK.
16. CONTRACTOR RETENTION BASIN AS SHOWN, CONTRACTOR TO SCARIFY BOTTOM OF BASIN TWO FEET DEEP AND NOT ALLOW COMPACTION OVER 80%.
17. THIS PROJECT REQUIRES A REGULAR ONGOING MAINTENANCE PROGRAM FOR THE DESIGNED DRAINAGE SYSTEM(S) TO PRESERVE THE DESIGN INTEGRITY AND THE ABILITY TO PERFORM ITS OPERATIONAL INTENT. FAILURE TO PROVIDE MAINTENANCE WILL JEOPARDIZE THE DRAINAGE SYSTEM(S) PERFORMANCE AND MAY LEAD TO ITS INABILITY TO PERFORM PROPERLY AND/OR CAUSE DAMAGE TO THE SEWER/IN THE PROJECT.
18. SEWER LINES DESIGNED IN PROFILE AND PUBLIC WATER LINES ARE REQUIRED TO BE ASBUILT AND THE INSTALLATION AND TESTING WITNESSED BY A PROFESSIONAL ENGINEER IN ACCORDANCE WITH ARIZONA ADMINISTRATIVE CODES R18-9-0307, "4.01 GENERAL PERMIT: SEWAGE COLLECTIONS SYSTEMS" AND R18-507 AND 508, "APPROVAL OF CONSTRUCTION" AND "RECORD DRAWINGS", RESPECTIVELY. IT IS THE CONTRACTOR'S RESPONSIBILITY TO NOTIFY OWNER 72 HOURS IN ADVANCE WHEN THOSE SYSTEMS ARE READY TO BE WITNESSED.
19. THE CONTRACTOR SHALL BE RESPONSIBLE FOR BEING COMPLIANT WITH THE INTENT OF THE CURRENT AMERICANS DISABILITIES ACT (ADA) REQUIREMENTS AS INTERPRETED BY THE REVIEWING AGENCY(IES), IF CONSTRUCTION OF THE PROJECT IS DELAYED, THIS WORK PRODUCT SHOULD BE UPDATED TO ACCOUNT FOR ANY RELEVANT ADA UPDATES BEFORE CONSTRUCTION BEGINS.
20. LOWEST FLOOR (LF) REFERS TO EITHER FLOOR/SLAB ELEVATION OR TOP OF BASEMENT SLAB. LF ELEVATIONS ON THE GRADING AND DRAINAGE PLANS FOR RESIDENTIAL UNITS REFLECT SLAB ON GRADE CONDITIONS AND CANNOT BE LOWERED WITHOUT THE APPROVAL OF THE DESIGNER. SPECIAL WORK NOT ABLE TO ADEQUATE RESIDENTIAL LOT DRAINAGE CAN BE ACHIEVED, A PROFESSIONAL ENGINEER SHOULD BE CONSULTED IF THE LF FOR THE SLAB IS PROPOSED TO BE LOWERED, OR IF A BASEMENT IS TO BE CONSTRUCTED.

A PORTION OF SECTION 35, TOWNSHIP 4 NORTH, RANGE 4 EAST
OF THE GILA AND SALT RIVER MERIDIAN, MARICOPA COUNTY, ARIZONA

RAW CUT:	15,888 CY
RAW FILL:	2,804 CY

QUANTITIES ARE ESTIMATED IN PLACE. NO PRECOMPACTION, SHRINK OR SWELL IS ASSUMED.

PLEASE REFER TO SHEET C-102 FOR CITY OF SCOTTSDALE NOTES.

PLEASE REFER TO SHEET C-102 FOR ESTIMATED QUANTITIES FOR WORK IN PUBLIC RIGHTS-OF-WAY AND EASEMENTS.

PLEASE REFER TO SHEET C-102 FOR LEGEND AND LIST OF ABBREVIATIONS.

1. THESE PLANS HAVE BEEN SUBMITTED TO THE FOLLOWING UTILITY COMPANIES FOR APPROVAL WITHIN THEIR AREA OF INTEREST. THE SIZE AND LOCATIONS, AS SHOWN OF THE GAS, TELEPHONE AND POWER LINES, AND CONNECTIONS AGREED TO BY THE UTILITIES, AND INFORMATION CONTAINED IN THE UTILITY COMPANIES RECORDS, WHERE THE WORK IS TO BE DONE, CONFLICTS WITH ANY OF THESE UTILITIES. THE CONFLICTS SHALL BE RESOLVED AS SPECIFIED IN THE SPECIAL PROVISIONS AND/OR AS OTHERWISE NOTED ON THESE PLANS. CONFLICTS ARISING DURING THE COURSE OF CONSTRUCTION FROM UNFORESEEN CIRCUMSTANCES SHALL BE REPORTED TO THE INTERESTED UTILITY COMPANY AND SHALL BE RESOLVED BY THE CITY AND THE UTILITY COMPANY.
2. THE CITY WILL NOT PARTICIPATE IN THE COST OF CONSTRUCTION OR UTILITY RELOCATION.

ACCORDING TO FEMA FLOOD INSURANCE RATE MAPPING, THE SUBJECT PROPERTY IS LOCATED IN "SPECIAL FLOOD HAZARD AREAS SUBJECT TO INUNDATION BY THE 1% ANNUAL CHANCE FLOOD "ZONE AO". ZONE AO IS DESCRIBED AS: "FLOOD DEPTHS OF 1 TO 3 FEET (USUALLY SHEET FLOW ON SLOPING TERRAIN); AVERAGE DEPTHS DETERMINED. FOR AREAS OF ALLUVIAL FAN FLOODING, VELOCITIES ALSO DETERMINED."

MAP NUMBER	COMMUNITY NUMBER	PANEL NUMBER	SUFFIX	DATE OF FIRM	INDEX DATE	FIRM ZONE	BASE FLOOD ELEVATION (IN AO ZONE, USE DEPTH)
04013C	045012	1320	L	10/16/2013	07/20/2021	AO	1

ENGINEER'S CERTIFICATION: THE LOWEST FLOOR ELEVATION(S) AND/OR FLOOD PROOFING ELEVATION(S) ON THIS PLAN ARE SUFFICIENTLY HIGH TO PROVIDE PROTECTION FROM FLOODING CAUSED BY A ONE-HUNDRED YEAR STORM, AND ARE IN ACCORDANCE WITH CITY OF SCOTTSDALE REVISED CODE, CHAPTER 37-FLOODPLAIN AND STORMWATER REGULATIONS.

I HEREBY CERTIFY THAT THE "RECORD DRAWING" MEASUREMENTS AS SHOWN
HEREON WERE MADE UNDER MY SUPERVISION OR AS NOTED AND ARE CORRECT TO
THE BEST OF MY KNOWLEDGE AND BELIEF.

REGISTERED ENGINEER/ LAND SURVEYOR _____ DATE _____

SEAL

LOT 2 OF FAIRMONT SCOTTSDALE PRINCESS, AS SHOWN ON MINOR SUBDIVISION PLAT
RECORDED IN BOOK 1104, PAGE 3, MARICOPA COUNTY RECORDS (MCR), LYING WITHIN
SECTION 35, TOWNSHIP 4 NORTH, RANGE 4 EAST, OF THE GILA AND SALT RIVER MERIDIAN
MARICOPA COUNTY, ARIZONA.

A SOILS GEOTECHNICAL REPORT HAS BEEN PREPARED FOR THIS PROJECT TITLED
GEOTECHNICAL ENGINEERING REPORT - FAIRMONT SCOTTSDALE PRINCESS - PARKING
STRUCTURE ADDITION BY ALPHA GEOTECHNICAL & MATERIALS, INC. DATED APRIL 24,
2023. REPORT NO. 22-G-13162.

"THE ENGINEER OF RECORD ON THESE PLANS HAS RECEIVED A COPY OF THE APPROVED STIPULATIONS FOR THIS PROJECT AND HAS DESIGNED THESE PLANS IN CONFORMANCE WITH THE APPROVED STIPULATIONS."


 ENGINEER SIGNATURE

06/02/2023
 DATE

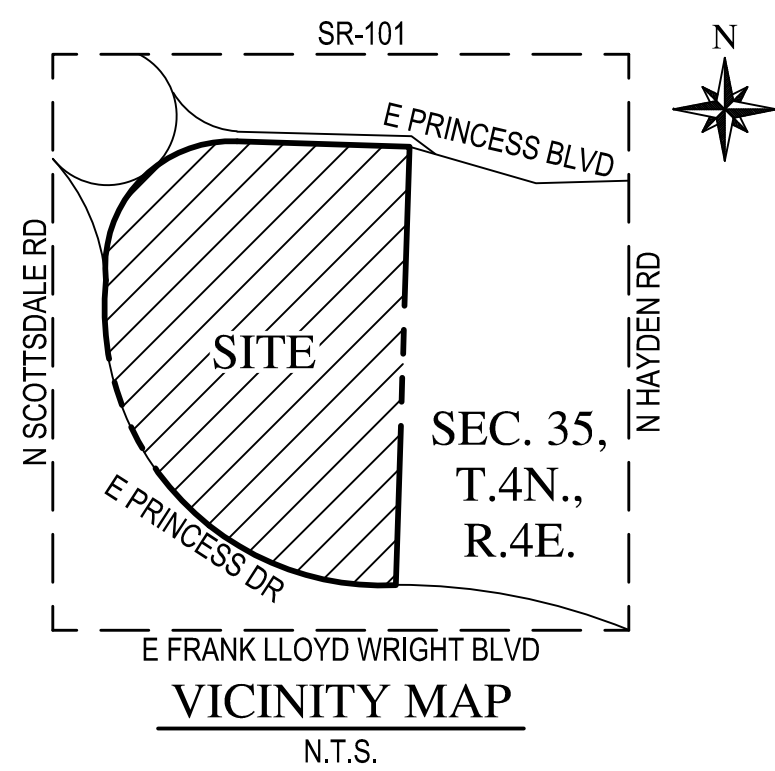
HAG = 1561.48
LAG = 1554.74
FF=1566.50
RFD=1563.48
ALL ELECTROMECHANICAL EQUIPMENT
SHALL BE ELEVATED TO RFD ELEVATION

C-101	COVER SHEET
C-102	NOTES AND QUANTITIES
C-103	INDEX MAP
C-104-C-105	DEMOLITION PLAN
C-106-C-107	GRADING AND DRAINAGE PLAN
C-108	WATER PLAN
C-109-C-110	SIGNING AND STRIPING PLAN
C-111-C-113	DETAILS AND SECTIONS

CITY OF SCOTTSDALE BRASS CAP FLUSH 450'± NORTH OF PRINCESS DRIVE ON SCOTTSDALE ROAD, BEING THE WEST QUARTER CORNER OF SECTION 35, TOWNSHIP 4 NORTH, RANGE 4 EAST.
CITY OF SCOTTSDALE DATUM, NAVD88 DATUM
ELEVATION=1553.22'.

I HEREBY CERTIFY THAT ALL ELEVATIONS REPRESENTED ON THIS PLAN ARE BASED ON NAVD 1988, MCDOT, AND MEET THE FEMA BENCHMARK MAINTENANCE (BMM) CRITERIA.

WATER	CITY OF SCOTTSDALE
SEWER	CITY OF SCOTTSDALE
ELECTRIC	APS
TELEPHONE	LUMEN
NATURAL GAS	SOUTHWEST GAS
CABLE TV	COX COMMUNICATIONS



STRATEGIC HOTELS & RESORTS
150 NORTH RIVERSIDE PLAZA, SUITE 4270
CHICAGO, IL 60606
CONTACT: TIMOTHY TAYLOR
PHONE: (312) 658-6038

WOOD, PATEL & ASSOCIATES, INC.
2051 WEST NORTHERN AVENUE, SUITE 100
PHOENIX, ARIZONA 85021
CONTACT: DARIN MOORE, P.E.
PHONE: (602) 335-8500
FAX: (602) 335-8580

KOLLIN ALTOMARE ARCHITECTS
4265 E. CONANT STREET, SUITE 101
LONG BEACH, CA 90808
CONTACT: PAUL ALTOMARE
PHONE: (562) 597-8760

ASSESSOR PARCEL NUMBER(S)
215-08-694
PROJECT SITE ADDRESS:
7575 E PRINCESS BLVD
SCOTTSDALE, ARIZONA 85255
PROJECT SITE AREA(S):
NET AREA = 9.02 AC
DISTURBED AREA = 5± AC
ZONING:
C2



Wood, Patel & Associates, Inc.

Civil Engineering
Water Resources
Land Survey
Construction Management

602.335.8500

www.woodpatel.com



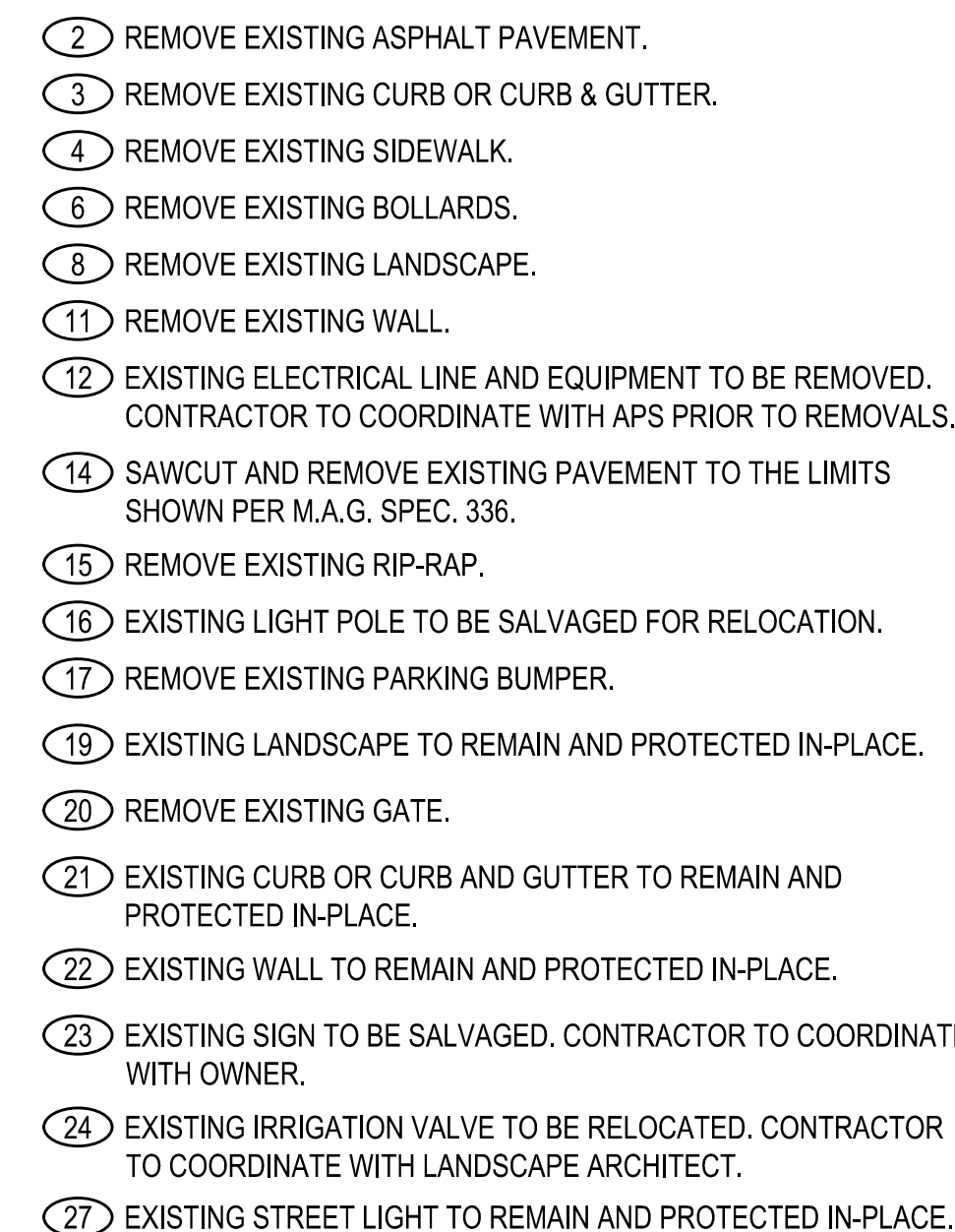
**FAIRMONT SCOTTSDALE PRINCESS
FAIRMONT PARKING GARAGE
IMPROVEMENT PLAN
SCOTTSDALE, ARIZONA
COVER SHEET**

[illegible]


CHECKED BY: DM DESIGNED BY: RS DRAFTED BY: DLH / JRS

C-102





**FAIRMONT SCOTTSDALE PRINCESS
FAIRMONT PARKING GARAGE
IMPROVEMENT PLAN**
SCOTTSDALE, ARIZONA
DEMOLITION PLAN

[illegible]

Registered Professional Engineer (C.E.)
CERTIFICATE NO.
36302
DARRYL L.
MOORE
06/30/2023
Date Signed
ARIZONA, U.S.A.

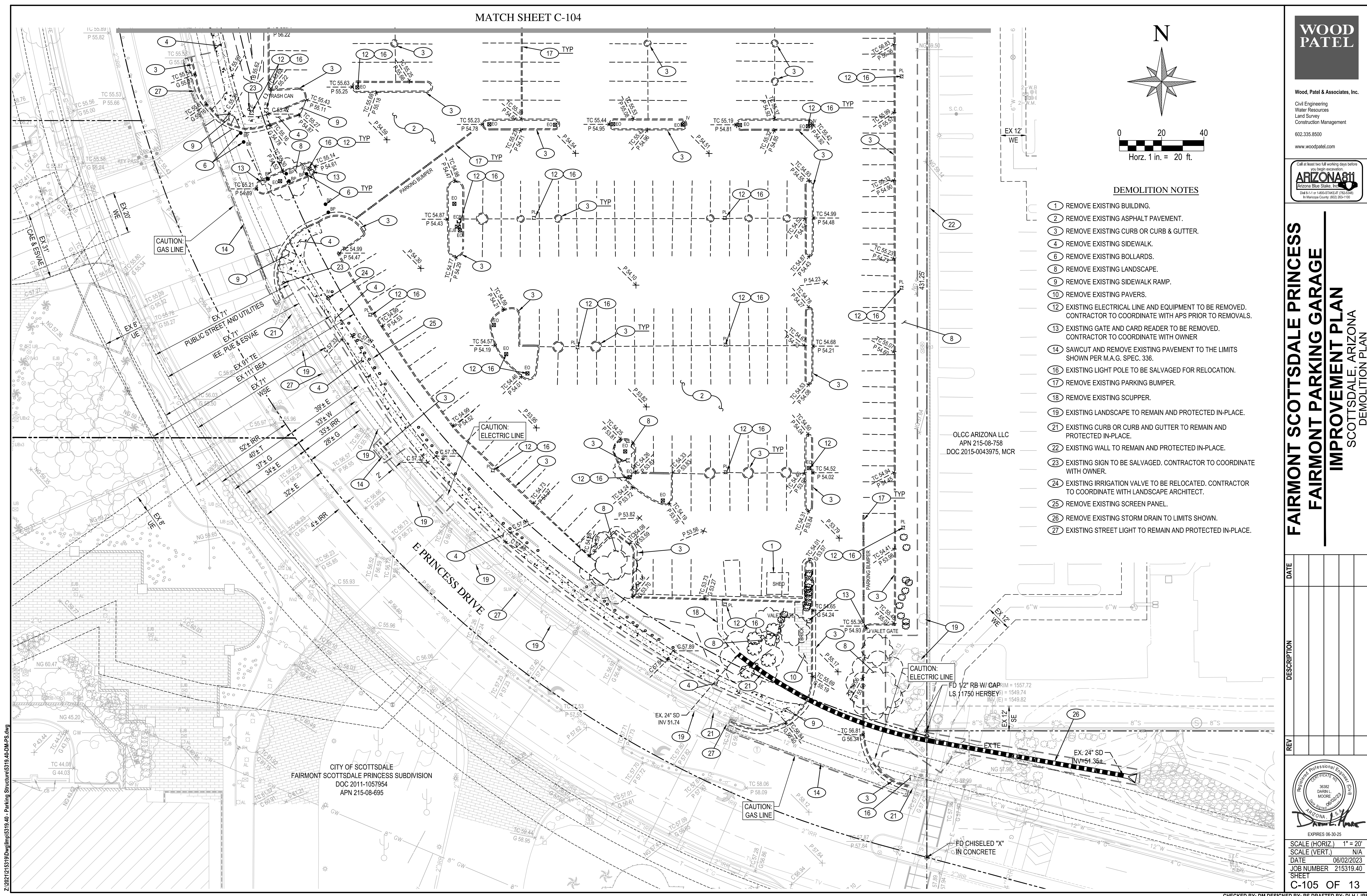
EXPIRES 06-30-25

SCALE (HORIZ.)	1" = 20'
SCALE (VERT.)	N/A
DATE	06/02/2023
JOB NUMBER	215319.40
SHEET	
C-104	OF 13

CHECKED BY: DM DESIGNED BY: RS DRAFTED BY: DLH / JRS

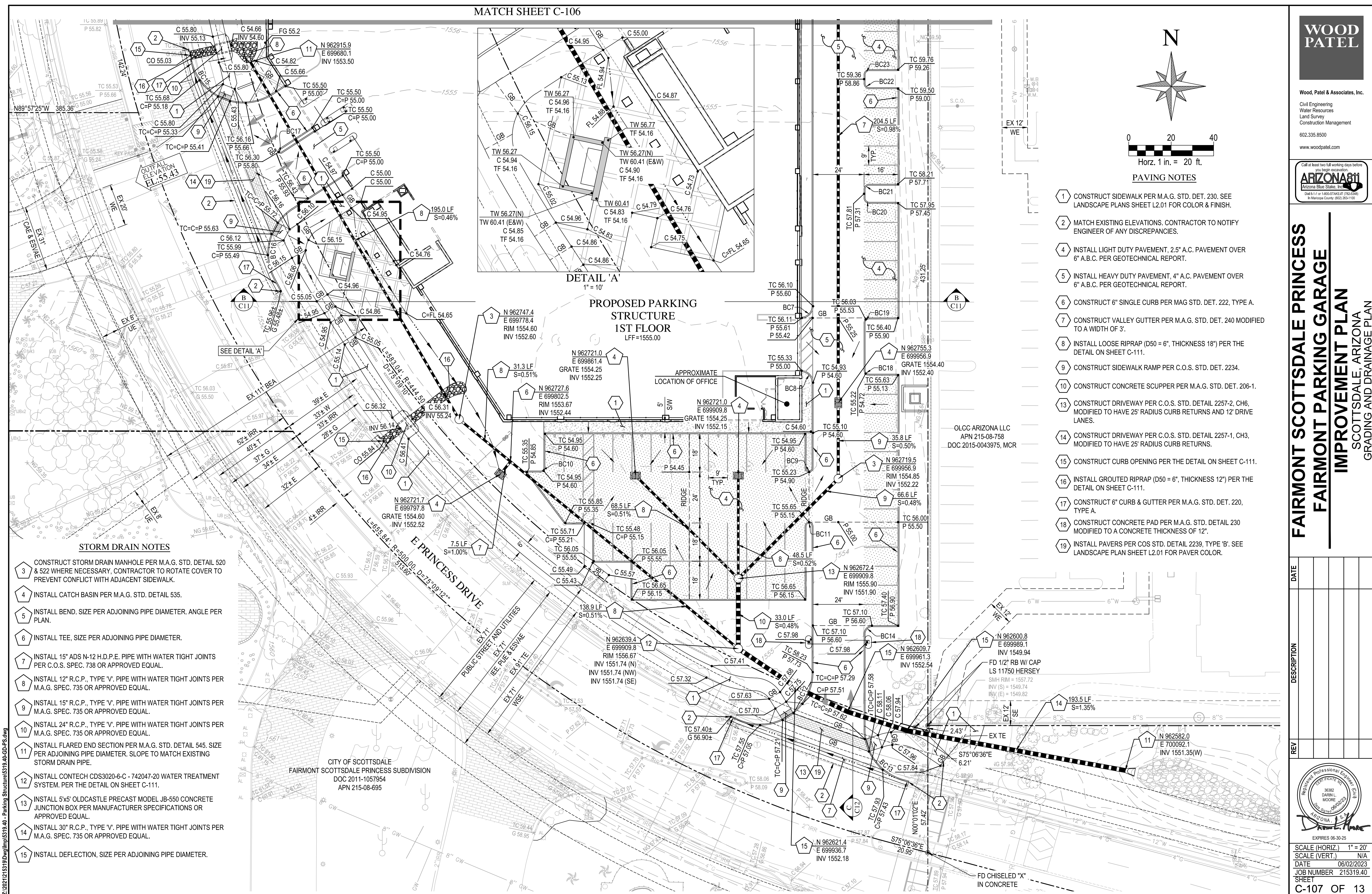


JOB NUMBER	2022-22
DATE	06/02/2023
SHEET NAME	DEMOLITION PLAN
SHEET NUMBER	





CHECKED BY: DM DESIGNED BY: RS DRAFTED BY: DLH / JRS





0 20 40

Horz. 1 in. = 20 ft.

SIGNAGE NOTES

1 INSTALL PAVEMENT SYMBOL PER ADOT STD. DETAIL M-10.

STRIPING LEGEND

4SW

4" SOLID WHITE LINE

Call at least two full working days before
you begin excavation.

ARIZONA811
Arizona Blue Stake, Inc.

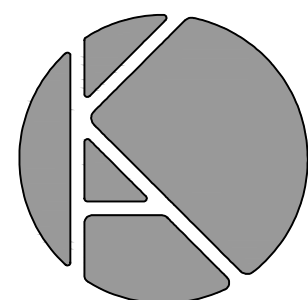
Dial 8-1-1 or 1-800-STAKE-IT (782-6348)
In Maricopa County: (602) 263-1100

**FAIRMONT SCOTTSDALE PRINCESS
FAIRMONT PARKING GARAGE
IMPROVEMENT PLAN**
SCOTTSDALE, ARIZONA
SIGNING AND STRIPING PLAN

[illegible]

SCALE (HORIZ.)	1" = 20'
SCALE (VERT.)	N/A
DATE	06/02/2023
JOB NUMBER	215319.40
SHEET	
C-109 OF 13	

CHECKED BY: DM DESIGNED BY: RS DRAFTED BY: DLH / JRS

[illegible]

ARCHITECT OF RECORD
Kollin Altomare Architects

Long Beach
4265 E. Conant Street, Suite 101
Long Beach, CA 90808
t: 562.597.8760

Chicago
900 N. Franklin Street, Suite 405-B
Chicago, IL 60610
t: 312.471.8760

PROJECT
FAIRMONT SCOTTSDALE PRINCESS
FAIRMONT PARKING GARAGE

575 EAST PRINCESS DRIVE, SCOTTSDALE, AZ 85255

JOB NUMBER
2022-22

DATE
06/02/2023

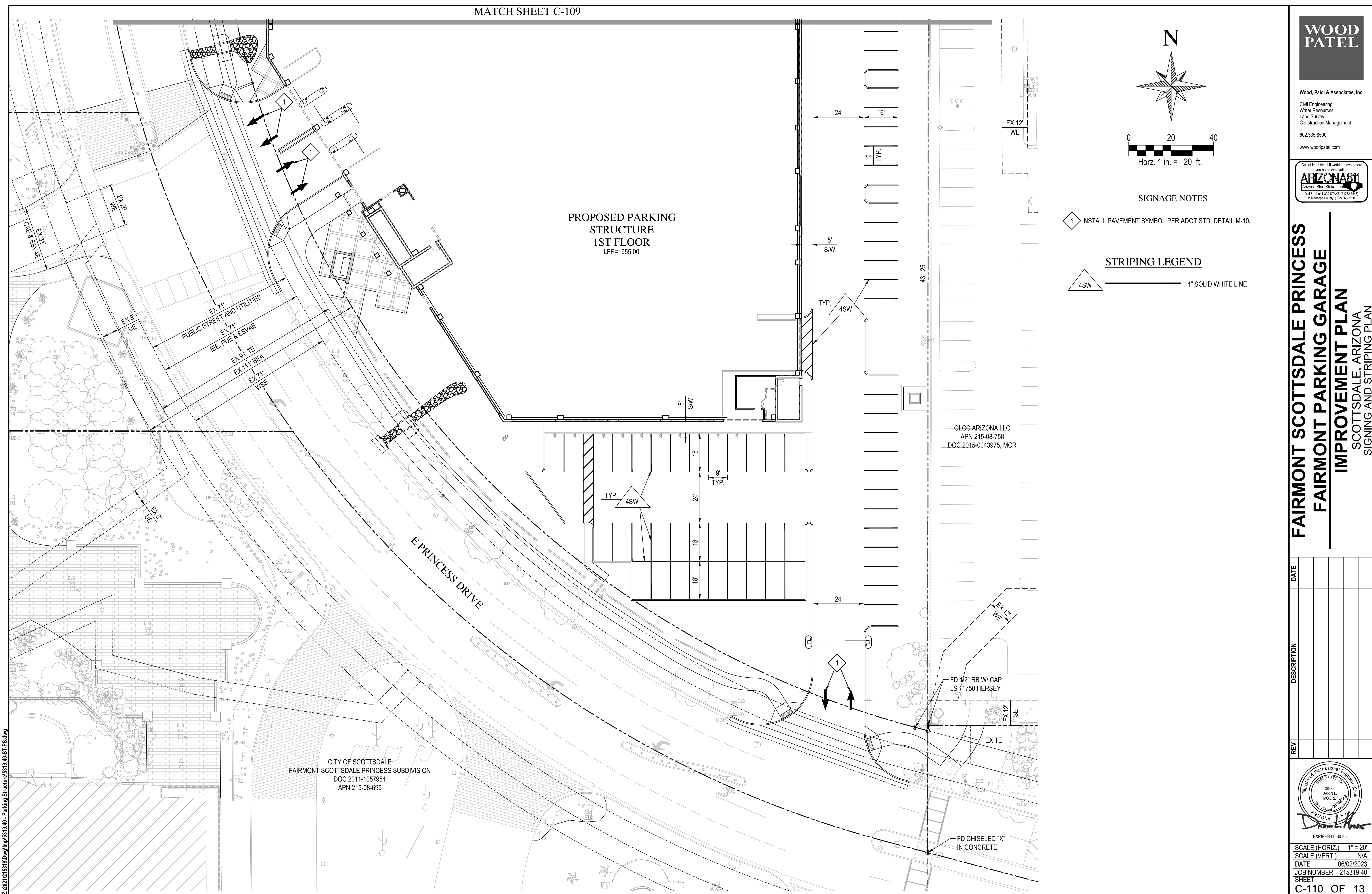
SHEET NAME

SIGNING AND
STRIPING PL

SHEET NUMBER

C-109

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SITE DESIGN DATA		MAX
WATER QUALITY FLOW RATE	0.52 CFS	2 CFS
PEAK FLOW RATE	22.39 CFS	25 CFS
RETURN PERIOD OF PEAK FLOW	10 YRS	

GENERAL NOTES:

- C. CONTRACTOR TO PROVIDE ALL MATERIALS UNLESS NOTED OTHERWISE.
- D. FOR FABRICATION DRAWINGS WITH DETAILLED STRUCTURE DIMENSIONS AND WEIGHT, PLEASE CONTACT YOUR CONTRACT ENGINEER (C/E) OR C/E REPRESENTATIVE.
- E. CDS WATER QUALITY STRUCTURE SHALL BE IN ACCORDANCE WITH ALL DESIGN DATA AND INFORMATION CONTAINED IN THIS SPECIFICATION.
- F. CDS WATER QUALITY STRUCTURE SHALL BE DESIGNED TO SUPPORT A MINIMUM OF 1000 PSF OF SURFACE LOAD. CASTING SHALL MEET ASHTO M3185H-20 LOAD RATING, ASSUMING EARTH COVER OF 0' 2" AND GROUNDWATER ELEVATION AT OR BELOW FINISHED GRADE. STRUCTURE SHALL BE DESIGNED TO SUPPORT 1000 PSF OF SURFACE LOAD, GROUNDWATER ELEVATION AT OR BELOW FINISHED GRADE, AND 1000 PSF OF SURFACE LOAD. CASTING SHALL MEET ASHTO M3185H-20 AND BE CAST WITH THE CONTECH LOG.
- G. STRUCTURE SHALL BE CAST IN PLACE AND SHALL BE PLACED ON SHELL AT BOTTOM OF SCREEN CYLINDER. REMOVE AND REPLACE AS NECESSARY DURING MAINTENANCE AND REPAIR.
- H. CDS STRUCTURE SHALL BE PRECAST CONCRETE CONCRETE TO ASTM C476 AND ASHTO LOAD FACTOR DESIGN METHOD.

INSTALLATION NOTES:

- A. STRUCTURE SHALL BE BACKFILL DETHL'D AND/OR ANTI-FLOTATION PROVISIONS ARE SITE-SPECIFIC; DESIGN CONSIDERATIONS AND SHALL BE SPECIFIED BY ENGINEER OF RECORD.
- B. STRUCTURE SHALL BE BACKFILLED WITH SUFFICIENT LIFTING AND REACH CAPACITY TO LIFT AND SET THE CDS MANHOLE STRUCTURE.
- C. CONTRACTOR TO INSTALL JOINT SEALANT BETWEEN ALL LIFTING SECTIONS AND ASSEMBLE STRUCTURE.
- D. CONTRACTOR TO PROVIDE, INSTALL, AND GROUT INLET AND OUTLET PIPES. MATCH PIPE INVERTS WITH ELEVATIONS SHOWN ON DRAWINGS.
- E. CONTRACTOR TO TAKE APPROPRIATE MEASURES TO ASSURE UNIT WATER TIGHT, HOLDING WATER TO FLOWLINE INVERT MINIMUM 18" ABOVE FINISHED GRADE.

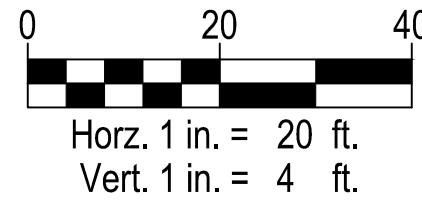
CONTECH
PROPOSAL
DRAWING



NOTES:

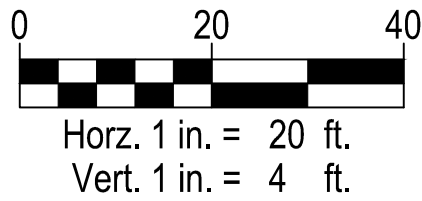
1. FOR LOOSE RIPRAP APPLICATIONS INSTALL "MIRAFI 140NL" FILTER FABRIC, OR APPROVED EQUAL, UNDER ALL LOOSE RIPRAP.
2. FOR GROUTED RIPRAP APPLICATIONS OMIT FILTER FABRIC.
3. DEPTH OF LOOSE RIPRAP SHALL BE $2d_{50}$ MINIMUM UNLESS OTHERWISE SPECIFIED. DEPTH OF GROUTED RIPRAP SHALL BE $2d_{50}$ MINIMUM UNLESS OTHERWISE SPECIFIED.
4. RIPRAP SHALL BE ANGULAR ROCK.
5. REFER TO LANDSCAPE PLAN FOR RIPRAP COLOR.

[illegible]

[illegible]

SCALE (HORIZ.)	1" = 20'
SCALE (VERT.)	1" = 4'
DATE	06/02/2023
JOB NUMBER	215319.40
SHEET	
C-112 OF 13	

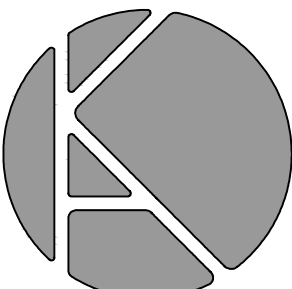
CHECKED BY: DM DESIGNED BY: RS DRAFTED BY: DLH / JRS



**FAIRMONT SCOTTSDALE PRINCESS
FAIRMONT PARKING GARAGE
IMPROVEMENT PLAN**
SCOTTSDALE, ARIZONA
DETAILS AND SECTIONS

REV	DESCRIPTION	DATE
	 SCALE (HORIZ.) 1" = 20' SCALE (VERT.) 1" = 4" DATE 06/02/2023 JOB NUMBER 215319.40 SHEET C-113 OF 13	

CHECKED BY: DM DESIGNED BY: RS DRAFTED BY: DLH / JRS

[illegible]

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Long Beach, CA 90808
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Chicago
900 N. Franklin Street, Suite 405-B
Chicago, IL 60610
t: 312.471.8760

PROJECT
FAIRMONT SCOTTSDALE PRINCESS
FAIRMONT PARKING GARAGE

7575 EAST PRINCESS DRIVE, SCOTTSDALE, AZ 85255
PREPARED FOR: STRATEGIC HOTELS & RESORTS

JOB NUMBER

DATE _____

SHEET NA

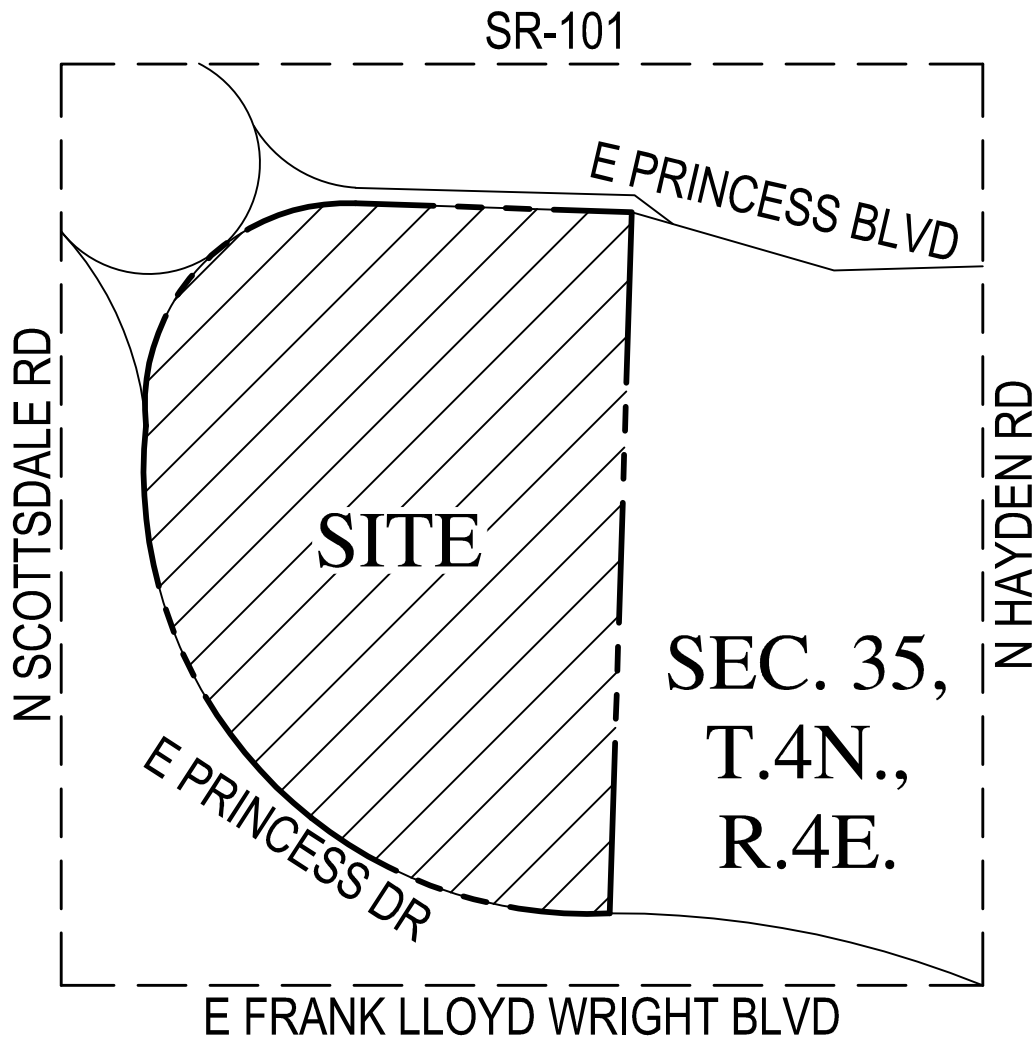
SECTIONS

SHEET NUMBER

C-113

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EXHIBIT 1 – VICINITY MAP



VICINITY MAP

N.T.S.

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FAIRMONT SCOTTSDALE PRINCESS

PARKING GARAGE VICINITY MAP EXHIBIT

DATE	06/02/2023	SCALE	N.T.S	SHEET	1 OF 1
JOB NO.	215319.40	DESIGN	AJS	CHECK	AJS
		DRAWN	NTS	RFI #	

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EXHIBIT 2 – FEMA FIRM

National Flood Hazard Layer FIRMette



111°55'26"W 33°39'5"N



0 250 500 1,000 1,500 2,000 Feet 1:6,000 111°54'48"W 33°38'35"N
Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT

SPECIAL FLOOD HAZARD AREAS		Without Base Flood Elevation (BFE) Zone A, V, A99
		With BFE or Depth Zone AE, AO, AH, VE, AR
OTHER AREAS OF FLOOD HAZARD		0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile Zone X
		Future Conditions 1% Annual Chance Flood Hazard Zone X
OTHER AREAS		Area with Reduced Flood Risk due to Levee. See Notes. Zone X
		Area with Flood Risk due to Levee Zone D
GENERAL STRUCTURES		NO SCREEN Area of Minimal Flood Hazard Zone X
		Effective LOMRs
OTHER FEATURES		Area of Undetermined Flood Hazard Zone D
		Channel, Culvert, or Storm Sewer
MAP PANELS		Levee, Dike, or Floodwall
		Cross Sections with 1% Annual Chance Water Surface Elevation
MAP PANELS		Coastal Transect
		Base Flood Elevation Line (BFE)
MAP PANELS		Limit of Study
		Jurisdiction Boundary
MAP PANELS		Coastal Transect Baseline
		Profile Baseline
MAP PANELS		Hydrographic Feature
		Digital Data Available
MAP PANELS		No Digital Data Available
		Unmapped



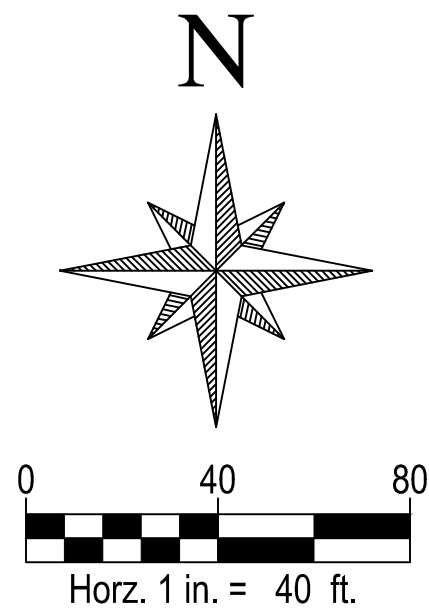
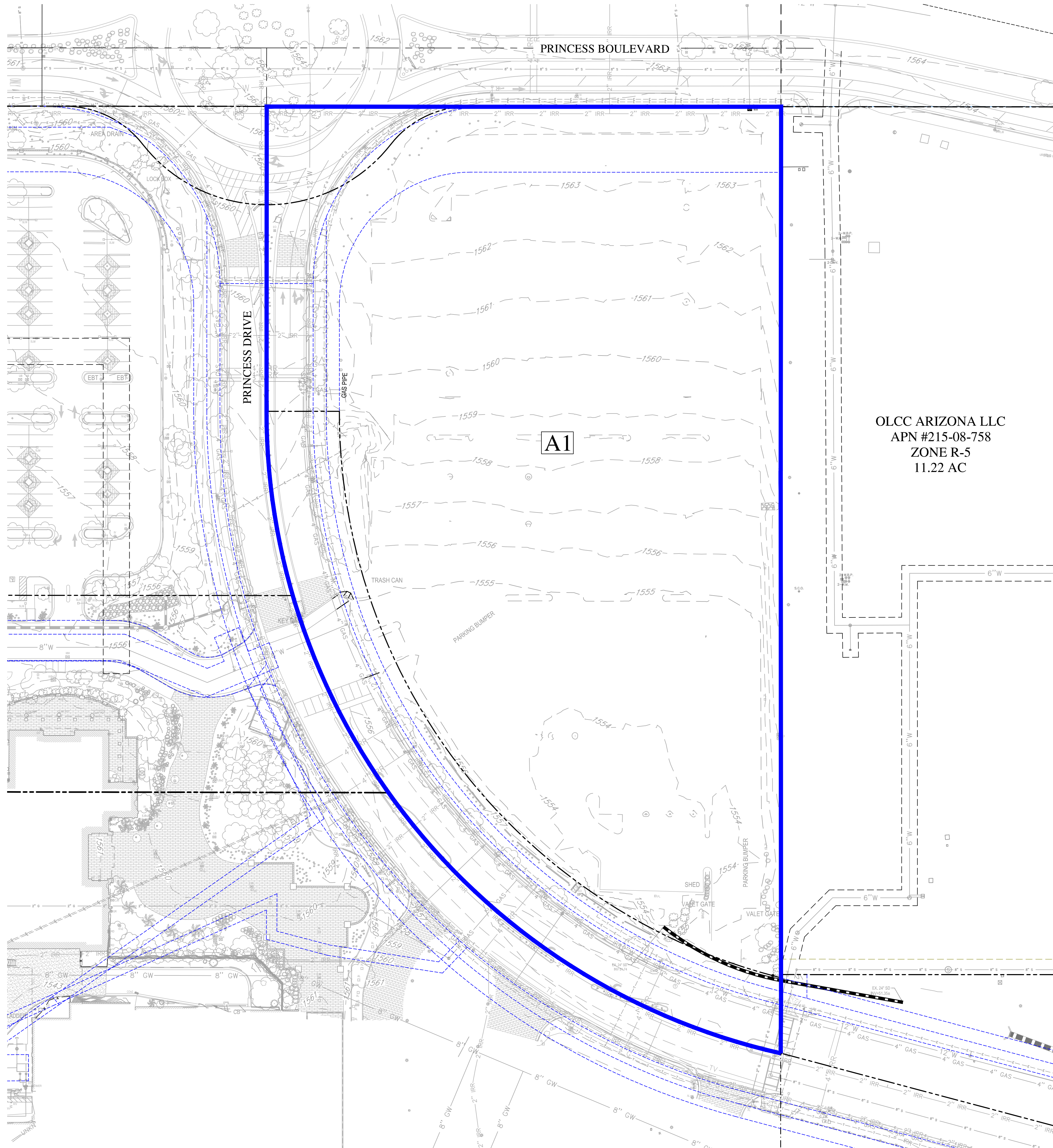
The pin displayed on the map is an approximate point selected by the user and does not represent an authoritative property location.

This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap accuracy standards



The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 3/2/2023 at 10:49 AM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

EXHIBIT 3 – EXISTING DRAINAGE AREA MAP



LEGEND

-  DRAINAGE AREA BOUNDARY
-  DRAINAGE AREA LABEL

OLCC ARIZONA LLC
APN #215-08-758
ZONE R-5
11.22 AC

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FAIRMONT SCOTTSDALE PRINCESS

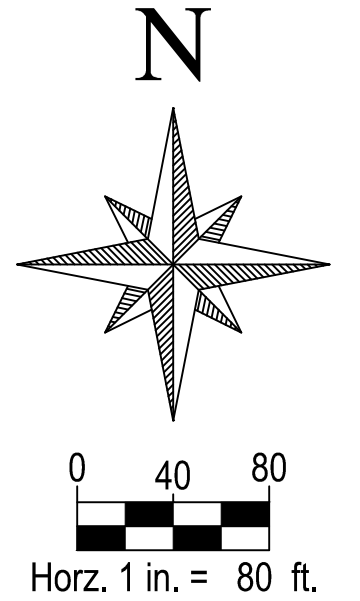
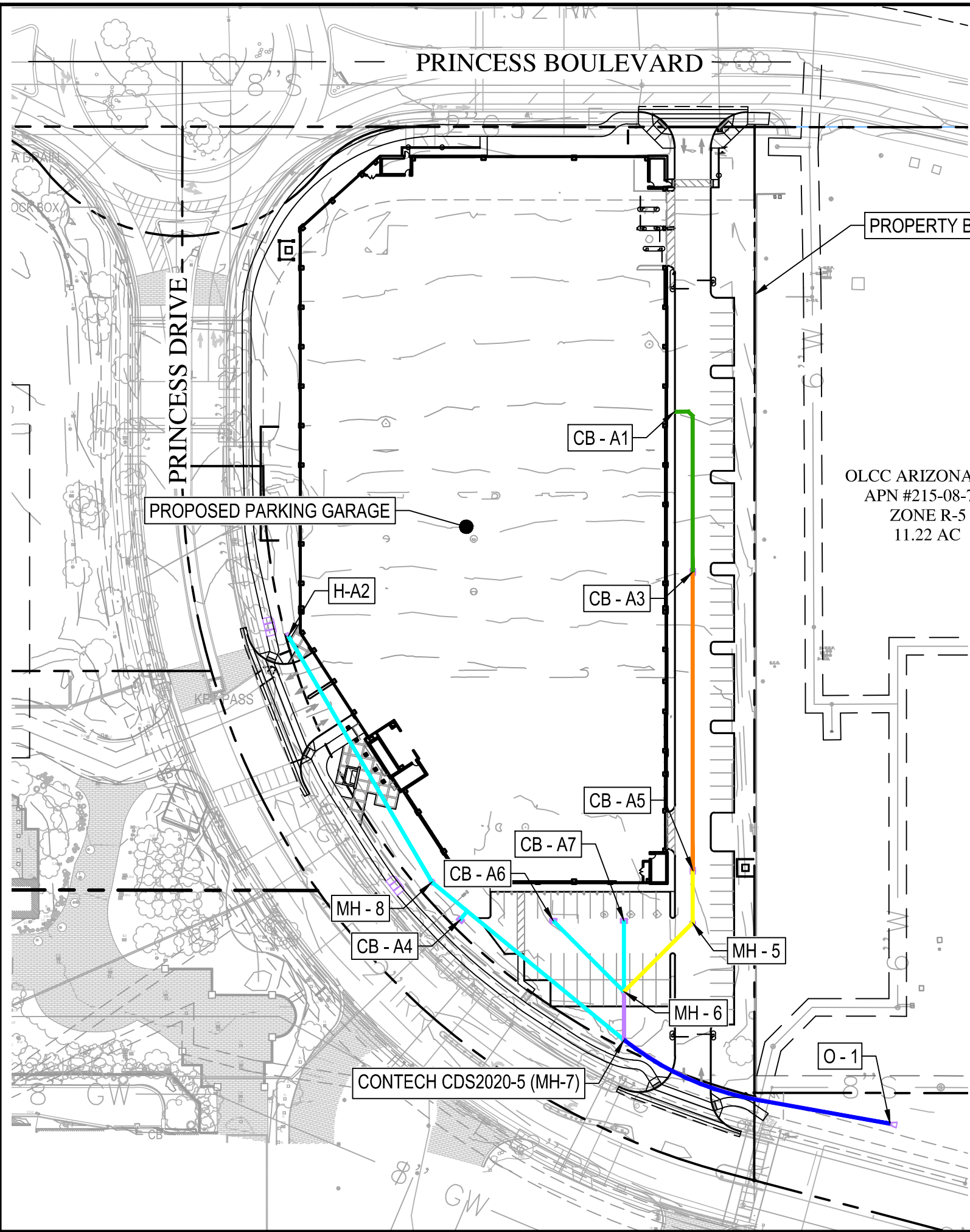
EXHIBIT 3 – EXISTING DRAINAGE AREA MAP

DATE	06/02/2023	SCALE	1" = 40'	SHEET	1 OF 1
JOB NO.	215319.40	DESIGN	AJS	DRAWN	AJS

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EXHIBIT 4 – PROPOSED DRAINAGE AREA MAP

EXHIBIT 5 – STORM DRAIN LAYOUT



LEGEND

- PROPOSED 12" STORM DRAIN PIPE
- PROPOSED 15" H.D.P.E PIPE
- PROPOSED 15" R.C.P PIPE
- PROPOSED 16" R.C.P PIPE
- PROPOSED 24" R.C.P PIPE
- PROPOSED 30" R.C.P PIPE
- MH-X MANHOLE
- CB-AX CATCH BASIN
- H-AX HEADWALL
- O-X OUTLET

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FAIRMONT SCOTTSDALE PRINCESS			
EXHIBIT 5 – STORM DRAIN LAYOUT			
DATE	06/02/2023	SCALE	1" = 80'
JOB NO.	215319.40	DESIGN	AJS
SHEET	1 OF 1	DRAWN	AJS
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