PRELIMINARY DRAINAGE REPORT

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Case #	6
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N.Baronas Reviewed By	3/11/2024 Date

Headwaters Scottsdale SEC of 100th Street and Frank Lloyd Wright Boulevard

Prepared for:

Headwater Group 5265 S Rio Grande Ste 201 Littleton, CO 80120



Prepared by:



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Headwaters Scottsdale

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SEC of 100th St and Frank Lloyd Wright Boulevard

MARCH 2023

Prepared By:

Kimley »Horn

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1 INTRODUCTION

1.1 PROJECT DESCRIPTION

Headwaters is proposing to build a 184,624 square foot building and five 3,861 square foot cottage buildings at 13850 North Frank Lloyd Wright Boulevard for a minimal residential heathcare development.

1.2 SITE LOCATION

The proposed minimal residential heathcare development encompasses approximately 6.71 net acres in a portion of the Southwest Quarter of Section 8 and a Portion of the Northeast Quarter of Section 17, Township 3 North, Range 5 East of the Gila and Salt River Base and Meridian in Maricopa County, Arizona. The site address is 13850 North Frank Lloyd Wright Boulevard, and the APN for the parcels are 217-26-953 and 217-26-954. More specifically, the Headwaters development is bounded by Frank Lloyd Wright Boulevard to the north, Belmont Village Senior Living to the east, single-family residential to the south, and 100th Street to the west (See Appendix A for Site Location Map and Legal Descriptions).

1.3 PURPOSE

This preliminary drainage report is intended to be the drainage guideline for development to take place for the minimal residential heathcare development and fulfill the City of Scottsdale drainage requirements. It describes the means and methods by which the storm water associated with the site will be handled post-development.

1.4 OBJECTIVES

This preliminary report provides a drainage plan for the proposed development that will meet the drainage standards and guidelines of the City of Scottsdale and the Flood Control District of Maricopa County (FCDMC). In particular, the report will demonstrate the following:

- 1. The project will designate on-site retention area requirements for the 100-year, 2-hour storm event and ensure that the retention tanks are drained within 36 hours.
- 2. Drainage facilities will be designed such that 100-year, 2-hour post-development flow is collected and conveyed in such a manner as to not cause damage to buildings and property

2 DESCRIPTION OF EXISTING DRAINAGE CONDITIONS AND CHARACTERISTICS

2.1 EXISTING ON-SITE DRAINAGE CONDITIONS

The site is currently an undeveloped vacant land. The north side of the subject parcel is currently bounded by Frank Lloyd Wright Boulevard. The east side of the is bounded by Belmont Village Senior Living. The south side is bounded by existing single family residential. The west is bounded by 100th Street.

The general topography of the site and surrounding areas is steep sloping terrain from the northeast to the southwest at a slope of approximately 2-2.5%. Storm water currently sheet flows across the site to the southwest to the existing on-site temporary surface retention area. Off-site flow from Frank Lloyd Wright Boulevard is captured by an existing catch basin and piped to a temporary retention basin. See Appendix D for Existing Conditions Topographic Map. The site outfalls at the southwest corner via storm drain pipe to a sidewalk pipe opening to the south.

2.2 EXISTING OFF-SITE DRAINAGE CONDITIONS

From field observation, site survey topography, and review of storm drain as-built drawings, no off-site flow from 100th Street will affect the site, but off-site flow from Frank Lloyd Wright Boulevard is anticipated to affect the site. The flow on Frank Lloyd Wright comes onto our site through an existing on grade 22-foot catch basin.

Off-site flows for stormwater from Frank Lloyd Wright Blvd were determined using City of Scottsdale topography. Based on the rational method the drainage watershed has a 13.5 cfs for the 100-year peak flow. The offsite curb opening was analyzed using flow master to determine the actual flow that would affect the site. Using the discharge for the entire drainage area, the existing slopes of the road and gutter it was determined that 68.28% of the flow will go to the curb opening and 31.72% would bypass the catch basin. This analysis determined that the actual flow going to the curb opening is 9.22 cfs and 4.28 cfs will bypass the curb opening. See Appendix H for the Flow Master results.

2.3 CONTEXT RELATIVE TO ADJACENT PROJECTS AND IMPROVEMENTS

The site is located north of the existing single-family residential development, west of 100th Street, south of Frank Lloyd Wright Boulevard and east of Belmont Village Senior Living. See Appendix G for Context Aerial of the site.

2.4 FEMA FLOOD HAZARD AREAS

The site is located in Flood Zone "X" according to the Flood Insurance Rate Map 4013C1780L, dated October 16, 2013. Zone "X" is designated by FEMA as "areas of 0.2% annual chance floor; areas of 1% annual chance floor with average depths of less than 1 foot or with drainage areas less than 1 square mile; and areas protected by levees from 1% annual chance flood."

3 PROPOSED DRAINAGE PLAN

3.1 GENERAL DESCRIPTION

The minimal residential heathcare development proposes to retain the 100-year, 2-hour storm event as outlined by the City of Scottsdale Drainage Guidelines. The 100-year, 2-hour storm will be retained in an underground retention tank located on the site. Due to the depth of the proposed underground retention tank, the stormwater will be disposed of using five drywells.

In the analysis of the proposed drainage conditions the following items are considered:

- > Area Types (asphaltic pavement, building, and desert landscaping)
- Magnitude of areas
- > Slopes
- Storm Drain
- Retention Tank

3.2 FUTURE CONDITIONS

No future drainage impacts are anticipated for the site due to the stormwater flow on Frank Lloyd Wright Boulevard already being accounted for and the fully developed area that surrounds the site.

3.3 STORM WATER STORAGE REQUIREMENTS

The on-site surface retention tank has been designed to retain the off-site runoff from Frank Lloyd Wright Boulevard and on-site runoff volume associated with the 100-year, 2-hour storm. The volume for the retention of Frank Llyod Wright was calculated by taking the flow captured percentage of the peak 100-year flow and applying it to the percent of drainage area of the contributing basin that would enter the site. 100th Street right-of-way drainage adjacent to the site is not included in the on-site hydraulic sub-areas due to the flow being kept in the road.

On-site retention volume will be provided by a 10' underground surface retention tank located along the west and north side of the site.

The high-water elevation of the tank has been designed to minimize the damage to site improvements such as paving, structures, utilities, walls, landscape, signs and lights.

The following Table 1 summarizes the retention basin name, type, total contributing area to the basin, runoff coefficient for the contributing area and the required and provided retention volume.

Basin	Land Use	Runoff Coefficient	Drainage Area (ac)	Required Volume (ac- ft)	Provided Volume (ac-ft)	Surplus
UG1	Landscaping	0.45	1.28	0.11		
	Parking/Building	0.95	7.04	1.28		
Total			8.32	1.39	1.39	0.00

Table 1: On-site Retention Volume

The on-site retention tank is designed such that the 100-year, 2-hour runoff volume is disposed of within 36 hours. The on-site retention tank will drain the storm water volume via five proposed drywells on-site in the required 36 hours. See in Appendix E for Basin Delineation and Appendix F for Preliminary Grading and Drainage Plan.

3.4 PROPOSED DRAINAGE STRUCTURES OR SPECIAL DRAINAGE FACILITIES

A retention tank is proposed at the northeast corner of the site to accommodate site-generated storm water for the 100-year, 2-hour storm event. Five proposed drywells located on the underground retention tank and dispose of the storm water. The final design will include a drainage easement to be dedicated to the City of Scottsdale for the proposed underground retention tank.

3.5 PROJECT PHASING

This project will be constructed in a single phase.

4 SPECIAL CONDITIONS

4.1 404 DISCUSSION

No 404/Jurisdictional Washes are anticipated to be located on-site.

4.2 STORM WATER QUALITY

The multifamily development will not be using any potential contaminants on site.

5 DATA ANALYSIS METHODS

5.1 HYDROLOGIC PROCEDURES, PARAMETER SELECTION, AND ASSUMPTIONS

Hydrologic calculations for the site will be performed using the rational equation in the FCDMC Drainage Design Manual Volume I, which is limited to drainage areas of up to 160 acres.

For on-site analysis of the minimal residential heathcare development, the site was sub-divided into four sub-basins consisting of the parking lot, landscaping, building, and Frank Lloyd Wright Boulevard. For each sub-basin, the Rational equation will be used to calculate the peak flow at each concentration point for each basin. Appendix E identifies the drainage subbasins for the proposed development. See Appendix C for the hydrologic calculations.

5.2 HYDRAULIC PROCEDURES, METHODS, PARAMETER SELECTION, AND ASSUMPTIONS

The site is divided into four sub-basins that drain into an on-site underground retention tank. See Appendix E for sub-basin boundaries and concentration points associated with each drainage basin.

All flows for proposed conditions were determined using the rational method as outlined by the Drainage Design Manual by Maricopa County Flood Control District. Due to the small nature of the watersheds for the individual sub-basins, a minimum time of concentration of five minutes was assumed. All of the drainage basins assume runoff coefficients of 0.95 (building/pavement) and 0.45 (landscape). The peak flows at the sub-basin concentration points will be calculated using the Rational equation.

The following criteria will be used to size the proposed pipes for on-site storm water conveyance and disposal:

- A maximum allowable 100-year ponding depth of 6 inches above the catch basin grate.
- A minimum of 12 inches of freeboard between the 100-year ponding depth and the building finish floor elevation.
- A maximum allowable 10-year ponding depth of 6 inches to contain all storm water runoff within the parking field.
- For the storm drain analysis, the tailwater condition for the 100-year event was assumed to be the depth of storage; the 10-year tailwater condition was assumed to be at the crown of the pipe.
- HGL's will be analyzed and provided with the final drainage report.
- Flow in and out both on-site and off-site will be provided with the final drainage report.

Storm drain calculations and profiles shall be provided in the final drainage report.

V_R =

5.3 STORM WATER STORAGE CALCULATION METHODS AND ASSUMPTIONS

Storm water storage requirements were calculated per City of Scottsdale and Flood Control District of Maricopa County design standards. The standard formula for determining the required storage volumes for the 100-year, 2-hour storm is as follows:

Equation 2: Standard Formula for On-Site Storage Requirement

 $V_R = CPA/12$

Where:

- C = weighted runoff coefficient
 - P = precipitation depth for 100-year, 2-hour event = 2.30 inches
 - A = contributing drainage area to basin (acres)

storage volume required (acre-feet)

6 CONCLUSION

6.1 OVERALL PROJECT

Based on the results of this preliminary drainage report, the following can be concluded:

- Based on the current Flood Insurance Rate Map, the minimal residential heathcare development is located in the zone "X".
- Underground retention tank will be provided to detain the post-development 100-year, 2-hour storm water.
- Underground retention tank will drain within 36 hours via five proposed on-site drywells.
- Storm drainage systems consisting of catch basins and storm drain pipe are provided to collect and convey drainage to the retention tank.
- Building finish floor elevation is at least fourteen inches above the ultimate site outfall elevation.
- A drainage easement for the surface retention tank will be dedicated with the final improvement plans and drainage report.

This preliminary drainage report is intended to provide a level of assurance that the minimal residential heathcare development will adhere to all appropriate reviewing agency guidelines with respect to drainage and flood protection.

7 REFERENCES

- 1. Federal Emergency Management Agency (FEMA), *Flood Insurance Rate Map (FIRM) of Maricopa County, Arizona and Incorporated Areas, Map Number 04013C1780 L*, October 16, 2013.
- 2. Flood Control District of Maricopa County (FCDMC), *Drainage Design Manual for Maricopa County, Hydrology Volume,* February, 2011.
- 3. Flood Control District of Maricopa County (FCDMC), *Drainage Design Manual for Maricopa County, Hydrology Volume,* February, 2011.

Appendix A – Site Location Map and Legal Descriptions



LEGAL DESCRIPTION

PARCEL 1:

LOTS 1 AND 2 OF FRANK LLOYD WRIGHT 100, ACCORDING TO THE PLAT OF RECORD IN THE OFFICE OF THE COUNTY RECORDER OF MARICOPA COUNTY, ARIZONA IN BOOK 1039 OF MAPS, PAGE 38.

PARCEL 2:

ALL EASEMENTS BENEFITTING THE LAND AS SET FORTH ON THE FINAL PLAT RECORDED IN THE OFFICE OF THE COUNTY RECORDER OF MARICOPA COUNTY, ARIZONA IN BOOK 1039 OF MAPS, PAGE 38.

PARCEL 3:

ALL EASEMENTS BENEFITTING THE LAND AS SET FORTH IN CROSS DRAINAGE EASEMENT AGREEMENT RECORDED IN THE OFFICE OF THE COUNTY RECORDER OF MARICOPA COUNTY, ARIZONA AS RECORDING NO. 2010–1100929 OF OFFICIAL RECORDS.

PARCEL 4:

ALL EASEMENTS BENEFITTING THE LAND AS SET FORTH IN DECLARATION OF COVENANTS, CONDITIONS AND RESTRICTIONS AND RECIPROCAL EASEMENT AGREEMENT RECORDED IN THE OFFICE OF THE COUNTY RECORDS OF MARICOPA COUNTY, ARIZONA AS RECORDING NO. 2010–1100559 OF OFFICIAL RECORDS.



Appendix B – FEMA Flood Insurance Rate Map (FIRM)

National Flood Hazard Layer FIRMette



Legend



Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020

Appendix C – Hydrologic Calculations

	Overall Retention Summary							
Drainage Area	Land Use	Area [A]		Runoff Coefficient	Rainfall Intensity (I)	Required Storage (V _{REQ} = C*I*A/12)		Detention Basin
		sf	ac	[C]	in	cf	ac-ft	
5	Pavement/Building	70,265	1.613	0.95	2.30	12,794	0.294	UG1
10	Landscaping	31,744	0.729	0.45	2.30	2,738	0.063	UG1
15	Landscaping	23,912	0.549	0.45	2.30	2,062	0.047	UG1
20	Pavement/Building	236,503	5.429	0.95	2.30	43,063	0.989	UG1
Total		362,425	8.320	-	-	60,658	1.393	

Basin	Land Use	Runoff Coefficient	Drainage Area (sf)	Required Volume (cf)	Provided Volume (cf)	Surplus (cf)
UG1	Landscaping	0.45	55,656	4,800		
	Pavement/Building	0.95	306,768	55,857		
			362,425	60,658	60,711	54

Underground Retention Summary						
Retention Basin	Required Volume Diameter Required Provided Provided					
	cf	ft	lf	If CMP	cf	
UG1	60,658	10	773	773	60,711	

Drywell Summary						
	Volumo	Percolation	Drywells	Drain Time		
Retention Basin	volume	Rate	Required	Drain Time		
	cf	cfs	ea	hr		
UG1	60,711	0.10	5	34		

Appendix D – Existing Conditions



K: \EAV_Civil \Headwaters Scottsdale \Drainage \Report \Appendix \Existing Conditions.dwg Mar 15, 2023 ally.fedor XREFS: xVF THS DOUMONT, TOGETHER WITH THE CONCEPTS AND DESIGNS PRESENTED HEREIN, AS AN INSTRUMENT OF SERVICE, IS INTENDED ONLY FOR THE SPECIFIC PURPOSE AND CLIENT FOR WHICH IT WAS PREPARED.



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Appendix E – Basin Delineation



LEGEND	

Appendix F – Preliminary Grading and Drainage



DESCRIPTION	QUANTITY	UNIT
INAL GRADE	9,108	CY
INAL GRADE	7,877	CY
	1,231	CY
ITIES LISTED ON THIS SHEET ARE APPROXIMATE /	AND ARE AN	



1 OF 4 SHEETS







GD3 3 OF 4 SHEETS





GD1 4 OF 4 SHEETS

Appendix G – Context Aerial Plan





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Appendix H – Flow Master Results

Project Description		
Solve For	Efficiency	
Input Data		
Discharge	13.50 cfs	
Slope	0.016 ft/ft	
Gutter Width	1.50 ft	
Gutter Cross Slope	0.111 ft/ft	
Road Cross Slope	0.032 ft/ft	
Roughness Coefficient	0.015	
Curb Opening Length	22.0 ft	
Local Depression	0.2 ft	
Local Depression Width	22.0 ft	
Results		
Efficiency	68.28 %	
Intercepted Flow	9.22 cfs	
Bypass Flow	4.28 cfs	
Spread	12.4 ft	
Depth	6.2 in	
Flow Area	2.6 ft ²	
Gutter Depression	0.1 ft	
Total Depression	0.3 ft	
Velocity	5.27 ft/s	
Equivalent Cross Slope	0.036 ft/ft	
Length Factor	0.472	
Total Interception Length	46.7 ft	

Offsite Curb Opening on FLW

Existing 18" Pipe N to S

Project Description		
Friction Method	Manning Formula	
Solve For	Full Flow Capacity	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.011 ft/ft	
Normal Depth	18.0 in	
Diameter	18.0 in	
Discharge	14.05 cfs	
Results		
Discharge	14.05 cfs	
Normal Depth	18.0 in	
Flow Area	1.8 ft ²	
Wetted Perimeter	4.7 ft	
Hydraulic Radius	4.5 in	
Top Width	0.00 ft	
Critical Depth	16.6 in	
Percent Full	100.0 %	
Critical Slope	0.009 ft/ft	
Velocity	7.95 ft/s	
Velocity Head	0.98 ft	
Specific Energy	2.48 ft	
Froude Number	(N/A)	
Maximum Discharge	15.11 cfs	
Discharge Full	14.05 cfs	
Slope Full	0.011 ft/ft	
Flow Type	Undefined	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0 00 ft	
	0.00 10	
Average End Depth Over Rise	0.0 %	
Average End Depth Over Rise Normal Depth Over Rise	0.00 % 100.0 %	
Average End Depth Over Rise Normal Depth Over Rise Downstream Velocity	0.0 % 100.0 % Infinity ft/s	
Average End Depth Over Rise Normal Depth Over Rise Downstream Velocity Upstream Velocity	0.0 % 100.0 % Infinity ft/s Infinity ft/s	
Average End Depth Over Rise Normal Depth Over Rise Downstream Velocity Upstream Velocity Normal Depth	0.0 % 100.0 % Infinity ft/s Infinity ft/s 18.0 in	
Average End Depth Over Rise Normal Depth Over Rise Downstream Velocity Upstream Velocity Normal Depth Critical Depth	0.0 % 100.0 % Infinity ft/s Infinity ft/s 18.0 in 16.6 in	
Average End Depth Over Rise Normal Depth Over Rise Downstream Velocity Upstream Velocity Normal Depth Critical Depth Channel Slope	0.0 % 100.0 % Infinity ft/s Infinity ft/s 18.0 in 16.6 in 0.011 ft/ft	

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Existing 18" Pipe E to W

Project Description		
Friction Method	Manning Formula	
Solve For	Full Flow Capacity	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.007 ft/ft	
Normal Depth	18.0 in	
Diameter	18.0 in	
Discharge	11.09 cfs	
Results		
Discharge	11.09 cfs	
Normal Depth	18.0 in	
Flow Area	1.8 ft ²	
Wetted Perimeter	4.7 ft	
Hydraulic Radius	4.5 in	
Top Width	0.00 ft	
Critical Depth	15.3 in	
Percent Full	100.0 %	
Critical Slope	0.006 ft/ft	
Velocity	6.28 ft/s	
Velocity Head	0.61 ft	
Specific Energy	2.11 ft	
Froude Number	(N/A)	
Maximum Discharge	11.93 cfs	
Discharge Full	11.09 cfs	
Slope Full	0.007 ft/ft	
Flow Type	Undefined	
GVF Input Data		
Downstream Depth	0.0 in	
Length	0.0 ft	
Number Of Steps	0	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	100.0 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	18.0 in	
Critical Depth	15.3 in	
Channel Slope	0.007 ft/ft	
Critical Slope	0.006 ft/ft	
	Bentley System	ns. Inc. Haestad Methods Solution

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Project Description		
Friction Method	Manning	
	Formula	
Solve For	Full FIOW Canacity	
	Capacity	
Input Data		
Roughness Coefficient	0.010	
Channel Slope	0.012 ft/ft	
Normal Depth	8.0 in	
Diameter	8.0 in	
Discharge	1.75 cfs	
Results		
Discharge	1 75 cfc	
Normal Denth	2.75 CIS & 0 in	
Flow Area	0.3 ft ²	
Wetted Perimeter	2.1 ft	
Hydraulic Radius	2.0 in	
Top Width	0.00 ft	
Critical Depth	7.3 in	
Percent Full	100.0 %	
Critical Slope	0.011 ft/ft	
Velocity	5.01 ft/s	
Velocity Head	0.39 ft	
Specific Energy	1.06 ft	
Froude Number	(N/A)	
Maximum Discharge	1.88 cfs	
Discharge Full	1.75 cfs	
Slope Full	0.012 ft/ft	
Flow Type	Undefined	
GVF Input Data		
Downstream Denth	0.0 in	
Length	0.0 m	
Number Of Steps	0.0 10	
GVF Output Data		
Upstream Depth	0.0 in	
Profile Description	N/A	
Profile Headloss	0.00 ft	
Average End Depth Over Rise	0.0 %	
Normal Depth Over Rise	100.0 %	
Downstream Velocity	Infinity ft/s	
Upstream Velocity	Infinity ft/s	
Normal Depth	8.0 in	
Critical Depth Channel Clane	7.3 in	
Channel Slope	0.012 π/ft	
Untical Slope	υ.υ11 π/ft	
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Existing Bleed Off Pipe

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