PRELIMINARY DRAINAGE REPORT

For MERCADO VILLAGE

10301 N. 92nd Street Scottsdale, AZ 85254

Prepared For:



8901 E. Mountain View Road, Suite 150 Scottsdale, AZ 85258 480.455.6480

Prepared by:



Sustainability Engineering Group

5240 N. 16th Street, Suite 105 Phoenix, AZ 85016 480.588.7226 <u>www.azSEG.com</u>

Project Number: 210414

Case #: 1-ZN-2024 Review Cycle: 2

Status: Accepted

Reviewed By: VM

Date:04/12/2024



1st Submittal Date: January 9, 2024 (Zoning) 2nd Submittal Date: March 18, 2024 (Zoning)

Case No: 1-ZN-2024 Plan Check No.: TBD



Table of Contents

LIST OF TABLES	2
LIST OF FIGURES:	2
APPENDIX:	2
1. INTRODUCTION	3
2. LOCATION AND PROJECT DESCRIPTION	3
2.1 LOCATION:	3
2.2 EXISTING AND PROPOSED DEVELOPMENTS SURROUNDING THE SITE:	3
2.3 EXISTING SITE DESCRIPTION:	3
2.4 PROPOSED SITE DEVELOPMENT:	4
2.5 FLOOD HAZARD ZONE:	4
3. EXISTING DRAINAGE CONDITIONS	4
3.1 OFF-SITE DRAINAGE PATTERNS	4
3.3 ON-SITE DRAINAGE	4
4. PROPOSED STORM WATER MANAGEMENT	6
4.1 DESIGN INTENT:	6
4.2 DESIGN STORM REQUIREMENTS:	7
4.3 LAND CHARACTERISTICS:	7
4.4 STORMWATER RETENTION:	g
4.8 ADEQ WATER QUALITY REQUIREMENTS	11
5. FLOOD SAFETY FOR DWELLINGS	11
5.1 FINISHED FLOOR ELEVATIONS	11
6. CONCLUSIONS	12
6.1 OVERALL PROJECT:	12
7. WARNING AND DISCLAIMER OF LIABILITY	12
8. REFERENCES	17





LIST OF TABLES

TABLE 1 - Existing Weighted Runoff Coefficients

TABLE 2 - EX. Basin 1 Provided Volume

TABLE 3 - Existing Onsite Flows

TABLE 4 - Proposed and Existing Flows ComparisonTABLE 5 - Proposed Conditions Runoff Calculations

TABLE 6 - Proposed Onsite Flows

TABLE 7 - Proposed Conditions Required Storage Volume



LIST OF FIGURES:

FIGURE 1 - Vicinity Map
FIGURE 2 - Aerial Map
FIGURE 3 - FIRM Map
FIGURE 4 - FIRMette Map

APPENDIX:

APPENDIX I - Rainfall Data
APPENDIX II - Calculations

APPENDIX III - Grading and Drainage Plan



1. INTRODUCTION

This Preliminary Drainage Report represents the storm water analysis for Mercado Village development proposed in Scottsdale, Arizona. Mercado Village is a proposed multi-family residential development located south and east of the Shea Boulevard and 92nd Street intersection. The purpose of this report is to provide the hydrologic and hydraulic analysis, required by the City of Scottsdale, to support the proposed rezoning for said development. This report includes discussions and calculations defining the storm water management concepts for the collection and conveyance necessary to comply with the drainage requirements of the City of Scottsdale and Maricopa County. Preparation of this report has been done in accordance with the requirements of the City of Scottsdale Design Standards & Policies Manual (DS&PM) 2018 ¹, and the Drainage Design Manuals for Maricopa County, Arizona, Volumes I² and Volume II³.

2. LOCATION AND PROJECT DESCRIPTION

2.1 LOCATION:

The subject property consists of five contiguous parcels located south and east of Shea Boulevard and 92nd Street in Scottsdale, AZ.

- A Portion of the Northeast Quarter of Section 30, Township 3 North, Range 5 East of The Gila and Salt River Base and Meridian, Maricopa County, Arizona.
- Parcel ID: Parcel 217-39-536, Zoning is PUD

Parcel 217-39-537A, Zoning is PUD Parcel 217-39-537B, Zoning is PUD Parcel 217-39-537C, Zoning is PUD Parcel 217-36-989B, Zoning is C-O PCD

Address: 10301 N. 92nd Street. Scottsdale, Arizona 85258.

Refer to **FIGURE 1** - **Vicinity Map** for the project's location with respect to major cross streets.

2.2 EXISTING AND PROPOSED DEVELOPMENTS SURROUNDING THE SITE:

- South: Parcel with APN 217-74-038, a medical office development; Zoning is C-O PCD.
- North: Parcel with APN 217-36-960L, Sprouts shopping center; Zoning is C-3 PCD.
- East: Parcel 217-36-001P; paved area and medical offices, Zoning is C-O PCD.
- West: Across N. 92nd St. is Parcel 217-36-962G; medical offices; Zoning is SC PCD.

2.3 EXISTING SITE DESCRIPTION:

The project area includes approximately 263,945 sq. ft. (6.06 acres) of land designated as PUD, with the exception of parcel with APN 217-36-989B at the east which has a zoning of C-O PCD. The site is partially developed, the west side includes medical offices with associated parking lot, driveways and landscape areas; the east area is mainly undeveloped but has a small parking lot constructed at the south which connects to the eastern area of the site. The parcels generally slope towards the southwest corner. Disturbed area of the site is approximately 277,578 sq. ft. (6.37 acres).

Refer to FIGURE 2 attached for an aerial of the site.



2.4 PROPOSED SITE DEVELOPMENT:

The proposed project will require the demolition of existing structures and associated parking lots. The proposed site will include a new high-density residential facility with 255 units, the building will have a central at-grade parking garage and rise to five floors.

Refer to **Appendix III** – Preliminary Grading and Drainage Plan for site layout.

2.5 FLOOD HAZARD ZONE:

FIRM Map Number 04013C1760L dated October 16, 2013 indicates the site has a Zone X-Shaded designation. Zone X-Shaded is defined as 0.2% Annual Chance Flood Hazard, Areas of 1% annual chance flood with average depth less than one foot or with drainage areas of less than one square mile.

Refer to **FIGURE 3** for the FIRM and FIRMette Maps.

3. EXISTING DRAINAGE CONDITIONS

3.1 OFF-SITE DRAINAGE PATTERNS

The topographic survey provides the following information for offsite drainage:

- The north of the site is bounded by Sprouts Shopping center, which has its own drainage system. A ridgeline prevents stormwater from Sprouts Shopping Center parking lot to enter the site. No offsite flows from the north affect the site.
- The west of the site is bounded by N. 92nd Street. Half of the street run-off drains towards the property and is conveyed via curb and gutter into an existing catch basin (EX-OFF-CB-1) adjacent to the property that discharges to an existing 36" CIP storm drain running along the east side of the road. No offsite flows from the west affect the site
- The south of the site is bounded by a medical office development. The medical office
 development has its own drainage system and a wall separating the two properties
 prevents stormwater from entering the site. No offsite flows from the south affect the
 site.
- The east of the site is adjacent to a paved area and medical offices. The medical office
 has its own drainage system and grades on the paved area go away from the site. No
 offsite flows from the east affect the site.

3.3 ON-SITE DRAINAGE

Most of the runoff from the site is collected by existing catch basins (EX. CB-1 and EX. CB-2) and slotted drains (EX. SD-1, EX. SD-2, EX. SD-3) ultimately conveyed to the public network storm system at 92nd Street. The majority of stormwater from drainage area EX-1 flows easterly into a gutter and then proceeds to flow south into EX. CB-1. A small portion of runoff from drainage area EX-2 flows towards the northeast into EX. CB-1. Runoff from drainage area EX-2 flows towards EX. CB-2 located in the mid-west of the drainage area. Runoff from drainage area EX-3 flows westerly into a wall opening which leads stormwater into a slotted drain (EX. SD-1). Stormwater on drainage area EX-4 follows the same pattern as drainage area EX-3, flowing westerly into an opening and discharging into a slotted drain (EX. SD-2). Runoff from drainage



area EX-5 flows southerly into an on-site curb and gutter, and then proceeds to flow westerly into a wall opening leading stormwater into a slotted drain (EX-SD-3). Stormwater from EX-6 flows westerly into N. 92nd Street, where half of the runoff flows northwesterly into EX-OFF-CB-1 and the other half flows southeasterly along the street via curb and gutter. Stormwater collected on EX-R-1 drains through roof drains towards drainage area EX-1 ultimately draining into EX-CB-1. Stormwater collected on EX-R-2 drains through roof drains towards drainage area EX-4 ultimately draining into EX. SD-2. Open retention basin, EX. Basin 1, collects stormwater on drainage area EX-7. Existing storm drains are ultimately connected to the existing 36" public drain along 92nd Street.

Refer to Appendix II for Existing Conditions Drainage Area Map.

Existing runoff coefficients and flows for the 100-year, 5 min. event are presented in the tables below. Coefficients of 0.95 and 0.45 were chosen for building or concrete and desert landscape respectively, in accordance with the city of Scottsdale DS&PM.

Table 1. Existing Weighted Runoff Coefficients.

W	Weighted Runoff Coefficient-Calculations (Cw)									
EXISTING OVERALL SITE C _w										
	BUILDING or CONCRETE	DESERT LANDSCAPE	TOTAL AREA	Cwt						
C-VALUE	0.95	0.45								
AREA (ac)	3.33	2.73	6.06	0.72						
EX-1	1.39	0.44	1.83	0.83						
EX-2	0.17	0.25	0.42	0.65						
EX-3	0.29	0.08	0.37	0.84						
EX-4	0.31	0.21	0.52	0.75						
EX-5	0.23	0.16	0.39	0.74						
EX-6	0.05	0.00	0.05	0.95						
EX-7	0.00	1.58	1.58	0.45						
EX-R-1	0.69	0.00	0.69	0.95						
EX-R-2	0.20	0.00	0.20	0.95						



The open retention Ex. Basin 1 provided volume is displayed in the table below:

Table 2. EX. Basin 1 Provided Volume

	EX. Basin 1									
ELEV. AREA DEPTH AVG V SUM V COMMENT										
(FT)	(SF)	(FT)	(CF)	(CF)						
1369.0	382			0.00	Bottom					
2.00 1,704.33										
1371.0	1,314			1,704.33	Volume					

Table 3. Existing Onsite Flows

	EXIST	ING ON	ISITE 100	YR 5 MII	N FLOWS		
Drainage Area	Area (ac)	Cw	i (in/hr)	Q (cfs)	Q Total (cfs)	Control Point	
EX-1	1.83	0.83	7.54	11.45			
EX-2	0.42	0.65	7.54	2.04		Public Storm	
EX-3	0.37	0.84	7.54	2.37			
EX-4	0.52	0.75	7.54	2.94	27.75		
EX-5	0.39	0.74	7.54	2.17	27.75	Drain at 92nd Street	
EX-6	0.05	0.95	7.54	0.39		Street	
EX-R-1	0.69	0.95	7.54	4.93			
EX-R-2	0.20	0.95	7.54	1.47			
EX-7	1.58	0.45	7.54	5.37	5.37	EX-BASIN 1	

Overall existing project area includes 6.06 Acres at C_{wt} = 0.72

Refer to **Appendix II** for 10-year event calculations.

4. PROPOSED STORM WATER MANAGEMENT

4.1 DESIGN INTENT:

Most of the on-site drainage will be directed off-site through a storm drain system to the historical outlets. The drainage proposal will be consistent with previous conditions of the site to avoid disrupting existing drainage patterns. Flows exposed to contaminated surfaces will also be treated prior to being released as a measure to control the quality of stormwater. Drainage areas A1 through A3 will be directed towards Basin 1 via catch basins and storm pipes. Drainage areas B1 through B6 will be directed to the city's public storm system. Proposed drainage patterns are as follow:

- Drainage area A1 will flow southerly into CB-1.
- Stormwater from drainage area A2 will flow towards its center into CB-2 (CMP riser).
- Runoff from drainage area A3 will flow via roof drain into Basin A



- Drainage area B1 will discharge into CB-3.
- Drainage area B2 will discharge runoff into the existing EX. SD-1 via a wall opening.
- Stormwater from Drainage area B3 will discharge into the EX. SD-2 via a wall opening.
- Runoff from drainage area B4 will flow southwesterly into CB-4. EX. SD-3 has been replaced due to increase in flow.
- Drainage area B5 will flow into CB-5.

Flows discharging to the existing slotted drains are reduced. The table below summarizes the flow reduction in the slotted drains and overall flows to the public storm drain system.

Table 4. Proposed and Existing Flows Comparison

P. DAM	Ex. DAM	Proposed Q100 CFS	Existing Q100 CFS	Difference	Inlet
B-2	EX-3	0.42	2.37	-1.96	EX. SD 1
B-3	EX-4	0.38	2.94	-2.56	EX. SD 2
Total On-site flows		27.10	27.75	-0.65	Public Storm Drain

Since the site has been previously developed, on-site retention shall be calculated per City of Scottsdale DSPM 4-1.201.

4.2 DESIGN STORM REQUIREMENTS:

In accordance with City of Scottsdale requirements, stormwater storage for the 100-year 2-hour storm event is required based on maintaining existing retention volume plus the difference between the pre vs. post development runoff from the 100-year 2-hour storm event if increased or first flush, whichever is greater. Per topographic information, there is an existing open retention basin in the site. As such, retention shall be provided by the sum of the existing retention volume plus the pre vs. post difference in volume or first flush.

4.3 LAND CHARACTERISTICS:

The proposed project site consists of residential spaces with a main drive and landscape areas. Based on the City of Scottsdale Design Standards & Policies Manual (DSPM), runoff coefficients for the 100-year storm event used are as follows:

- C=0.95 for building or concrete
- C=0.95 for paved surface
- C=0.45 for undisturbed natural desert or desert landscape

HYDROLOGIC ANALYSIS: The hydrologic analysis is determined using the procedures in the DSPM and the Drainage Design Manual for Maricopa County, Arizona, Volume I.



Table 5: Proposed Conditions Runoff Calculations

Wei	ghted Runoff C	Coefficient-Calc	culations (C	Cw)						
PROPOSED OVERALL SITE C _w										
	BUILDING or CONCRETE	DESERT LANDSCAPE	TOTAL AREA	Cwt						
C-VALUE	0.95	0.45								
AREA (ac)	4.34	1.72	6.06	0.81						
A1	0.29	0.37	0.66	0.67						
A2	0.31	0.14	0.44	0.80						
A3	0.51	0.06	0.57	0.90						
B1	0.44	0.25	0.69	0.77						
B2	0.03	0.06	0.09	0.61						
В3	0.01	0.10	0.10	0.48						
B4	0.36	0.29	0.65	0.73						
B5	0.06	0.26	0.32	0.54						
В6	2.34	0.19	2.53	0.91						

Overall project area includes **6.06** Acres at C_{wt} = **0.81**.

Table 6. Proposed Onsite Flows.

	PROPOSED ONSITE 100 YR 5 MIN FLOWS									
Drainage Area	Area (ac)	Cw	i (in/hr)	Q (cfs)	Q Total (cfs)	Control Point				
A1	0.66	0.67	7.54	3.31						
A2	0.44	0.80	7.54	2.65	9.81	BASIN A				
A3	0.57	0.90	7.54	3.85						
B1	0.69	0.77	7.54	4.01						
B2	0.09	0.61	7.54	0.42						
В3	0.10	0.48	7.54	0.38	27.10	Public Storm				
B4	0.65	0.73	7.54	3.58	27.10	Drain at 92 nd Street				
B5	0.32	0.54	7.54	1.30		Jueet				
В6	2.53	0.91	7.54	17.41						

Refer to the **Proposed Cwt Exhibit (Exhibit B)**, **Proposed Conditions Drainage Area Map (Exhibit D)** and Calculations in **Appendix II**.



4.4 STORMWATER RETENTION:

100-YR, 2-HR STORM: Per City of Scottsdale DSPM 4-1.201, development storage requirements for the 100-yr, 2-hr storm event are calculated as follows:

$$V_r = \Delta C \left(\frac{R}{12}\right) A$$

where:

 V_r = Required storage (cf)

R =Precipitation amount =2.22 in per NOAA Atlas 14 Precipitation Frequency Estimates

A = Total area of site (sf)

 $\Delta C = C_{post} - C_{pre}$

$$V_r = (0.81 - 0.72) \left(\frac{2.22}{12}\right) (263,945) = 4,394.68 \, cf$$

Since the difference of the weighted coefficient is greater than 0, an increase in stormwater flows will be generated. Therefore, stormwater retention is required for the development following the pre vs. post analysis. The volume provided by EX. Basin 1 must be added to the pre vs. post analysis volume to compare it with the first flush volume. The addition of the volumes is 1,704.33 cf + 4,394.68 cf = 6,099.01 cf.

FIRST FLUSH: First Flush storage required is calculated in accordance with City of Scottsdale DSPM 4-1.201. Only the areas where runoff could be affected by vehicular contact are considered in the first flush calculation. The roof drainage is considered to be free of heavy traffic pollutants, therefore, on-site driveway areas and sidewalks will be considered for the calculation (277,578 sf (total area) - 75,047 sf (landscape) - 124,050 sf (roof) = 78,481 sf.

$$FF_r = C\left(\frac{P}{12}\right)A$$

where:

 FF_r = First Flush required storage volume (cf)

A =Area of site excluding roofs and landscape (sf)

C = The weighted average runoff coefficient =0.95

$$FF_r = (0.95) \left(\frac{0.5}{12}\right) 78,481 = 3,106 \ cf$$

The above assessment indicates that First Flush storage is required (3,106 cf). Since the volume from the pre vs. post analysis is greater than the volume from the first flush analysis, retention must be provided for a minimum of 6,099.01 cf per the City of Scottsdale DS&PM.

Given that stormwater volume will be increased, underground storage (Basin A) is proposed to retain the required pre vs post volume plus existing required volume.

To comply with the City of Scottsdale DS&PM, flows from drainage areas A1 and A2 will be directed to Basin A. Below is a summary of their required volumes.



Table 7. Proposed Conditions Required Storage Volume

	Required Storage Volume									
Vr=1*(P/12)*Cw*A										
				P=100-yr, 2-hr=2.22 in.						
Drainage	Area	Cw	Precipitation	Volume Req.	Volume Req.					
<u>Area ID</u>	(acres)	<u>(-)</u>	<u>(in)</u>	(acre-ft)	<u>(CF)</u>					
A1	0.66	0.67	2.22	0.08	3,534.66					
A2	0.44	0.80	2.22	0.07	2,836.78					
A3	0.57	0.90	2.22	0.09	4,113.86					
В	BASIN A Total Retention: 10,485.									

A volume of 10,485 cf will be retained by the proposed underground storage Basin A in order to comply with the pre vs post analysis and reduce flows to historical outfalls.

UNDERGROUND STORMWATER STORAGE POLICY

Per Section 4-1.202 of the City of Scottsdale's Design Standards & Policies Manual (DSPM), the proposed underground stormwater storage tanks (USSTs) must meet the City's Underground Stormwater Storage Policy, which states the following items:

- a) The owner must dedicate a public drainage easement over the USST and a minimum of 10' wide vehicular access easements to the basin, with no major vegetation such as trees within the easement. At a minimum, the easement should extend at a projected slope of 1:1 from the bottom of the pipe.
- b) The USST must have at least a 75-year life, including the lining and coating.
- c) The USST must drain by gravity.
- d) Specify MAG supplemental standard detail 2554 for corrugated metal pipes.
- e) A minimum of two access points must be provided for each USST.
- f) An Operations and Maintenance (O&M) Manual must be prepared for the system prior to approval of final plans.
- g) Final plans must include signs at each end of the USST.
- h) A signed and notarized Ownership and Responsibility Statement must be provided prior to approval of final plans.
- i) Add the required warning signs.

PROVIDED STORMWATER STORAGE

The proposed development will provide storage for the pre vs post analysis and existing required volume through a corrugated metal pipe underground system. Stormwater will be discharged by the use of drywells.



Basin A provided storage:

Basin A will consist of 10' diameter corrugated metal pipe and will have a length of 135 LF.

 $V_P = \pi^*$ Pipe radius² * Pipe length

 $V_P = (\pi * 5^2)*(135) = 10,603 \text{ cf}$

Refer to **Appendix II** for existing and proposed volume calculations.

4.6 STORMWATER DISCHARGE

For basins with no direct bleed-off available, drywells are proposed in the on-site storage facilities to dispose of stormwater within thirty six (36) hours. The calculation is as follows:

- Minimum percolating rate of a drywell (for planning purposes) = 0.1 cfs
- Volume to be drained in 36 hours = 0.1 cfs * 36 hours * 3600 sec/hour = 12,960 cf = 0.298 acre-feet.
- The number of drywells will be reduced if geotechnical testing for percolation rates determine adequate infiltration is available in the native soils at lower depths. If the percolation rate of the drywells is less than 0.1 cfs the number of drywells may have to be increased.

Basin A:

Total provided storage = 10,603 CF 10,603 CF / 12,960 CF per drywell = 0.82 = 1 drywell required.

4.7 PIPE HYDRAULICS CALCULATIONS

The proposed drainage system consists of HDPE pipes (n=0.013) conveying a portion of the runoff flows towards the Public Storm Drain System at 92nd Street and the remainder runoff towards Basin A. Capacity of the system was evaluated for the 100-year event scenario using StormCAD, the storm pipes have the capacity to convey the total runoff of the drainage areas.

Refer to Appendix IV for StormCAD Results.

4.8 ADEQ WATER QUALITY REQUIREMENTS

The Arizona Department of Environmental Quality (ADEQ) requires that any site disturbance over an acre is required to submit an NOI. An NOI will be submitted to ADEQ for this site after the first submittal of the construction documents as this site disturbance is over 1 acre and has flows going off-site.

5. FLOOD SAFETY FOR DWELLINGS

5.1 FINISHED FLOOR ELEVATIONS

Since project lies in an "X-Shaded" Flood Zone, finished floor elevations will also comply with the minimum elevation of 14 inches above the Ultimate Outfall of the site (1,368.66'), located on the southwest corner of the site and at least 12 inches above adjacent HWE's. The minimum proposed finish floor elevation of 1,371.25' within the project is in accordance with the previous criteria, ensuring that the building will be safe from flooding during a 100-year storm.



6. CONCLUSIONS

6.1 OVERALL PROJECT:

- 1. The finished floor elevations will be designed a minimum of 14 inches above the lot Ultimate Outfall.
- 2. Historical outfalls will be maintained at proposed conditions and no detrimental effects will be posed to existing drainage patterns.
- 3. On-site retention facilities will be provided to account for pre vs. post analysis plus existing retention.

7. WARNING AND DISCLAIMER OF LIABILITY

RE: Following page.

8. REFERENCES

- 1. Design Standards & Policies Manual, City of Scottsdale January 2018
- 2. Drainage Design Manual for Maricopa County, Arizona, Volume I, Hydrology, Flood Control District of Maricopa County, Fourth Edition, December 14, 2018
- 3. Drainage Design Manual for Maricopa County, Arizona, Volume II, Hydraulics, Flood Control District of Maricopa County, December 14, 2018

GRADING & DRAINAGE LANGUAGE

WARNING AND DISCLAIMER OF LIABILITY

The City's Stormwater and Floodplain Management Ordinance is intended to minimize the occurrence of losses, hazards and conditions adversely affecting the public health, safety and general welfare which might result from flooding. The Stormwater and Floodplain Management Ordinance identifies floodplains, floodways, flood fringes and special flood hazard areas. However, a property outside these areas could be inundated by floods. Also, much of the city is a dynamic flood area; floodways, floodplains, flood fringes and special flood hazard areas may shift from one location to another, over time, due to natural processes.

WARNING AND DISCLAIMER OF LIABILITY

The flood protection provided by the Stormwater and Floodplain Management Ordinance is considered reasonable for regulatory purposes and is based on scientific and engineering considerations. Floods larger than the base flood can and will occur on rare occasions. Floodwater heights may be increased by constructed or natural causes. The Stormwater and Floodplain Management Ordinance does not create liability on the part of the city, any officer or employee thereof, or the federal, state or county government for any flood damages that result from reliance on the Ordinance or any administrative decision lawfully made thereunder.

Compliance with the Stormwater and Floodplain Management Ordinance does not ensure complete protection from flooding. Flood-related problems such as natural erosion, streambed meander, or constructed obstructions and diversions may occur and have an adverse effect in the event of a flood. You are advised to consult your own engineer or other expert regarding these considerations. I have read and understand the above.

Plan Check # Owner Date



FIGURES

Figure 1. Vicinity Map

Figure 2. Aerial

Figure 3. FIRM

Figure 4. FIRMette

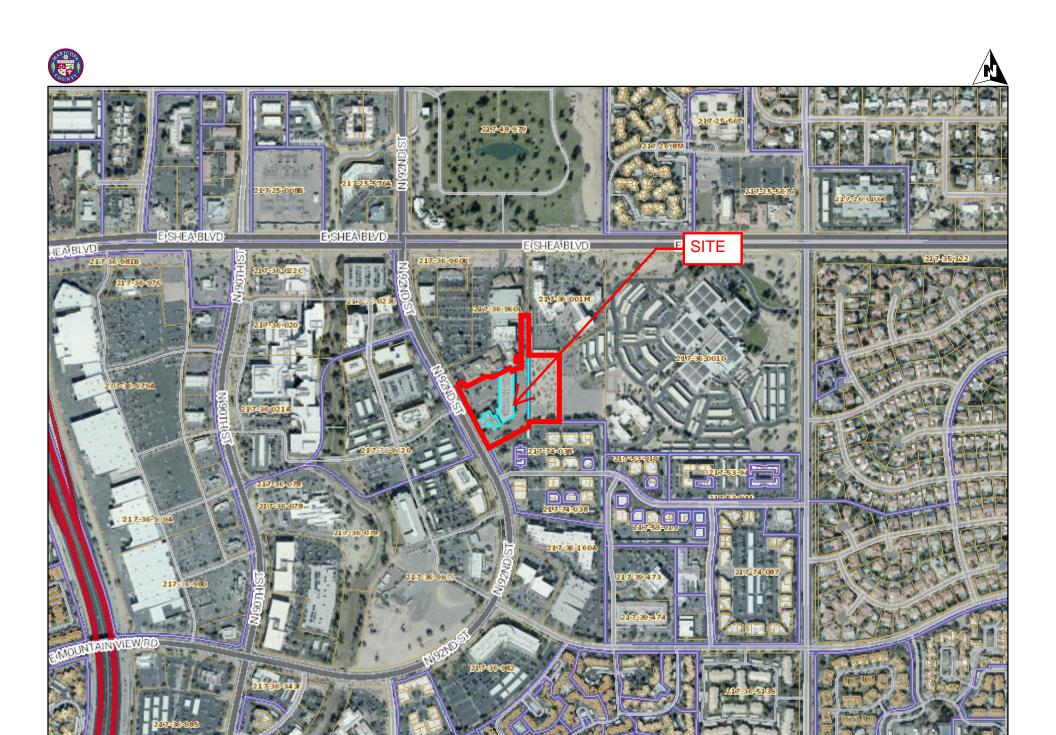
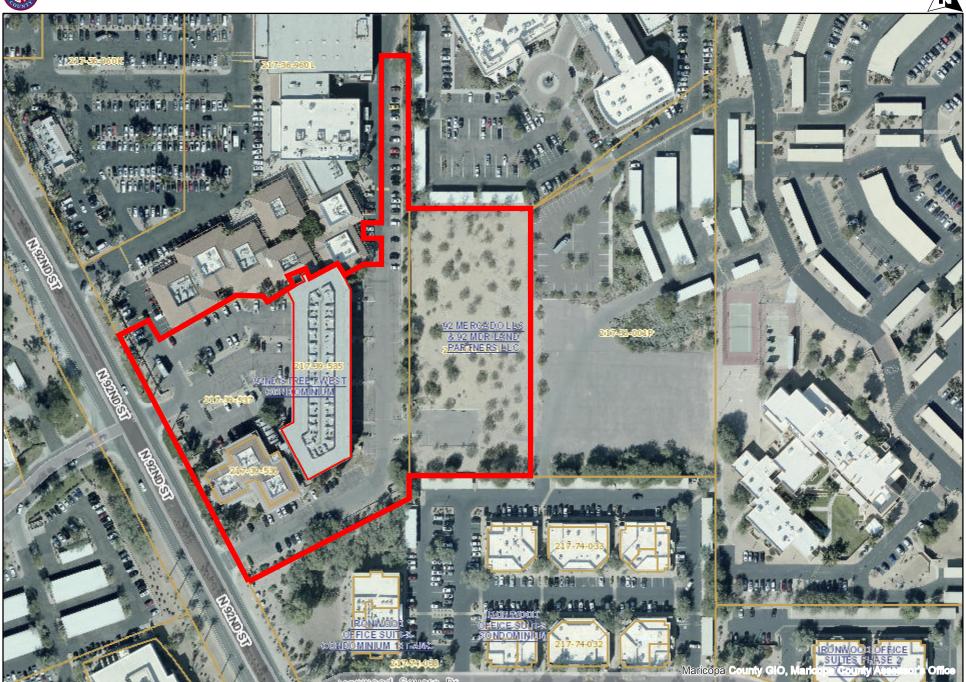


Figure 1. Vicinity Map

4/30/2021 8:28:32 AM





4/29/2021 5:23:10 PM

Figure 2. Aerial

NOTES TO USERS

This map is for use in administering the Nation Flood Insurance Program. It does not necessarily identify all areas subject to flooding, particularly from local drainage sources of small size. The community map repository should be consulted for possible updated or additional flood hazard information.

position of position of additional information is incrementative. Base Fixed Exercision To offician more information in the many of the position of the Fixed Profiles and Fixed Profile

Coastal Base Flood Elevations shown on this map apply only landward of 0.07 who find merican Portical Datum of 1989 (NAVD 98), users of this Fifth should be wavere that coastal flood elevations are also provided in the Summary of Stillward Elevations table in the Flood Instance Study report for this jurisdiction. Elevations shown in the Summary of Stillward Elevations table should be used for construction and/of Bootplain management purposes when they are higher than

Boundaries of the **floodways** were computed at cross sections and interpolated between cross sections. The floodways were based on hydraulic considerations with regard to requirements of the National Flood Insurance Program. Floodway widths and other pertinent floodway data are provided in the Flood Insurance Study

Certain areas not in Special Flood Hazard Areas may be protected by **flood control structures**. Refer to Section 2.4 "Flood Protection Measures" of the Flood Insurance Study report for information on flood control structures for this buriefletieties.

The projection used on the preparation of this map was Arizona State Plane Central zone (FIPSZONE 0202.) The horizontal datum was NAD 83 HARN GRS1980 spheroid. Differences in datum, spheroid, projection or State Plane zones used in the production of FIRMs for adjacent purisdictions may result in slight positional differences in map features across jurisdiction boundaries. These differences do not affect the accuracy of this FIRMs.

Flood elevations on this image are reterenced to the North American Vertical Laturu of 1988 (NAND 88). These flood elevations must be compared to structure and ground elevations referenced to the same vertical daturu. Map users wishing to obtain flood elevations referenced to the National Geodetic Vertical Daturu of 1929 (NGVD 29) may use the following Maricopa Country website application: better the control of the Country of the Country

This web tool allows users to obtain point-specific datum conversion values by zooming in and hovering over a VERTICON checkbox on the layers menu on the left side of the screen. The VERTICON gird referenced in this web application was also used to convert existing flood elevations from NGVD 29 to NAVD 88.

Gacdetic Survey bench marks shown on this map, please contact the Information Services Branch of the National Geodetic Survey at (301) 17:33-242, or visit at website at http://www.ngs.noaa.gov. To obtain information about Gacdet Densitification and Gadstartal Survey bench marks produced by the Maricop County Department of Transportation, please visit the Flood Control District of Maricopa County website at:

Maricopa County website at: http://www.fod.maricopa.gov/Maps/gismaps/apps/gdacs/application/index.cfm.

Aerial imagery was provided in digital format by the Maricopa County Department of Public Works, Flood Control Obstrict. The imagery is dated Cottoe 2009 to November 2009. Additional National Agricultural Imagery Program (NAIP) imagory was provided by the Airzona State Land Department (ALRIS) and is dated 2007. The coordinate system used for the production of the digital FIFIM is State Plane Arizona Central NADSS HARN, Infernational Feet.

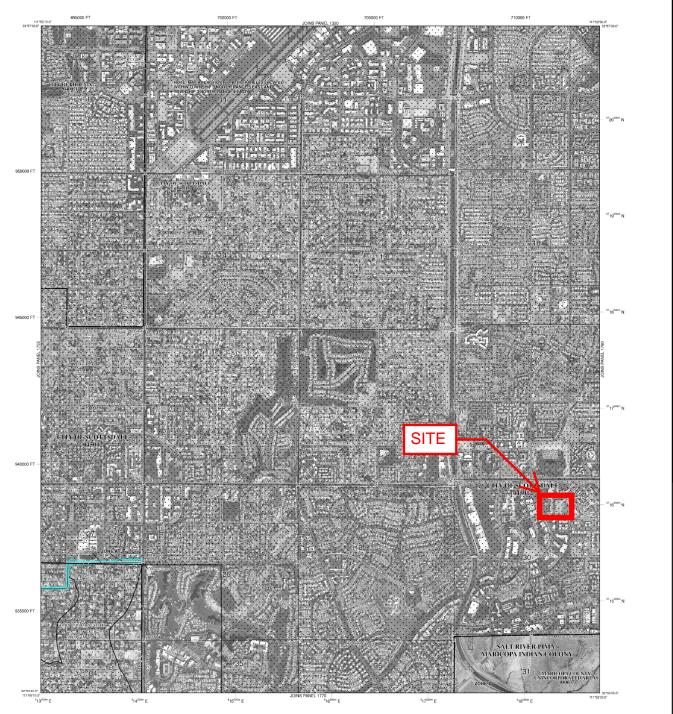
The profile base line depicted on this map represents the hydraulic modeling baselines that match flood profiles in the FIS report. As a result of improver topographic data, the profile base line, in some cases, may deviate significantly from the channel centerline or appear outside the SFHA.

Corporate limits shown on this map are based on the best data available at the time of publication. Because changes due to annexations or de-annexations may have occurred after this may eva published, map users should contact appropriate community officials to verify current corporate limit locations.

Please refer to the separately printed Map Index for an overview map of the county showing the layout of map panels; community map repository addresses; and a listing of Communities table containing National Flood Insurance Program dates for each community, as well as a listing of the panels on which each community is bestead.

For Information on available products associated with this FIFM, visit the FEMM Map Service Center (MSC) website at http://mscfema.gov. Available products may include previously issued Letters of Map Change, a Flood Insurance Study. Report of update versions of this map, Many of these products can be ordered or obtained directly from the MSC website.

To you have questions about this map, how to order products, or the National Flood insurance Program in general, please call the FEMA Map Information exchange (FMX) at 1-877-FEMA MAP (1-877-398-2627) or vieit the FEMA website at http://www.fema.gov/.





LEGEND

No Base Flood Elevations determined.

SPECIAL, FLOOD MAZARD AREAS (SFMAe) SUBBECT TO INNINDATION BY THE 1% ANNUAL CHANCE FLOOD annual chance flood (160-year flood), also innien as the base flood, is the flood a 1% chance of being equaled or exceeded in any given year. The Special search was in the are subject to flooding by the 1% annual chance flood. Areas all Flood Hazard include Zinnes A, AF, AH, AD, AH, APP, V and VE. The Base directs the water-static elevation of the 's annual chance flood.

National Flood Hazard Layer FIRMette

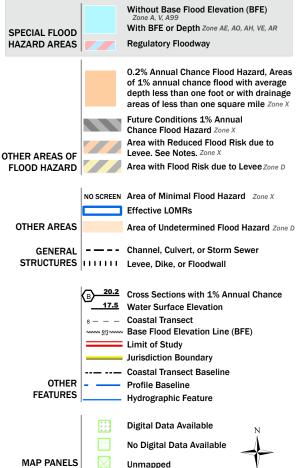


Basemap: USGS National Map: Orthoimagery: Data refreshed October, 2020



Legend

SEE FIS REPORT FOR DETAILED LEGEND AND INDEX MAP FOR FIRM PANEL LAYOUT



This map complies with FEMA's standards for the use of digital flood maps if it is not void as described below. The basemap shown complies with FEMA's basemap

accuracy standards

an authoritative property location.

The flood hazard information is derived directly from the authoritative NFHL web services provided by FEMA. This map was exported on 4/28/2021 at 12:52 PM and does not reflect changes or amendments subsequent to this date and time. The NFHL and effective information may change or become superseded by new data over time.

This map image is void if the one or more of the following map elements do not appear: basemap imagery, flood zone labels, legend, scale bar, map creation date, community identifiers, FIRM panel number, and FIRM effective date. Map images for unmapped and unmodernized areas cannot be used for regulatory purposes.

The pin displayed on the map is an approximate point selected by the user and does not represent



APPENDIX I RAINFALL DATA



NOAA Atlas 14, Volume 1, Version 5 Location name: Scottsdale, Arizona, USA* Latitude: 33.5798°, Longitude: -111.8816° Elevation: 1370.67 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

D				Avera	ge recurren	ce interval (y	/ears)			
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	2.26 (1.87-2.77)	2.94 (2.46-3.61)	3.98 (3.29-4.87)	4.78 (3.94-5.83)	5.86 (4.74-7.13)	6.68 (5.35-8.08)	7.54 (5.93-9.08)	8.40 (6.49-10.1)	9.56 (7.20-11.5)	10.4 (7.70-12.6)
10-min	1.72 (1.43-2.11)	2.24 (1.87-2.75)	3.03 (2.51-3.71)	3.64 (2.99-4.44)	4.46 (3.61-5.42)	5.09 (4.07-6.14)	5.74 (4.51-6.92)	6.39 (4.94-7.69)	7.28 (5.48-8.76)	7.95 (5.87-9.58)
15-min	1.42 (1.18-1.74)	1.85 (1.55-2.28)	2.50 (2.07-3.06)	3.00 (2.47-3.67)	3.68 (2.98-4.48)	4.20 (3.36-5.08)	4.74 (3.73-5.72)	5.28 (4.08-6.36)	6.01 (4.53-7.24)	6.57 (4.85-7.92)
30-min	0.954 (0.792-1.17)	1.25 (1.04-1.53)	1.69 (1.39-2.06)	2.02 (1.67-2.47)	2.48 (2.01-3.02)	2.83 (2.27-3.42)	3.19 (2.51-3.85)	3.56 (2.75-4.28)	4.05 (3.05-4.87)	4.42 (3.26-5.33)
60-min	0.591 (0.491-0.725)	0.771 (0.645-0.948)	1.04 (0.863-1.28)	1.25 (1.03-1.53)	1.53 (1.24-1.87)	1.75 (1.40-2.12)	1.98 (1.55-2.38)	2.20 (1.70-2.65)	2.51 (1.89-3.02)	2.74 (2.02-3.30)
2-hr	0.346 (0.292-0.415)	0.448 (0.378-0.538)	0.596 (0.501-0.714)	0.710 (0.590-0.850)	0.866 (0.714-1.03)	0.984 (0.800-1.17)	1.11 (0.884-1.31)	1.23 (0.966-1.46)	1.40 (1.07-1.65)	1.53 (1.15-1.81)
3-hr	0.256 (0.215-0.313)	0.328 (0.277-0.404)	0.429 (0.360-0.524)	0.509 (0.423-0.618)	0.621 (0.508-0.750)	0.710 (0.573-0.853)	0.803 (0.636-0.964)	0.900 (0.701-1.08)	1.03 (0.781-1.24)	1.14 (0.842-1.37
6-hr	0.154 (0.132-0.184)	0.195 (0.168-0.232)	0.249 (0.213-0.295)	0.293 (0.247-0.345)	0.351 (0.293-0.412)	0.397 (0.326-0.465)	0.445 (0.360-0.519)	0.494 (0.393-0.578)	0.561 (0.434-0.655)	0.613 (0.464-0.71)
12-hr	0.085 (0.074-0.100)	0.107 (0.093-0.126)	0.136 (0.117-0.159)	0.158 (0.135-0.184)	0.188 (0.159-0.219)	0.210 (0.176-0.245)	0.234 (0.193-0.272)	0.258 (0.210-0.299)	0.290 (0.230-0.338)	0.315 (0.245-0.37)
24-hr	0.050 (0.044-0.057)	0.063 (0.056-0.073)	0.082 (0.072-0.094)	0.096 (0.085-0.111)	0.117 (0.102-0.134)	0.133 (0.115-0.152)	0.149 (0.128-0.171)	0.167 (0.142-0.190)	0.191 (0.160-0.218)	0.209 (0.173-0.24)
2-day	0.027 (0.024-0.031)	0.034 (0.030-0.039)	0.045 (0.039-0.051)	0.053 (0.047-0.061)	0.065 (0.056-0.074)	0.074 (0.064-0.085)	0.084 (0.072-0.096)	0.094 (0.080-0.108)	0.109 (0.091-0.125)	0.120 (0.099-0.13
3-day	0.019 (0.017-0.022)	0.025 (0.022-0.028)	0.032 (0.028-0.037)	0.038 (0.034-0.044)	0.047 (0.041-0.054)	0.054 (0.047-0.062)	0.062 (0.053-0.070)	0.069 (0.059-0.079)	0.080 (0.067-0.092)	0.089 (0.074-0.102
4-day	0.015 (0.014-0.018)	0.020 (0.017-0.022)	0.026 (0.023-0.030)	0.031 (0.027-0.035)	0.038 (0.033-0.043)	0.044 (0.038-0.050)	0.050 (0.043-0.057)	0.057 (0.048-0.065)	0.066 (0.056-0.075)	0.074 (0.062-0.084
7-day	0.010 (0.009-0.011)	0.013 (0.011-0.014)	0.017 (0.015-0.019)	0.020 (0.017-0.023)	0.025 (0.021-0.028)	0.028 (0.024-0.032)	0.032 (0.028-0.037)	0.037 (0.031-0.042)	0.043 (0.036-0.049)	0.047 (0.039-0.054
10-day	0.007 (0.007-0.009)	0.010 (0.008-0.011)	0.013 (0.011-0.014)	0.015 (0.013-0.017)	0.019 (0.016-0.021)	0.021 (0.018-0.024)	0.024 (0.021-0.027)	0.027 (0.023-0.031)	0.032 (0.027-0.036)	0.035 (0.029-0.040
20-day	0.005 (0.004-0.005)	0.006 (0.005-0.007)	0.008 (0.007-0.009)	0.009 (0.008-0.010)	0.011 (0.010-0.013)	0.013 (0.011-0.014)	0.014 (0.012-0.016)	0.016 (0.014-0.018)	0.018 (0.015-0.020)	0.019 (0.016-0.02)
30-day	0.004 (0.003-0.004)	0.005 (0.004-0.005)	0.006 (0.005-0.007)	0.007 (0.006-0.008)	0.009 (0.008-0.010)	0.010 (0.009-0.011)	0.011 (0.010-0.012)	0.012 (0.011-0.014)	0.014 (0.012-0.016)	0.015 (0.013-0.01
45-day	0.003 (0.002-0.003)	0.004 (0.003-0.004)	0.005 (0.004-0.005)	0.006 (0.005-0.006)	0.007 (0.006-0.008)	0.008 (0.007-0.008)	0.008 (0.007-0.009)	0.009 (0.008-0.010)	0.010 (0.009-0.012)	0.011 (0.010-0.01
60-day	0.002	0.003	0.004	0.005	0.005 (0.005-0.006)	0.006	0.007	0.007	0.008	0.009

¹ Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

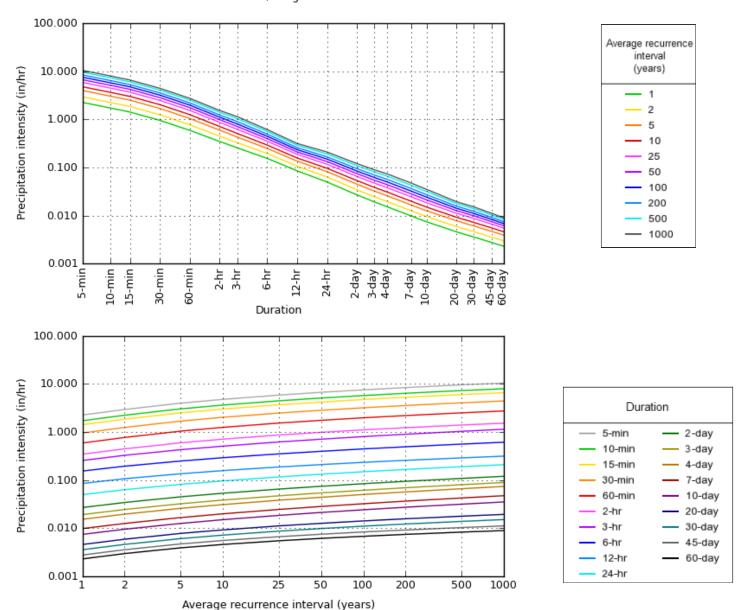
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top

PF graphical

PDS-based intensity-duration-frequency (IDF) curves Latitude: 33.5798°, Longitude: -111.8816°



NOAA Atlas 14, Volume 1, Version 5

Created (GMT): Tue Apr 27 19:35:19 2021

Back to Top

Maps & aerials

Small scale terrain



NOAA Atlas 14, Volume 1, Version 5 Location name: Scottsdale, Arizona, USA* Latitude: 33.5798°, Longitude: -111.8816° Elevation: 1370.67 ft**

* source: ESRI Maps ** source: USGS



POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF tabular | PF graphical | Maps & aerials

PF tabular

	S-based p	onit preci	pitation		ge recurrenc			ce interva	15 (111 111011	(3)
Duration	1	2	5	10	25	50	100	200	500	1000
5-min	0.188 (0.156-0.231)	0.245 (0.205-0.301)	0.332 (0.274-0.406)	0.398	0.488 (0.395-0.594)	0.557 (0.446-0.673)	0.628 (0.494-0.757)	0.700 (0.541-0.842)	0.797 (0.600-0.959)	0.870 (0.642-1.05)
10-min	0.286 (0.238-0.351)	0.373 (0.312-0.459)	0.505 (0.418-0.618)	0.606 (0.499-0.740)	0.743 (0.602-0.903)	0.848 (0.679-1.02)	0.956 (0.752-1.15)	1.07 (0.823-1.28)	1.21 (0.913-1.46)	1.33 (0.978-1.60
15-min	0.355 (0.295-0.435)	0.463 (0.387-0.569)	0.626 (0.518-0.766)	0.751 (0.618-0.917)	0.921 (0.746-1.12)	1.05 (0.841-1.27)	1.19 (0.932-1.43)	1.32 (1.02-1.59)	1.50 (1.13-1.81)	1.64 (1.21-1.98)
30-min	0.477 (0.396-0.586)	0.623 (0.521-0.766)	0.843 (0.697-1.03)	1.01 (0.833-1.23)	1.24 (1.00-1.51)	1.42 (1.13-1.71)	1.60 (1.25-1.92)	1.78 (1.37-2.14)	2.03 (1.52-2.44)	2.21 (1.63-2.67)
60-min	0.591 (0.491-0.725)	0.771 (0.645-0.948)	1.04 (0.863-1.28)	1.25 (1.03-1.53)	1.53 (1.24-1.87)	1.75 (1.40-2.12)	1.98 (1.55-2.38)	2.20 (1.70-2.65)	2.51 (1.89-3.02)	2.74 (2.02-3.30)
2-hr	0.693 (0.583-0.830)	0.895 (0.756-1.08)	1.19 (1.00-1.43)	1.42 (1.18-1.70)	1.73 (1.43-2.06)	1.97 (1.60-2.34)	2.22 (1.77-2.62)	2.46 (1.93-2.91)	2.80 (2.14-3.31)	3.05 (2.29-3.63)
3-hr	0.769 (0.647-0.941)	0.985 (0.831-1.21)	1.29 (1.08-1.58)	1.53 (1.27-1.86)	1.87 (1.53-2.25)	2.13 (1.72-2.56)	2.41 (1.91-2.90)	2.70 (2.11-3.24)	3.10 (2.35-3.72)	3.43 (2.53-4.11)
6-hr	0.925 (0.793-1.10)	1.17 (1.00-1.39)	1.49 (1.27-1.77)	1.75 (1.48-2.06)	2.10 (1.76-2.47)	2.38 (1.95-2.78)	2.67 (2.16-3.11)	2.96 (2.35-3.46)	3.36 (2.60-3.92)	3.67 (2.78-4.30)
12-hr	1.03 (0.887-1.21)	1.29 (1.12-1.52)	1.63 (1.41-1.91)	1.90 (1.62-2.22)	2.26 (1.91-2.63)	2.54 (2.12-2.95)	2.82 (2.32-3.27)	3.11 (2.53-3.61)	3.49 (2.77-4.08)	3.80 (2.95-4.45)
24-hr	1.20 (1.06-1.38)	1.52 (1.34-1.75)	1.96 (1.73-2.26)	2.31 (2.03-2.65)	2.80 (2.44-3.21)	3.19 (2.75-3.64)	3.59 (3.08-4.10)	4.00 (3.40-4.57)	4.57 (3.83-5.23)	5.03 (4.16-5.77)
2-day	1.29 (1.14-1.48)	1.65 (1.45-1.89)	2.16 (1.89-2.47)	2.56 (2.24-2.93)	3.13 (2.71-3.57)	3.57 (3.08-4.08)	4.05 (3.45-4.63)	4.54 (3.84-5.19)	5.22 (4.36-5.99)	5.76 (4.76-6.63)
3-day	1.38 (1.22-1.58)	1.77 (1.55-2.02)	2.32 (2.04-2.65)	2.77 (2.42-3.16)	3.40 (2.96-3.87)	3.90 (3.37-4.44)	4.44 (3.80-5.05)	5.00 (4.25-5.71)	5.79 (4.86-6.61)	6.43 (5.33-7.36)
4-day	1.47 (1.30-1.68)	1.88 (1.66-2.15)	2.49 (2.19-2.83)	2.98 (2.61-3.39)	3.67 (3.20-4.17)	4.23 (3.66-4.80)	4.83 (4.15-5.48)	5.46 (4.66-6.22)	6.36 (5.35-7.23)	7.09 (5.91-8.08)
7-day	1.65 (1.45-1.90)	2.11 (1.85-2.42)	2.80 (2.45-3.20)	3.35 (2.92-3.83)	4.13 (3.58-4.72)	4.76 (4.11-5.43)	5.44 (4.65-6.20)	6.15 (5.22-7.02)	7.16 (6.00-8.18)	7.97 (6.61-9.13)
10-day	1.79 (1.57-2.04)	2.29 (2.01-2.61)	3.02 (2.65-3.44)	3.61 (3.16-4.11)	4.44 (3.86-5.04)	5.11 (4.42-5.79)	5.81 (4.99-6.59)	6.56 (5.59-7.44)	7.60 (6.40-8.63)	8.44 (7.04-9.60)
20-day	2.20 (1.95-2.51)	2.84 (2.50-3.22)	3.75 (3.30-4.25)	4.44 (3.89-5.03)	5.37 (4.69-6.07)	6.08 (5.30-6.88)	6.81 (5.90-7.72)	7.55 (6.51-8.57)	8.55 (7.31-9.72)	9.32 (7.90-10.6)
30-day	2.58 (2.27-2.93)	3.32 (2.93-3.77)	4.38 (3.86-4.96)	5.19 (4.56-5.86)	6.27 (5.48-7.08)	7.10 (6.19-8.01)	7.96 (6.90-8.97)	8.82 (7.61-9.95)	9.99 (8.56-11.3)	10.9 (9.26-12.3)
45-day	3.00 (2.65-3.39)	3.86 (3.42-4.37)	5.09 (4.51-5.75)	6.01 (5.30-6.78)	7.21 (6.34-8.13)	8.11 (7.11-9.16)	9.03 (7.87-10.2)	9.95 (8.63-11.3)	11.2 (9.61-12.7)	12.1 (10.3-13.7)
60-day	3.31 (2.95-3.74)	4.28 (3.81-4.83)	5.64 (5.00-6.35)	6.62 (5.86-7.46)	7.90 (6.98-8.89)	8.85 (7.79-9.97)	9.80 (8.59-11.1)	10.7 (9.37-12.1)	12.0 (10.4-13.5)	12.9 (11.1-14.6)

Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

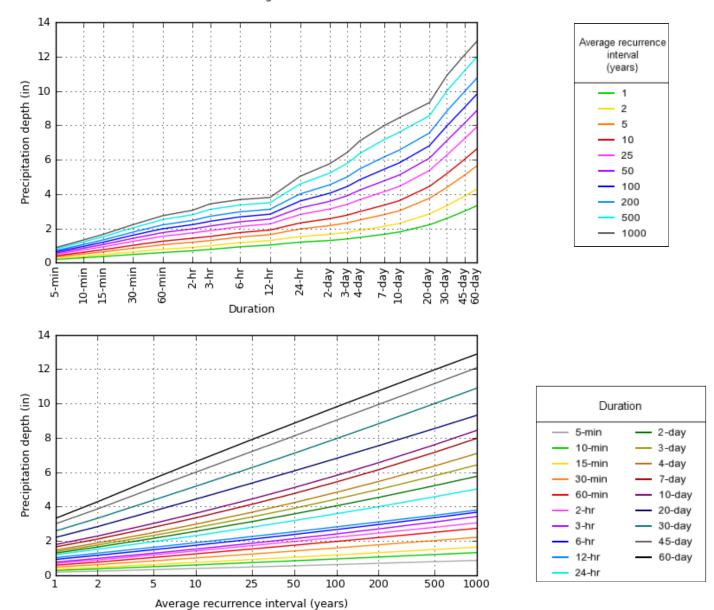
Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

Back to Top

PF graphical

PDS-based depth-duration-frequency (DDF) curves Latitude: 33.5798°, Longitude: -111.8816°



NOAA Atlas 14, Volume 1, Version 5

Created (GMT): Tue Apr 27 19:33:20 2021

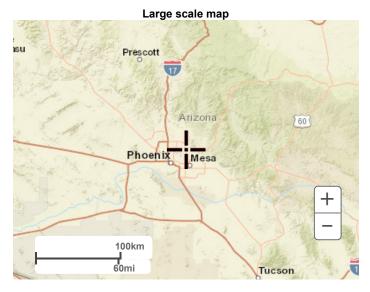
Back to Top

Maps & aerials

Small scale terrain



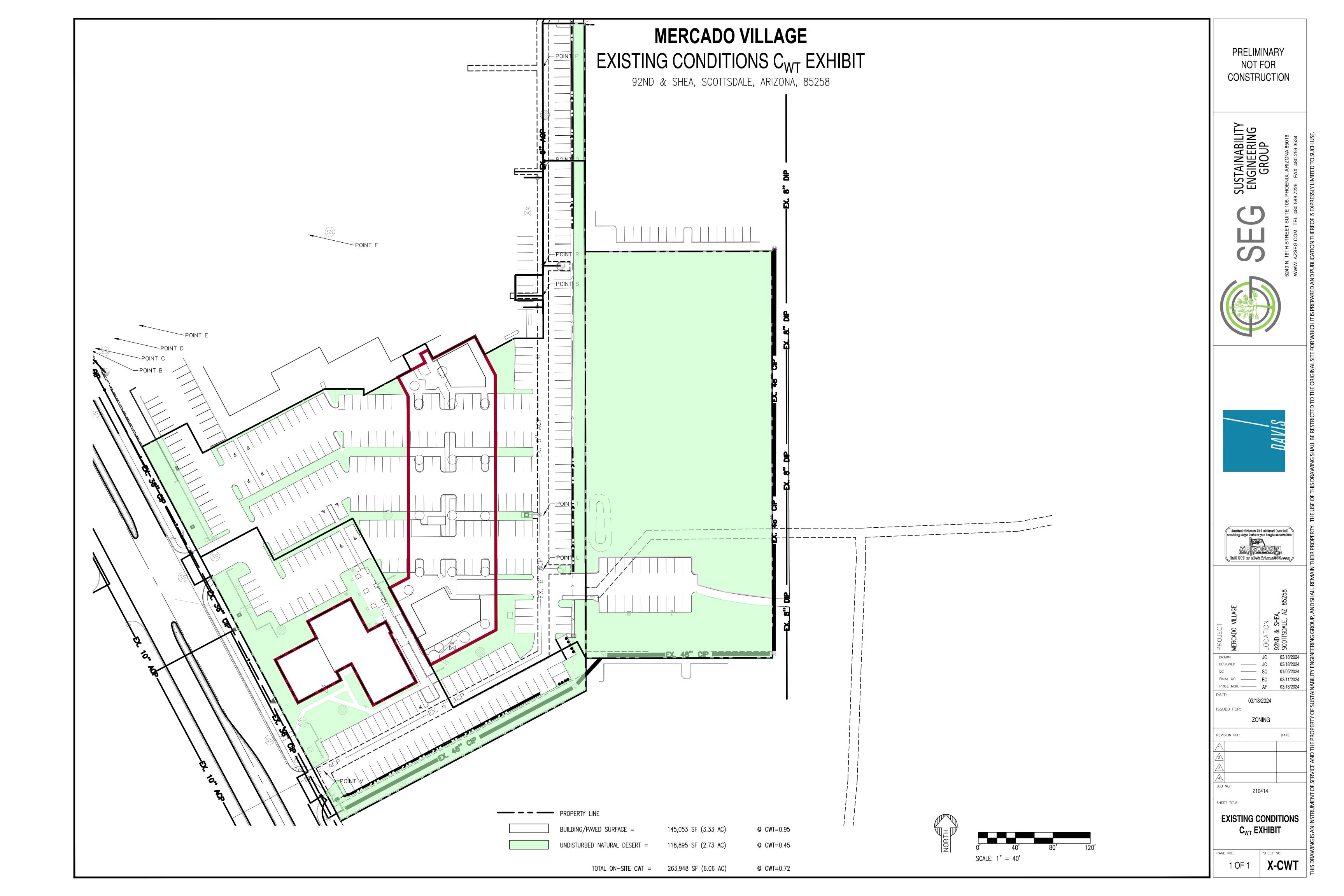


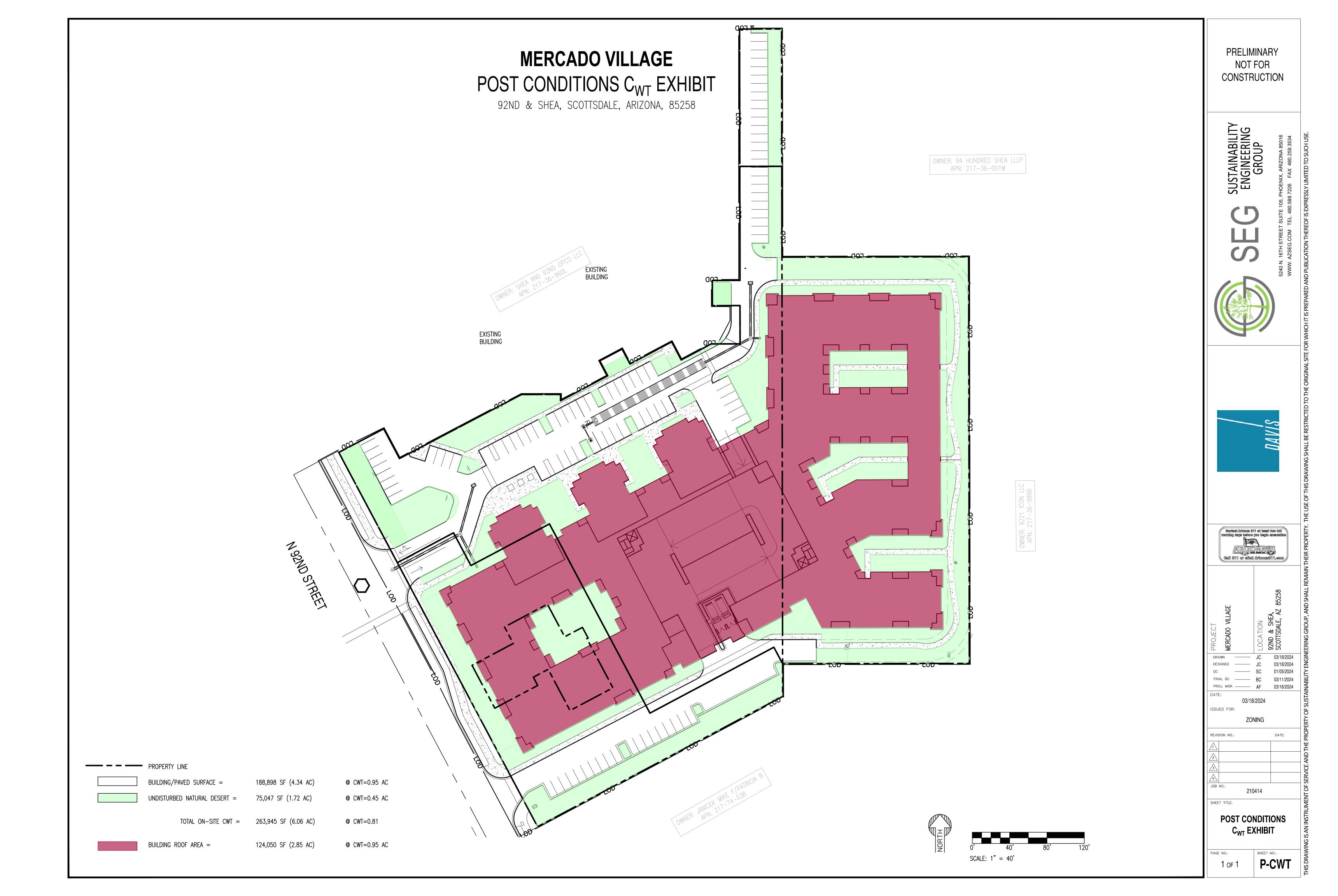


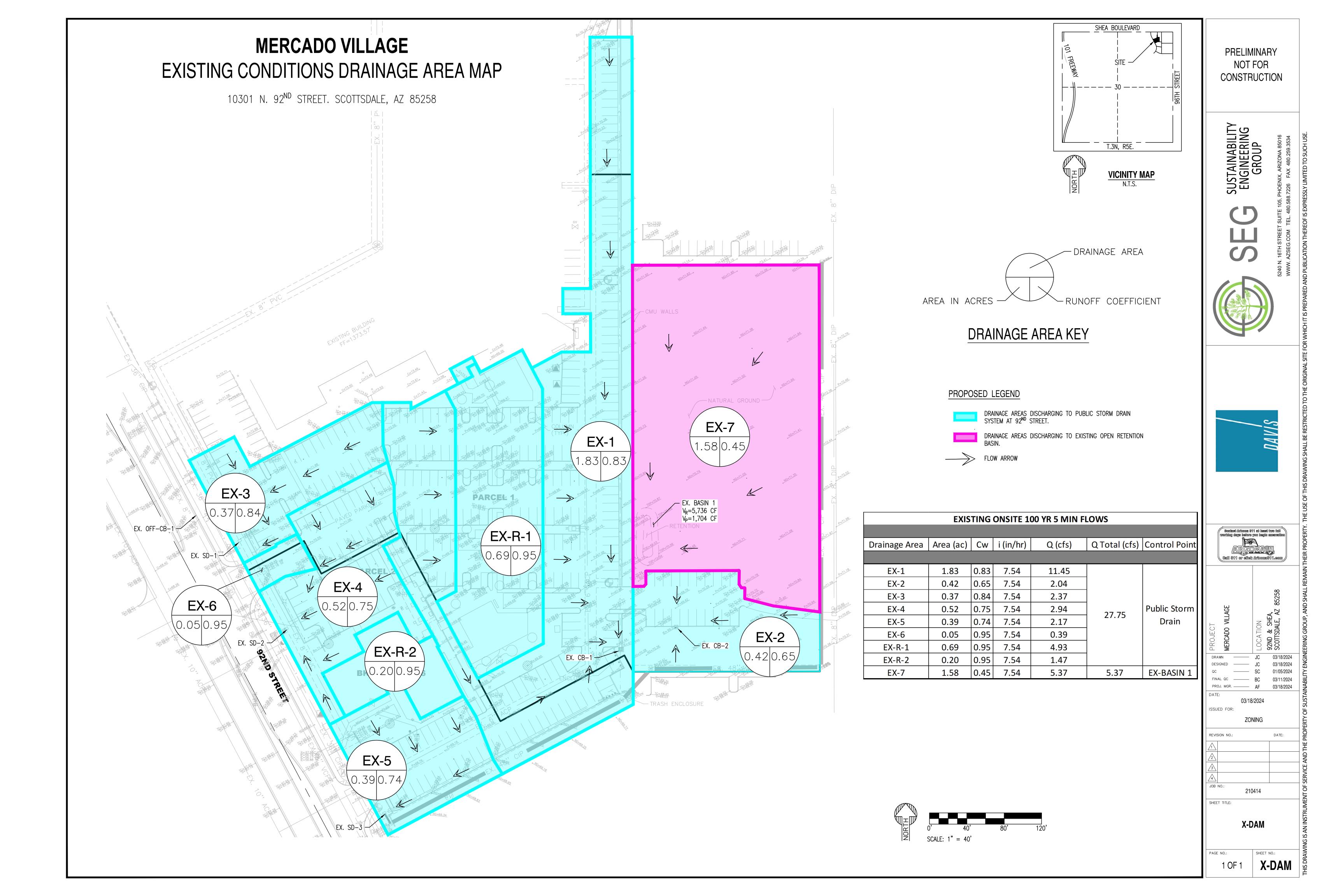
Large scale aerial

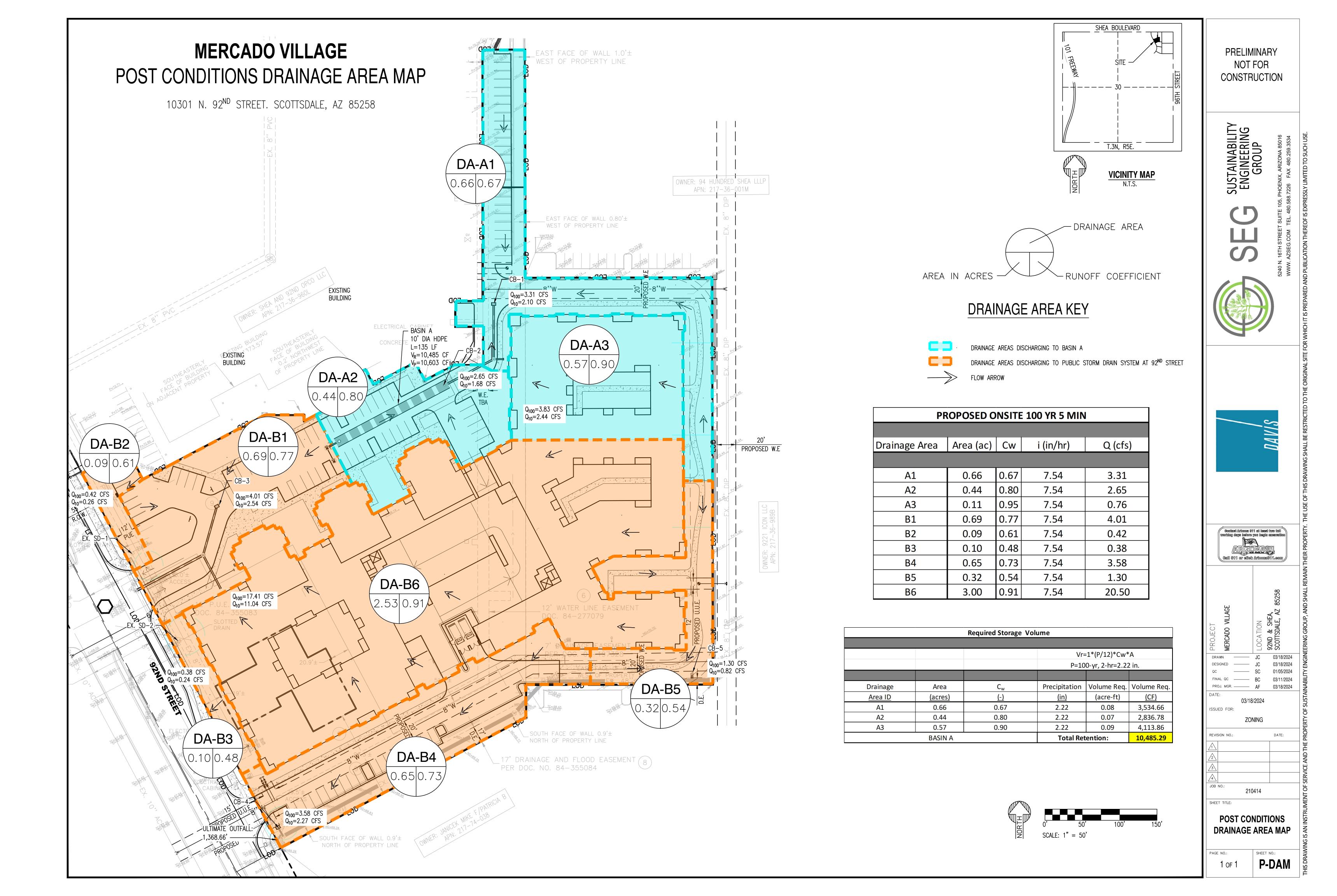


APPENDIX II CALCULATIONS









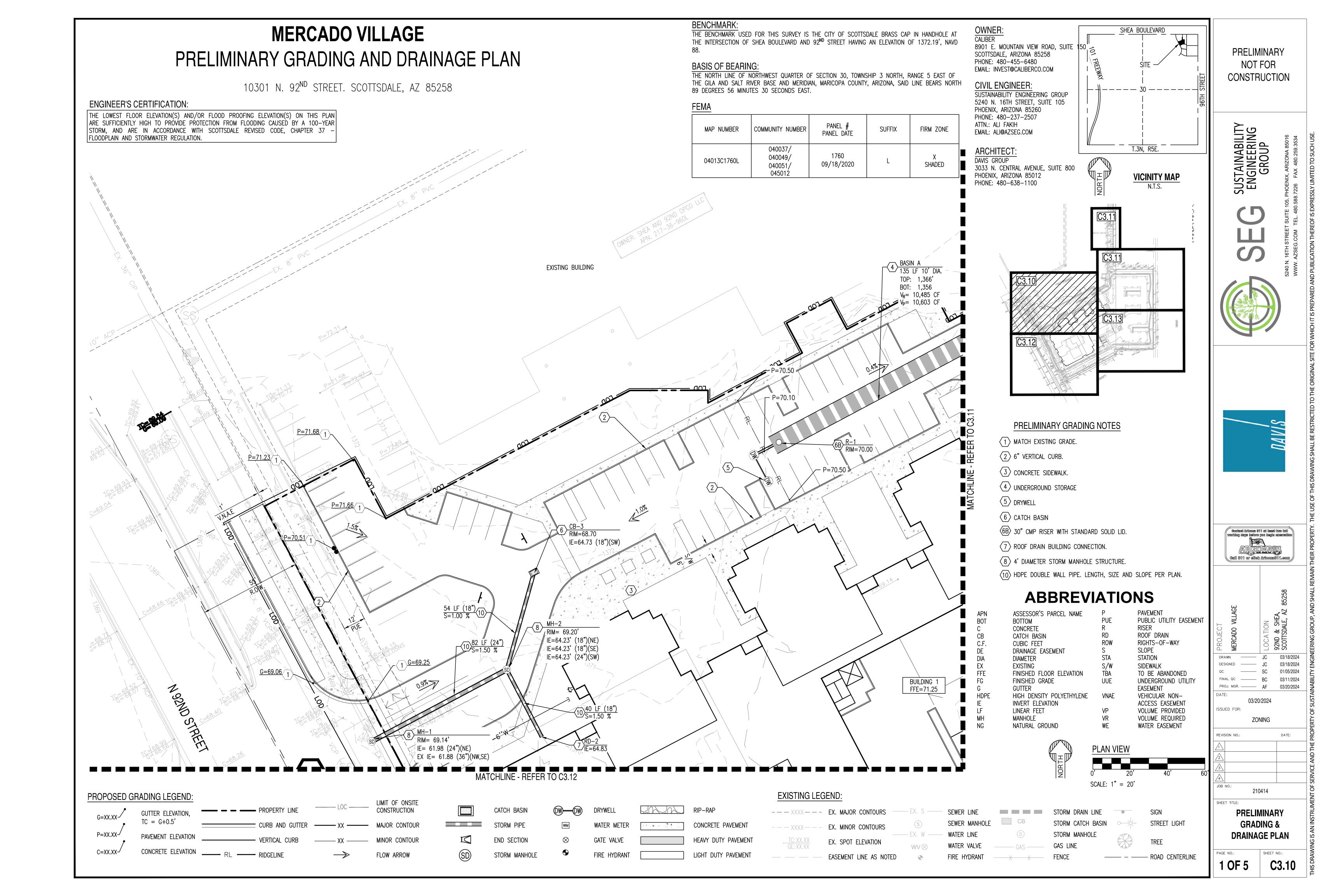


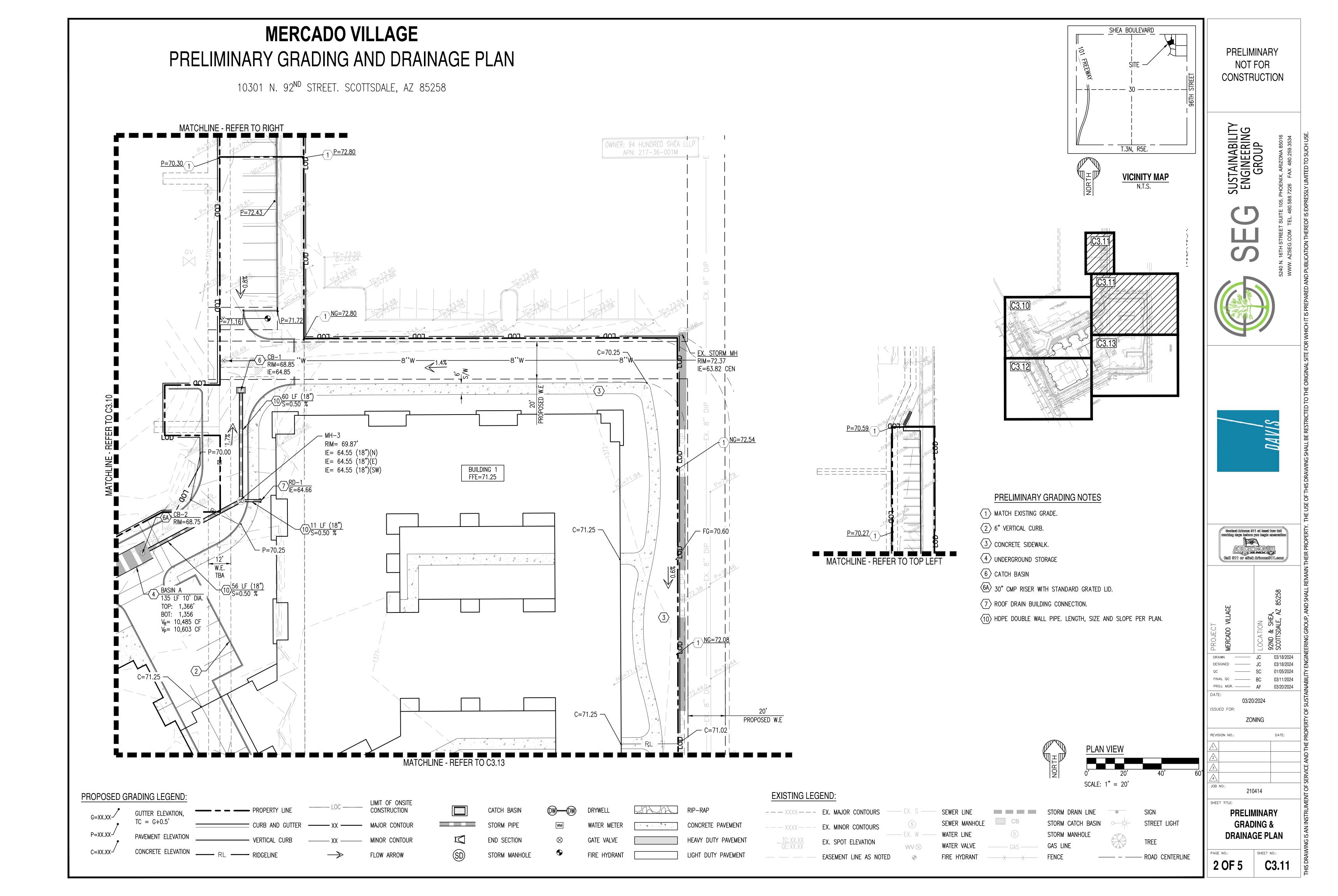
	EXIS	TING C	NSITE 10	YR 5 MIN	I FLOWS	
Drainage Area	Area (ac)	Cw	i (in/hr)	Q (cfs)	Q Total (cfs)	Control Point
EX-1	1.83	0.83	4.78	7.26		
EX-2	0.42	0.65	4.78	1.29		Public Storm
EX-3	0.37	0.84	4.78	1.50		
EX-4	0.52	0.75	4.78	1.86	17 50	
EX-5	0.39	0.74	4.78	1.37	17.59	Drain
EX-6	0.05	0.95	4.78	0.25		
EX-R-1	0.69	0.95	4.78	3.13		
EX-R-2	0.20	0.95	4.78	0.93		
EX-7	1.58	0.45	4.78	3.40	3.40	EX-BASIN 1

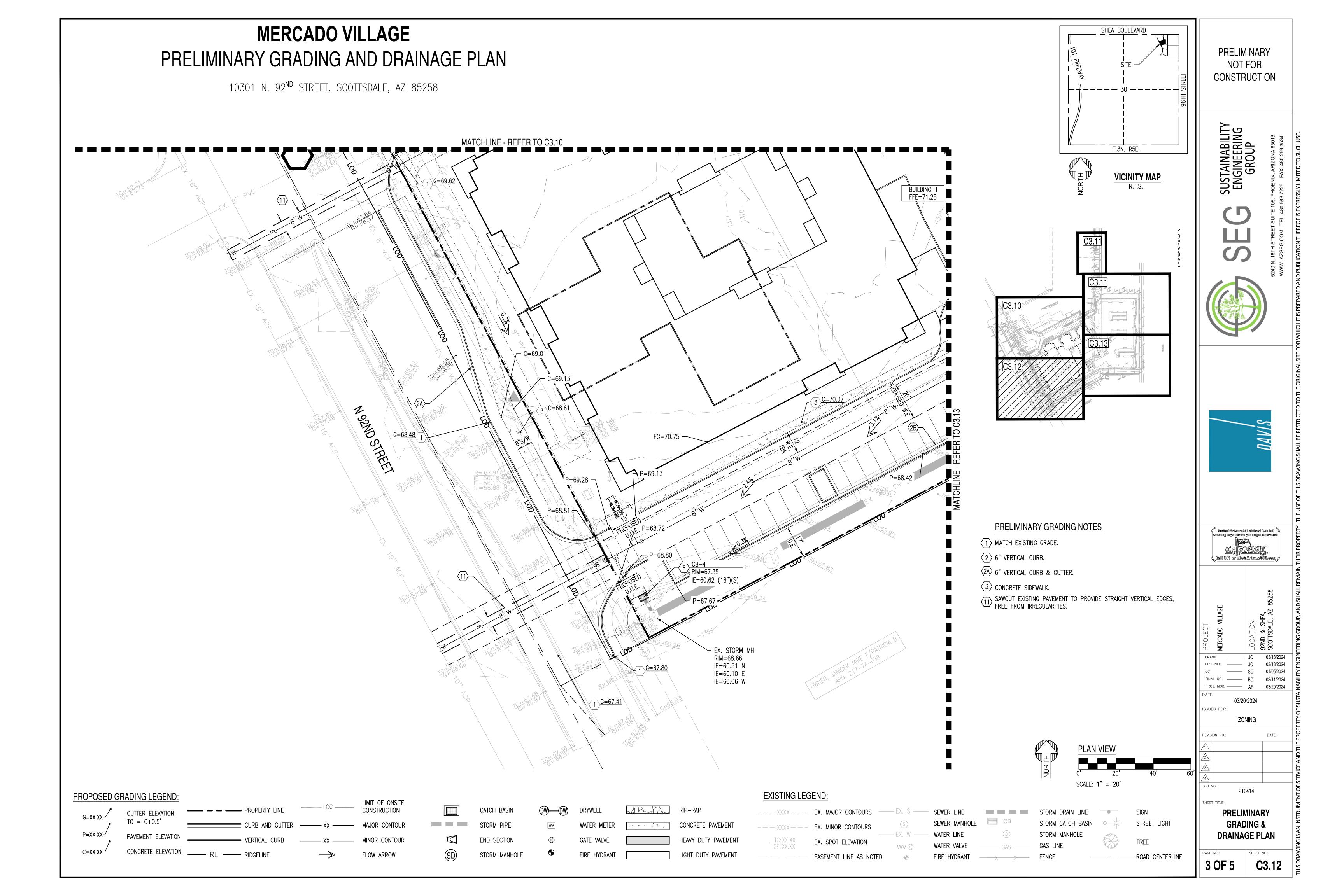
	PROPOSED ONSITE 10 YR 5 MIN FLOWS									
Drainage Area	Area (ac)	Cw	i (in/hr)	Q (cfs)	Q Total (cfs)	Control Point				
A1	0.66	0.67	4.78	2.10						
A2	0.44	0.80	4.78	1.68						
A3	0.57	0.90	4.78	2.44	6.22	BASIN A				
B1	0.69	0.77	4.78	2.54						
B2	0.09	0.61	4.78	0.26						
В3	0.10	0.48	4.78	0.24	17.18	Public Storm				
B4	0.65	0.73	4.78	2.27	17.18	Drain				
B5	0.32	0.54	4.78	0.82						
В6	2.53	0.91	4.78	11.04						



APPENDIX III Grading & Drainage Plans







MERCADO VILLAGE SHEA BOULEVARD **PRELIMINARY** PRELIMINARY GRADING AND DRAINAGE PLAN NOT FOR CONSTRUCTION 10301 N. 92ND STREET. SCOTTSDALE, AZ 85258 MATCHLINE - REFER TO C3.11 T.3N, R5E. VICINITY MAP N.T.S. - EX. BASIN 1 TOP: 1,371' BOT: 1,369 V_R= 5,736 CF V_P= 1,704 CF C=70.35 BUILDING 1 FFE=71.25 PROPOSED W.E 6 CB-5 RIM=69.95 IE= 60.85 S PRELIMINARY GRADING NOTES $\langle 1 \rangle$ MATCH EXISTING GRADE. 2 6" VERTICAL CURB. Contact Arizona 311 at least two full ②A 6" VERTICAL CURB & GUTTER. EX. STORM MH RIM=69.95 3 CONCRETE SIDEWALK. Call 811 or click Artzona311.com IE=60.91 N IE=60.75 W 6 CATCH BASIN 10 HDPE DOUBLE WALL PIPE. LENGTH, SIZE AND SLOPE PER PLAN. SAWCUT EXISTING PAVEMENT TO PROVIDE STRAIGHT VERTICAL EDGES, FREE FROM IRREGULARITIES. EX. STORM MH RIM=70.41 (12) TRASH ENCLOSURE IE=61.42 E IE=61.56 SW EX. STORM MH RIM=69.83 IE=62.60 N IE=61.27 CEN ISSUED FOR: ZONING REVISION NO.: PLAN VIEW SCALE: 1" = 20'210414 **EXISTING LEGEND:** PROPOSED GRADING LEGEND: LIMIT OF ONSITE CONSTRUCTION --- XXXX--- EX. MAJOR CONTOURS SEWER LINE **PRELIMINARY GUTTER ELEVATION** G=XX.XX-/ TC = G+0.5'STORM CATCH BASIN STREET LIGHT **GRADING &** STORM PIPE MAJOR CONTOUR CONCRETE PAVEMENT EX. MINOR CONTOURS **DRAINAGE PLAN** WATER LINE STORM MANHOLE P=XX.XX~ PAVEMENT ELEVATION END SECTION MINOR CONTOUR HEAVY DUTY PAVEMENT EX. SPOT ELEVATION WATER VALVE

LIGHT DUTY PAVEMENT

EASEMENT LINE AS NOTED

STORM MANHOLE

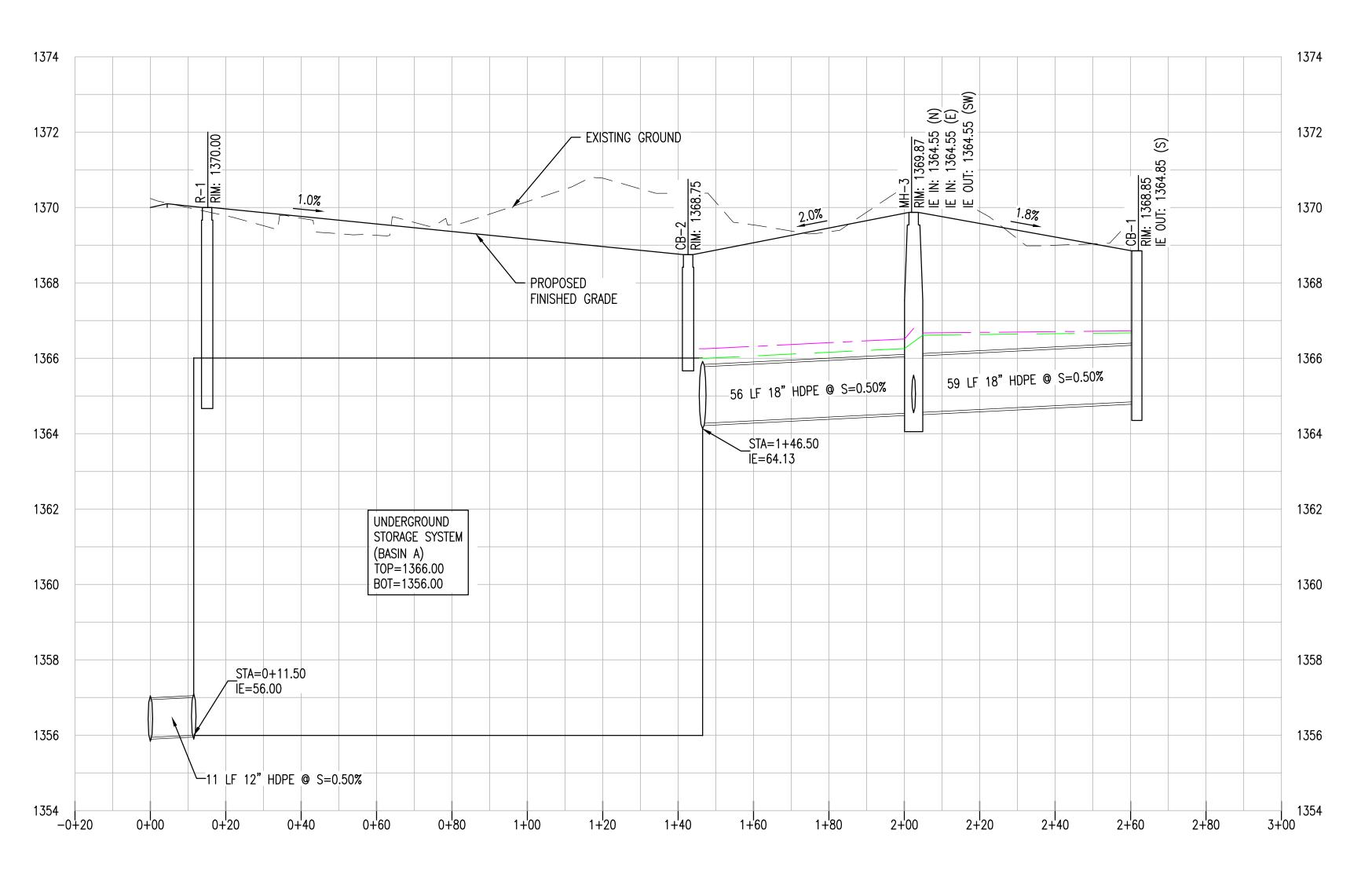
FIRE HYDRANT

CONCRETE ELEVATION

C=XX.XX~

4 OF 5 C3.13

----- ROAD CENTERLINE



PRELIMINARY
NOT FOR
CONSTRUCTION

USTAINABILITY ENGINEERING GROUP

SEG





ENERGY GRADE LINE

HYDRAULIC GRADE LINE

DRAWN — JC 03/18/2024
DESIGNED — JC 03/18/2024
QC — SC 01/05/2024
FINAL QC — BC 03/11/2024
PROJ. MGR. — AF 03/20/2024

DATE:

03/20/2024

ISSUED FOR:

ED FOR:

ZONING

REVISION NO.: DATE:

1
2
3
JOB NO.:
210414

PRELIMINARY GRADING & DRAINAGE CROSS SECTIONS

5 OF 5 C3.20

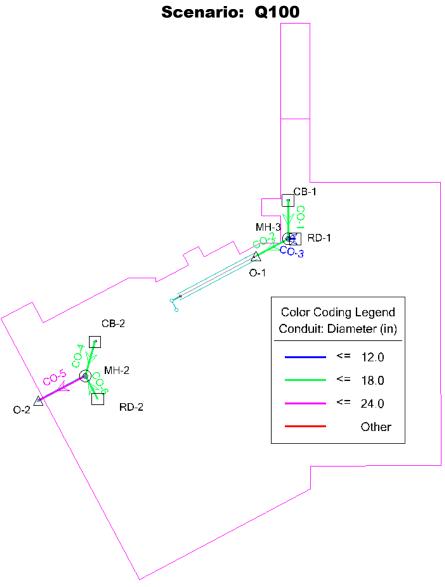
CB-1 TO BASIN A

HORIZONTAL SCALE: 1" = 20'

VERTICAL SCALE: 1" = 2



APPENDIX IV StormCAD Results



StormCAD [10.04.00.158] Page 1 of 1

Bentley Systems, Inc. Haestad Methods Solution Center 76 Watertown Road, Suite 2D Thomaston, CT 06787 USA +1-203-755-1666

FlexTable: Conduit Table

Label	Start Node	Invert (Start)	Stop Node	Invert (Stop)	Length (Scaled)	Slope (Calculated)	Section Type	Diameter (in)	Manning's n	Flow (cfs)	Velocity (ft/s)	Depth (Out)	Capacity (Full Flow)	Flow / Capacity	Hydraulic Grade Line	Hydraulic Grade Line
		(ft)		(ft)	(ft)	(ft/ft)						(ft)	(cfs)	(Design) (%)	(In) (ft)	(Out) (ft)
CO-1	CB-1	1,364.85	MH-3	1,364.55	59.0	0.005	Circle	18.0	0.013	3.31	4.09	1.71	7.44	44.5	1,366.32	1,366.26
CO-2	MH-3	1,364.55	O-1	1,364.27	56.2	0.005	Circle	18.0	0.013	7.14	4.04	1.73	7.41	96.3	1,366.26	1,366.00
CO-3	RD-1	1,364.66	MH-3	1,364.55	10.7	0.010	Circle	12.0	0.013	3.83	4.88	1.71	3.57	107.1	1,366.38	1,366.26
CO-4	CB-2	1,364.02	MH-2	1,363.21	54.4	0.015	Circle	18.0	0.013	4.01	2.27	2.40	12.83	31.2	1,365.69	1,365.61
CO-5	MH-2	1,363.21	0-2	1,361.98	81.5	0.015	Circle	24.0	0.013	21.42	6.82	2.90	27.78	77.1	1,365.61	1,364.88
CO-6	RD-2	1,364.83	MH-2	1,363.21	40.1	0.040	Circle	18.0	0.013	17.41	9.85	2.40	21.11	82.5	1,366.71	1,365.61

FlexTable: Catch Basin Table

Label	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert) (ft)	Inlet Type	Capture Efficiency (Calculated) (%)	Flow (Captured) (cfs)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)
CB-1	1,368.85	1,368.85	1,364.85	Full Capture	100.0	3.31	1,366.32	1,366.32
CB-2	1,369.90	1,369.90	1,364.02	Full Capture	100.0	4.01	1,365.69	1,365.69
RD-1	1,371.50	1,371.50	1,364.66	Full Capture	100.0	3.83	1,366.38	1,366.38
RD-2	1,371.25	1,371.25	1,364.83	Full Capture	100.0	17.41	1,366.71	1,366.71

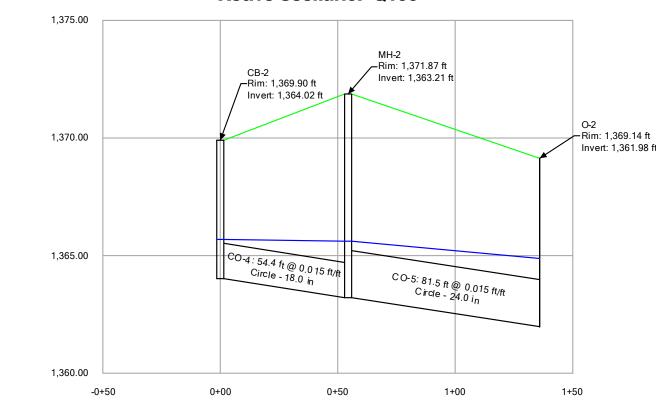
FlexTable: Manhole Table

Label	Elevation (Ground) (ft)	Elevation (Rim) (ft)	Elevation (Invert in 1) (ft)	Flow (Total Out) (cfs)	Depth (Out) (ft)	Hydraulic Grade Line (In) (ft)	Hydraulic Grade Line (Out) (ft)	Specific Energy (In) (ft)	Specific Energy (Out) (ft)
MH-2	1,371.87	1,371.87	1,363.21	21.42	2.40	1,365.61	1,365.61	3.91	3.12
MH-3	1,369.87	1,369.87	1,364.55	7.14	1.71	1,366.26	1,366.26	1.76	1.96

FlexTable: Outfall Table

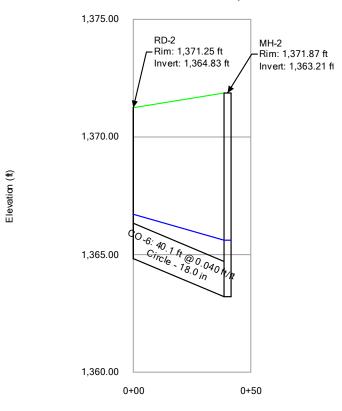
Label	Elevation (Ground) (ft)	Elevation (Invert) (ft)	Boundary Condition Type	Elevation (User Defined Tailwater) (ft)	Hydraulic Grade (ft)	Flow (Total Out) (cfs)
0-1	1,368.80	1,364.27	User Defined Tailwater	1,366.00	1,366.00	7.14
0-2	1,369.14	1,361.98	User Defined Tailwater	1,364.88	1,364.88	21.42

Profile Report Engineering Profile - CB-2 TO O-2 (Mercado Courtyard StormCAD.stsw) Active Scenario: Q100



Station (ft)

Profile Report Engineering Profile - RD-2 TO MH-2 (Mercado Courtyard StormCAD.stsw) Active Scenario: Q100

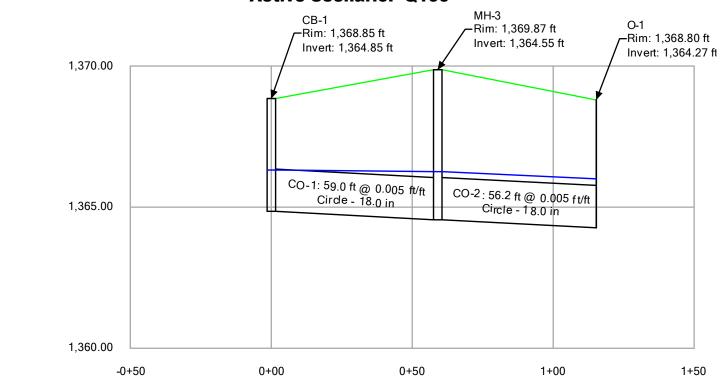


Station (ft)

Profile Report

Engineering Profile - CB-1 TO BASIN A (Mercado Courtyard StormCAD.stsw)

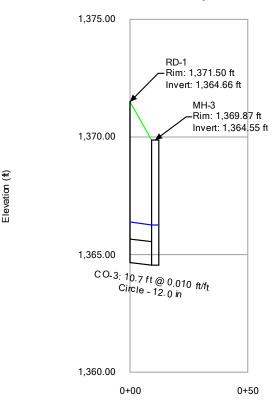
Active Scenario: Q100



Station (ft)

Elevation (ft)

Profile Report Engineering Profile - RD-1 TO MH-3 (Mercado Courtyard StormCAD.stsw) Active Scenario: Q100



Station (ft)