



CONSTRUCTION AND INSTALLATION SHALL BE IN ACCORDANCE WITH THIS PLAN AND ANY AND ALL DEVIATIONS WILL REQUIRE REAPPROVAL

# HONOR HEALTH SHEA PARKING STRUCTURE Drainage Basis of Design Report 1124070

Prepared For: Lamar Johnson Collaborative

November 8, 2024





# HONOR HEALTH SHEA PARKING STRUCTURE

# Drainage Basis of Design Report

9003 E Shea Blvd, Scottsdale, AZ

1124070

Prepared For: Lamar Johnson Collaborative Brian Dolan Lamar Johnson Collaborative 4300 E Camelback Road Phoenix, Arizona 85018

November 8, 2024

Adrian Carvajal, PE Senior Project Manager **Dibble & Associates Consulting Engineers, Inc., dba Dibble** 



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## **1.INTRODUCTION**

This report presents a preliminary drainage plan for the City of Scottsdale as a part of the Honor Health Shea Parking Garage project. The purpose of this report is to provide analysis and results for the existing and proposed drainage concept at the site. The Honor Health Shea Parking Structure site will impact approximately 2.5 acres of the approximate 14.29 acre site and is fully developed with a hospital complex and associated parking areas. The Honor Health Shea Parking Structure project includes the demolition of an existing parking lot for the construction of a five-story parking structure. This report provides the on-site drainage analysis for the project.

The project is located on the east side of 90<sup>th</sup> Street, between Shea Boulevard and Mountain View Road, in the northeast quadrant of Township 3 North, Range 5 East, Section 30. This site has an Assessor's Parcel Numbers (APNs) of 217-36-020 and 217-36-021A. See **Figure 1** for a location map.



Figure 1 – VICINITY MAP



# 2. EXISTING CONDITIONS

The site is located in a FEMA Zone 'X', defined as "areas of 0.2% annual chance flood: areas of 1% annual chance of flood with average depth less than 1 foot or areas less than 1 square mile: and areas protected by levees from 1% annual chance of flood." This hazard designation is considered minimal, and flood insurance is not federally mandated. The FEMA Flood Insurance Rate Map (FIRM) panel for this area is provided in **Appendix A**.

There is an existing drainage channel along the east side of the hospital building and campus. The parking garage site is located on the south side of campus and west of the drainage channel. The west portion of the site drains west to a landscape zone along 90<sup>th</sup> Street through turned CMU blocks in the site screen wall. Any water that overtops this landscape zone outfalls to 90<sup>th</sup> Street. The east portion of the site drains south to four drywells within the parking lot limits. Any water that overtops these drywells flows east to the existing drainage channel. The access road from the east drains to the existing storm drain system which flows east to the existing drainage channel.

## **3. DESIGN CRITERIA**

This project is designed consistent with standards set forth in the 2018 City of Scottsdale *Design Standards and Policies Manual* and the Flood Control District of Maricopa County (FCDMC) Drainage Design Manual for Maricopa County Volume I Hydrology (2018) and Volume II Hydraulics (2018) with exceptions noted herein.

Examples of specific design criteria for various design elements are provided in the following sections:

#### 3.1 Rainfall

National Oceanic and Atmospheric Administration (NOAA) Atlas 14 values are used for this project. Rainfall precipitation values obtained directly from the NOAA Atlas 14 Precipitation Data Frequency Server. NOAA Atlas 14 rainfall depths and intensities may be found in **Appendix B**.

#### 3.2 Finished Floors

Building finished floors will be placed a minimum 12-inches above emergency outfall elevations of adjacent retention facility or high-water elevation and a positive drainage flow path will be provided through the site around all buildings. The existing hospital building finish floor elevation is 1365.70. The new parking structure finish floor elevation is also set to 1365.70.

#### 3.3 Storm Runoff Conveyance

Storm runoff will be conveyed through the site via a combination of surface flow, drain basin inlets & storm drain pipe. Site storm drain pipes & inlets will be designed to convey the 10-year design storm. The 100-year flow rate to existing catch basins will not be increased.

#### 3.4 Surface Retention Basin

Site retention has been analyzed from both pre vs post and first flush perspectives. The proposed site reduces the impervious area compared to the existing site. Therefore, the first flush storm water volume governs the design. The site retention has been designed to retain the first flush storm event with a precipitation depth of 0.5-inches.

- The maximum side slope of retention basins will be 4:1.
- The finish floor elevation of structures must be at least 1 foot above the retention basin water surface elevation of the 100-yr, 2-hr storm event.

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- The design of all storm water storage facilities shall be such that the stored runoff shall be disposed of or evacuated completely from the facility within 36 hours.
- Retention basins greater than 1 foot of ponding depth from the 100-yr 2-hr storm event require a minimum of one drywell for storm water disposal.

## 4. STUDY APPROACH & METHODOLOGY

Based on the proposed conditions and existing ground surrounding the project site, a proposed Grading & Drainage Plan was created to illustrate drainage areas that would be affecting the site. This drainage plan is shown in **Appendix C**.

The discharge into each proposed storm drain is calculated by the following formula:

Q=C\*i\*A

where:

Q = peak discharge (cubic feet per second) C = weighted runoff coefficient i = rainfall intensity (inch/hour) A = drainage area (acre) Min Tc = 5 (min)

Required retention volume is calculated by the following formula:

$$V_R = C\left(\frac{P}{12}\right)A$$

where:

 $V_R$  = retention volume required (cubic feet) C = weighted runoff coefficient P = first flush rainfall depth (inches) A = drainage area (square feet)

Number of drywells required is calculated by the following formula:

No. of Drywells 
$$=$$
  $\frac{V_P}{rT} * \frac{1 hr}{3600 s}$ 

where:

 $V_P$  = retention volume provided (cubic feet) r = percolation rate (cubic feet per second, assumed value 0.10) T = allowable drain time (hrs, required value 36)

Drainage time is calculated by the following formula:

$$t = \left(\frac{V_{P1}}{r_1} + \frac{V_{P2}}{r_2}\right) * \frac{1}{d} * \frac{1 hr}{3600 s}$$

t = drainage time (hrs)
V<sub>P</sub> = retention volume provided (cubic feet)
r = percolation rate (cubic feet per second, assumed value 0.2)
d = number of drywells

Refer to **Appendix D** for Drainage Calculations.

# **5. PROPOSED DRAINAGE CONDITIONS**

The Honor Health Shea Parking Structure project includes a new building and associated site improvements. Refer to the Drainage Area Maps provided in **Appendix C**.

Drainage Area A includes the west portion of the parking garage roof as well as the north, south, and west side of the project site. All stormwater located within Drainage Area A is conveyed via surface drainage and storm drain piping to the proposed Retention basin A north of the parking garage. A dual chamber drywell is needed to drain this basin within 36 hours. Drainage Area A outfalls to the west into 90<sup>th</sup> Street.

A pre-vs.-post versus first flush analysis was done to determine which of the two controls. The greater of the two will be used to design the retention system.

See Table 1 below for Proposed Retention Volume Summary. Refer to **Appendix D** for drainage calculations.

Table 1 -	- Proposed	Retention	Volume	Summary
-----------	------------	-----------	--------	---------

Retention Basin ID	Drainage Area	Weighted Coefficient (First Flush)	Pre vs Post Volume Required	First Flush Volume Required	Volume Provided	Drywells	Drain Time
А	120,005 sqft	1.0	657 cf	5,000 cf	5,133 cf	1	13.9 hrs

In addition to retaining the first flush, a Q100 analysis was completed comparing the existing and proposed conditions.

In the existing condition, the catch basin at the north end of the site receives 3.8 cfs from the intersection at the main driveway along with a portion of parking lot along the north end of the project area. In the proposed condition, the north parking lot is now replaced with a retention basin. The Q100 flow from the main driveway intersection is reduced to 2 cfs while the added overflow from the retention basin is 0.3 cfs, totaling 2.3 cfs. This is a reduction of 1.5 cfs to the existing northern catch basin. Refer to **Appendix D** for peak flow calculations.

# **6. CONCLUSIONS**

New drainage improvements were analyzed in this report to verify the demands of the project. Proposed storm drain infrastructure at the Honor Health Shea Parking Structure will be able to convey storm water runoff generated by first flush storm event while maintaining standards set by the City of Scottsdale Storm Water Drainage System Design Manual and Flood Control District of Maricopa County (FCDMC) Drainage Design Manual. Applicable City of Scottsdale and Flood Control District requirements have been satisfied.

# 7. REFERENCES

Flood Control District of Maricopa County, Engineering Division, Drainage Design Manual for Maricopa County, Arizona Volume I, Hydrology. December, 2018.

Flood Control District of Maricopa County, Engineering Division, Drainage Design Manual for Maricopa County, Arizona Volume II, Hydraulics. December, 2018.

City of Scottsdale Public Works. Design Standards & Policies Manual. 2018.

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#### Appendix A - FEMA Flood Insurance Rate Map

# National Flood Hazard Layer FIRMette



#### Legend



Basemap Imagery Source: USGS National Map 2023



D

#### Appendix B – NOAH Atlas 14 Rainfall Information



NOAA Atlas 14, Volume 1, Version 5 Location name: Scottsdale, Arizona, USA\* Latitude: 33.5787°, Longitude: -111.8857° Elevation: 1364 ft\*\*

\* source: ESRI Maps \*\* source: USGS



#### POINT PRECIPITATION FREQUENCY ESTIMATES

Sanja Perica, Sarah Dietz, Sarah Heim, Lillian Hiner, Kazungu Maitaria, Deborah Martin, Sandra Pavlovic, Ishani Roy, Carl Trypaluk, Dale Unruh, Fenglin Yan, Michael Yekta, Tan Zhao, Geoffrey Bonnin, Daniel Brewer, Li-Chuan Chen, Tye Parzybok, John Yarchoan

NOAA, National Weather Service, Silver Spring, Maryland

PF\_tabular | PF\_graphical | Maps\_&\_aerials

#### **PF** tabular

PDS-based point precipitation frequency estimates with 90% confidence intervals (in inches) <sup>1</sup>											
Duration				Avera	ge recurrenc	e interval (y	/ears)				
Duration	1	2	5	10	25	50	100	200	500	1000	
5-min	<b>0.187</b>	<b>0.244</b>	<b>0.330</b>	<b>0.397</b>	<b>0.487</b>	<b>0.556</b>	<b>0.627</b>	<b>0.698</b>	<b>0.795</b>	<b>0.869</b>	
	(0.156-0.230)	(0.204-0.300)	(0.273-0.405)	(0.327-0.485)	(0.394-0.592)	(0.445-0.672)	(0.492-0.756)	(0.539-0.841)	(0.598-0.958)	(0.641-1.05)	
10-min	<b>0.285</b>	<b>0.371</b>	<b>0.503</b>	<b>0.604</b>	<b>0.741</b>	<b>0.845</b>	<b>0.954</b>	<b>1.06</b>	<b>1.21</b>	<b>1.32</b>	
	(0.237-0.350)	(0.311-0.457)	(0.416-0.616)	(0.497-0.738)	(0.599-0.901)	(0.677-1.02)	(0.749-1.15)	(0.821-1.28)	(0.911-1.46)	(0.975-1.60)	
15-min	<b>0.353</b>	<b>0.461</b>	<b>0.623</b>	<b>0.749</b>	<b>0.918</b>	<b>1.05</b>	<b>1.18</b>	<b>1.32</b>	<b>1.50</b>	<b>1.64</b>	
	(0.293-0.434)	(0.385-0.567)	(0.516-0.764)	(0.616-0.914)	(0.743-1.12)	(0.839-1.27)	(0.929-1.43)	(1.02-1.59)	(1.13-1.81)	(1.21-1.98)	
30-min	<b>0.475</b> (0.395-0.584)	<b>0.620</b> (0.519-0.763)	<b>0.840</b> (0.695-1.03)	<b>1.01</b> (0.830-1.23)	<b>1.24</b> (1.00-1.50)	<b>1.41</b> (1.13-1.71)	<b>1.59</b> (1.25-1.92)	<b>1.77</b> (1.37-2.14)	<b>2.02</b> (1.52-2.43)	<b>2.21</b> (1.63-2.66)	
60-min	<b>0.588</b> (0.489-0.723)	<b>0.768</b> (0.642-0.944)	<b>1.04</b> (0.860-1.27)	<b>1.25</b> (1.03-1.52)	<b>1.53</b> (1.24-1.86)	<b>1.75</b> (1.40-2.11)	<b>1.97</b> (1.55-2.38)	<b>2.20</b> (1.70-2.64)	<b>2.50</b> (1.88-3.01)	<b>2.73</b> (2.01-3.30)	
2-hr	<b>0.689</b> (0.580-0.826)	<b>0.890</b> (0.753-1.07)	<b>1.19</b> (0.997-1.42)	<b>1.41</b> (1.18-1.69)	<b>1.73</b> (1.42-2.05)	<b>1.96</b> (1.59-2.33)	<b>2.21</b> (1.76-2.61)	<b>2.45</b> (1.92-2.90)	<b>2.79</b> (2.14-3.30)	<b>3.04</b> (2.28-3.62)	
3-hr	<b>0.764</b>	<b>0.978</b>	<b>1.28</b>	<b>1.52</b>	<b>1.86</b>	<b>2.12</b>	<b>2.40</b>	<b>2.69</b>	<b>3.09</b>	<b>3.41</b>	
	(0.642-0.935)	(0.826-1.20)	(1.08-1.57)	(1.26-1.85)	(1.52-2.24)	(1.71-2.55)	(1.90-2.88)	(2.10-3.22)	(2.34-3.70)	(2.52-4.09)	
6-hr	<b>0.919</b>	<b>1.16</b>	<b>1.48</b>	<b>1.74</b>	<b>2.09</b>	<b>2.37</b>	<b>2.65</b>	<b>2.94</b>	<b>3.34</b>	<b>3.66</b>	
	(0.788-1.09)	(0.996-1.38)	(1.27-1.76)	(1.47-2.05)	(1.75-2.45)	(1.94-2.76)	(2.15-3.09)	(2.34-3.44)	(2.59-3.90)	(2.77-4.28)	
12-hr	<b>1.02</b>	<b>1.28</b>	<b>1.62</b>	<b>1.89</b>	<b>2.24</b>	<b>2.52</b>	<b>2.80</b>	<b>3.09</b>	<b>3.47</b>	<b>3.77</b>	
	(0.880-1.20)	(1.11-1.51)	(1.40-1.90)	(1.61-2.20)	(1.90-2.61)	(2.11-2.92)	(2.31-3.25)	(2.52-3.58)	(2.76-4.05)	(2.94-4.42)	
24-hr	<b>1.19</b>	<b>1.51</b>	<b>1.95</b>	<b>2.30</b>	<b>2.78</b>	<b>3.16</b>	<b>3.56</b>	<b>3.97</b>	<b>4.54</b>	<b>4.99</b>	
	(1.05-1.36)	(1.33-1.73)	(1.72-2.24)	(2.02-2.63)	(2.43-3.18)	(2.74-3.61)	(3.06-4.07)	(3.38-4.53)	(3.81-5.18)	(4.14-5.72)	
2-day	<b>1.28</b>	<b>1.64</b>	<b>2.14</b>	<b>2.54</b>	<b>3.10</b>	<b>3.55</b>	<b>4.02</b>	<b>4.51</b>	<b>5.19</b>	<b>5.73</b>	
	(1.13-1.47)	(1.44-1.88)	(1.88-2.45)	(2.23-2.91)	(2.70-3.54)	(3.06-4.05)	(3.44-4.59)	(3.83-5.15)	(4.35-5.94)	(4.74-6.58)	
3-day	<b>1.37</b>	<b>1.75</b>	<b>2.30</b>	<b>2.74</b>	<b>3.37</b>	<b>3.86</b>	<b>4.40</b>	<b>4.95</b>	<b>5.73</b>	<b>6.36</b>	
	(1.21-1.57)	(1.54-2.00)	(2.02-2.63)	(2.40-3.13)	(2.93-3.83)	(3.34-4.40)	(3.77-5.00)	(4.22-5.64)	(4.82-6.54)	(5.29-7.27)	
4-day	<b>1.46</b>	<b>1.86</b>	<b>2.46</b>	<b>2.94</b>	<b>3.63</b>	<b>4.18</b>	<b>4.77</b>	<b>5.40</b>	<b>6.28</b>	<b>7.00</b>	
	(1.29-1.66)	(1.64-2.13)	(2.16-2.80)	(2.58-3.34)	(3.16-4.12)	(3.62-4.74)	(4.11-5.41)	(4.60-6.13)	(5.29-7.13)	(5.84-7.97)	
7-day	<b>1.63</b>	<b>2.09</b>	<b>2.76</b>	<b>3.31</b>	<b>4.08</b>	<b>4.70</b>	<b>5.36</b>	<b>6.06</b>	<b>7.05</b>	<b>7.85</b>	
	(1.44-1.87)	(1.84-2.39)	(2.42-3.16)	(2.89-3.78)	(3.54-4.65)	(4.05-5.35)	(4.59-6.10)	(5.15-6.92)	(5.91-8.04)	(6.52-8.98)	
10-day	<b>1.77</b>	<b>2.26</b>	<b>2.98</b>	<b>3.57</b>	<b>4.38</b>	<b>5.04</b>	<b>5.73</b>	<b>6.46</b>	<b>7.49</b>	<b>8.32</b>	
	(1.56-2.02)	(1.99-2.58)	(2.62-3.40)	(3.12-4.06)	(3.82-4.97)	(4.36-5.70)	(4.93-6.50)	(5.52-7.33)	(6.31-8.50)	(6.94-9.44)	
20-day	<b>2.18</b>	<b>2.80</b>	<b>3.70</b>	<b>4.38</b>	<b>5.29</b>	<b>5.99</b>	<b>6.71</b>	<b>7.44</b>	<b>8.42</b>	<b>9.17</b>	
	(1.92-2.48)	(2.47-3.18)	(3.26-4.20)	(3.85-4.96)	(4.63-5.99)	(5.23-6.78)	(5.82-7.60)	(6.42-8.44)	(7.21-9.57)	(7.79-10.4)	
30-day	<b>2.55</b> (2.25-2.89)	<b>3.28</b> (2.90-3.72)	<b>4.32</b> (3.81-4.89)	<b>5.11</b> (4.50-5.77)	<b>6.18</b> (5.41-6.98)	<b>7.00</b> (6.10-7.89)	<b>7.84</b> (6.81-8.83)	<b>8.69</b> (7.51-9.79)	<b>9.84</b> (8.43-11.1)	<b>10.7</b> (9.12-12.1)	
45-day	<b>2.95</b> (2.62-3.34)	<b>3.81</b> (3.38-4.30)	<b>5.02</b> (4.44-5.66)	<b>5.92</b> (5.22-6.68)	<b>7.10</b> (6.24-8.00)	<b>7.98</b> (7.00-9.00)	<b>8.88</b> (7.75-10.0)	<b>9.78</b> (8.49-11.0)	<b>11.0</b> (9.45-12.4)	<b>11.9</b> (10.2-13.5)	
60-day	<b>3.27</b> (2.91-3.68)	<b>4.22</b> (3.75-4.75)	<b>5.55</b> (4.93-6.24)	<b>6.52</b> (5.78-7.34)	<b>7.78</b> (6.87-8.74)	<b>8.71</b> (7.67-9.80)	<b>9.64</b> (8.46-10.9)	<b>10.6</b> (9.22-11.9)	<b>11.8</b> (10.2-13.3)	<b>12.6</b> (10.9-14.3)	

<sup>1</sup> Precipitation frequency (PF) estimates in this table are based on frequency analysis of partial duration series (PDS).

Numbers in parenthesis are PF estimates at lower and upper bounds of the 90% confidence interval. The probability that precipitation frequency estimates (for a given duration and average recurrence interval) will be greater than the upper bound (or less than the lower bound) is 5%. Estimates at upper bounds are not checked against probable maximum precipitation (PMP) estimates and may be higher than currently valid PMP values.

Please refer to NOAA Atlas 14 document for more information.

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12 10 Precipitation depth (in) 8 6 4 2 0 60-min 10-min 15-min 30-min 0-pr Duration 7-day 10-day 45-day 60-day 2-hr 3-hr 24-hr 2-day 3-day 4-day 20-day 30-day 5-min 12 10 Precipitation depth (in) 8 6 4 2 0 1 2 5 10 25 50 100 200 500 1000 Average recurrence interval (years)





Created (GMT): Tue Aug 27 16:13:55 2024

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Maps & aerials

Small scale terrain







Large scale terrain





Large scale aerial



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US Department of Commerce National Oceanic and Atmospheric Administration National Weather Service National Water Center 1325 East West Highway Silver Spring, MD 20910 Questions?: <u>HDSC.Questions@noaa.gov</u>

**Disclaimer** 



#### Appendix C – Drainage Area Maps



D

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С

/2024 11:25:35 AM FILE:J:\2024/1124070 HH Shea Parking Structure\CAD\24070 PRE G&D MAP.dwg DATE:11/8/2024 TIME:4:02 PM (by:zachary.)

# <u>LEGEND</u>



DESERT LANDSCAPING C VALUE = 0.45 DESERT LANDSCAPING AREA = 9,579 SF PAVEMENT BUILDING C VALUE = 0.95 PAVEMENT & BUILDING = 101,154 SF

Cw=(C1\*A1+C2\*A2)/(A1+A2) Cw=0.91



В

0'	10'	20'	40'
	SCAL	E: 1"=2	20'
wo	Contact Arizo rking days be	ona 811 at least the fore you begin ex ZONA8	wo full cavation

Job # 008229





D

С

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F

Е



80 QL

NEW ASPHALT PAVEMENT

NEW LANDSCAPE

<u>LEGEND</u>

NEW RIPRAP

NEW SIDEWALK

NEW CONCRETE PAVEMENT

 $\bigtriangledown$ 

NEW BUILDING

DESERT LANDSCAPING C VALUE = 0.45DESERT LANDSCAPING AREA = 3,243 SF PAVEMENT BUILDING C VALUE = 0.95 PAVEMENT & BUILDING = 116,762 SF

Cw=(C1\*A1+C2\*A2)/(A1+A2) Cw=0.94



В

0' 10' 20' 40 SCALE: 1"=20' Contact Arizona 811 at least two ful prking days before you begin excavat AR ZONA81 811 or click Arizona8

DRAWING NO.

Job # 008229

PR01.0

5	Collaporative Phoenix, AZ 85018 Phoenix, AZ 8501
4	<text><text><text><text></text></text></text></text>
3	RHEALTH SHEA GARAGE d. Scottsdale, AZ 85260 <i>iew</i>
2	Image: Second Stress of the second stress
1	DRAWING TITLE PROPOSED DRAINAGE MAP



#### Appendix D – Drainage Calculations

# **Dibble** Engineering

#### HH Shea Parking Garage DIBBLE PROJECT NO. 1124070 ON-SITE DRAINAGE CALCULATIONS

DES: ZDL DATE: 2024-1108

HYDROLOGY	CALCULATIC	NS								
DRAINAGE	TOTAL	DESERT	PAVEMENT &	WEIGHTED	*RAINFALL	VOLUME				
AREA	AREA	LANDSCAPING	BUILDING	COEFFICIENT	DEPTH	REQUIRED				
	[SF]	[SF]	[SF]		[IN]	[CF]				
		0.45	0.95							
PRE CONSTRUCTION 100-YEAR, 2-HOUR										
А	120,005	9,579	101,154	0.91	2.21	20,040				
					TOTAL	20,040				
POST CONST	RUCTION 10	D-YEAR, 2-HOUR								
А	120,005	3,243	116,762	0.94	2.21	20,697				
					TOTAL	20,697				
				PR	E VS POST	657				
FIRST FLUSH										
DRAINAGE	TOTAL			RUNOFF	RAINFALL	VOLUME				
AREA	AREA			COEFFICIENT	DEPTH	REQUIRED				
	[SF]				[IN]	[CF]				
Α	120,005			1.00	0.50	5,000				
First flush is greater than Pre vs Post. First flush value is used. * NOAA Atlas 14 Rainfall depth obtained from www.nws.noaa.gov										

ON-SITE RET	ENTION BASIN	VOLUME CALC	JULATIONS				
BASIN			INCREMENTAL	CUMULATIVE			
ELEV	AREA	DEPTH	VOLUME	VOLUME	DRYWELLS	**DRAIN TIME	
[FT]	[SF]	[FT]	[CF]	[CF]	[EA]	[HR]	
Basin B			_				
1,363.5	3,243	2.0	2,283	3,120			
1,362.5	1,323	1.0	837	837			
1,361.5	351	N/A	N/A	N/A			
UNDERGROU	JND RETENTIO	N VOLUME CA	LCULATIONS				
DRAINAGE	PIPE	VOLUME	PIPE			TOTAL	
AREA	DIAMETER	PER FT	LENGTH			VOLUME	
	[FT]	[CF/FT]	[FT]			[CF]	
1	2	3.14	686			2,155	
TOTAL				5,275	1	13.9	
**Assumed	d Drywell Perco	lation Rate [Cl	-S]:	0.10			

 $No. of Drywells Required = \frac{Volume Required [CF]}{Percolation Rate [CFS]} * \frac{1 hour}{3600 seconds} * \frac{1}{Allowable Drain Time [hrs]}$ 

#### HYDROLOGIC DESIGN DATA RECORD - RATIONAL METHOD

Project: HH Shea Parking Garage Project No: 1124070 Concentration Point: Existing Catch Basin Existing Condition

Design Data: Design Frequency								
		2	5	10	25	50	100	Year
Drainage Areas:	$A_1$	0.50	0.50	0.50	0.50	0.50	0.50	Acres
	A <sub>2</sub>	0.05	0.05	0.05	0.05	0.05	0.05	Acres
	A <sub>3</sub>	-	-	-	-	-	-	Acres
Total Drainage Area	А	0.55	0.55	0.55	0.55	0.55	0.55	Acres
Drainage Length		303.00	303.00	303.00	303.00	303.00	303.00	Feet
Elevations:								
Top of Drainage Area		1365.63	1365.63	1365.63	1365.63	1365.63	1365.63	Feet
Bottom of Drainage Area		1361.40	1361.40	1361.40	1361.40	1361.40	1361.40	Feet
Drainage Area Slope		1.40	1.40	1.40	1.40	1.40	1.40	%
Hydrologic Soil Group		А	А	А	А	А	А	
Design Computations:		Design	Frequen	су				
		2	5	10	25	50	100	Year
Time of Concentration	$T_{c}$	5.55	5.00	5.00	5.00	5.00	5.00	Min
Rainfall Intensity	i	2.85	3.96	4.76	5.84	6.67	7.52	In/Hr
Runoff Coefficients:	$C_1$	0.85	0.85	0.85	0.94	0.95	0.95	
	C <sub>2</sub>	0.40	0.40	0.40	0.44	0.48	0.50	
	C <sub>3</sub>	-	-	-	-	-	-	
Weighted Runoff Coefficient	$C_W$	0.81	0.81	0.81	0.89	0.91	0.91	
Peak Discharge $Q_P = C_W I A$		1.3	1.8	2.1	2.9	3.3	3.8	cfs
Volume Computations:		2	5	10	25	50	100	Year
Volume $V = C_W P_{2hr} A$		0.03	0.04	0.05	0.07	0.08	0.09	ac-ft
Computed by:		Date:						

Notes:

 Runoff coefficients for 25-, 50- and 100-year storm frequencies were derived using adjustment factors of 1.10, 1.20 and 1.25, respectively, applied to the 2-10 year values with an upper limit of 0.95.

- 2. The ranges of runoff coefficients shown for urban land uses were derived from lot coverage standards specified in the zoning ordinances for Maricopa County.
- 3. Runoff coefficients for urban land uses are for lot coverage only and do not include the adjacent street and rights-of-way, or alleys.
- 4. Values based on the NDR terrain class. Values should be increased for NHS and NMT terrain classes by the difference between NHS (or NMT) and the NDR C values, up to a maximum of 0.95. Engineering judgement should be used.

#### HYDROLOGIC DESIGN DATA RECORD - RATIONAL METHOD

Project: HH Shea Parking Garage Project No: 1124070

#### Concentration Point: Existing Catch Basin Proposed Condition - Area to Exst Catch Basin

Design Data:	Design Frequency								
		2	5	10	25	50	100	Year	
Drainage Areas:	$A_1$	0.25	0.25	0.25	0.25	0.25	0.25	Acres	
	A <sub>2</sub>	0.05	0.05	0.05	0.05	0.05	0.05	Acres	
	$A_3$	-	-	-	-	-	-	Acres	
Total Drainage Area	А	0.30	0.30	0.30	0.30	0.30	0.30	Acres	
Drainage Length		167.00	167.00	167.00	167.00	167.00	167.00	Feet	
Elevations:									
Top of Drainage Area		1364.47	1364.47	1364.47	1364.47	1364.47	1364.47	Feet	
Bottom of Drainage Area		1361.40	1361.40	1361.40	1361.40	1361.40	1361.40	Feet	
Drainage Area Slope		1.84	1.84	1.84	1.84	1.84	1.84	%	
Hydrologic Soil Group		А	А	А	А	А	А		
Design Computations:		Design	Frequen	су					
		2	5	10	25	50	100	Year	
Time of Concentration	$T_{c}$	5.00	5.00	5.00	5.00	5.00	5.00	Min	
Rainfall Intensity	i	2.93	3.96	4.76	5.84	6.67	7.52	In/Hr	
Runoff Coefficients:	C1	0.85	0.85	0.85	0.94	0.95	0.95		
	C <sub>2</sub>	0.40	0.40	0.40	0.44	0.48	0.50		
	C <sub>3</sub>	-	-	-	-	-	-		
Weighted Runoff Coefficient	$C_W$	0.77	0.77	0.77	0.85	0.87	0.87		
Peak Discharge $Q_P = C_W I A$		0.7	0.9	1.1	1.5	1.8	2.0	cfs	
		. <u> </u>							
Volume Computations:		2	5	10	25	50	100	Year	
Volume $V = C_W P_{2hr} A$		0.02	0.02	0.03	0.04	0.04	0.05	ac-ft	
Computed by:		Date:							

Notes:

 Runoff coefficients for 25-, 50- and 100-year storm frequencies were derived using adjustment factors of 1.10, 1.20 and 1.25, respectively, applied to the 2-10 year values with an upper limit of 0.95.

- 2. The ranges of runoff coefficients shown for urban land uses were derived from lot coverage standards specified in the zoning ordinances for Maricopa County.
- 3. Runoff coefficients for urban land uses are for lot coverage only and do not include the adjacent street and rights-of-way, or alleys.
- 4. Values based on the NDR terrain class. Values should be increased for NHS and NMT terrain classes by the difference between NHS (or NMT) and the NDR C values, up to a maximum of 0.95. Engineering judgement should be used.

#### HYDROLOGIC DESIGN DATA RECORD - RATIONAL METHOD

Project: HH Shea Parking Garage Project No: 1124070

#### Concentration Point: Existing Catch Basin Proposed Condition - Overtopping from Basin A

Design Data:	Design Frequency								
		2	5	10	25	50	100	Year	
Drainage Areas:	$A_1$	0.04	0.04	0.04	0.04	0.04	0.04	Acres	
	A <sub>2</sub>	-	-	-	-	-	-	Acres	
	$A_3$	-	-	-	-	-	-	Acres	
Total Drainage Area	А	0.04	0.04	0.04	0.04	0.04	0.04	Acres	
Drainage Length		122.00	122.00	122.00	122.00	122.00	122.00	Feet	
Elevations:									
Top of Drainage Area		1364.10	1364.10	1364.10	1364.10	1364.10	1364.10	Feet	
Bottom of Drainage Area		1361.40	1361.40	1361.40	1361.40	1361.40	1361.40	Feet	
Drainage Area Slope		2.21	2.21	2.21	2.21	2.21	2.21	%	
Hydrologic Soil Group		А	А	А	А	А	А		
Design Computations:		Design	Frequen	су					
		2	5	10	25	50	100	Year	
Time of Concentration	$T_{c}$	5.00	5.00	5.00	5.00	5.00	5.00	Min	
Rainfall Intensity	i	2.93	3.96	4.76	5.84	6.67	7.52	In/Hr	
Runoff Coefficients:	$C_1$	0.85	0.85	0.85	0.94	0.95	0.95		
	C <sub>2</sub>	0.40	0.40	0.40	0.44	0.48	0.50		
	C <sub>3</sub>	-	-	-	-	-	-		
Weighted Runoff Coefficient	$C_W$	0.85	0.85	0.85	0.94	0.95	0.95		
Peak Discharge $Q_P = C_W I A$		0.1	0.1	0.2	0.2	0.3	0.3	cfs	
		<u> </u>	L	L	L				
Volume Computations:		2	5	10	25	50	100	Year	
Volume $V = C_W P_{2hr} A$		0.00	0.00	0.00	0.01	0.01	0.01	ac-ft	
Computed by:		Date:							

Notes:

 Runoff coefficients for 25-, 50- and 100-year storm frequencies were derived using adjustment factors of 1.10, 1.20 and 1.25, respectively, applied to the 2-10 year values with an upper limit of 0.95.

- 2. The ranges of runoff coefficients shown for urban land uses were derived from lot coverage standards specified in the zoning ordinances for Maricopa County.
- 3. Runoff coefficients for urban land uses are for lot coverage only and do not include the adjacent street and rights-of-way, or alleys.
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