

Case File Copy

Preliminary Drainage Report
Storage at Shea
SEC 116th Street & Shea Boulevard
Scottsdale, Arizona
COS
Case No. 50-DR-2017
Plan Check No. : 9-ZN-2017

Plan # _____
Case # 50-DR-2017
Q-S # _____

Accepted
 Corrections

DB 3/15/18
Reviewed By Date

Prepared for:
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[Signature]
15 FEB 18
EXP 9/30/20

50-DR-2017
02/28/18

EA #2259.01

August 9, 2017
Revised: February 13, 2018






JOB NO. 2259.01

DATE: 6/19/2017

SCALE: 1"=2000'



ERIE & ASSOCIATES, INC.
 3120 NORTH 24th STREET
 PHOENIX, ARIZONA 85016
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STORAGE AT SHEA

PLATE 2 - FEMA MAP

3.3 Drainage Concepts

- Detention basins will be provided for the 100-year, 2-hour onsite runoff volume from the developed portions of the site.
- Detention basins drain within 36 hours.
- Offsite flow will be collected in a constructed perimeter channel and routed around the east side of the development. For post-development conditions the flows will leave the site in the pre-development location. *Plate 5 – Master Drainage Plan.*
- Peak flows leaving the site during post-development conditions will not exceed predevelopment flows.

4.0 Hydrology

A hydrologic analysis was completed to determine the flows entering the site, for pre-development conditions. The peak flows for the 100-year storm event were calculated using the Rational Method for offsite subareas and HEC-1 for onsite subareas. See *Appendix A* for hydrologic data and calculations. The methodology used to calculate the peak flows is consistent with requirements outlined in the City of Scottsdale's Design Standards and Policies Manual.

Table 5 - 100-Year Flow Summary
 Existing Hydrology

4.1 Existing Hydrology

The offsite tributary area was delineated using City of Scottsdale topo and field reconnaissance. The remainder of the offsite and onsite tributary was determined using a one foot contour interval topo and point elevations survey completed as part of this project and field reconnaissance. See *Plate 4 - Existing Tributary Map* for the existing tributary areas. See *Appendix A* for the hydrologic worksheets and calculations.

4.2 Developed Hydrology

The onsite area was divided into two sub-areas for developed conditions. See *Plate 5 - Master Drainage Plan* for the developed tributary areas. The north portion of the site drains to detention basin DB-2 and the south portion drains to detention basin DB-2.

The sub-area parameters are summarized in *Table 1* and *Table 2*.

Table 1 - Offsite Sub-Area Parameters

Sub-Area	Area (acres)	i (in/hr)	C	Tc (min)
SA-1	0.65	7.8	0.7	5
SA-2	0.89	7.8	0.7	5
SA-3	1.17	7.8	0.7	5

Table 2 - Onsite Sub-Area Parameters

Sub-Area	Area (acres)	Length (mi)	Tc (hr)
SA-4 (existing)	1.8	0.086	0.198
SA-4N (developed)	0.7	0.060	0.102
SA-4S (developed)	1.4	0.105	0.155

7.0 References

“Drainage Design Manual for Maricopa County, Arizona”, prepared by Flood Control District of Maricopa County, dated 2009.

“Design Standards and Policies Manual”, prepared by City of Scottsdale, dated January 2010.

SA-1 (RATIONAL) EXISTING

Revised
Aug 8, 2017
by LE

$$Q = C i A$$

$$A = 0.65 \text{ ac}$$

$$Q = 0.7(7.8)(0.65)$$

$$i = 7.8 \text{ in/hr}$$

$$Q = 4 \text{ CFS}$$

$$C = 0.5(0.95) + 0.5(0.45)$$

$$C = 0.7$$

SA-2 EXISTING

$$A = 0.89 \text{ ac}$$

$$Q = 0.7(7.8)(0.89)$$

$$i = 7.8 \text{ in/hr}$$

$$Q = 5 \text{ CFS}$$

$$C = 0.7$$

SA-3 EXISTING

$$A_{SA-3} = 1.17 \text{ ac} + SA_2 = 1.17 + 0.89$$

$$= 2.06 \text{ ac} \quad T_C = 5 \text{ min}$$

$$i = 7.8 \text{ in/hr}$$

$$C = 0.7$$

$$Q = (0.7)(7.8)(2.06) \approx 11.0 \text{ CFS}$$

SA-4 EXISTING

$$A = 220(320) = 1.98 \text{ ac}$$

$$T_C = 5 \text{ min} \quad i = 7.8 \text{ in/hr}$$

$$C = 0.45 \text{ unid. desert}$$

$$Q_{EX} = (0.45)(7.8)(1.98) = 6.95 \text{ CFS}$$

$$\text{SAY } 7. \text{ CFS}$$

SA₄ developed

$$A = 27 \times (320) = 1,980 \text{ c}$$

$$T_c = 5 \text{ min}, \quad \dot{L} = 7.8 \text{ in/hr}$$

C composite

$$A_{\text{factory and building}} = 1,310 \text{ c} \quad C = 0.95$$

$$A_{\text{open}} = 1,980 - 1,310 = 0.67 \quad C = 0.45$$

$$C_{\text{AVE}} = \frac{1,310(0.95) + 0.67(0.45)}{1,980}$$

$$C_{\text{AVE}} = 0.78$$

$$\therefore Q_{\text{INTO BUILDING}} = (0.78)(7.8)(1,980) = 12,445$$

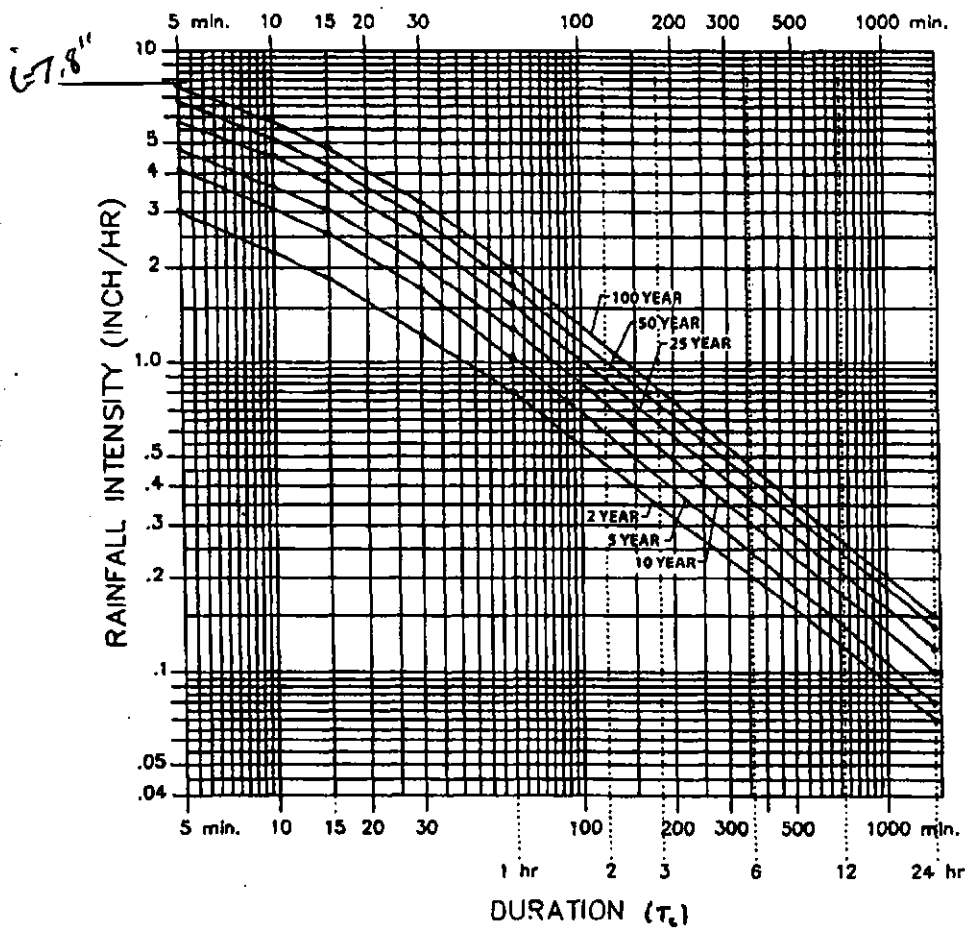
given flood event. For infrastructure design, the estimate of the actual split based on a hydraulic analysis of the current channel cross sections must include a minimum safety factor of 30 percent of the total flow. If the designer feels that there are extenuating factors affecting the stability of the split, the safety factor should be increased accordingly. The report should include a description of all assumptions made regarding watershed conditions used to calculate the peak flow rates.

C. The Rational Method

The Rational Method is limited to use on small, uniform, regularly shaped watersheds less than or equal to 160 acres in size. The methodology is provided in the Drainage Design Manual for Maricopa County, Hydrology.

1. Precipitation

Precipitation input is rainfall intensity, "I," and can be obtained directly from NOAA 14 at http://hdsc.nws.noaa.gov/hdsc/pfds/sa/az_pfds.html or from Figure 4.1-3. The time of concentration, "Tc," is all that is required to determine "I" from this figure.(source: NOAA 14)



RAINFALL INTENSITY-DURATION-FREQUENCY RELATION FOR MARICOPA COUNTY, ARIZONA

FIGURE 4.1-3 RAINFALL INTENSITY (I) VALUES FOR USE IN RATIONAL METHOD

100-2. VOLUME CALCULATION (EAST PARCEL)

$$V_r = \frac{P}{12} A C$$

$$A_T = 3.28 \text{ ac}$$

$$A_{\text{STEEL AC}} = 0.32 \text{ ac} \quad C = 0.95$$

$$A_{\text{PARK + BLDG}} = 1.31 \text{ ac} \quad C = 0.95$$

$$A_{\text{UNDEV}} = 1.65 \text{ ac} \quad C = 0.45$$

$$\Sigma = 3.28 \text{ ac}$$

$$C = \frac{1.63(0.95) + 1.65(0.45)}{3.28}$$

$$C = 0.70$$

$$V_r = \frac{2.3}{12} (3.28)(0.70) = 0.44 \text{ ac-ft}$$

2. Time of Concentration

Time of concentration "Tc" is the total time of travel from the most hydraulically remote part of the watershed to the concentration point of interest. The calculation of "Tc" must follow FCDMC Hydrology Manual procedures.

***Note:** Do not add a standard set amount of time to the estimated "Tc" for lot runoff delay (such as 5 or 10 minutes). Natural land slopes are too variable in Scottsdale to add a set amount of time for lot runoff.

3. Runoff Coefficients

Use Figure 4.1-4 or equivalent to obtain the runoff coefficients or "C" values. Composite "C" values for the appropriate zoning category or weighted average values calculated for the specific site are both acceptable approaches.

RUNOFF COEFFICIENTS - "C" VALUE			
Land Use	Storm Frequency		
	2-25 Year	50 Year	100 Year
Composite Area-wide Values			
Commercial & Industrial Areas	0.80	0.83	0.86
Residential Areas-Single Family (average lot size)			
R1-1-1901	0.33	0.50	0.53
R1-130	0.35	0.51	0.59
R1-70	0.37	0.52	0.60
R1-43	0.38	0.55	0.61
R1-35 (35,000 square feet/lot)	0.40	0.56	0.62
R1-18 (18,000 square feet/lot)	0.43	0.58	0.64
R1-10 (10,000 square feet/lot)	0.47	0.62	0.67
R1-7 (7,000 square feet/lot)	0.51	0.64	0.94
Townhouses (R-2, R-4)	0.63	0.74	0.94
Apartments & Condominiums (R-3, R-5)	0.76	0.83	0.94
Specific Surface Type Values			
Paved streets, parking lots (concrete or asphalt), roofs, drive-ways, etc.	0.90	0.93	0.95
Lawns, golf courses, & parks (grassed areas)	0.20	0.25	0.30
Undisturbed natural desert or desert landscaping (no impervious weed barrier)	0.37	0.42	0.45
Desert landscaping (with impervious weed barrier)	0.63	0.73	0.83
Mountain terrain – slopes greater than 10%	0.60	0.70	0.80
Agricultural areas (flood-irrigated fields)	0.16	0.18	0.20

FIGURE 4.1-4 RUNOFF COEFFICIENTS FOR USE WITH RATIONAL METHOD

ONSITE HEC-1

RAINFALL

SA-4 (EXISTING)

MAP=64,1219

$$A = 1.82 \text{ ac} = 0.0028 \text{ mi}^2$$

$$L = 455 \text{ ft} = 0.086 \text{ mi}$$

$$\text{USGE} = 1475$$

$$\text{DSGE} = 1465$$

SOIL TYPE

3

AREA

0.0028 mi²

LAND USE

DESERT

AREA

0.0028 mi²

SA-4N (DEVELOPED)

$$A = 0.71 \text{ ac} = 0.001 \text{ mi}^2$$

$$L = 315 \text{ ft} = 0.060 \text{ mi}$$

$$USGE = 1473$$

$$DSGE = 1468$$

SOILTYPE

3

AREA

0.001 mi²

LANDUSE

COMM

AREA

0.001 mi²

(USE 310 WAREHOUSE)

SA-4S (DEVELOPED)

$$A = 1.40 \text{ ac} = 0.002 \text{ mi}^2$$

$$L = 555 \text{ ft} = 0.105 \text{ mi}$$

$$USGE = 1473$$

$$DSGE = 1467.5$$

SOILTYPE

3

AREA

0.002 mi²

LANDUSE

COMM

AREA

0.002 mi²

DB-1

$$V = \frac{1983 + 8678}{2} \left(\frac{1}{3}\right) \frac{1}{43560} = \underline{0.37 \text{ ac-ft}}$$

- CHECK DRAW TIME

$$Q = C_d A \sqrt{2gh} \quad \text{ORIFICE EQUATION}$$

$$C_d = 0.62$$

$$A_g'' = \pi (0.25')^2 = 0.196 \text{ FT}^2$$

$$g = 32.2 \text{ ft/s}^2$$

$$h = 1.5' - 0.25' = 1.25' \quad \text{HEAD @ CENTERLINE}$$

$$Q = 0.62 (0.196 \text{ FT}^2) \sqrt{2(32.2)(1.25)}$$

$$Q = 1.1 \text{ CFS}$$

$$t = \frac{V}{Q} = \frac{0.37 \text{ ac-ft} (43560)}{1.1 \frac{\text{CF}}{\text{s}} \times \frac{3600 \text{ s}}{\text{hr}}}$$

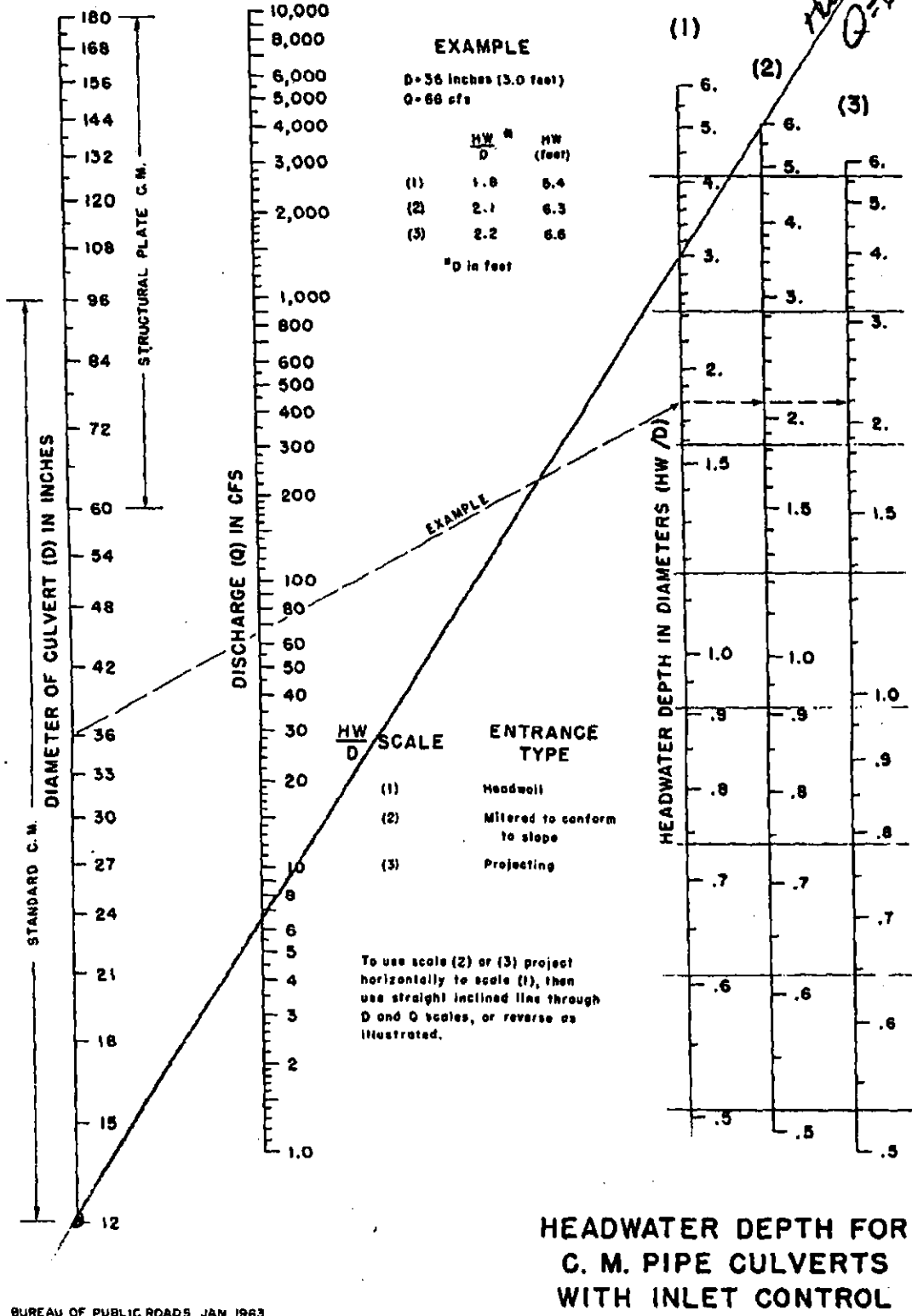
$$\underline{t = 4.1 \text{ hr}}$$

DB-2

$$V = \frac{650 + 2901}{2} \left(\frac{1}{3}\right) \frac{1}{43560} = \underline{0.12 \text{ ac-ft}}$$

$$t = \frac{0.13 (43560)}{1.1 (3600)} = \underline{1.3 \text{ hr}}$$

CHART 2



BUREAU OF PUBLIC ROADS JAN. 1963

Appendix B – HEC-1 input/output


```

X   X   XXXXXXX   XXXXX   X
X   X   X   X   X   XX
X   X   X   X   X   X
XXXXXXX   XXXX   X   XXXXX   X
X   X   X   X   X   X
X   X   X   X   X   X
X   X   XXXXXXX   XXXXX   XXX
  
```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.
 THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE.
 THE DEFINITION OF -AMSK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION
 NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY,
 DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION
 KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT											PAGE 1
LINE	ID	1	2	3	4	5	6	7	8	9	10
1	ID	Flood Control District of Maricopa County									
2	ID	2259 - STORAGE AT SHEA									
3	ID	100 YEAR									
4	ID	6 Hour Storm									
5	ID	Unit Hydrograph: Clark									
6	ID	Storm: Multiple									
7	ID	02/14/2018									
	*DIAGRAM										
8	IT	1	1JAN99	0	2000						
9	IO	5									
10	IN	15									
	*										
11	JD	2.723	0.0001								
12	PC	0.000	0.008	0.016	0.025	0.033	0.041	0.050	0.058	0.066	0.074
13	PC	0.087	0.099	0.118	0.138	0.216	0.377	0.834	0.911	0.931	0.950
14	PC	0.962	0.972	0.983	0.991	1.000					
15	JD	2.707	0.5000								
16	PC	0.000	0.008	0.016	0.025	0.033	0.041	0.050	0.058	0.066	0.074
17	PC	0.087	0.099	0.118	0.138	0.216	0.377	0.834	0.911	0.931	0.950
18	PC	0.962	0.972	0.983	0.991	1.000					
	*										
19	KK	SA-4	BASIN								
20	BA	0.003									
21	LG	0.35	0.35	3.39	0.64	80					
22	UC	0.198	0.244								
23	UA	0	3.0	5.0	8.0	12.0	20.0	43.0	75.0	90.0	96.0
24	UA	100									
	*										
25	KK	SA-4N	BASIN								
26	BA	0.001									
27	LG	0.10	0.27	3.39	1.00	80					
28	UC	0.102	0.159								
29	UA	0	5.0	16.0	30.0	65.0	77.0	84.0	90.0	94.0	97.0
30	UA	100									
	*										
31	KK	DB-2	STORAGE								
32	KO										
33	RS	1	STOR								
34	SV		0.12								
35	SQ		6.00								
36	SE	1465.0	1468.00								
	*										
37	KK	SA-4S	BASIN								
38	BA	0.002									
39	LG	0.10	0.27	3.39	1.00	80					
40	UC	0.155	0.277								
41	UA	0	5.0	16.0	30.0	65.0	77.0	84.0	90.0	94.0	97.0
42	UA	100									
	*										

1

HEC-1 INPUT											PAGE 2
LINE	ID	1	2	3	4	5	6	7	8	9	10
43	KK	CP.A	COMBINE								
44	HC	2									
	*										
45	KK	DB-1	STORAGE								
46	KO										
47	RS	1	STOR								
48	SV		0.37								
49	SQ		2.00								
50	SE	1464.5	1467.50								
	*										
51	ZZ										

1
 INPUT LINE (V) ROUTING [--->] DIVERSION OR PUMP FLOW

19 SA-4
25 SA-4N
V
V
31 DB-2
37 SA-4S
43 CP.A.....
V
V
45 DB-1

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

FLOOD HYDROGRAPH PACKAGE (HEC-1)
JUN 1998
VERSION 4.1
RUN DATE 14FEB18 TIME 09:55:52

U.S. ARMY CORPS OF ENGINEERS
HYDROLOGIC ENGINEERING CENTER
609 SECOND STREET
DAVIS, CALIFORNIA 95616
(916) 756-1104

Flood Control District of Maricopa County
2259 - STORAGE AT SHEA
100 YEAR
6 Hour Storm
Unit Hydrograph: Clark
Storm: Multiple
02/14/2018

9 IO OUTPUT CONTROL VARIABLES
IPRNT 5 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 1 MINUTES IN COMPUTATION INTERVAL
IDATE 1JAN99 STARTING DATE
ITIME 0000 STARTING TIME
NQ 2000 NUMBER OF HYDROGRAPH ORDINATES
MDDATE 2JAN99 ENDING DATE
NDTIME 0919 ENDING TIME
ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 0.02 HOURS
TOTAL TIME BASE 33.32 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FeET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

11 JD INDEX STORM NO. 1
STRM 2.72 PRECIPITATION DEPTH
TRDA 0.00 TRANSPOSITION DRAINAGE AREA

12 PI PRECIPITATION PATTERN
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
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15 JD INDEX STORM NO. 2
STRM 3.71 PRECIPITATION DEPTH

