Wastewater Basis of Design Report

Happy Valley - 18

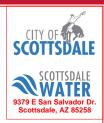
Prepared for:

Camelot Homes, Inc. 6607 North Scottsdale Road, Suite H-100 Scottsdale, AZ 85250 FINAL Basis of Design Report

APPROVED

☐ APPROVED AS NOTED





Disclaimer: If approved; the approval is granted under the condition that the final construction documents submitted for city review will match the information herein. Any subsequent changes in the water or sewer design that materially impact design criteria or standards will require re-analysis, re-submittal, and approval of a revised basis of design report prior to the plan review submission.; this approval is not a guarantee of construction document acceptance. For questions or clarifications contact the Water Resources Planning and Engineering Department at 480-312-5685.

BY scan

DATE 6/1/2020

Prepared by:

Kimley-Horn & Associates, Inc. 7740 North 16th Street, Suite 300 Phoenix, AZ 85020



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1.0 INTRODUCTION

Kimley-Horn and Associates, Inc. has prepared this wastewater basis of design report for the proposed residential development at the southwest corner of Alma School Road and Happy Valley Road in Scottsdale, Arizona. This report will demonstrate that the proposed project conforms to the City of Scottsdale design requirements.

Happy Valley 18, the "project", encompasses approximately 29 acres and contains a total of 21 single family residential lots. The project lies within a portion of the southwest quarter of Section 8, Township 4 North, Range 5 East of the Gila and Salt River Base and Meridian in Maricopa County, Arizona. More specifically, the project is bounded by Alma School Road to the east, Happy Valley Road to the north, with single family residential subdivisions to the north, east, and west. The site slopes from the northeast to the southwest at approximately 4.0%. Refer to **Figure 1** in **Appendix A** for the project Vicinity Map.



2.0 WASTEWATER COLLECTION SYSTEM

2.1 SYSTEM LAYOUT

There is an existing 12" sanitary sewer main in Alma School Road that flows to the south towards Pinnacle Peak Road. A proposed 8" sewer main is proposed to connect to the existing 12" sewer in Alma School at the southeast portion of the project. The 8" line is aligned in Tract A until the southern leg where the 8" line turns south in the proposed water and sewer easement. From there, the proposed 8" sewer line tees in East Desert Vista Drive where it remains an 8" line. To the west the line terminates in the existing cul-desac in a proposed manhole. To the east, the proposed 8" sewer line continues until it taps into the existing 12" sewer main in Alma School Road. A new manhole will be required at the point of connection in Alma School Road. A majority of the sewer will be located within the private street tract, Tract A, with a blanket water and sewer facilities easement located over it. The portion of the sewer outside the private street tract will be within a 30-foot water and sewer facilities easement.

Due to odor issues in Alma School sewer a chemical dosing station will be required with site dimensions of 30 ft X 40 ft. The site will have access to a manhole for the chemical feed. Final determination of the design and location will be made at the time of preliminary plat and will be made as a stipulation of approval

All 8" sewer lines will be PVC SDR 35 at a minimum slope of 0.52%. Sewer Manhole sections and cones will be precast concrete as detailed in the MAG Standard Detail No. 420, without the manhole steps and/or cast in anchors for steps. Manholes shall be 4 feet in diameter, and for depths less than 10 feet. Manholes shall be 5 feet in diameter for all depths greater than 10 foot. Refer to **Figure 2** in **Appendix A** for the wastewater layout.

2.2 SYSTEM ANALYSIS AND RESULTS

2.5

To determine the capacity of the proposed onsite wastewater collection system, design flows were calculated and analyzed with minimum pipe design slopes. Design flows are calculated based on the criteria in Section 7-1.403 of **Reference 1**. For residential developments, the design flow is 100 gallons per capita per day (gpcd) with a peaking factor of 4. Residential densities are assumed to be 2.5 persons per dwelling unit. Average Day Flow (ADF) and Peak Day Flow (PDF) are summarized in Table 2 below:

Density (persons/DU) Design flow ADF Peaking PDF PDF

(GPD)

5,250

Factor

4.0

(GPD)

21,000

(GPM)

14.59

(gpcpd)

100

Table 2: Wastewater Design Flows

Sanitary sewer lines will be designed to maintain a full flow velocity between 2.5 ft/sec – 10 ft/sec with a maximum depth to diameter ratio (d/D) of 0.65 in the ultimate peak flow condition. To achieve the velocity requirements, the minimum slope of 0.52% and maximum slope of 8.33% will be utilized. Using the peak flow calculated in **Table 2** and the minimum design slope, an 8" sewer main has the capacity to convey the proposed design flows with a flow depth of 1.08" and a d/D ratio of 0.14. Sewer pipe capacity calculations can be seen in **Appendix B**.

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3.0 CONCLUSION

This project proposes a new 8" sanitary sewer main to serve the proposed development which will gravity flow into the existing 12" sanitary main in Alma School Road. Based on the analysis in this report, an 8" sewer main has the capacity to convey the proposed design flow for the development.



4.0 REFERENCES

- 1. City of Scottsdale, Design Standards and Policies Manual. 2018.
- 2. International Code Council, 2015 International Fire Code. May 2014.

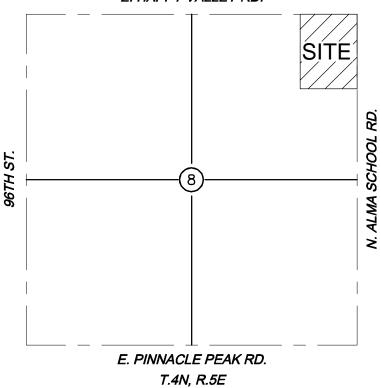
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Appendix A – Figures

Figure 1 – Vicinity Map

Figure 2 – Wastewater Layout

E. HAPPY VALLEY RD.



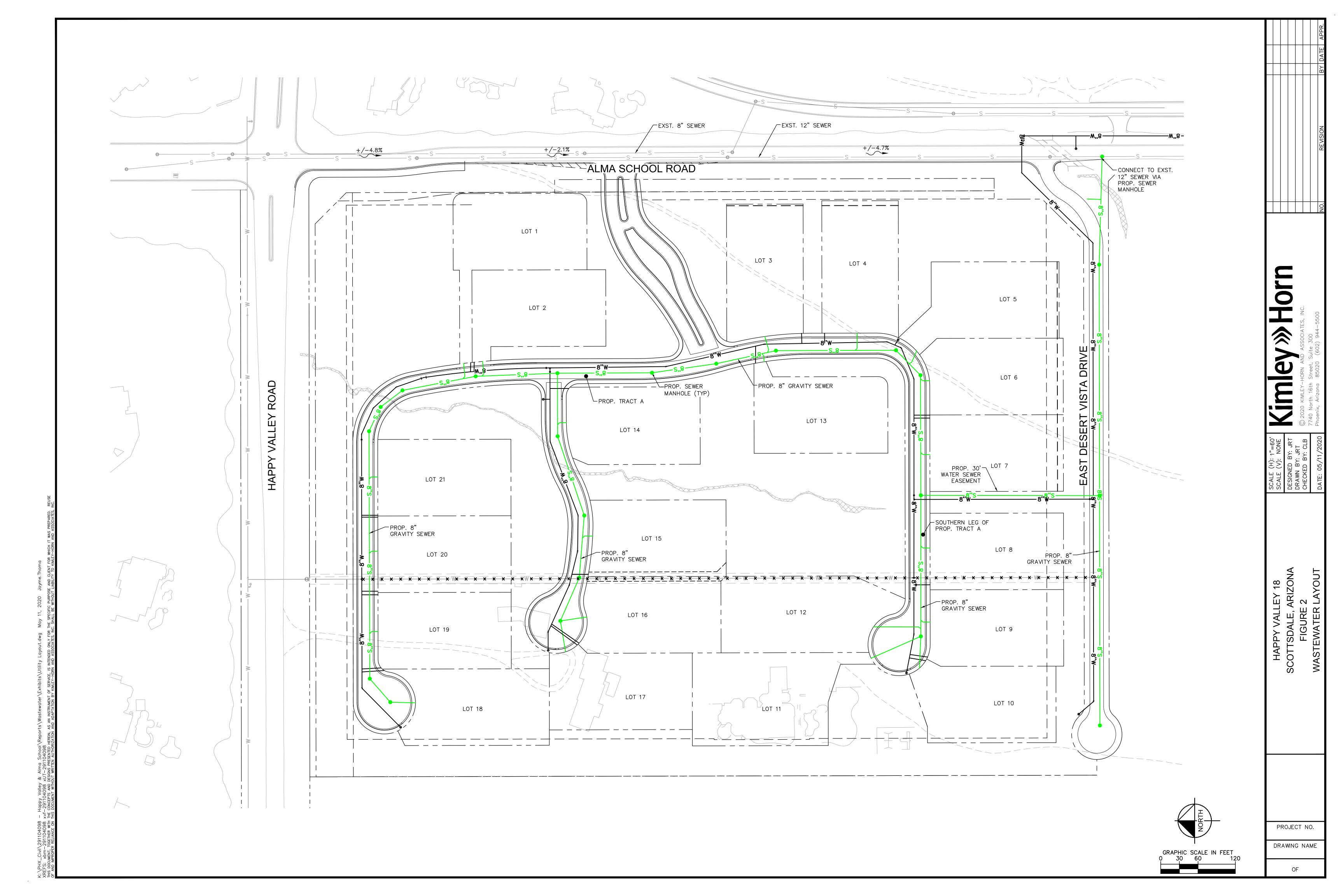
PROJECT NO. 291104098 DRAWNG NAME

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HAPPY VALLEY 18 FIGURE 1 VICINITY MAP SCALE (H): NTS
SCALE (V): NTS
DESIGNED BY: MML
DRAWN BY: MML
CHECKED BY: MML
DATE: 5/30/2019



| NO. | REVISION | DATE |
|-----|----------|------|



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Appendix B – Sewer Capacity Calculations

Worksheet for 8" Capacity

| Project Description | | |
|-----------------------------|---------------------|---|
| Friction Method | Manning | |
| | Formula | |
| Solve For | Normal Depth | |
| Input Data | | |
| Roughness Coefficient | 0.013 | |
| Channel Slope | 0.00520 ft/ft | |
| Diameter | 8.0 in | |
| Discharge | 21,000.00 gpd | _ |
| Results | | |
| Normal Depth | 1.1 in | |
| Flow Area | 0.0 ft ² | |
| Wetted Perimeter | 0.5 ft | |
| Hydraulic Radius | 0.7 in | |
| Top Width | 0.45 ft | |
| Critical Depth | 1.0 in | |
| Percent Full | 13.2 % | |
| Critical Slope | 0.00722 ft/ft | |
| Velocity | 1.19 ft/s | |
| Velocity Head | 0.02 ft | |
| Specific Energy | 0.11 ft | |
| Froude Number | 0.856 | |
| Maximum Discharge | 606,286.92 gpd | |
| Discharge Full | 563,617.75 gpd | |
| Slope Full | 0.00001 ft/ft | |
| Flow Type | Subcritical | |
| GVF Input Data | | |
| Downstream Depth | 0.0 in | |
| Length | 0.0 ft | |
| Number Of Steps | 0 | |
| GVF Output Data | | |
| Upstream Depth | 0.0 in | |
| Profile Description | | |
| Profile Headloss | 0.00 ft | |
| Average End Depth Over Rise | 0.0 % | |
| Normal Depth Over Rise | 13.5 % | |
| Downstream Velocity | Infinity ft/s | |
| Upstream Velocity | Infinity ft/s | |
| Normal Depth | 1.1 in | |
| Critical Depth | 1.0 in | |
| Channel Slope | 0.00520 ft/ft | |
| Critical Slope | 0.00722 ft/ft | |
| Critical Slope | 0.00722 ft/ft | |

Worksheet for 8" Full Flow Capacity

Friction Method Manning Formula
Solve For Full Flow Capacity

Input Data

 Roughness Coefficient
 0.013

 Channel Slope
 0.00520
 ft/ft

 Normal Depth
 8.00
 in

 Diameter
 8.00
 in

 Discharge
 563617.75
 gal/day

Results

Discharge 563617.75 gal/day Normal Depth 8.00 in Flow Area 0.35 ft2 Wetted Perimeter 2.10 ft Hydraulic Radius 2.00 in Top Width 0.00 ft Critical Depth 0.44 ft Percent Full 100.0 % Critical Slope 0.00857 ft/ft Velocity 2.50 ft/s Velocity Head 0.10 ft Specific Energy 0.76 ft Froude Number 0.00 Maximum Discharge 0.94 ft³/s Discharge Full 0.87 ft³/s Slope Full 0.00520 ft/ft SubCritical Flow Type

GVF Input Data

Downstream Depth 0.00 in Length 0.00 ft Number Of Steps 0

GVF Output Data

Upstream Depth 0.00 in Profile Description

Profile Headloss 0.00 ft

Average End Depth Over Rise 0.00 %

Worksheet for 8" Full Flow Capacity

GVF Output Data

| Normal Depth Over Rise | 100.00 | % |
|------------------------|----------|-------|
| Downstream Velocity | Infinity | ft/s |
| Upstream Velocity | Infinity | ft/s |
| Normal Depth | 8.00 | in |
| Critical Depth | 0.44 | ft |
| Channel Slope | 0.00520 | ft/ft |
| Critical Slope | 0.00857 | ft/ft |



Abbreviated Water and Sewer Needs

Water Basis of Design Report

Happy Valley - 18

Prepared for:

Camelot Homes, Inc. 6607 North Scottsdale Road, Suite H-100 Scottsdale, AZ 85250

Prepared by:

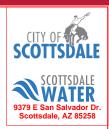
Kimley-Horn & Associates, Inc. 7740 North 16th Street, Suite 300 Phoenix, AZ 85020

Kimley» Horn

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FINAL Basis of Design Report

- **APPROVED**
- ☐ APPROVED AS NOTED
- ☐ REVISE AND RESUBMIT



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BY scan

DATE 6/1/2020



2-PP-2020 5/15/2020

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Appendix A: Exhibits

Exhibit 1 - Vicinity Map

Exhibit 2 – Water System Layout

Exhibit 3 – WaterCAD Network

Appendix B: Average Day Demand Results

Appendix C: Peak Hour Demand Results

Appendix D: Maximum Day Demand + Fire Flow Results

Appendix E: Fire Hydrant Flow Test Results

1.0 INTRODUCTION

Happy Valley 18, the "project", is a proposed 21-lot single family residential subdivision located on approximately 29 acres at the southwest corner of Happy Valley Road and Alma School Road in Scottsdale, Arizona. The project lies within a portion of the northeast quarter of Section 8, Township 4 north, Range 5 east of the Gila and Salt River Base and Meridian, Maricopa County, Arizona. Refer to **Exhibit 1** for a Vicinity Map.

The purpose of this report is to calculate the project's water demands, determine the available system capacity and proposed hydraulics of the planned water system while meeting the requirements of the City of Scottsdale and the 2015 International Fire Code (IFC). As a result of this analysis, it will be determined if the potable water infrastructure is capable of satisfying the projected fire flow and domestic water demands for the project.

2.0 EXISTING WATER DISTRIBUTION SYSTEM

There is an existing 8" water main in Happy Valley Road along the north boundary of the project. This existing water main transitions to a 12" main near the intersection of Alma School Road. There is also an existing 6" waterline in Alma School Road approximately 452' south of the site. There is an existing stub provided in Alma School Road before the line jogs northeast into the North Greenman Road alignment.

3.0 PROPOSED WATER DISTRIBUTION SYSTEM

There is an existing 8" water line that runs from Happy Valley Road south through the site. In order to serve the project, the existing 8" water line will be cut at the northern leg of Tract A and tied into the proposed 8" waterline system with an 8" tee. The remainder of the existing 8" waterline will be abandoned. This proposed 8" water main will extend throughout the site and follow the roadway alignment to provide a domestic water service connection for each lot and fire hydrants spaced no more than 600' apart. Refer to **Exhibit 2** for a water system layout.

The second connection for the site is provided approximately 452' south of the site in the Alma School Road alignment. There is an existing 6" water line, with stub, that the proposed 8" waterline will tie into.

For more detail on the proposed connections see **Section 4.3**.

4.0 BASIS OF DESIGN

4.1 DOMESTIC WATER DEMAND

Per Figure 6-1.2 of the *City of Scottsdale Design Standards & Policies Manual*, the average day demand (ADD) for residential land use (<2 du/acre) is 0.69 gallons per minute per unit (gpm/du). Maximum Day Demand (MDD) is calculated as 2.0 times the ADD and Peak Hour Demand (PHD) is calculated as 3.5 times the ADD. Refer to **Table 1** below for a summary of domestic water demands.

Table 1 Domestic Water Demands

| Land Use | ADD | Dwelling | ADD | MDD | PHD |
|--------------------------|----------|------------|-------|-------|-------|
| | (gpm/du) | units (du) | (gpm) | (gpm) | (gpm) |
| Residential (<2 du/acre) | 0.69 | 21 | 14.5 | 29 | 50.8 |

4.2 FIRE FLOW DEMAND

Per Table B105.1(1) of the 2015 IFC, the required fire flow for single family residential dwellings is 1,000 gpm for a 1-hour duration.

4.3 DESIGN PARAMETERS

The following design criteria will be utilized for this project:

Table 2 Design Parameters

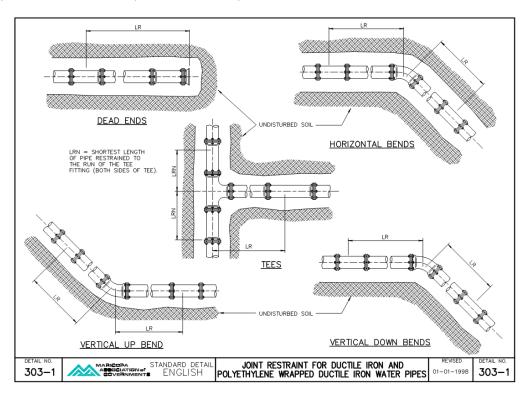
| Design Criteria | ADD | PHD | MDD + Fire Flow |
|---------------------------|-----|-----|--------------------|
| Minimum Pressure (psi) | 50 | 50 | 30 |
| Maximum Pressure (psi) | 100 | 100 | 100 |
| Maximum Velocity (ft/sec) | 5 | 5 | 10 |

The Happy Valley 18 project will connect in two places to the existing City of Scottsdale water system, one to the existing waterline stubbing south from Happy Valley Road and the second through East Desert Vista Drive, south of the Site. The first connection will require a tee to be cut into the existing 8" waterline with isolation valves per the DSPM. The 8" waterline off Happy Valley Road has sufficient valves located to isolate the waterline during construction. Refer to **Exhibit 2** for a water system layout.

For the second connection, the proposed 8" line is aligned in Tract A until the southern leg of Tract A where the 8" line turns south in the proposed water and sewer easement. From there, the proposed 8" water line tees in East Desert Vista Drive where it remains an 8" line. To the west the line terminates in the existing cul-de-sac in a proposed fire hydrant. To the east, the proposed 8" water line continues until it turns south in the Alma School Road alignment. The 8" water line continues approximately 452' south to the existing 6" water line stub where a proposed connection is made. A reducer is proposed to connect the proposed 8" waterline to the existing 6" waterline. A majority of the water line will be located within the private street tract, Tract A, with a blanket water and sewer facilities easement located over it. The portion of the water line outside the private street tract will be within a 30-foot water and sewer facilities easement. The waterline in Alma School Road has existing isolation valves north of the connection in North Greenman Road and south of the connection in Alma School Road (see QS 46-53). Refer to **Exhibit 2** for a water system layout.

All waterlines will be 8" DIP Class 350, with 3 foot of minimum cover. The ends of the proposed cul-desacs will have fire hydrants to allow for flushing the waterlines. The dip sections under the proposed

storm drains will be realigned per MAG STD DTL 404. All waterlines will be located within water/sewer facility easements. Thrust restraints will be located at horizontal and vertical bends and lateral branches per MAG Standard Detail 303-1 and 303-2. Thrust blocks will not be utilized. All restrained pipe lengths will be specified on the final Improvement Plans per the detail and table below.



| NOMINAL | VERTICAL OFFSETS | | | | | | | | | | | |
|-----------------|------------------|--------|-----------|-------------------------|------------|--------------|---------------------|--------------|------------|--------------|-------------|------|
| PIPE | HORIZ | ONTAL | BENDS | TEES | | 90, BEND | FITTINGS | | FITTINGS | | ND FITTINGS | DEAD |
| SIZE INCHES | 90* | 45* | 22-1/2* | LRN=0' | LRN=10' | DOWN BEND | UP BEND | DOWN BEND | UP BEND | DOWN BEND | UP BEND | ENDS |
| 4 | 18 | 7 | 4 | 30 | 8 | 31 | 18 | 13 | 7 | 6 | 3 | 31 |
| 6 | 25 | 10 | 5 | 4.3 | 20 | 44 | 25 | 18 | 10 | 9 | 5 | 44 |
| 8 | 32 | 13 | 6 | 56 | 34 | 58 | 32 | 24 | 13 | 11 | 6 | 58 |
| 10 | 38 | 16 | 8 | 68 | 45 | 69 | 38 | 29 | 16 | 14 | 8 | 69 |
| 12 | 45 | 19 | 9 | 80 | 57 | 81 | 45 | 34 | 19 | 16 | 9 | 81 |
| 14 | 51 | 21 | 10 | 91 | 68 | 92 | 51 | 38 | 21 | 18 | 10 | 92 |
| 16 | 57 | 24 | 11 | 103 | 79 | 104 | 57 | 43 | 24 | 21 | 11 | 104 |
| 18 | 62 | 26 | 12 | 113 | 90 | 115 | 62 | 48 | 26 | 23 | 12 | 115 |
| 20 | 68 | 28 | 14 | 125 | 100 | 126 | 68 | 52 | 28 | 25 | 14 | 126 |
| 24 | 79 | 33 | 16 | 145 | 121 | 147 | 79 | 61 | 33 | 29 | 16 | 147 |
| NOMINAL PIPE | HORIZ | ONTAL | BENDS | TEES | 90' BEND | FITTINGS | ERTICAL 45° BEND | FITTINGS | | END FITTINGS | DEAD | |
| SIZE INCHES | 90* | 45* | 22-1/2 | LRN=0' | 1.01.40 | DOWN BEND | UP BEND | DOWN BEND | UP BEND | DOWN BEND | UP BEND | ENDS |
| 4 | 26 | 11 | 5 | 69 | LRN=10' | 72 | 26 | 30 30 | 11 | 14 | 5 | 72 |
| 6 | 36 | 15 | 7 | 99 | 47 | 102 | 36 | 42 | 15 | 20 | 7 | 102 |
| 8 | 47 | 19 | 9 | 130 | 78 | 133 | 47 | 55 | 19 | 26 | 9 | 133 |
| 10 | 56 | 23 | 11 | 157 | 103 | 159 | 56 | 66 | 23 | 32 | 11 | 159 |
| 12 | 65 | 27 | 13 | 185 | 131 | 187 | 65 | 77 | 27 | 37 | 13 | 187 |
| 14 | 74 | 31 | 15 | 211 | 156 | 214 | 74 | 89 | 31 | 42 | 15 | 214 |
| 16 | 82 | 34 | 16 | 238 | 183 | 241 | 82 | 100 | 34 | 48 | 16 | 241 |
| 18 | 90 | 37 | 18 | 263 | 207 | 266 | 90 | 110 | 38 | 53 | 18 | 266 |
| 20 | 98 | 41 | 20 | 289 | 233 | 292 | 98 | 121 | 41 | 58 | 20 | 292 |
| 24 | 113 | 47 | 22 | 337 | 280 | 340 | 113 | 141 | 47 | 68 | 22 | 340 |
| | | | JOINTS WI | THIN THE S ARE GIVEN | | NGTH LR MI | JST BE RES | TRAINED. | | | | |
| | | 2. THE | MAXIMUM | TEST PRES | SURE SHALL | NOT EXCE | D 200 PSI | | | | | |
| | | 3. THE | MINIMUM I | DEPTH OF E | BURY SHALL | BE 3' TO ' | TOP OF PIPE | Ε. | | | | |
| | | | | | | | IDD OD TED | | RING CALC | | | |

4.4 HYDRAULIC MODEL

A water model, using Bentley's WaterCAD V8i program, was used to analyze the proposed water system. To determine the existing and static and residual water pressures in the area, a fire hydrant flow test was completed using the adjacent fire hydrants near the project. The results from this test produced three different data points for static, residual, and maximum water pressures with associated flow rates. This data was then input into the water model and simulated as a reservoir and pump. Refer to **Appendix E** for Fire Hydrant Flow Test results.

The following scenarios were modeled to evaluate the existing and proposed water infrastructure to demonstrate compliance with the design parameters identified in this report:

- Average Day Demand
- Peak Hour Demand
- Maximum Day Demand + Fire Flow Demand

Refer to Exhibit 3 for the WaterCAD network.

4.5 HYDRAULIC MODEL RESULTS

The results for Average Day Demand and Peak Hour Demand can be seen in **Appendix B** and **Appendix C**, respectively. All junctions maintained a minimum pressure of 72 psi or greater and all pipes maintained a velocity of 0.32 ft/sec or less.

The results for Maximum Day Demand + Fire Flow Demand can be seen in **Appendix D**. All proposed fire hydrants meet the minimum required fire flow of 1,000 gpm at a minimum pressure of 30 psi with a maximum velocity of 10 ft/sec.

5.0 CONCLUSION

Based on the results presented in this report, the existing water infrastructure has the capability to support the proposed development while conforming to the City of Scottsdale's design criteria. An 8" water main is proposed onsite which will connect to an existing 8" water main in Happy Valley Road.

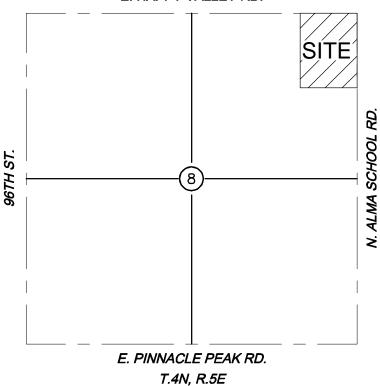
APPENDIX A: Exhibits

Exhibit 1 - Vicinity Map

Exhibit 2 – Water System Layout

Exhibit 3 – WaterCAD Network

E. HAPPY VALLEY RD.

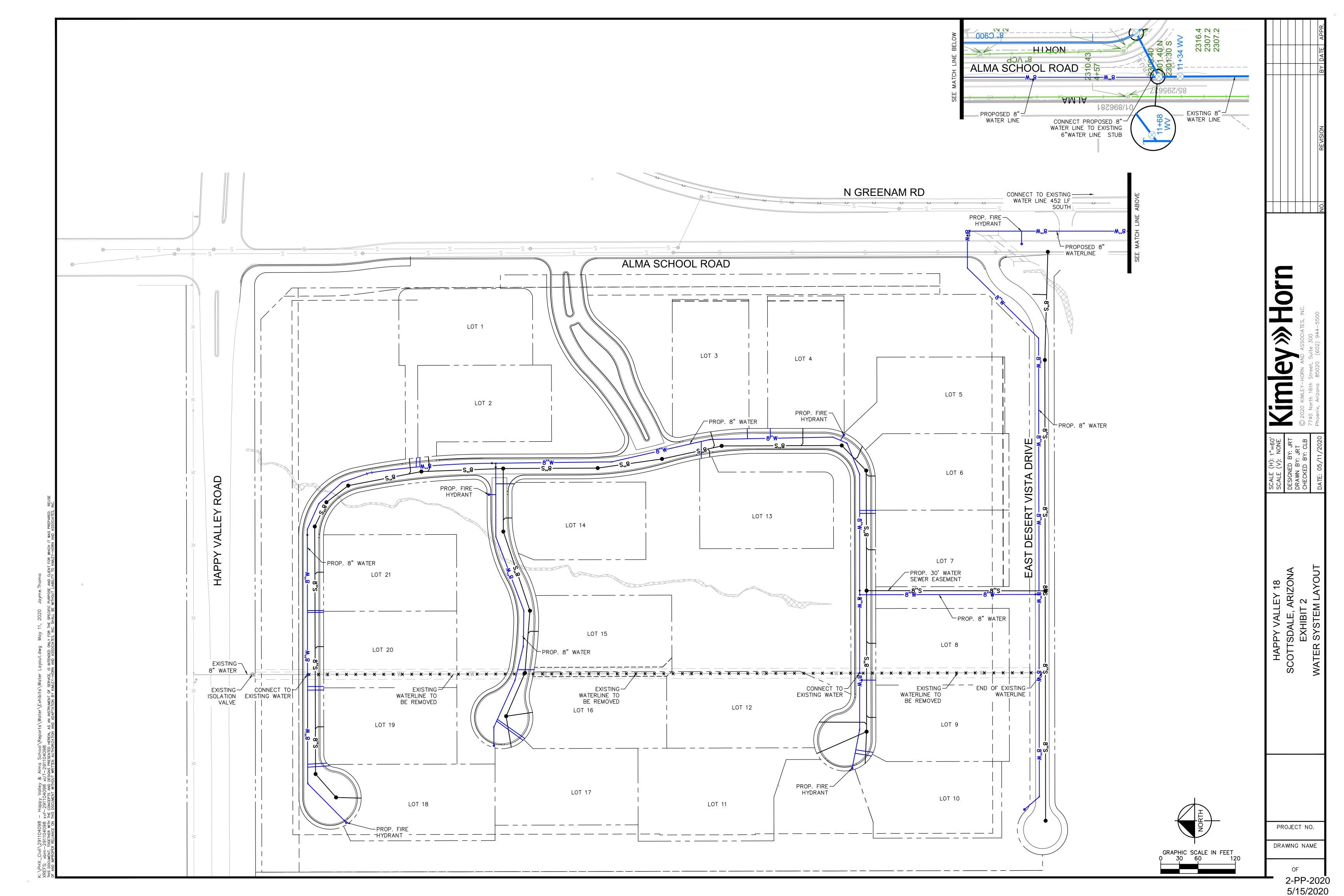


PROJECT NO. 291104098 DRAWING NAME

1 of

HAPPY VALLEY 18 EXHIBIT 1 VICINITY MAP SCALE (H): NTS
SCALE (V): NTS
DESIGNED BY: MML
DRAWN BY: MML
CHECKED BY: MML





Scenario: Average Day

HV18.wtg 1/20/2020

APPENDIX B: Average Day Demand Results

Pipe Table

Junction Table

Hydrant Table

Reservoir Table

Pump Table

Pipe Table - Time: 0.00 hours

| Label | Length (Scaled) (ft) | Start Node | Stop Node | Diameter (in) | Material | Hazen-Williams C | Flow (gpm) | Velocity (ft/s) | Headloss Gradient (ft/ft) |
|------------|----------------------------|---------------|--------------|------------------|--------------|---------------------|---------------|--------------------|---------------------------------|
| P-1 | 39 | R-1 | PMP-1 | 48.0 | Ductile Iron | 130.0 | 15 | 0.00 | 0.000 |
| P-2 | 50 | PMP-1 | J-1 | 48.0 | Ductile Iron | 130.0 | 15 | 0.00 | 0.000 |
| EX P- 3 | 72 | J-1 | EX H-1 | 8.0 | Ductile Iron | 130.0 | 15 | 0.09 | 0.000 |
| EX P- 4 | 182 | EX H-1 | J-2 | 8.0 | Ductile Iron | 130.0 | 15 | 0.09 | 0.000 |
| P-5 | 262 | J-2 | H-1 | 8.0 | Ductile Iron | 130.0 | 1 | 0.01 | 0.000 |
| P-6 | 581 | J-2 | J-3 | 8.0 | Ductile Iron | 130.0 | 12 | 0.07 | 0.000 |
| P-7 | 55 | J-3 | H-2 | 8.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-10 | 560 | J-3 | H-3 | 8.0 | Ductile Iron | 130.0 | 8 | 0.05 | 0.000 |
| P-15 | 424 | H-2 | H-5 | 8.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-12 | 266 | H-3 | J-9 | 8.0 | Ductile Iron | 130.0 | 6 | 0.04 | 0.000 |
| P-13 | 275 | J-9 | H-4 | 8.0 | Ductile Iron | 130.0 | 6 | 0.04 | 0.000 |
| P-15 | 282 | J-9 | J-10 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-16 | 560 | J-10 | J-11 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-17 | 406 | J-11 | J-12 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-18 | 378 | J-10 | J-13 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-19 | 37 | J-13 | H-7 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-20 | 71 | H-8 | J-11 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |

Junction Table - Time: 0.00 hours

| ID | Label | Elevation (ft) | Demand (gpm) | Hydraulic Grade (ft) | Pressure (psi) |
|----|-------|-------------------|-----------------|----------------------------|-------------------|
| 33 | J-1 | 2,365.00 | 0 | 2,532.08 | 72 |
| 37 | J-2 | 2,365.85 | 1 | 2,532.08 | 72 |
| 41 | J-3 | 2,352.35 | 4 | 2,532.07 | 78 |
| 70 | J-9 | 2,335.76 | 0 | 2,532.07 | 85 |
| 73 | J-10 | 2,316.00 | 0 | 2,532.07 | 93 |
| 75 | J-11 | 2,325.00 | 0 | 2,532.07 | 90 |
| 77 | J-12 | 2,312.00 | 0 | 2,532.07 | 95 |
| 79 | J-13 | 2,313.00 | 0 | 2,532.07 | 95 |

Hydrant Table - Time: 0.00 hours

| ID | Label | Length (Hydrant Lateral) (ft) | Elevation (ft) | Demand (gpm) | Hydraulic Grade (ft) | Pressure (psi) |
|----|--------|--|-------------------|-----------------|----------------------------|-------------------|
| 35 | EX H-1 | 20 | 2,365.51 | 0 | 2,532.08 | 72 |
| 39 | H-1 | 20 | 2,366.54 | 1 | 2,532.08 | 72 |
| 43 | H-2 | 20 | 2,347.39 | 0 | 2,532.07 | 80 |
| 47 | H-3 | 20 | 2,342.69 | 2 | 2,532.07 | 82 |
| 53 | H-4 | 20 | 2,328.61 | 6 | 2,532.07 | 88 |
| 60 | H-5 | 20 | 2,352.89 | 0 | 2,532.07 | 78 |
| 81 | H-7 | 20 | 2,314.00 | 0 | 2,532.07 | 94 |
| 83 | H-8 | 20 | 2,324.00 | 0 | 2,532.07 | 90 |

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Reservoir Table - Time: 0.00 hours

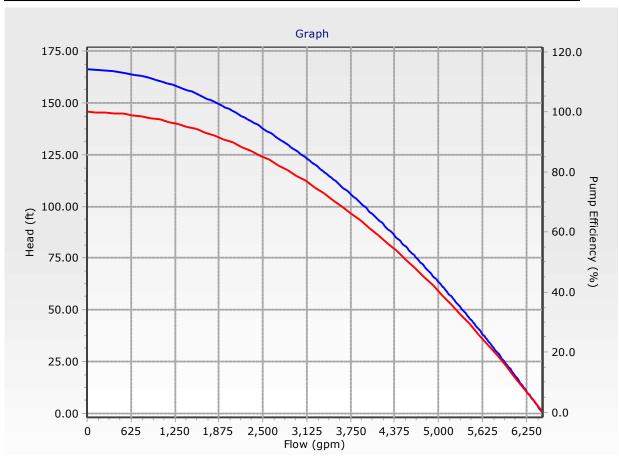
| ID | Label | Elevation (ft) | Zone | Flow (Out net) (gpm) | Hydraulic Grade (ft) |
|----|-------|-------------------|---------------|-------------------------|----------------------------|
| 30 | R-1 | 2,366.00 | <none></none> | 15 | 2,366.00 |

Pump Table - Time: 0.00 hours

| ID | Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade (Suction) (ft) | Hydraulic Grade (Discharge) (ft) | Flow (Total) (gpm) |
|-------------------|-------|-------------------|--------------------|------------------|---|---|-----------------------|
| 31 | PMP-1 | 2,366.00 | Flow Test | On | 2,366.00 | 2,532.08 | 15 |
| Pump Head (ft) | | | | | | | |
| 166.08 | | | | | | | |

Pump Definition Detailed Report: Flow Test

| Element Details | | | |
|--------------------------|-----------------------------|--------------------------|-------------------|
| ID | 62 | Notes | |
| Label | Flow Test | | |
| Pump Definition Type | | | |
| Pump Definition Type | Standard (3 Point) | Design Head | 152.24 ft |
| Shutoff Flow | 0 gpm | Maximum Operating Flow | 5,441 gpm |
| Shutoff Head | 166.08 ft | Maximum Operating Head | 46.13 ft |
| Design Flow | 1,695 gpm | | |
| Pump Efficiency Type | | | |
| Pump Efficiency Type | Best Efficiency Point | Motor Efficiency | 100.0 % |
| BEP Efficiency | 100.0 % | Is Variable Speed Drive? | False |
| BEP Flow | 0 gpm | · | |
| Transient (Physical) | | · | |
| Inertia (Pump and Motor) | 0.000 lb·ft² | Specific Speed | SI=25, US=1280 |
| Speed (Full) | 0 rpm | Reverse Spin Allowed? | True |



APPENDIX C: Peak Hour Demand Results

Pipe Table

Junction Table

Hydrant Table

Reservoir Table

Pump Table

Pipe Table - Time: 0.00 hours

| Label | Length (Scaled) (ft) | Start Node | Stop Node | Diameter (in) | Material | Hazen-Williams C | Flow (gpm) | Velocity (ft/s) | Headloss Gradient (ft/ft) |
|------------|----------------------------|---------------|--------------|------------------|--------------|---------------------|---------------|--------------------|---------------------------------|
| P-1 | 39 | R-1 | PMP-1 | 48.0 | Ductile Iron | 130.0 | 51 | 0.01 | 0.000 |
| P-2 | 50 | PMP-1 | J-1 | 48.0 | Ductile Iron | 130.0 | 51 | 0.01 | 0.000 |
| EX P- 3 | 72 | J-1 | EX H-1 | 8.0 | Ductile Iron | 130.0 | 51 | 0.32 | 0.000 |
| EX P- 4 | 182 | EX H-1 | J-2 | 8.0 | Ductile Iron | 130.0 | 51 | 0.32 | 0.000 |
| P-5 | 262 | J-2 | H-1 | 8.0 | Ductile Iron | 130.0 | 5 | 0.03 | 0.000 |
| P-6 | 581 | J-2 | J-3 | 8.0 | Ductile Iron | 130.0 | 41 | 0.26 | 0.000 |
| P-7 | 55 | J-3 | H-2 | 8.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-10 | 560 | J-3 | H-3 | 8.0 | Ductile Iron | 130.0 | 27 | 0.17 | 0.000 |
| P-15 | 424 | H-2 | H-5 | 8.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-12 | 266 | H-3 | J-9 | 8.0 | Ductile Iron | 130.0 | 19 | 0.12 | 0.000 |
| P-13 | 275 | J-9 | H-4 | 8.0 | Ductile Iron | 130.0 | 19 | 0.12 | 0.000 |
| P-15 | 282 | J-9 | J-10 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-16 | 560 | J-10 | J-11 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-17 | 406 | J-11 | J-12 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-18 | 378 | J-10 | J-13 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-19 | 37 | J-13 | H-7 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |
| P-20 | 71 | H-8 | J-11 | 6.0 | Ductile Iron | 130.0 | 0 | 0.00 | 0.000 |

Junction Table - Time: 0.00 hours

| ID Label | | Elevation (ft) | Demand (gpm) | Hydraulic Grade (ft) | Pressure (psi) |
|----------|------|-------------------|-----------------|----------------------------|-------------------|
| 33 | J-1 | 2,365.00 | 0 | 2,532.06 | 72 |
| 37 | J-2 | 2,365.85 | 5 | 2,532.04 | 72 |
| 41 | J-3 | 2,352.35 | 14 | 2,532.01 | 78 |
| 70 | J-9 | 2,335.76 | 0 | 2,532.00 | 85 |
| 73 | J-10 | 2,316.00 | 0 | 2,532.00 | 93 |
| 75 | J-11 | 2,325.00 | 0 | 2,532.00 | 90 |
| 77 | J-12 | 2,312.00 | 0 | 2,532.00 | 95 |
| 79 | J-13 | 2,313.00 | 0 | 2,532.00 | 95 |

Hydrant Table - Time: 0.00 hours

| ID | Label | Length (Hydrant Lateral) (ft) | Elevation (ft) | Demand (gpm) | Hydraulic Grade (ft) | Pressure (psi) |
|----|--------|--|-------------------|-----------------|----------------------------|-------------------|
| 35 | EX H-1 | 20 | 2,365.51 | 0 | 2,532.05 | 72 |
| 39 | H-1 | 20 | 2,366.54 | 5 | 2,532.04 | 72 |
| 43 | H-2 | 20 | 2,347.39 | 0 | 2,532.01 | 80 |
| 47 | H-3 | 20 | 2,342.69 | 7 | 2,532.00 | 82 |
| 53 | H-4 | 20 | 2,328.61 | 19 | 2,531.99 | 88 |
| 60 | H-5 | 20 | 2,352.89 | 0 | 2,532.01 | 77 |
| 81 | H-7 | 20 | 2,314.00 | 0 | 2,532.00 | 94 |
| 83 | H-8 | 20 | 2,324.00 | 0 | 2,532.00 | 90 |

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Reservoir Table - Time: 0.00 hours

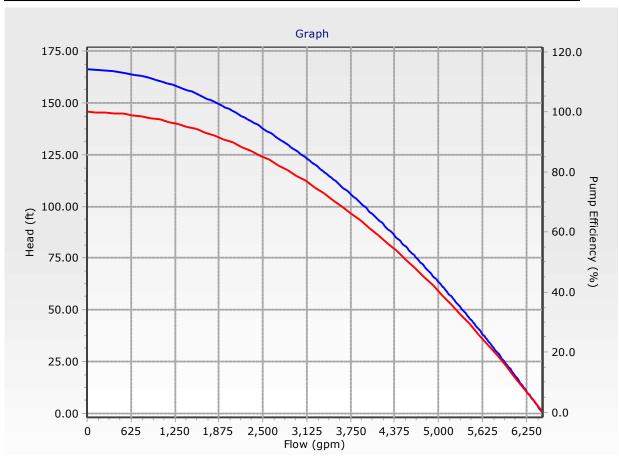
| ID | Label | Elevation (ft) | Zone | Flow (Out net) (gpm) | Hydraulic Grade (ft) |
|----|-------|-------------------|---------------|-------------------------|----------------------------|
| 30 | R-1 | 2,366.00 | <none></none> | 51 | 2,366.00 |

Pump Table - Time: 0.00 hours

| ID | Label | Elevation (ft) | Pump Definition | Status (Initial) | Hydraulic Grade (Suction) (ft) | Hydraulic Grade (Discharge) (ft) | Flow (Total) (gpm) |
|-------------------|-------|-------------------|--------------------|------------------|---|---|-----------------------|
| 31 | PMP-1 | 2,366.00 | Flow Test | On | 2,366.00 | 2,532.06 | 51 |
| Pump Head (ft) | | | | | | | |
| 166.06 | | | | | | | |

Pump Definition Detailed Report: Flow Test

| Element Details | | | |
|--------------------------|-----------------------------|--------------------------|-------------------|
| ID | 62 | Notes | |
| Label | Flow Test | | |
| Pump Definition Type | | | |
| Pump Definition Type | Standard (3 Point) | Design Head | 152.24 ft |
| Shutoff Flow | 0 gpm | Maximum Operating Flow | 5,441 gpm |
| Shutoff Head | 166.08 ft | Maximum Operating Head | 46.13 ft |
| Design Flow | 1,695 gpm | | |
| Pump Efficiency Type | | | |
| Pump Efficiency Type | Best Efficiency Point | Motor Efficiency | 100.0 % |
| BEP Efficiency | 100.0 % | Is Variable Speed Drive? | False |
| BEP Flow | 0 gpm | · | |
| Transient (Physical) | | · | |
| Inertia (Pump and Motor) | 0.000 lb·ft² | Specific Speed | SI=25, US=1280 |
| Speed (Full) | 0 rpm | Reverse Spin Allowed? | True |



| APPENDIX D: Maximum Day Demand + Fire Flow Results | |
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| Fire Flow Table | |
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Fire Flow Node FlexTable: Fire Flow Report

| Label | Elevation (ft) | Fire Flow (Needed) (gpm) | Pressure (Residual Lower Limit) (psi) | Pressure Head (ft) | Pressure (psi) |
|--------|-------------------|--------------------------------|--|-----------------------|-------------------|
| EX H-1 | 2,365.51 | 1,000 | 0 | 166.57 | 72 |
| H-1 | 2,366.54 | 1,000 | 0 | 165.54 | 72 |
| H-2 | 2,347.39 | 1,000 | 0 | 184.68 | 80 |
| H-3 | 2,342.69 | 1,000 | 0 | 189.38 | 82 |
| H-4 | 2,328.61 | 1,000 | 0 | 203.46 | 88 |
| H-5 | 2,352.89 | 1,000 | 0 | 179.18 | 78 |
| H-7 | 2,314.00 | 1,000 | 0 | 218.07 | 94 |
| H-8 | 2,324.00 | 1,000 | 0 | 208.07 | 90 |
| J-1 | 2,365.00 | 1,000 | 0 | 167.08 | 72 |
| J-2 | 2,365.85 | 1,000 | 0 | 166.23 | 72 |
| J-3 | 2,352.35 | 1,000 | 0 | 179.72 | 78 |
| J-9 | 2,335.76 | 1,000 | 0 | 196.31 | 85 |
| J-10 | 2,316.00 | 1,000 | 0 | 216.07 | 93 |
| J-11 | 2,325.00 | 1,000 | 0 | 207.07 | 90 |
| J-12 | 2,312.00 | 1,000 | 0 | 220.07 | 95 |
| J-13 | 2,313.00 | 1,000 | 0 | 219.07 | 95 |

Alternative Summary Report Alternative: Base Fire Flow

| Base Fire Flow | | | |
|--|---------------------------------|-------------------------------------|-----------------------------|
| Fire Flow (Needed) | 1,000 gpm | Fire Flow Auxiliary Results Type | None |
| Fire Flow (Upper Limit) | 3,500 gpm | Velocity (Upper Limit) | 10.00 ft/s |
| Pressure (Residual Lower Limit) | 0 psi | Pressure (System Lower Limit) | 30 psi |
| Pressure (Zone Lower Limit) | 0 psi | Pipe Velocity Greater Than | 0.00 ft/s |
| Use Minimum System Pressure Constraint? | True | Node Pressure Less Than | 0 psi |
| Use Velocity Constraint? | True | Pipe Set | All Pipes |
| Use Pipe Velocity Greater Than? | False | Fire Flow Nodes | All Fire Flow Nodes |
| Use Node Pressure Less Than? | False | Fire Flow Auxiliary Results Type | None |
| Apply Fire Flows By | Adding to Baseline Demand | Auxiliary Output Selection Set | <no Elements></no |

13: Base Fire Flow, Junction and Hydrant Alternative Report

| * | ID | Label | Specify Local Fire Fl Constraints? | ow Fire Flow (Needed) (gpm) | Fire Flow (Upper Limit) (gpm) |
|------------|----|-------------------|---------------------------------------|-----------------------------|-------------------------------|
| True | 35 | EX H-1 | False | 1,000 | 3,500 |
| True | 39 | H-1 | False | 1,000 | 3,500 |
| True | 43 | H-2 | False | 1,000 | 3,500 |
| True | 47 | H-3 | False | 1,000 | 3,500 |
| True | 53 | H-4 | False | 1,000 | 3,500 |
| True | 60 | H-5 | False | 1,000 | 3,500 |
| True | 81 | H-7 | False | 1,000 | 3,500 |
| True | 83 | H-8 | False | 1,000 | 3,500 |
| True | 33 | J-1 | False | 1,000 | 3,500 |
| True | 37 | J-2 | False | 1,000 | 3,500 |
| True | 41 | J-3 | False | 1,000 | 3,500 |
| True | 70 | J-9 | False | 1,000 | 3,500 |
| True | 73 | J-10 | False | 1,000 | 3,500 |
| True | 75 | J-11 | False | 1,000 | 3,500 |
| True | 77 | J-12 | False | 1,000 | 3,500 |
| True | 79 | J-13 | False | 1,000 | 3,500 |
| Pressure (| _ | ssure (7one Lower | Pressure (System | Velocity (Unner Limit) |] 3,3 |

| Pressure (Residual Lower Limit) (psi) | Pressure (Zone Lower Limit) (psi) | Pressure (System Lower Limit) (psi) | Velocity (Upper Limit) (ft/s) |
|---|---|---|----------------------------------|
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |

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Alternative Summary Report Alternative: Base Fire Flow

13: Base Fire Flow, Junction and Hydrant Alternative Report

| Pressure (Residual Lower Limit) (psi) | Pressure (Zone Lower Limit) (psi) | Pressure (System Lower Limit) (psi) | Velocity (Upper Limit) (ft/s) |
|---|---|---|----------------------------------|
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |
| 0 | 0 | 30 | 10.00 |

| APPENDIX E: Fire Hydrant Flow Test Results |
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Flow Test Summary

Project Name: **EJFT 19101**

Project Address: 24770 N Alma School Rd, Scottsdale, AZ 85255

Date of Flow Test: 2019-05-08 Time of Flow Test: 7:36 AM Data Reliable Until: 2019-11-08

Conducted By: Cesar Reyna & Austin Gourley (EJ Flow Tests) 602.999.7637

Sonny Schreiner (City of Scottsdale) 602.819.7718 Witnessed By:

City Forces Contacted: City of Scottsdale (602.819.7718)

Permit Number: C58208

Scottsdale requires a max static pressure of 72 psi for safety factor Note

Raw Flow Test Data

Static Pressure: 116.0 PSI Residual Pressure: 110.0 PSI Flowing GPM: 1,695 GPM @ 20 PSI: 7,576

Data with a 44 PSI Safety Factor

Static Pressure: 72.0 PSI Residual Pressure: 66.0 PSI Flowing GPM: 1,695 GPM @ 20 PSI: 5,441

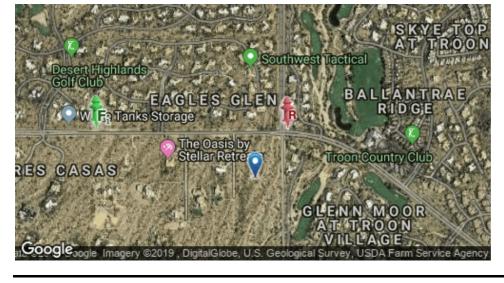
Hydrant F₁

Pitot Pressure (1): **PSI**

Coefficient of Discharge (1): 0.9

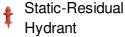
Hydrant Orifice Diameter (1): 2.5 inches Pitot Pressure (2): Coefficient of Discharge (2): 0.9

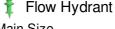
Hydrant Orifice Diameter (2): 2.5 inches





Project Site





Main Size 8 inches

Distance Between F₁ and R 2619 ft (measured linearly)

Static-Residual Elevation 2375 ft (above sea level)

Flow Hydrant (F₁) Elevation 2316 ft (above sea level)

Elevation & distance values are approximate



Flow Test Summary

Static-Residual Hydrant



Flow Hydrant (only hydrant F1 shown for clarity)



Approximate Project Site



Water Supply Curve N^{1.85} Graph

